

# Fatigue crack initiation and fatigue life testing of high-strength austenitic stainless steel tubing with internal hydrogen (PVP2023-106413)

Chris San Marchi  
Joe Ronevich

Sandia National Laboratories (Livermore CA)

Johan Pohl  
Severin Ramseyer  
Davide Cortinovis

Endress + Hauser Flow AG (Reinach Switzerland)

Stefan Eckmann

Fraunhofer Institute for Mechanics and Materials IWM (Freiburg, Germany)

**ASME PVP2023 Conference**  
**Atlanta GA, 16-21 July 2023**



# Hydrogen technologies include diverse range of operations



## Hydrogen delivery

- hydrogen pipelines: carbon steels
- Challenge: cyclic pressure

## Hydrogen storage

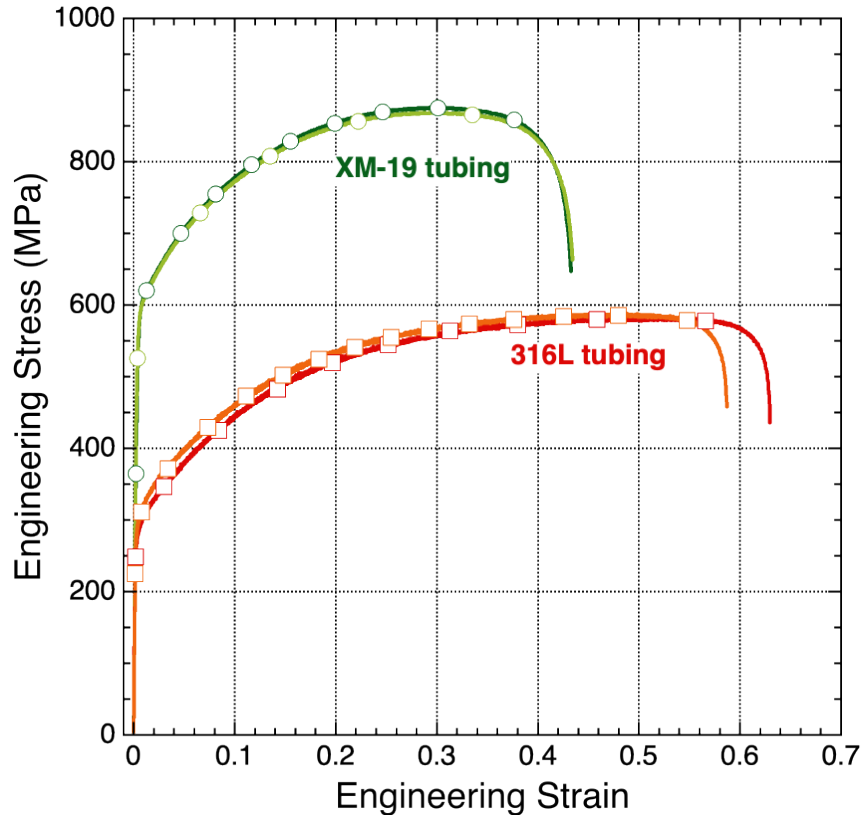
- hydrogen forklifts: Cr-Mo ferritic steels
- Challenge: filling ~6/day



## Pressure manifold components

- Valves, tubing, and other devices: austenitic stainless steels
- Challenges: low temperature, lower-cost alternatives (e.g., aluminum or higher strength), alloy content, welding

# High-strength austenitic stainless steel tubing: XM-19



## XM-19 / Nitronic 50 / 22 Cr – 13 Ni – 5 Mn

Fe	Cr	Ni	Mn	Mo	C	N
Bal	22.0	13.1	5.3	2.1	0.015	0.32

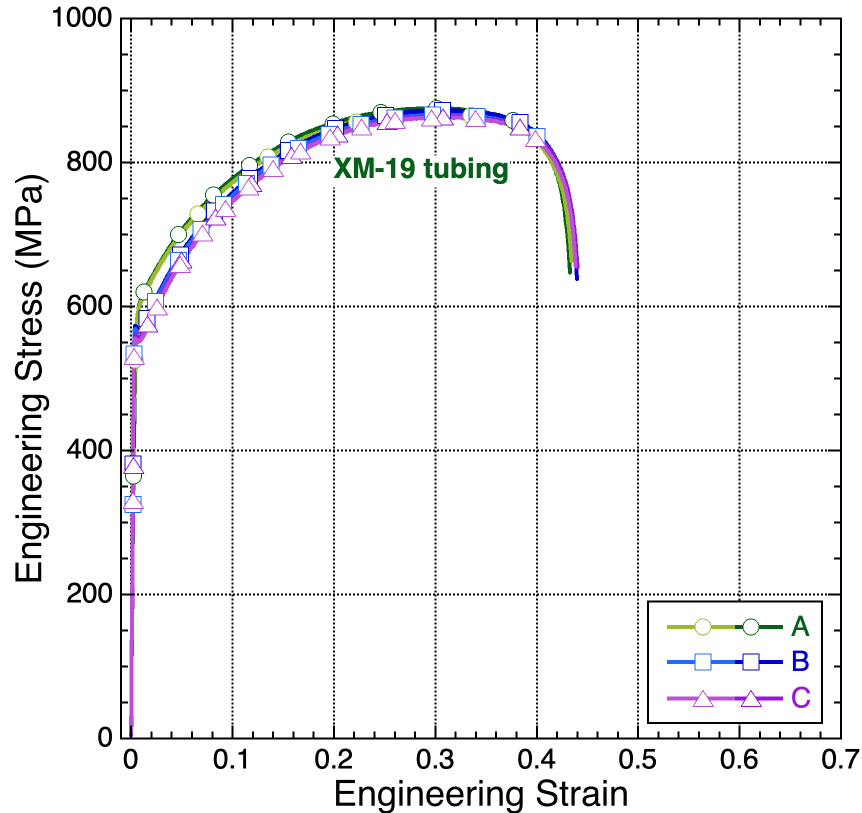
### XM-19 tubing

- 6 mm OD
- 3.6 mm ID
- Yield strength: 566 MPa
- Elongation to failure: >40%

**Annealed XM-19 tubing displays yield strength almost 2X of annealed 316L tubing**



# XM-19 tubing has a stable microstructure



Consider the potential effects of processing-driven thermal cycles on XM-19 tubing

1. **Condition A** – as received (solution-annealed condition)
2. **Condition B** – 1050°C exposure
3. **Condition C** – condition B + second 1050°C exposure

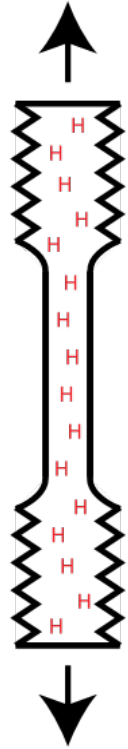
Thermal exposure (1050°C) does not significantly change the strength of the XM-19 tubing:  
**<1% change of yield strength**

# Thermal hydrogen-precharging is an effective way to simulate hydrogen-assisted fracture

- **Thermal H-precharging**

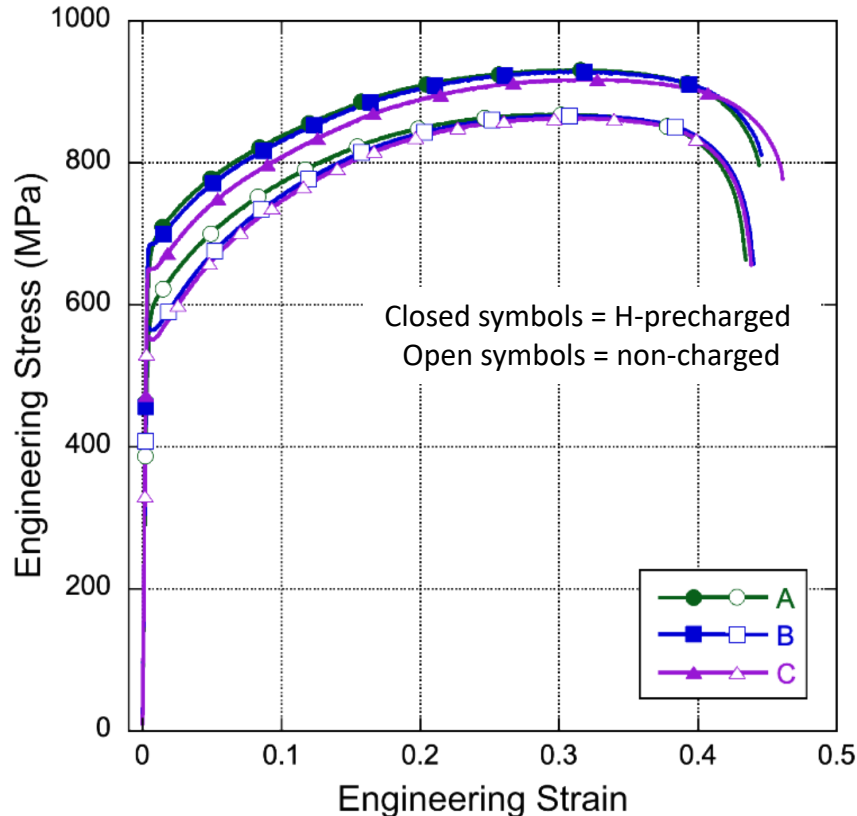
- **Exposure to gaseous  $H_2$  until saturated with H**
  - **Time = ~10 days**
  - **Pressure = 1,380 bar (20,000 psi)**
  - **Temperature = 300°C**
- **Hydrogen content ~ 210 to 220 wt ppm**
  - **Note:** concentration is alloy dependent  
(304/316 = ~140 wt ppm for same conditions)

- **Testing is conducted in air after H-precharging**



See PVP2023-106086 for more details and comparison between testing with internal H and testing in external  $H_2$  (in situ)

# Internal hydrogen provides strengthening (10-20%)



## Internal H has modest effect on tensile properties

- **H concentration:** 210-220 wt ppm
- **Yield strength:** ~20% increase
- **Tensile strength:** ~10% increase
- **Elongation:** effectively unchanged

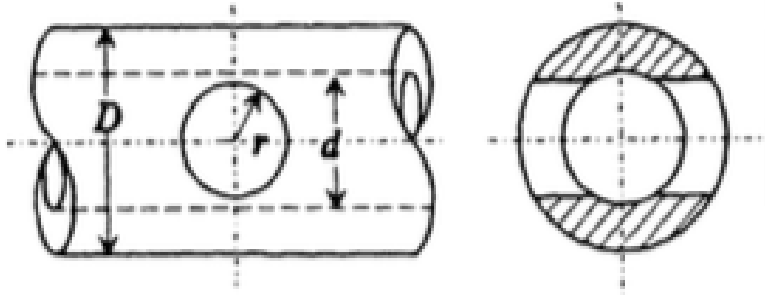
**Internal H does not degrade tensile properties for the conditions considered in this study**

Previous work on forged XM-19 shows some degradation of properties:

- *J Pressure Vessel Technol* **130** (2008) 041401
- *Metall Mater Trans* **41A** (2010) 3348

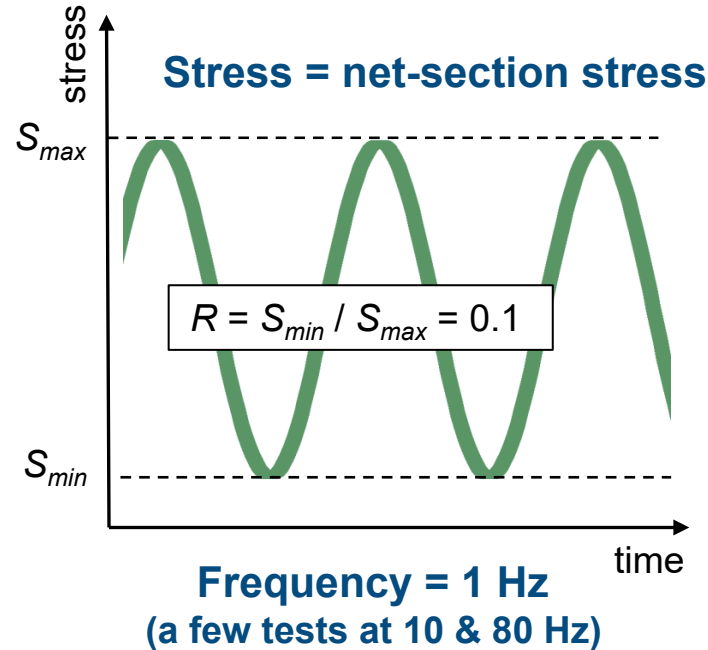
# Stress concentration is used to facilitate fatigue life testing

## Transverse circular hole in tube

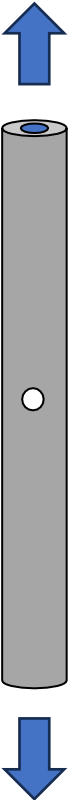


### XM-19 tubing

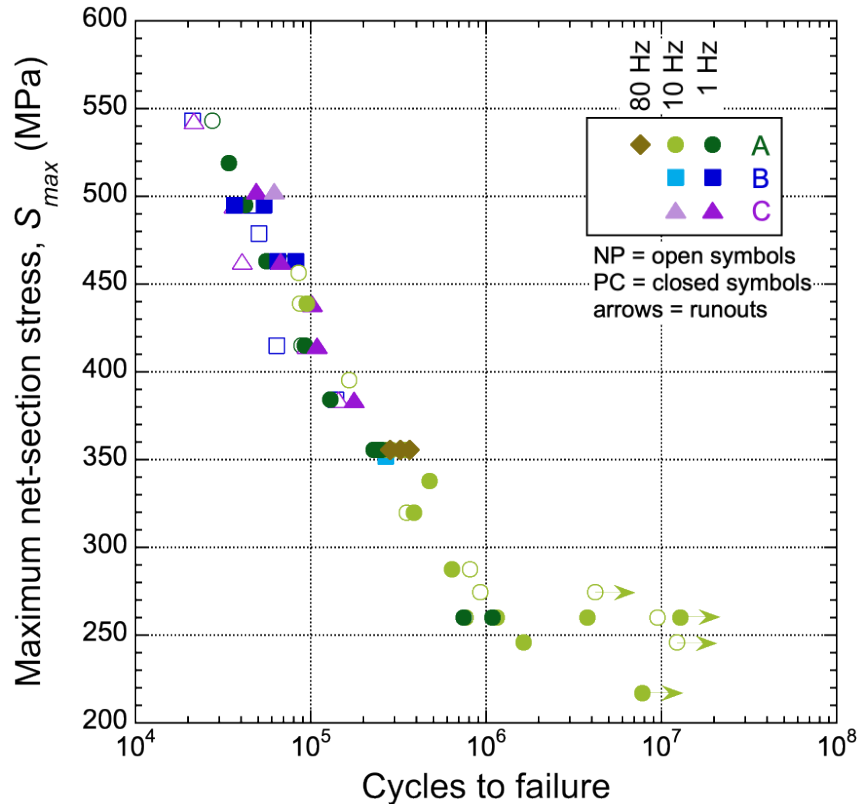
- 6 mm OD
- 3.6 mm ID
- 1.7 mm hole diameter
- $K_t = 4$   
(relative to net section)



Test configuration is intended to be analogous to fatigue testing of circumferentially notched round bar



# Fatigue life of XM-19 tubing shows consistent trends



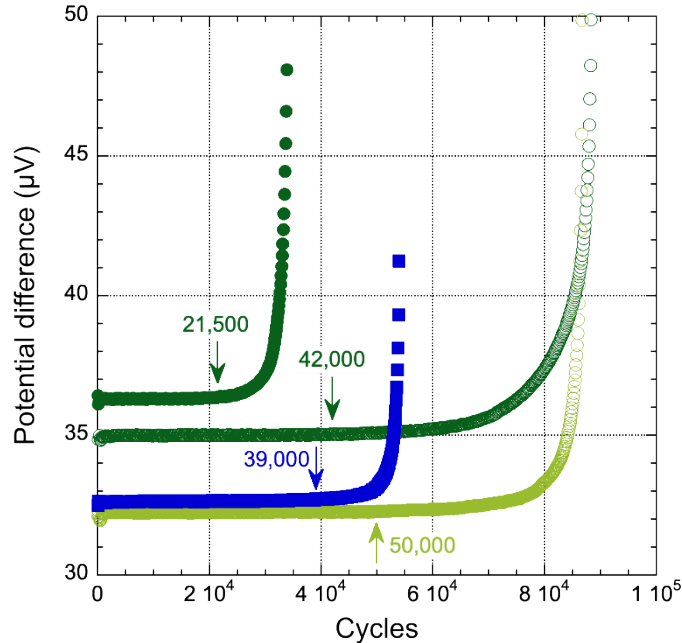
- Cycles to failure of XM-19 tubing is essentially unchanged by the incorporation of internal H
  - Can be represented by simple power law

$$N_f = 1.29 \times 10^{18} (S_{max})^{-5}$$

- Although data is limited, higher frequency did not change fatigue life with or without internal H
  - Higher frequency (up to 80 Hz) may aid acceleration of future testing
  - It remains unclear if frequency will be effective for materials that are more susceptible to hydrogen-assisted fatigue



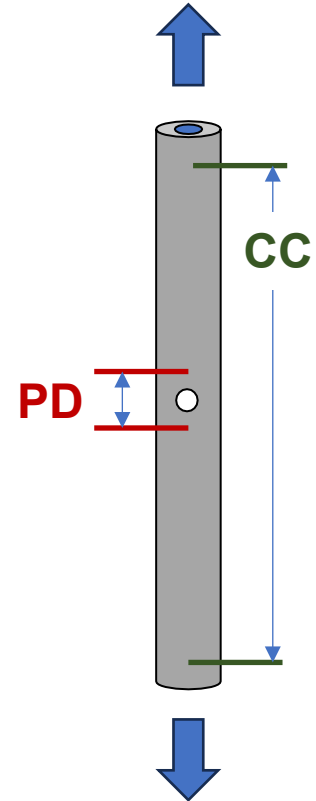
# Crack initiation is monitored by DCPD



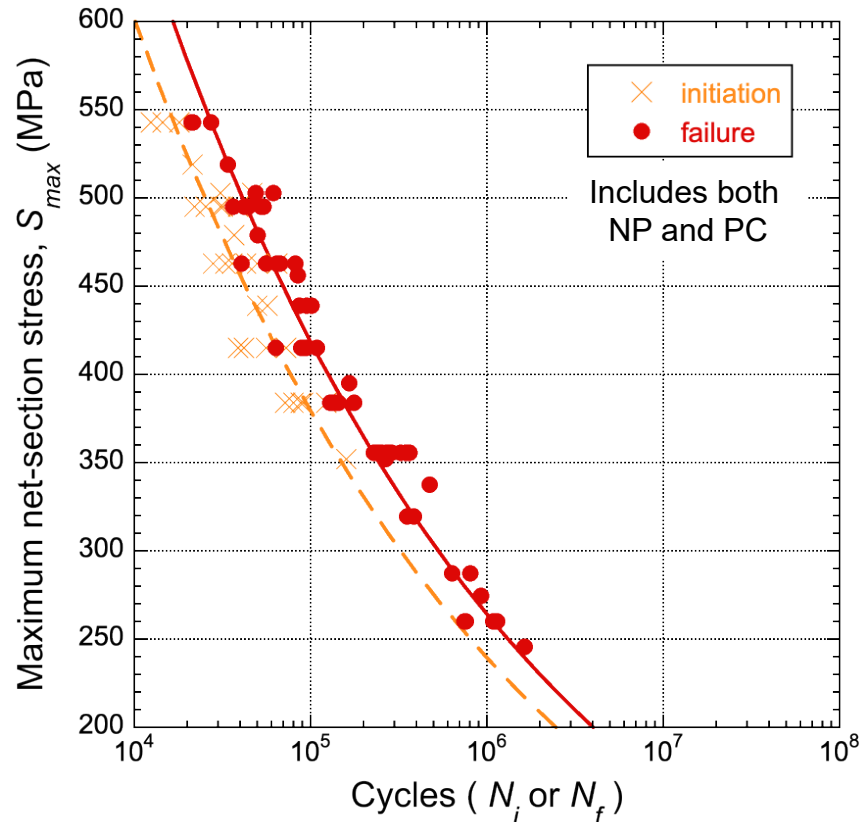
**Crack initiation determined at inflection in PD-N curve**

## Direct current potential difference (DCPD) method

- **Constant current (CC) applied near ends**
  - Wire leads welded to cotter pins
  - Typically 1 A
- **Potential difference (PD) monitored near stress concentration**
  - Wire leads spot welded either side of hole but 180° apart
  - Measured in μV range



# Crack initiation nominally follows stress response of failure



- Crack initiation both with and without internal H can be represented by a simple power law

$$N_i = 7.91 \times 10^{17} (S_{max})^{-5}$$

- No obvious effective of frequency (although limited data)
- Since the power-law exponent is the same for initiation and failure, cycles to crack initiation can be idealized as a constant fraction of cycles to failure:

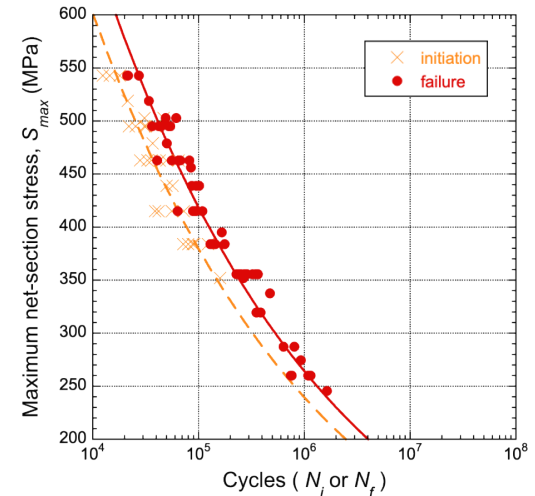
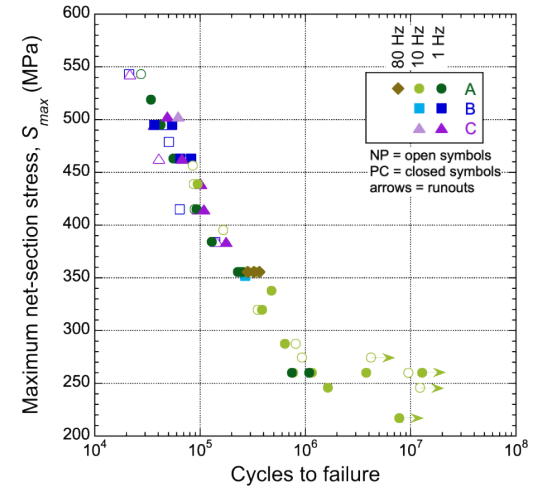
$$N_i = 0.613 N_f$$

# Summary

- The transverse circular hole geometry and hydrogen precharging enabled evaluation of hydrogen effects on fatigue life of XM-19 tubing
  - Tension-tension, notched fatigue
- Crack initiation was also evaluated by instrumenting specimens for DCPD measurements

## Results:

- Internal H had virtually no effect on fatigue life for tested conditions
- Cracks initiated at transverse hole at a constant fraction of cycles to failure



# Thank You!

**Chris San Marchi**  
**cwsanma@sandia.gov**

**Joe Ronevich**  
**jaronev@sandia.gov**

<https://h-mat.org/>

<https://www.sandia.gov/matlsTechRef/>

<https://granta-mi.sandia.gov/>

Special thanks to Sandia's  
Hydrogen Effects on Materials  
Laboratory (HEML) team:

- Brendan Davis
- James McNair
- Keri McArthur
- Tanner McDonnell
- Robert Wheeler
- Milan Agnani
- Fernando Leon