

CONF-960794--1

UCRL-JC-123851
PREPRINT

Errors in Using Two Dimensional Methods to Measure Motion About an Offset Revolute

K. Hollerbach
Lawrence Livermore National Laboratory
and
A. Hollister, LSU Medical Center
Shreveport, LA

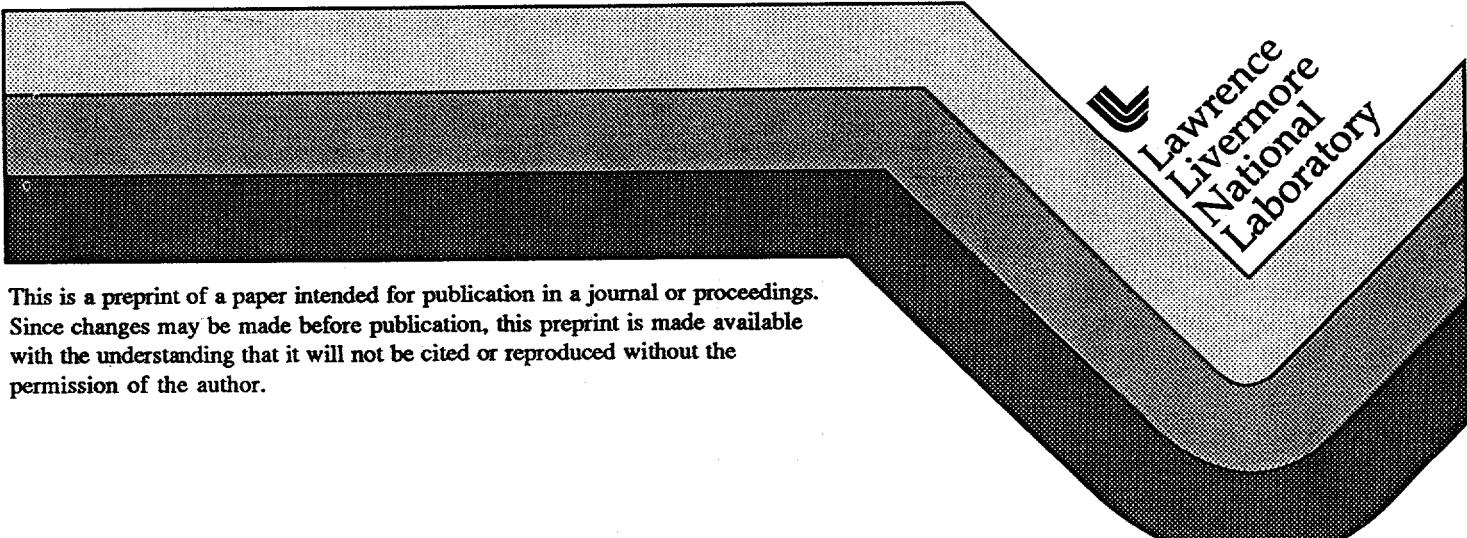
RECEIVED

MAY 06 1996

OSTI

This paper was prepared for submittal to the
4th International Symposium of 3D Analysis of Human
Movement, Grenoble, France
July 1-2, 1996

March 1996



This is a preprint of a paper intended for publication in a journal or proceedings. Since changes may be made before publication, this preprint is made available with the understanding that it will not be cited or reproduced without the permission of the author.

DISCLAIMER

This document was prepared as an account of work sponsored by an agency of the United States Government. Neither the United States Government nor the University of California nor any of their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial products, process, or service by trade name, trademark, manufacturer, or otherwise, does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or the University of California. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States Government or the University of California, and shall not be used for advertising or product endorsement purposes.

ERRORS IN USING TWO DIMENSIONAL METHODS TO MEASURE MOTION ABOUT AN OFFSET REVOLUTE

K. Hollerbach

Institute for Scientific Computing Research,
Lawrence Livermore National Laboratory, Livermore, CA

A. Hollister

LSU Medical Center, Shreveport, LA

INTRODUCTION

Two dimensional measurement of human joint motion involves the analysis of three dimensional displacements in an observer selected measurement plane. Accurate marker placement and alignment of joint motion plane with the observer plane are difficult. Nonetheless, alignment of the two planes is essential if one is to accurately record and understand the joint mechanism as well as the movement about it.

In nature, joint axes can exist at any orientation and location relative to an arbitrarily chosen global reference frame. An arbitrary axis is any axis that is not coincident with a reference coordinate. We calculate the errors that result from measuring joint motion about an arbitrary axis using two dimensional methods.

REVIEW AND THEORY

Kinematic and anatomic analyses of a number of human joints have suggested that they move about fixed revolutes that are not parallel to the anatomic reference planes (Hollister, et al. 1991, Hollister, et al. 1993, Inman 1976, London 1981). Analysis of kinematic data has traditionally been done using planar analysis

(Reuleaux 1876) in an anatomic reference planes (Frankel et al. 1976, Sudan and Auderkerke 1979). This method of describing motion is subject to error (Panjabi et al. 1982, Sudan and Auderkerke 1979) and intra-observer variability. Furthermore, these methods for describing motion do not relate directly to the kinematic mechanism of the joint itself.

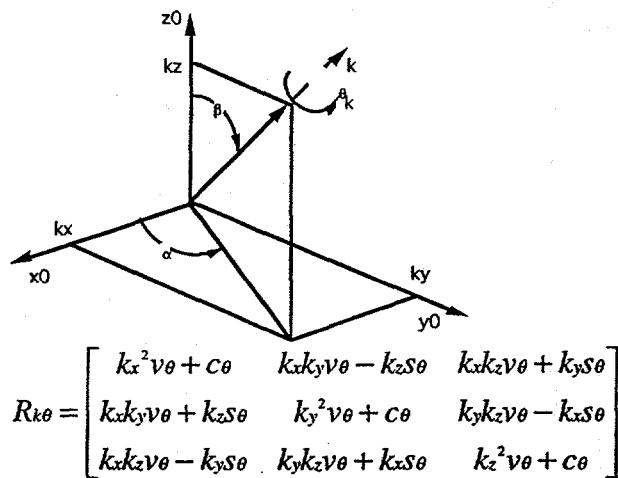
PROCEDURES AND RESULTS

Rotations of a body moving about an arbitrary axis in a reference frame are determined by the axis' α and β angles of offset from the reference frame and the θ_k angle of rotation about the arbitrary axis, k (Fig. 1).

Displacements of a body moving about an arbitrary axis in a reference frame are determined by the axis' α and β angles, the θ_k angle of rotation, r , the distance of the body from the axis of rotation, and d , the distance from the axis to the reference frame (Fig. 2).

When the arbitrary axis, k , is coincident with the reference z-axis ($d, \alpha, \beta = 0$) and with $r = 1$, the x and y positions of the point trace out cosine and sine waves, respectively, and the z position

remains at zero for varying θ_k . For perfect alignment, but with $r \neq 1$, the amplitude of the cosine and sine curves is scaled accordingly. When the arbitrary axis is parallel to the reference z-axis, but is translated by non-zero x_k , y_k , and/or z_k , the corresponding measured x, y, and z trajectories are shifted by x_k , y_k , and z_k , respectively (Fig. 3).



where $v_\theta = 1 - c_\theta$

Figure 1: Rotation about an arbitrary axis.

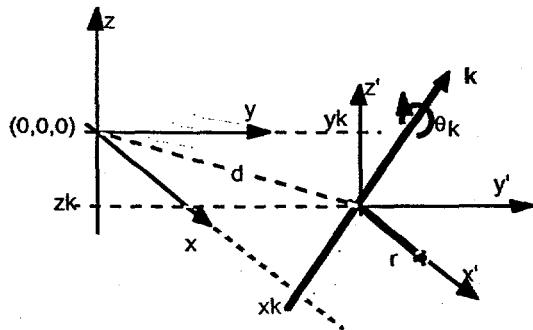


Figure 2: Rotation, θ_k , about an arbitrary axis, k , with translation (by amounts x_k , y_k , z_k) from the reference frame, x , y , z . The distance of the arbitrary axis is given by: $d = (x_k^2 + y_k^2 + z_k^2)^{1/2}$. The point moved about the arbitrary frame is a distance, r , from the arbitrary axis.

With the arbitrary axis offset from the reference frame's axes, but still passing through the origin

($d = 0$), the xyz trajectories vary significantly with the offset angles, α and β (Fig. 4). The trajectories can be made to vary qualitatively as well as quantitatively depending on the choice of α and β . The resulting planar projections used in 2D motion analysis methods can, therefore, also varied at will, with means to recover the complete trajectory unless the offset angles relating the plane of motion to the observer plane are known.

A 2 dimensional method would analyze only 2 of the 3 displacement dimensions. If the plane analyzed is not the motion plane the total displacement will not be measured. Furthermore, displacements in the third dimension will move the segments closer to or farther from the observer and will introduce perspective error in the planar analysis. Both of these factors introduce significant errors for instant center analysis or other 2D methods if the motion plane is not the plane analyzed.

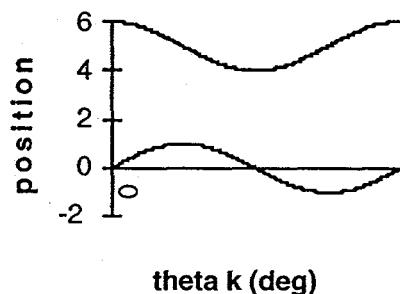


Figure 3: xyz positions with a shift of $x_k = 5$, for θ_k varying from zero to 90 deg. The z trajectory is zero; the y trajectory traces out the cosine function; the x trajectory traces out an offset sine, centered about $x_k = 5$.

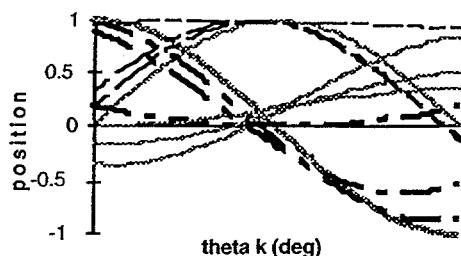


Figure 4: xyz positions for axes of rotation with varying offset angles, α and β ($d=0$, $r=1$): shown are x trajectories (thick lines; $\alpha, \beta = 0$, solid; $\alpha, \beta = 10$ and 20 deg, dashed; $\alpha=80$ deg, $\beta = 0$, dashed), y trajectories (thin dashed), and z trajectories (thin, solid).

One method that is commonly used in kinematic analysis is that of Euler angles. This method, though not inherently 2D, is also affected by varying α and β offsets. With zero offsets, the Euler angles correspond with the θ_k rotations (with variation in only one of the Euler angles). The resulting displacements then occur only in the plane that is perpendicular to the axis corresponding to the non-zero Euler angle, and 2D analysis of the displacements in that plane is appropriate. With rotation about a single arbitrary axis with 10 deg offset, this relationship breaks down: α and β offset angles produce rotations about all three Euler coordinates, and the relationships are nonlinear (Fig. 5). Furthermore, the plane of motion, although the displacements still occur in 2D, cannot be simply determined from the Euler angle analysis.

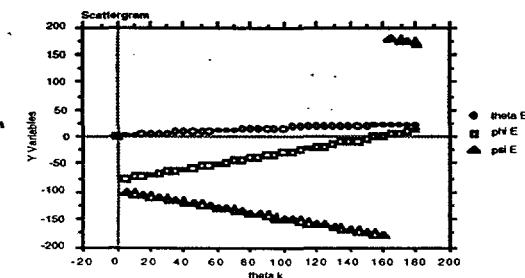


Figure 5: Euler angle rotations calculated from rotations about an arbitrary axis with α and $\beta = 10$ deg.

Different results are obtained for different α and β offsets. If the motion plane is not the plane studied, the rotations will not be perpendicular to the analyzed plane and will not be directly related to the recorded displacements.

DISCUSSION

Slight offsets of the measurement plane from the axis of rotation produce significant errors in recording displacements and rotations for motion about the joint axis with 2D methods. We conclude that, if 2D methods are used, the relationship of the reference frame to the axis of rotation must be known in order to perform accurate kinematic measurements.

REFERENCES

- [1] Frankel VH, and Burstein AH, and Brooks DB: Biomechanics of Internal Derangement of the Knee. *J. Bone and Joint Surg.* **53-A**: 945-962, 1971.
- [2] Hollister A, et al. The Axes of Rotation of the Thumb Carpometacarpal Joint, *JOR*, **10**:445-460, 1991.
- [3] Hollister AM, et al. The axes of rotation of the knee, *Clin Orthop*, **290**:259-268, 1993.
- [4] Inman VT: The Joints of the Ankle. pp. 45-112, Williams & Wilkins, 1976.
- [5] London JT: Kinematics of the Elbow. *J Bone Joint Surg*, **63-A**, 529-35, 1981.
- [6] Panjabi MM, Goel VK, and Walter SD: Errors in Kinematic Parameters of a Planar Joint: Guidelines for Optimal Experimental Design. *J. Biomechanics*. **15**:537-44, 1982.
- [7] Reuleaux F: Theoretische Kinematik: Grundzüge einer Theorie des Maschinenwesens, F. Kievel und Sohn, Braunschweig. 1876. (Translated by A. B. W. Kennedy: The Kinematics of Machinery: Outline of a Theory of Machines.) London, Macmillan, 1960
- [8] Soudan K and Auderkerke RV: Methods, Difficulties and Inaccuracies in the Study of Human Joint Mechanics and Pathokinematics by the Instant Axis Concept, Example: The Knee Joint. *J. Biomechanics*. **12**: 27-33, 1979.

*This work was performed under the auspices of the U.S. Department of Energy by Lawrence Livermore National Laboratory under contract No. W-7405-Eng-48.

DISCLAIMER

**Portions of this document may be illegible
in electronic image products. Images are
produced from the best available original
document.**