

1 **Kinetic Study of Polyvinyl chloride (PVC) Pyrolysis with Characterization of Dehydrochlorinated**  
2 **PVC**

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10 **Abstract**

11 In this paper we study the kinetics of polyvinyl chloride (PVC) decomposition using a combination of  
12 experimental and computational approaches. We develop a simplified kinetic model that contains only two  
13 steps: dehydrochlorination of PVC and further decomposition of PVC residue. The model is consistent with  
14 density function theory (DFT) calculations and experimental data. Dehydrochlorination is an autocatalytic  
15 reaction that starts with a tertiary chloride (Cl) and generates hydrogen chloride (HCl) and benzene as the  
16 main products. Benzene and HCl formation rates showed similar trends indicating that HCl likely catalyzes  
17 a homolytic carbon-carbon (C–C) bond cleavage, which gives rise to benzene and an aliphatic fragment.  
18 We characterized the structure of dehydrochlorinated PVC (PVC residue) using thermal gravimetric  
19 analysis (TGA), Fourier-transform infrared spectroscopy (FTIR), and nuclear magnetic resonance  
20 spectroscopy (NMR). FTIR and NMR results indicate that PVC residue contains 20% quaternary carbon  
21 content, indicating a high concentration of crosslinked molecules. We predict that the most probable  
22 structure in the crosslinked centers of PVC residue is cyclohexadiene, which is supported by DFT  
23 calculations, FTIR and NMR.

24  
25 Key words: Plastic pyrolysis, PVC dehydrochlorination, Kinetic model, DFT calculations

26 **1. Introduction**

27 Polyvinyl chloride (PVC) is the third most widely used synthetic polymer after polyethylene (PE)  
28 and polypropylene (PP) in the United States and the fourth most used plastic in the world after PE, PP, and  
29 polyethylene terephthalate (PET).<sup>1</sup> As of 2020, global demand for PVC reached 43.4 million metric tons,  
30 with a 4.6% projected growth rate through 2025.<sup>2</sup> PVC and Polyvinylidene Chloride (PVDC) are commonly  
31 used as oxygen barriers in multilayer packaging materials.<sup>3,4</sup> PVC and PVDC are also used in several other  
32 commonly used materials including: 1) credit cards, 3) PVC safety seals, 4) PVC liners, 5) PVC labels on  
33 PET bottles and 6) occasionally in rigid PVC bottles.<sup>3,5,6</sup> While PVC bottles constitute only a small percent  
34 of all rigids, globally over 576 ktions of PVC bottles were produced in 2020.<sup>2</sup> PVC is thus a common  
35 contaminant in waste plastics that can cause major concerns. For example in PET recycling as little as 100  
36 ppm of PVC contamination can cause degradation and discoloration of PET.<sup>7</sup>

37 PVC is also problematic in thermal depolymerization or pyrolysis of waste plastics. Pyrolysis is a  
38 thermal method to convert waste plastics into plastic pyrolysis oils, which can be further upgraded by  
39 approaches such as steam reforming.<sup>8-10</sup> Over ten companies have made announcements that they are  
40 building or have built commercial plants to thermally degrade waste plastics into a pyrolysis oil.<sup>11</sup> The oil  
41 will be sent to steam crackers for further upgrading.<sup>12</sup> The chlorine concentration in the pyrolysis oil is  
42 directly associated with PVC removal efficiency at the waste sorting facility or potential  
43 dehydrochlorination processes during the thermochemical recycling method.<sup>12,13</sup> If the Cl in PVC is not  
44 efficiently removed from the plastic mixture before pyrolysis, it causes corrosion on stainless steel pyrolysis  
45 reactors and steam crackers due to the formation of HCl.<sup>14,15</sup> If the halogen forms organic halogen in the  
46 pyrolysis products, hydrotreatment is a prospective method to remove it, but has a significant cost.<sup>16</sup>

47 Pyrolysis of even a small amount of PVC can cause corrosion issues. For example, 1-3 wt% of  
48 PVC in the plastic waste feedstock leads to 5,000-10,000 ppm of chlorinated compounds in the final  
49 pyrolysis product.<sup>17</sup> In 1983, a German company added limestone (CaCO<sub>3</sub>) to crushed waste plastic and  
50 processed the mixture in a rotary kiln reactor, pyrolyzed the waste plastics under temperatures from 400 ~  
51 500 °C.<sup>14, 18</sup> However, the chlorine content in the pyrolysis oil was above the requirements.<sup>14</sup> A Japanese  
52 company developed a dechlorination pre-treatment preceding the thermal degradation of mixed waste  
53 plastics. The plastic was mixed with calcium hydroxide (Ca(OH)<sub>2</sub>) and introduced into a twin-screw unit  
54 operating at a temperature of 300 °C or higher, resulting in the removal of approximately 95% of chlorine  
55 through this process.<sup>13, 14</sup> However, the threshold of the chlorine content in modern industry facilities is 3  
56 ppm.<sup>12, 19</sup> In addition, common stainless steel (304 and 316) are considered non-resistant to HCl at any  
57 concentration and temperature.<sup>20</sup> Thus, efficient removal of chlorine from mixed plastics wastes before  
58 pyrolysis is a critical technology.

59 PVC thermal decomposition occurs in two stages. In the first stage, approximately 65% weight loss  
60 occurs in a temperature range between 250 and 350 °C in an autocatalytic dehydrochlorination process that  
61 begins at structural defects like internal C=C bonds and butyl branches associated with tertiary Cl.<sup>21, 22</sup> In  
62 this stage, most of the Cl atoms are removed to form HCl molecules, with the remaining polymer forming  
63 π-conjugated polyenes.<sup>23-28</sup> After sufficient removal of Cl, the polyenes are unstable and thereby prone to  
64 form crosslinked intermediates as char precursors through pericyclic reactions.<sup>15, 29</sup> The main products of  
65 polyene degradation are multicyclic aromatic hydrocarbons, non-condensable gases, and chars.<sup>30, 31</sup>

66 There is ongoing debate about the mechanism of PVC thermal degradation. PVC decomposition  
67 can be described by either consecutive reactions<sup>24, 31-35</sup> or by competitive reactions.<sup>36-38</sup> In 1995, Beltran *et al.*<sup>32</sup>  
68 proposed a PVC degradation model involving two steps and three reactions: in the first  
69 dehydrochlorination stage, HCl and volatile compounds were generated through parallel reactions so that  
70 the first stage could be described as a parallel reaction model. In the second degradation stage, a model  
71 based on a single reaction corresponds to the pyrolysis of the polyene chains. In 2001, Jordan *et al.*<sup>24</sup>  
72 proposed a four consecutive step reaction model that involves: 1) PVC dehydrochlorination; 2) random  
73 chain scission reactions of dechlorinated PVC, 3) cyclization/aromatization, and 4) degradation from coke  
74 formation. In 2013, Gui *et al.*<sup>34</sup> suggested another PVC degradation mechanism involving four different  
75 stages: 1) dechlorination with inner cyclization, 2) scission of aromatic chains, 3) release of quasi-three  
76 rings or three rings, and 4) release of the two-ring group. In 2020, Xu *et al.*<sup>33</sup> proposed a more complex  
77 PVC dehydrochlorination model that involved four consecutive reactions and fit this model to TGA data.

78 Previous models seldom predict Cl removal efficiency in dehydrochlorination process, and the  
79 degradation stages for dechlorinated PVC were difficult to define. For example, in the Jordan *et al.* model,<sup>24</sup>  
80 the cyclization rate would be difficult to determine if some polyaromatics remained on the PVC carbon  
81 back chain. In the Gui *et al.* mechanism,<sup>34</sup> the third and fourth stage could be difficult to distinguish in order  
82 to calculate the kinetics for each stage.

83 In this study, we developed a simpler model that contains two steps: dehydrochlorination of PVC  
84 and further decomposition of PVC residue. A first order reaction model of dehydrochlorination PVC was  
85 used to predict the Cl removal efficiency, and a lumped model was used to predict the overall mass loss of  
86 further decomposition of PVC residue. The model in the dehydrochlorination stage was consistent with  
87 DFT calculations and can predict the residual Cl content during the pretreatment till 0.1 wt. %. In addition,  
88 we characterized the structure of PVC residue using TGA, FTIR, and NMR. These results provide insight  
89 into the final structure of PVC residue, which may be used for further upgrading through pyrolysis or  
90 mechanical recycling.

## 91 2. Experimental methods

### 92 2.1 Materials

93 Plastics: PVC (#81387) was obtained from Sigma-Aldrich, and both Polystyrene (PS 608A) and Low-  
94 density polyethylene (LDPE 524B) were obtained from Amcor. The PVC was used without modification.  
95 PS and LDPE were mixed by cryogrinding with a 1:1 ratio to prepare the standards on NMR analysis.

97 Gas chromatography (GC) standards: Benzene (#401765) and the polycyclic aromatic hydrocarbon standards  
98 (EPA 8270 Calibration Mix 1, #5M00720) were obtained from Sigma-Aldrich.

## 99 100 2.2 Thermogravimetric analysis (TGA) of PVC

101 TGA was carried out using a TA Instruments SDT Q500 system with nitrogen ( $N_2$ ) used as the  
102 sweep gas. Different  $N_2$  flow rates (50-200 sccm) and sample weights (2-10 mg) were used in the  
103 experiments. The PVC particle sizes are less than 80 mesh (174 micron) with a molecular weight of 90,000  
104 Da. To study the PVC dehydrochlorination process, 10 mg PVC was heated to 320 °C with a temperature  
105 ramping rate of 2 °C/min and held at 320 °C isothermally for 20 min. To obtain the data for our kinetic  
106 model, 10 mg PVC was heated to 600 °C with a temperature ramping rate of 10 °C/min.

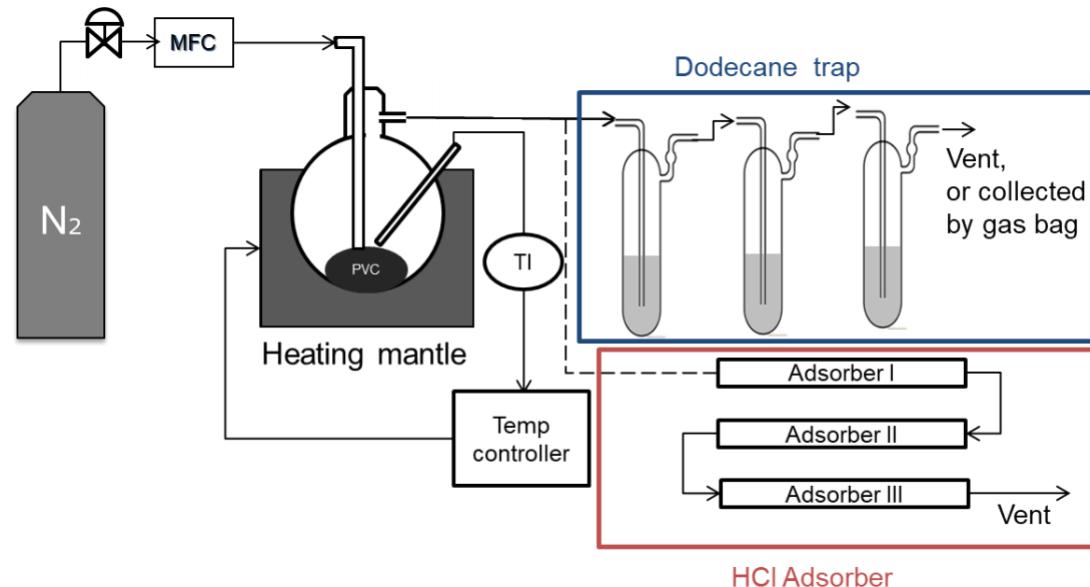
## 107 2.3 PVC pretreatment system

108 The pretreatment system setup is shown in Figure 1. The system contained two sets of gas  
109 treatments for (1) collecting the organic product and (2) removing the generated HCl. Nitrogen was used  
110 as the inert gas with a flow rate at 100 sccm. The temperature of the reactor was ramped from room  
111 temperature to 320 °C with a 2 °C/min ramping rate and held isothermally for 20 min. For each batch, 1-  
112 10 g of PVC was used.

113 For collecting the organic effluents released from the dehydrochlorination process, the system was  
114 connected to a dodecane trap, which was composed of three bubblers with 10 mL dodecane in series. The  
115 dodecane solution collected in each condenser was analyzed using a GC shown in section 2.41. Excess  
116  $Na_2CO_3$  powder was mixed with the PVC in the reactor to capture the generated HCl.

117 For collecting the dehydrochlorinated PVC, no base was mixed with PVC in the reactor, so the  
118 system was connected to three adsorbers in series to remove the generated HCl. The adsorbers were filled  
119 with a mixture of calcium hydroxide powder and alumina pellets. The dehydrochlorinated PVC obtained  
120 from the pretreatment system will be referred to as PVC residue later in the paper.

121



122  
123 **Figure 1.** Reactor scheme of PVC thermal pretreatment system.

## 124 125 2.4 Characterization of PVC residue

### 126 2.4.1 GC- Flame ionization detection (GC-FID)

127 The liquid products collected from the dodecane trap were analyzed by GC- FID using Shimadzu  
128 GC-2010 with an RTX-VMS column. The temperature of the GC was held at 40 °C for five minutes and

129 then increased to 240 °C with a ramping rate of 7.5 °C/min and held for 10 minutes. The temperature of the  
130 FID detector was 240 °C. Products were quantified using external standards.

#### 131 **2.4.2 TGA**

132 Ten mg of PVC residue was tested using a TGA with a TA Instruments SDT Q500 system (same  
133 as the above). The sample was heated to 600 °C with the purge of nitrogen 50 sccm at a temperature ramp  
134 rate of 10 °C/min.

#### 135 **2.4.3 FT-IR spectroscopy**

136 A Bruker Vertex 70 with a liquid nitrogen-cooled MCT detector was used for the FTIR-ATR  
137 analysis. A MIRacle single reflection cell with a diamond crystal was utilized as the ATR cell (Pike  
138 Technologies). The samples were tested with 128 scans, a resolution of 4 cm<sup>-1</sup>, and a range of 4000-600  
139 cm<sup>-1</sup>.

#### 140 **2.4.4 GC-MS/FID Polyarc analysis of extractable compounds**

141 Five hundred to seven hundred mg of the PVC residue was extracted using 25 mL of  
142 dichloromethane in amber borosilicate hermetically sealed vials. Vials were sonicated for 10 minutes prior  
143 to equilibrating in the dichloromethane for 10 days. Polyaromatic hydrocarbons have low solubility and  
144 high affinity for solids, and therefore equilibration times are long (at least 7 days in water depending on the  
145 molecular weight).<sup>39</sup> The extract was filtered and the remaining PVC residue was rinsed with 5 mL of  
146 dichloromethane, for a total of 30 mL extract. The dichloromethane extract was concentrated to 1 mL under  
147 a gentle stream of nitrogen and then spiked with 5 µL internal standard (EPA 8270 deuterated internal  
148 standard mix from Sigma Aldrich). Quantification of PAHs and estimation of unknowns were analyzed  
149 using an Agilent GC- mass spectroscopy (MS)/FID Polyarc. Details on analysis including standard  
150 information, GC-MS conditions, and chromatograms are included in electronic supplementary materials  
151 (ESI) Text S1 and Figure S1. The cleaned PVC residue was dried for 24 hours at 40 °C, and then analyzed  
152 by NMR.

153

#### 154 **2.4.5 Solid-state NMR**

155 All solid-state NMR experiments were collected using a 600 MHz Bruker Avance-III NMR  
156 spectrometer equipped with a PhoenixNMR HXY MAS probe with a 4 mm probe head, configured in HX  
157 dual resonance mode. Approximately 50 mg of each material was center-packed into thin-walled 4 mm  
158 Revolution NMR zirconium rotors and sealing spacers. All data was collected using 14 kHz MAS. For all  
159 experiments, typical hard pulses were 4 µs for <sup>13</sup>C and either 3.15 or 4.0 µs for <sup>1</sup>H, cross-polarization (CP)  
160 was achieved a square 60 kHz RF spin-lock pulse on the <sup>13</sup>C channel, and a 10% linear ramped spin-lock  
161 pulse on the <sup>1</sup>H channel set to the +1 sideband of the Hartman-Hahn profile. Near-quantitative <sup>13</sup>C spectra  
162 were obtained using the composite pulse MultiCP pulse sequence<sup>40</sup> using the following parameters: 7  
163 ramped cross-polarization steps of 1100 µs each and a 1100 µs final CP step, a 0.8 second proton  
164 polarization delay, a 0.5 second recycle delay, and a rotor-synchronized Hahn-echo was used prior to  
165 acquisition for a clean baseline. 84 kHz <sup>1</sup>H decoupling (Bruker sequence swftppm) was used during both  
166 the Hahn echo and during acquisition. MultiCP conditions were optimized using cryomilled model  
167 aromatic-containing and aliphatic-containing polymers PS and LDPE.

168 2D <sup>13</sup>C-<sup>1</sup>H Frequency-Switched Lee-Goldberg Heteronuclear Correlation (FSLG-HETCOR)<sup>41</sup> data  
169 were collected using the lghetfq Bruker pulse sequence. To observe correctly scaled <sup>1</sup>H chemical shifts,  
170 which evolve under the LG condition in the indirect dimension, we set from 10 to 3 and allowed for the  
171 pulse sequence to directly account for the scaling factor of 0.577. <sup>1</sup>H shifts were referenced externally to  
172 TMS at 0 ppm by acquiring the identical FSLG-HETCOR experiment on crystalline  $\alpha$ -glycine, for which  
173 the observed <sup>1</sup>H shifts for the CH<sub>2</sub> site were set to 3.8 and 2.6 ppm.<sup>42,43</sup> The experiment was collected using  
174 a short (100 µs) cross-polarization time to preferentially observe directly bonded CH pairs. All data were  
175 processed using MestreNova version 14.

#### 176 **2.4.6 Total halogen analysis**

177 The PVC residue samples were sent to Huffman Hazen Laboratories (Golden, CO) for a total  
178 halogen analysis. A Mitsubishi TOX-100 instrument was used with a dual zone high temperature  
179 (800 °C/900 °C) quartz combustion furnace in an oxygen atmosphere. This converted any halogen to halides  
180 and oxyhalides. These compounds then were transported to an absorber solution within a coulometric cell  
181 and titrated against silver to the potentiometric endpoint. Since pure PVC only contains Cl, all detected  
182 halogens were measured as Cl.

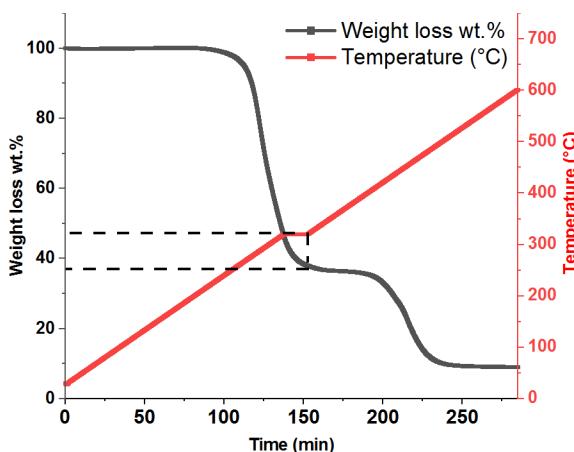
183  
184 **2.5 Computational details**

185 The formation of benzene from polyene chains was modelled by means of DFT calculations using  
186 Gaussian 09.<sup>44</sup> All calculations were performed at the M06-2X/6-31++g (d,p) level of theory and the  
187 computed Gibbs free energies are reported at 327 °C.<sup>45, 46</sup> This level of theory is appropriate for  
188 computational studies of thermal decomposition of PVC.<sup>15</sup> All reported transition states had a single  
189 imaginary frequency that involved motion along the reaction coordinate, whereas there was no imaginary  
190 frequency for states that represent stationary points in the potential energy diagram (PED).

191  
192 **3. Results**

193 **3.1 Quantification of organic products generated from PVC dehydrochlorination**

194 Figure 2 shows the TGA result for PVC decomposition. The red line represents the TGA  
195 temperature program and the black line represents the normalized weight loss of PVC. The PVC was 1)  
196 ramped at a rate of 2 °C/min from room temperature to 320°C, 2) held at 320 °C for 20 min, and 3) heated  
197 to 600°C with a ramp rate of 2 °C/min. The dash lines show the mass loss for the first two stages of the  
198 TGA temperature program (the PVC dehydrochlorination process). In the first stage, 53.1 wt.% of the  
199 original mass of PVC was lost, and in the second stage, 8.3 wt.% of the PVC was lost. The first stage mass  
200 loss is due to the release of Cl from PVC where the solid PVC forms an unstable polyene species.<sup>25</sup> The  
201 polyene then starts cyclization and decomposing into aromatics, non-condensable gases, and  
202 polyaromatics/coke species during the second stage.<sup>25, 30</sup>



204  
205 **Figure 2.** PVC degradation in TGA with a ramping rate of 2 °C/min from room temperature to 320 °C,  
206 held at 320 °C for 20 min, then ramped 2 °C/min to 600°C, with a 50 sccm N<sub>2</sub> flow.

207  
208 In the PVC pretreatment system, 1g of PVC was mixed with 3g of Na<sub>2</sub>CO<sub>3</sub> and decomposed at the  
209 same temperature program shown in Figure 2. This allowed us to quantify the aromatic formation during  
210 the pretreatment process. The aromatics were condensed in a dodecane solution and analyzed by GC-FID.  
211 Benzene was the only detected chemical in the dodecane trap by GC-FID and accounted for 2.8 wt.% of  
212 the initial PVC mass. This is consistent with other literature studies where HCl and benzene are coproduced.

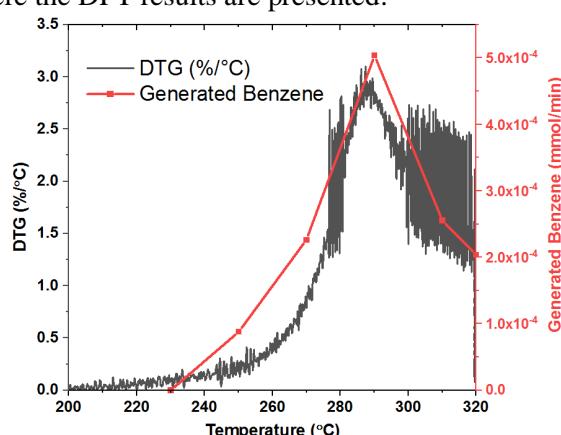
213 <sup>30, 33</sup> The amount of HCl formed was estimated from the stoichiometric composition of pure PVC, which is  
214 58.4 wt.%. The overall mass loss obtained from the pretreatment system was 61.2 wt.%, which is consistent  
215 with the TGA result (61.4 wt.%). Therefore, both PVC pretreatment and TGA results suggest that the main  
216 volatile products of PVC dehydrochlorination are HCl and benzene.

217 A previous study reported that both naphthalene and anthracene are trace products from the  
218 dehydrochlorination of PVC,<sup>33</sup> and DFT calculations have shown that Gibbs free energy barriers associated  
219 with the formation of such products are substantial (> 200 kJ/mol).<sup>47</sup> We did not see these products using  
220 GC-FID. We used dichloromethane to extract any compounds in the PVC residue and analyzed by GC-MS.  
221 Traces of the polycyclic aromatic hydrocarbons, such as naphthalene, methylnaphthalene, anthracene, and  
222 phenanthrene were detected, as well as many unknown species. Detailed extraction results are shown in  
223 Figure S1 and Table S1 in the ESI. Grimes *et al.* and Gui *et al.* also reported that heavier aromatics were  
224 generated after the PVC dehydrochlorination stage.<sup>34, 48</sup> We estimated the yields of these polycyclic aromatic  
225 hydrocarbons to be less than 0.08 wt. %.

### 226 3.2 Stepwise benzene formation and quantification during PVC dehydrochlorination

227 Aromatic compounds are mainly generated in the second stage (the degradation of polyenes) of  
228 PVC degradation with small amounts of benzene forming during the first stage.<sup>30</sup> A stepwise benzene  
229 quantification could help estimate the benzene formation rate and better understand the chemistry of PVC  
230 dehydrochlorination.

231 Gas products generated from the PVC dehydrochlorination were collected in a dodecane trap  
232 connected with a gas bag in the PVC pretreatment system. Temperature segments of 20 °C from 140 to  
233 320 °C were used for these experiments. The collected sample in the dodecane traps and the gas bags were  
234 quantified by GC-FID. Benzene was the only product detected by the GC. The benzene formation rate was  
235 calculated by the mass detected by the GC divided by the time collected for each trap. Figure 3 shows that  
236 the DTG of PVC's TGA curve and the benzene generation rate follow similar trends with temperature.  
237 Benzene formation starts at 220 ~ 240°C. The quantity of benzene generated (2.8 wt.%) during  
238 dehydrochlorination was observed to be notably lower than the stoichiometry generation of HCl (58.4  
239 wt.%). Therefore, the derivative thermogravimetric (DTG) curve was employed to depict the rate of HCl  
240 formation, suggesting the formation rates of both benzene and HCl follow a similar trend. HCl could  
241 potentially catalyze benzene formation during the dehydrochlorination process. This hypothesis is further  
242 examined in section 3.3, where the DFT results are presented.



244

245 **Figure 3.** Comparison of the first derivative of TGA (PVC dehydrochlorination signal) and the rate of  
246 benzene formation with a temperature ramp rate of 2 °C/min.

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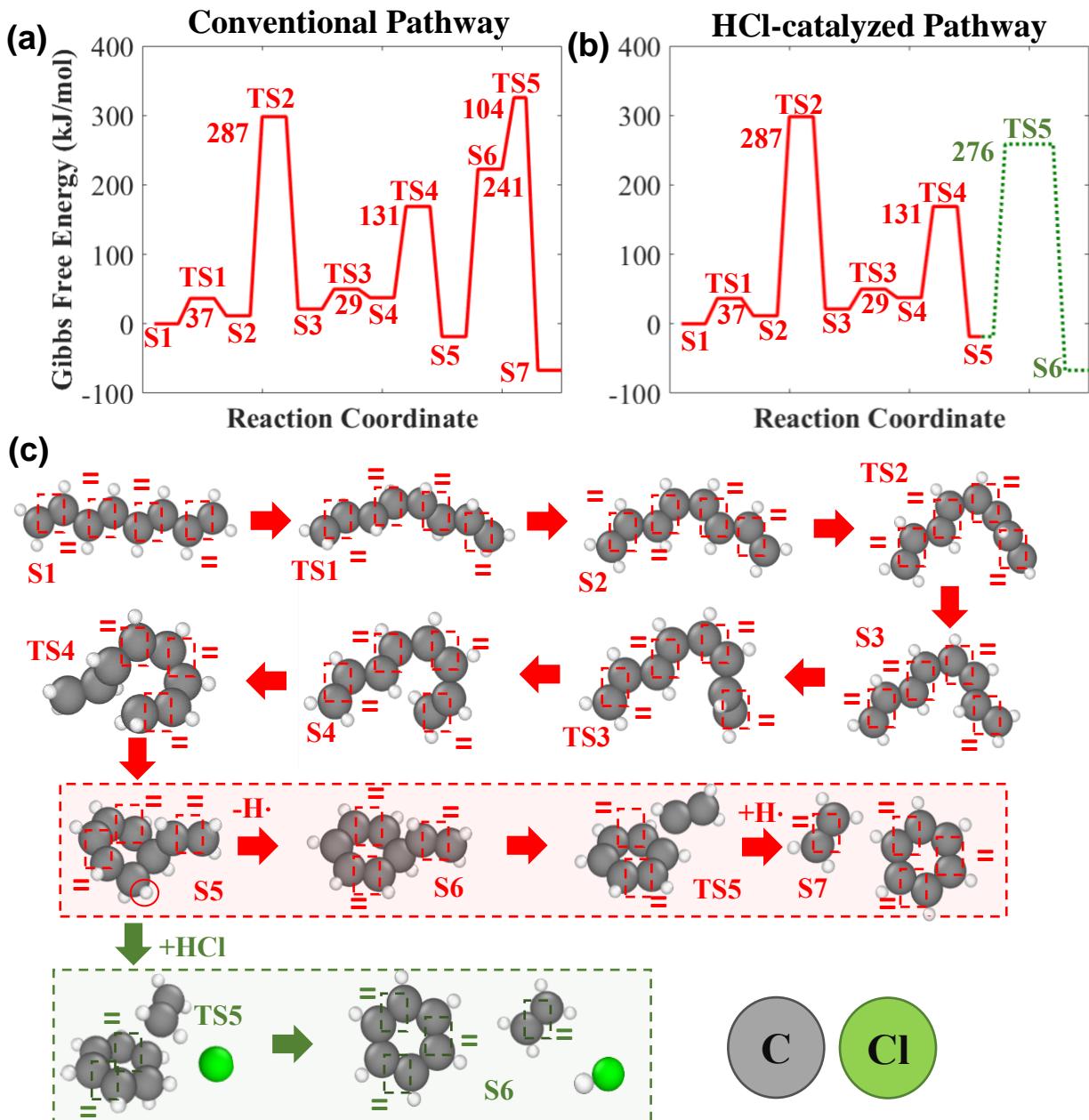
### 248 3.3. DFT calculations of benzene formation during PVC dehydrochlorination

249 The detailed benzene formation mechanism predicted by our DFT calculations is shown in Figure  
250 4. DFT calculations support the synergistic effect between dehydrochlorination and benzene formation  
251 demonstrated by TGA in Figure 3. Figure 4a shows the Gibbs free energy diagram for benzene formation  
252 starting from a single polyene chain via a conventional pathway reported in the literature.<sup>15</sup> This pathway  
253 is intramolecular and involves the cyclization of a polyene chain to cyclohexadiene followed by a bond  
254 cleavage.<sup>49</sup> It begins with three isomerization reactions of the polyene (**S1** → **S2**, **S2** → **S3**, **S3** → **S4**) before  
255 a ring closure reaction (**S4** → **S5**) (Figure 4c and Figure S2 in the ESI), which gives rise to a cyclohexadiene  
256 ring (**S5**) (Figure 4c and Figure S2 in the ESI). The latter reaction step is exergonic by 56.0 kJ/mol and  
257 requires a Gibbs free energy barrier of 131.0 kJ/mol (Figure 4a). The isomerization reactions exhibit low  
258 Gibbs free energy barriers except for **S2** → **S3**. This step involves a rotation around a double bond and has  
259 a high activation energy barrier (287.0 kJ/mol) (Figure 4a). After ring closure, the formation of benzene  
260 occurs via an atomic hydrogen abstraction from **S5** followed by a homolytic C–C cleavage (**S6** → **S7** Figure  
261 4a and Figure S2 in the ESI). The short segment shown in **S6** and **S7** in Figure 4c refers to the residual  
262 polyene chain after the benzene cleavage. We compute that the effective Gibbs free energy barrier from **S5**  
263 to **S7** is 345.0 kJ/mol (Figure 4a).

264 We found that the C–C cleavage reaction step (**S6** → **S7** in Figure 4a and Figure 4c), which is  
265 kinetically the least favorable in the conventional pathway (Figure 4a), may be catalyzed by HCl (Figure  
266 4c and Figure S2 in the ESI). HCl catalysis is likely to occur during the dehydrochlorination stage where a  
267 considerable amount of HCl is released from PVC. This is corroborated by the presented experimental data  
268 in Figure 3. The HCl-catalyzed C–C cleavage takes place via a hydrogen exchange, whereby HCl  
269 withdraws a hydrogen from the cyclohexadiene ring and donates its hydrogen to the aliphatic fragment.  
270 Structure **S5** decomposes directly to ethylene and benzene in the presence of HCl (**S5** → **S6** via **TS5** in  
271 Figure 4b and Figure 4c). This concerted process requires a Gibbs free energy barrier of 276.0 kJ/mol,  
272 which is lower than that for the **S5** → **S7** reaction step in the conventional pathway (Figure 4a) by 69.0  
273 kJ/mol. Therefore, the DFT results obtained here confirm that benzene formation is catalyzed by HCl,  
274 thereby justifying the detection of benzene in the first decomposition stage of PVC.

275 This result may help understand char formation at the final stage of pyrolysis. At the end of the 2<sup>nd</sup>  
276 stage of PVC degradation, there is little Cl in the system, and the energy barrier of benzene formation  
277 becomes high. Thus, the carbon backbones tend to build more crosslinks and form chars instead of forming  
278 aromatic compounds.

279



280  
281 **Figure 4.** (a) Gibbs free energy diagram for the formation of benzene via a conventional pathway (red  
282 line). (b) Gibbs free energy diagram for the formation of benzene via a catalyzed pathway by HCl (green  
283 dashed line); the two pathways are alike up to state S5, but they differ in the way the C–C cleavage occurs  
284 (green dotted line in panel b). The numbers in the plot represent Gibbs free energy barriers in kJ/mol. (c)  
285 Optimized structures for the initial, final and transition states of the two pathways. States that are involved  
286 only in pathway 1 (pathway 2) are shaded in red (green). C, Cl and H atoms are shown with grey, green  
287 and white circles, respectively. Gibbs free energies are reported at 327 °C. Double bonds are indicated by  
288 an equal sign and a dashed square on the molecular structures. The hydrogen atom that is abstracted from  
289 the ring of S5 is marked with a red solid circle.

290  
291

292

293 **3.4 Kinetic model for PVC degradation**

294 PVC degradation occurs in two main steps: (1) dehydrochlorination followed by (2) the  
 295 decomposition of the crosslinked intermediates.<sup>28, 30, 32, 37, 38</sup> During the PVC dehydrochlorination only 2.8  
 296 wt.% of the mass of the PVC converts to benzene. Therefore, to simplify the modeling process on PVC  
 297 dehydrochlorination stage, we assume that the formation of benzene (second step) is negligible during the  
 298 PVC degradation at temperatures lower than 320 °C. The PVC degradation model can be divided into two  
 299 regions: (1) below 320 °C, where dehydrochlorination dominates, which is a first order reaction and (2)  
 300 above 320 °C, where the decomposition of the crosslinked intermediates is the prevailing process, which is  
 301 a random scission reaction that generates mainly aromatics and some non-condensable gases.<sup>24</sup>

302 The Arrhenius equation (Eq 1) was used to fit the PVC degradation data for both stages. In the first  
 303 degradation stage, the Arrhenius equation was modified into Eq 2 to obtain the kinetic of  
 304 dehydrochlorination.  $A$  represents the Arrhenius pre-exponential factor,  $R$  represents the gas constant,  $E_a$   
 305 represents the activation energy,  $T$  represents the temperature, and  $\beta$  represents the heating rate. The  $x$  in  
 306 Eq 2 and Eq 3 represent the normalized non-decomposed PVC (PVC residue). The  $w$  in Eq 3 represents the  
 307 current weight,  $w_0$  the initial weight, and  $w_f$  the weight of the char formed after the pyrolysis process.

$$308 \quad k = A \exp\left(\frac{-E_a}{RT}\right) \quad (\text{Eq 1})$$

$$309 \quad k_{HCl} = \frac{\partial x}{dT} = \frac{A_{HCl}}{\beta} \exp\left(\frac{-E_{aHCl}}{RT}\right) (1 - x) \quad (\text{Eq 2})$$

$$310 \quad x = \frac{w}{w_0 - w_f} \quad (\text{Eq 3})$$

311 In the second degradation stage, PVC residue forms a polyene-like structure, which is further  
 312 thermally decomposed by random-scission reactions.<sup>24</sup> Zhao *et al.* reported a parallel first order random-  
 313 scission reaction that can describe polyethylene degradation better than a single first order model.<sup>50-52</sup> We  
 314 applied this model to simulate the polyene decomposition process. The single first order model ( $k_{CI\_single}$ )  
 315 is derived from Arrhenius equation directly shown as Eq 4 to describe the decomposition of the crosslinked  
 316 intermediates. The parallel model for the crosslinked intermediates ( $k_{CI\_parallel}$ ) is shown as Eq 5. The  
 317 AIC statistical analysis Eq 6 was used to compare different proposed models.<sup>52-54</sup> The RSS represents the  
 318 residual sum of squares,  $n$  represents the total data points (sample size), and  $k$  represents the number of  
 319 estimated parameters in the model.

$$320 \quad k_{CI\_single} = \frac{\partial x}{dT} = \left[ \frac{A_1}{\beta} \exp\left(\frac{-Ea_1}{RT}\right) \right] (1 - x) \quad (\text{Eq 4})$$

$$321 \quad k_{CI\_parallel} = \frac{\partial x}{dT} = \left[ \frac{A_1}{\beta} \exp\left(\frac{-Ea_1}{RT}\right) + \frac{A_2}{\beta} \exp\left(\frac{-Ea_2}{RT}\right) \right] (1 - x) \quad (\text{Eq 5})$$

$$322 \quad AIC = n \ln\left(\frac{RSS}{n}\right) + 2k \quad (\text{Eq 6})$$

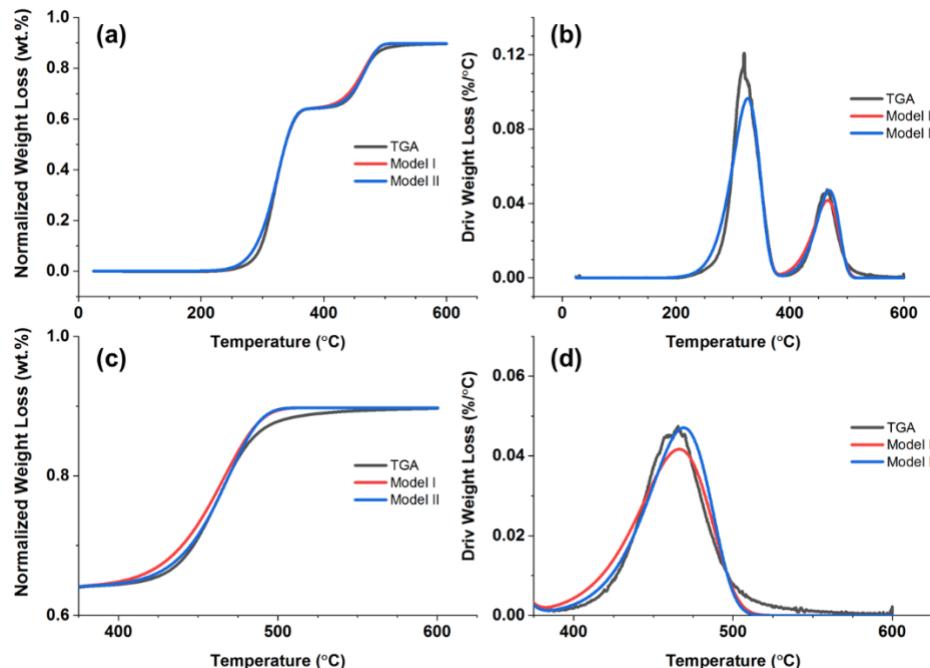
323 The final expression of the PVC decomposition is a linear combination of first and second  
 324 decomposition stage, as shown in Eq 7.  $\alpha$  represents the normalized mass loss of the PVC.  $m_{HCl}$  and  $m_{CM}$   
 325 are the mass of HCl and crosslinked intermediates, respectively. These two values are calculated from the  
 326 mass loss of the 1<sup>st</sup> and 2<sup>nd</sup> stage of PVC degradation. Two PVC kinetic models are proposed here: the main  
 327 difference between Model I and Model II is that Model I refers to the single first order decomposition of  
 328 PVC residue ( $k_{CI} = k_{CI\_single}$ ) and Model II refers to the parallel first order decomposition of PVC residue  
 329 ( $k_{CI} = k_{CI\_parallel}$ ).

$$330 \quad \alpha = m_{HCl}[-1 \times \exp(-k_{HCl} \times t) + 1] + m_{CI}[-1 \times \exp(k_{CI} \times t) + 1] \quad (\text{Eq 7})$$

331 The "nlinfit" function in Matlab was used to fit the model ( $A$  and  $E_a$ ) parameters to the experimental  
 332 data by minimizing the residual sum of squares (RSS). Figure 5a and 5b compare the actual TGA mass loss  
 333 to Models I and II. Figure 5c and 5d show the zoomed in spectrum of the secondary PVC degradation stage.  
 334 The fitted parameters for PVC degradation are shown in Table 1 with a 95% confidence interval. Model II  
 335 better describes the second stage of PVC decomposition according to the AIC equation as shown in Table  
 336 2 and Figure 5. The kinetic model for PVC degradation that best fits the data thus contains two stages: a

337 first order reaction model for the dehydrochlorination, and a parallel first order reaction model for the  
 338 further thermal decomposition of polyenes.

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**Figure 5.** Comparison of weight loss curve of PVC between model and experimental results, including (a) TGA, (b) DTG with  $10\text{ }^{\circ}\text{C}/\text{min}$  ramping rate to  $600\text{ }^{\circ}\text{C}$  with both first stage degradation, (c) zoomed in secondary degradation of TGA, and (d) DTG results.

345 **Table 1.** Kinetic parameters for PVC degradation. Rate constants ( $k$ ) correspond to reactions shown in  
 346 Figure 5.

PVC Model I		PVC Model II	
$E_a$ (kJ/mol)	$A$ ( $\text{s}^{-1}$ )	$E_a$ (kJ/mol)	$A$ ( $\text{s}^{-1}$ )
$115.72 \pm 0.69$	$8.63 \times 10^6 \pm 1.23 \times 10^5$	$k_1$	$115.72 \pm 0.69$
$201.24 \pm 1.32$	$3.05 \times 10^{12} \pm 4.84 \times 10^9$	$k_3'$	$5.98 \pm 0.03$
		$k_3''$	$230.60 \pm 1.24$

347  
 348

**Table 2.** AIC values for PVC models

Model	Number of parameters	RSS	Sample size N	$\text{AIC}_C$
PVC model I	4	0.56	3757	$-3.31 \times 10^4$
PVC model II	6	0.48	3757	$-3.37 \times 10^4$

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The kinetic model was further validated by both TGA isothermal experiments and DFT calculations. Ten mg of PVC was tested on PVC at  $210$  and  $300\text{ }^{\circ}\text{C}$  isothermally for 2 h. The kinetic model accurately predicted Cl loss for these isothermal experiments (Figure S3 in the ESI). DFT calculations verified the catalytic effect of HCl in the dehydrochlorination reaction step. Figure S4 in the ESI shows the DFT-computed initial, transition and final state structures for the HCl-catalyzed and non-catalyzed dehydrochlorination. The DFT calculated dehydrochlorination energy barrier with HCl autocatalysis is  $135\text{ kJ/mol}$  which is in reasonable agreement with the experimental barrier of  $116\text{ kJ/mol}$ .<sup>47</sup> Also, we have

357 previously shown that dehydrochlorination barriers of 110 kJ/mol are observed at increasing  $\pi$ -conjugation  
358 lengths.<sup>47</sup>

359

### 360 **3.5 Quantification of the residual Cl content**

361 Four PVC residue samples were characterized by total halogen analysis using the followed  
362 temperature program: increases to 320 °C with a ramping rate of 2 °C/min and hold isothermal for 20 min.  
363 The Cl removal degree was calculated by Eq 8. The initial theoretical Cl was obtained from stoichiometry.  
364 The average Cl removal degree for the four pretreatment samples was 99.69% with a standard deviation of  
365  $2.944 \times 10^{-4}$ . These results confirm that a lower temperature treatment can remove the majority of Cl from  
366 PVC. The remaining Cl may form some organic chlorine compounds during the PVC second degradation  
367 step.

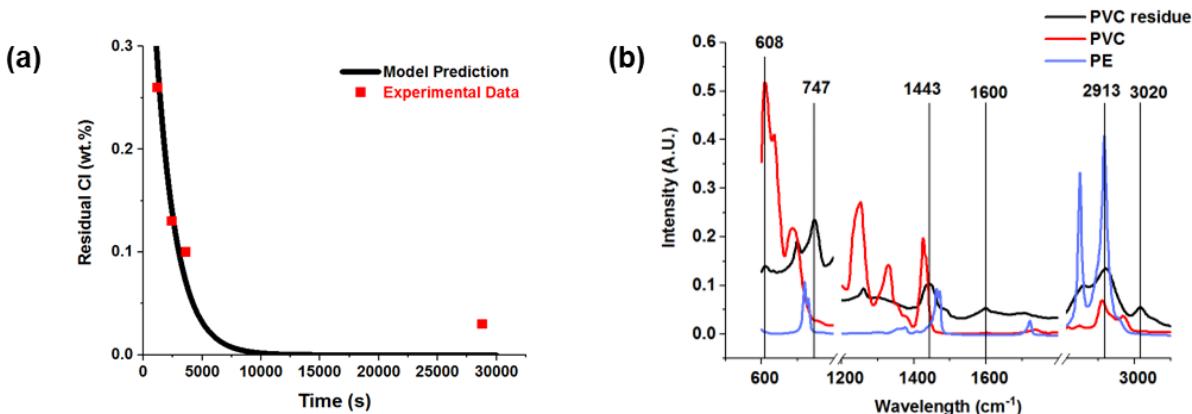
368 
$$\text{Cl removal degree} = \left(1 - \frac{\text{Cl content in the PVC residue}}{\text{Initial theoretical Cl content in virgin PVC}}\right) \times 100\% \quad (\text{Eq 8})$$

369 To further improve the Cl removal efficiency, we extended the isothermal treatment at 320 °C from  
370 20 min to 40, 60, and 480 min. The Cl content decreased with increasing treatment time. Our kinetic model  
371 ( $k_1$ ) can be used to accurately predict the amount of residual Cl when the Cl content was above 0.1 wt.%,  
372 as shown in Figure 6a.

### 373 **3.6 FT-IR spectroscopy of PVC residue**

374 FT-IR spectroscopy was used to characterize the PVC residue, virgin PVC, and virgin PE. The  
375 PVC residue is the residue prepared by PVC thermal treatment shown as Figure 1. The assignments of the  
376 peaks are shown in Table 3 and Figure 6b. There are two major differences between the spectra of PVC  
377 residue and virgin PVC. First, in the spectrum of virgin PVC, the highest peak is shown in 608 cm<sup>-1</sup>, which  
378 corresponds to the C-Cl peak.<sup>55</sup> This peak decreases in the PVC residue spectrum, indicating most of Cl  
379 was removed from the PVC. This statement is supported by both TGA (Figure S5 in the supplementary  
380 information) and total halogen analysis. Second, there are two peaks at 1600 cm<sup>-1</sup> and 3020 cm<sup>-1</sup> in the  
381 spectrum of the PVC residue, while the same peaks are not observed in the spectrum of virgin PVC; these  
382 peaks have assigned to aromatic structures in the literature.<sup>56, 57</sup> However, since aromatics exhibit a  
383 conjugated- $\pi$  system,<sup>58</sup> these two peaks could also represent the conjugated  $\pi$ -bond structures, contributing  
384 via the crosslinked polyene structures.<sup>47</sup>

385 Both virgin PVC and the PVC residue have a peak at around 1440 cm<sup>-1</sup>, which represents the  
386 methylene group (alkene structure).<sup>56, 59</sup> For the virgin PVC, internal double bond defects could cause this  
387 peak, while for the PVC residue, the double bond structures could be the remaining double bonds after  
388 crosslinking between polyenes. Therefore, the FT-IR results confirm the majority of Cl is removed during  
389 dehydrochlorination of PVC, and that the residual PVC backbone is likely composed of a crosslinked center  
390 with conjugated  $\pi$ -bonds, and surrounding structures with PE-like alkyl structure with some double bonds.  
391



392  
393 **Figure 6.** (a) PVC first stage degradation model (k1) prediction of Cl removal with the experimental data.  
394 (b) FT-IR spectra of PVC residue, pristine PVC, and PE

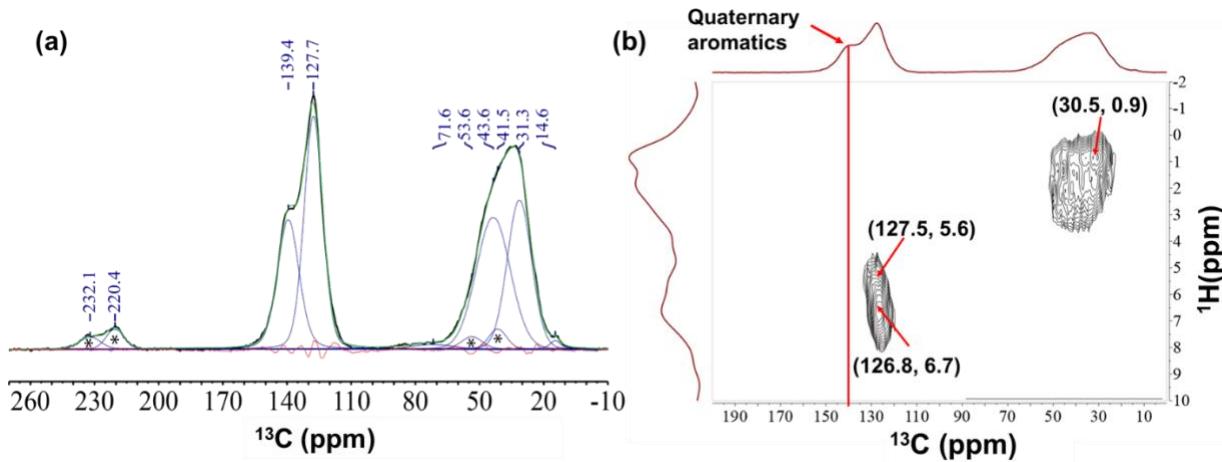
395 **Table 3.** Assignments of FT-IR peaks reported in the literature.

Bond type	Adsorption Band (cm <sup>-1</sup> )
C=C-H stretching (conjugated $\pi$ system)	3000~3100 <sup>60</sup>
Alkyl C-H stretching	2850-2920 <sup>61</sup>
conjugated $\pi$ C=C	1600 <sup>56</sup> , 740 <sup>56, 57</sup>
Alkene C=C scissoring	1422-1453 <sup>57, 59</sup>
C-Cl stretching	600-800 <sup>55</sup>

396

397 **3.7 <sup>13</sup>C Solid-state NMR analysis of PVC residue**

398 The PVC residue was extracted and washed with dichloromethane before NMR analysis to remove  
399 extractable organics. Seventy-eight extractable compounds were identified, of which 11 were known  
400 polycyclic aromatic hydrocarbons and 67 were unknown structures. The semi-quantification total  
401 estimation of these extractable organics accounted for 0.07-0.08 wt.% of the PVC residue mass. A table  
402 including the total weight for each compound and sum total wt.% can be found in Table S1 in ESI. The <sup>1</sup>H-  
403 <sup>13</sup>C multiple cross-polarization magic angle spinning (MultiCP-MAS) solid-state NMR method provides  
404 quantitative information related to carbon structures without the need for long relaxation delays.<sup>22</sup> To  
405 confirm that the MultiCP method is capable of quantitative <sup>13</sup>C analysis, acquisition parameters were  
406 calibrated and validated using model aromatic- and aliphatic-containing polymers PS and LDPE (Figure  
407 S6 in the supplementary information). Figure 7a shows the fitted peak of MultiCP <sup>13</sup>C NMR results of PVC  
408 residue. The NMR spectrum has two main groups of peaks, 20~ 60 ppm, and 120~150 ppm, which are  
409 assigned as the aliphatic and aromatic/alkene groups, respectively. There is another small signal observed  
410 at 15 ppm which is assigned as the primary carbon and can be regarded as an end group of the polymer.  
411 The peaks with asterisks indicate spinning side bands from the aromatic carbons, which are exactly 14 kHz  
412 on either side of the center band.



413  
414 **Figure 7.** (a) Fitted peak results of MultiCP 13C solid-state NMR (b) 2D 13C-1H LG-HETCOR extracts  
415 1H chemical shifts of PVC residue. The NMR data are shown in black, and each peak is labeled in blue,  
416 the fitted peak is shown in green, and the residue is shown in red.

417 To further support the assignments, we collected a 2D  $^{13}\text{C}$ - $^1\text{H}$  FSLG-HETCOR NMR experiment  
418 on the PVC residue, shown as Figure 7b. The signal near 137 ppm was confirmed quaternary, as they have  
419 no immediate protons, while the protonated C=C region near 127 ppm seems to have associations with two  
420 proton types, at roughly 6.6 and 5.5 ppm. The two proton types could refer to the hydrogen attached on a  
421 single C=C bond or  $\pi$ -conjugated C=C bonds but it is difficult to quantify the total amount of each type due  
422 to the resolution of the spectrum. We therefore must quantify the aromatic and alkene protonated C=C  
423 environments together. The quantification of different carbon species based on spectral deconvolution of  
424 MultiCP  $^{13}\text{C}$  spectrum is shown in Table 4.

425  
426 **Table 4.** Integrals of specific peaks corresponding to different carbon types obtained from  $^{13}\text{C}$  MultiCP  
427 NMR analysis of PVC residue.

Carbon Type	Percent Area
Protonated C=C	33.2%
Quaternary Aromatics	22.6%
Aliphatic	42.5%
Primary C	0.8%
Unknowns	1.1%

428  
429 **4. Discussion**

430  
431 **4.1 Kinetic model**

432 PVC model II can predict the PVC decomposition accurately within a temperature range from 300  
433 to 480 °C. Some error between the model and the experimental results occurs at the beginning of the  
434 dehydrochlorination (240-300 °C) and the end of the crosslinked intermediates decomposition stage (480-  
435 520 °C). At the lower temperature range, from 240 to 300 °C dehydrochlorination likely starts at PVC  
436 structure defect sites that are thermally labile without autocatalysis.<sup>25</sup> When the quantities of HCl and  
437 polyenes reach a specific point, they react to generate polyenyl cation radicals, which promote  
438 autocatalysis.<sup>22, 25</sup> While the model we built is a lumped model fitted by nonlinear least error regression, the  
439 model fits well to the kinetics that represent the entire dehydrochlorination process. The empirical fitted  
440 activation energy value is lower than the non-catalyzed dehydrochlorination values reported by DFT,<sup>47</sup> but

441 is in reasonable agreement with the computed activation energies for HCl catalyzed dehydrochlorination of  
442 chlorinated segments adjacent to alternating single and double C–C bonds. Figure 6a demonstrates that our  
443 model can predict the PVC degradation under autocatalytic conditions and shows the model can predict the  
444 residual Cl when the residual Cl level is higher than 0.1 wt.%. However, when the level of residual Cl is  
445 less than 0.1 wt.%, the autocatalytic effect does not occur due to the low Cl concentration. Therefore, our  
446 model is not sensitive enough to predict the residual Cl for 8h pretreatments which has a 0.03 wt.% of the  
447 Cl content.

448

## 449 **4.2 Structure of PVC residue**

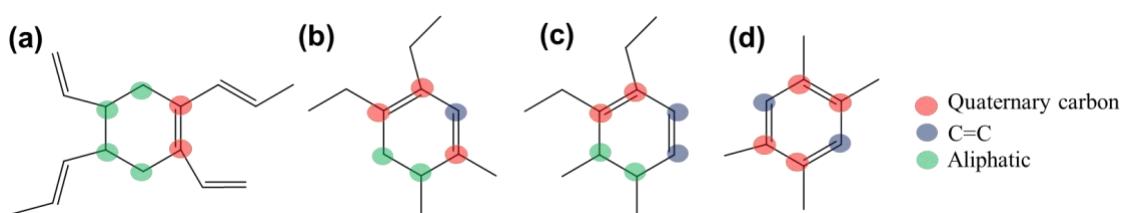
450 The high concentration of the quaternary aromatic carbons (Table 4) indicates high concentration  
451 of crosslinked intermediates. Starnes reported the most likely crosslinked intermediate center in  
452 dehydrochlorinated PVC is cyclohexene that forms by intermolecular reactions with two polyene chains.<sup>22</sup>  
453 The maximum quaternary carbons would be two if cyclohexene is the crosslinked center (Figure 8a).  
454 However, if the cyclohexene is the most abundant structure, all aliphatic carbons must contribute to the  
455 crosslinked center and all HC=C bonds would form the surrounding structure. A surrounding chain with all  
456 HC=C bonds is not stable at high temperatures,<sup>62</sup> hence cyclohexene is less likely to be the most abundant  
457 structure of crosslinked centers in pretreated PVC.

458 We propose that cyclohexadiene is a more probable crosslinked center structure based on the  
459 carbon balance calculated from Table 4 as shown in Figure 8b and 8c. The formation of cyclohexadiene  
460 has two possible explanations. First, the cyclohexene center is formed but is not stable. Thus, hydrogen  
461 transfers from the crosslinked centers to the surrounding structures at 320 °C, resulting in the formation of  
462 cyclohexadiene center. Second, the formation of crosslinked intermediates could be more complex than the  
463 mechanism proposed in the literature,<sup>22</sup> as more than two polyene chains can react with each other and form  
464 a crosslinked center.

465 The high percentage of quaternary carbon indicates a high concentration of crosslinked centers. If  
466 the cyclohexadiene obtains three quaternary carbons, the crosslink concentration in the PVC residue will  
467 be approximately 50% and the surrounding chain would be composed of C=C and aliphatic groups with a  
468 1:1 ratio. If the cyclohexadiene has two quaternary carbons, the crosslink concentration would be around  
469 67%, and the surrounding chain will be composed of C=C and aliphatic groups with a 1 to 2 ratio. A small  
470 amount of char precursor (Figure 8d) could be formed at 320 °C with aromatics as the center structure,  
471 which would reduce the amount of the quaternary carbon contributing to the crosslinked center.

472

473



474

475 **Figure 8.** Proposed crosslinked center structure with (a) cyclohexene, (b) cyclohexadiene with three  
476 quaternary carbons, (c) cyclohexadiene with two quaternary carbons, (d) benzene with four quaternary  
477 carbons as a char precursor.

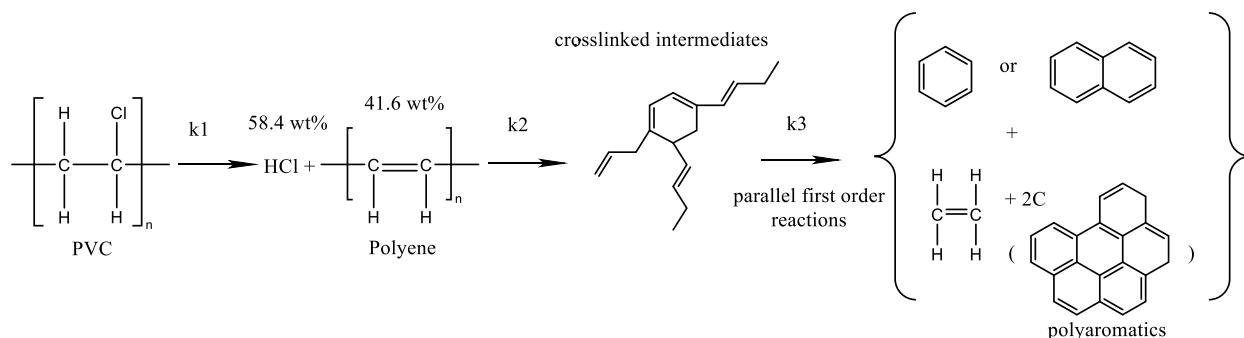
478

## 479 **4.3 PVC decomposition reaction pathway**

480 A reaction pathway for the decomposition of PVC is shown in Figure 9. The first step in this process  
481 is the dehydrochlorination to form HCl and linear polyenes with a rate constant of  $k_1$ . The

482 dehydrochlorination is catalyzed by HCl, which also appears to catalyze the formation of benzene (see  
 483 Figure 3 and Figure 5).<sup>47</sup> As HCl is eliminated, the generated polyenes have a  $\pi$ -conjugated structure and  
 484 start to cyclize to form crosslinked segments through intermolecular reactions.<sup>29</sup> The crosslinked  
 485 intermediates are likely to be composed of cyclohexadiene as the crosslinked center structure and LDPE-  
 486 like structures with random double bonds in the surrounding chains. The structure of the crosslinked  
 487 intermediates is discussed in Section 4.2. As the temperature increases, the crosslinked intermediates  
 488 continue to decompose and generate aromatics and polyaromatics, as well as non-condensable products ( $k_3$ ).  
 489 The formation of aromatics and non-condensable gas from the crosslinked intermediates can be considered  
 490 parallel first order reactions. The intermediates will further convert into polyaromatics, or chars (written as  
 491 2C in Figure 9) after all volatile components are removed.

492



493

494 **Figure 9.** Proposed reaction pathway for PVC thermal decomposition.

495

## 496 5. Conclusions

497 PVC decomposes at temperatures between 250 and 320 °C to form HCl, small amounts of benzene,  
 498 and a solid residue of crosslinked backbones containing LDPE-like polyene as the surrounding chain with  
 499 cyclohexadiene as the most probable crosslinked center. Up to 99.7% percent of Cl is removed during inert  
 500 thermal treatment of PVC at 320 °C after 20 min. The formation rates of HCl and benzene have a similar  
 501 trend which indicates that formation of benzene is likely catalyzed by HCl in the first stage of thermal  
 502 decomposition, a finding corroborated by both TGA results and DFT calculations. The crosslinked  
 503 intermediates contain 22.6% of quaternary carbons which indicates a high crosslink concentration. In other  
 504 words, 50-67% of the carbon in the solid residue contributes to forming crosslinked centers. The solid  
 505 residue continues to decompose in the range of 320-600 °C along with the production of small amounts of  
 506 non-condensable gases and large amounts of aromatics. The crosslinked polymer backbone does not  
 507 decompose and instead forms carbon-rich polyaromatic chars. The overall PVC decomposition could be  
 508 regarded as the combination of a first order dehydrochlorination reaction and a parallel first order  
 509 crosslinked intermediates decomposition. The dehydrochlorination reaction is likely an autocatalytic  
 510 reaction catalyzed by HCl. The apparent activation energy that fits our experimental data for  
 511 dehydrochlorination is 116 kJ/mol (according to TGA), which is in reasonable agreement with the DFT  
 512 prediction of 135 kJ/mol. The apparent activation energy for the crosslinked intermediates decomposition  
 513 is estimated at 231 kJ/mol.

514 The model in this paper predicts Cl removal during PVC thermal pretreatment accurately. The  
 515 model can help design Cl removal pretreatment before pyrolyzing post-waste plastic that contains PVC.  
 516 FT-IR and Solid-state 2D NMR was used to study the structure of the dehydrochlorinated PVC. These  
 517 results provide more information on the intermediate product structures formed during PVC pyrolysis, and  
 518 insights on PVC pyrolysis chemistry.

519

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536  
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