

# Ionic Blockades Control the Efficiency of Energy Recovery in Forward Bias Bipolar Membranes

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## Abstract

Limited understanding exists about the operation of bipolar membranes (BPMs) in forward bias to convert protonic gradients into electrical work, despite its emerging role in many electrochemical devices. In these device contexts, the BPM is typically exposed to complex electrolyte mixtures, but their impact on polarization remains poorly understood. Herein, we develop a mechanistic model explaining the forward bias polarization behavior of BPMs in mixed electrolytes with different acidities/basicities. This model invokes that weak acids/bases accumulate in the BPM and impose an ionic blockade that inhibits the recombination of stronger acids/bases, resulting in a substantial neutralization overpotential. We demonstrate the utility of our model to fuel cells and redox flow batteries, and introduce two materials design strategies for mitigating this inhibition. Lastly, we apply our findings to enhance the energy efficiency of carbonate management in CO<sub>2</sub> electrolyzers. This work highlights how non-equilibrium local environments at membrane-membrane interfaces can define the efficiency of protonic-to-electrical energy conversion.

## Keywords

bipolar membranes, weak electrolytes, buffers, forward bias polarization, ionic blockade, neutralization overpotential, fuel cells, redox flow batteries, CO<sub>2</sub> electrolysis

## Introduction

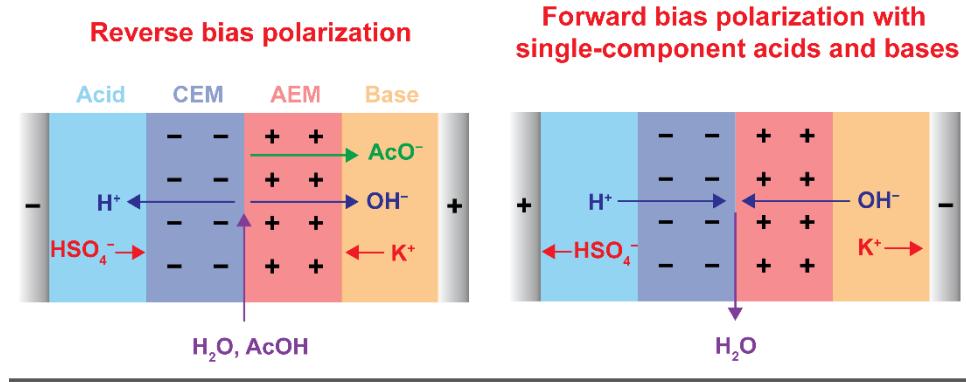
The interconversion of chemical and electrical potential energy gradients underpins the function of electrochemical energy technologies.<sup>1</sup> Typically, this interconversion is mediated by charge transfer reactions at electrode-electrolyte interfaces.<sup>2</sup> However, electrical energy can also be converted into chemical energy in solution, via the formation of ion gradients across membrane-electrolyte interfaces.<sup>3</sup> This mode of energy conversion is key to ion separations and electrodialysis and can be used to enhance the efficiency, selectivity, and durability of flow batteries, fuel cells, and electrolyzers.<sup>3</sup> Thus, mechanistic understanding of ion transfer processes across membrane-electrolyte interfaces is critical for addressing frontier challenges in energy and sustainability.

Bipolar membranes (BPMs) are an emerging electrochemical technology that enables the interconversion of protonic free energy gradients in solution into electrical potential gradients.<sup>4-8</sup> This capability arises from their unique structure comprising a cation exchange membrane (CEM) laminated onto an anion exchange membrane (AEM), giving rise to the

property of ionic current rectification and allowing the maintenance of a stable pH gradient between the catholyte and the anolyte.<sup>4-8</sup> BPMs can be operated in both reverse and forward bias modes. In reverse bias, an applied potential drives the dissociation of water or other proton donors into charged acid and base species.<sup>5,6,9,10</sup> This mode transduces electrical work into a chemical protonic gradient, and allows the continuous generation of acid and base. As a result, it has been extensively studied and applied to water electrolyzers,<sup>11-16</sup> CO<sub>2</sub> electrolyzers,<sup>17-24</sup> and bipolar membrane electrodialysis (BPMED) cells.<sup>25,26</sup> In contrast, in forward bias, the spontaneous recombination of charged acids and bases at the bipolar junction is employed to generate a potential difference that can be used to drive electrical work in an external circuit.<sup>27-29</sup> Consequently, this mode of operation transduces a proton gradient into electrical potential, which can be used to reduce the overall voltage of an electrolytic cell or increase the overall voltage of a galvanic cell. Indeed, forward bias BPMs have been applied to access larger cell voltages in redox flow batteries.<sup>28-30</sup> The foregoing examples showcase the opportunities BPMs offer for interconverting protonic and electrical energy.

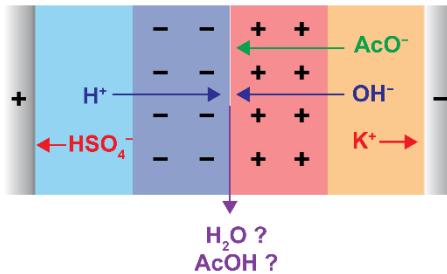
Despite its immense potential, there is limited understanding of the factors that control the efficiency of protonic to electrical energy conversion under forward bias polarization. Existing BPM studies have predominantly examined the reverse bias mode,<sup>5</sup> and the studies on forward bias have largely examined the recombination of only binary electrolytes (i.e. containing only one type of cation and one type of anion), commonly hydronium and hydroxide (**Figure 1**),<sup>31-33</sup> with only a few reports investigating the effect of salt and buffer ions.<sup>10,32,34</sup> To our knowledge, there have been no systematic studies of BPMs in electrolyte mixtures that contain two or more species of different acidities and basicities. This is despite the prevalence of mixed electrolytes in variety of device contexts. For example, in H<sub>2</sub> fuel cells and CO<sub>2</sub> electrolyzers, in addition to hydroxide ions, (bi)carbonates invariably co-exist as a result of CO<sub>2</sub> absorption.<sup>35</sup> In addition, in CO<sub>2</sub> electrolyzers, weak organic bases such as acetate and formate can be produced as liquid products of CO<sub>2</sub> reduction.<sup>36</sup> This knowledge gap of how mixed electrolytes affect the speciation and polarization behavior within forward bias BPMs severely hampers the utilization of this bias mode in complex electrolyte environments.

**Previous work**



**This work**

**Forward bias polarization with mixed acids/bases**

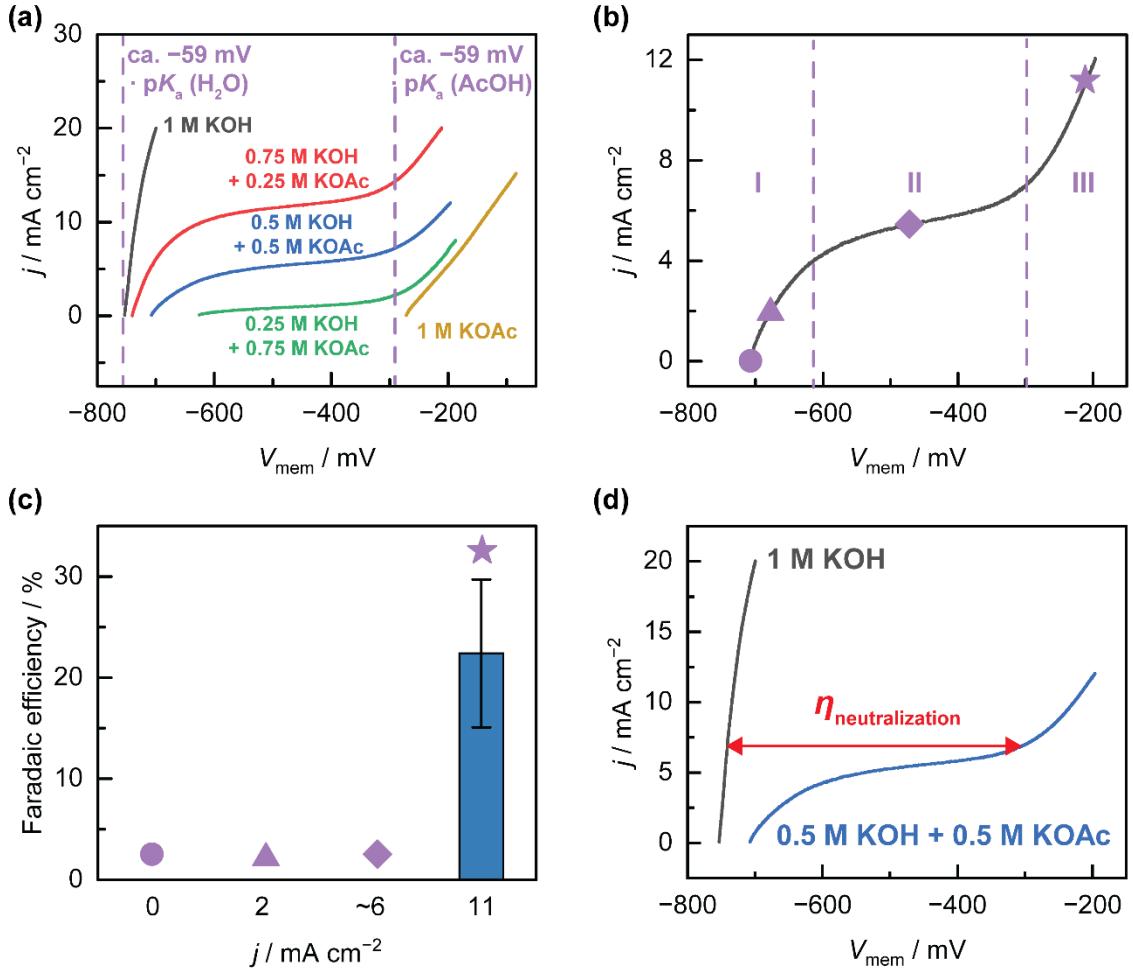


**Figure 1: Existing understanding of ionic processes in BPMs.** BPM cells operating in reverse bias and in forward bias with single-component acids and bases have been extensively studied, but the behaviour of a forward bias cell containing mixed acids or bases is poorly understood.

Herein, we develop a mechanistic model to explain the forward bias polarization behavior of a BPMs in the presence of mixed electrolytes. We show that each constituent in the mixture undergoes neutralization at a distinct membrane voltage dictated by its  $\text{p}K_a$ . Critically, we find that the presence of even a minority concentration of weak acids/bases can impose a large overpotential for the neutralization of stronger acids/bases. We show that this *neutralization overpotential* manifests in a potential-independent limiting current for forward bias operation, and results from an ionic blockade imposed by the accumulation of unreactive weak acid/base ions in the BPM. We demonstrate the utility of this model in the context of fuel cells and redox flow batteries and apply this model to develop improved BPM materials with reduced neutralization overpotentials. Finally, we apply our findings to enhance energy recovery in the context of reversing electrolyte carbonation during  $\text{CO}_2$  electrolysis. Our studies provide a mechanistic framework for understanding the current-voltage behavior of BPMs in mixed electrolytes and enable high-efficiency protonic to electrical energy conversion.

## Mechanism of forward bias polarization in mixed electrolytes

In this work, two types of BPMs were employed: a homemade BPM, denoted by the nomenclature (Acid) | CEM | AEM | (Base), and the commercial Fumasep FBM, denoted by (Acid) | FBM | (Base) (see **Methods** for further detail). Unless the membranes are the subject of the experiment, FBM will be used, and these notations will be abbreviated to (Acid) | (Base) in the text. In addition, as all measurements of membrane voltage ( $V_{\text{mem}}$ ) were made by sensing the electric potential of the acid solution with respect to the base solution,  $V_{\text{mem}}$  will be reported as a negative value, with polarization to less negative values indicating forward bias. Currents are reported based on measurements of electrical current through the external circuit, and hence positive currents correspond to forward bias polarization. In this study, to simplify the analysis of  $V_{\text{mem}}$ , we assume that the concentration of fixed charges in the CEM and AEM is 1 M, and that Donnan potentials at the membrane-electrolyte interfaces are constant at 0 mV. Hence, changes in  $V_{\text{mem}}$  reflect only changes in the bipolar junction voltage ( $V$ ).<sup>37</sup> Here, we will use the term *weak electrolytes* to refer to charged bases whose conjugate acids have a  $pK_a < 14$  (e.g.,  $\text{OAc}^-$ ) or charged acids with a  $pK_a > 0$  (e.g.,  $\text{NH}_4^+$ ), and the term *strong electrolytes* to refer to  $\text{H}^+$  and  $\text{OH}^-$ .



**Figure 2: Electrochemical characterization of BPMs containing KOH-KOAc mixtures.** (a) Forward bias polarization curve of  $1 \text{ M H}_2\text{SO}_4 \text{ | FBM | } x \text{ M KOH} + y \text{ M KOAc}$  (where  $x + y = 1$ ). (b) Forward bias polarization curve of  $1 \text{ M H}_2\text{SO}_4 \text{ | FBM | } 0.5 \text{ M KOH} + 0.5 \text{ M KOAc}$ , with different regions delineated. (c) Faradaic efficiency for AcOH based on analysis of aliquots taken from acid compartment after controlled current or voltage polarization at points indicated in (b). The error bar in (c) represents the standard deviation of three independent replicates. (d) Forward bias polarization curve of  $1 \text{ M H}_2\text{SO}_4 \text{ | FBM | } 1 \text{ M KOH}$  and  $1 \text{ M H}_2\text{SO}_4 \text{ | FBM | } 0.5 \text{ M KOH} + 0.5 \text{ M KOAc}$ , with the neutralization overpotential,  $\eta_{\text{neutralization}}$ , marked for  $7.5 \text{ mA cm}^{-2}$ .

**Forward bias polarization is gated by acid-base equilibria.** In order to understand how mixed electrolytes influence forward bias polarization behavior, we investigated a BPM cell containing a mixture of a hydroxide and acetate in the catholyte paired with a sulfuric acid anolyte. Specifically, we employed cells of the type  $1 \text{ M H}_2\text{SO}_4 \text{ | } x \text{ M KOH} + y \text{ M KOAc}$  ( $x+y=1$ ), where  $\text{OAc}^-$  = acetate. KOH and KOAc were chosen due to the large separation in the  $pK_a$  values for their conjugate acids (14 vs 4.75), allowing us to sample behavior over a wide basicity range. The open-circuit  $V_{\text{mem}}$  values for catholytes containing  $1 \text{ M KOH}$ ,  $0.75 \text{ M KOH} + 0.25 \text{ M KOAc}$  and  $0.25 \text{ M KOH} + 0.75 \text{ M KOAc}$  were found to be close to  $-59 \text{ mV} \cdot \Delta\text{pH}$  (where  $\Delta\text{pH} = \text{pH}_{\text{catholyte}} - \text{pH}_{\text{anolyte}}$ ) or, equivalently,  $-59 \text{ mV} \cdot pK_a(\text{H}_2\text{O})$ , whereas that for the catholyte containing  $1 \text{ M KOAc}$  was close to  $-59 \text{ mV} \cdot pK_a(\text{AcOH})$  (Figure 2(a)). The  $pK_a$ -pinned open-circuit  $V_{\text{mem}}$  value, or  $V_{pK_a}$ , for the latter case is consistent with our findings in our

previous study,<sup>37</sup> in which we showed that ionic short-circuiting processes led to buffering of the bipolar interface by the acid-base couple present ( $\text{H}_2\text{O}/\text{OH}^-$  and  $\text{AcOH}/\text{OAc}^-$ , respectively). In the case of  $1 \text{ M H}_2\text{SO}_4 | 0.75 \text{ M KOH} + 0.25 \text{ M KOAc}$  and  $1 \text{ M H}_2\text{SO}_4 | 0.25 \text{ M KOH} + 0.75 \text{ M KOAc}$ , the presence of  $\text{OH}^-$  ensures a high pH in the region of the AEM close to the bipolar interface, resulting in the open-circuit  $V_{\text{mem}}$  being dominated by the  $\text{H}^+/\text{OH}^-$  recombination couple and pinned to ca.  $-59 \text{ mV}\cdot\Delta\text{pH}$  despite the presence of  $\text{OAc}^-$ . These open-circuit membrane voltages reflect the expected pH gradients at the bipolar interface.

The forward bias polarization curves display a high degree of complexity when mixed electrolytes are used. For the  $1 \text{ M H}_2\text{SO}_4 | 1 \text{ M KOH}$  and  $1 \text{ M H}_2\text{SO}_4 | 1 \text{ M KOAc}$  cells, we observed a monotonic current rise (**Figure 2(a)**), which must correspond to the recombination reactions in **Equation 1** and **Equation 2**, respectively.



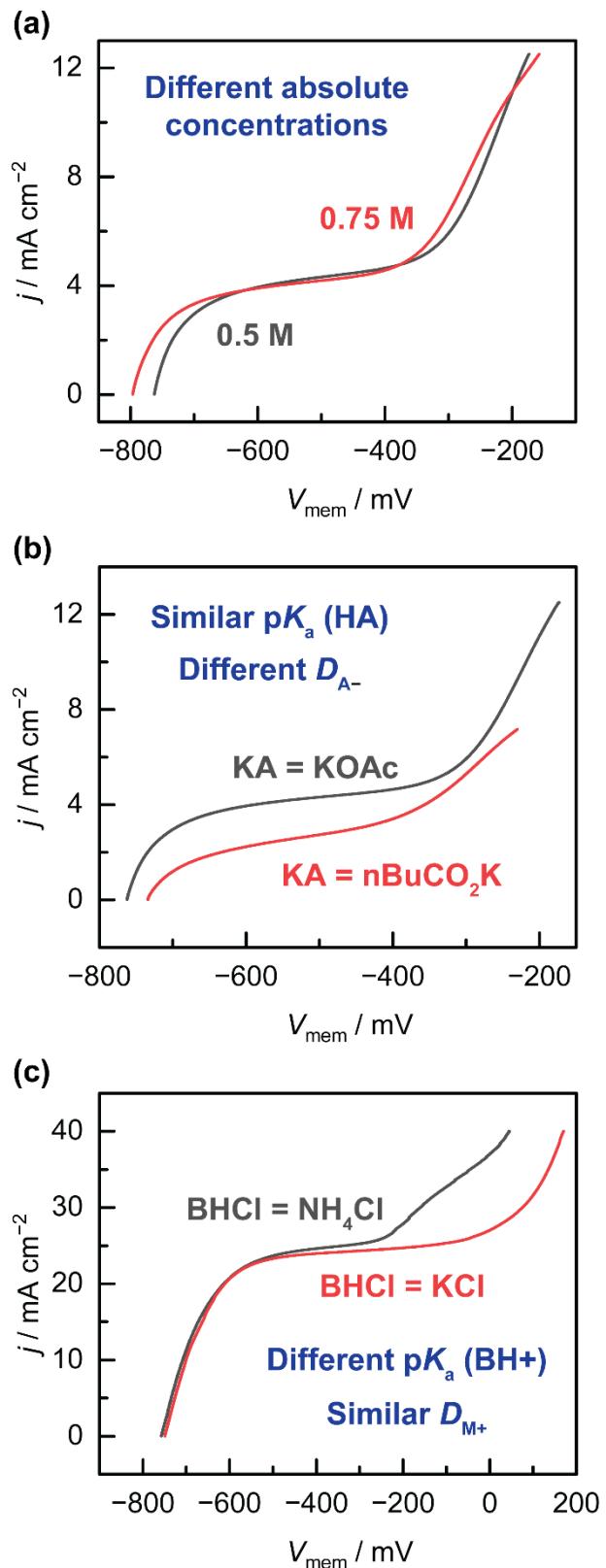
Indeed, surveying other cells of the type  $1 \text{ M H}_2\text{SO}_4 | 1 \text{ M KA}$  containing the monoprotic base  $\text{A}^-$  revealed similar forward bias polarization curves with monotonic current rising from the respective open-circuit  $V_{\text{mem}}$  values set by the  $\text{p}K_a$  of each HA (**Supplementary Figure 3**). In contrast to these single-component catholytes, in the presence of a mixture of hydroxide and acetate, the current rise is interrupted by a broad limiting current plateau (**Figure 2(a)**, red and blue traces). As the KOH: KOAc concentration ratio increases from 0.25:0.75 to 0.5:0.5, the limiting current density increases from  $7.3 \text{ mA cm}^{-2}$  to  $29 \text{ mA cm}^{-2}$ . This potential-independent limiting current is observed despite the large undepleted pool of  $\text{OH}^-$  in the bulk electrolyte that could undergo protonation at the bipolar interface. In addition, the  $V_{\text{mem}}$  at which additional current flows beyond the limiting plateau was found to overlap with the open-circuit  $V_{\text{mem}}$  of  $1 \text{ M H}_2\text{SO}_4 | 1 \text{ M KOAc}$ , occurring at ca.  $-59 \text{ mV}\cdot\text{p}K_a(\text{AcOH})$  (**Figure 2(a)**). When an analogous series of cells of the type  $x \text{ M H}_2\text{SO}_4 + y \text{ M NH}_4\text{Cl} | 1 \text{ M KOH}$  ( $x + y = 1$ ) were polarized in forward bias (**Supplementary Figure 4**), we observed identical behavior to the  $1 \text{ M H}_2\text{SO}_4 | x \text{ M KOH} + y \text{ M KOAc}$  cells. Additionally, consistent with previous experimental<sup>37,38</sup> and computational<sup>32</sup> reports, we observe that the presence of polyprotic buffer species in the cell  $1 \text{ M H}_2\text{SO}_4 | 1 \text{ M K}_x\text{H}_y\text{PO}_4$  ( $x + y = 3$ ), gave multiple limiting current plateaus with inflection points coinciding with ca.  $-59 \text{ mV}\cdot\text{p}K_a(\text{H}_3\text{PO}_4)$  ( $-130 \text{ mV}$ ), ca.  $-59 \text{ mV}\cdot\text{p}K_a(\text{H}_2\text{PO}_4^-)$  ( $-430 \text{ mV}$ ) and ca.  $-59 \text{ mV}\cdot\text{p}K_a(\text{HPO}_4^-)$  ( $-620 \text{ mV}$ ), respectively (**Supplementary Figure 5**). Together, these data reveal that the sigmoidal current-voltage profile is universal to electrolyte mixtures with species of different acidities, regardless of whether those species arise from a common polyprotic acid (e.g., phosphates), or are structurally distinct (e.g., the  $\text{OH}^-/\text{OAc}^-$  and  $\text{H}^+/\text{NH}_4^+$  mixtures).

The foregoing experiments show how electrolyte mixtures impact the current-voltage behavior, but do not shed light on which reaction (**Equation 1** or **Equation 2**) is occurring at each voltage. We postulated that net protonation of a given species can only occur at  $V_{\text{mem}}$  values more positive than its corresponding  $V_{\text{p}K_a}$ . In order to determine the identity of the species being protonated at the bipolar junction, we polarized the  $1 \text{ M H}_2\text{SO}_4 | 0.5 \text{ M KOH} + 0.5 \text{ M KOAc}$  cell galvanostatically or potentiostatically within the three distinct regions of the polarization curve (**Figure 2(b)**); chronopotentiograms/chronoamperograms in

**Supplementary Figure 6–10**), and analyzed aliquots taken from the acid compartment via  $^1\text{H}$  NMR to determine the AcOH concentration. No AcOH was detected for polarizations in the underlimiting (I) and limiting (II) regions of the polarization curve (**Figure 2(c)**). Only when the cell was polarized in the overlimiting (III) region, where  $V_{\text{mem}} > V_{\text{pKa(AcOH)}}$ , did we observe an appreciable concentration of AcOH, corresponding to ca. 22% faradaic efficiency (FE) relative to the total ionic current (**Figure 2(c)**; see section below for quantitative analysis of observed FE). AcOH was also produced at appreciable FEs when the cell was polarized to higher currents (22, 33  $\text{mA cm}^{-2}$ ) in the overlimiting region (**Supplementary Figure 11**). On the other hand, when the 1 M  $\text{H}_2\text{SO}_4$  | 1 M KOAc cell was polarized at the same current densities, quantitative FE was observed for AcOH formation (**Supplementary Figure 12**). The observation that AcOH is produced in net only when  $V_{\text{mem}} > V_{\text{pKa(AcOH)}}$  suggests that  $V_{\text{mem}}$  is directly correlated to the interfacial pH gradient and speciation at the bipolar junction. Since the pH within the CEM, which contains the strong acid  $\text{H}^+$ , is unlikely to change, this observation implies that the increase in  $V_{\text{mem}}$  from  $-760$  mV to  $-280$  mV is consistent with the near-interfacial region of the AEM decreasing in pH from ca. 13 to ca. 4.76. This in turn indicates an accumulation of  $\text{OAc}^-$  and depletion of  $\text{OH}^-$  near the bipolar interface. This correlation of  $V_{\text{mem}}$  to the interfacial acid-base chemistry is discussed further in **Supplementary Note 1**. Indeed, when open-circuit  $V_{\text{mem}}$  measurements of the 1 M  $\text{H}_2\text{SO}_4$  |  $x$  M KOH +  $y$  M KOAc cells were performed immediately after collection of the forward bias polarization curves, the open-circuit transients for return to the unpolarized equilibrium state were found to parallel the polarization curves, with inflection points conserved at the same  $V_{\text{pKa(AcOH)}}$  value (**Supplementary Figure 15**). These observations highlight the strong correlation between the speciation at the bipolar interface, the interfacial pH differential, and  $V_{\text{mem}}$ .

Importantly, these results highlight that a substantial overpotential is imposed on the neutralization of a strong electrolyte ( $\text{OH}^-$ ) by the presence of the weaker electrolyte ( $\text{OAc}^-$ ). Despite the fact that  $\text{OH}^-$  protonation is exergonic at all voltages positive of the open-circuit value, the current plateaus in the presence of  $\text{OAc}^-$ , even in electrolyte mixtures where  $\text{OAc}^-$  is the minority species (**Figure 2(a)**). Consequently, accessing an  $\text{OH}^-$  neutralization current in excess of the limiting value requires the application of a substantial *neutralization overpotential*,  $\eta_{\text{neutralization}}$ , which subtracts from the thermodynamic potential available in the  $\text{H}^+/\text{OH}^-$  neutralization reaction. For example, at  $7.5$   $\text{mA cm}^{-2}$ , even though  $\text{OH}^-$  is expected to carry all the neutralization current,  $V_{\text{mem}}$  for 1 M  $\text{H}_2\text{SO}_4$  | 1 M KOH is  $-740$  mV, but  $V_{\text{mem}}$  for 1 M  $\text{H}_2\text{SO}_4$  | 0.25 M KOH + 0.75 M KOAc is  $-300$  mV, which translates into  $\eta_{\text{neutralization}} = 440$  mV (**Figure 2(d)**). We note that this neutralization overpotential will increase as the concentration of the weak acid/base increases and for  $\text{p}K_{\text{a}}/\text{p}K_{\text{b}}$  values further removed from that of the strong acid/base. Collectively, the foregoing findings evince that the net protonation of a given species  $\text{A}^-$  can only occur at  $V_{\text{mem}} < V_{\text{pKa(HA)}}$ , and that the presence of a weak electrolyte can result in large overpotentials for the neutralization of a strong electrolyte.

**Forward bias limiting currents arise from interfacial ionic blockades.** In order to shed additional light on the factors controlling the limiting current and the neutralization overpotential, we conducted several experiments varying the electrolyte composition. First, for cells of the type 1 M  $\text{H}_2\text{SO}_4$  |  $x$  M KOH +  $x$  M KOAc ( $x = 0.5$  or  $0.75$ ), we held the concentration ratio between KOH and KOAc constant at 1:1 but increased the absolute concentration of KOH/KOAc from 0.5 to 0.75 M, and found that  $j_{\text{lim}}$  remained unchanged at ca.  $4.3$   $\text{mA cm}^{-2}$  (**Figure 3(a)**). This shows that  $j_{\text{lim}}$  is sensitive to the concentration ratio of mixed electrolytes but not to their absolute concentrations.



**Figure 3: Electrochemical characterization of BPMs with varied electrolyte properties.** Forward bias polarization curves for (a) 1 M H<sub>2</sub>SO<sub>4</sub> | FBM | x M KOH + x M KOAc (x = 0.5 or 0.75), (b) 1 M H<sub>2</sub>SO<sub>4</sub> | FBM | 0.5 M KOH + 0.5 M KA (A<sup>-</sup> = OAc<sup>-</sup> or nBuCO<sub>2</sub><sup>-</sup>), and (c) 0.5 M H<sub>2</sub>SO<sub>4</sub> + 0.5 M MCl | FBM | 1 M KOH (M<sup>+</sup> = NH<sub>4</sub><sup>+</sup> or K<sup>+</sup>). We attribute the slight

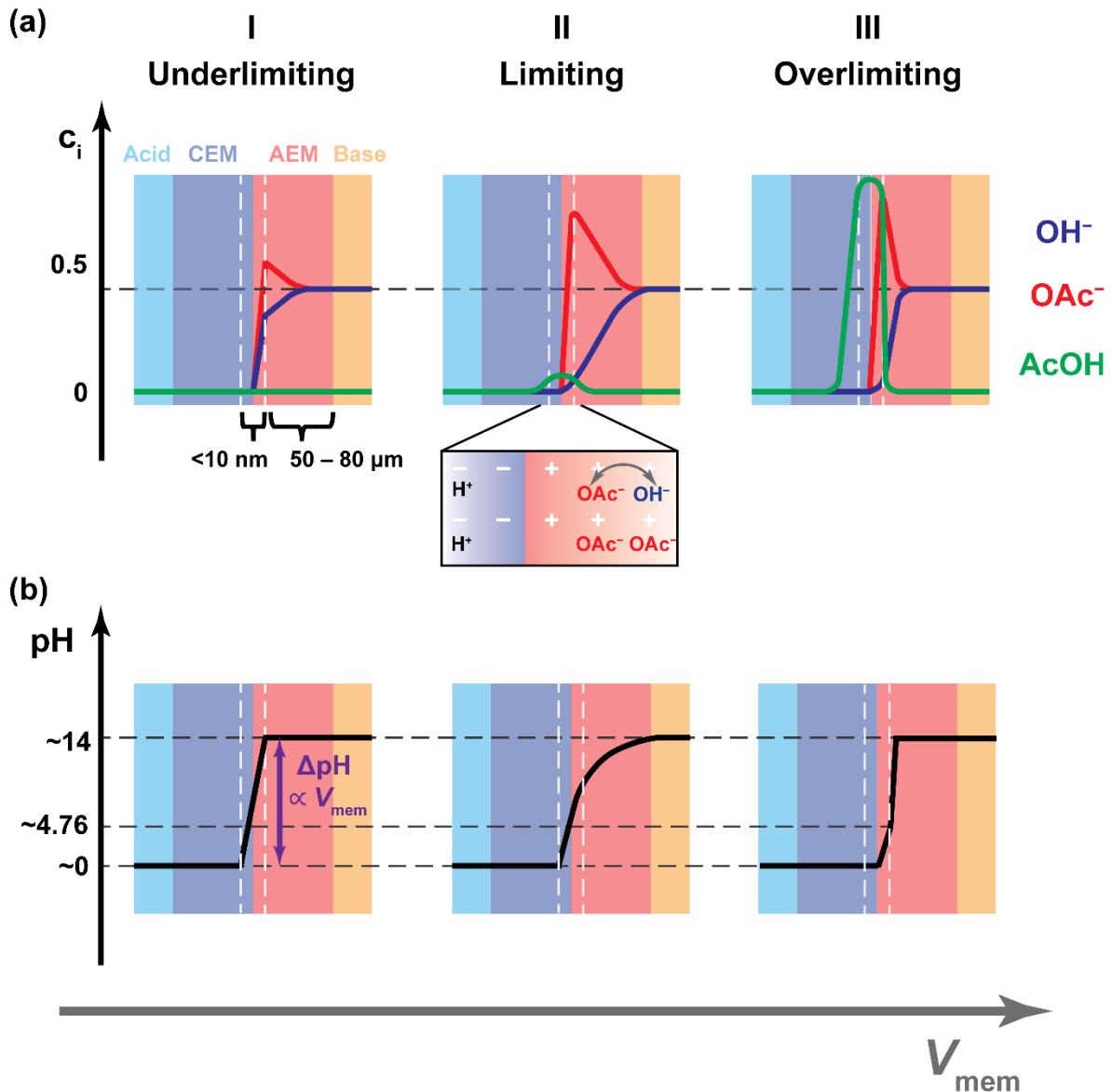
differences in polarization date for 1 M H<sub>2</sub>SO<sub>4</sub> | FBM | 0.5 M KOH + 0.5 M KOAc between **Figures 2** and **3** to the lot-to-lot variability in FBM.

Next, we substituted acetate for n-butyrate in the analyte compartment. Specifically, for cells of the type 1 M H<sub>2</sub>SO<sub>4</sub> | 0.5 M KOH + 0.5 M KA (A<sup>-</sup> = OAc<sup>-</sup> or nBuCO<sub>2</sub><sup>-</sup>, where nBuCO<sub>2</sub> = butyrate), acetate and butyrate have similar proton affinities (pK<sub>a</sub> = 4.76 for AcOH, 4.82 for nBuCO<sub>2</sub>H) but distinct diffusion coefficients ( $D_{OAc^-} = 1.089 \times 10^{-5} \text{ cm}^2 \text{ s}^{-1}$ ,  $D_{nBuCO_2^-} = 0.868 \times 10^{-5} \text{ cm}^2 \text{ s}^{-1}$ ).<sup>39</sup> This substitution leads to a lower  $j_{lim}$  for the nBuCO<sub>2</sub>K cell (ca. 2.7 mA cm<sup>-2</sup>) than the KOAc cell (ca. 4.3 mA cm<sup>-2</sup>) (**Figure 3(b)**), correlated with  $D_{nBuCO_2^-}$  being lower than  $D_{OAc^-}$ . We note that  $V_{mem}$  for the current onset in the overlimiting region is conserved between the two cells, owing to  $V_{pK_a(AcOH)} \approx V_{pK_a(nBuCO_2H)}$ . Conversely, with cells of the type 0.5 M H<sub>2</sub>SO<sub>4</sub> + 0.5 M MCl | 1 M KOH (M<sup>+</sup> = NH<sub>4</sub><sup>+</sup> or K<sup>+</sup>) (note that the electrolyte mixture is now in the acid instead of the base compartment), we selected unreactive ions with similar diffusion coefficients ( $D_{NH_4^+} = D_{K^+} = 1.957 \times 10^{-5} \text{ cm}^2 \text{ s}^{-1}$ ) but different proton affinities (pK<sub>a</sub> = 9.25 for NH<sub>4</sub><sup>+</sup>, 14 for K<sup>+</sup> (H<sub>2</sub>O)).<sup>39</sup> Since K<sup>+</sup> is not deprotonatable, it can be considered a weak acid in the extreme whose acidity is levelled to that of H<sub>2</sub>O (see **Supplementary Note 2**). Here,  $j_{lim}$  was found to be almost identical in value between the two cells (ca. 24 mA cm<sup>-2</sup>) (**Figure 3(c)**), indicating that the diffusive properties of the unreactive ion, rather than its proton affinity, defines the limiting current density. To determine whether  $j_{lim}$  depended on the diffusion coefficient of only the unreactive electrolyte or both the unreactive and reactive electrolyte, we examined the cell with 0.5 M NH<sub>4</sub>Cl + 0.5 M KCl | 1 M KOH, and measured a  $j_{lim}$  that was significantly lower (ca. 7 mA cm<sup>-2</sup>) than that with the 0.5 M H<sub>2</sub>SO<sub>4</sub> + 0.5 M KCl anolyte (24 mA cm<sup>-2</sup>) (**Supplementary Figure 16**). These findings demonstrate that  $j_{lim}$  depends on the diffusion coefficients of both the unreactive and reactive electrolyte, but not on the acid-base thermochemistry of either electrolyte.

Collectively, the foregoing data depicting the effect of electrolyte composition on forward bias polarization suggest a transport model whereby different reactive species in the mixed electrolyte (e.g., OH<sup>-</sup> vs OAc<sup>-</sup>) compete for a finite number of fixed charge sites to charge-pair with in the membrane (e.g., AEM). Specifically, we propose that site competition on the order of the depletion layer thickness (ca. 4 – 10 nm)<sup>32,40</sup> controls speciation at the near-interfacial region (within several nm) of the bipolar junction and consequently the  $V_{mem}$ , and that site competition on diffusional lengthscales (ca. 10s – 100s of  $\mu\text{m}$ ) controls speciation within the bulk of the AEM and consequently the value of  $j_{lim}$ . Our putative model reflects the following boundary conditions: (a) the composition within the AEM near the AEM | Base interface is controlled by the Donnan equilibria for OH<sup>-</sup> and OAc<sup>-</sup>;<sup>32</sup> (b) OH<sup>-</sup> and OAc<sup>-</sup> are the only mobile charges within the AEM, and hence their concentrations must sum to the fixed charge concentration everywhere in the AEM except at the interfacial depletion region; (c)  $V_{mem}$  directly reports on the interfacial pH gradient, and hence reveals the speciation of OH<sup>-</sup>, OAc<sup>-</sup> and AcOH at the bipolar interface.<sup>32,40</sup> Applying these constraints, postulated concentration profiles as a function of the region of the polarization curve in the near-interfacial and bulk regions of the AEM for OH<sup>-</sup>, OAc<sup>-</sup> and AcOH are depicted in **Figure 4(a)**, and postulated pH profiles across the BPM in the same regions are depicted in **Figure 4(b)**. These profiles are in qualitative agreement with a previous computational study.<sup>32</sup>

At open-circuit, we postulate that the concentration ratio of OH<sup>-</sup>:OAc<sup>-</sup> in the bulk of the AEM becomes identical to that in the base solution upon complete equilibration (**Supplementary Figure 17**). The concentrations of OH<sup>-</sup> and OAc<sup>-</sup> near the interface, however,

depend on neutralization equilibria attained between  $\text{H}^+$ ,  $\text{OH}^-$  and  $\text{OAc}^-$ , which we envision to lead to a much lower  $\text{OH}^-:\text{OAc}^-$  ratio than that in the bulk due to the higher reactivity of  $\text{OH}^-$  compared to  $\text{OAc}^-$  (Supplementary Figure 17).



**Figure 4: Concentration and pH profiles across BPMs as a function of polarization region.** (a) Postulated concentration profiles of  $\text{OH}^-$ ,  $\text{OAc}^-$ , and  $\text{AcOH}$  in different regions of the polarization curve (as demarcated in Figure 2(b)). Vertical dashed lines indicate the near-interfacial regions, where equilibration of the proton activity with the electric potential profile in the bipolar interface is rapid. (b) pH profiles in different regions of the polarization curve. Profiles in (a) and (b) are qualitatively plotted based on the initial quasi-steady-state conditions attained upon short-duration polarization of the cell (whereby concentrations of  $\text{OH}^-$  and  $\text{OAc}^-$  in the solution have not significantly changed). The fixed charge concentration in the AEM is assumed to be 1 M to simplify the analysis.

As the cell is polarized into the underlimiting region (region I), the net protonation of  $\text{OH}^-$  according to **Equation 1** allows the passage of current at the bipolar interface, resulting in the steep current-voltage slope (Figure 2(b), region I). Since  $V_{\text{p}K_a(\text{H}_2\text{O})} < V_{\text{mem}} < V_{\text{p}K_a(\text{AcOH})}$ ,  $\text{OH}^-$

is the only base species capable of being protonated in net within this region. This results in the near-interfacial region of the AEM being gradually depleted in reactive  $\text{OH}^-$  and enriched in unreactive  $\text{OAc}^-$  with increasing  $V_{\text{mem}}$  (**Figure 4(a)**, region I). Since the applied field across the BPM induces the migration of both  $\text{OH}^-$  and  $\text{OAc}^-$  towards the bipolar interface, the unreactive  $\text{OAc}^-$  accumulates in the bulk of the AEM while the reactive  $\text{OH}^-$  depletes (**Figure 4(a)**, region I).

Entering the limiting region (region II), the current flatlines and becomes roughly voltage-independent (**Figure 2(b)**, region II). Since  $V_{\text{p}K_a(\text{H}_2\text{O})} < V_{\text{mem}} < V_{\text{p}K_a(\text{AcOH})}$ , the majority of the current is still due to  $\text{OH}^-$  protonation, as the interfacial pH gradient does not yet permit significant net  $\text{OAc}^-$  protonation. We propose that current passed at the bipolar interface is now limited by  $\text{OH}^-$  diffusion. The near-interfacial region of the AEM is now almost completely depleted of the reactive  $\text{OH}^-$  and dominated by the unreactive  $\text{OAc}^-$  (**Figure 4(a)**, region II). Due to the rigidity of fixed charge groups within the AEM, the transport of  $\text{OH}^-$  to reach the interfacial region must be accompanied by coupled motion with  $\text{OAc}^-$ , the only other mobile species, in order to avoid electrical charge gradients and maintain electroneutrality. This results in a type of net place-exchange mechanism for  $\text{OH}^-$  transport, whereby a  $\text{OH}^-$  ion diffusing towards the interface swaps sites with an  $\text{OAc}^-$  ion diffusing away from the interface (**Figure 4(a)**, region II, blowup), leading to the observed potential-independent polarization curve. The observation that  $j_{\text{lim}}$  depends on the  $\text{OH}^-:\text{OAc}^-$  concentration ratio (**Figure 2(a)**) and the diffusion coefficient of both the reactive and unreactive species (**Figure 3(b) – (c)**, **Supplementary Figure 16**) is evidence for this electrolyte exchange mechanism, and furthermore suggests that the overall process is rate-limited by the aggregate place exchange dynamics. We term this overall phenomenon an *ionic blockade*, and emphasize its two key mechanistic aspects: firstly, both the strong and weak electrolytes compete for the same fixed charge sites for occupancy within the membrane; and, secondly, the weak electrolyte is unreactive under the applied membrane voltages and therefore has the net effect of inhibiting the transport of the reactive strong electrolyte to the bipolar interface. Consequently, the concentration of  $\text{OH}^-$  in the bulk of the AEM continues to decrease, whereas the concentration of  $\text{OAc}^-$  continues to increase as  $V_{\text{mem}}$  is swept more positively. However, while we invoke that the overall process for  $\text{OH}^-$  transport to the bipolar interface must involve aggregate place exchange with the unreactive  $\text{OAc}^-$  present to conserve electroneutrality, we are unable to infer whether the limiting region can be entirely explained by depletion and concentration polarization of  $\text{OH}^-$  within the AEM, or whether there are also ion-ion correlations between  $\text{OH}^-$  and  $\text{OAc}^-$  that attenuate the diffusivity of the former on the molecular level.<sup>41</sup> Hence, while our qualitative model captures the key mechanistic principles, we emphasize that a detailed computational model would be better suited to quantitative calculations of concentration profiles and transport fluxes, as well as dissecting the nuances of correlated ion transport. An alternative explanation for the limiting region is that net protonation current can only be passed when the  $\text{AcOH}$  at the bipolar interface diffuses into the AEM and reacts with  $\text{OH}^-$ , but this is a less plausible mechanism (see **Supplementary Note 3**). Another consideration was how the presence of electrolyte mixtures in both acid and base compartments would impact overall polarization. Comparing the polarization curve for  $0.5 \text{ M H}_2\text{SO}_4 + 0.5 \text{ M KCl} | 0.5 \text{ M KOH} + 0.5 \text{ M KOAc}$  to that for  $1 \text{ M H}_2\text{SO}_4 | 0.5 \text{ M KOH} + 0.5 \text{ M KOAc}$ , we found that the former exhibited a lower  $j_{\text{lim}}$ , indicating that electrolyte exchange rates in both the CEM ( $\text{H}^+/\text{K}^+$ ) and AEM ( $\text{OH}^-/\text{OAc}^-$ ) contribute to controlling the overall  $j_{\text{lim}}$  (**Supplementary Figure 19**). Finally, to rule out the co-ion playing a significant role in controlling  $j_{\text{lim}}$ , we polarized the cells  $1 \text{ M H}_2\text{SO}_4 | 0.625 \text{ M MOH} + 0.375 \text{ M MOAc}$  ( $\text{M}^+ = \text{Li}^+, \text{Na}^+$  or  $\text{K}^+$ ) and found a minor dependence on the identity of the co-ion (**Supplementary**

**Figure 20).** Together, the evidence suggests that the ionic blockade imposed by unreactive weak acids/bases in the CEM/AEM is the origin of the aforementioned neutralization overpotential.

Finally, as the cell is polarized past  $V_{pK_a(AcOH)}$ , the current rapidly takes off again (**Figure 2(b)**, region III). This is due to the net protonation of  $OAc^-$  being turned on, which allows for the unfettered flow of both  $OH^-$  and  $OAc^-$ . The concentration of  $OH^-$  rises in the bulk of the AEM and the concentration of  $OAc^-$  decreases as the concentration polarization from the ionic blockade is reduced. In this region, the current is expected to partition between  $OH^-$  protonation and  $OAc^-$  protonation as per their relative migration fluxes through the AEM (**Equation 3**, derivation in **Supplementary Note 4**).

$$\frac{N_{OH-}}{N_{OAc-}} = \frac{D_{OH-}c_{OH-}}{D_{OAc-}c_{OAc-}}$$

**Equation 3**

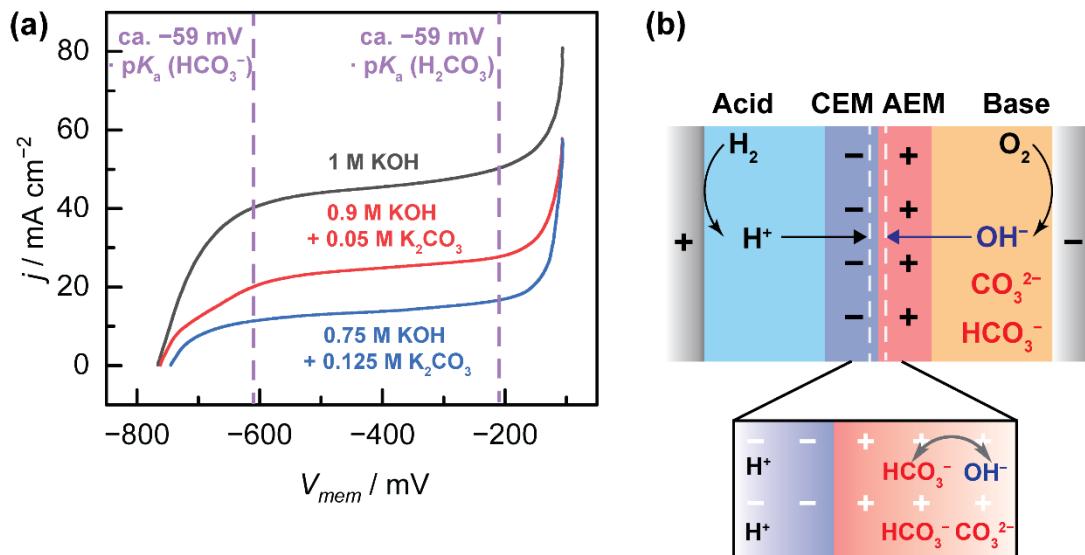
This explains the 22% FE for AcOH production (**Figure 2(c)**), which results from  $D_{OAc-}:D_{OH-} = 1:4$  when the solution  $OH^-:OAc^-$  concentration ratio is kept at 1:1. Further evidence corroborating our model of site competition comes from the open-circuit equilibration data, where we find that relative diffusive fluxes of  $OH^-$  and  $OAc^-$  control the near-interfacial composition of the AEM and the resulting  $V_{mem}$  (**Supplementary Note 5**). We note that some of the AcOH present in the AEM can be neutralized by  $OH^-$ , leading to an asymmetric concentration profile favoring AcOH diffusion into the AEM that leads to a disparity between the FE measured with our methodology (see **Methods**) compared to that predicted by **Equation 3**. Indeed, we see FEs decreasing to below ca. 20% at higher current densities (**Supplementary Figure 11; Supplementary Figure 23**), but postulate that this asymmetry in acetic acid diffusion is a minor contributor at modest current densities (**Figure 2(c)**). Collectively, our studies on electrolyte variation have established a mechanistic basis for the forward bias current-voltage behavior of BPMs containing mixed electrolytes of different acidities/basicities.

### Implications of mechanistic model for galvanic cells

The preceding mechanistic picture is relevant to a number of BPM galvanic cell types including  $H_2$  fuel cells<sup>42,43</sup> and aqueous redox flow batteries.<sup>28,29</sup> For example, BPMs can be employed in fuel cells to pair facile hydrogen oxidation kinetics in acid with the use of earth-abundant catalysts for oxygen reduction in base.<sup>42</sup> The production of water at the bipolar junction in forward bias also endows fuel cells with the property of self-humidification.<sup>42</sup> However, the operation of fuel cells can be complicated by the formation and accumulation of (bi)carbonates in the alkaline electrolyte due to exposure to ambient  $CO_2$ .<sup>35</sup>

To understand the effect of trace carbonate on the performance of a  $H_2SO_4 | KOH$  BPM fuel cell, we measured polarization curves of cells of the type  $1\text{ M }H_2SO_4 | FBM | x\text{ M }KOH + y\text{ M }K_2CO_3$  ( $x + 2y = 1$ ) (**Figure 5(a)**). We find that even with pristine KOH solutions, a limiting current region develops, due to the presence of trace carbonate from  $CO_2$  absorption. Importantly, the limiting current decreases dramatically from ca. 45 to ca.  $14\text{ mA cm}^{-2}$  as the

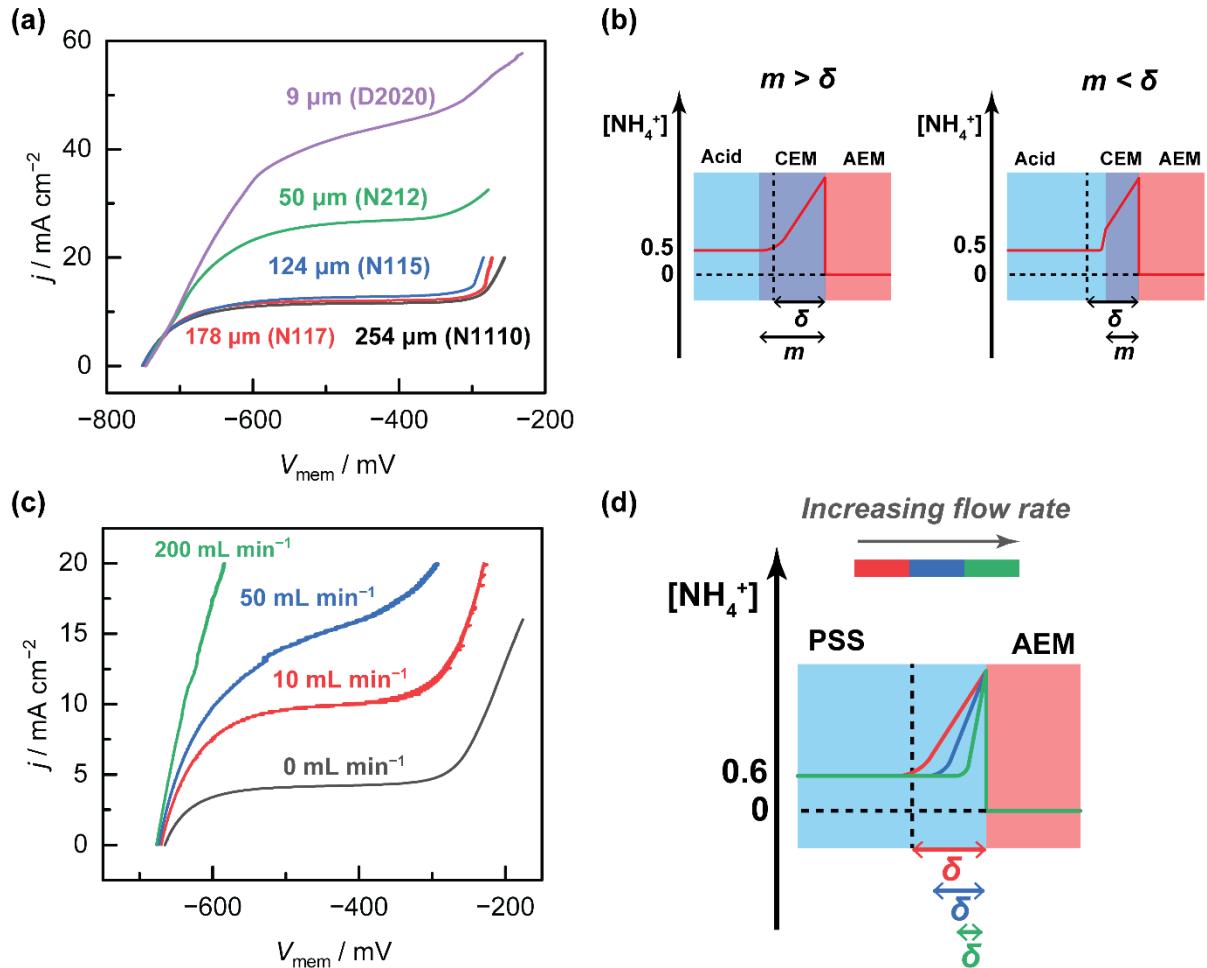
concentration of  $\text{K}_2\text{CO}_3$  present increases from trace levels to 0.125 M. Following from the model developed above, this limiting current results from the accumulation of  $\text{CO}_3^{2-}$  and  $\text{HCO}_3^-$  species at the BPM junction, inhibiting  $\text{OH}^-$  transport to the interface. In this case, it is expected that only  $\text{OH}^-$  and  $\text{CO}_3^{2-}$  are protonated at currents below the limiting current, and that  $\text{HCO}_3^-$  is only protonated at currents above the limiting current. Operating the BPM at a  $V_{\text{mem}}$  that results in bicarbonate protonation and  $\text{CO}_2$  formation is an option, but the resulting ca. 450 mV neutralization overpotential will sap the power output of the fuel cell, particularly given that the peak power point of most hydrogen fuel cells occurs in the high-current range at  $V_{\text{mem}} > -200$  mV. Importantly, ionic blockading by (bi)carbonates occurs even when these species are minority constituents of the strongly alkaline electrolyte and the bulk of the current is carried by  $\text{OH}^-$  ions (**Figure 5(b)**). In addition, gas evolution at the bipolar junction can lead to delamination, which can be problematic for conventional bipolar membranes (see below for a detailed discussion of this topic). We note that if the basic solution progressively accumulates (bi)carbonate, operating in the under-limiting and limiting regions will not clear these species from the cell, and so periodic polarization in the over-limiting region may be necessary to re-establish the hydroxide pool. Notwithstanding, our model explains the pernicious effect of even trace (bi)carbonates on the efficiency of forward bias BPM fuel cells. This motivates the development of strategies for raising the limiting current (see below) to enable access to high power densities for fuel cells as well as other galvanic devices, such as redox flow batteries (see **Supplementary Note 6**).



**Figure 5: Electrochemical characterization of BPMs with varying concentrations of  $\text{CO}_2$  dissolved in KOH.** (a) Forward bias polarization curves for the cells  $1 \text{ M H}_2\text{SO}_4 \mid \text{FBM} \mid x \text{ M KOH} + y \text{ M K}_2\text{CO}_3$  ( $x + 2y = 1$ ). Note that the current takeoff in the high current region is pinned to the  $\text{p}K_a$  of 3.49 for  $\text{H}_2\text{CO}_3$ . (b) Cell schematic showing the faradaic reactions at the electrodes and the ionic reactions within the BPM for a forward bias BPM  $\text{H}_2$  fuel cell.  $\text{CO}_3^{2-}$  and  $\text{HCO}_3^-$  ions formed from  $\text{CO}_2$  absorption into the alkaline electrolyte accumulate in the AEM and inhibit  $\text{OH}^-$  transport.

## Materials design enhances limiting current for galvanic cells

Analysis of forward bias BPM galvanic cells using our mechanistic framework revealed the importance of high limiting currents, and motivated us to explore the experimental handles that were available to control the limiting current. We first investigated the effect of varying the properties of the membrane. Using cells of the type  $0.5\text{ M NH}_4\text{Cl} + 0.5\text{ M H}_2\text{SO}_4 | \text{CEM} | \text{FAA-3-50} | 1\text{ M KOH}$ , where the CEM was varied in thickness, we observed that  $j_{\text{lim}}$  (considered at  $V_{\text{mem}} = -450\text{ mV}$ ) decreased from  $44\text{ mA cm}^{-2}$  to  $26.6\text{ mA cm}^{-2}$  as the CEM thickness increased from  $9\text{ }\mu\text{m}$  to  $124\text{ }\mu\text{m}$  (**Figure 6(a)**). However, as the CEM thickness increased past the threshold value of  $124\text{ }\mu\text{m}$  to  $178\text{ }\mu\text{m}$  and subsequently  $254\text{ }\mu\text{m}$ ,  $j_{\text{lim}}$  remained invariant at ca.  $12.5\text{ mA cm}^{-2}$  (**Figure 6(a)**). We suggest that this non-monotonic change in  $j_{\text{lim}}$  can be attributed to the relative lengthscale of the thickness of the CEM ( $m$ ) relative to the thickness of the diffusional boundary layer ( $\delta$ ) for the electrolyte exchange mechanism described in the preceding section (albeit applied to  $\text{H}^+/\text{NH}_4^+$  exchange here) (**Figure 6(b)**). Although we previously established that the overall electrolyte exchange rate depends on both the reactive and unreactive ion, for simplicity, only the concentration profile for  $\text{NH}_4^+$  has been depicted here. We note that the concentration profiles for  $\text{NH}_4^+$  and  $\text{H}^+$  should be inversely correlated, since no other counterions for the AEM exist. When  $m > \delta$ , then the diffusional boundary layer is entirely contained within the CEM and varying  $m$  has no bearing on the rate of  $\text{NH}_4^+/\text{H}^+$  exchange (**Figure 6(b)**). Conversely, when  $m < \delta$ , then variations in  $m$  result in changes in the rate of  $\text{NH}_4^+/\text{H}^+$  rate. This is due to the effective diffusion coefficient of  $\text{NH}_4^+$  being lower in the CEM than in solution, i.e.  $D_{\text{NH}_4^+}(\text{CEM}) < D_{\text{NH}_4^+}(\text{Solution})$ . Consequently, the rate of  $\text{NH}_4^+$  diffusion exchange is slower within the CEM than in solution. In addition, the ionic blockade effect of  $\text{NH}_4^+$  on  $\text{H}^+$  transport only occurs within the CEM, where there are no mobile anions occur. Hence, the smaller the value of  $m$ , the faster the net  $\text{NH}_4^+/\text{H}^+$  exchange, and the higher the value of  $j_{\text{lim}}$  (**Figure 6(b)**). This analysis brackets  $\delta$  between  $50$  and  $124\text{ }\mu\text{m}$  for the experiments in **Figure 6(a)**. These membrane thickness variation data demonstrate a materials handle for tuning  $j_{\text{lim}}$  and further support the notion that sluggish diffusion impeded by ionic place-exchange in the membrane is the origin of the limiting current.



**Figure 6: Materials design strategies to raise limiting current densities.** (a) Forward bias polarization curve of  $0.5 \text{ M H}_2\text{SO}_4 + 0.5 \text{ M NH}_4\text{Cl} \mid \text{CEM} \mid \text{AEM} \mid 1 \text{ M KOH}$ , wherein CEM thickness = 9, 50, 124, 178 or 254 µm (see **Supplementary Table 3** for list of CEMs used). (b) Putative concentration profiles for  $\text{NH}_4^+$  in the CEM and acid solution when CEM thickness ( $m$ ) is larger or smaller than the diffusional boundary layer thickness ( $\delta$ ). (c) Forward bias polarization curve of  $0.4 \text{ M PSS-H} + 0.6 \text{ M PSS-NH}_4 \mid \text{AEM} \mid 1 \text{ M KOH}$  with varying flow rates. (d) Concentration profile for  $\text{NH}_4^+$  in the PSS solution as a function of flow rate.

Finally, with mounting evidence that the limiting region is diffusively controlled, we sought to design a BPM system that afforded dynamic control over the current-voltage characteristics of the limiting region. In electrochemical systems, improved transport of species to a reactive surface of an electrode can be induced by introducing advection (e.g., by stirring the solution or the use of a rotating electrode setup).<sup>44</sup> In order to set up a system where advection could be directly applied to the bipolar interface, we employed a hybrid liquid-membrane system with the cell  $0.4 \text{ M PSS-H} + 0.6 \text{ M PSS-NH}_4 \mid \text{AEM} \mid 1 \text{ M KOH}$ , where the CEM and the  $\text{H}^+$ - and  $\text{NH}_4^+$ -containing acid solution of a conventional BPM setup are replaced with a poly(4-styrene sulfonate) ( $\text{PSS}^-$ ) solution. Owing to its high molecular weight ( $M_w$  ca. 70 kDa on average), the  $\text{PSS}^-$  co-ion is size-excluded from crossing the AEM, and is able to form a stable bipolar interface, with the PSS-H solution playing the dual role of CEM and acid solution.<sup>37</sup> With this cell type, we were able to collect polarization curves with different flow rates applied to the bipolar interface. Indeed, as the flow rate increased from 0 to  $200 \text{ mL min}^{-1}$ , the current density

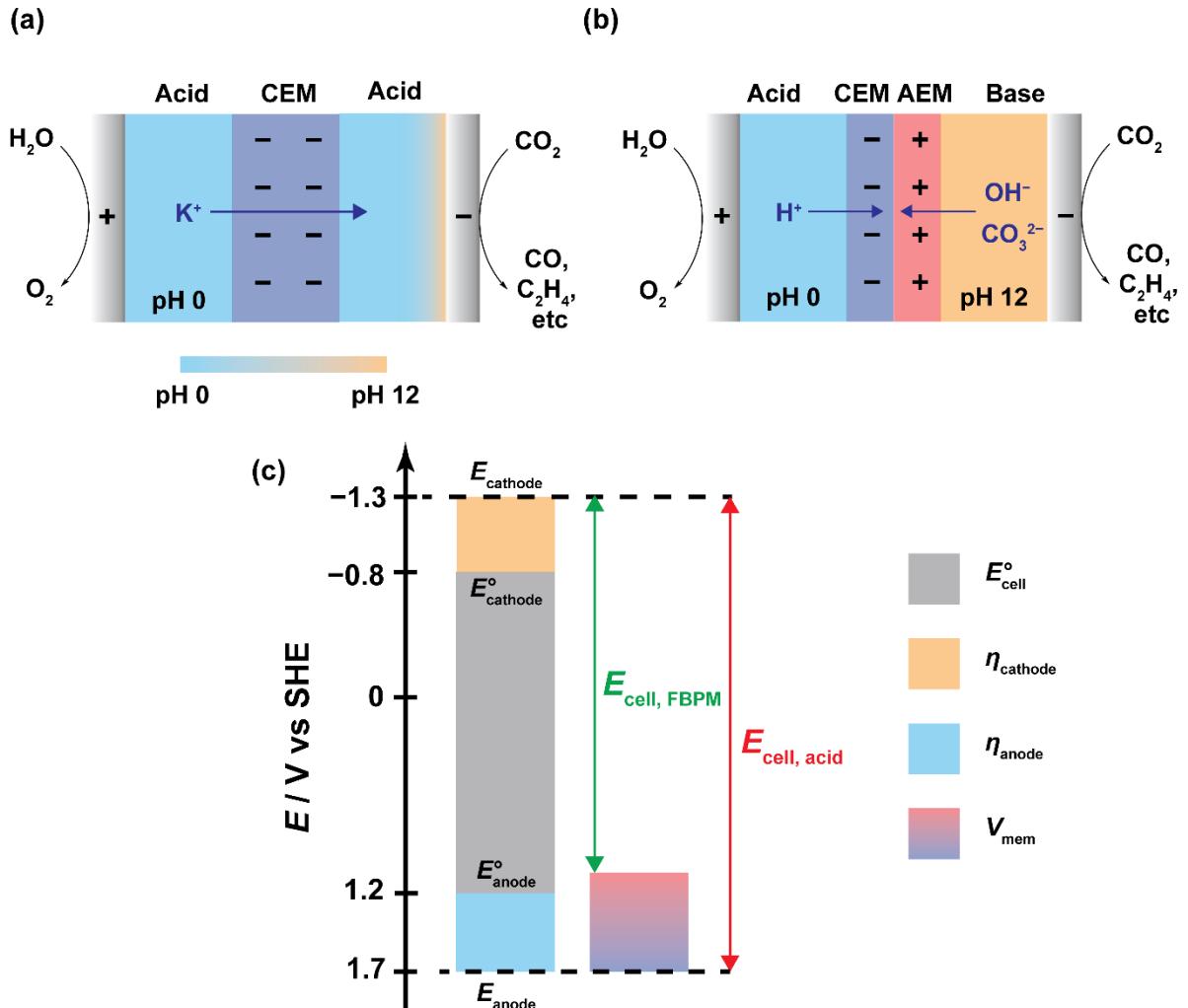
considered at the same  $V_{\text{mem}}$  of  $-600$  mV increased nearly fivefold from  $3.4 \text{ mA cm}^{-2}$  to  $17.4 \text{ mA cm}^{-2}$  (**Figure 6(c)**). Analogous to conventional hydrodynamic electrochemical methods (e.g. rotating electrodes),<sup>44</sup> this correlation can be explained by the thickness of the diffusional boundary layer shrinking with increasing flow rate, leading to steeper concentration gradients for  $\text{NH}_4^+$  and faster  $\text{H}^+/\text{NH}_4^+$  exchange rates (**Figure 6(d)**). The polyelectrolyte advection data here are in agreement with the limiting region being diffusion-controlled, and demonstrate a facile methodology for controlling the value of  $j_{\text{lim}}$  in this region.

Together, the strategies introduced above provide additional levers for managing electrolyte speciation across the BPM, mitigating the effect of ionic blockades, and decreasing overpotential losses in BPM electrochemical devices.

### Implications for forward bias BPM $\text{CO}_2$ electrolyzers

The electrocatalytic  $\text{CO}_2$  reduction reaction ( $\text{CO}_2\text{RR}$ ) enables the production of carbon-based feedstocks and fuels powered by renewable electrical energy sources, and is a keystone transformation underpinning the clean energy transition.<sup>45,46</sup> Selective  $\text{CO}_2$  reduction requires an alkaline environment at the cathode interface.<sup>47–50</sup> However, the absorption of  $\text{CO}_2$  into alkaline solutions is a thermodynamically favorable process and leads to the formation of (bi)carbonates over time, lowering the energy efficiency for electrolysis.<sup>51,52</sup> To circumvent this issue,  $\text{CO}_2$  electrolyzers operating with acidic electrolytes (**Figure 7(a)**), which avoid carbonate formation, have been developed.<sup>47–50</sup> However, these systems universally rely on the presence of alkali metal cations in the electrolyte to engineer an alkaline pH swing local to the cathode surface.<sup>51,53</sup> This leads to the development of a large pH gradient between the alkaline cathode surface and the bulk acidic electrolyte, which can add a significant but oft-overlooked concentration overpotential to the overall cell voltage. Therefore, while attractive for avoiding carbonate formation and allowing improved  $\text{CO}_2$  utilization, the operation of acidic  $\text{CO}_2$  electrolyzers invariably incurs large energy losses in the form of large pH swing overpotentials.

Forward bias BPM systems comprising a basic catholyte and an acidic anolyte have been employed in  $\text{CO}_2$  electrolyzers to enable regeneration of  $\text{CO}_2$  from carbonated electrolytes in operando and increase overall  $\text{CO}_2$  utilization (**Figure 7(b)**).<sup>54–57</sup> However, owing to the limited understanding of the mechanism of forward-bias BPM operation in carbonate electrolytes, the utilization of this device construct for energy recovery has been largely ignored.<sup>54–56</sup> In contrast to acidic  $\text{CO}_2$  electrolyzers that operate with a locally alkaline pH swing, the incorporation of a BPM between the acid and base compartments theoretically engenders the ability to transduce the chemical potential gradient into an electrical potential gradient that can offset part of the cell voltage (**Figure 7(c)**). Hence, forward bias BPM  $\text{CO}_2$  electrolyzers represent an attractive and potentially more energy-efficient alternative to acidic  $\text{CO}_2$  electrolyzers. However, the lack of understanding of forward bias operation with carbonate electrolytes impedes the development of strategies to further improve the efficiency of  $\text{CO}_2$  electrolyzers via BPM incorporation.

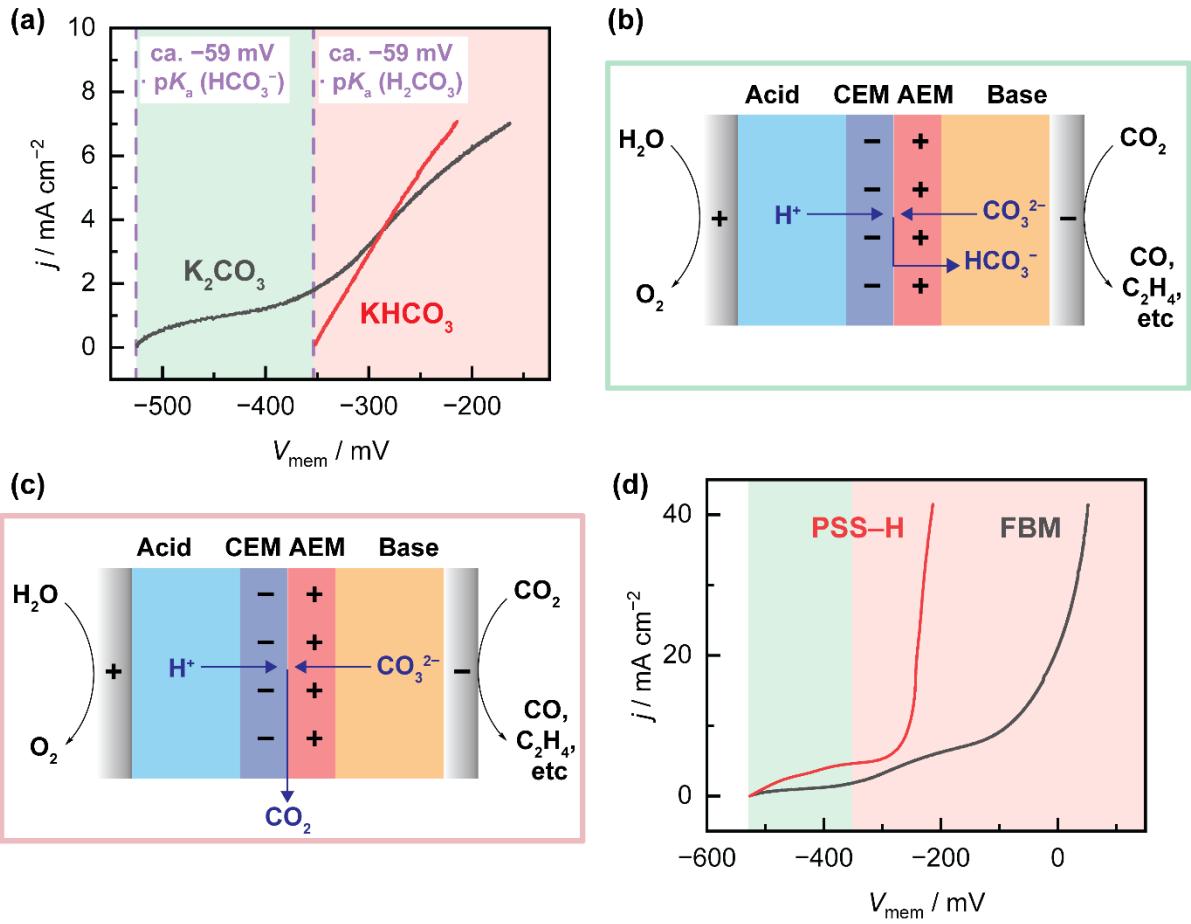


**Figure 7: Comparing pH swing and forward bias BPM CO<sub>2</sub> electrolyzers.** Cell schematics for (a) an acidic CO<sub>2</sub> electrolyzer employing an interfacial pH swing and (b) a forward bias BPM CO<sub>2</sub> electrolyzer. (c) Corresponding cell voltage breakdowns for (a) and (b), showing the voltage offset enabled by the BPM.  $E_{\text{anode}}^{\circ}$  and  $E_{\text{cathode}}^{\circ}$  refer to thermodynamic cell potentials in pH 0 and 12, respectively. Ohmic losses are assumed to be identical between the two types of cells and are not treated in this analysis. Approximate values are taken from the literature.<sup>51,53</sup>

In order to understand the intrinsic forward bias polarization behavior of a BPM cell containing (bi)carbonates, we collected polarization curves for 1 M H<sub>2</sub>SO<sub>4</sub> | 1 M K<sub>x</sub>H<sub>y</sub>CO<sub>3</sub> (x + y = 2). Analogous to the 1 M H<sub>2</sub>SO<sub>4</sub> | x M KOH + y M KOAc mixed electrolyte cells, the open-circuit  $V_{\text{mem}}$  values for the K<sub>2</sub>CO<sub>3</sub> cell and the KHCO<sub>3</sub> cell were found to pin to ca. -59 mV·pK<sub>a</sub> (HCO<sub>3</sub><sup>-</sup>) and ca. -59 mV·pK<sub>a</sub> (H<sub>2</sub>CO<sub>3</sub>) (Figure 8(a)). In addition, we observed polarization behavior for both cells that was analogous with the 1 M H<sub>2</sub>SO<sub>4</sub> | x M KOH + y M KOAc cells: the KHCO<sub>3</sub> cell showed current takeoff from the open-circuit voltage (Figure 8(a)) similar to the 1 M H<sub>2</sub>SO<sub>4</sub> | 1 M KOAc cell (Figure 2(a)), whereas the K<sub>2</sub>CO<sub>3</sub> cell exhibited a plateau current between  $V_{\text{mem}}$  values pinned to ca. -59 mV·pK<sub>a</sub> (HCO<sub>3</sub><sup>-</sup>) and ca. -59 mV·pK<sub>a</sub> (H<sub>2</sub>CO<sub>3</sub>) (Figure 8(a)), analogous to the 1 M H<sub>2</sub>SO<sub>4</sub> | x M KOH + y M KOAc (x = 0.5, y = 0.5 or x = 0.75, y = 0.25) cells (Figure 2(a)). Applying the foregoing mechanistic model, we expect that only CO<sub>3</sub><sup>2-</sup> will be protonated in net in the underlimiting and limiting regions, and that net HCO<sub>3</sub><sup>-</sup> protonation and CO<sub>2</sub> evolution can only occur at  $V_{\text{mem}} > V_{\text{pK}_a(\text{H}_2\text{CO}_3)} = \text{ca. } -380 \text{ mV}$

(**Figure 8(a)**). Operating at membrane voltages lower than this value will lead to progressive accumulation of the bicarbonate in the catholyte (**Figure 8(b)**) and thus operation at membrane voltages greater than this value is essential for continuous CO<sub>2</sub> clearance and steady state operation (**Figure 8(c)**). Consequently, the maximum electrical work recoverable is  $-380$  mV rather than the  $-710$  mV corresponding to the full 0-12 pH differential across a typical CO<sub>2</sub> electrolyzer.<sup>53,58</sup> Nonetheless, this recovered voltage is a substantial fraction (54%), of that required to sustain the pH gradient, which is otherwise lost to heat in acidic pH swing CO<sub>2</sub> electrolyzers (**Figure 7(a)**). These findings establish a quantitative basis for the expected  $V_{\text{mem}}$  for a forward bias BPM regenerating CO<sub>2</sub>, and highlight the leveling effect that the  $pK_a$  of H<sub>2</sub>CO<sub>3</sub> can have on the resultant  $V_{\text{mem}}$ .

High-current forward bias BPM operation requires efficient CO<sub>2</sub> removal. We polarized a 1 M PSS-H | AEM | 1 M K<sub>2</sub>CO<sub>3</sub> cell and found that lower overpotentials were required compared to the 1 M H<sub>2</sub>SO<sub>4</sub> | FBM | 1 M K<sub>2</sub>CO<sub>3</sub> cell at high current densities in the overlimiting region (**Figure 8(d)**). We invoke that the FBM traps small pockets of CO<sub>2</sub> within the bipolar junction that occlude the bipolar interface and reduce the total electroactive surface area, and attribute the improved electrochemical performance of the PSS-H cell to the non-trapping liquid-membrane interface formed between PSS-H and the AEM. In addition, in contrast to the FBM cells, we observe a second plateau for the 1 M H<sub>2</sub>SO<sub>4</sub> | CEM | AEM | 1 M K<sub>x</sub>H<sub>y</sub>CO<sub>3</sub> cells outfitted with homemade BPMs in the overlimiting region that is absent for the former (**Supplementary Figure 25**). We postulate that the second plateau is the result of significant CO<sub>2</sub> evolution rates severely reducing the bipolar interfacial contact area and leading to some degree of membrane delamination for the more loosely attached homemade BPMs. Alternative approaches that avoid the trapping of CO<sub>2</sub> (e.g., a porous<sup>56</sup> or microchanneled<sup>55</sup> CEM structure) have also been found to result in improved device performance, but these studies expose, for the first time, the mechanistic importance of CO<sub>2</sub> removal for optimal I-V characteristics. Taken together, these observations suggest that polarization of a (bi)carbonate-containing BPM cell in the over-limiting region can be inhibited by the trapping and accumulation of CO<sub>2</sub>, and that a hybrid liquid-membrane interface strategy can circumvent this issue by allowing rapid CO<sub>2</sub> clearance.



**Figure 8: Modes of operation for forward bias BPM  $\text{CO}_2$  electrolyzers.** (a) Forward bias polarization curve of 1 M  $\text{H}_2\text{SO}_4$  | FBM | 1 M  $\text{K}_x\text{H}_y\text{CO}_3$  (where  $x + y = 2$ ). Current-voltage regions where  $\text{HCO}_3^-$  is produced are shaded in green, and regions where  $\text{CO}_2$  is produced are shaded in red. Cell schematics and polarization curves for a forward bias BPM  $\text{CO}_2$  electrolyzer with a fully carbonated catholyte (e.g., 1 M  $\text{K}_2\text{CO}_3$ ) operating in (b) the under-limiting and limiting regions (corresponding to the green regions) and (c) the over-limiting region (corresponding to the red regions). (d) Forward bias polarization curve of 1 M PSS-H | AEM | 1 M  $\text{K}_2\text{CO}_3$  and 1 M  $\text{H}_2\text{SO}_4$  | FBM | 1 M  $\text{K}_2\text{CO}_3$ .

Revisiting BPM  $\text{CO}_2$  electrolyzers where the forward bias mode is implemented to allow the recovery of liquid products from the  $\text{CO}_2\text{RR}$ ,<sup>59,60</sup> a similar analysis can be performed for the impact of the region of operation on the speciation at the bipolar interface (**Supplementary Figure 26**). Using a  $\text{CO}_2$  electrolyzer that produces acetate in an alkaline catholyte as an example, our earlier findings (**Figure 2(c)**) reveal that acetate is only protonated at  $V_{\text{mem}} > V_{\text{p}K_a(\text{AcOH})}$  in the overlimiting region, and not in the underlimiting or limiting regions. This implication highlights two distinct modes of operation that are possible for such a device: (a) operating in the overlimiting region and continuously generating protonated liquid  $\text{CO}_2\text{RR}$  products at the bipolar interface, or (b) operating in the underlimiting and limiting regions and preferentially protonating hydroxide so as to concentrate acetate in the catholyte to enable more energy-efficient downstream separations outside the device. Operating in the concentrator mode would enable the recovery of a large  $V_{\text{mem}}$  from the pH gradient to offset the cell voltage, but would require strategies for raising  $j_{\text{lim}}$  to match the currents passed at the electrodes, which

can be accomplished via the use of a thin AEM layer or a flowing cationic polyelectrolyte (in place of the AEM) as discussed above. Hence, our studies illustrate how the current-voltage profile of the forward bias BPM platform can be a powerful atlas for manipulating ion speciation at the bipolar interface and controlling catholyte composition in a CO<sub>2</sub> electrolyzer.

## Conclusions

Herein, by systematically varying the properties of electrolyte mixtures and membranes, we establish a general mechanistic framework for understanding the forward bias current-voltage profile of weak electrolyte-containing BPM cells. We find that the net protonation of a given acid/base onsets at voltages beyond those pinned by their  $pK_a$  values. Furthermore, we reveal that an ionic blockade exerted by unreactive counterions can lead to limiting currents in forward bias. We expose the factors controlling this limiting current as well as materials design strategies for augmenting its magnitude, paving the way for designing galvanic cells that incorporate forward bias BPMs. Finally, we perform a detailed analysis on the implications of our studies to CO<sub>2</sub> electrolyzers, revealing how forward bias BPM electrolyzers can operate at lower cell voltages and higher efficiencies than acidic electrolyzers, as well as how knowledge of the current-voltage profile enables versatility in controlling ion speciation at the bipolar interface for performing liquid CO<sub>2</sub>RR product recovery.

The results here shine a spotlight on the non-linear current-voltage relationship of forward bias BPMs interfaced with electrolyte mixtures, and the large, oft-overlooked overpotentials that can arise at the bipolar junction. Particularly pernicious is the levelling effect that even trace quantities of weak acids/bases (e.g., HCO<sub>3</sub><sup>-</sup>) in the electrolyte can have on  $V_{mem}$  when they accumulate in the bipolar membrane and inhibit the transport of stronger acids and bases (e.g., OH<sup>-</sup>, CO<sub>3</sub><sup>2-</sup>), leading to large neutralization overpotentials (**Figure 5**). The limiting current density is expected to depend on the intrinsic transport rates of ions in the BPM, which is controlled by the ion exchange capacity, as well as the relative transport rates of strong and weak electrolytes. Since the ionic blockade effect ultimately stems from conventional ion-exchange membranes being highly charge-selective for counterions over coions but not chemoselective between ions of the same charge (e.g., for OH<sup>-</sup> vs OAc<sup>-</sup> or CO<sub>3</sub><sup>2-</sup> in AEMs), we suggest that the development of membranes highly chemoselective for the transport of strong electrolytes could effectively mitigate the inhibition and significantly augment limiting current densities towards technologically relevant values (>100 mA cm<sup>-2</sup>). For example, specific complexation interactions with a metal oxide have been exploited to engineer highly phosphate-selective membranes.<sup>61</sup> As a final note, although not discussed here, an important secondary consideration for forward bias operation at high current densities is the need for facile product (water, CO<sub>2</sub>, etc) removal from the bipolar interface in order to avoid membrane ballooning and delamination. Together, the conclusions presented here provide a basis for predicting and understanding the forward bias polarization of BPMs with a multiplicity of mobile ions, and pave the way for the rational design of next-generation forward bias BPM applications.

## Methods

### Chemicals and Materials.

Potassium hydroxide (KOH, 99.98%), potassium formate (HCOOK, 99%), boric acid (H<sub>3</sub>BO<sub>3</sub>, Puratronic, 99.9995%), sodium acetate (CH<sub>3</sub>COONa, 99.997%), ammonium chloride (NH<sub>4</sub>Cl, 99.999%) were purchased from Alfa Aesar and used as received. Potassium chloride (KCl, 99%), potassium acetate (CH<sub>3</sub>COOK, 99%), potassium bicarbonate (KHCO<sub>3</sub>, 99.95%), potassium phosphate monobasic (KH<sub>2</sub>PO<sub>4</sub>, 99.5%), potassium phosphate dibasic trihydrate (K<sub>2</sub>HPO<sub>4</sub>.3H<sub>2</sub>O, 99%), acetic acid (CH<sub>3</sub>COOH, glacial, 99.7%), potassium phosphate tribasic (K<sub>3</sub>PO<sub>4</sub>, >98%), ammonium acetate (CH<sub>3</sub>COONH<sub>4</sub>, 97%), trimethylamine hydrochloride (N(CH<sub>3</sub>)<sub>3</sub>.HCl, 98%), guanidine hydrochloride (CH<sub>5</sub>N<sub>3</sub>.HCl, 99%), imidazole hydrochloride (C<sub>3</sub>H<sub>4</sub>N<sub>2</sub>.HCl, >98%), pyridine hydrochloride (C<sub>5</sub>H<sub>5</sub>N.HCl, 98%), poly(sodium 4-styrenesulfonate) (PSS-Na, M<sub>w</sub> = 70,000, 30 wt. % in H<sub>2</sub>O), and poly(diallyldimethylammonium chloride) (PDADMA-Cl, M<sub>w</sub> < 100,000, 35 wt. % in H<sub>2</sub>O) were purchased from Sigma-Aldrich and used as received. Sulfuric acid (OmniTrace, 93-98%) and hydrochloric acid (OmniTrace, 34–37%) were purchased from VWR and used as received. Potassium carbonate (K<sub>2</sub>CO<sub>3</sub>, 99.995%) was purchased from Beantown Chemical and used as received. Platinum wire and mesh (99.995%) used as driving electrodes were purchased from VWR. The commercial bipolar membrane Fumasep FBM was purchased from Fuel Cell Store and stored in Millipore water before use. The CEMs Nafion 212, 115, 117 and 1110, and the AEM Fumasep FAA-3-50 were purchased from Fuel Cell Store and stored dry prior to use. Nafion D2020 (1000 EW, 20 wt% in alcohols) dispersion was purchased from Fuel Cell Store and used as received. Graphene oxide (GO) dispersion (4 wt%) was purchased from Graphenea and used as received. Dialysis tubing (molecular weight cut-off of 14,000 Da) was obtained from Ward's Science and thoroughly rinsed with Millipore water prior to use. All aqueous electrolyte solutions were prepared with type I water (EMD Millipore, 18.2 ΩM cm resistivity). Glass Ag/AgCl reference electrodes were obtained from CH Instruments and stored in 1 M KCl solution before measurements.

### Preparation of Poly(4-Styrenesulfonic Acid) (PSS-H)

PSS-H was prepared in a similar manner to a previous report.<sup>37</sup> To prepare PSS-H samples, 200 mL of a nominal 0.5 M PSS-Na solution were prepared by dilution from the purchased stock solution, transferred into dialysis tubing, and dialyzed against 800 mL of 1 M HCl for 1 h. The HCl was then discarded and replaced with fresh 1 M HCl solution. This procedure was repeated for a total of four times, with the final dialysis step carried out overnight. The dialysis tubing was then thoroughly rinsed and exhaustively dialyzed against Millipore water (with at least 10 exchanges with 1.2 L water) to remove excess HCl. The PSS-H solution was finally concentrated under reduced pressure at 50 °C on a rotary evaporator. An aliquot of this solution was analyzed as is using ICP-OES for S content, and the total volume was adjusted using the measured S concentration to prepare a 1 M PSS-H solution. <sup>1</sup>H NMR characterization performed using a 500 MHz Bruker spectrometer was consistent with a previous preparation.<sup>37</sup> The Cl<sup>-</sup> content was measured using a chloride ion selective electrode (ISE) (Hach IntelliCAL™ ISECL181 Probe) and found to be negligible (ca. 6.8 mM).

## Preparation of Bipolar Membranes

In this study, two types of bipolar membranes were used: commercial Fumasep FBMs, and homemade BPMs. The commercial FBM was typically used in scenarios where quantitative comparisons of limiting currents were required, since it was less prone to sample-to-sample variation, whereas homemade BPMs were used when there was a need to vary the characteristics (e.g. thickness) of one of the ionomer components of the BPM.

Homemade BPMs were prepared by sequential layering of a GO water dissociation catalyst onto an AEM followed by a Nafion ionomeric binder and a CEM. The GO and Nafion dispersions were separately sonicated for at least 1 hour before being coated onto membranes. The FAA-3-50 AEM (3 cm x 3 cm) was heated on a hot plate at 70 °C for 5 minutes while keeping the PET backing intact. 0.5 mL of the GO dispersion were then airbrushed onto the AEM (GO loading = 0.15 – 0.2 mg/cm<sup>2</sup>) using an Iwata CM-SB spray gun manipulated with a custom CNC set-up. GO was included as a water dissociation reaction (WDR) catalyst in order to facilitate WDR kinetics and pin the WDR onset potential to ca. –830 mV, and the loading used here was found to be optimal based on a previous report.<sup>62</sup> The GO | AEM composite was then mounted on a glass slide using Kapton tape, and 0.35 mL of Nafion dispersion was spin-coated on at 3000 rpm for 30 s. The Nafion-coated GO | AEM was subsequently dried at 60 °C for 2 min. The Nafion ionomer coating was included to improve the interfacial contact between the CEM and the GO | AEM layers and improve the reproducibility of electrochemical measurements. The Nafion CEM was pressed by hand onto the Nafion-coated GO | AEM between a pair of clean glass slides. Caution was taken to prevent the trapping of air bubbles. The Kapton tape and backing foil on the AEM were then removed, yielding the ready-to-use BPM.

To prepare the 9 µm CEM for the thickness dependence study in **Figure 6(a)**, 2 mL of a 3.15 wt% Nafion D2020 dispersion made by dilution of the 20 wt% stock with isopropyl alcohol was airbrushed onto the GO | AEM composite in place of the spin-coated D2020 layer. The resulting BPM was then dried at 60 °C for 15 min prior to electrochemical measurements. The thickness of the CEM layer was determined via profilometry (Bruker DektakXT) on a silicon wafer coated with a Nafion film prepared in the exact same manner.

## General Electrochemical Methods

The voltage across the BPM was probed using a four-electrode setup (**Supplementary Figure 1**). For all experiments, the area of the BPM exposed between the two solution compartments was 2 cm<sup>2</sup>. In polarization experiments, two glass Ag/AgCl reference electrodes were installed at the ends of the Luggin capillaries. The tips of the capillaries were positioned about 0.5 cm from the BPM surface. Platinum meshes or wires were used as cathode and anode, and each compartment was vented to prevent the build-up of gas during polarization. Acid solutions were added to the compartment facing the CEM, and base solutions were added to the compartment facing the AEM. All electrochemical measurements were performed on either a BioLogic VMP-300 or Gamry Reference 600 potentiostat, and were conducted at ambient temperature (24 ± 1 °C). All glassware and Pt meshes/wires used were cleaned by soaking in a 1:1 mixture by volume of concentrated HNO<sub>3</sub> and H<sub>2</sub>SO<sub>4</sub> for at least 30 min before use. For all electrochemical experiments, the  $V_{mem}$  values reported were compensated by the drift between the Ag/AgCl reference electrodes measured in a two-electrode setup in 1 M KCl beforehand (typically < 5 mV).

## Galvanodynamic Polarization

To obtain the forward and reverse bias polarization curves, galvanodynamic scans were recorded using a scan rate of  $10 \mu\text{A cm}^{-2} \text{s}^{-1}$  on either a BioLogic VMP-3 or Gamry REF 600 potentiostat. This scan rate was compared to independent chronopotentiometry measurements and determined to be sufficiently slow to capture steady-state polarization behavior. In cases for which both forward and reverse bias curves needed to be collected, the latter was always collected first since the formation of water and other products in forward bias could delaminate the BPM and affect performance. All polarization curves were typically corrected for Ohmic losses ( $iR_u$ ) post-experiment using 80 – 90% of uncompensated resistance ( $R_u$ ) values determined using the Current Interrupt (CI) program on the BioLogic VMP-3 or the galvanostatic electrochemical impedance spectroscopy (GEIS) program on the Gamry REF 600.

## Quantitative $^1\text{H}$ NMR for Determination of Acetic Acid Concentration and Faradaic Efficiency

Experiments to determine the Faradaic efficiency for AcOH production in the various regions of the forward bias polarization curve were performed as follows. A BPM cell containing 20 mL solutions in the acid and base compartments respectively was polarized galvanostatically until a given quantity of charge had been passed. For the data point in the limiting region, the cell was polarized potentiostatically instead to ensure that it would fall within the narrow current range of the limiting region. The duration of polarization was chosen to ensure that the resulting concentration of AcOH produced in the acid compartment would be well above the limit of detection for NMR quantitation assuming a 1% Faradaic efficiency (FE). For all polarizations, this 1% FE threshold represented  $> 1 \text{ mM}$  of AcOH produced in the cell. 250  $\mu\text{L}$  aliquots were collected from the acid compartment of the cell at the end of each polarization, and 50  $\mu\text{L}$  of each aliquot were added to 450  $\mu\text{L}$  of a calibrant mixture composed of 8 parts 1 M HCl, 1 part  $\text{D}_2\text{O}$ , and 1 part 0.1 M DMSO (aq) as the internal standard. All NMR spectra were collected on a 500 MHz Bruker spectrometer.

Faradaic efficiencies for AcOH production were calculated as follows.

Faradaic Efficiency for AcOH

$$= 2 * \frac{\text{Concentration of AcOH produced} * \text{Volume of acid compartment}}{\text{Charge passed} * F} * 100\%$$

where the factor of 2 is included under the assumption that AcOH produced has equal probability of diffusing either through the CEM into the acid compartment or through the AEM into the base compartment. The volumes used in these calculations were adjusted according to the changes that occurred upon withdrawing aliquots.

## Polyelectrolyte Advection Experiment

The influence of polyelectrolyte advection was examined by flowing the anolyte in the cell set-up depicted in **Supplementary Figure 2**. 0.4 M PSS-H + 0.6 M PSS-NH<sub>4</sub> solution was

prepared by addition of 0.639 mL of 28% ammonium hydroxide solution to 15 mL of 1 M PSS-H solution. Advection of the PSS-H/NH<sub>4</sub> electrolyte mixture was carried out by flowing the solution with a peristaltic pump through a custom 3D-printed adapter (Formlabs Form 3+) attached in-between the ports of a glass H-cell (**Supplementary Figure 2(a)**). An additional CEM was installed in order to confine advection to a small pocket of electrolyte contained within the adapter, between the CEM and the AEM. Electrolyte was recirculated between the flow adapter and a glass half-cell containing a reservoir of PSS-H/NH<sub>4</sub>. The voltage measurement was performed between a reference electrode in contact with the PSS-H/NH<sub>4</sub> solution within the flow adapter (RE1) and a reference electrode in the KOH solution (RE2), and hence was not sensitive to any potential drops between the CEM and PSS-H/NH<sub>4</sub> solution. The exposed AEM surface area was 1 cm<sup>2</sup>. The assembled cell with its electrolyte flow circuit is shown in **Supplementary Figure 2(b)**.

## **Data availability**

The data that support the findings of this study are included in the published article and its Supplementary Information. Source data are provided with this paper.

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## **Author contributions**

W.L.T., H.D. and Y.S. conceptualized the project. W.L.T., H.D., A.C., and E.S. conducted experiments. W.L.T., H.D. and Y.S. wrote and edited the manuscript.

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## **Ethics declaration**

The authors declare no competing interest

## References

- (1) Gileadi, E. *Physical Electrochemistry: Fundamentals, Techniques and Applications*; Wiley-VCH: Weinheim, 2011.
- (2) Tributsch, H.; Pohlmann, L. Electron Transfer: Classical Approaches and New Frontiers. *Science*. **1998**, 279 (5358), 1891–1895. <https://doi.org/10.1126/science.279.5358.1891>.
- (3) Kontturi, K.; Murtomäki, L.; Manzanares, J. A. *Ionic Transport Processes*; Oxford University Press, 2008; Vol. 9780199533.
- (4) Pärnamäe, R.; Mareev, S.; Nikonenko, V.; Melnikov, S.; Sheldeshov, N.; Zabolotskii, V.; Hamelers, H. V. M.; Tedesco, M. Bipolar Membranes: A Review on Principles, Latest Developments, and Applications. *J. Memb. Sci.* **2021**, 617, 118538. <https://doi.org/10.1016/j.memsci.2020.118538>.
- (5) Giesbrecht, P. K.; Freund, M. S. Recent Advances in Bipolar Membrane Design and Applications. *Chem. Mater.* **2020**, 32 (19), 8060–8090. <https://doi.org/10.1021/acs.chemmater.0c02829>.
- (6) Blommaert, M. A.; Aili, D.; Tufa, R. A.; Li, Q.; Smith, W. A.; Vermaas, D. A. Insights and Challenges for Applying Bipolar Membranes in Advanced Electrochemical Energy Systems. *ACS Energy Lett.* **2021**, 6, 2539–2548. <https://doi.org/10.1021/acsenergylett.1c00618>.
- (7) Tufa, R. A.; Blommaert, M. A.; Chanda, D.; Li, Q.; Vermaas, D. A.; Aili, D. Bipolar Membrane and Interface Materials for Electrochemical Energy Systems. *ACS Appl. Energy Mater.* **2021**, 4 (8), 7419–7439. <https://doi.org/10.1021/acsaelm.1c01140>.
- (8) Yan, Z.; Mallouk, T. E. Bipolar Membranes for Ion Management in (Photo)Electrochemical Energy Conversion. *Accounts Mater. Res.* **2021**, 2 (12), 1156–1166. <https://doi.org/10.1021/accountsmr.1c00113>.
- (9) Simons, R.; Khanarian, G. Water Dissociation in Bipolar Membranes: Experiments and Theory. *J. Membr. Biol.* **1978**, 38 (1–2), 11–30. <https://doi.org/10.1007/BF01875160>.
- (10) Ramírez, P.; Rapp, H.-J.; Mafé, S.; Bauer, B. Bipolar Membranes under Forward and Reverse Bias Conditions. Theory vs. Experiment. *J. Electroanal. Chem.* **1994**, 375 (1–2), 101–108. [https://doi.org/10.1016/0022-0728\(94\)03379-X](https://doi.org/10.1016/0022-0728(94)03379-X).
- (11) McDonald, M. B.; Ardo, S.; Lewis, N. S.; Freund, M. S. Use of Bipolar Membranes for Maintaining Steady-State PH Gradients in Membrane-Supported, Solar-Driven Water Splitting. *ChemSusChem* **2014**, 7 (11), 3021–3027. <https://doi.org/10.1002/cssc.201402288>.
- (12) Vargas-Barbosa, N. M.; Geise, G. M.; Hickner, M. A.; Mallouk, T. E. Assessing the Utility of Bipolar Membranes for Use in Photoelectrochemical Water-Splitting Cells. *ChemSusChem* **2014**, 7 (11), 3017–3020. <https://doi.org/10.1002/cssc.201402535>.
- (13) Luo, J.; Vermaas, D. A.; Bi, D.; Hagfeldt, A.; Smith, W. A.; Grätzel, M. Bipolar Membrane-Assisted Solar Water Splitting in Optimal PH. *Adv. Energy Mater.* **2016**, 6 (13), 1600100. <https://doi.org/10.1002/aenm.201600100>.

(14) Mayerhöfer, B.; McLaughlin, D.; Böhm, T.; Hegelheimer, M.; Seeberger, D.; Thiele, S. Bipolar Membrane Electrode Assemblies for Water Electrolysis. *ACS Appl. Energy Mater.* **2020**, *3* (10), 9635–9644. <https://doi.org/10.1021/acsaem.0c01127>.

(15) Oener, S. Z.; Foster, M. J.; Boettcher, S. W. Accelerating Water Dissociation in Bipolar Membranes and for Electrocatalysis. *Science*. **2020**, *369* (6507), 1099–1103. <https://doi.org/10.1126/science.aaz1487>.

(16) Oener, S. Z.; Twilight, L. P.; Lindquist, G. A.; Boettcher, S. W. Thin Cation-Exchange Layers Enable High-Current-Density Bipolar Membrane Electrolyzers via Improved Water Transport. *ACS Energy Lett.* **2021**, *6* (1), 1–8. <https://doi.org/10.1021/acsenergylett.0c02078>.

(17) Vermaas, D. A.; Smith, W. A. Synergistic Electrochemical CO<sub>2</sub> Reduction and Water Oxidation with a Bipolar Membrane. *ACS Energy Lett.* **2016**, *1* (6), 1143–1148. <https://doi.org/10.1021/acsenergylett.6b00557>.

(18) Li, Y. C.; Zhou, D.; Yan, Z.; Gonçalves, R. H.; Salvatore, D. A.; Berlinguette, C. P.; Mallouk, T. E. Electrolysis of CO<sub>2</sub> to Syngas in Bipolar Membrane-Based Electrochemical Cells. *ACS Energy Lett.* **2016**, *1* (6), 1149–1153. <https://doi.org/10.1021/acsenergylett.6b00475>.

(19) Zhou, X.; Liu, R.; Sun, K.; Chen, Y.; Verlage, E.; Francis, S. A.; Lewis, N. S.; Xiang, C. Solar-Driven Reduction of 1 Atm of CO<sub>2</sub> to Formate at 10% Energy-Conversion Efficiency by Use of a TiO<sub>2</sub>-Protected III–V Tandem Photoanode in Conjunction with a Bipolar Membrane and a Pd/C Cathode. *ACS Energy Lett.* **2016**, *1* (4), 764–770. <https://doi.org/10.1021/acsenergylett.6b00317>.

(20) Salvatore, D. A.; Weekes, D. M.; He, J.; Dettelbach, K. E.; Li, Y. C.; Mallouk, T. E.; Berlinguette, C. P. Electrolysis of Gaseous CO<sub>2</sub> to CO in a Flow Cell with a Bipolar Membrane. *ACS Energy Lett.* **2018**, *3* (1), 149–154. <https://doi.org/10.1021/acsenergylett.7b01017>.

(21) Pătru, A.; Binninger, T.; Pribyl, B.; Schmidt, T. J. Design Principles of Bipolar Electrochemical Co-Electrolysis Cells for Efficient Reduction of Carbon Dioxide from Gas Phase at Low Temperature. *J. Electrochem. Soc.* **2019**, *166* (2), F34–F43. <https://doi.org/10.1149/2.1221816jes>.

(22) Blommaert, M. A.; Sharifian, R.; Shah, N.; Nesbitt, N.; Smith, W.; Vermaas, D. A. Orientation of Bipolar Membrane Determines the Dominant Ion and Carbonic Species Transport in Membrane Electrode Assemblies for CO<sub>2</sub> Reduction. *J. Mater. Chem. A* **2021**. <https://doi.org/10.1039/D0TA12398F>.

(23) Siritanaratkul, B.; Forster, M.; Greenwell, F.; Sharma, P. K.; Yu, E. H.; Cowan, A. J. Zero-Gap Bipolar Membrane Electrolyzer for Carbon Dioxide Reduction Using Acid-Tolerant Molecular Electrocatalysts. *J. Am. Chem. Soc.* **2022**, *144* (17), 7551–7556. <https://doi.org/10.1021/jacs.1c13024>.

(24) Xie, K.; Miao, R. K.; Ozden, A.; Liu, S.; Chen, Z.; Dinh, C.; Huang, J. E.; Xu, Q.; Gabardo, C. M.; Lee, G.; Edwards, J. P.; O'Brien, C. P.; Boettcher, S. W.; Sinton, D.; Sargent, E. H. Bipolar Membrane Electrolyzers Enable High Single-Pass CO<sub>2</sub> Electroreduction to Multicarbon Products. *Nat. Commun.* **2022**, *13* (1), 3609. <https://doi.org/10.1038/s41467-022-31295-3>.

(25) Sullivan, I.; Goryachev, A.; Digdaya, I. A.; Li, X.; Atwater, H. A.; Vermaas, D. A.;

Xiang, C. Coupling Electrochemical CO<sub>2</sub> Conversion with CO<sub>2</sub> Capture. *Nat. Catal.* **2021**, *4* (11), 952–958. <https://doi.org/10.1038/s41929-021-00699-7>.

(26) Sharifian, R.; Wagterveld, R. M.; Digdaya, I. A.; Xiang, C.; Vermaas, D. A. Electrochemical Carbon Dioxide Capture to Close the Carbon Cycle. *Energy Environ. Sci.* **2021**, *14* (2), 781–814. <https://doi.org/10.1039/D0EE03382K>.

(27) Ding, Y.; Cai, P.; Wen, Z. Electrochemical Neutralization Energy: From Concept to Devices. *Chem. Soc. Rev.* **2021**, *50* (3), 1495–1511. <https://doi.org/10.1039/D0CS01239D>.

(28) Yan, Z.; Wycisk, R. J.; Metlay, A. S.; Xiao, L.; Yoon, Y.; Pintauro, P. N.; Mallouk, T. E. High-Voltage Aqueous Redox Flow Batteries Enabled by Catalyzed Water Dissociation and Acid–Base Neutralization in Bipolar Membranes. *ACS Cent. Sci.* **2021**, *7* (6), 1028–1035. <https://doi.org/10.1021/acscentsci.1c00217>.

(29) Metlay, A. S.; Chyi, B.; Yoon, Y.; Wycisk, R. J.; Pintauro, P. N.; Mallouk, T. E. Three-Chamber Design for Aqueous Acid–Base Redox Flow Batteries. *ACS Energy Lett.* **2022**, *7* (3), 908–913. <https://doi.org/10.1021/acsenergylett.2c00040>.

(30) Pärnamäe, R.; Gurreri, L.; Post, J.; van Egmond, W. J.; Culcasi, A.; Saakes, M.; Cen, J.; Goosen, E.; Tamburini, A.; Vermaas, D. A.; Tedesco, M. The Acid–Base Flow Battery: Sustainable Energy Storage via Reversible Water Dissociation with Bipolar Membranes. *Membranes (Basel)*. **2020**, *10* (12), 409. <https://doi.org/10.3390/membranes10120409>.

(31) Al-Dhubhani, E.; Pärnamäe, R.; Post, J. W.; Saakes, M.; Tedesco, M. Performance of Five Commercial Bipolar Membranes under Forward and Reverse Bias Conditions for Acid–Base Flow Battery Applications. *J. Memb. Sci.* **2021**, *7*, 119748. <https://doi.org/10.1016/j.memsci.2021.119748>.

(32) Bui, J. C.; Digdaya, I.; Xiang, C.; Bell, A. T.; Weber, A. Z. Understanding Multi-Ion Transport Mechanisms in Bipolar Membranes. *ACS Appl. Mater. Interfaces* **2020**, *12* (47), 52509–52526. <https://doi.org/10.1021/acsami.0c12686>.

(33) Mitchell, J. B.; Chen, L.; Langworthy, K.; Fabrizio, K.; Boettcher, S. W. Catalytic Proton–Hydroxide Recombination for Forward-Bias Bipolar Membranes. *ACS Energy Lett.* **2022**, *7* (11), 3967–3973. <https://doi.org/10.1021/acsenergylett.2c02043>.

(34) Sokirko, A. V.; Ramírez, P.; Manzanares, J. A.; Mafés, S. Modeling of Forward and Reverse Bias Conditions in Bipolar Membranes. *Berichte der Bunsengesellschaft für Phys. Chemie* **1993**, *97* (8), 1040–1048. <https://doi.org/10.1002/bbpc.19930970814>.

(35) Ziv, N.; Mustain, W. E.; Dekel, D. R. The Effect of Ambient Carbon Dioxide on Anion-Exchange Membrane Fuel Cells. *ChemSusChem* **2018**, *11* (7), 1136–1150. <https://doi.org/10.1002/cssc.201702330>.

(36) Lee, M.-Y.; Park, K. T.; Lee, W.; Lim, H.; Kwon, Y.; Kang, S. Current Achievements and the Future Direction of Electrochemical CO<sub>2</sub> Reduction: A Short Review. *Crit. Rev. Environ. Sci. Technol.* **2020**, *50* (8), 769–815. <https://doi.org/10.1080/10643389.2019.1631991>.

(37) Dinh, H. Q.; Toh, W. L.; Chu, A. T.; Surendranath, Y. Neutralization Short-Circuiting with Weak Electrolytes Erodes the Efficiency of Bipolar Membranes. *ACS Appl. Mater. Interfaces* **2023**, *15* (3), 4001–4010. <https://doi.org/10.1021/acsami.2c18685>.

(38) Vermaas, D. A.; Wiegman, S.; Nagaki, T.; Smith, W. A. Ion Transport Mechanisms in Bipolar Membranes for (Photo)Electrochemical Water Splitting. *Sustain. Energy Fuels* **2018**, *2* (9), 2006–2015. <https://doi.org/10.1039/C8SE00118A>.

(39) Haynes, W. M.; Lide, D. R.; Bruno, T. J. *CRC Handbook of Chemistry and Physics*, 97th ed.; CRC Press, 2016. <https://doi.org/10.1201/9781315380476>.

(40) Grew, K. N.; McClure, J. P.; Chu, D.; Kohl, P. A.; Ahlfield, J. M. Understanding Transport at the Acid-Alkaline Interface of Bipolar Membranes. *J. Electrochem. Soc.* **2016**, *163* (14), F1572–F1587. <https://doi.org/10.1149/2.0941614jes>.

(41) Marioni, N.; Zhang, Z.; Zofchak, E. S.; Sachar, H. S.; Kadulkar, S.; Freeman, B. D.; Ganesan, V. Impact of Ion–Ion Correlated Motion on Salt Transport in Solvated Ion Exchange Membranes. *ACS Macro Lett.* **2022**, *11* (11), 1258–1264. <https://doi.org/10.1021/acsmacrolett.2c00361>.

(42) Ünlü, M.; Zhou, J.; Kohl, P. A. Hybrid Anion and Proton Exchange Membrane Fuel Cells. *J. Phys. Chem. C* **2009**, *113* (26), 11416–11423. <https://doi.org/10.1021/jp903252u>.

(43) Daud, S. S.; Norrdin, M. A.; Jaafar, J.; Sudirman, R. The Effect of Material on Bipolar Membrane Fuel Cell Performance: A Review. *IOP Conf. Ser. Mater. Sci. Eng.* **2020**, *736* (3), 032003. <https://doi.org/10.1088/1757-899X/736/3/032003>.

(44) Bard, A. J.; Faulkner, L. R. *Electrochemical Methods: Fundamentals and Applications*, 2nd ed.; John Wiley & Sons: New York, 2001. <https://doi.org/10.1016/B978-0-12-381373-2.00056-9>.

(45) Chu, S.; Cui, Y.; Liu, N. The Path towards Sustainable Energy. *Nat. Mater.* **2017**, *16* (1), 16–22. <https://doi.org/10.1038/nmat4834>.

(46) De Luna, P.; Hahn, C.; Higgins, D.; Jaffer, S. A.; Jaramillo, T. F.; Sargent, E. H. What Would It Take for Renewably Powered Electrosynthesis to Displace Petrochemical Processes? *Science*. **2019**, *364* (6438). <https://doi.org/10.1126/science.aav3506>.

(47) Zhang, Y.-J.; Sethuraman, V.; Michalsky, R.; Peterson, A. A. Competition between CO 2 Reduction and H 2 Evolution on Transition-Metal Electrocatalysts. *ACS Catal.* **2014**, *4* (10), 3742–3748. <https://doi.org/10.1021/cs5012298>.

(48) Wuttig, A.; Yaguchi, M.; Motobayashi, K.; Osawa, M.; Surendranath, Y. Inhibited Proton Transfer Enhances Au-Catalyzed CO 2 -to-Fuels Selectivity. *Proc. Natl. Acad. Sci.* **2016**, *113* (32), E4585–E4593. <https://doi.org/10.1073/pnas.1602984113>.

(49) Ooka, H.; Figueiredo, M. C.; Koper, M. T. M. Competition between Hydrogen Evolution and Carbon Dioxide Reduction on Copper Electrodes in Mildly Acidic Media. *Langmuir* **2017**, *33* (37), 9307–9313. <https://doi.org/10.1021/acs.langmuir.7b00696>.

(50) Goyal, A.; Marcandalli, G.; Mints, V. A.; Koper, M. T. M. Competition between CO 2 Reduction and Hydrogen Evolution on a Gold Electrode under Well-Defined Mass Transport Conditions. *J. Am. Chem. Soc.* **2020**, *142* (9), 4154–4161. <https://doi.org/10.1021/jacs.9b10061>.

(51) Rabinowitz, J. A.; Kanan, M. W. The Future of Low-Temperature Carbon Dioxide Electrolysis Depends on Solving One Basic Problem. *Nat. Commun.* **2020**, *11* (1), 5231. <https://doi.org/10.1038/s41467-020-19135-8>.

(52) Xie, K.; Ozden, A.; Miao, R. K.; Li, Y.; Sinton, D.; Sargent, E. H. Eliminating the Need for Anodic Gas Separation in CO<sub>2</sub> Electroreduction Systems via Liquid-to-Liquid Anodic Upgrading. *Nat. Commun.* **2022**, *13* (1), 3070. <https://doi.org/10.1038/s41467-022-30677-x>.

(53) Huang, J. E.; Li, F.; Ozden, A.; Sedighian Rasouli, A.; García de Arquer, F. P.; Liu, S.; Zhang, S.; Luo, M.; Wang, X.; Lum, Y.; Xu, Y.; Bertens, K.; Miao, R. K.; Dinh, C.-T.; Sinton, D.; Sargent, E. H. CO<sub>2</sub> Electrolysis to Multicarbon Products in Strong Acid. *Science* **2021**, *372* (6546), 1074–1078. <https://doi.org/10.1126/science.abg6582>.

(54) O'Brien, C. P.; Miao, R. K.; Liu, S.; Xu, Y.; Lee, G.; Robb, A.; Huang, J. E.; Xie, K.; Bertens, K.; Gabardo, C. M.; Edwards, J. P.; Dinh, C.; Sargent, E. H.; Sinton, D. Single Pass CO<sub>2</sub> Conversion Exceeding 85% in the Electrosynthesis of Multicarbon Products via Local CO<sub>2</sub> Regeneration. *ACS Energy Lett.* **2021**, *6* (8), 2952–2959. <https://doi.org/10.1021/acsenergylett.1c01122>.

(55) Xu, Y.; Miao, R. K.; Edwards, J. P.; Liu, S.; O'Brien, C. P.; Gabardo, C. M.; Fan, M.; Huang, J. E.; Robb, A.; Sargent, E. H.; Sinton, D. A Microchanneled Solid Electrolyte for Carbon-Efficient CO<sub>2</sub> Electrolysis. *Joule* **2022**, *6* (6), 1333–1343. <https://doi.org/10.1016/j.joule.2022.04.023>.

(56) Kim, J. Y. ‘Timothy’; Zhu, P.; Chen, F.-Y.; Wu, Z.-Y.; Cullen, D. A.; Wang, H. Recovering Carbon Losses in CO<sub>2</sub> Electrolysis Using a Solid Electrolyte Reactor. *Nat. Catal.* **2022**, *5* (4), 288–299. <https://doi.org/10.1038/s41929-022-00763-w>.

(57) Ozden, A.; García de Arquer, F. P.; Huang, J. E.; Wicks, J.; Sisler, J.; Miao, R. K.; O'Brien, C. P.; Lee, G.; Wang, X.; Ip, A. H.; Sargent, E. H.; Sinton, D. Carbon-Efficient Carbon Dioxide Electrolysers. *Nat. Sustain.* **2022**, *5* (7), 563–573. <https://doi.org/10.1038/s41893-022-00879-8>.

(58) Qiao, Y.; Lai, W.; Huang, K.; Yu, T.; Wang, Q.; Gao, L.; Yang, Z.; Ma, Z.; Sun, T.; Liu, M.; Lian, C.; Huang, H. Engineering the Local Microenvironment over Bi Nanosheets for Highly Selective Electrocatalytic Conversion of CO<sub>2</sub> to HCOOH in Strong Acid. *ACS Catal.* **2022**, *12* (4), 2357–2364. <https://doi.org/10.1021/acscatal.1c05135>.

(59) Fan, L.; Xia, C.; Zhu, P.; Lu, Y.; Wang, H. Electrochemical CO<sub>2</sub> Reduction to High-Concentration Pure Formic Acid Solutions in an All-Solid-State Reactor. *Nat. Commun.* **2020**, *11* (1), 3633. <https://doi.org/10.1038/s41467-020-17403-1>.

(60) Miao, R. K.; Xu, Y.; Ozden, A.; Robb, A.; O'Brien, C. P.; Gabardo, C. M.; Lee, G.; Edwards, J. P.; Huang, J. E.; Fan, M.; Wang, X.; Liu, S.; Yan, Y.; Sargent, E. H.; Sinton, D. Electroosmotic Flow Steers Neutral Products and Enables Concentrated Ethanol Electroproduction from CO<sub>2</sub>. *Joule* **2021**, *5* (10), 2742–2753. <https://doi.org/10.1016/j.joule.2021.08.013>.

(61) Iddy, A.; Zarzycki, P.; Kingsbury, R.; Khor, C. M.; Ma, S.; Wang, J.; Wheeldon, I.; Ren, Z. J.; Hoek, E. M. V.; Jassby, D. A Reverse-Selective Ion Exchange Membrane for the Selective Transport of Phosphates via an Outer-Sphere Complexation–Diffusion Pathway. *Nat. Nanotechnol.* **2022**, *17* (11), 1222–1228. <https://doi.org/10.1038/s41565-022-01209-x>.

(62) Chen, Y.; Wrubel, J. A.; Klein, W. E.; Kabir, S.; Smith, W. A.; Neyerlin, K. C.; Deutsch, T. G. High-Performance Bipolar Membrane Development for Improved

Water Dissociation. *ACS Appl. Polym. Mater.* **2020**, *2* (11), 4559–4569.  
<https://doi.org/10.1021/acsapm.0c00653>.