

Optical Diagnostic for Index of Refraction Measurements across Shock Waves

Gwen Wang

PhD Student

Sensing and Technologies Laboratory, Georgia Institute of Technology

Advisor: Dr. Ellen Mazumdar, Assistant Professor

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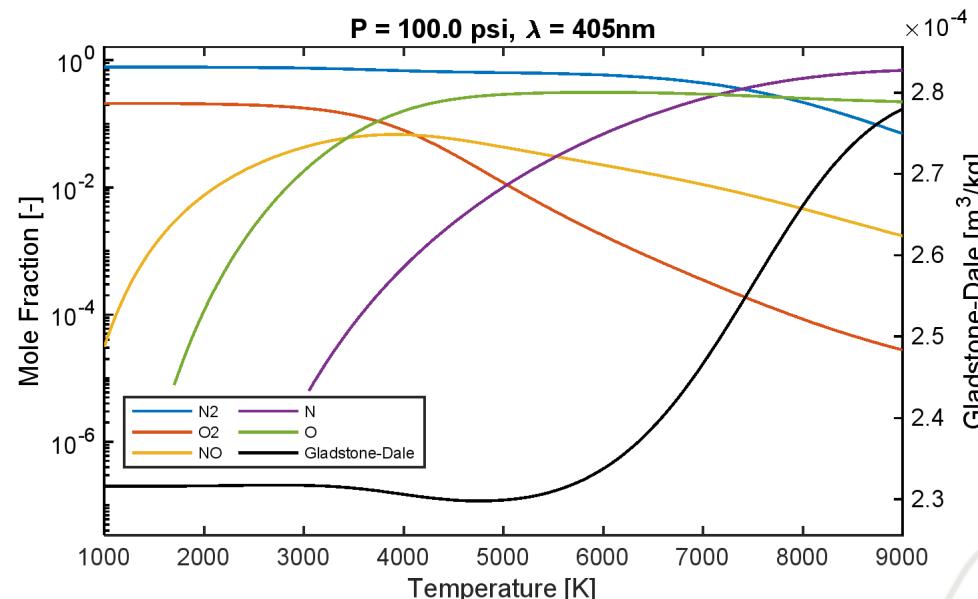
Motivation

- Dissociation at high temperatures will affect optical properties of air
- Constant Gladstone-Dale (GD) coefficient cannot be assumed
- GD has a temperature and pressure dependance
- No experimental validation
- High temperature conditions can be reached with modern shock tubes
- New diagnostics are needed to make this type of measurement

index of refraction

$$\frac{n - 1}{\rho} = GD = \sum GD_s \frac{\rho_s}{\rho}$$

density Gladstone-Dale Coefficient



Motivation

- Interferometry is used to measure index of refraction, which has wavelength and species dependence
- Composite index for gas mixtures are well tabulated values for common gas species

Post shock conditions introduces challenges

- Density changes are nearly discrete
- Low pressure \rightarrow small fringe shift number and lower uncertainties
- Moderate densities are necessary to produce measurable index change

Interferometer capable of resolving large discrete density gradients is needed

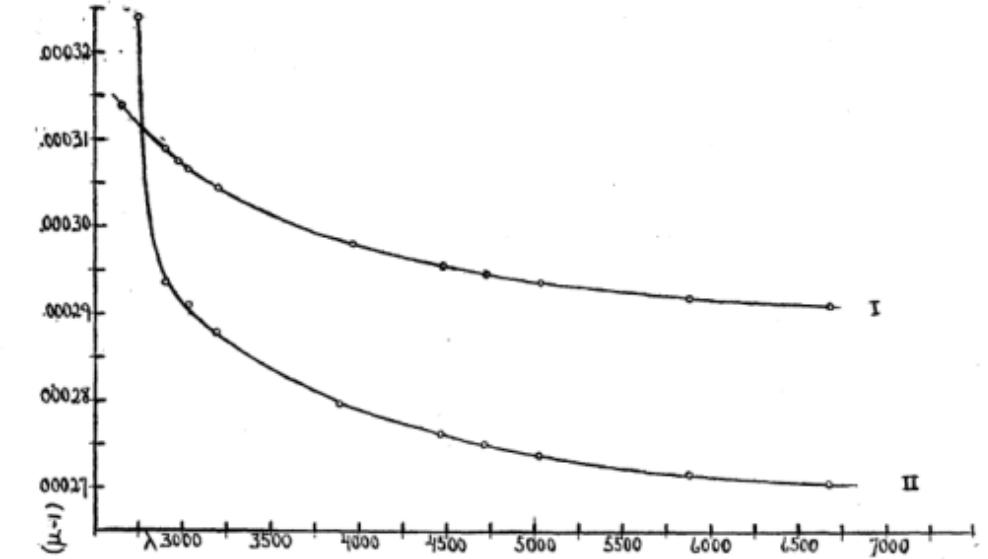
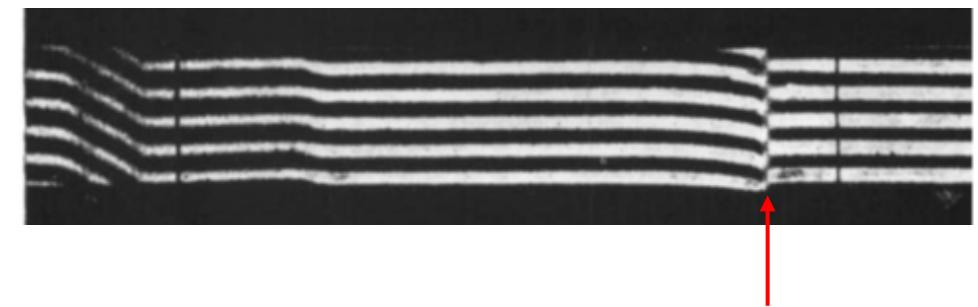
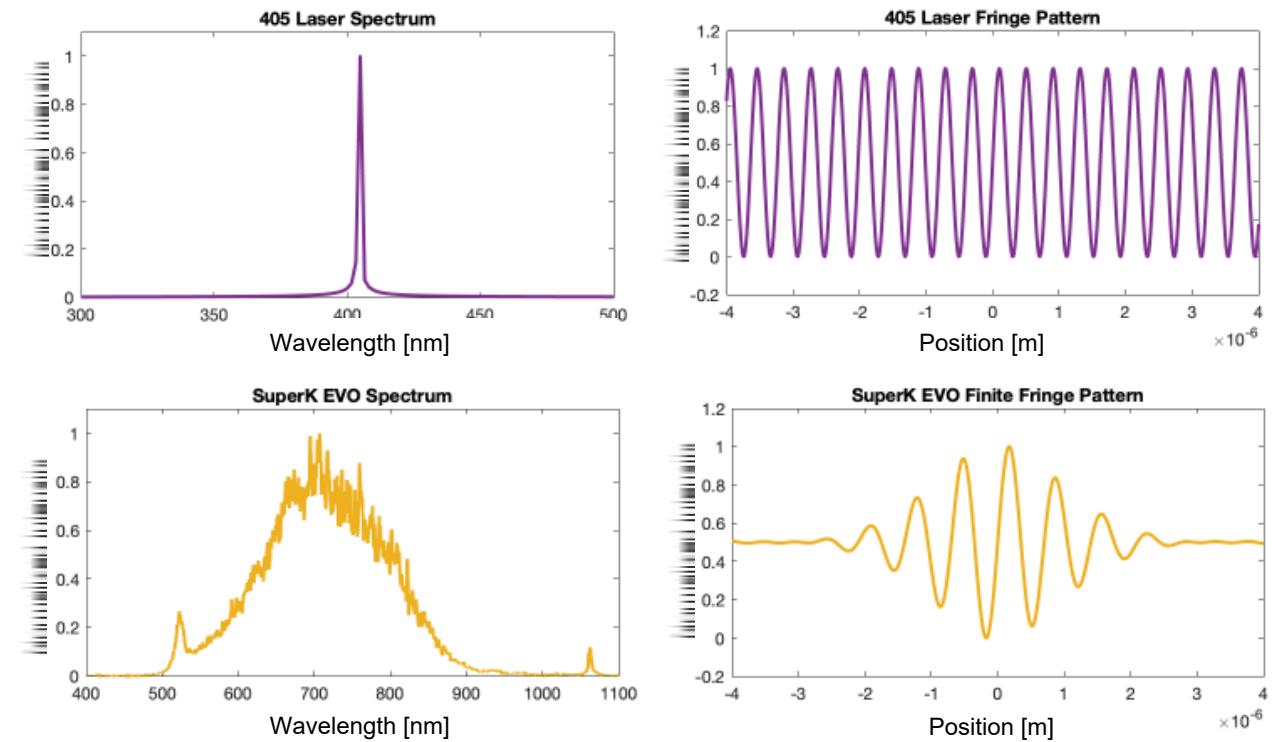


Fig. 3.
Dispersion Curves: I., Air; II., Oxygen. Abscissae: λ in Ångstrom units.
Ordinates: $(\mu - 1)$.

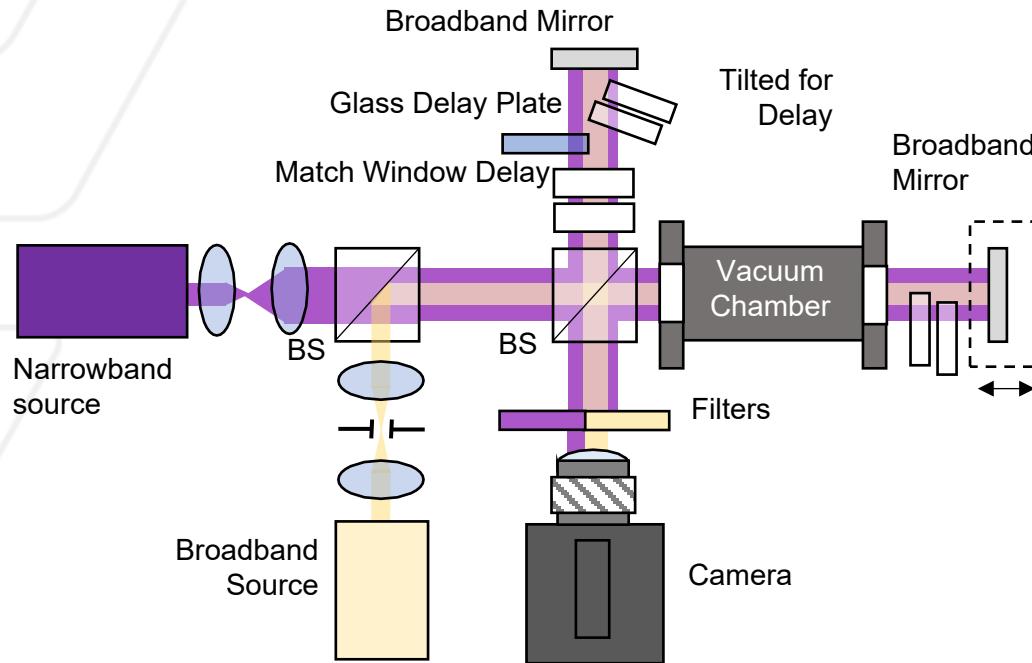


Quadrature Fringe Imaging Interferometer (QFII)

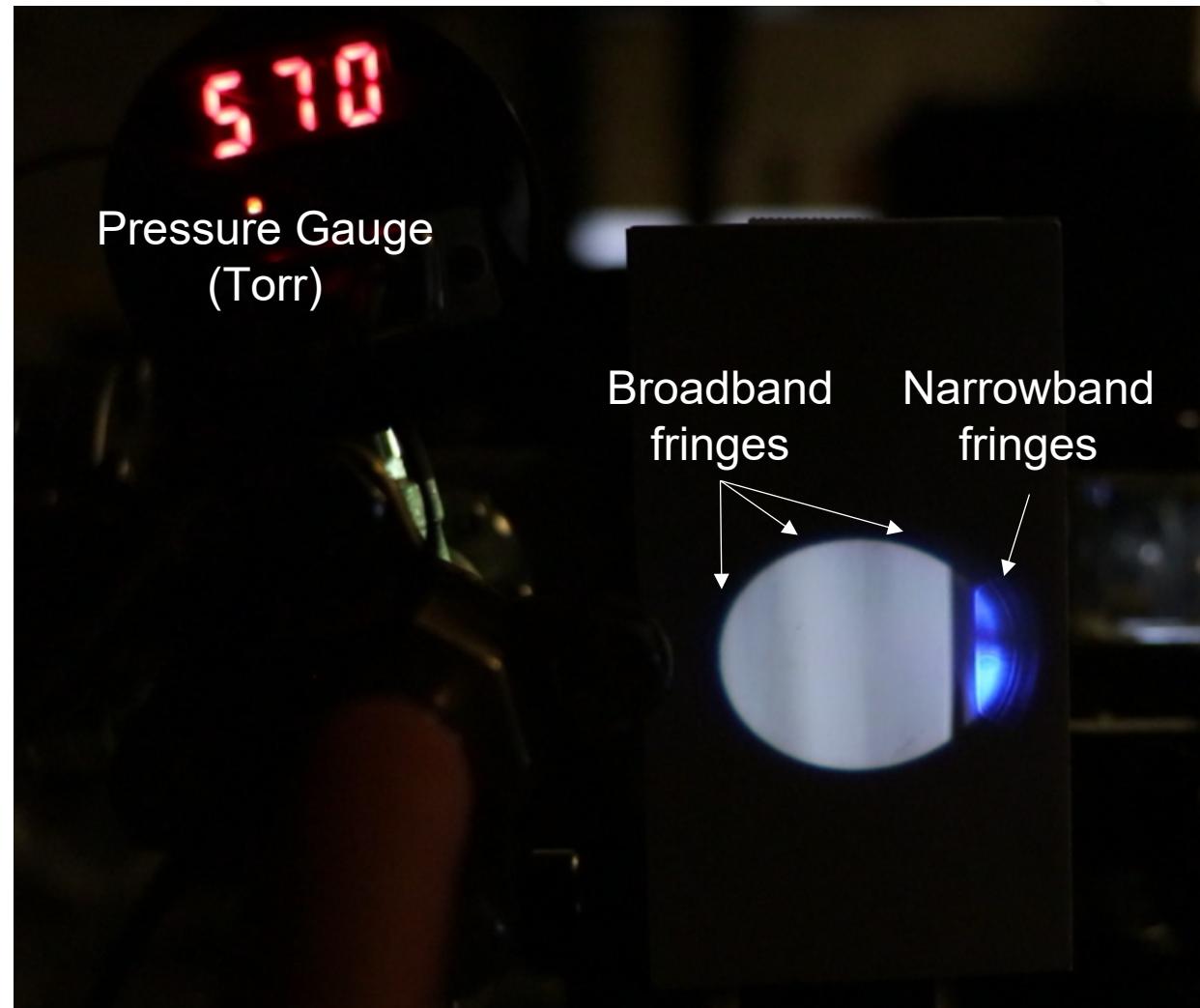
- Develop a diagnostic to resolve large discrete density changes
- Use narrowband and broadband source
 - Narrowband for analog quadrature
 - Broadband for absolute reference
- Broadband sources tested
 - LED bulb
 - Halogen bulb
 - Xenon flash lamp
 - SuperLED
- SuperK EVO supercontinuum laser is the only source that provides enough power for ultra-high-speed frame rates



Early Development



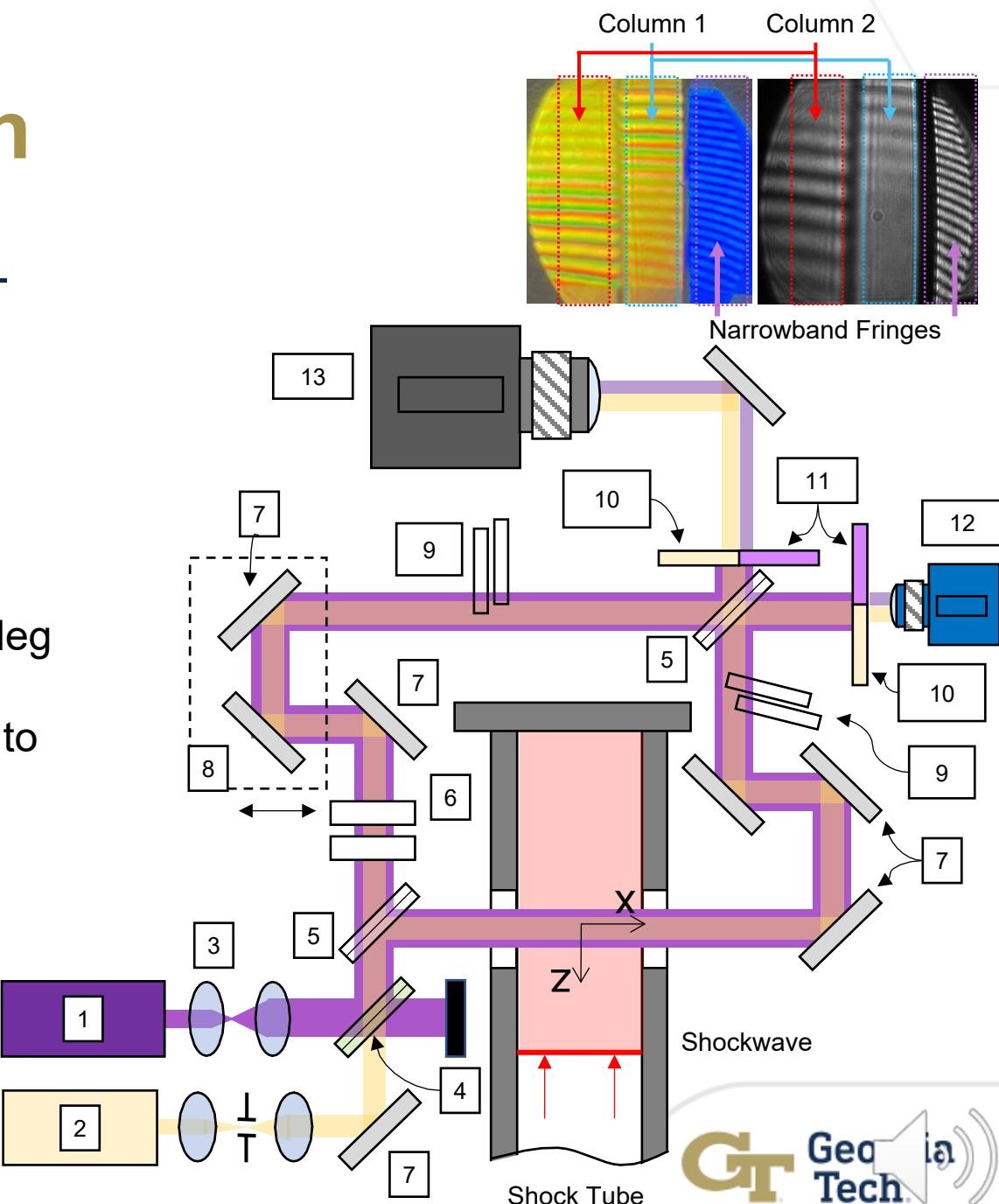
- Michelson interferometer with vacuum cell
 - Micrometer stage to balance and offset center
 - Glass delay plates to increase dynamic range
- Developed a calibration method for narrowband measurement using an analog quadrature



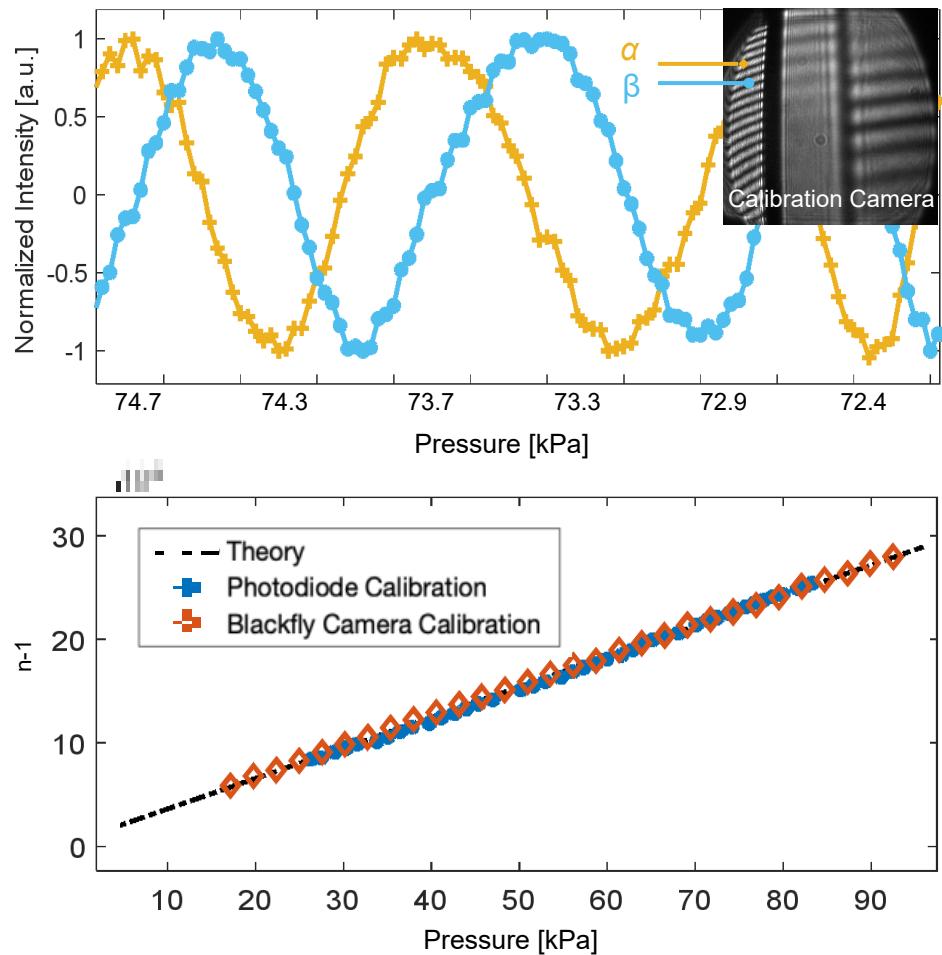
Mach-Zehnder Configuration

- For a Shock Tube implementation, we use a Mach-Zehnder configuration, which gives more flexibility and degrees of freedom for alignment than a Michelson configuration
- Filters and dichroic mirrors are used to combine and separate beams
- Windows of same thickness are placed in the reference leg to match divergence
- Glass delay plates create columns of broadband fringes to increase the dynamic range of measurement

1. 405 nm Laser	7. Broadband Mirrors
2. Broadband Source	8. Adjustable Leg
3. Lenses	9. Glass Delay Plates
4. 425 nm Long Pass Dichroic	10. 420 nm Long Pass Filter
5. Beam Splitter	11. 425 nm Short Pass Dichroic
6. Windows to Match Delay	12. Calibration Camera
	13. High Speed Camera



Calibration



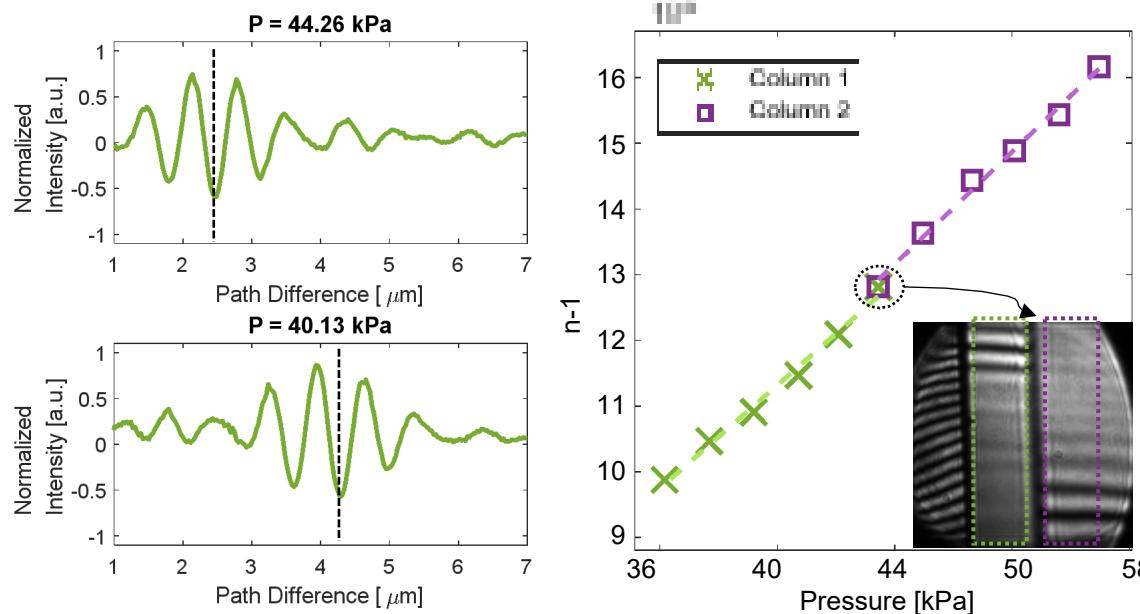
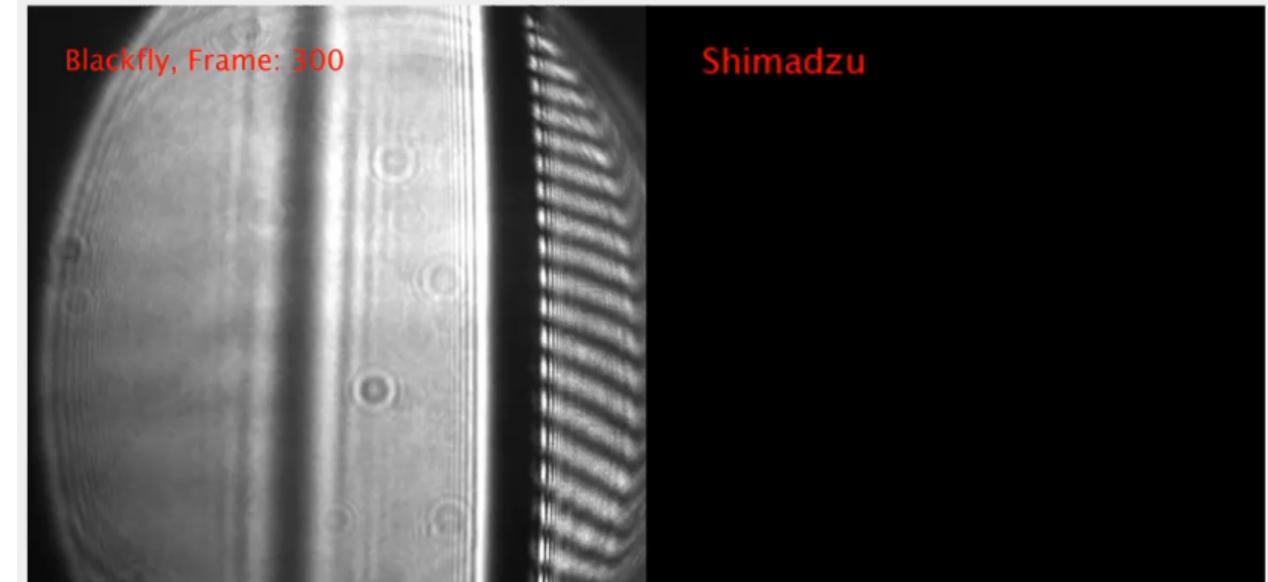
- Calculate absolute index with narrowband analog quadrature
 - High resolution and automated tracking
 - Photodiodes or camera can be used
 - Camera provides more flexibility
- Calibration verified with constant GD relationship at ambient conditions

For two sinusoidal signals α, β with phase shift $\phi_{\alpha\beta}$, the change in index is:

$$\Delta n = \frac{\lambda}{\pi W} \tan^{-1} \left(\frac{\beta(\Delta n) + \alpha(\Delta n) \sin(\phi_{\alpha\beta})}{\alpha(\Delta n) \cos(\phi_{\alpha\beta})} \right)$$

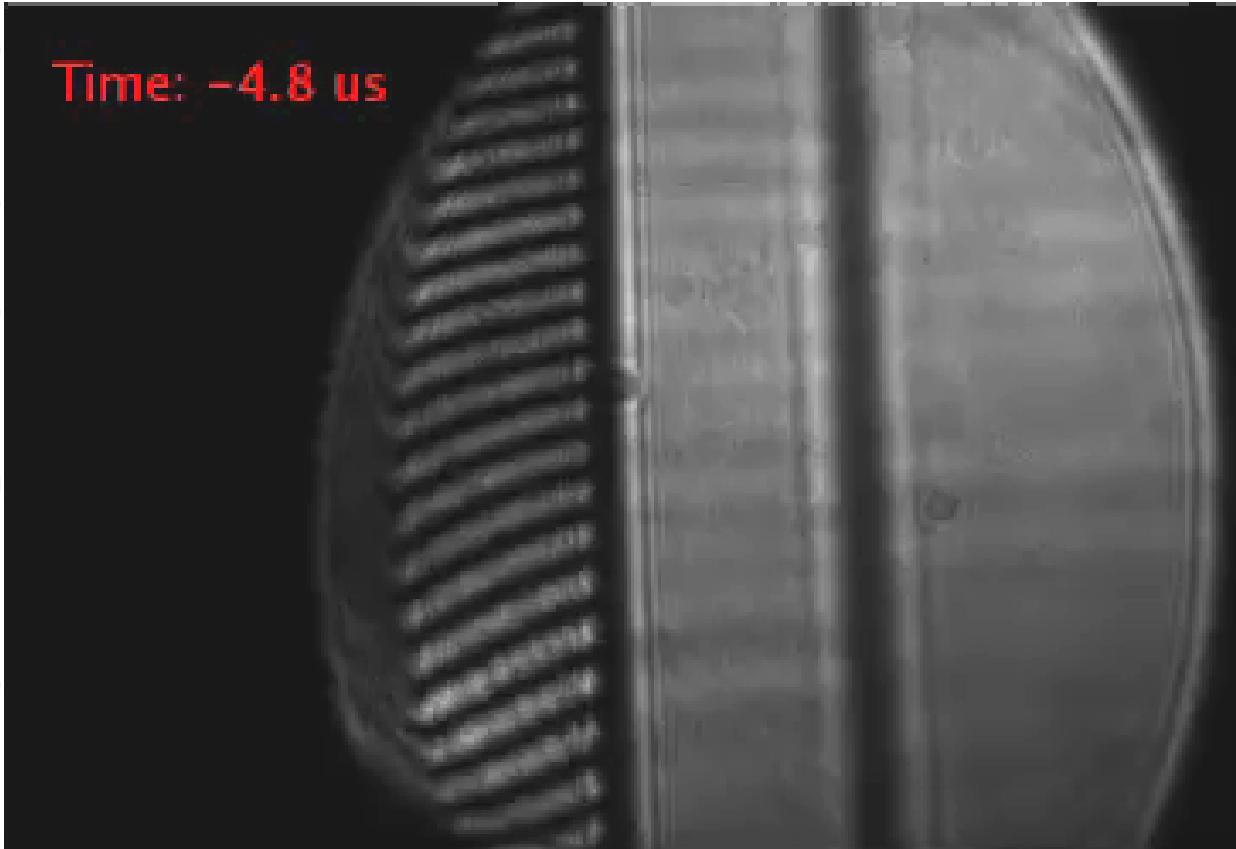
Calibration

- Relate broadband fringe center to absolute index
- Simultaneously trigger calibration camera and high-speed camera, note difference in quantum efficiency for different cameras
- Track center fringe



- Highest resolution with narrowband calibration
 - In presence of large external vibrations, calibration can be modified to use broadband for index calibration
 - Narrowband quadrature then used to reduce uncertainty
 - Can be challenging if interference pattern is not clear

Experiments: Georgia Tech Shock Tube

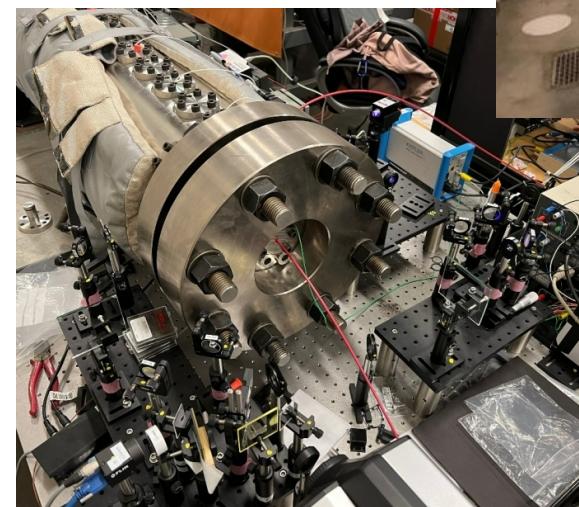


Direction of Incident Shock Wave
Incident Wave Speed: M2.92

Shimadzu HPV-X2

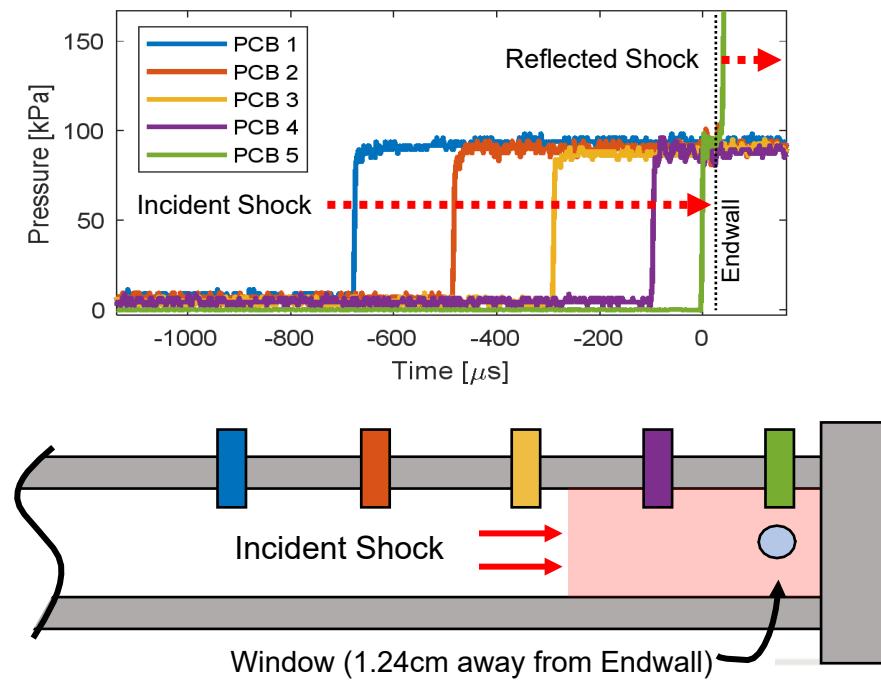
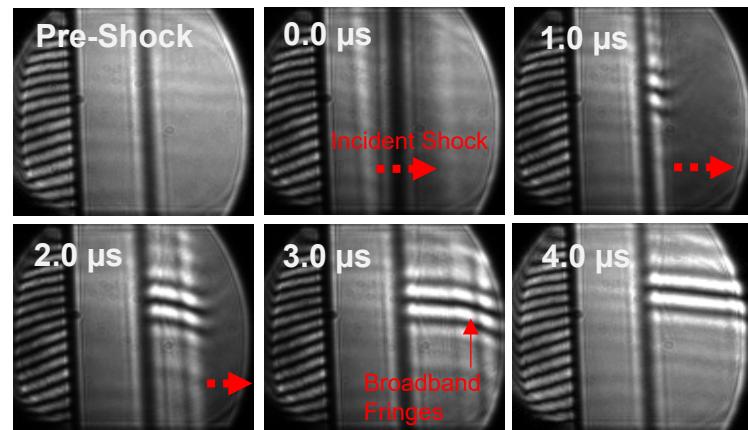
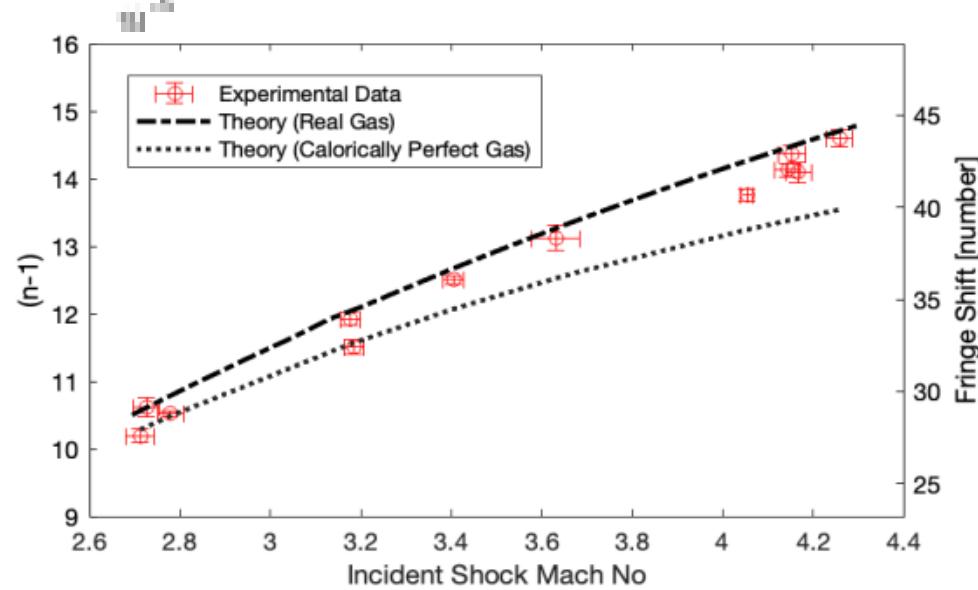
- 5 MHz frame rate
- 200 ns exposure
- Centered triggered on frame 64

$T_2 = 749 \text{ K}$
 $P_2 = 1.05 \text{ atm}$

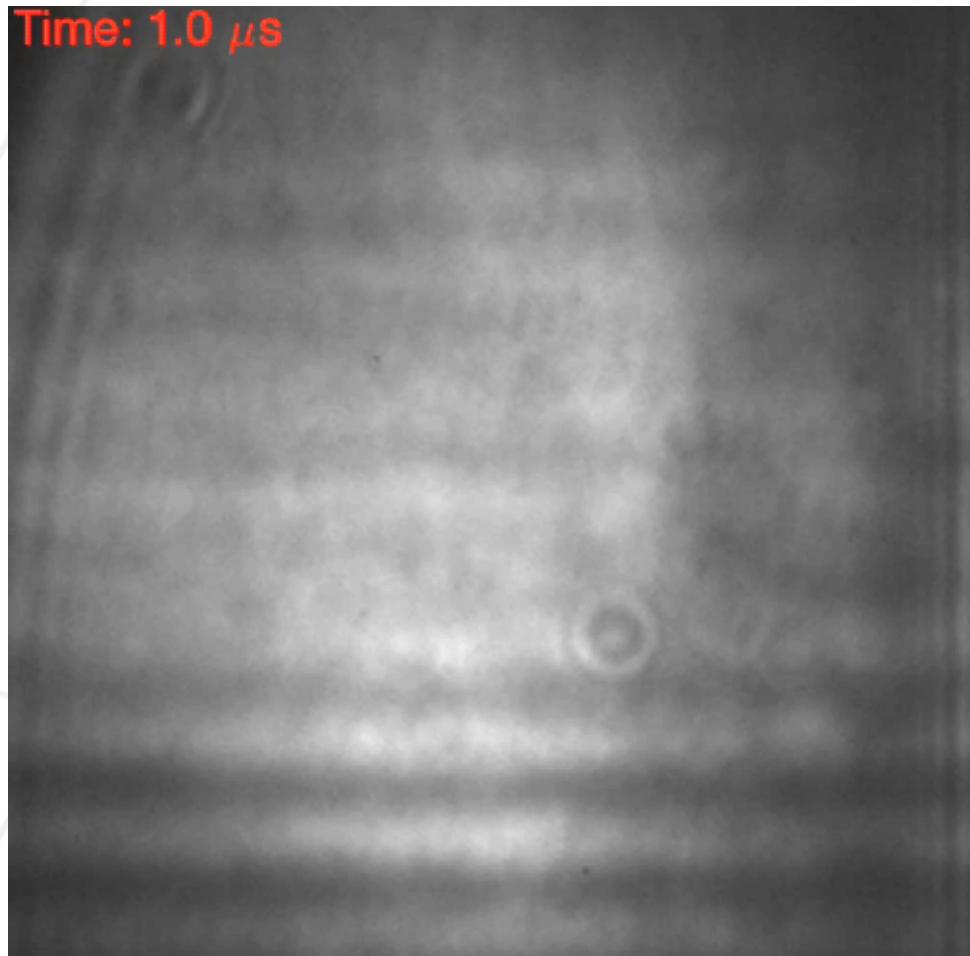


Experiments: Georgia Tech Shock Tube

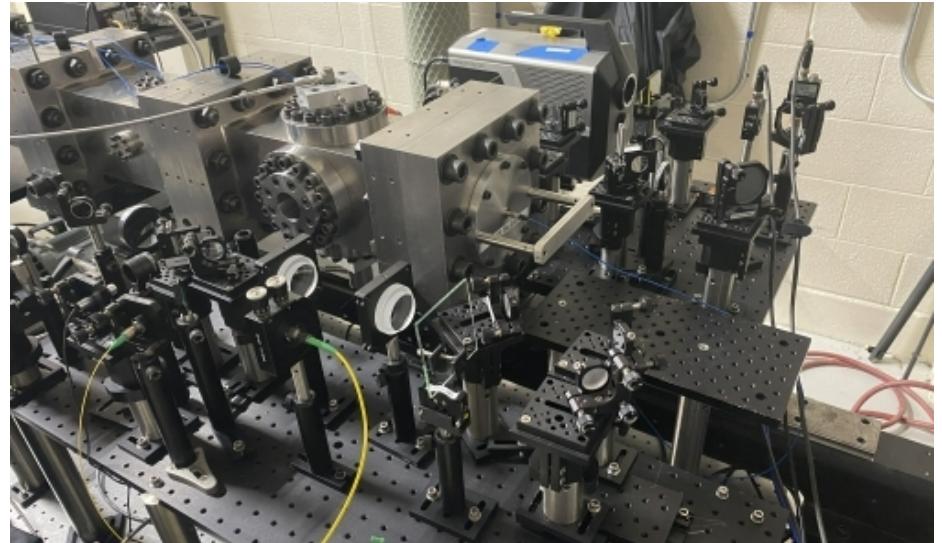
- Post incident-shock conditions measured with QFII
 - M2.7 - M4.3
 - Constant $P_1 = 10.7 \text{ kPa} = 80 \text{ Torr}$
 - He driver gas and air driven gas
- Results agree with theory within 2%



Experiments - Sandia HST



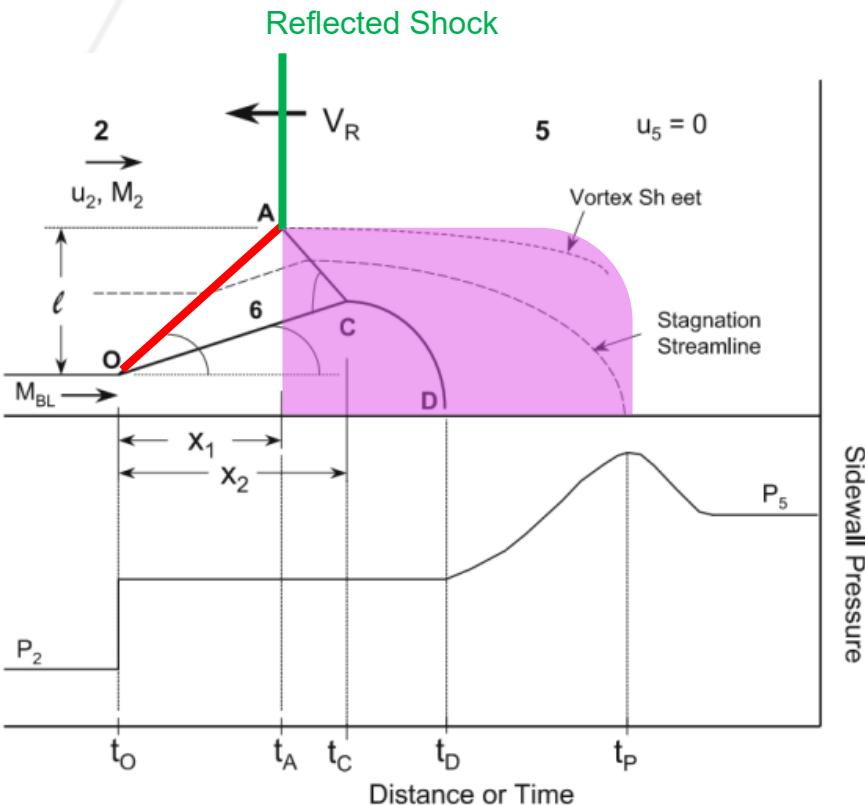
Direction of Reflected Shock Wave
(Incident Shock M13.95)



Shimadzu HPV-X2
1MHz, 200 ns exposure

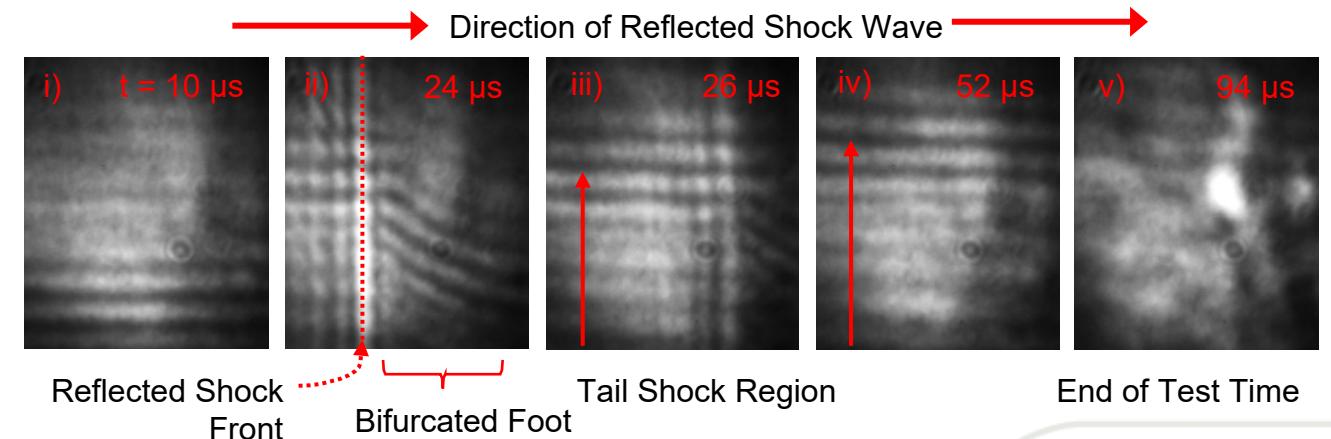
State 5		State 2	
P5	7.87 Bar	P2	0.63 Bar
T5	7653 K	T2	5343 K
ρ_5	0.24 kg/m ³	ρ_2	0.03 kg/m ³

Reflected Shock Flow Bifurcation



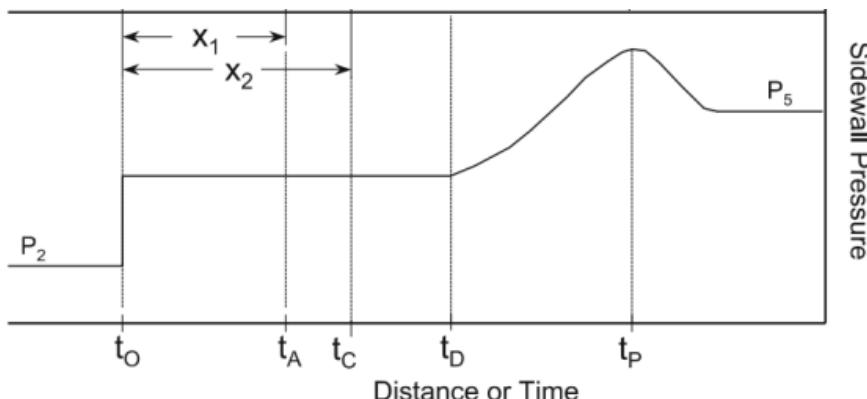
Petersen, E.L., Hanson, R.K. *Shock Waves* **15**, 333–340 (2006).

- In GT experiments, post-incident shock flow shows a nearly discrete index change
- Boundary layer interaction with reflected shock front causes bifurcation
 - Foot
 - Tail Shock (Vortex sheet and stagnation streamline)
- Petersen and Hansen reported similar time scale
 - 20-30 μ s before actual P5, T5 conditions

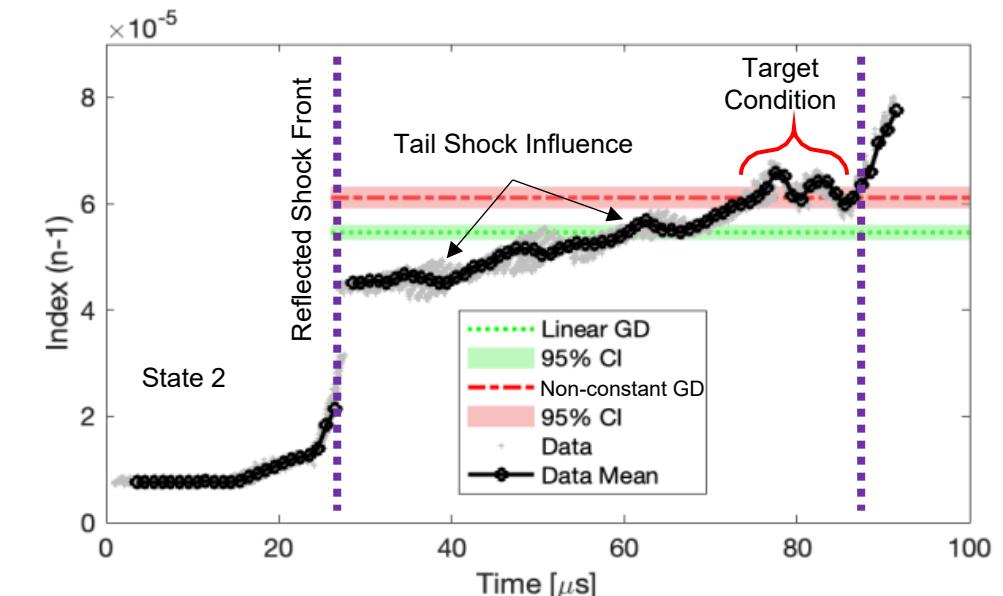
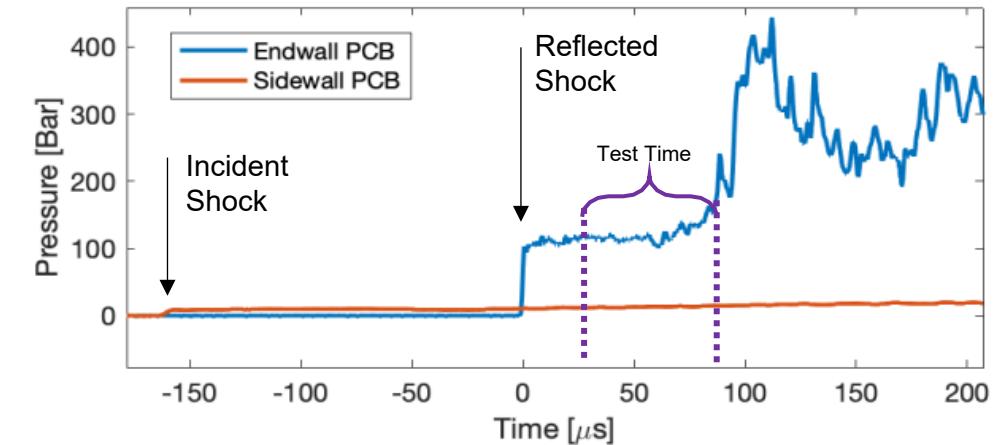


Results - Index of Refraction

- Post-incident and post-reflected shock were within the measurement range
- Rising index right before shock front captures the bifurcation foot
- Index continues to rise due to tail shock influence before measurement time ends
- Bifurcation produces additional challenges to extract index measurement at a single condition

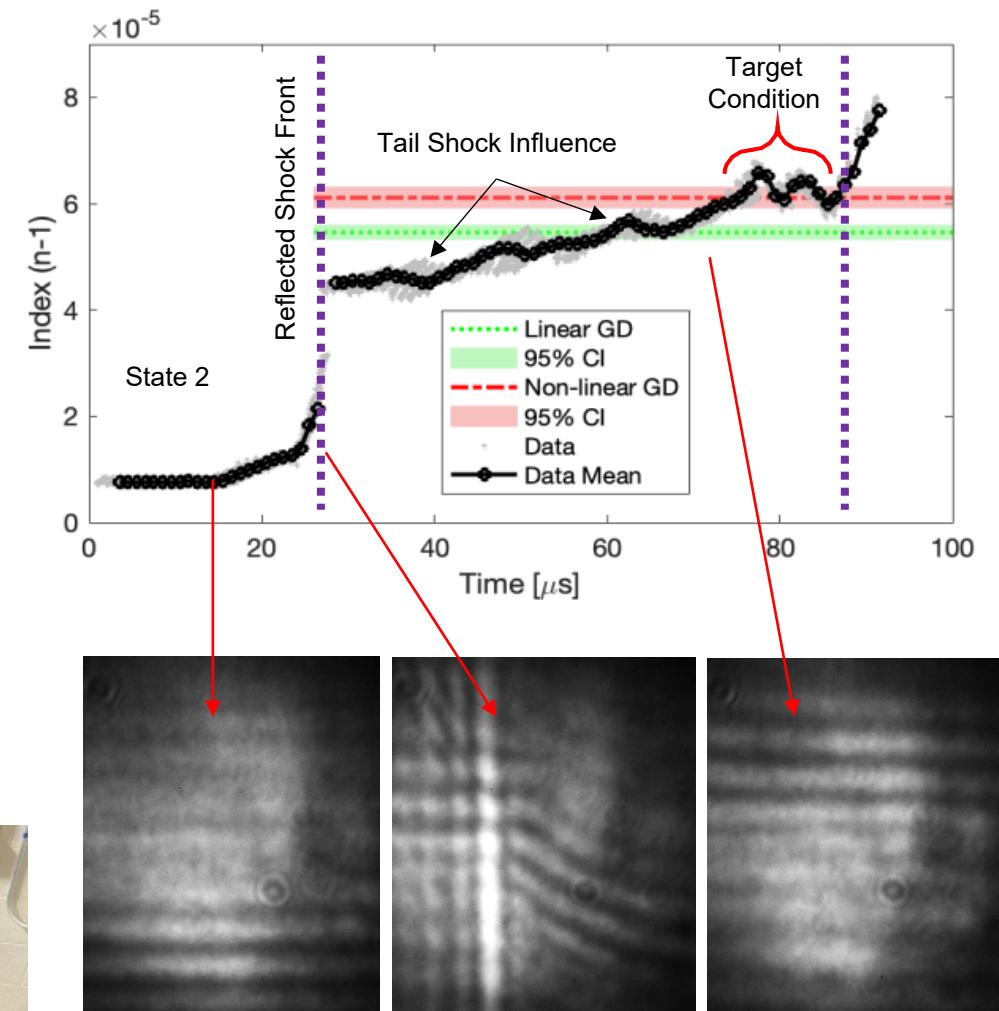
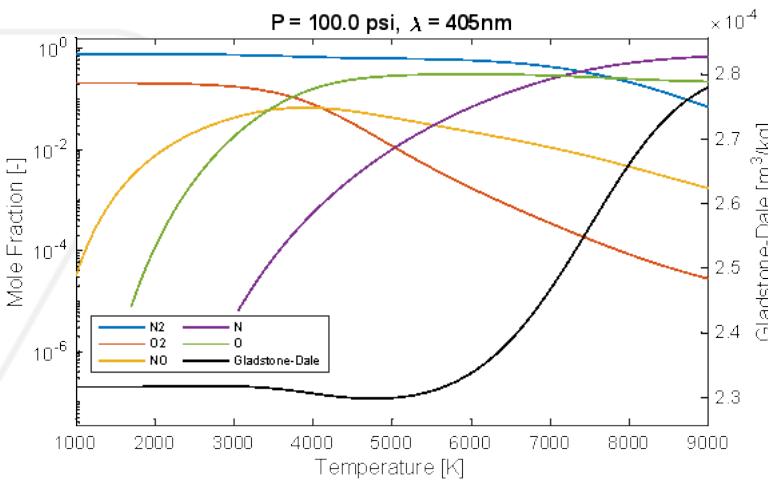


Petersen, E.L., Hanson, R.K. Shock Waves 15, 333–340 (2006).



Summary and Conclusion

- Development of optical diagnostic capable of measuring large discrete index of refraction changes
- Free-piston facility combined with QFII diagnostic to measure high pressure, high temperature incident and reflected shock conditions
- Reflected shock flow has complex bifurcation features
- Higher density conditions are necessary to generate better validation data



Thank you for listening!

Questions?

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