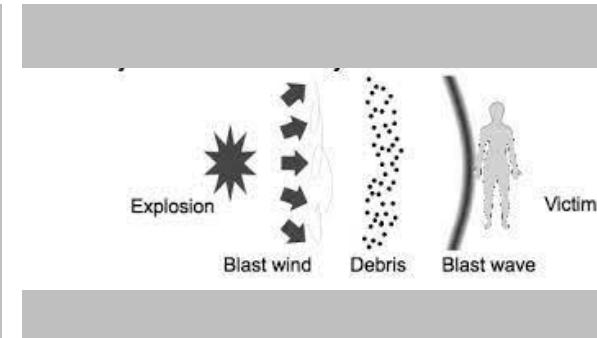
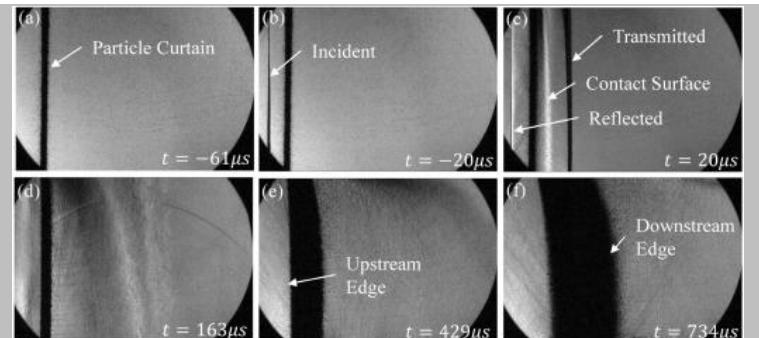


*Exceptional service in the national interest*



## Shock Induced Particle Curtain Dispersion: Asymptotic Drag Law Scaling Formulations and Relationship to Streamwise Pressure Difference Models

**Lawrence DeChant, Kyle Daniel, Justin Wagner and Russ Teeter**



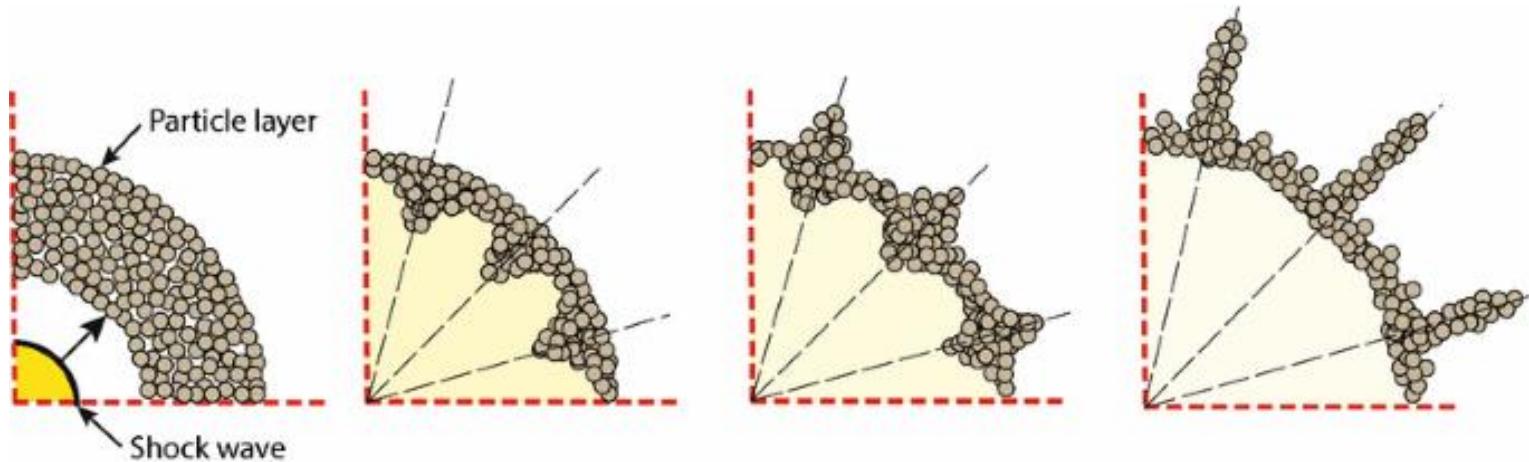
Sandia National Laboratories is a multimission laboratory managed and operated by National Technology & Engineering Solutions of Sandia, LLC, a wholly owned subsidiary of Honeywell International Inc., for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-NA0003525.

# Outline

- **Particle Shock Interaction**
- **Early-Late Time Asymptotic Drag-Based Models**
- **Streamwise Pressure Difference Shock Particle Curtain Dispersion Models**
- **Appendix: Compressible Rapid Expansion Pressure Loss Model**
- **Conclusions**
- **Future Work**

# Particle Shock Interaction...

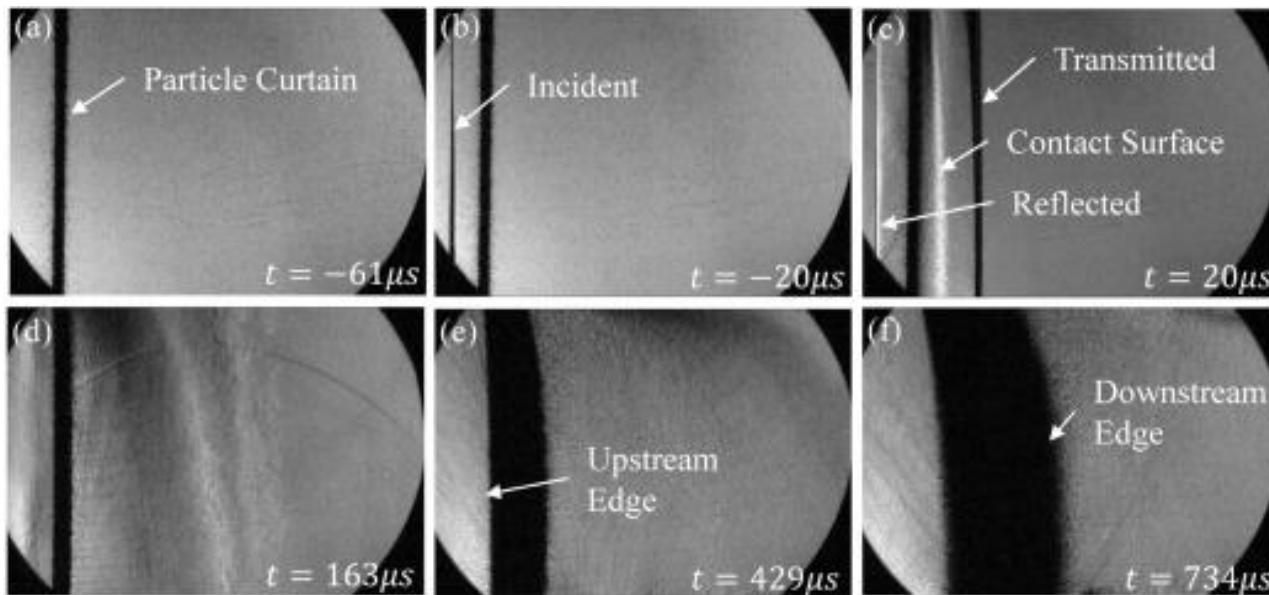
- Shock interaction with a planar particle curtain is a fundamental physical problem, with application for blast/fragmentation, shrapnel dispersion etc.



( Following Frost 2018)

# Particle Shock Interaction

- Shock interaction with a planar particle curtain measurement and development
- DeMauro et. al. (2019)...
- Daniel and Wagner (2022)...
- Provides a canonical, geometrically least complex problem...



Following (Ling, Wagner, Beresh, Kearney and Balachandar (2021)

# Early-Late Time Asymptotic Drag-Based Models

- Determination of particle curtain dynamics provides insight into local drag-dispersion behavior.
- The particle curtain width  $x(t)$  is described by:

$$\varphi \rho_p \delta_0 \frac{d^2 x}{dt^2} = \rho \left( \alpha_1 \frac{\nu}{d} + \alpha_2 \left( U - \frac{dx}{dt} \right) \right) \left( U - \frac{dx}{dt} \right)$$

- Nondimensionalize:

$$t^{**} = \frac{U}{\delta_0} t \quad ; \quad x^* = \frac{x}{\delta_0}$$

- Expected (non-dimensional) differential equation

$$\frac{d^2 x^*}{dt^{**2}} = \varphi^{1/2} \left( \frac{\rho}{\rho_p} \right) \left( C_1 \text{Re}_d^{-1} + C_2 \left( 1 - \frac{dx^*}{dt^{**}} \right) \right) \left( 1 - \frac{dx^*}{dt^{**}} \right)$$

- “laminar” low Re drag; “turbulent” high Re drag

# Early-Late Time Asymptotic Drag-Based Models

- Flow field is broadly modified by the presence of the particles, freestream (velocity) is no longer constant/attainable... modify relative velocity terms as ( $a=1/4$ ):

$$(1 - \frac{dx^*}{dt^{**}}) \rightarrow (1 - \alpha \varphi^{-a} \frac{dx^*}{dt^{**}})$$

- Yields ODE

$$\frac{d^2 x^*}{dt^{*2}} = \left( c_1 + c_2 \left( 1 - \alpha^{-1} \frac{dx^*}{dt^{**}} \right) \right) \left( 1 - \alpha^{-1} \frac{dx^*}{dt^{**}} \right)$$

- Where:

$$c_1 \equiv \left( \frac{\rho}{\rho_p} \right) \text{Re}_d^{-1} C_1 \quad c_2 \equiv \left( \frac{\rho}{\rho_p} \right) C_2 \quad t^* = \varphi^{1/4} t^{**} = \varphi^{1/4} \frac{U}{\delta_0} t$$

- Exact solution

$$x^* = \alpha t^* - \frac{\alpha}{c_2} \ln \left( 1 - \frac{c_2}{c_1} \left( 1 - \exp \left( -\frac{c_1}{\alpha} t^* \right) \right) \right)$$

# Early-Late Time Asymptotic Drag-Based Models

- Solution has early and late attributes; leverage

$$\frac{d^2 x_{early}^*}{dt^{*2}} \approx (c_1 + c_2)$$

$$x_{late}^* = \alpha t^* + b$$

- Use a matching argument: function value, slope and curvature we can get an estimate parameter:

$$\alpha = 9(c_1 + c_2)$$

- The constants  $c_1$  and  $c_2$  are easily estimated empirically...

$$c_1 = 0.032 \quad c_2 = 0.041$$

- A traditional Galerkin/collocation procedure model is shown to provide similar estimates  $c_1$  and  $c_2$ ... detail in manuscript

# Early-Late Time Asymptotic Drag-Based Models

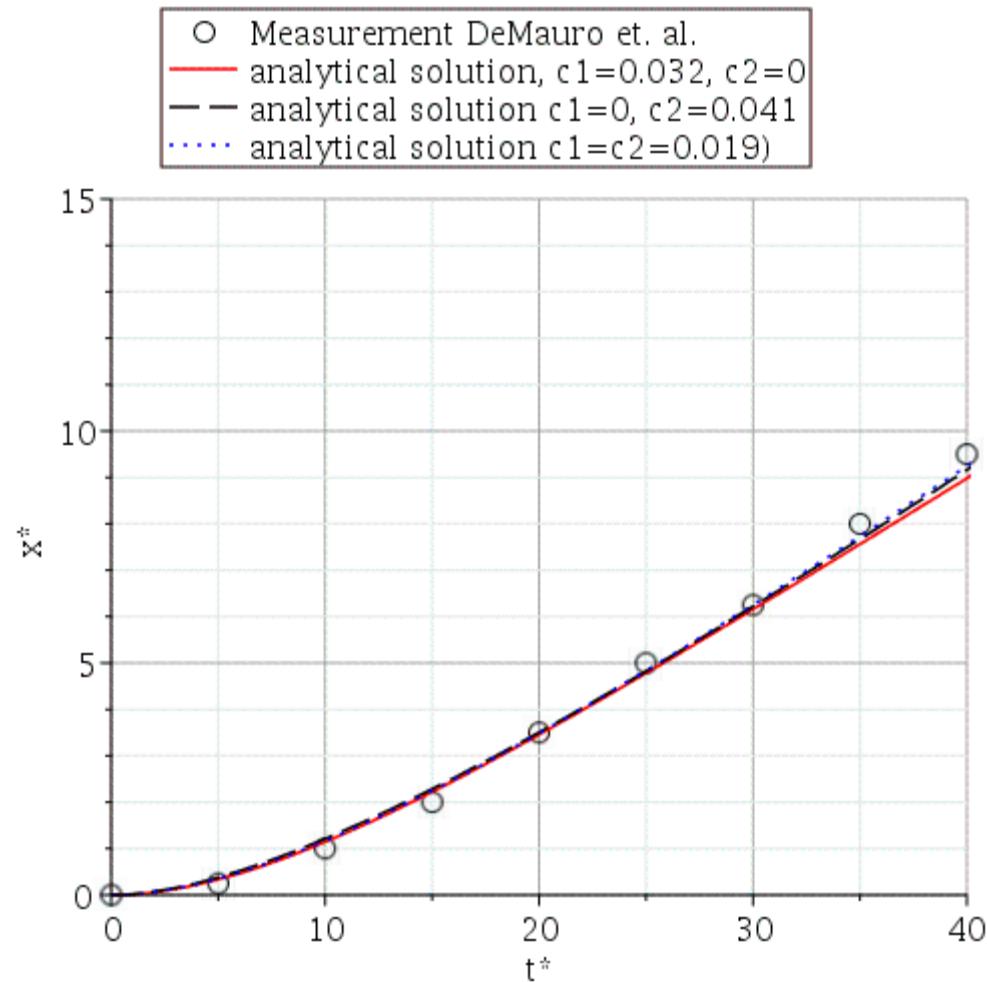
- Fit of data with measurements De Mauro et. al. 2019 shows good agreement for a wide range of possible  $c_1$  and  $c_2$  closures... It's not very sensitive..
- The key behavior is not so much the particular values of  $c_1$  and  $c_2$  , but the functional form to change the asymptotic behavior via:

$$(1 - \frac{dx^*}{dt^{**}}) \rightarrow (1 - \alpha \varphi^{-a} \frac{dx^*}{dt^{**}})$$

- The matching argument provides information for  $\alpha$ ... Combined with the scaling..

$$t^* = \varphi^{1/4} t^{**} = \varphi^{1/4} \frac{U}{\delta_0} t$$

- Supports the flow behavior



- A simple force balance based on the pressure difference across the particle curtain obviates the use of the drag closure...

$$\varphi \rho_p \delta_0 A \frac{d^2 x}{dt^2} = F_P \propto \varphi A (p_u - p_d)$$

- To use this model... we need  $(p_u - p_d)$  Daniel and Wagner (2022)... provide just such a model...

$$p_u - p_d = C_{meas} \varphi^{1/2} \rho_1 u_2^2 \quad ; \quad C_{meas} = 9.6$$

- Estimation of the closure constant  $C_{meas}$  is our goal.
- Approach... leverage classical wind tunnel screen/mesh pressure loss: Pinker and Herbert (1967)/ Huang (1991)

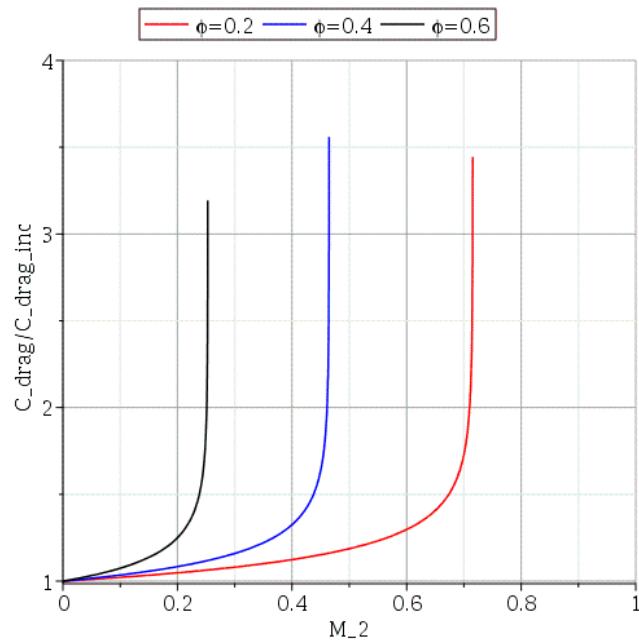
- leverage classical wind tunnel screen/mesh pressure loss: Pinker and Herbert (1967)/ Huang (1991)
- Simple Incompressible... power law approximation

$$\Delta p = \frac{1}{2} \lambda_0 \rho_2 u_2^2 \quad ; \quad \lambda_0 = \lambda_0(\varphi) \quad \lambda_0(\varphi) \approx 3.5 \varphi^{3/2}$$

- Must be extended to compressible flow, to honor inter-particle choking; Empirically..

$$\frac{C_{drag}}{C_{drag\_inc}} = \left( \frac{M^*}{M^* - M_0} \right)^b \quad b \approx 1/7$$

- But this expression is not bounded for choking.. We need another model



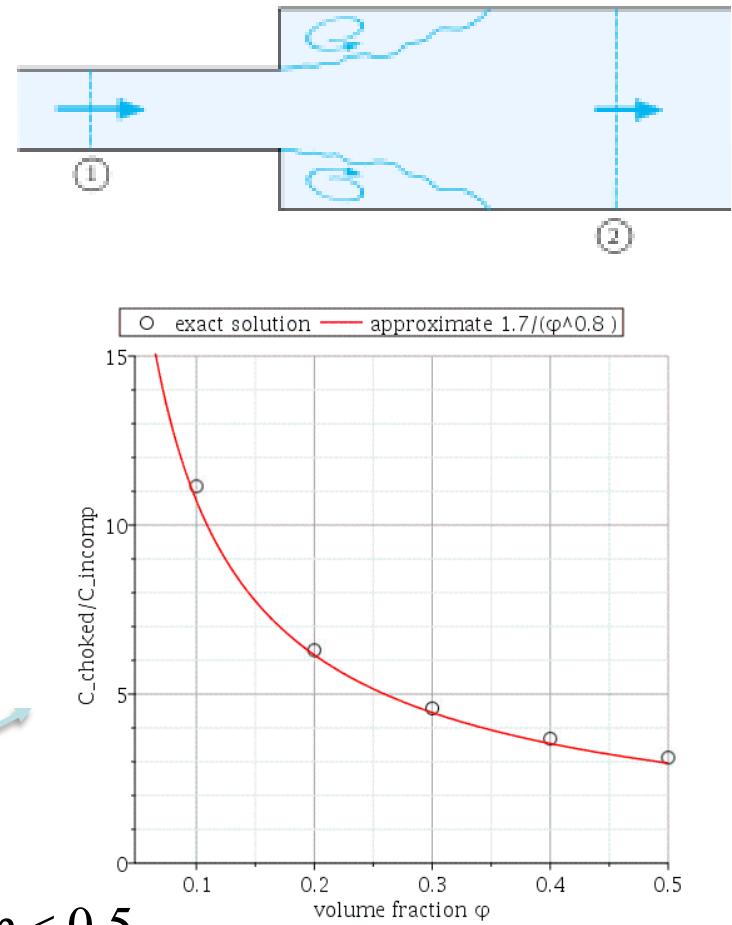
- Compressible sudden expansion...
- Simple balance of mass, momentum and energy balance in compressible form..
- Two basic equations...

$$\frac{p_2 - p_1}{\frac{1}{2} \rho_0 u_0^2} = 2 \frac{M_1}{M_0} \left( \frac{1 + \frac{\gamma-1}{2} M_0^2}{1 + \frac{\gamma-1}{2} M_1^2} \right)^{1/2} \left( 1 - \frac{M_2}{M_1} \left( \frac{1 + \frac{\gamma-1}{2} M_1^2}{1 + \frac{\gamma-1}{2} M_2^2} \right)^{1/2} \right)$$

$$\frac{(p_0 - p_1)}{\frac{1}{2} \rho u_0^2} = \frac{p_0}{\frac{1}{2} \rho u_0^2} \left( 1 - \frac{p_1}{p_0} \right) = \frac{2}{\gamma M_0^2} \left( 1 - \left( \frac{1 + \frac{\gamma-1}{2} M_0^2}{1 + \frac{\gamma-1}{2} M_1^2} \right)^{\frac{\gamma}{\gamma-1}} \right)$$

- These expressions are solvable and can be mapped to a more convenient closure expression as:

$$\left. \frac{C_{drag}}{C_{drag\_inc}} \right|_{M^* = 1} \approx 1.7 \varphi^{-4/5} \quad 0.1 < \varphi < 0.5$$



- **Build up estimate of pressure difference**
- **Incompressible term:**

$$\lambda_0(\varphi) \approx 7c_0\varphi^{3/2} = 3.5\varphi^{3/2} \quad ; \quad c_0 \approx 0.5$$

- **Choked flow correction (integral average)**

$$\left. \frac{C_{drag}}{C_{drag\_inc}} \right|_{ave} \approx 3.5 \quad \left. \frac{C_{drag}}{C_{drag\_inc}} \right|_{ave} = \frac{1.7}{1-0.1} \int_{0.1}^1 \varphi^{-4/5} d\varphi \approx 3.5$$

- **Density ratio (integral average)**

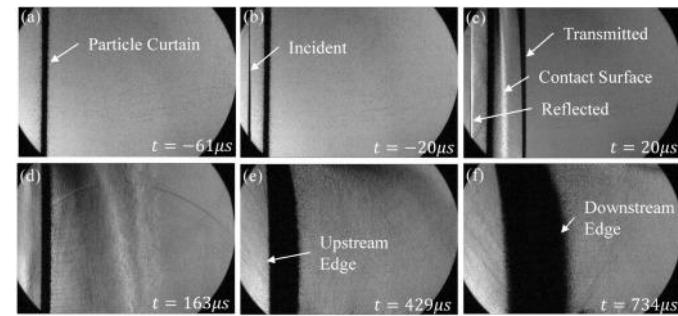
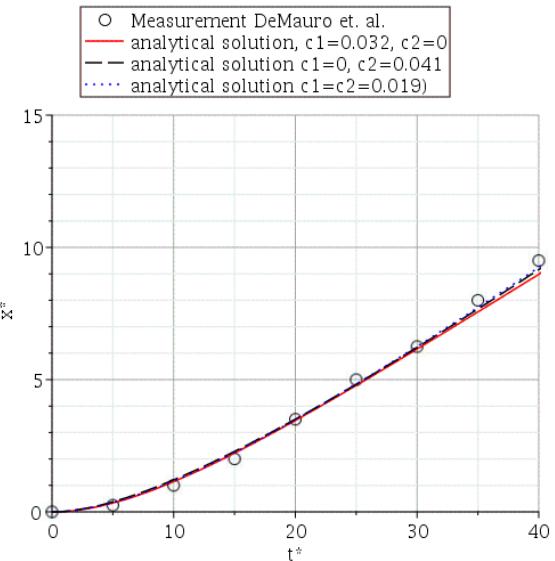
$$\left. \frac{\rho_2}{\rho_1} \right|_{ave} = \frac{1}{1.7-1} \int_1^{1.7} \frac{\rho_2}{\rho_1} dM_s = 1.6$$

- **Final result.... In good agreement with Daniel and Wagner...  $C_{meas}=9.6$**

$$\Delta p = \frac{1}{2} \lambda_0(\varphi) \left( \left. \frac{C_{drag}}{C_{drag\_inc}} \right|_{ave} \right) \left( \left. \frac{\rho_2}{\rho_1} \right|_{ave} \right) \rho_1 u_2^2 = (3.5\varphi^{3/2})(3.5)(1.6)\rho_1 u_2^2 = 9.8\varphi^{3/2} \rho_1 u_2^2$$

# Conclusions and Future Work

- **Early-Late Time Asymptotic Drag-Based Models**
  - **Particle curtain spreading well predicted**
  - **The key behavior=the functional form to change the asymptotic behavior to honor drastic change to flow field**
- **Streamwise Pressure Difference Shock Particle Curtain Dispersion Models**
  - **Pressure difference model (Daniel and Wagner (2022) provide useful description**
  - **closure constants in good agreement with measurement**
- **Future work:**
  - **Apply results to shock-physics framework e.g. CTH**
  - **Support particle shock application space**



# Acknowledgements/Questions

- *Sandia National Laboratories is a multimission laboratory managed and operated by National Technology & Engineering Solutions of Sandia, LLC, a wholly owned subsidiary of Honeywell International Inc., for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-NA0003525.*

**Questions???**