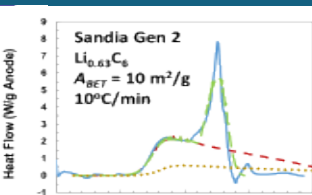
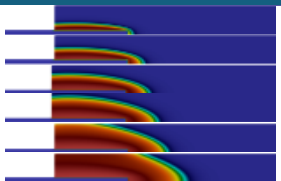
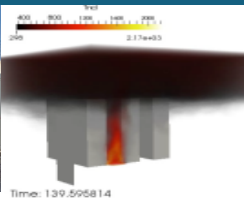
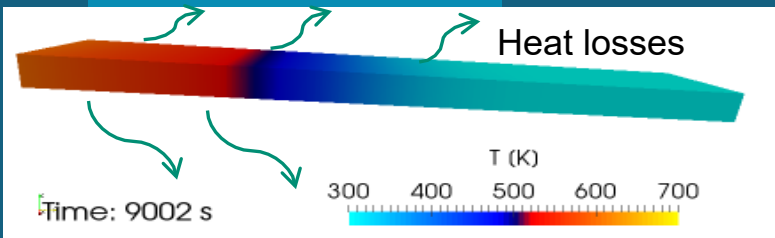




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# Battery safety research at Sandia: Moving toward designs that mitigate cascading failure



Presented by

John Hewson, with Andrew Kurzawski  
Randy Shurtz, Loraine Torres-Castro

Battery Safety Council

Nov. 16, 2022

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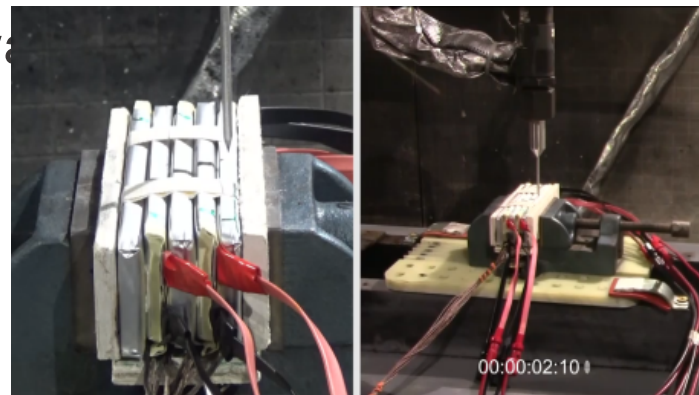
# Predicting and Mitigating Thermal Runaway

Validated safety and reliability is one of the critical challenges in deploying large-scale or mission-essential energy storage

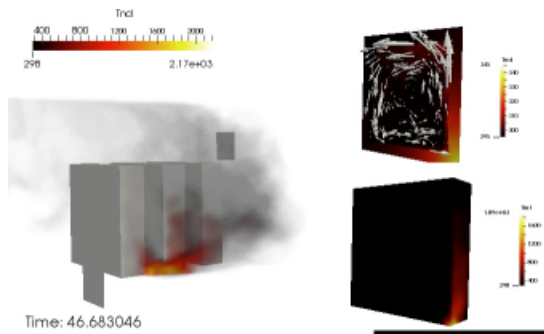
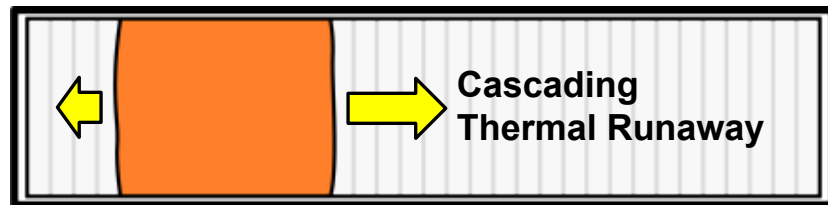
Safety incidents are rare but possible, incl. external

causes. How can we reduce risk?

- Prevent single-point failure from cascading to large-scale system risk.
- Design inherently safer systems that are resistant to cascading failure.



Module



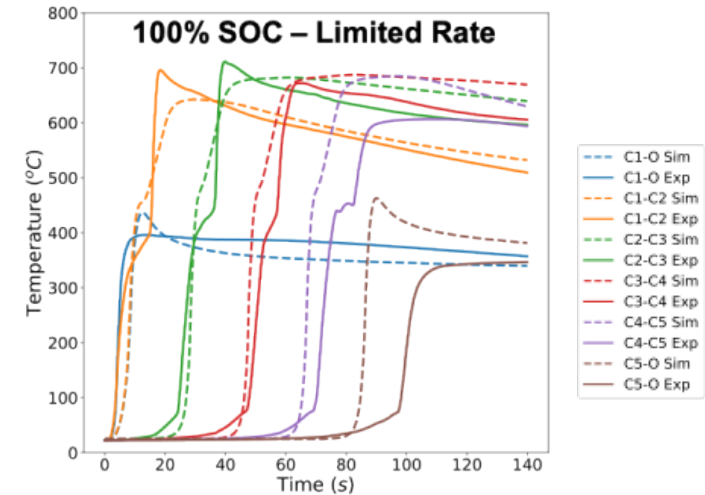
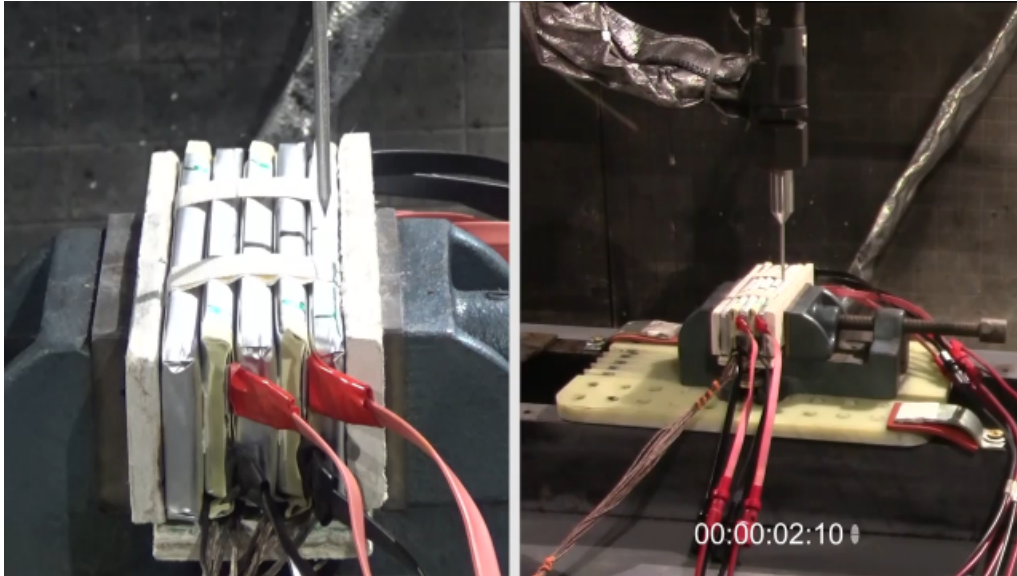
Simulations allow exploration of the design space if well grounded in reality.

A parameter space analysis can provide general safety-focused design guidelines





Venting removes electrolyte, changes the energy available. Calibrate on max temp.



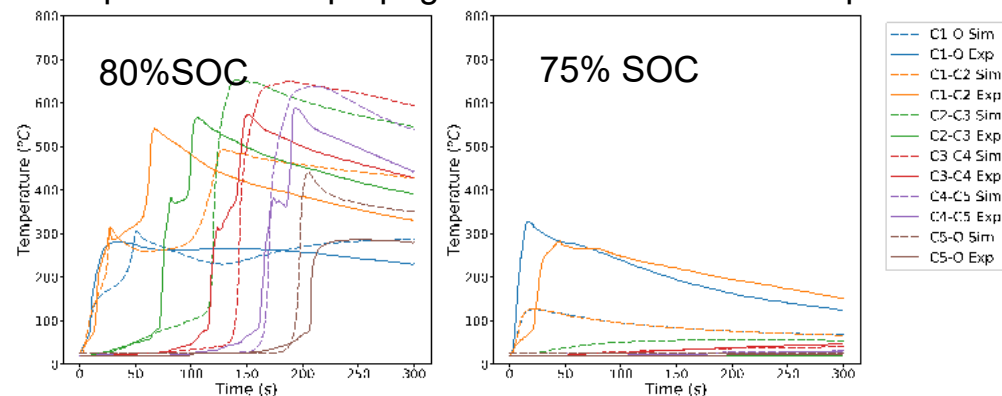


# New chemistry models successfully predict full range of scenarios

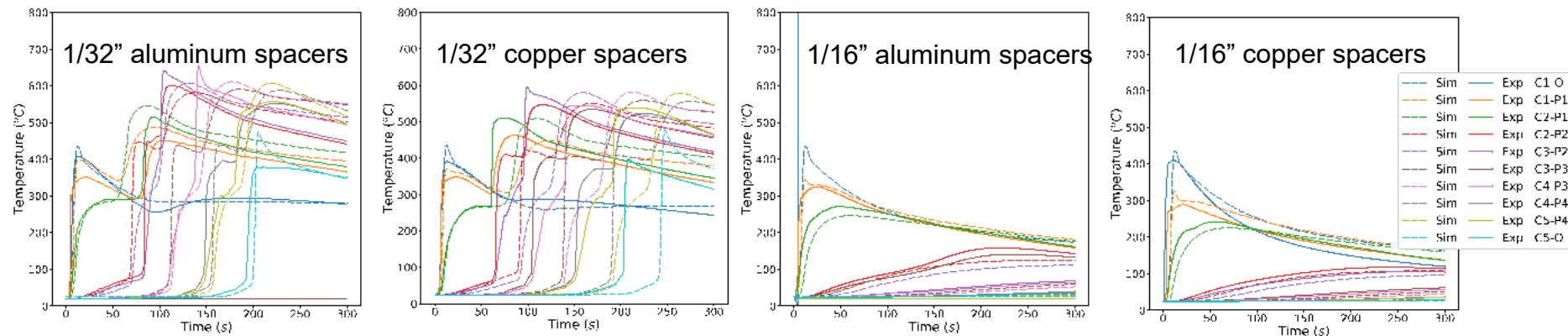
5



## Temperature-time propagation measurements and predictions



- Successful prediction over a range of reduced SOC and metallic inserts.
- Collectively add heat capacity & increase time delay for cell runaway.
- Prevent propagation for 30% increase in net heat capacity.





Cells have a characteristic thermal runaway temperature.

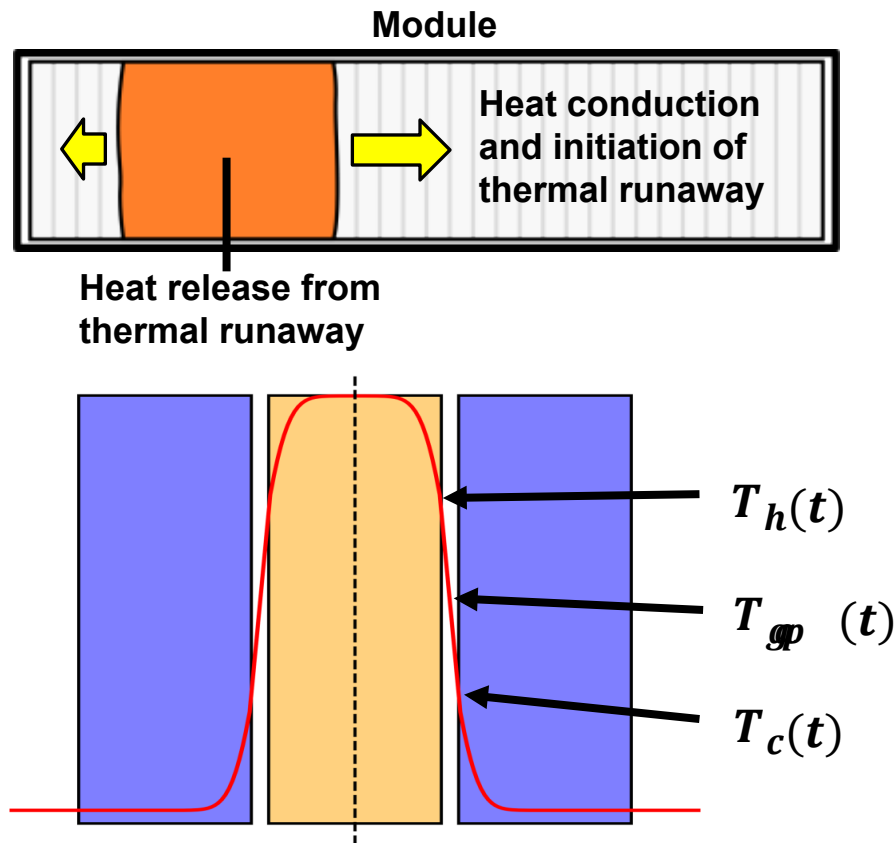
- Propagation mitigated if the next cell temperature is less than this.
- Dissipate heat to avoid propagation.

Where can the heat from a failed cell go?

- Along a cell stack and to the surroundings.

Parameters affecting next-cell temperature:

- Thermal resistance along the stack.
- Ability to dissipate heat.
- Heat sinks (structure/cooling system).

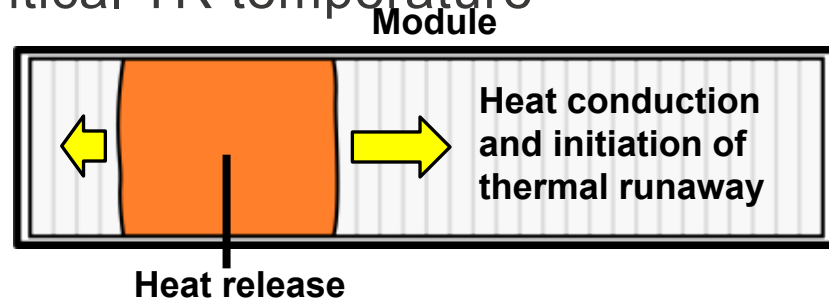
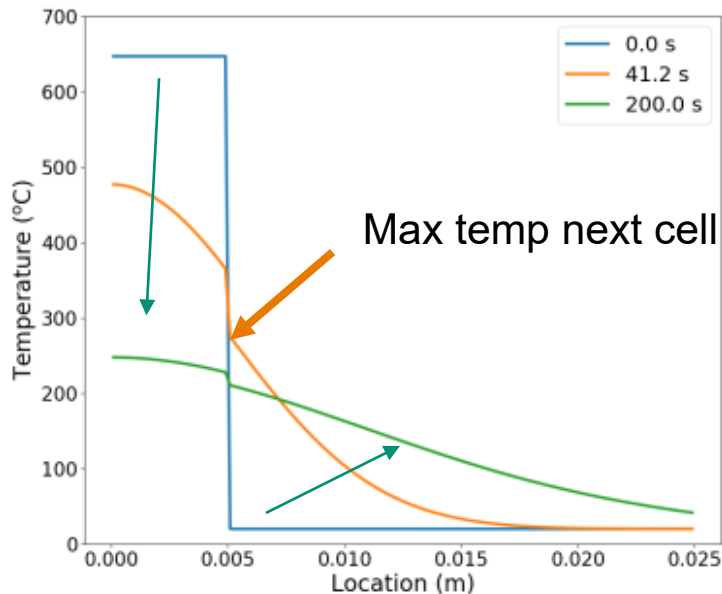


Heat transfer along adiabatic stack with thermal resistance,  $R''$

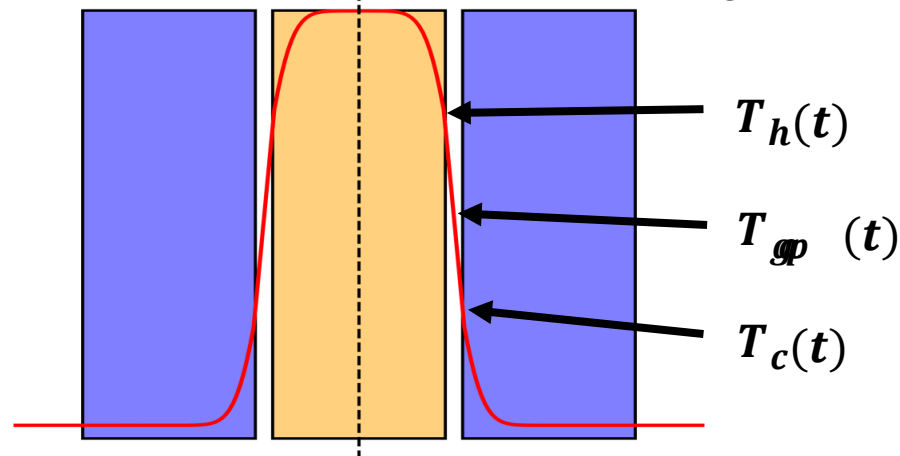
Chemistry turned off to look for critical TR temperature



Adiabatic module scenario at first

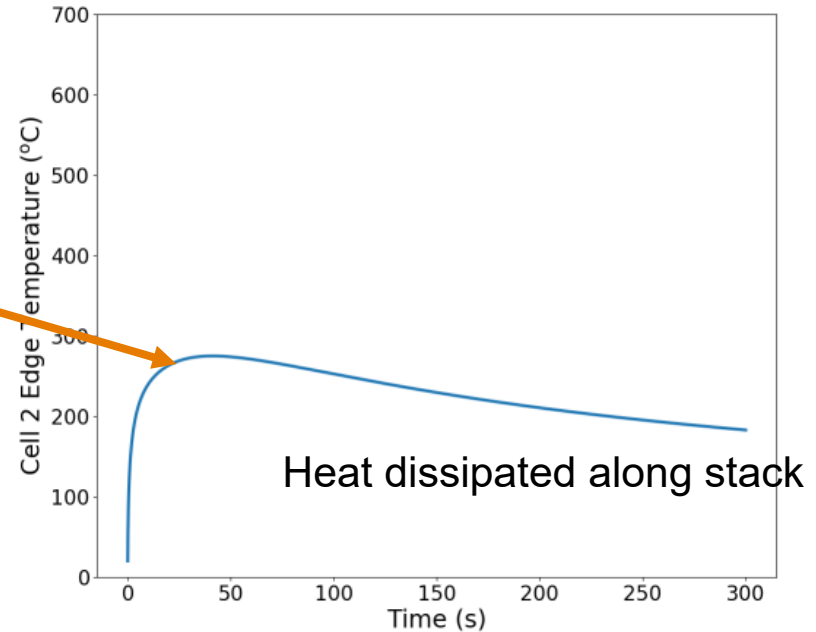
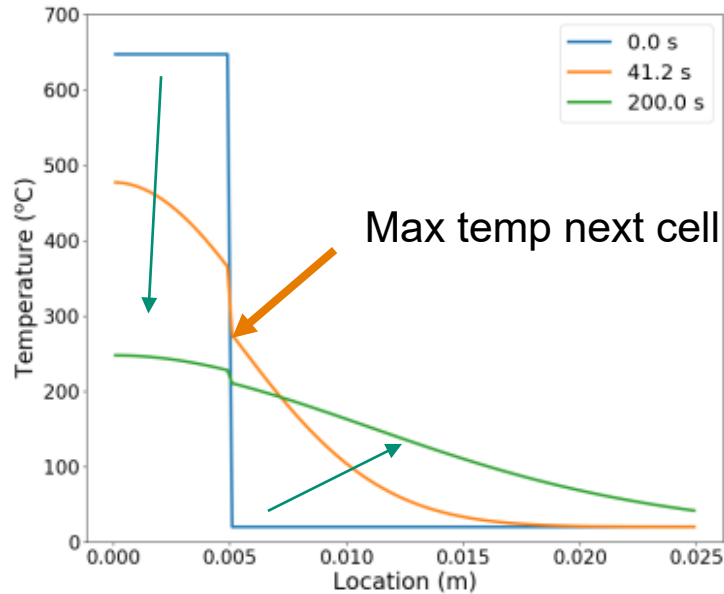


TR in cell affects surrounding cells



Heat transfer along adiabatic stack with thermal resistance,  $R''$

Chemistry turned off to look for critical TR temperature



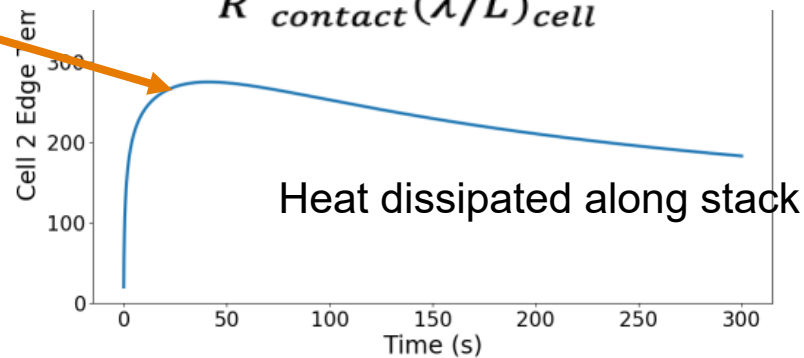
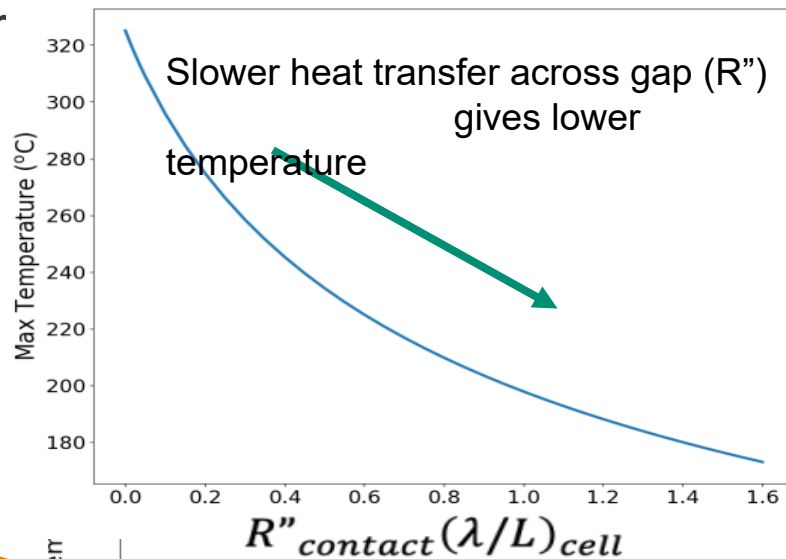
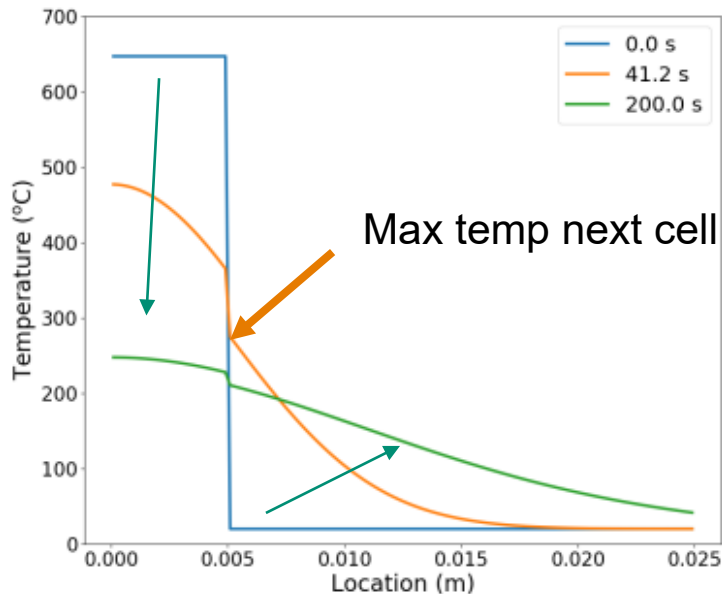


Heat transfer along adiabatic stack with thermal resistance,  $R''$



Chemistry turned off to look for  
Max temp of next cell depends on

$$\frac{1}{Bi} = \frac{R''_{contact}}{(L/\lambda)_{cell}} = \frac{R''_{contact}}{R''_{cell}}$$



# Conduction with thermal dilution

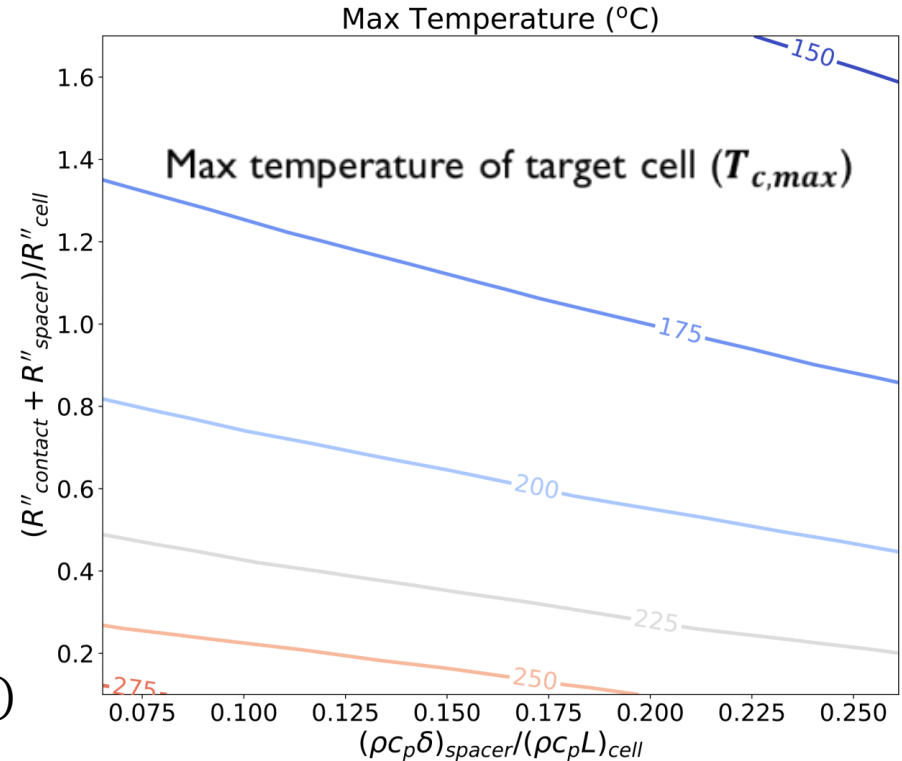
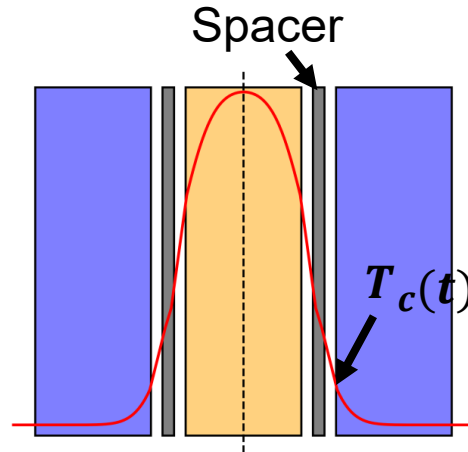


Additional temperature reduction can be achieved by adding inert material (ex: structure, casing, spacers).

$$\frac{1}{Bi} = \frac{R''_{contact} + (\delta/\lambda)_{spacer}}{(L/\lambda)_{cell}}$$

The heat capacity ratio of inert spacer material to cells is:

$$\phi_{capacity} = \frac{(\rho c_p \delta)_{spacer}}{(\rho c_p L)_{cell}}$$



# Thermal runaway temperature leading to propagation versus max cell temperature



Previous results determine max target cell temperature. Relate this to thermal runaway/propagation temperature.

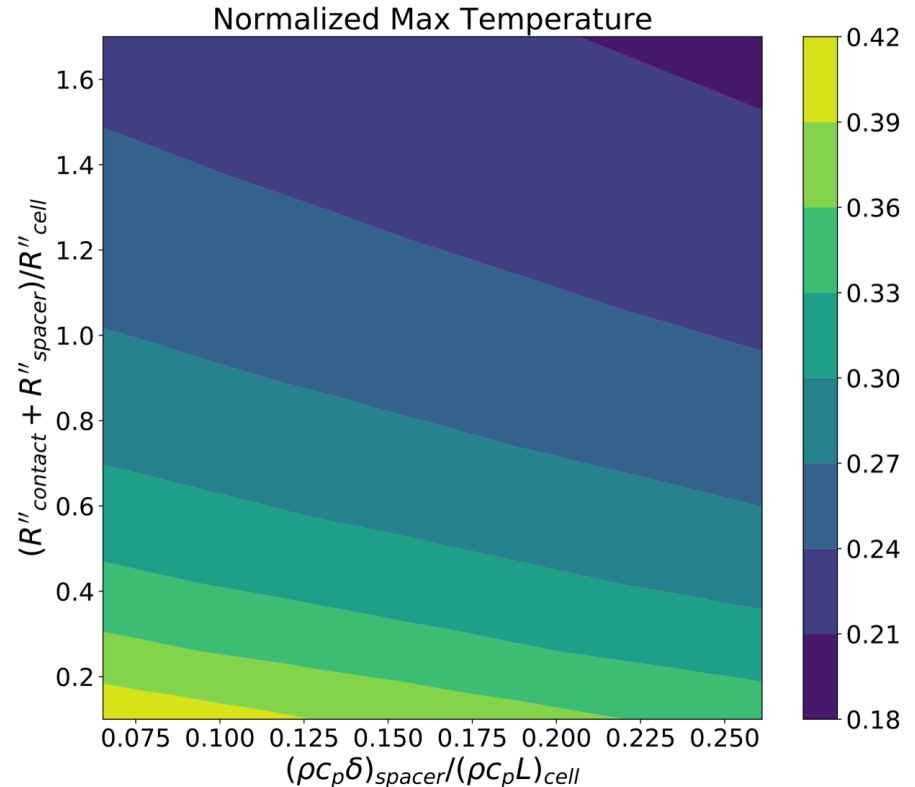
Ratio of temperature rise to get thermal runaway,  $\Delta T_{TR}$ , to the temperature rise of initiating cell,  $T_{h,0} - T_{c,0}$ .

$$\theta_{TR} = \frac{\Delta T_{TR}}{T_{h,0} - T_{c,0}}$$

Normalize max temperature of target cell similarly:

$$\theta_{max} = \frac{T_{c,max} - T_{c,0}}{T_{h,0} - T_{c,0}}$$

No propagation if:  $\theta_{max} < \theta_{TR}$



## Summary: Cell-to-cell failure mitigation

Non-dimensional parameters can be used to describe heat flows.

- Thermal conduction:

$$\frac{1}{Bi} = \frac{R''_{contact}}{(L/\lambda)_{cell}}$$

- Heat capacity:

$$\phi_{struct} = \frac{(\rho c_p \delta)_{struct}}{(\rho c_p L)_{cell}}$$

- TR temp over heat release:

$$\theta_{TR} = \frac{\Delta T_{TR}}{T_{h,0} - T_{c,0}}$$

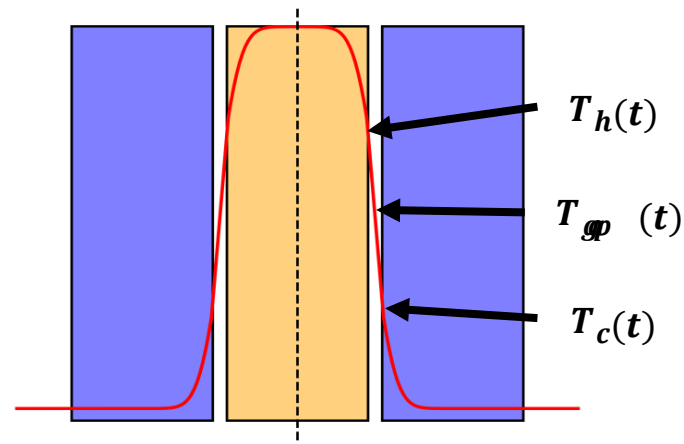
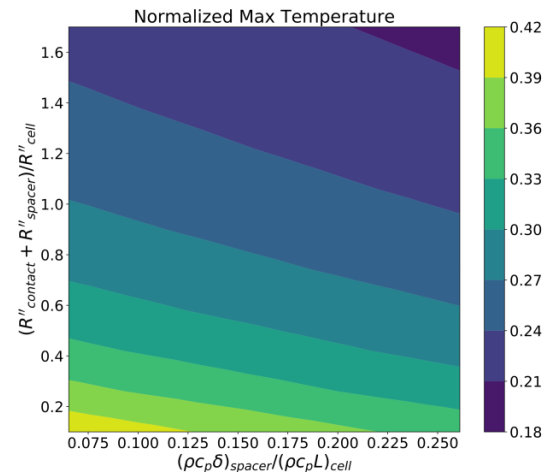
- Propagation criteria

$$\theta_{max}(Bi, \phi_{struct}, T_{h,0} - T_{c,0}) < \theta_{TR}$$

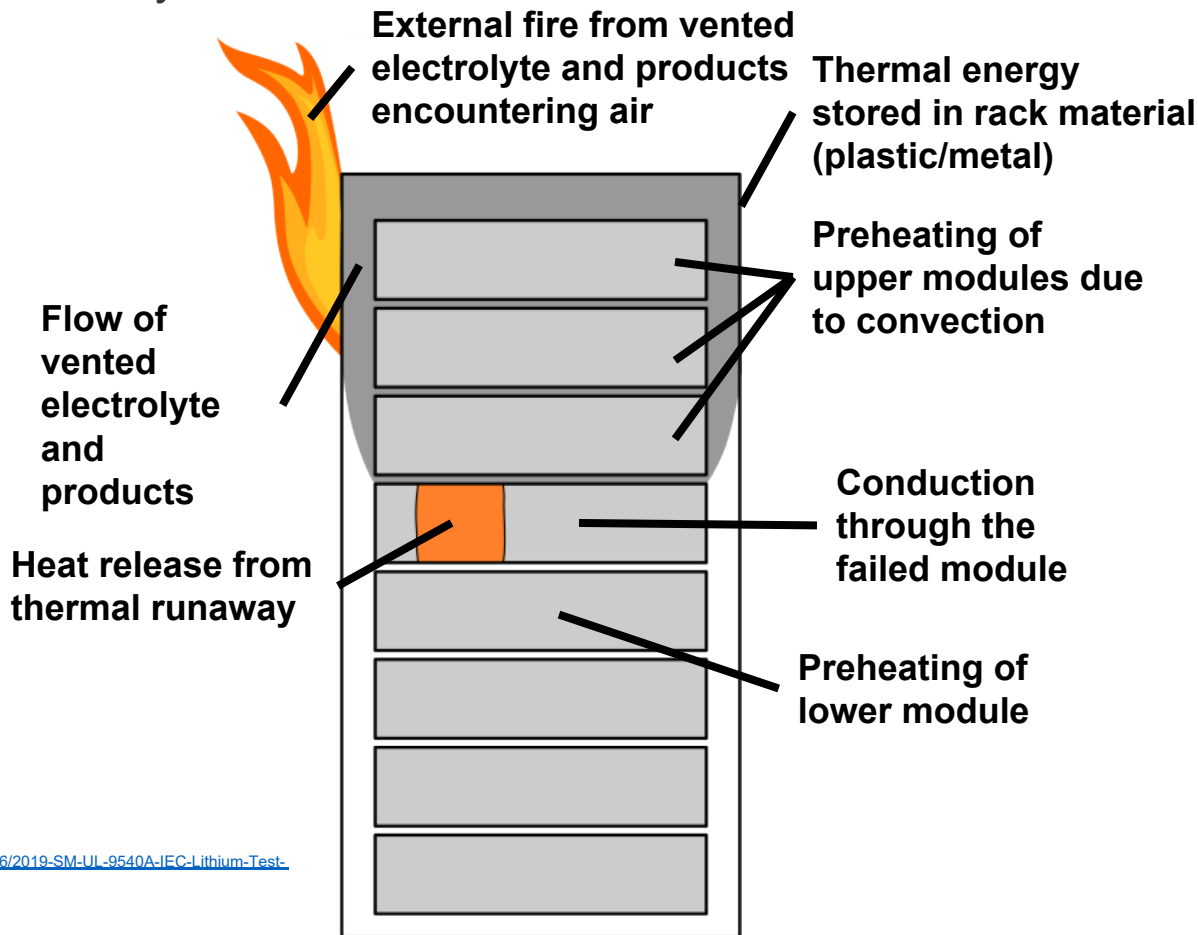
Heat must be removed before the onset of thermal runaway 150~200°C.

Relative time scales of heat flows determine the propagation rate.

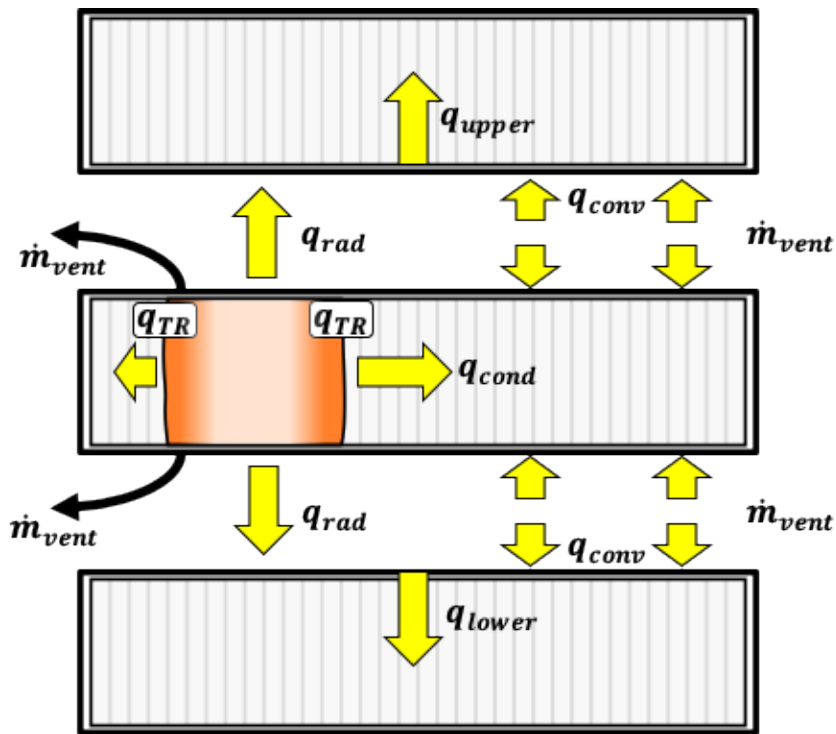
Understanding of heat transfer scales is critical for system design.



## Energy flows at the rack/system scale

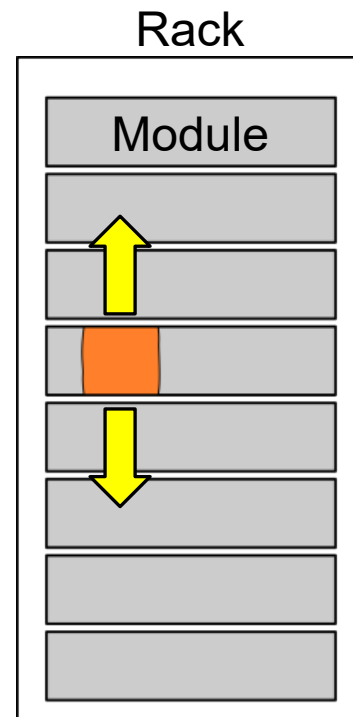
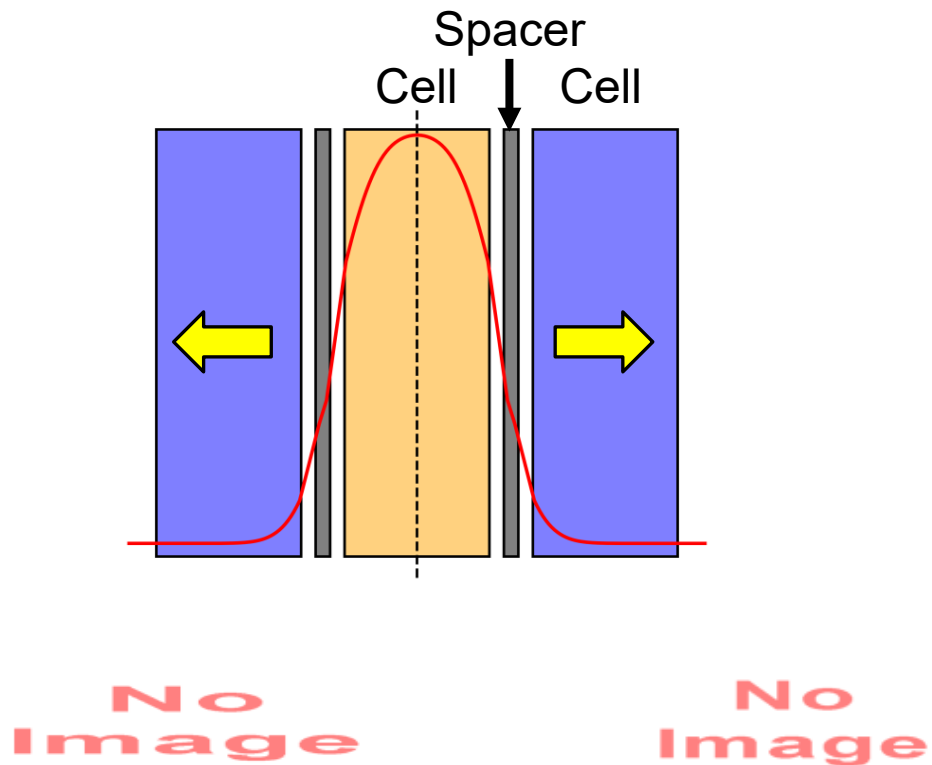


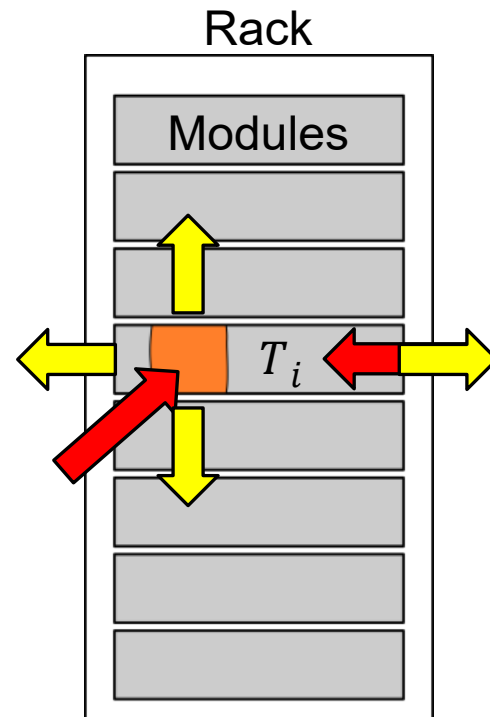
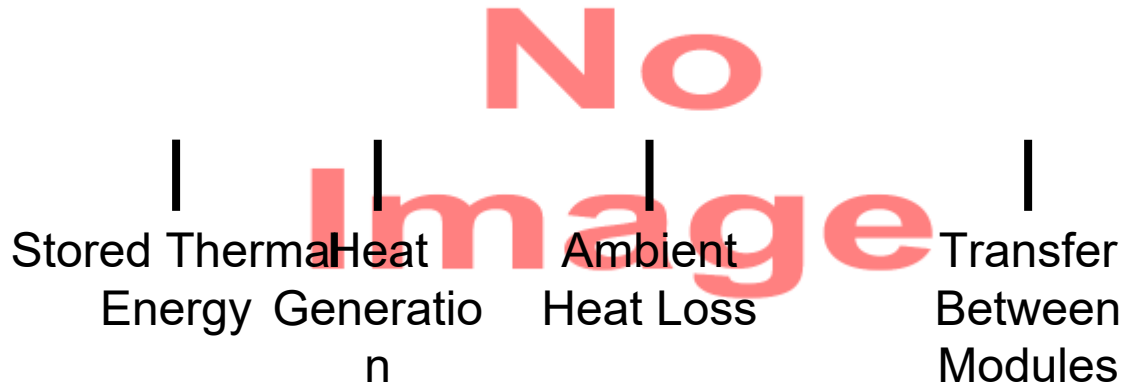
Need a reduced parameter set to span failure scenarios.



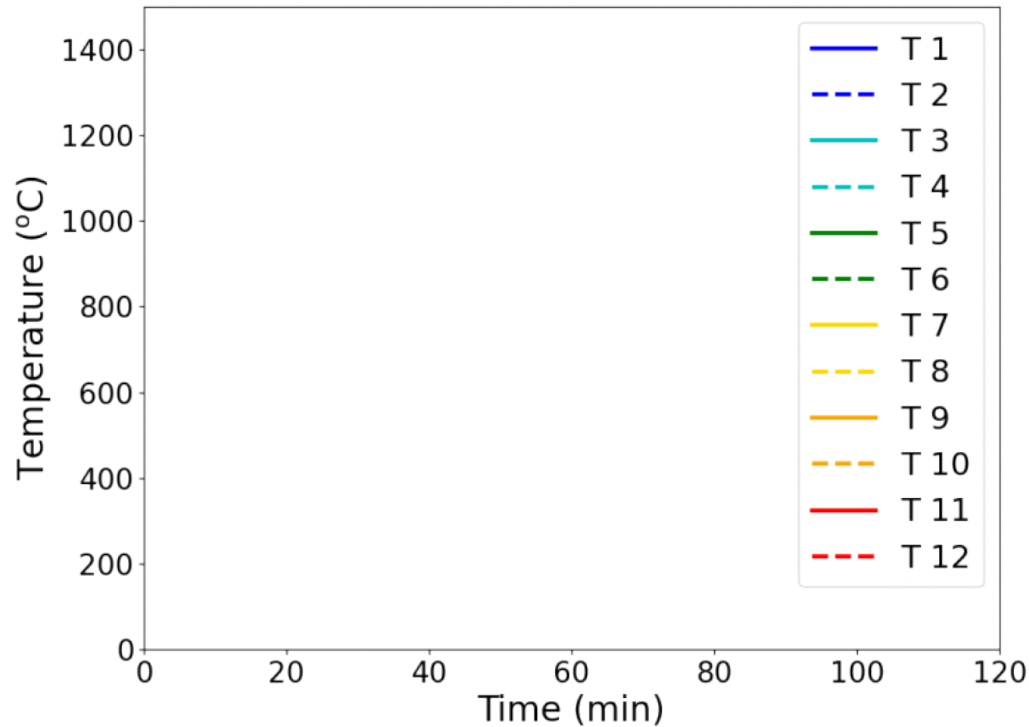


## Extending heat transfer concepts from module to rack scale





## Example scenario: thermal runaway in a rack of 12 modules

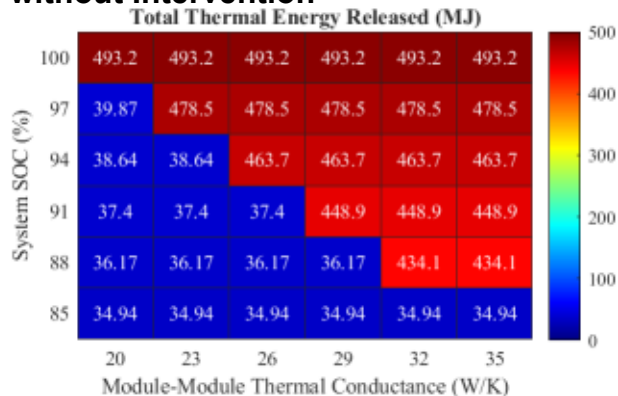
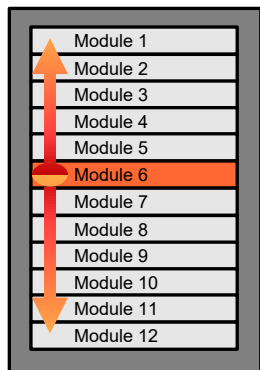


Nominal case consisting of 12 modules at 96% state of charge.

Thermal runaway spreads through the system in about 1 hour.

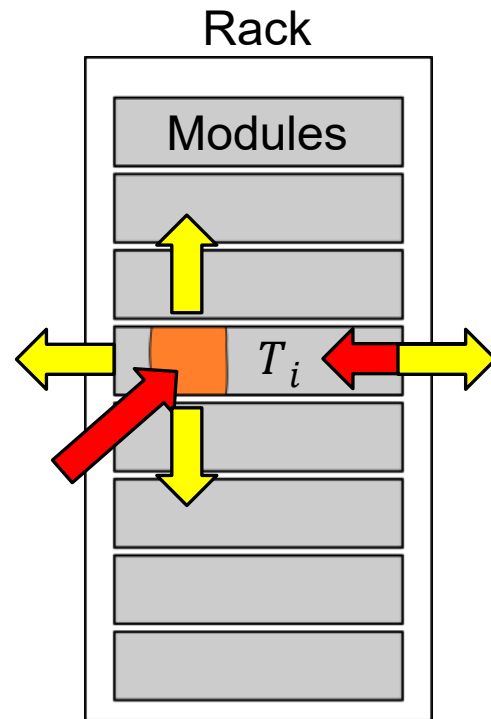
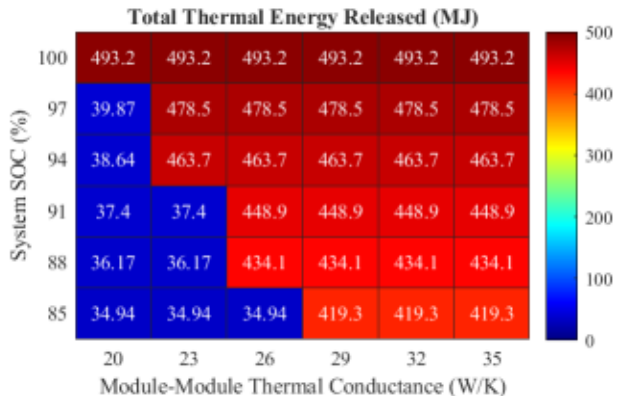
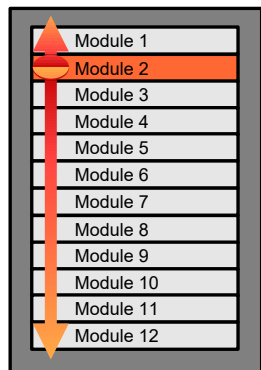


### Module 6 Failure without Intervention



Crude network models allow preliminary simulation of module-to-module propagation

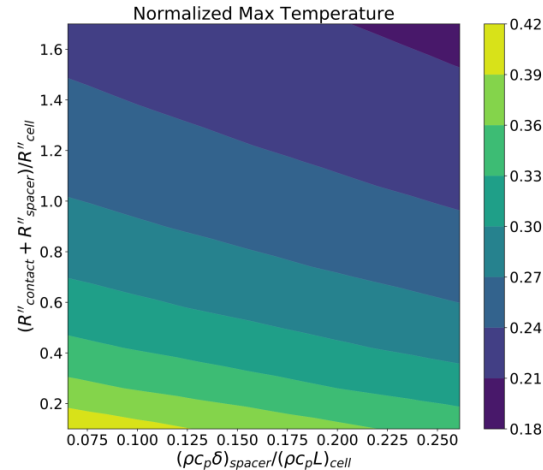
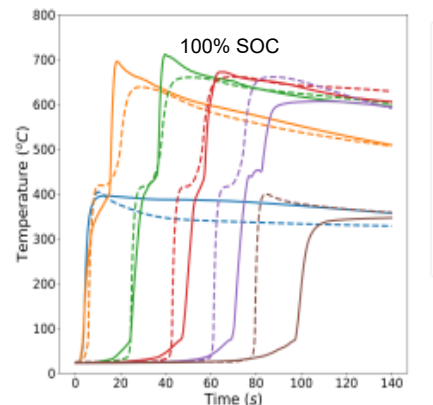
### Module 2 Failure without Intervention



# Summary: Propagation/Mitigation

Finite element model with chemical source terms tested against range of propagation/mitigation experimental data

- Models capture propagation trends including mitigation using plates and insulation between cells.
- Models improve understanding of mitigation:
  - Heat capacity to absorb energy.
  - Thermal resistance to allow heat dissipation along stack and cooling to surroundings.
- Parameter space maps out limits of propagation for above parameters and cell runaway temperature.
  - Moving toward more universal parameter space maps.

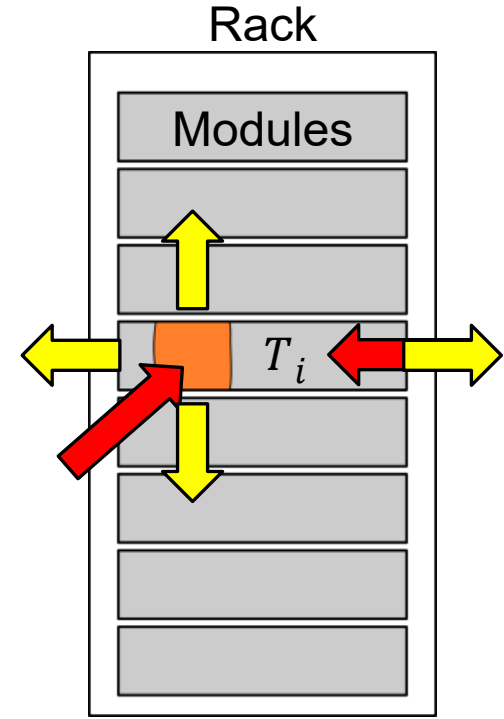
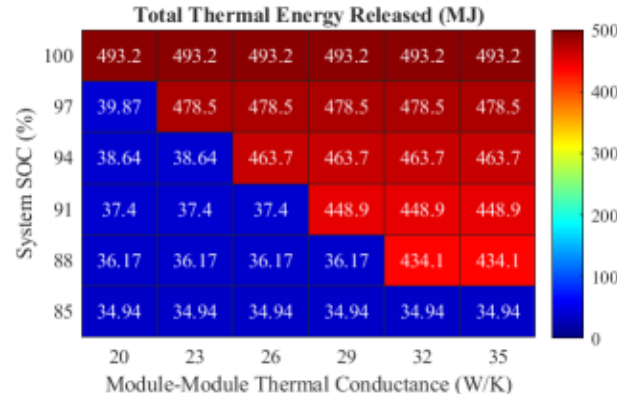


# Summary: Moving toward module-to-module mitigation



- Crude network models allow preliminary simulation of module-to-module propagation

Understanding mitigation boundaries is important for designing safe energy storage systems.







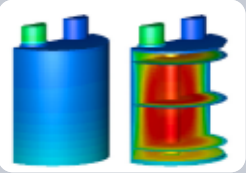
### Materials R&D

- Non-flammable electrolytes and electrolyte salts
- Coated active materials
- Thermally stable materials
- Battery calorimetry



### Testing

- Electrical, thermal, mechanical abuse testing
- Battery calorimetry
- Large scale thermal and fire testing (TTC)
- Failure propagation testing on batteries/systems
- Degradation and diagnostics during and post battery failure



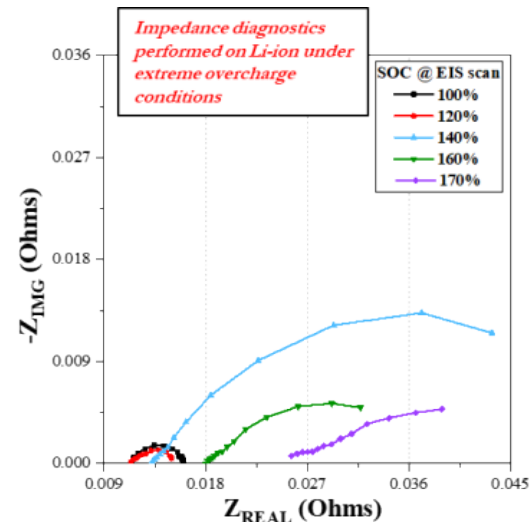
### Simulations and Modeling

- Multi-scale models for understanding thermal runaway
- Validating failure propagation models
- Fire Simulations to predict the size, scope, and consequences of battery fires



### Procedure Development and Stakeholder Interface

- USABC Abuse Testing Manual (SAND 2005 3123)
- OE Energy Storage Safety Roadmap
- R&D programs with NHTSA/DOT to inform best practices, policies, and requirements



Sandia is uniquely positioned to study the entire life cycle of a technology.

New technologies present new risks. A high rigor environment at Sandia allows those risks to be adequately managed.



### Cell and Module Testing Battery Abuse Testing Laboratory (BATLab)



### Battery Pack/System Testing Thermal Test Complex (TTC) and Burnsite



### Battery Calorimetry



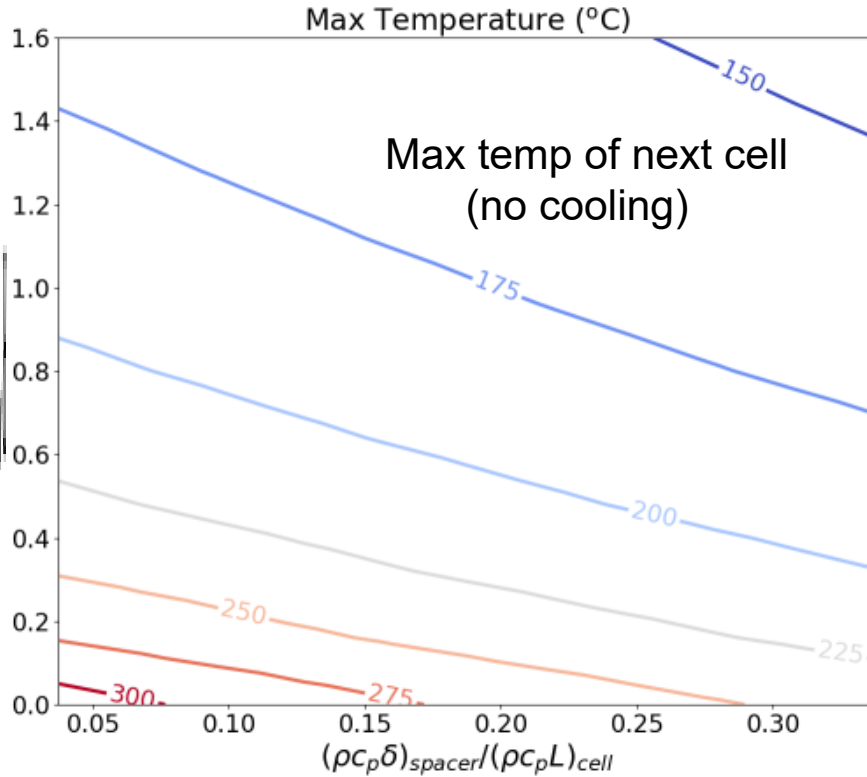


# Thank you

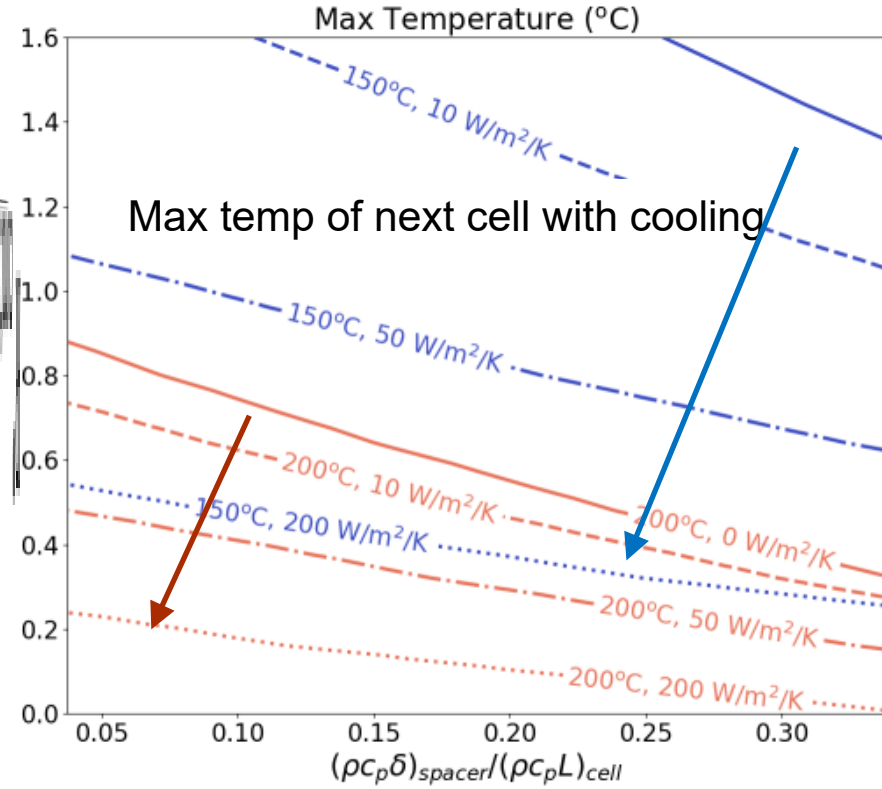
- Funded by the U.S. Department of Energy, Office of Electricity, Energy Storage program under the guidance of Dr. Imre Gyuk, Program Director.
- Sandia National Laboratories is a multi-mission laboratory managed and operated by National Technology and Engineering Solutions of Sandia, LLC., a wholly owned subsidiary of Honeywell International, Inc., for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-NA-0003525.
- For further information: John Hewson - [jchewso@sandia.gov](mailto:jchewso@sandia.gov)



# Map of limiting temperature versus thermal resistance, heat capacity and cooling

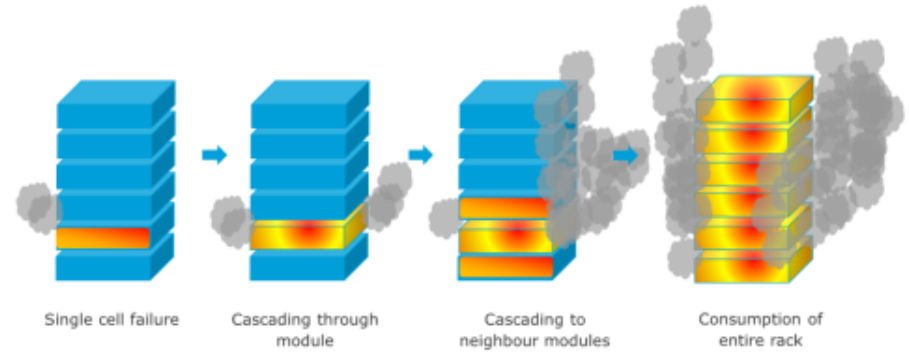
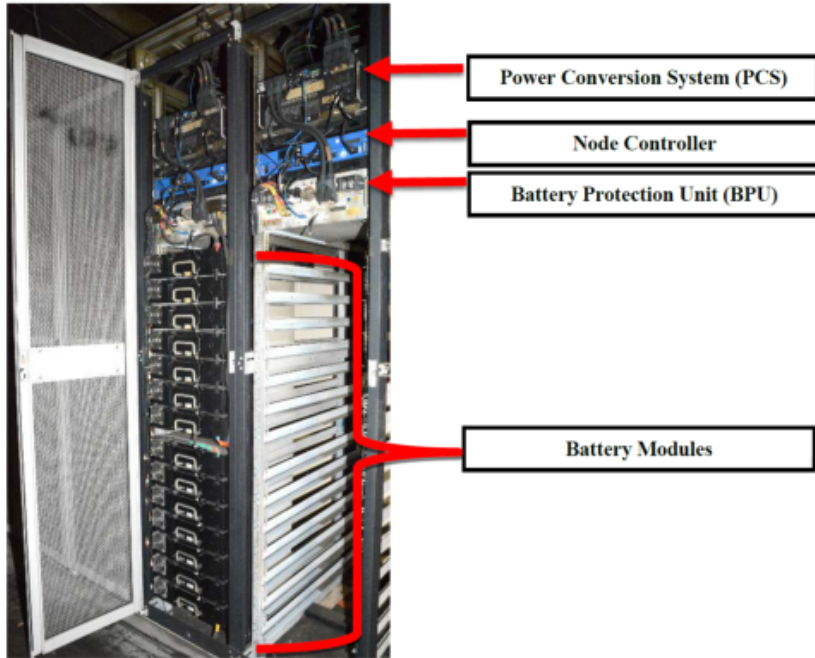


Heat capacity ratio



Heat capacity ratio

# Propagating Thermal Runaway



All images on this slide from: "McMicken Battery Energy Storage System Event - Technical Analysis and Recommendations," DNV GL Energy Insights USA, Inc., Doc. No. 10209302-HOU-R-01, July 18, 2020.