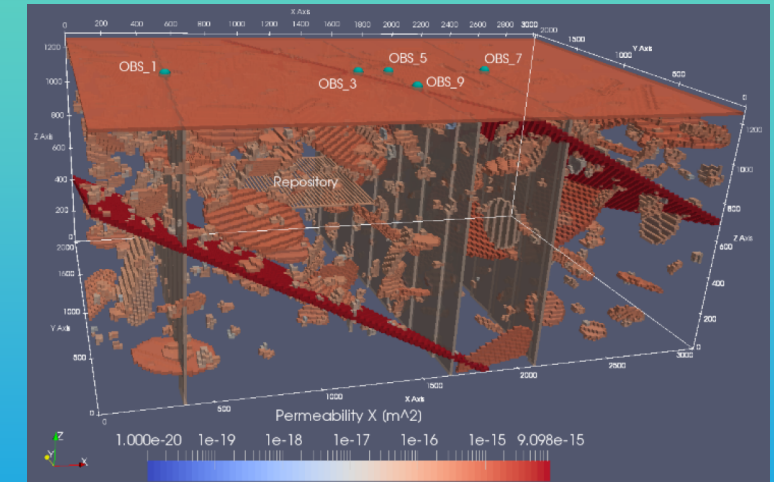




## Spent Fuel and Waste Science and Technology (SFWST)



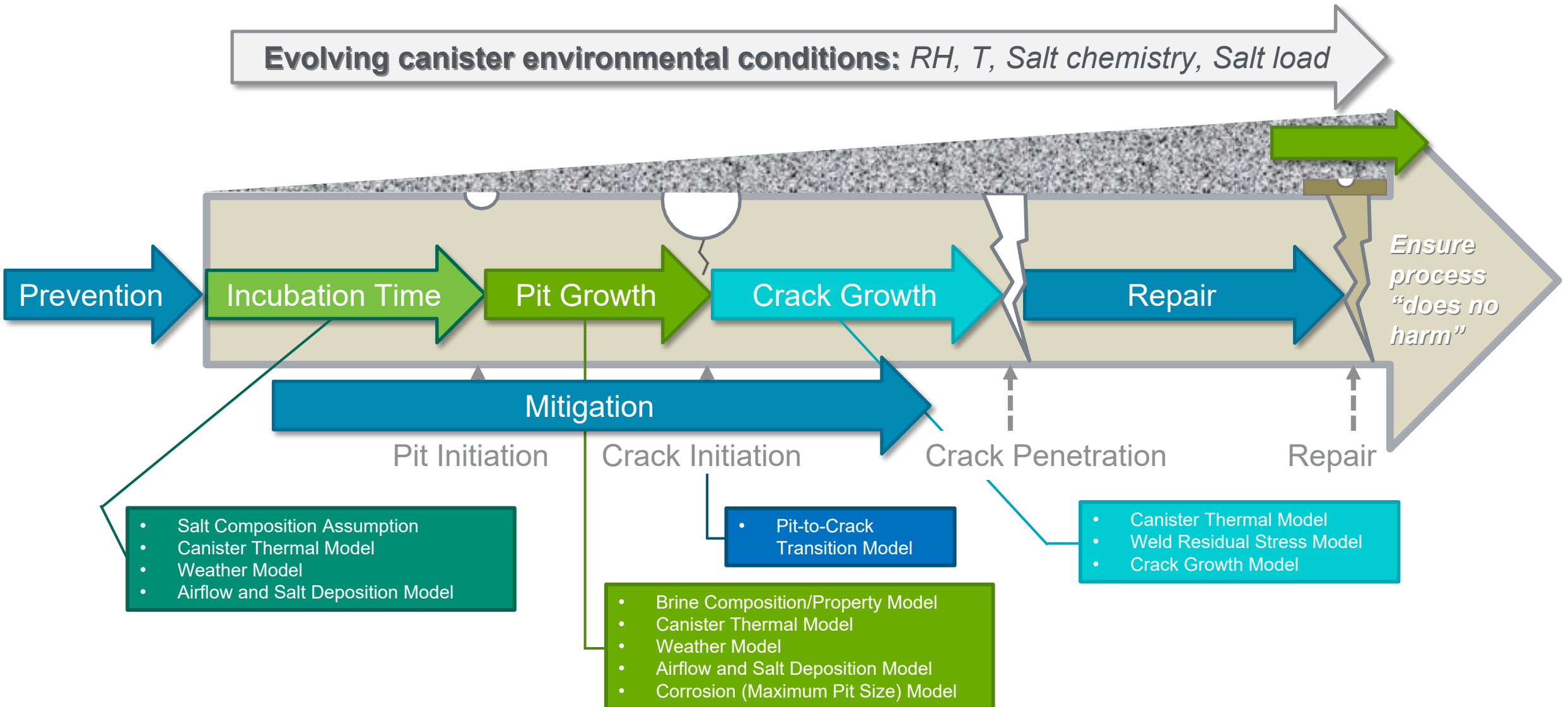
## Evaluation of Coatings and Cold Spray as Potential Mitigation and Repair Strategies

Andrew Knight, Rebecca Schaller,  
Brendan Nation, and Charles Bryan  
Sandia National Laboratories

EPRI ESCP 2022  
November 9, 2022

Sandia National Laboratories is a multi-mission laboratory managed and operated by National Technology and Engineering Solutions of Sandia LLC, a wholly owned subsidiary of Honeywell International Inc. for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-NA0003525.

# Mitigation and Repair

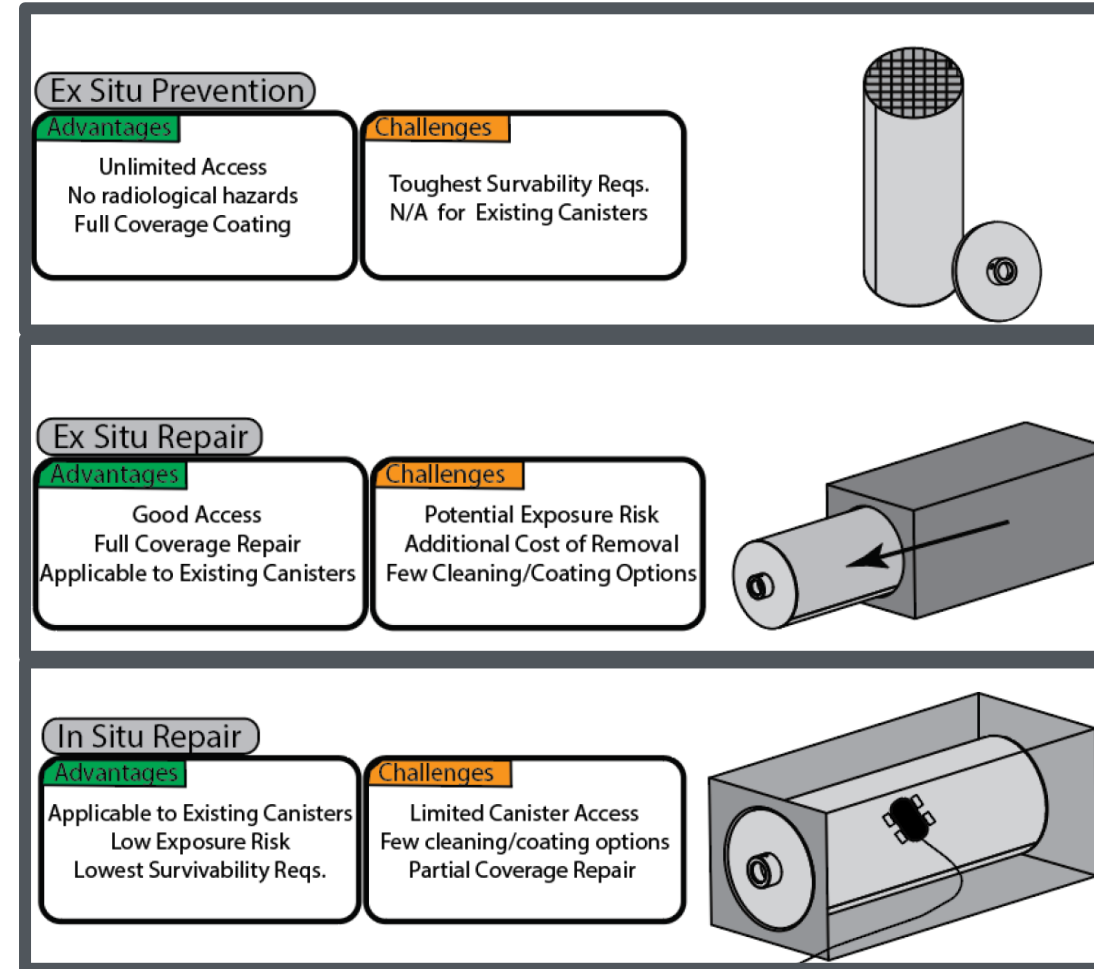


# What Makes an Effective Mitigation and Repair Technology?

- Primary goal of any mitigation and repair technology is to “**Do No Harm**”
- Environment experienced by the coating depends on when it is applied
  - Acceptance criteria dependent on application scenario
- ***What are the acceptance criteria for a particular mitigation and repair technology?***

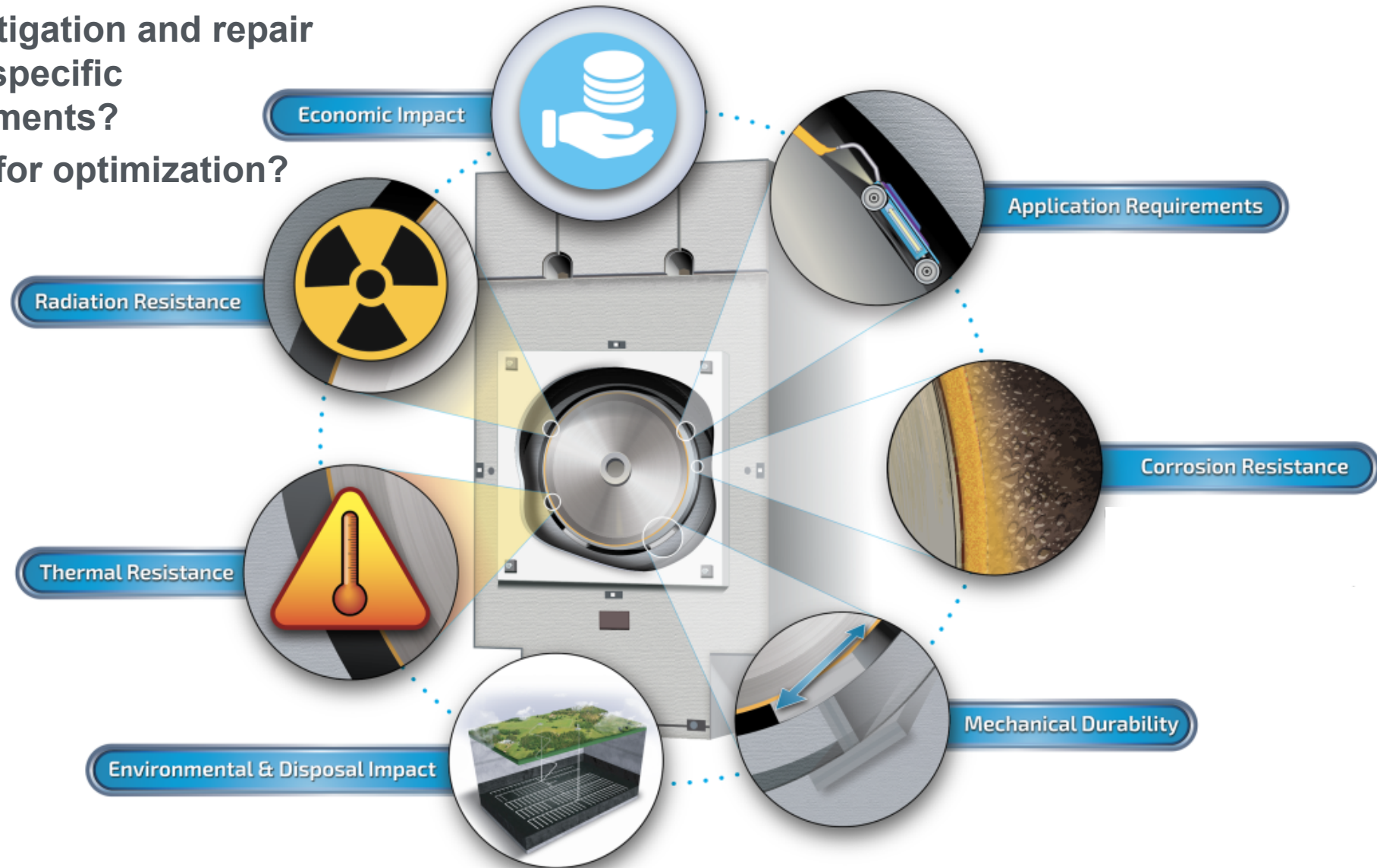
## ***Initial Scoping studies on:***

- 1)) Cold Spray*
- 2)) Coatings technologies*



# Mitigation and Repair Strategies – How to evaluate?

- How to evaluate mitigation and repair strategies without specific guidelines/ requirements?
- What is necessary for optimization?



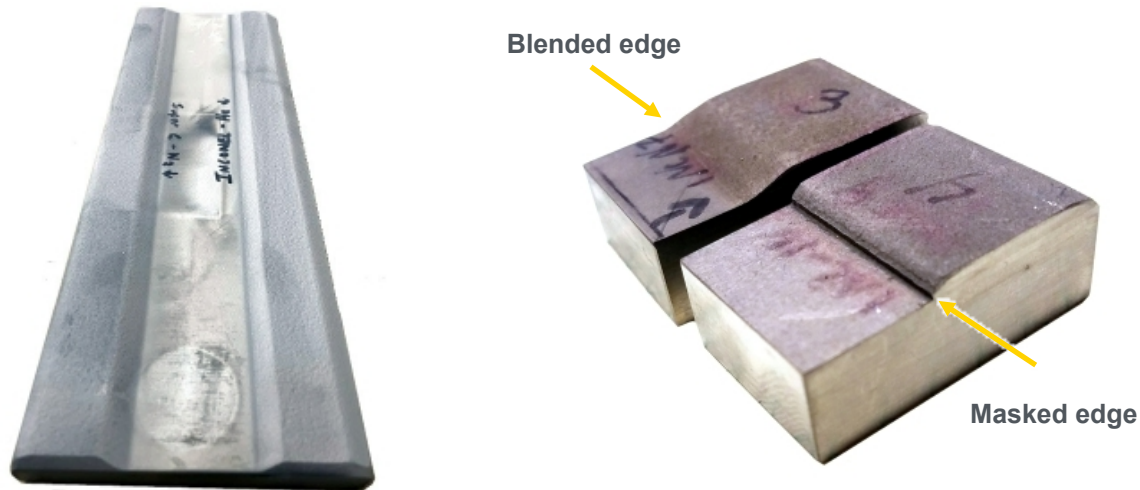


# Cold Spray – Potential Mitigation/Repair Strategy

## “Requirements”:

- Withstand T ~ 300 °F
- Remote Application (6 in. annulus at best)
- Radiation resistance
- Wear resistance
- Corrosion resistance
- “Do no harm”

*Cold Spray is a promising mitigation candidate*



*Cold Spray Samples with Edge Processing*

## *Cold Spray Testing of Samples Provided by PNNL in FY22*

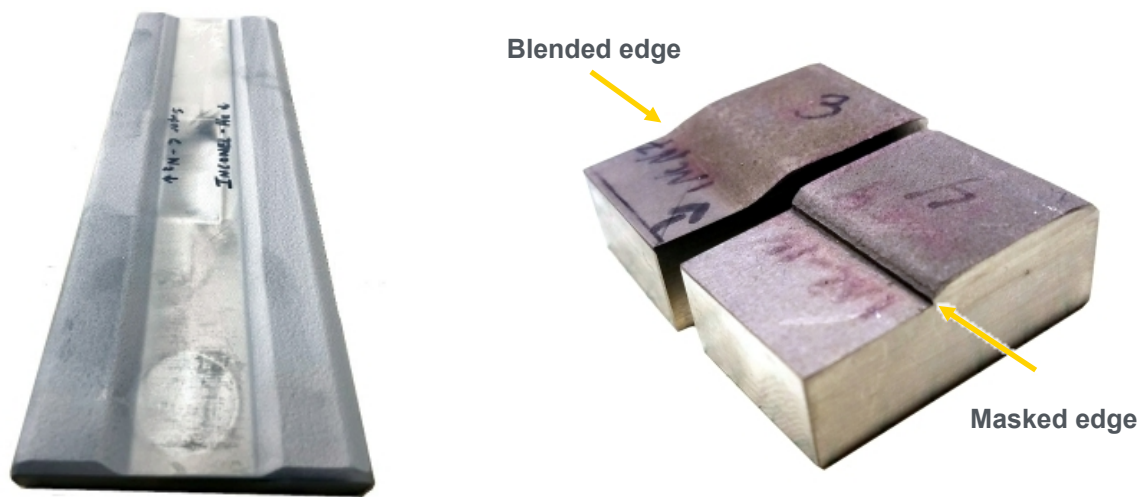
Cold Spray	Edge	Process Gas	Potentiodynamic Polarization		Accelerated Pitting Exposure	Atmospheric Exposure			Boiling MgCl <sub>2</sub> Exposure
			NaCl	FeCl <sub>3</sub>		40 % RH, 35 °C	75 % RH, 35 °C	Cyclic	
Inc	Tapered	He	X	X	X	X	-	X	X
Inc	Tapered	N	X	X	X	-	-	X	X
Inc	Masked	N	-	-	X	X	X	X	X
Ni	Tapered	N	X	X	X	X	-	X	X
Ni	Masked	N	-	-	X	X	X	X	X
Ni	Tapered	He	-	-	X	-	-	-	-
Ni	Masked	He	-	-	X	-	-	-	-
SC	Tapered	N	X	X	X	X	X	X	-
SC	Tapered	He	-	-	X	-	-	-	-
SC	Masked	He	-	-	X	-	-	-	-
SS316 + 25% CrC 410	Tapered	N	-	-	X	-	-	-	-
SS316 + 25% CrC 410	Tapered	N	-	-	X	-	-	-	-
SS316 + 25% CrC 410	Tapered	N	-	-	X	-	-	-	-

# Cold Spray – Potential Mitigation/Repair Strategy

## “Requirements”:

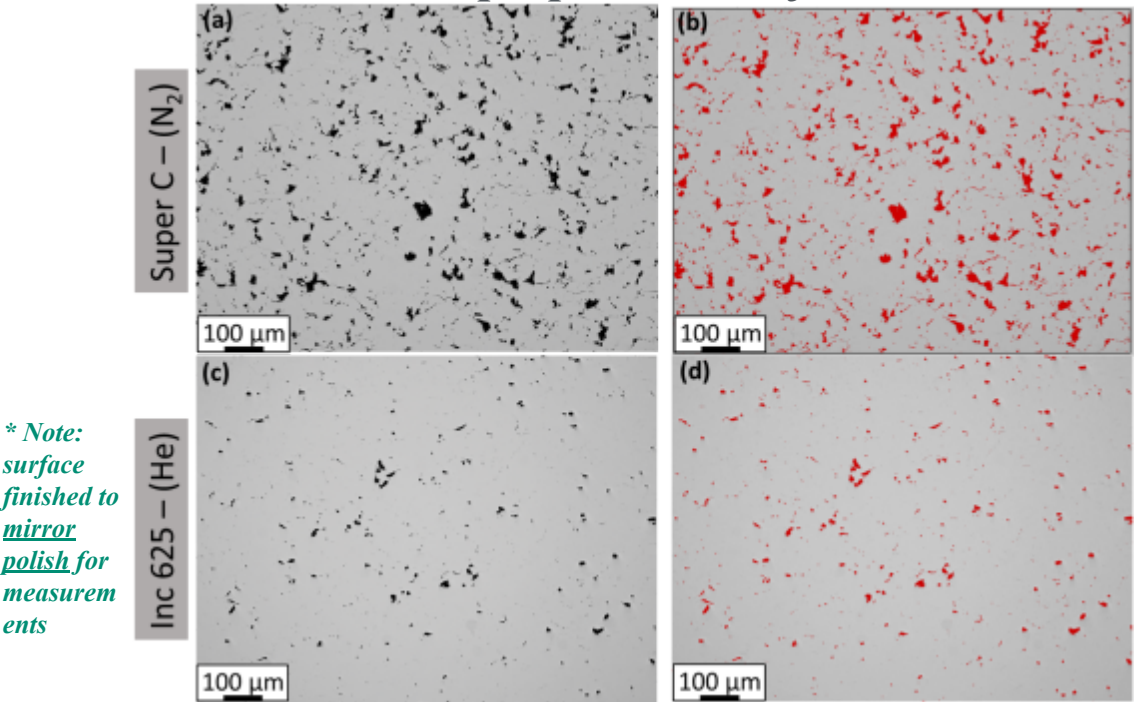
- Withstand T ~ 300 °F
- Remote Application (6 in. annulus at best)
- Radiation resistance
- Wear resistance
- Corrosion resistance
- “Do no harm”

Cold Spray is a promising mitigation candidate



Cold Spray Samples with Edge Processing

## Example polished surfaces



## Porosity Measurements:

- Calculated from image processing of bright field optical measurements
- Influenced by carrier gas type

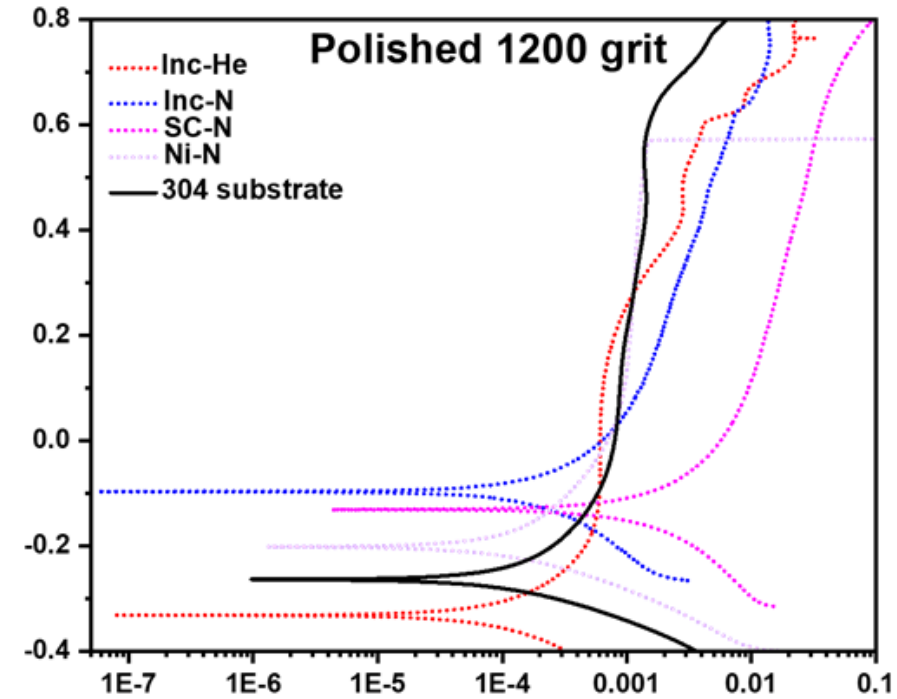
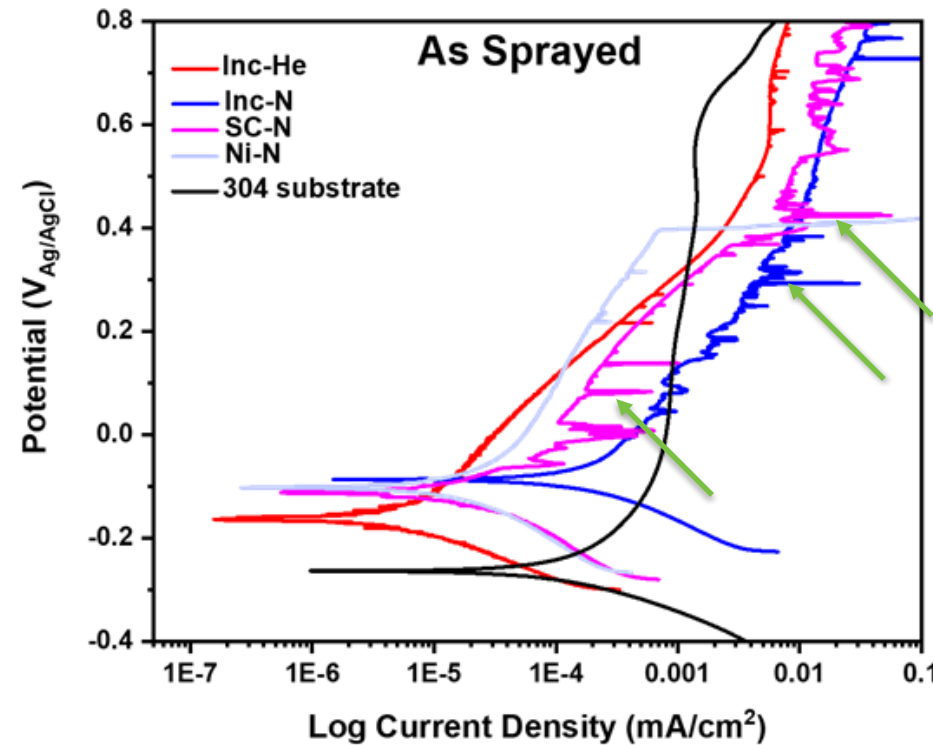
PNNL M3 Report 2021

CS	Super C (N <sub>2</sub> )	Inc-625 (He)	Inc-625 (N <sub>2</sub> )	Ni (N <sub>2</sub> )
Porosity (%)	5.51 ± 0.44	1.21 ± 0.20	5.79 ± 0.18	3.78 ± 0.59

# Cold Spray – Accelerated testing for optimization

## Electrochemical Characterization:

- 0.6 M NaCl
- 1 h Open circuit potential followed by anodic polarization, 0.1667 mV/s
- CS or base material examined
  - As-sprayed, 600, and 1200 grit



**Metastable pitting reduced when polished**



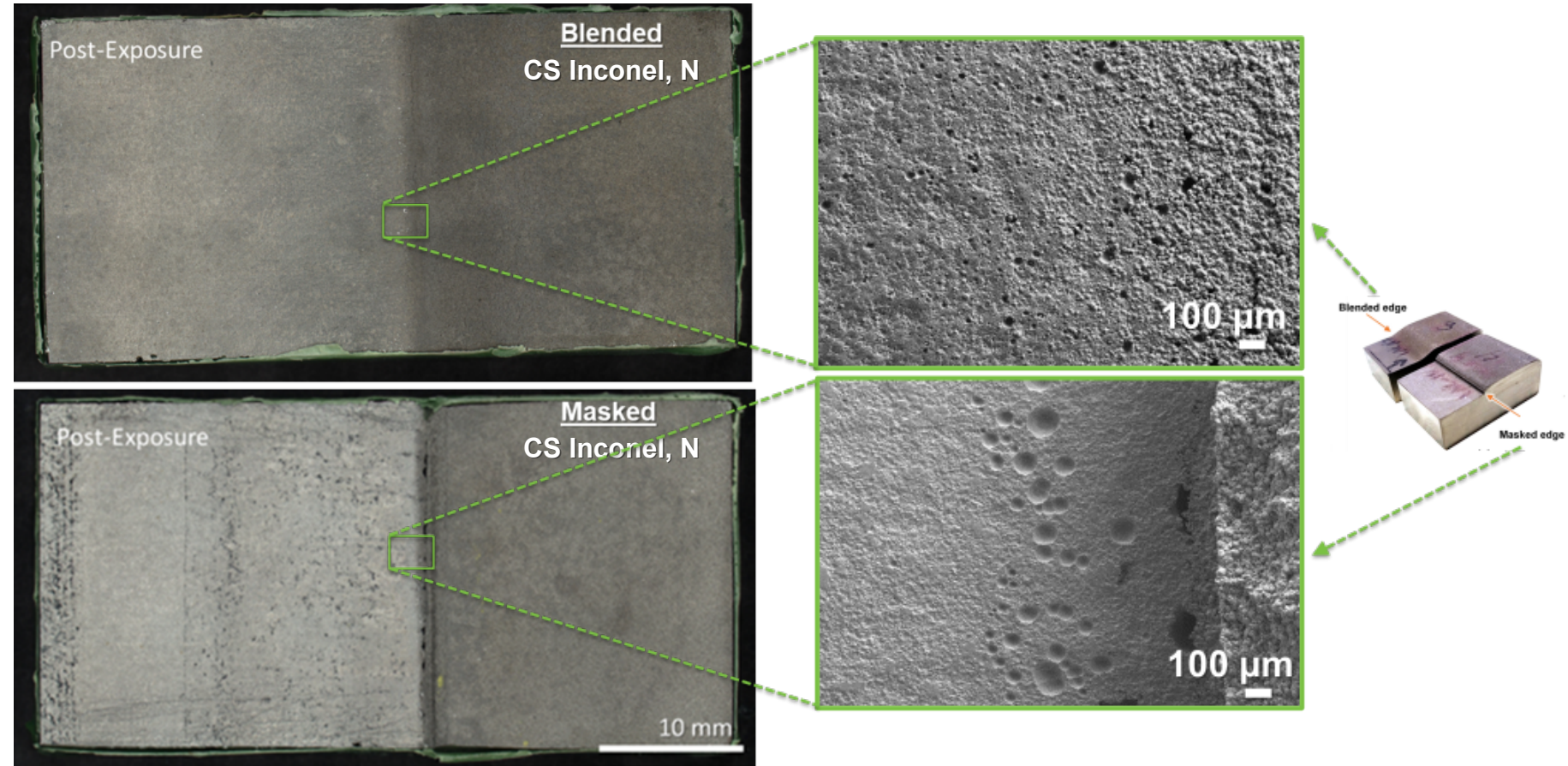
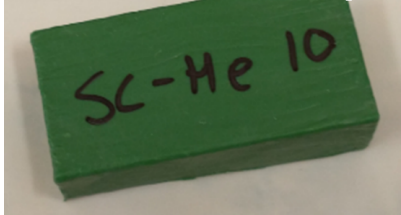
# Cold Spray – Accelerated testing for optimization

## Pitting

### Characterization:

- 6% by mass Ferric Chloride
- Full Immersion 72 h, 22 °C
- Entire top surface tested
  - Other surfaces painted

CS Painted Sample



**Edge morphology influences corrosion morphology**

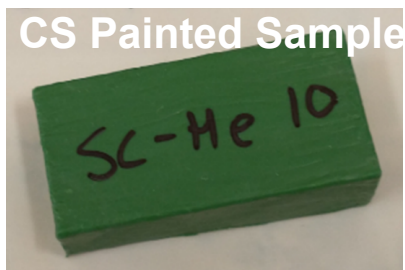


# Cold Spray – Accelerated testing for optimization

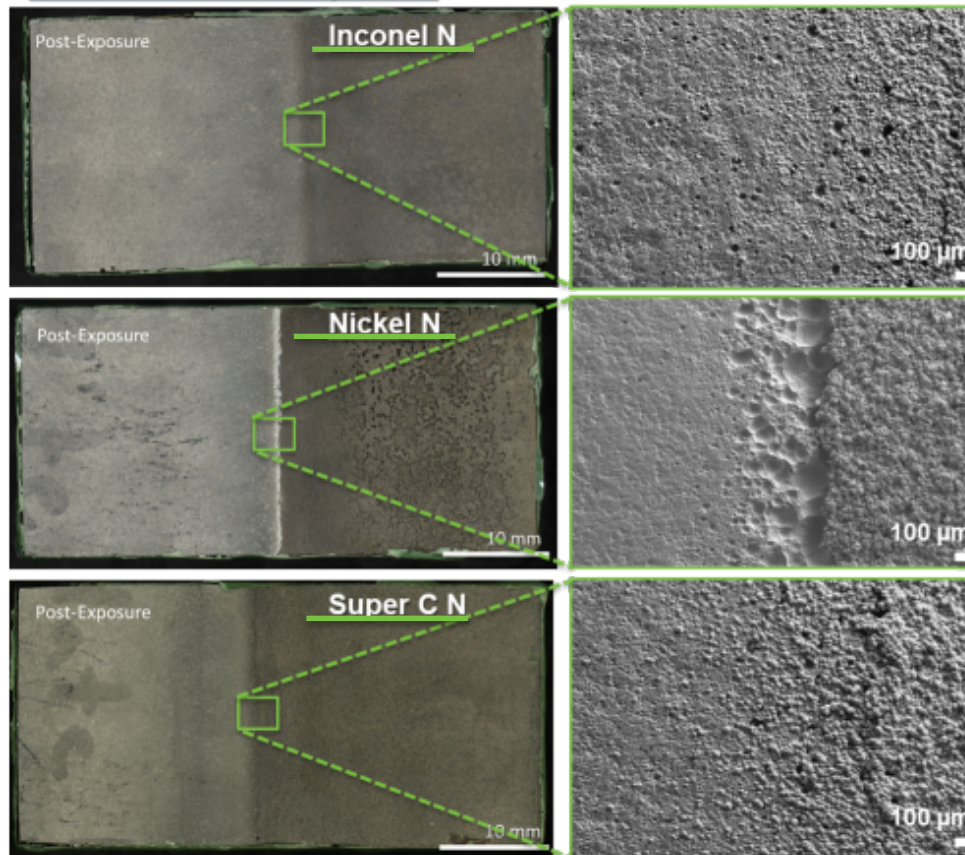
## Pitting

### Characterization:

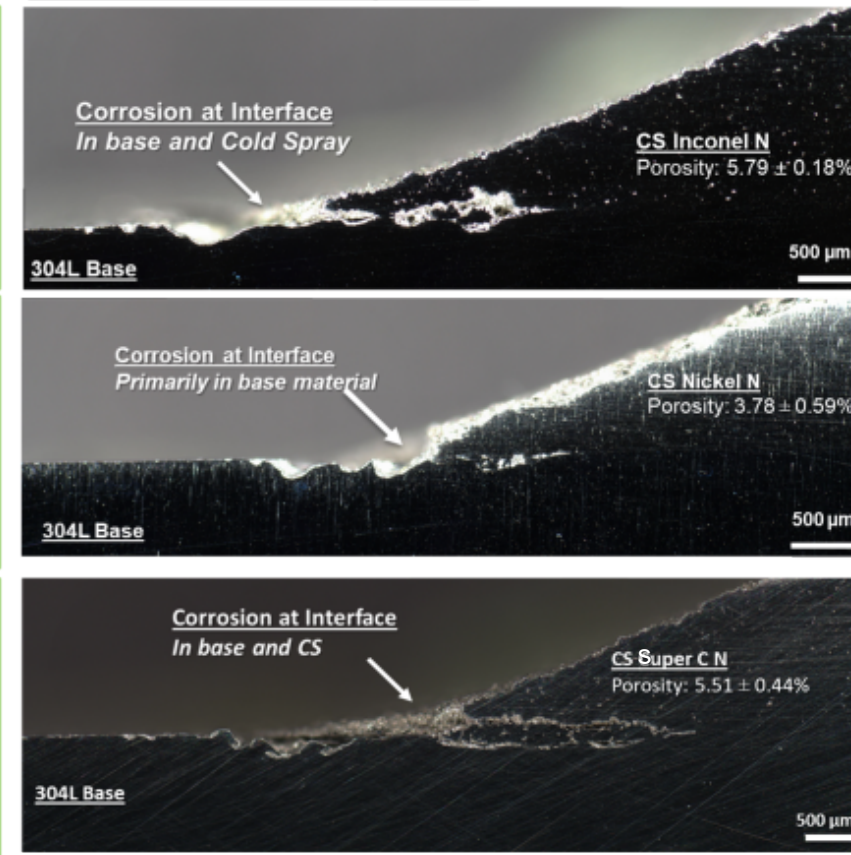
- 6% by mass Ferric Chloride
- Full Immersion 72 h, 22 °C
- Entire top surface tested
  - Other surfaces painted



Post ASTM G-48 Exposure



Cross section Post Exposure



**Attack at interface influenced by cold spray material**

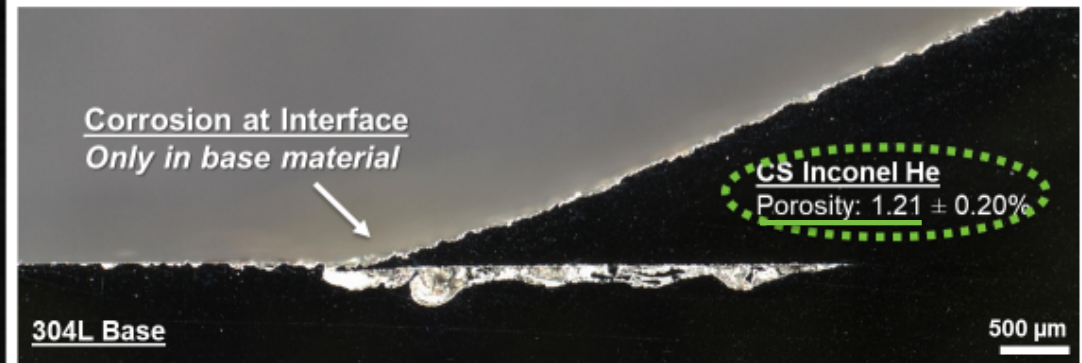
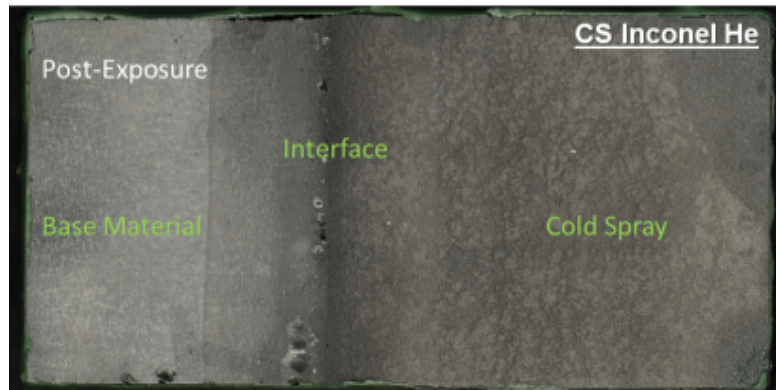
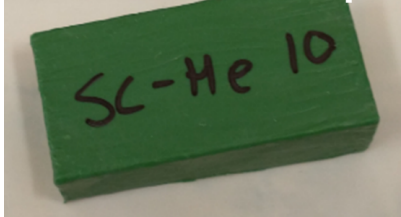
# Cold Spray – Accelerated testing for optimization

## Pitting

### Characterization:

- 6% by mass Ferric Chloride
- Full Immersion 72 h, 22 °C
- Entire top surface tested
  - Other surfaces painted

CS Painted Sample



**Process gas can influence porosity and thus corrosion at the interface**



# Cold Spray – Comparison to Atmospheric Exposures

## Pitting

### Characterization:

- Ferric chloride test compared to atmospheric exposure:
  - 1 month exposure at 75% RH and 35°C with 300  $\mu\text{g}/\text{cm}^2$  Artificial seawater

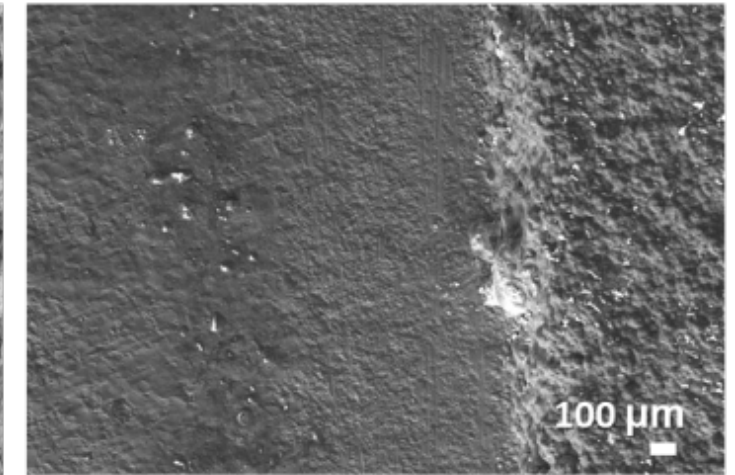
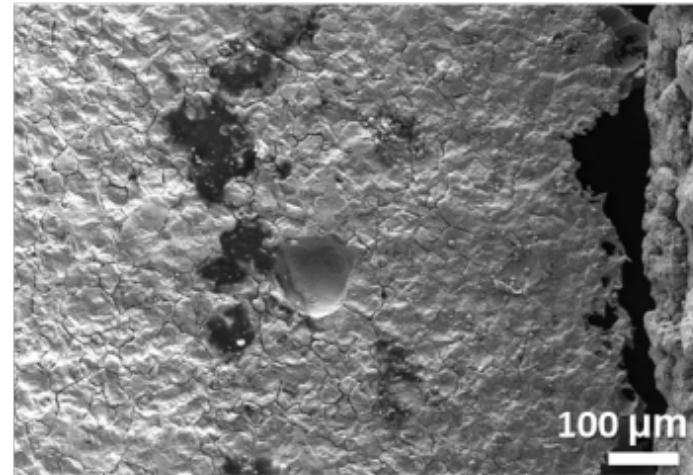
**Corrosion morphology is similar for accelerated full immersion exposures and atmospheric exposures**

### Ni-N Masked

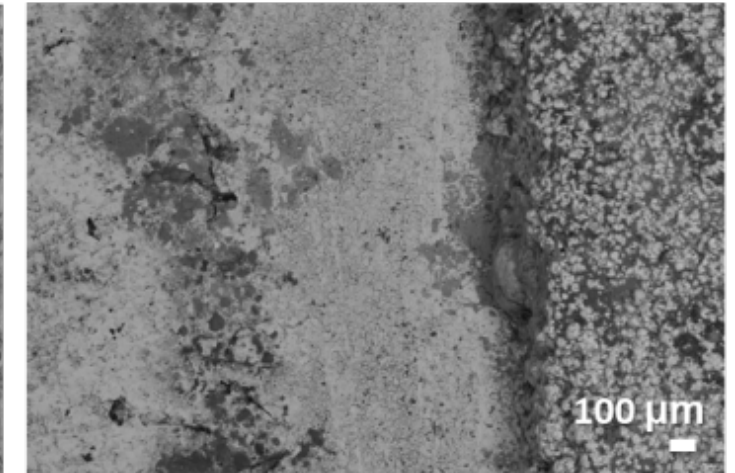
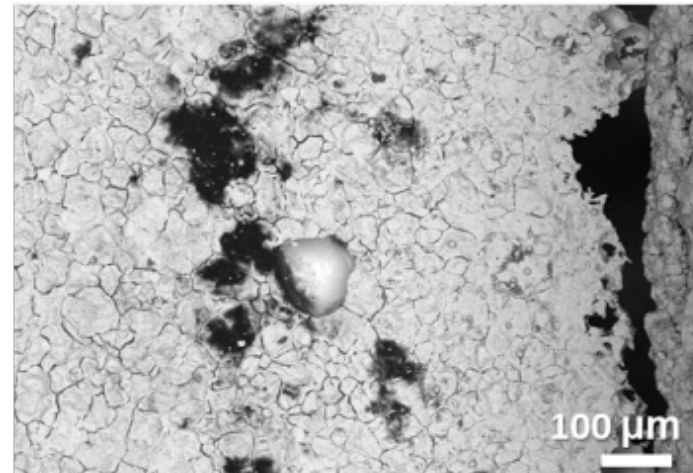
FeCl<sub>3</sub> accelerated pitting

75% RH 35°C w/ seawater

SEM-SE

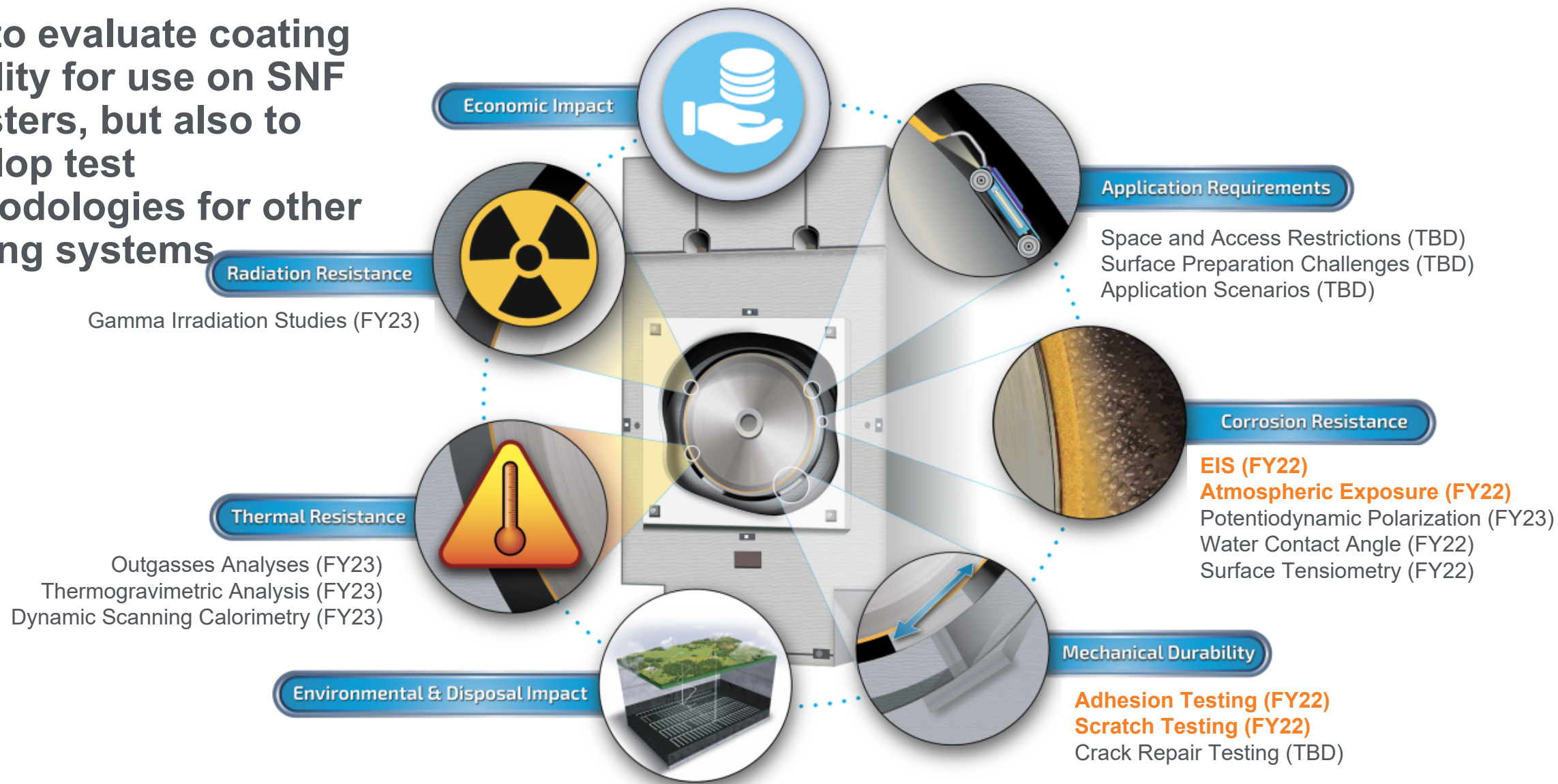


SEM-BSE



# Evaluating Coating Performance

Aim to evaluate coating viability for use on SNF canisters, but also to develop test methodologies for other coating systems



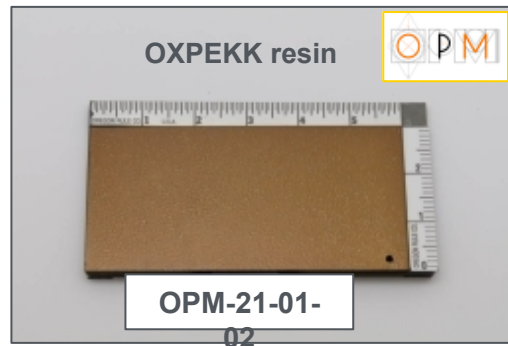


# Corrosion Resistant Coatings

Naming Convention  
VENDOR-YEAR-VARIANT#-COUPON#

4 collaborating companies, 11 total coating variants (\*adding 2 Coatings from TDA, Research in FY23)

## Polymeric (5)



2 variants of Polyetherketoneketone. High temperature thermoplastic with high radiation resistance

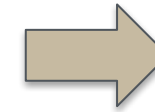


3 variants of modified polyimide, polyurea, phenolic resins. Durable, chemically inert and can be loaded with desired additives to increase corrosion and radiation resistance

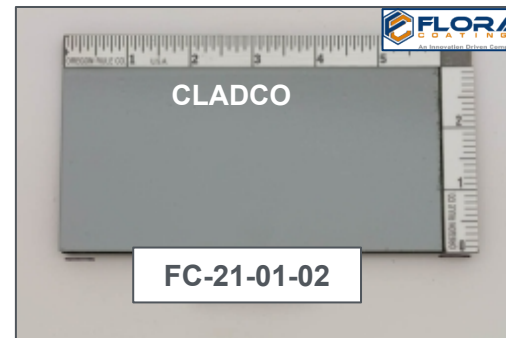
## Ceramic/Organic



2 variants of GENTOO with and without Zn-rich primer to provide a durable ceramic hybrid inorganic/polymer coating with/without galvanic protection



## With Zn-Rich



Single component hybrid inorganic/modified polyurethane coating resulting in a quasi-ceramic structure.

*More detail  
can be found  
in our recent  
report*

*FY22 Status: Corrosion-Resistant Coatings on Spent Nuclear Fuel Canisters to Mitigate and Repair Potential Stress Corrosion Cracking*

[Spent Fuel and Waste Disposition](#)

# Atmospheric Exposures

## Colorimetric Assessment and visible inspection to track possible coating degradation

Coupon ID	Baseline	After 30-day Exposure
WHRD-21-03-06		
WHRD-21-03-08		
WHRD-21-02-08		
WHRD-21-02-06		
WHRD-21-01-06		
WHRD-21-01-08		
OPM-21-02-06		
OPM-21-02-08		
OPM-21-01-08		
OPM-21-01-06		
LUNA-21-05-08		
LUNA-21-05-06		
LUNA-21-04-06		
LUNA-21-04-08		
LUNA-21-03-08		
LUNA-21-03-06		
LUNA-21-02-06		
LUNA-21-02-08		
LUNA-21-01-06		
LUNA-21-01-08		
FC-21-01-08		
FC-21-01-06		

WHRD-21-02-08

Delamination

OPM-21-02-06

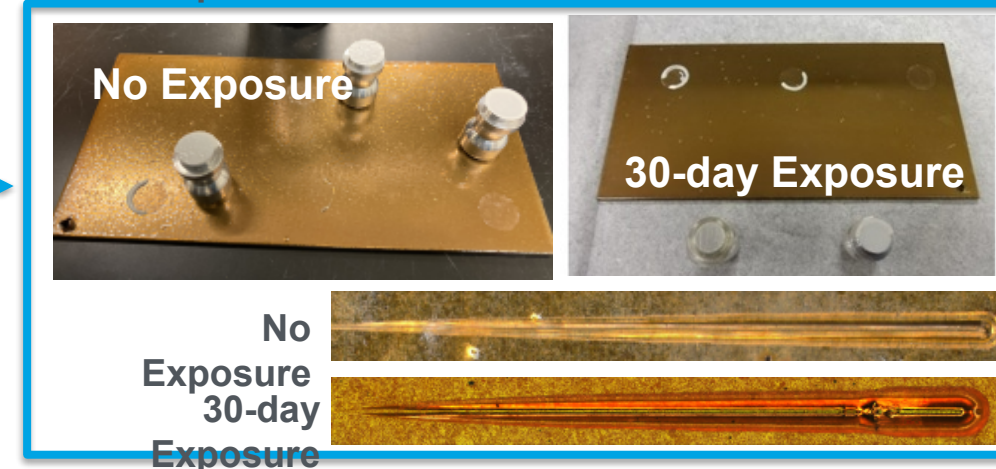
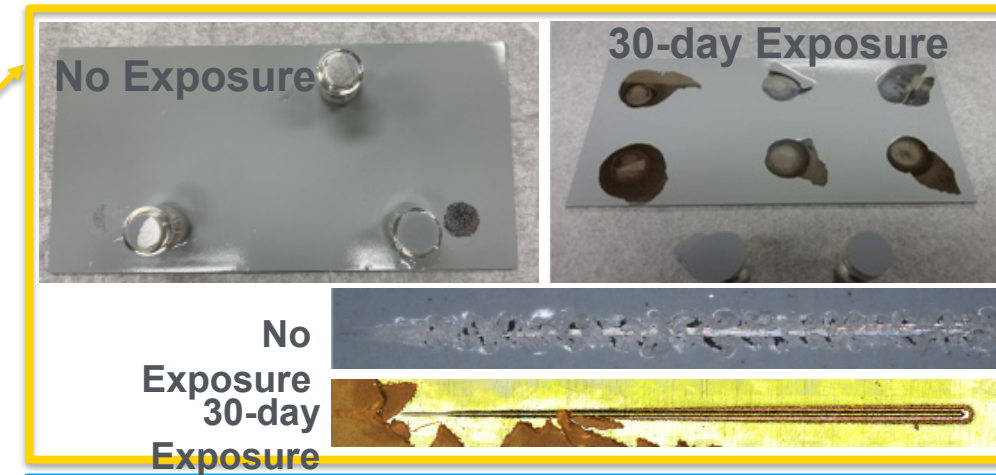
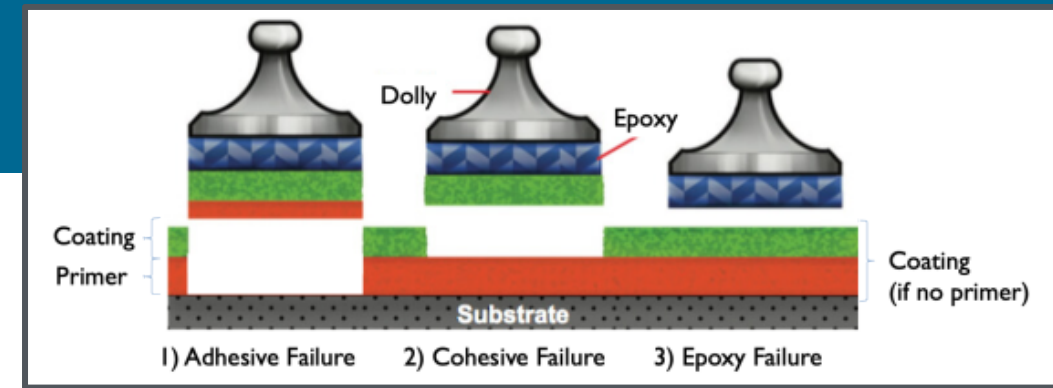
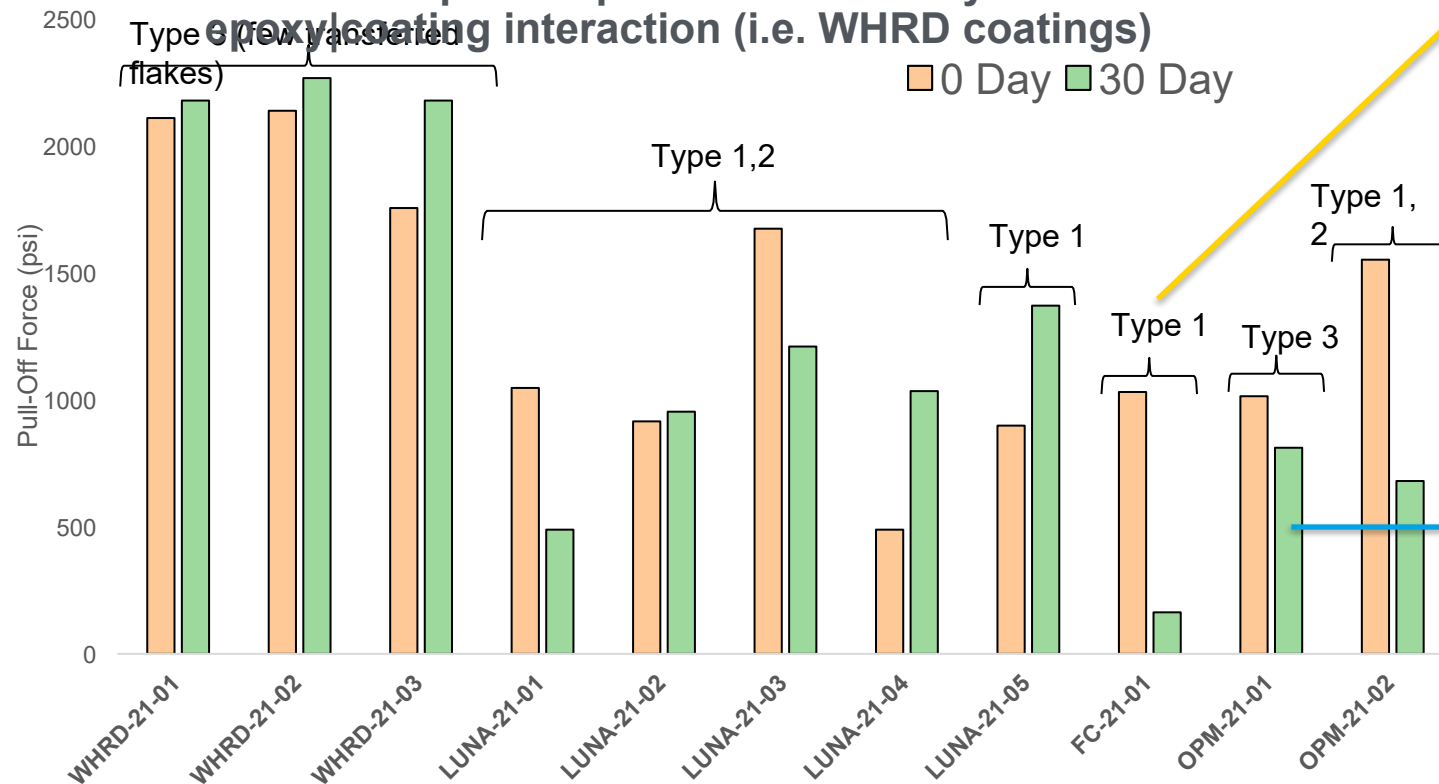
OPM-21-02-02 Baseline had evidence of "mud cracking"

LUNA-21-02-08

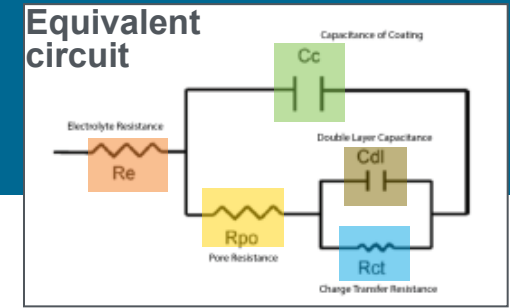
# Adhesion and Scratch

The adhesive strength of...

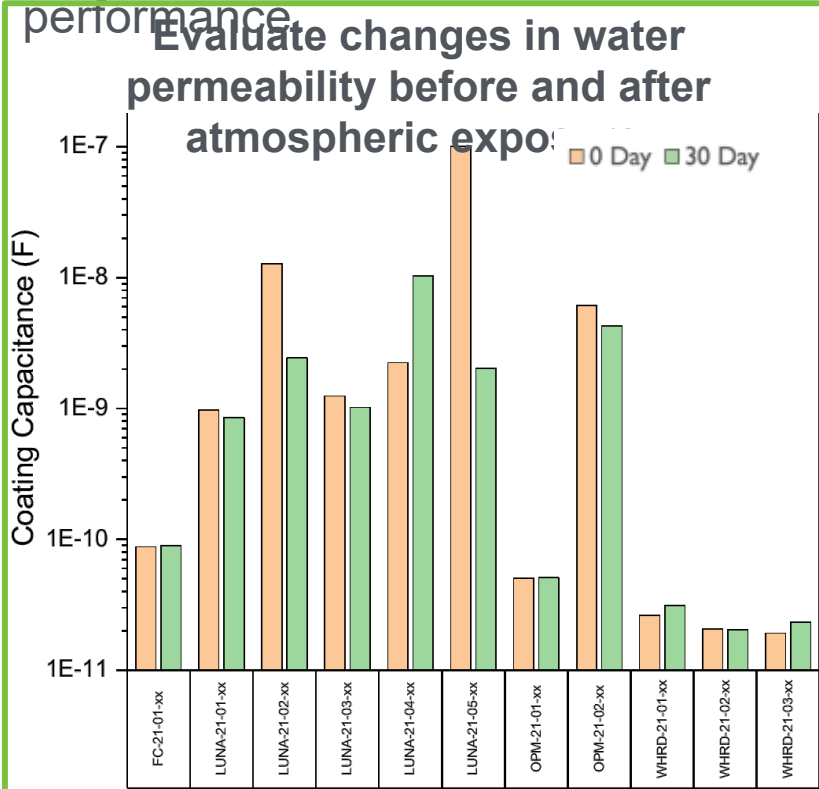
- Ceramic coatings generally decreased following atmospheric exposure.
  - In most cases, adhesive failure was observed
- Organic coatings generally did not fail to the substrate
  - Except OPM-21-02
  - Increase in pull-off pressure was likely due to increase in epoxy/coating interaction (i.e. WHRD coatings)



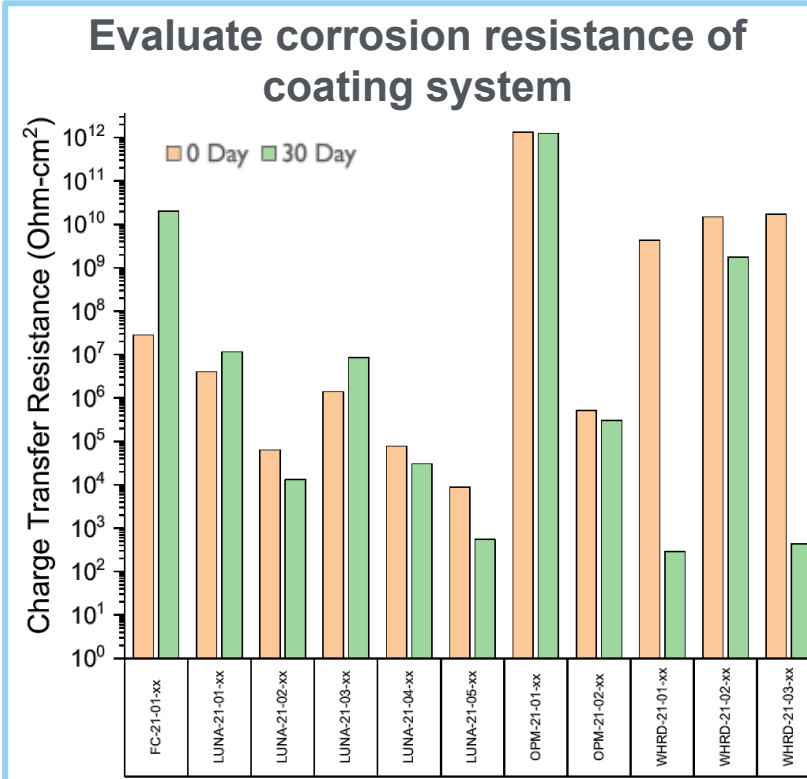
# Electrochemical Impedance Spectroscopy



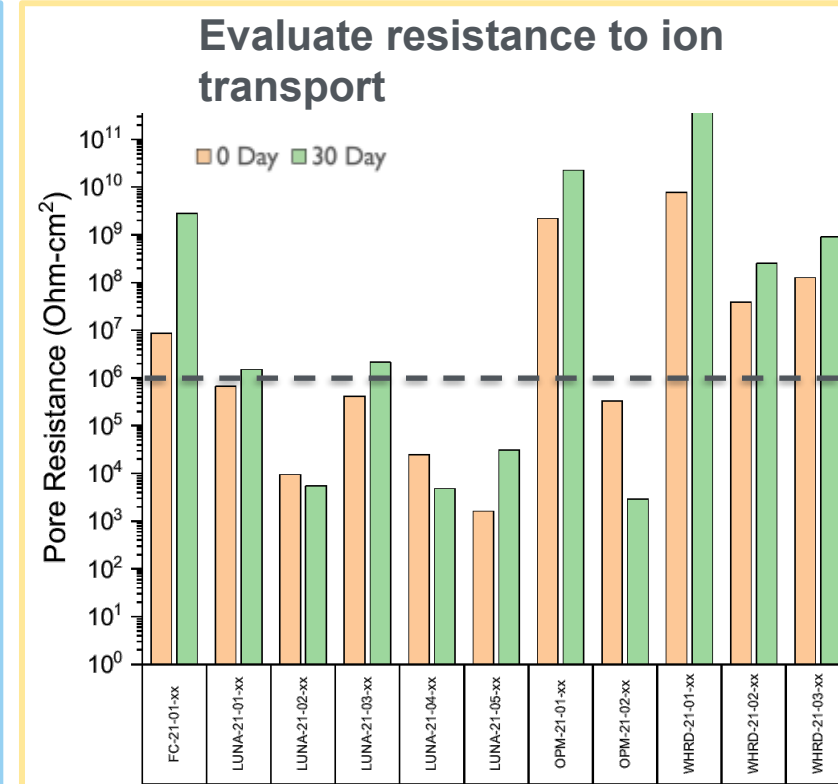
EIS evaluates the impedance of an electrochemical system as a function of the frequency of an applied a.c. wave. EIS is a common method to evaluate coating performance.



- Permeation of water into coating causes increased capacitance, but so can oxidation.
- Therefore OPM-21-02 and the LUNA coating with the Zn-rich primer showed highest  $C_c$  values



- $R_{CT}$  is most direct analogue to corrosion resistance. High  $R_{CT} \approx$  Low Corrosion Rate
- Large changes in  $R_{CT}$  in WHRD-21-01 and WHRD-21-03
  - OPM-21-01 and FC-21-01 had highest  $R_{CT}$  after exposures

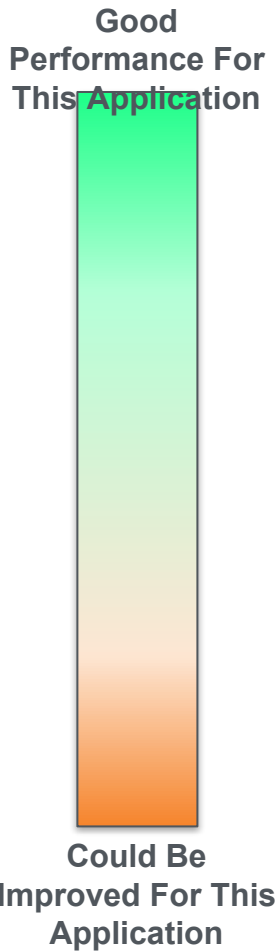


- $\geq 10^6 \Omega\text{cm}^2$  is considered a protective coating
- Criteria generally met by all coatings except for coatings with Zn-rich primer (different mechanism of protection) and OPM-21-02 (degradation and exposed SS).



# Initial Qualitative Assessment of Coating Viability

Changes in physical and chemical properties as a result of exposure can help indicate how a coating will perform over time.



Coating		Initial					Change as a result of exposure					Radiation Exposure	Thermal Exposure
		R <sub>CT</sub>	R <sub>PO</sub>	C <sub>C</sub>	Adhesion	Scratch	R <sub>CT</sub>	R <sub>PO</sub>	C <sub>C</sub>	Adhesion	Scratch		
Ceramic/Hybrid Coating	FC-21-01											FY23	FY23
	LUNA-21-01												
	LUNA-21-02*	—	—	—			—	—	—				
	LUNA-21-03												
	LUNA-21-04*	—	—	—			—	—	—				
	LUNA-21-05*	—	—	—			—	—	—				
Polymeric Coating	OPM-21-01												
	OPM-21-02												
	WHRD-21-01												
	WHRD-21-02												
	WHRD-21-03												

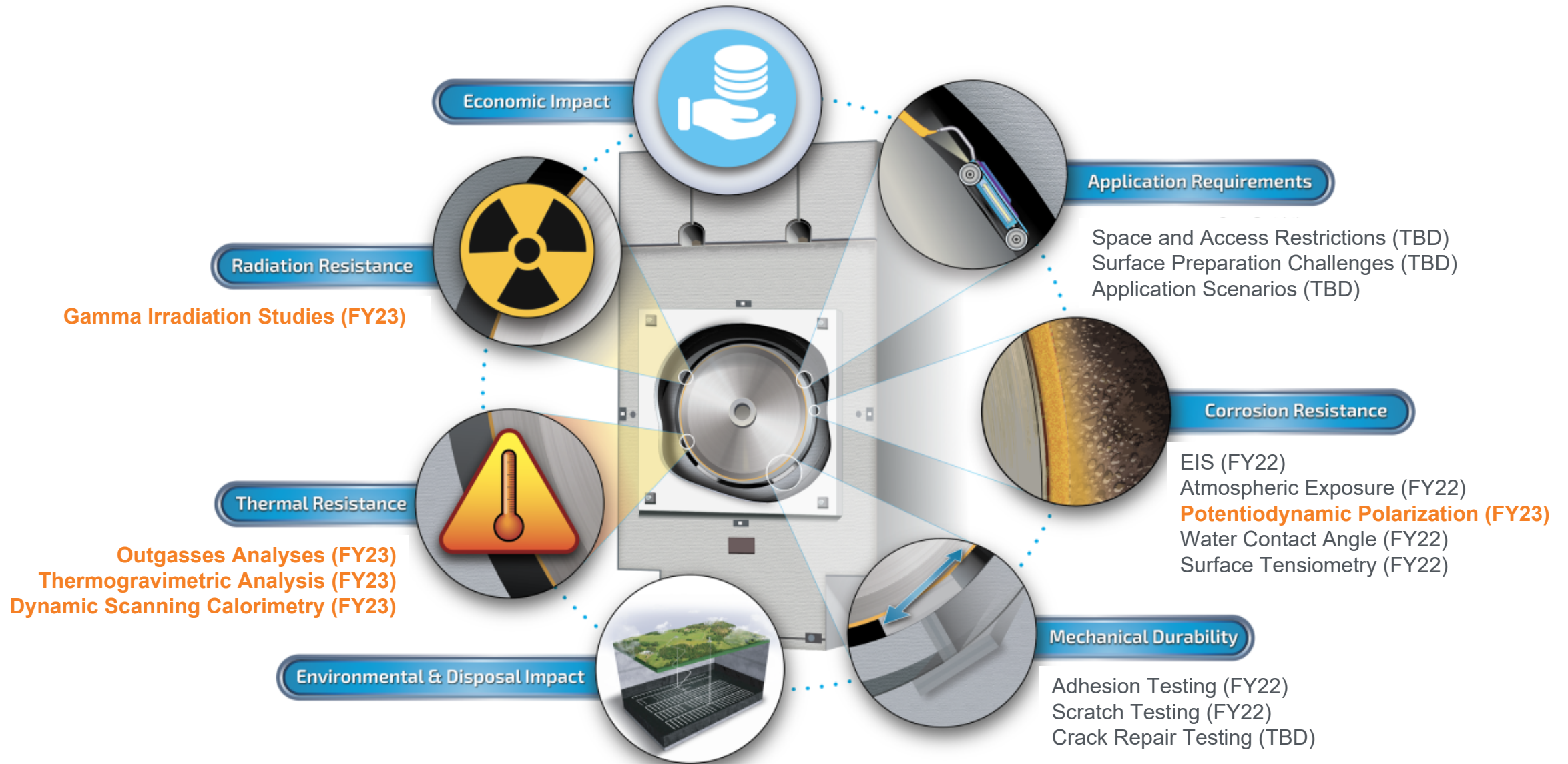
# Initial Qualitative Assessment of Coating Viability

Changes in physical and chemical properties as a result of exposure can help indicate how a coating will perform over time.

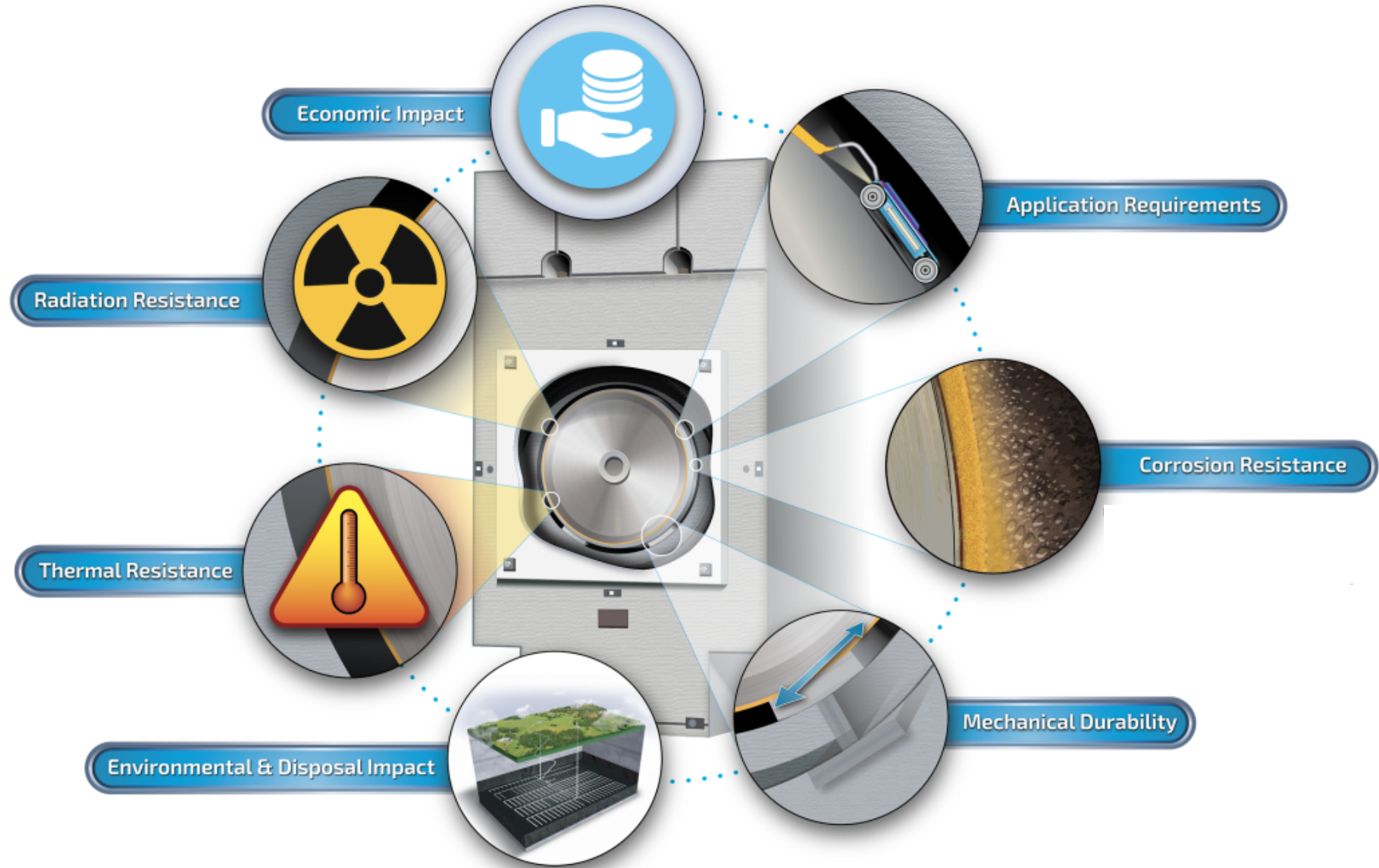
Coating		Initial					Change as a result of exposure					Radiation Exposure	Thermal Exposure
		R <sub>CT</sub>	R <sub>PO</sub>	C <sub>C</sub>	Adhesion	Scratch	R <sub>CT</sub>	R <sub>PO</sub>	C <sub>C</sub>	Adhesion	Scratch		
Ceramic/Hybrid Coating	FC-21-01												
	LUNA-21-01												
	LUNA-21-02*	—	—	—			—	—	—				
<div> <div>Good Performance For This Application</div> <div>Need to define performance criteria relevant to interim storage to guide screening decisions</div> <div>Could Be Improved For This Application</div> </div>													
Polymeric Coating	OPM-21-01												
	OPM-21-02												
	WHRD-21-01												
	WHRD-21-02												
	WHRD-21-03												

FY23

# Future Work



# To Optimize M&R Technology, We Must Define Performance Metrics





Questions?

Cold Spray	Edge	Process Gas	Potentiodynamic Polarization		Accelerated Pitting Exposure	Atmospheric Exposure			Boiling MgCl <sub>2</sub> Exposure
			NaCl	FeCl <sub>3</sub>		40 % RH, 35 °C	75 % RH, 35 °C	Cyclic	
Inc	Tapered	He	X	X	X	X	-	X	X
Inc	Tapered	N	X	X	X	-	-	X	X
Inc	Masked	N	-	-	X	X	X	X	X
Ni	Tapered	N	X	X	X	X	-	X	X
Ni	Masked	N	-	-	X	X	X	X	X
Ni	Tapered	He	-	-	X	-	-	-	-
Ni	Masked	He	-	-	X	-	-	-	-
SC	Tapered	N	X	X	X	X	X	X	-
SC	Tapered	He	-	-	X	-	-	-	-
SC	Masked	He	-	-	X	-	-	-	-
SS316 + 25% CrC 410	Tapered	N	-	-	X	-	-	-	-
SS316 + 25% CrC 410	Tapered	N	-	-	X	-	-	-	-
SS316 + 25% CrC 410	Tapered	N	-	-	X	-	-	-	-

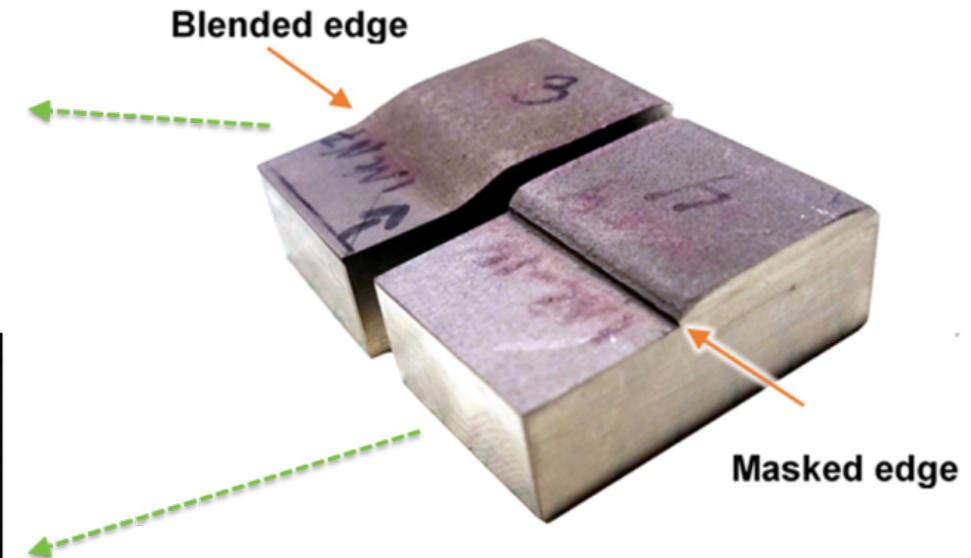
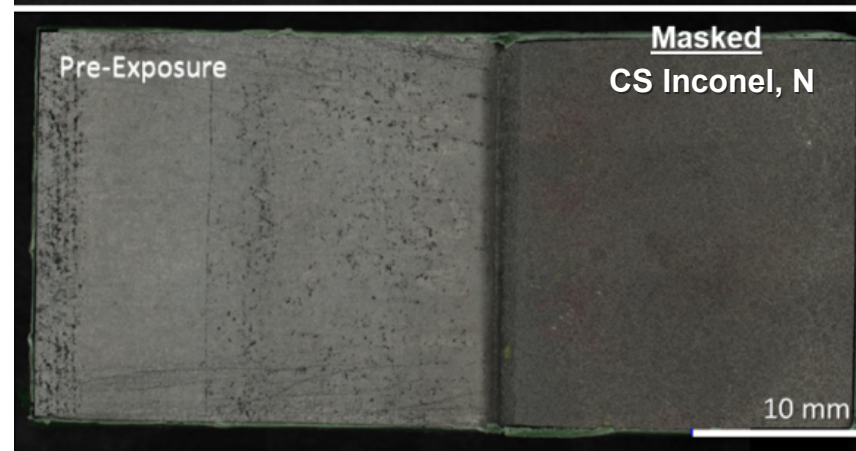
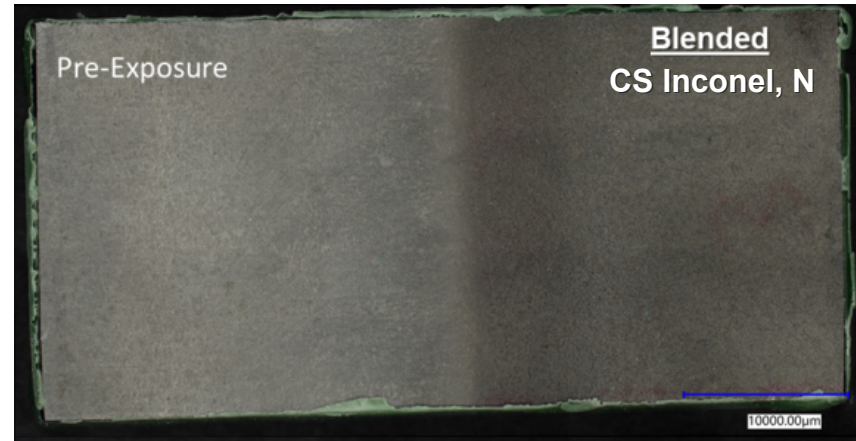
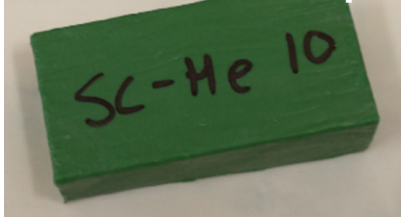
# Cold Spray – Accelerated testing for optimization

## *Pitting*

### *Characterization:*

- 6% by mass Ferric Chloride
- Full Immersion 72 h, 22 °C
- Entire top surface tested
  - Other surfaces painted

CS Painted Sample

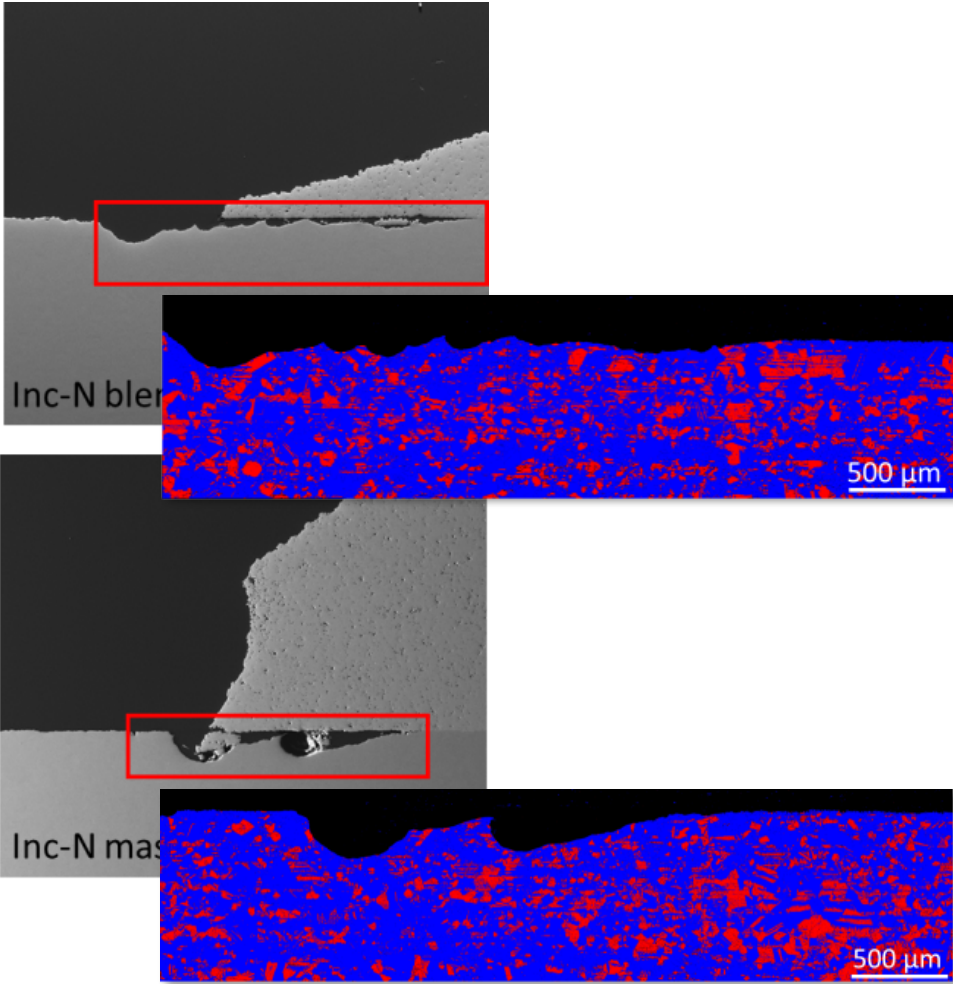
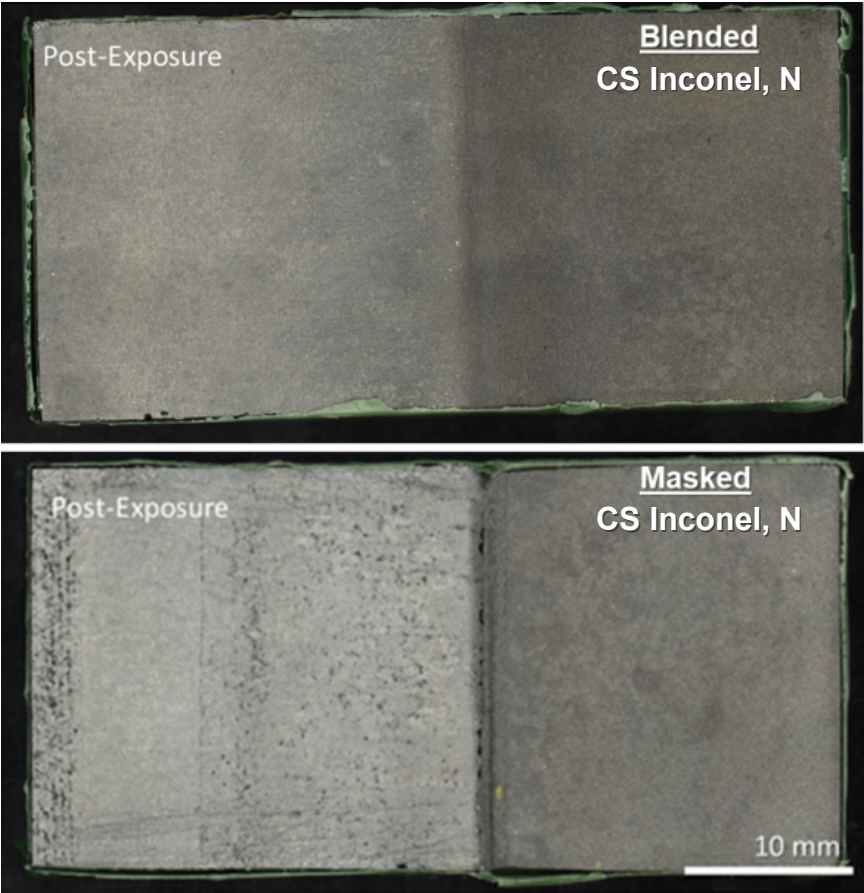
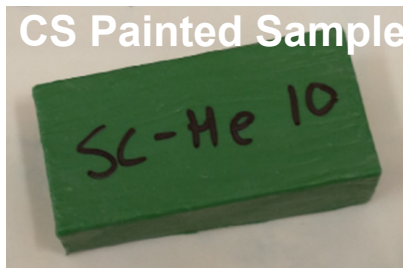


# Cold Spray – Accelerated testing for optimization

## Pitting

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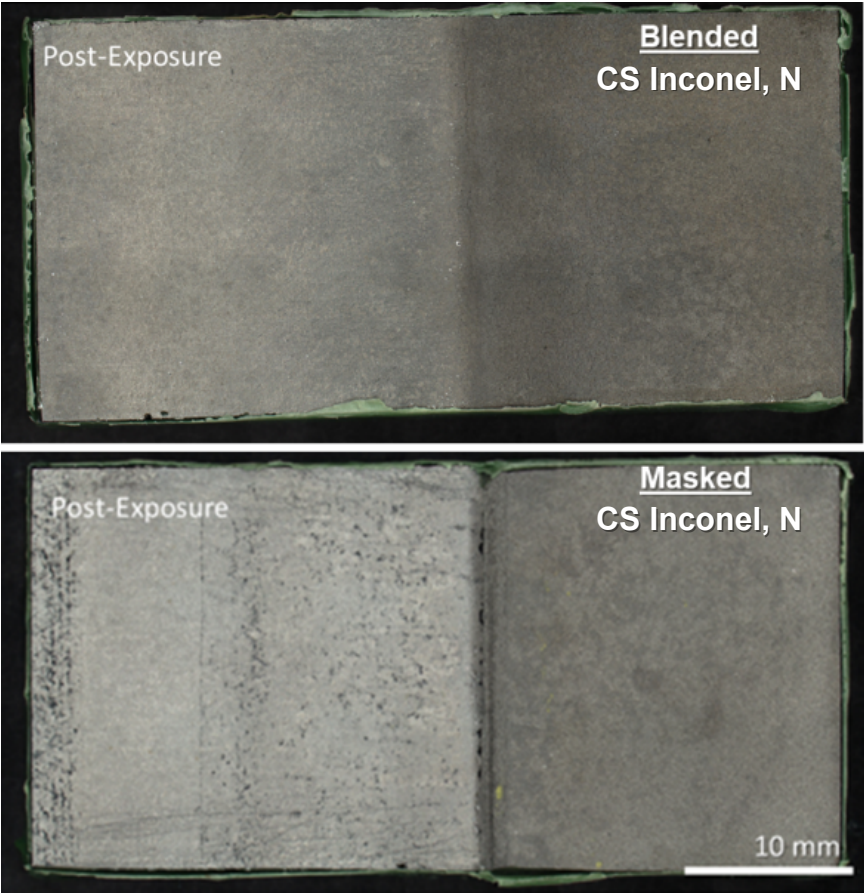
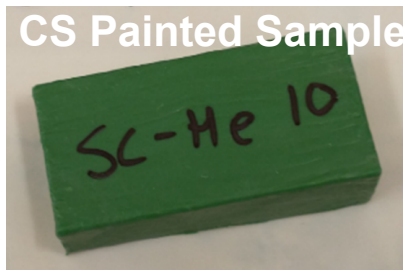


# Cold Spray – Accelerated testing for optimization

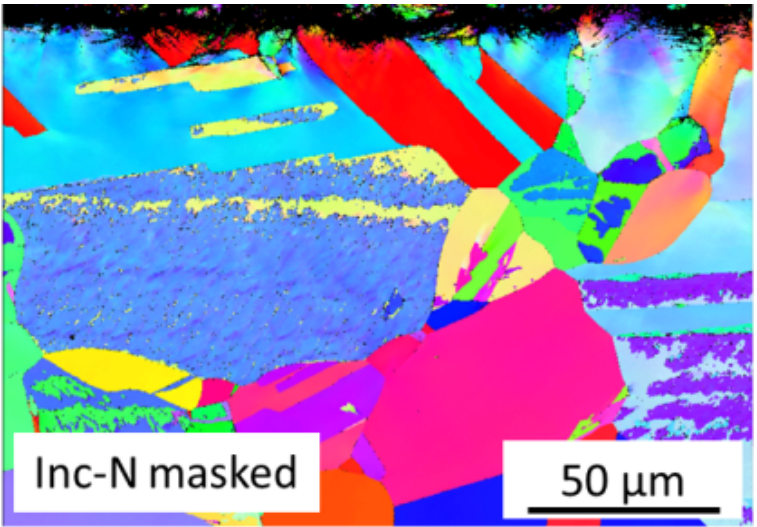
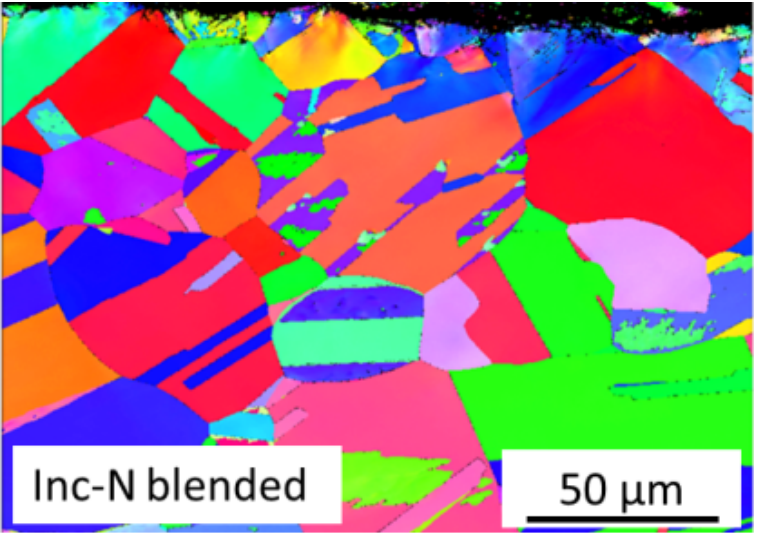
## Pitting

### Characterization:

- 6% by mass Ferric Chloride
- Full Immersion 72 h, 22 °C
- Entire top surface tested
  - Other surfaces painted



*EBSD of interface far from corrosion attack (uncorroded region)*



# Cold Spray – Summary and Moving Forward

## ***Summary of initial optimization:***

1. *Metastable pitting in full immersion is reduced when the cold spray coating surface is polished*
2. *The morphology of the edge interface (tapered vs masked) influences the resultant corrosion morphology*
3. *The porosity (due to carrier gas) of the cold spray coating influences the extent of corrosion damage*
4. *Initial observations of accelerated testing as compared to more relevant atmospheric testing indicate similar damage morphologies*

## ***Future work/ questions:***

1. *Further testing under relevant conditions*
2. *What qualifies as “good enough” for a mitigation and repair strategy?*
  - *How can we optimize coatings with initial observations, and how will we know when they meet sufficient requirements?*
3. *How does cold spray behave on a pre-corroded or pre-exposed surface?*
  - *What surface preparation is necessary, if at all?*