

# Molecular Dynamics Studies of Helium Bubble Effects on Grain Boundary Fracture in $Fe_{70}Ni_{11}Cr_{19}$ -1%H Austenitic Stainless Steel

## International Conference on Plasticity, Damage & Fracture

Jan. 3-9, 2023, Barcelo Bavaro Punta Cana, Dominican Republic



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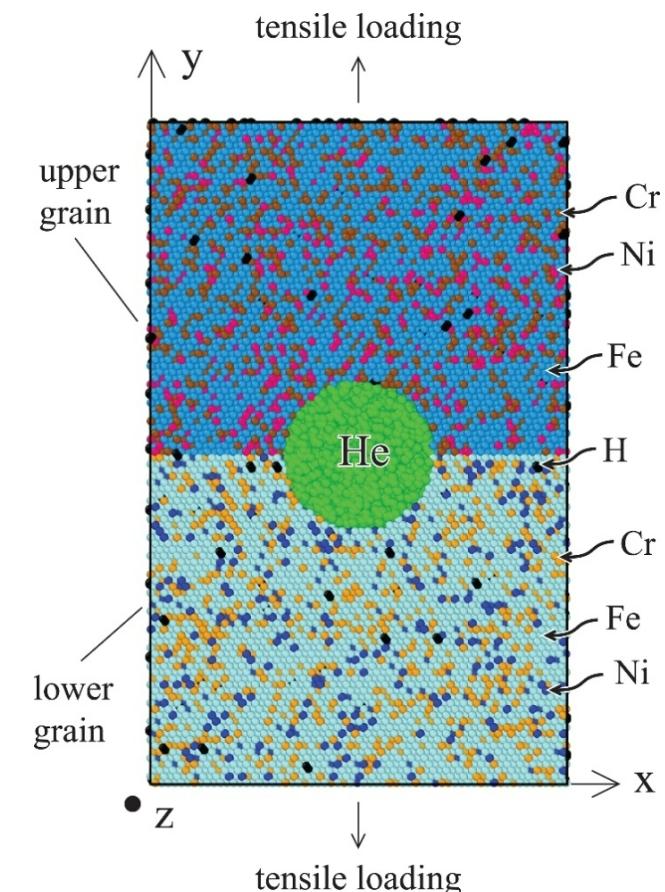
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# Motivation

- Stainless steels for nuclear applications develop He bubbles.
- Bubbles promote brittle fracture especially at grain boundaries (GB).
- Improved applications require an understanding of effects on:
  - He bubble areal density on grain boundaries
  - Bubble pressure
  - Temperature
  - Bubble radius
  - Grain boundary types
- We attempt to use molecular dynamics (MD) simulations to address these problems.

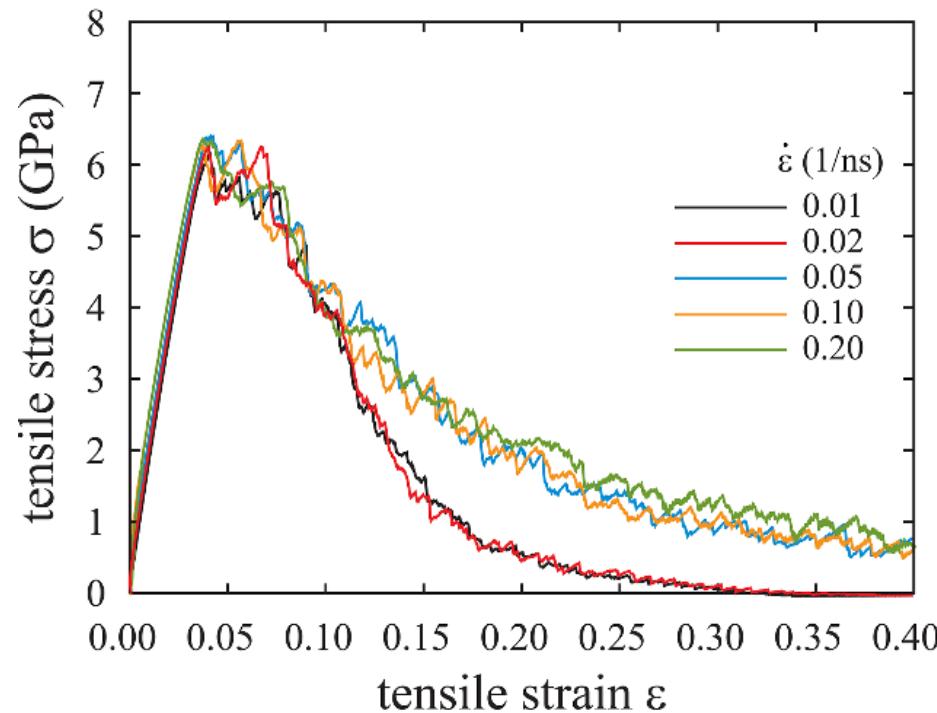
# Approach

- Tensile tests of  $\text{Fe}_{70}\text{Ni}_{11}\text{Cr}_{19}$ (304L)-1%H with a bubble on GB are simulated.
- Ten GB/cleavage planes are considered:  $\Sigma 1\{111\}$ ,  $\Sigma 3\{111\}$ ,  $\Sigma 5\{100\}$ ,  $\Sigma 7\{111\}$ ,  $\Sigma 9\{411\}$ ,  $\Sigma 11\{311\}$ ,  $\text{R}\{100\}/\{411\}$ ,  $\Sigma 1\{100\}$ ,  $\Sigma 1\{311\}$ , and  $\Sigma 1\{411\}$ .
- Periodic boundary conditions are used in all three directions.
- Strain controlled simulations with NVT ensemble are used.
- Strain is applied in segments to allow time-averaged energies and stresses to be calculated for each of the segments.
- Various system dimensions ranging from  $\sim 200,000$  to 700,000 atoms are explored.
- The Fe-N-Cr-H EAM potential in Inter. J. Hydro. Ener., 47, 651 (2022), the He-He and He-metal pair potentials in J. Nuc. Mater., 565, 153753 (2022) are used.

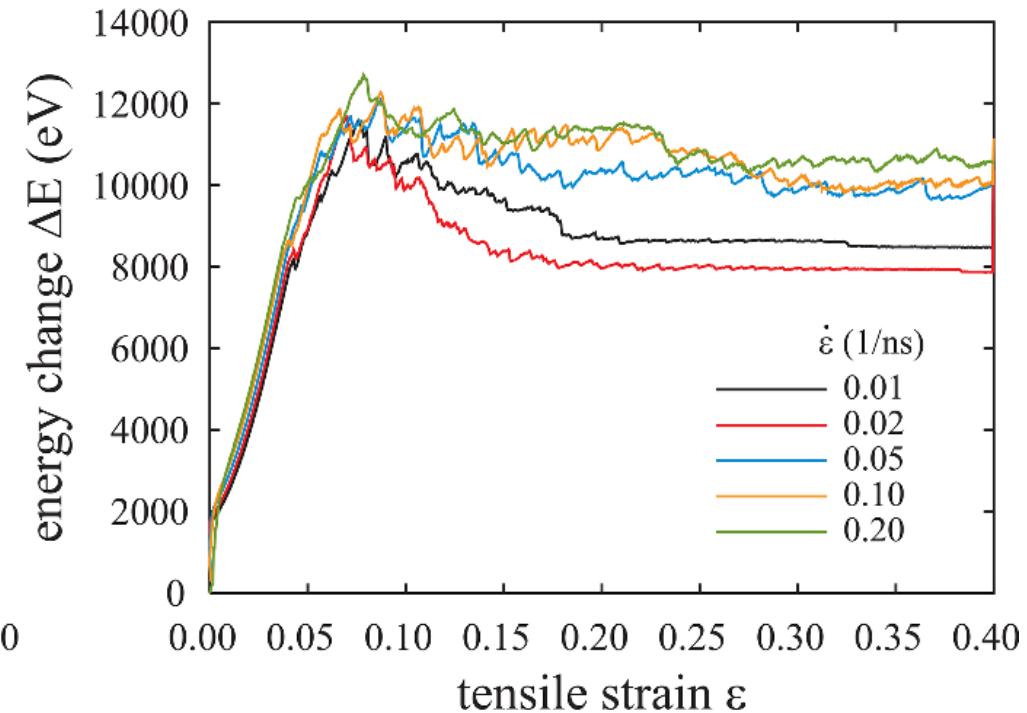


# Effects of Accelerated MD Strain Rate

(a)  $\sigma$  vs.  $\varepsilon$



(b)  $\Delta E$  vs.  $\varepsilon$



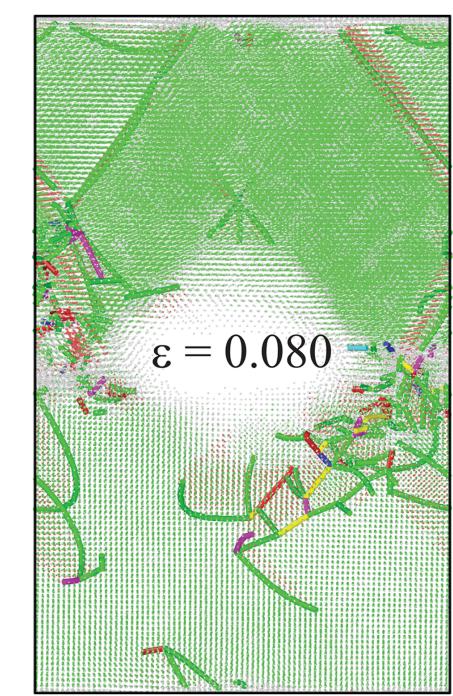
$\Sigma 5\{100\}$ , system volume  $V \sim 4600 \text{ nm}^3$ , interfacial area  $A \sim 210 \text{ nm}^2$   
bubble radius  $r = 3.0 \text{ nm}$ , bubble pressure  $P = 2 \text{ GPa}$ , temperature  $T = 300 \text{ K}$

Large strain rate overshoots stresses and energies. We will use  $\dot{\varepsilon} = 0.02 \text{ /ns}$ .

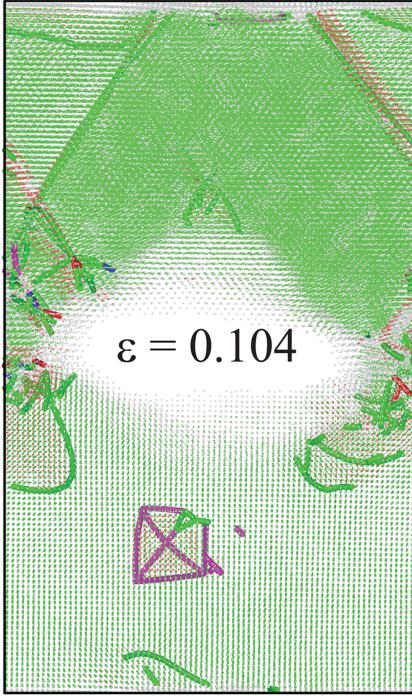
# Structures from Low and High Strain

## Rates

(a) low strain rate of 0.01 (1/ns)

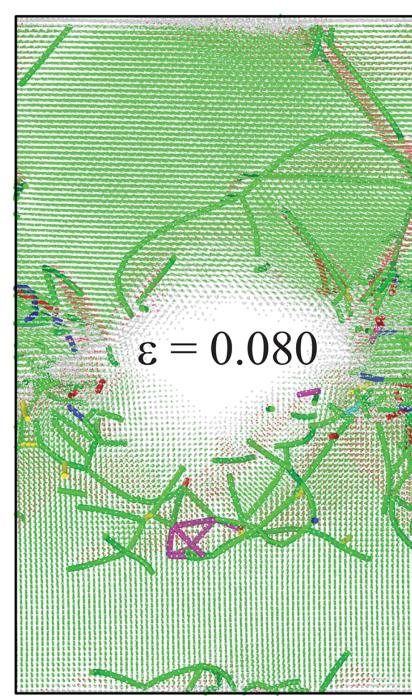


69.2% FCC  
281 nm dislocations

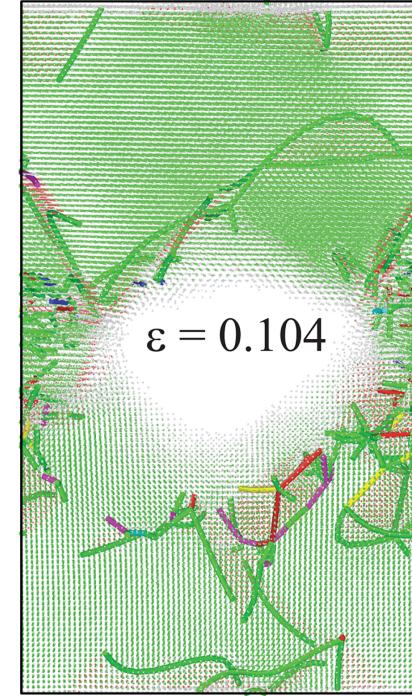


71.4% FCC  
208 nm dislocations

(b) high strain rate of 0.20 (1/ns)



79.7% FCC  
367 nm dislocations



80.6% FCC  
357 nm dislocations

— :  $<110>/2$  — :  $<112>/6$  — :  $<110>/6$  — :  $<001>/3$  — :  $<111>/3$  ■: FCC ■: HCP

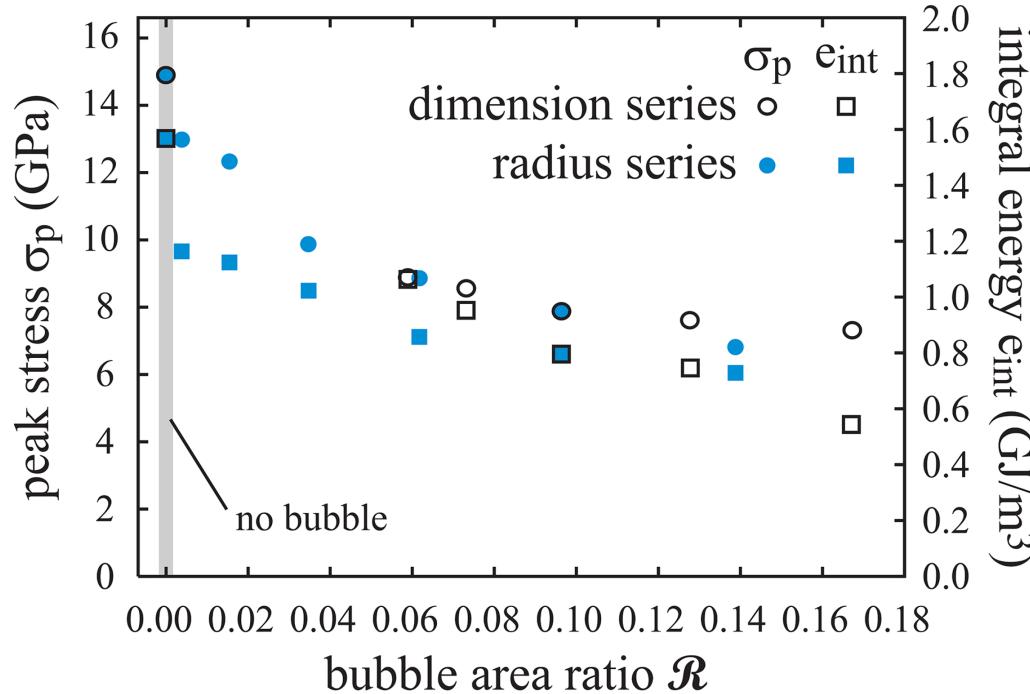
8 nm slice on x-y plane near bubble,  $\Sigma 5 \{100\}$  grain boundary

bubble radius  $r = 3.0$  nm, bubble pressure  $P = 2$  GPa, temperature  $T = 300$  K

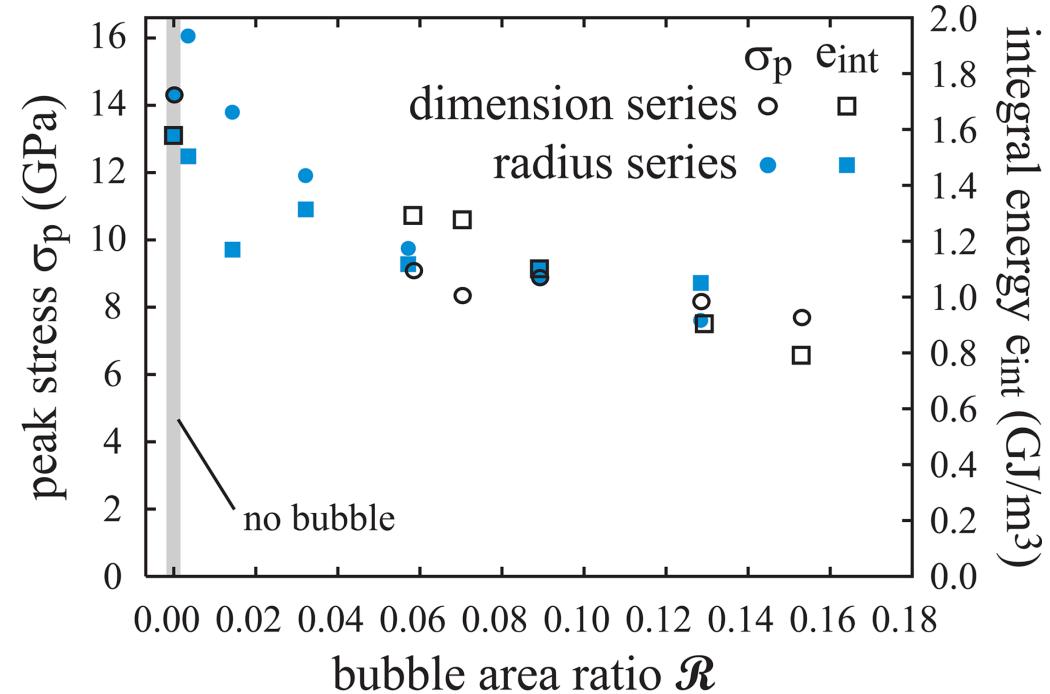
Large strain rate overshoots stresses and energies because dislocations do not have time to migrate and annihilate.

# Areal Coverage Effects

(a)  $\sigma_p$  and  $e_{int}$  vs.  $\mathcal{R}$  for  $\Sigma 9\{411\}$



(b)  $\sigma_p$  and  $e_{int}$  vs.  $\mathcal{R}$  for  $\Sigma 11\{311\}$



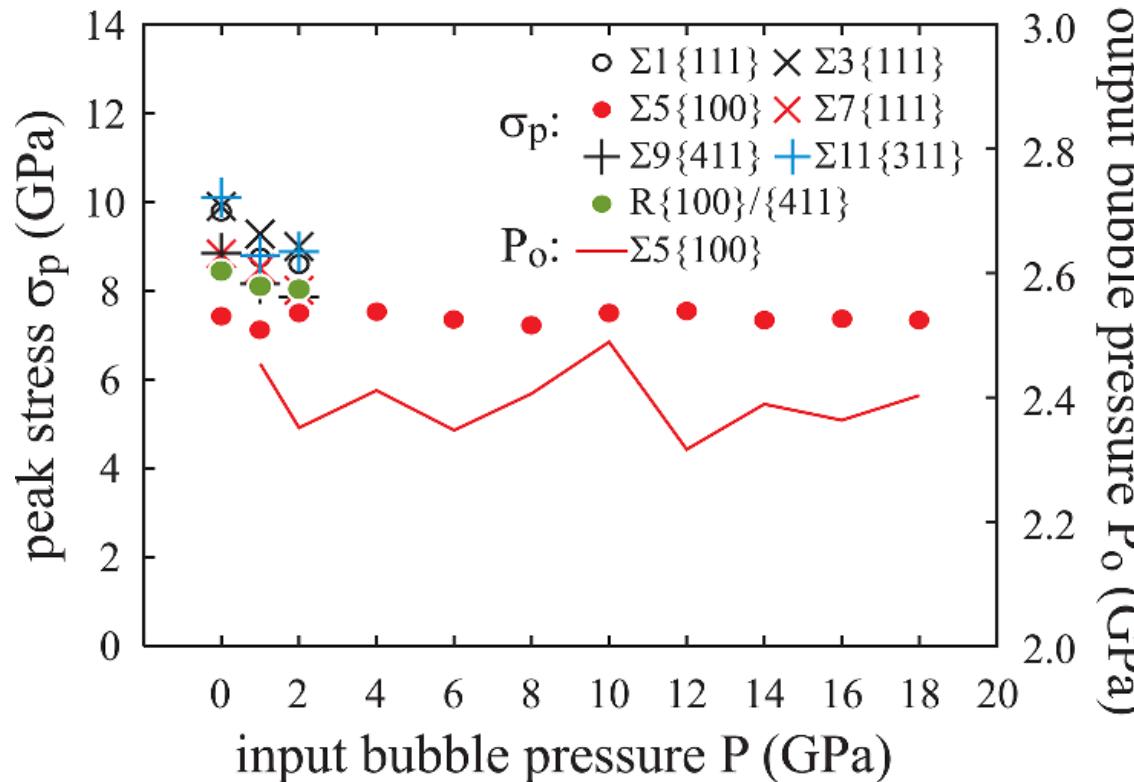
dimension series: bubble radius  $r = 2.5$  nm; radius series: cross section area  $\sim 15 \times 15$  nm<sup>2</sup>

bubble pressure  $P = 2$  GPa, temperature  $T = 300$  K, strain rate  $\dot{\epsilon} = 0.02$  /ns

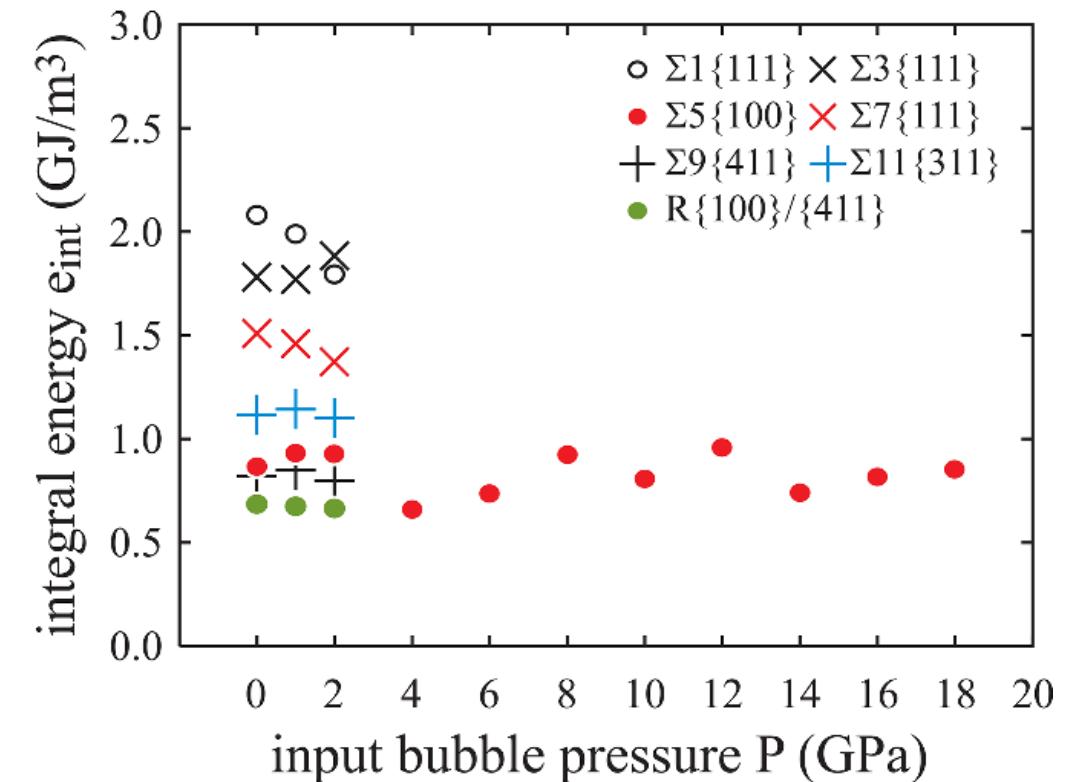
- Areal ratio can be changed by bubble radius or sample cross section area.
- The peak stress  $\sigma_p$  and integral energy  $e_{int}$  both decrease as bubble areal ratio increases.
- With the area effect understood, We will use cross section area  $\sim 15 \times 15$  nm<sup>2</sup> below.

# Bubble Pressure Effects

(a)  $\sigma_p$  for various interfaces



(b)  $e_{int}$  for various interfaces

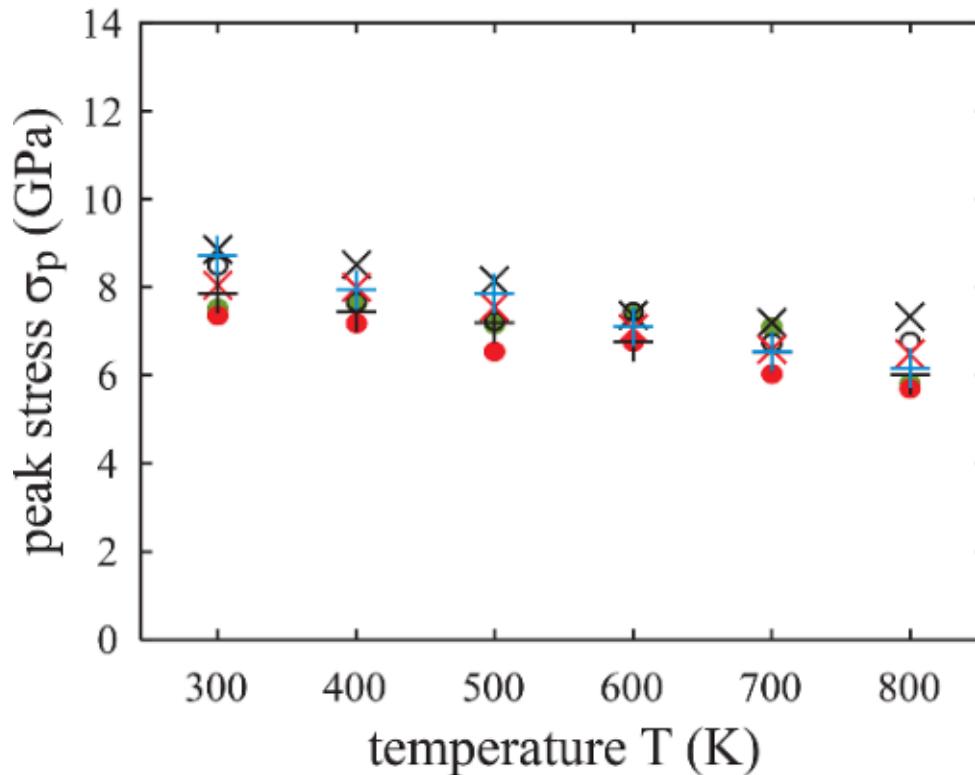


bubble radius  $r = 2.5$  nm, temperature  $T = 300$  K, strain rate  $\dot{\varepsilon} = 0.02$  /ns

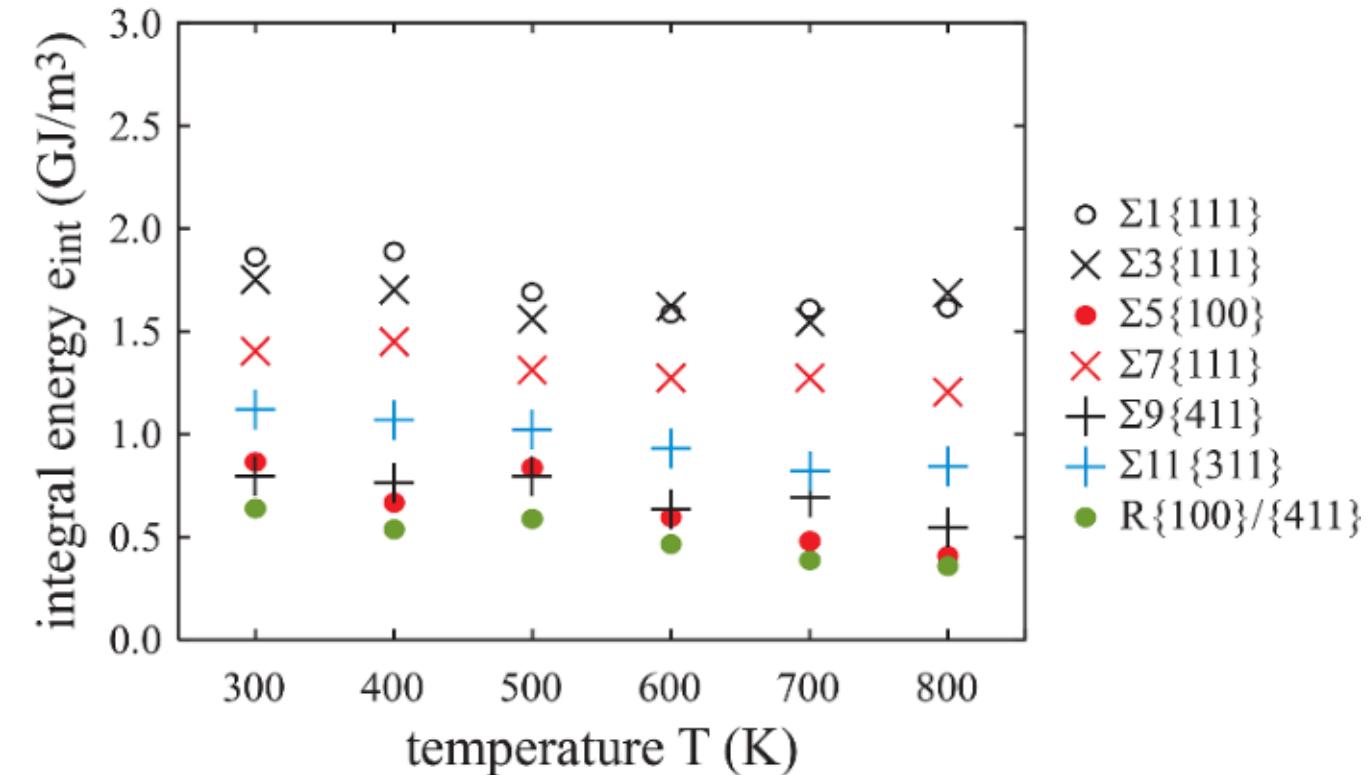
- Output pressure remains around 2.4 – 2.6 GPa in the input pressure range 0 – 20 GPa.
- Overall, increasing input pressure from 0 to 2 GPa decreases  $\sigma_p$  and  $e_{int}$ .

# Temperature Effects

(a)  $\sigma_p$  for various interfaces



(b)  $e_{int}$  for various interfaces

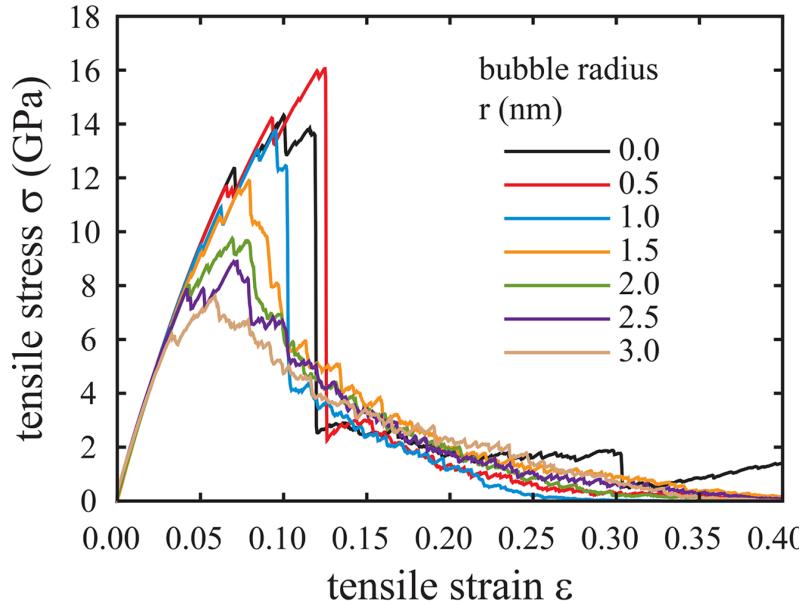


bubble radius  $r = 2.5$  nm, bubble pressure  $P = 2$  GPa, strain rate  $\dot{\varepsilon} = 0.02$  /ns

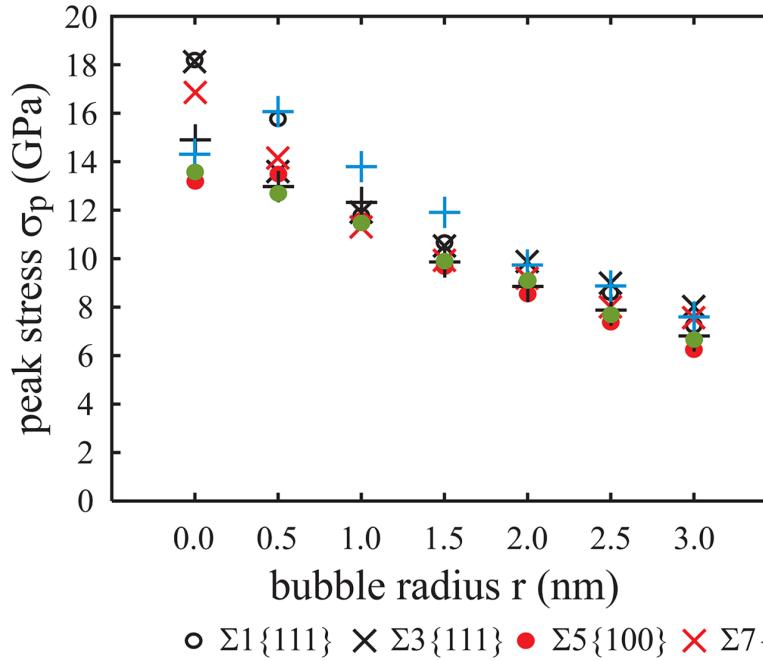
- Increasing temperature slightly reduces peak stress and integral energy.
- This is consistent with thermally activated nucleation and migration of dislocations.

# Bubble Radius Effects

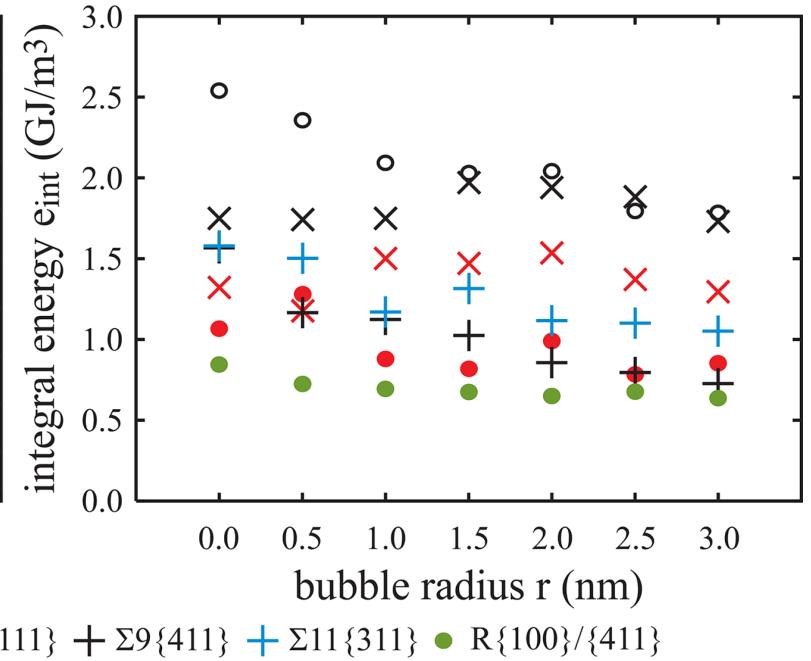
(a)  $\sigma$  vs.  $\varepsilon$  for  $\Sigma 11\{311\}$



(b)  $\sigma_p$  for various interfaces



(c)  $e_{int}$  for various interfaces

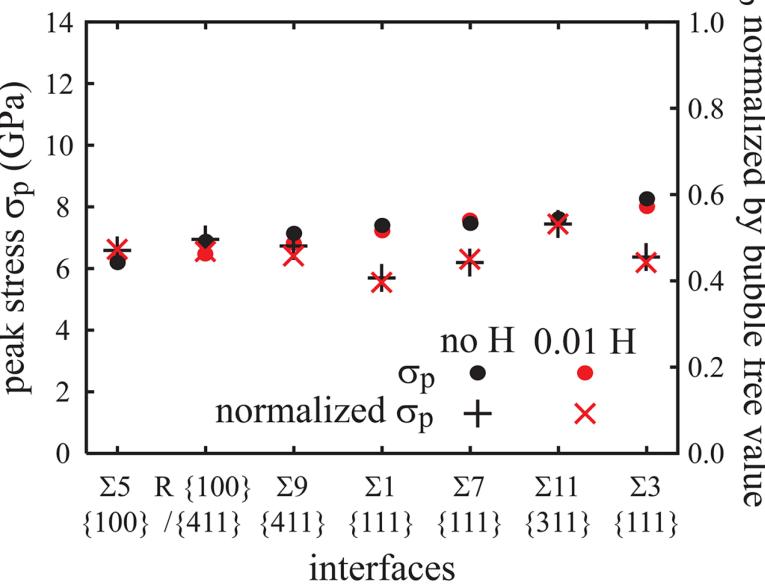


bubble pressure  $P = 2$  GPa, temperature  $T = 300$  K, strain rate  $\dot{\varepsilon} = 0.02$  /ns

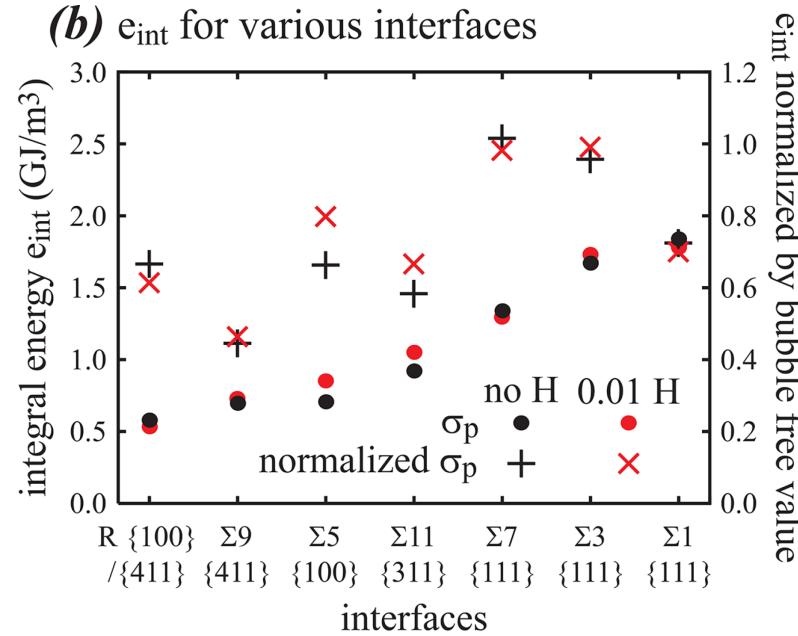
- Increasing bubble radius reduces peak stress and integral energy.
- Areal ratio seems to be more important than bubble radius.

# Interface Type Effects

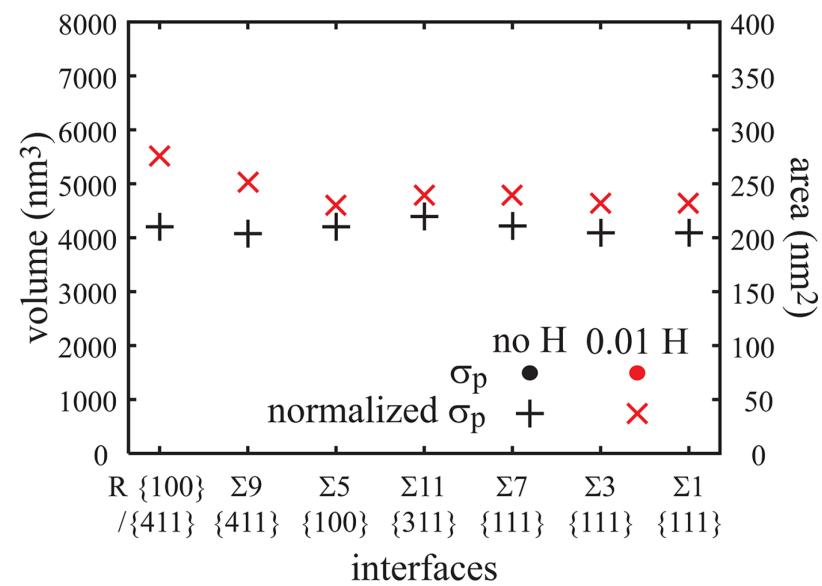
(a)  $\sigma_p$  for various interfaces



(b)  $e_{int}$  for various interfaces



(c) system dimension parameters

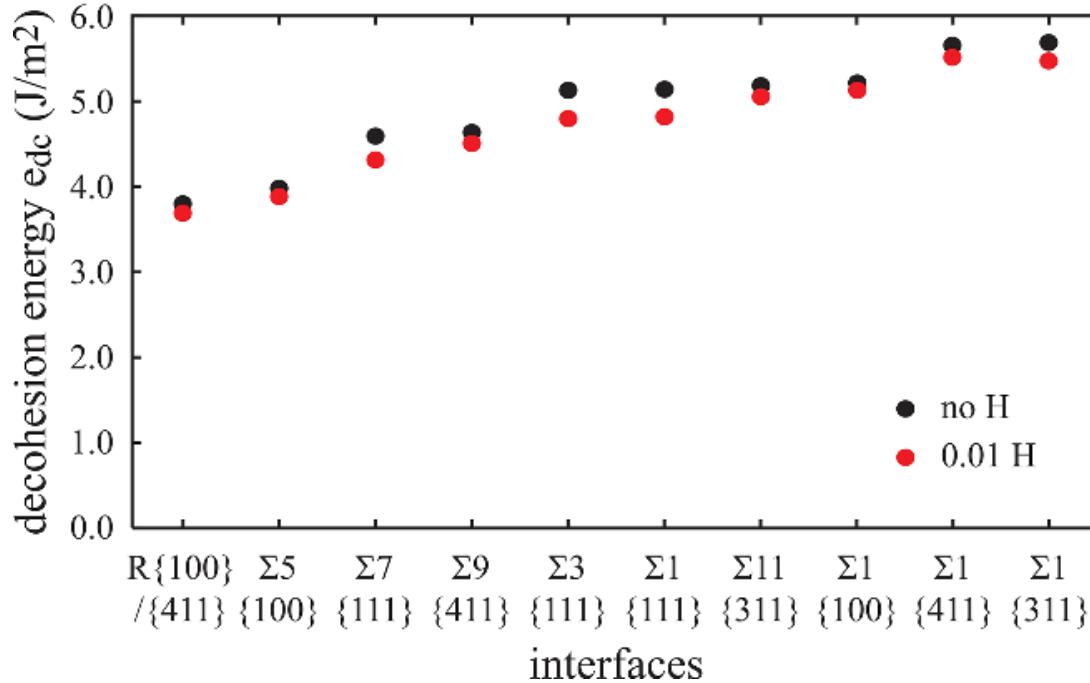


bubble radius  $r = 3.0$  nm, bubble pressure  $P = 2$  GPa, temperature  $T = 300$  K, strain rate  $\dot{\epsilon} = 0.02$  /ns

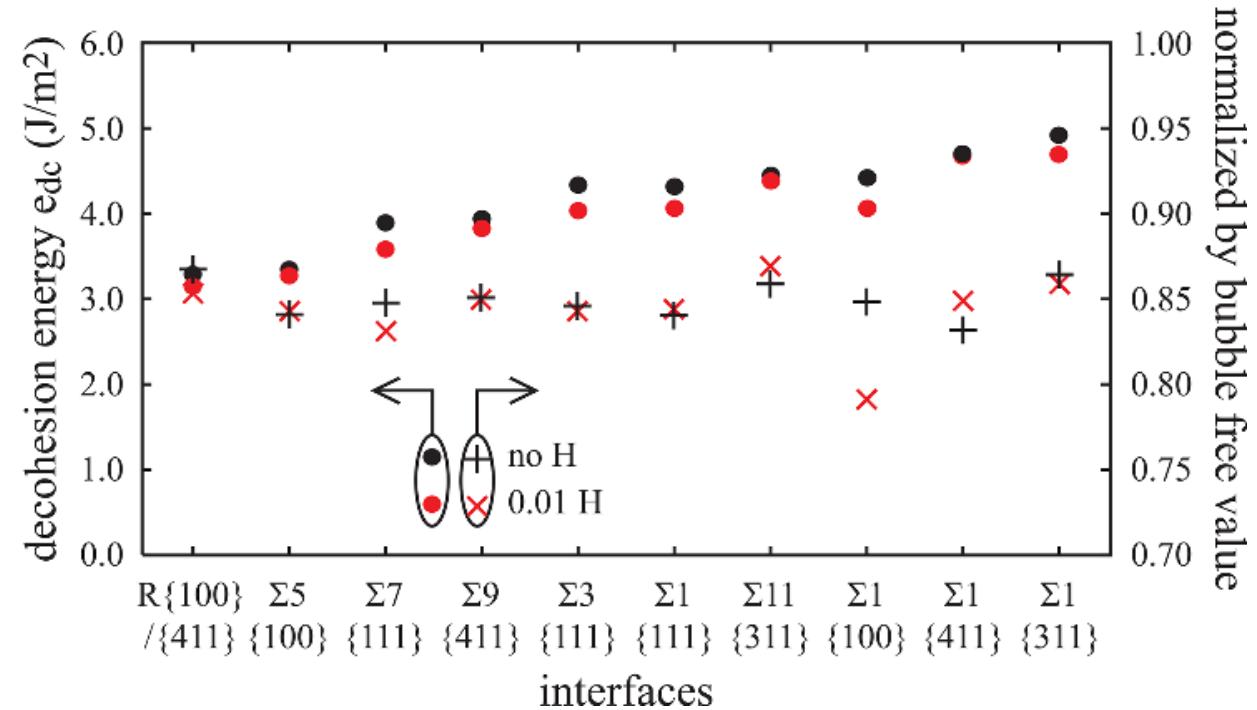
- $\sigma_p$  and  $e_{int}$  trends are not the same,  $e_{int}$  is more reflective of fracture.
- Interface type more sensitively impacts  $e_{int}$ .

# Decohesion Energies vs. Interfaces (averaged over 40 ns)

(a) no bubble

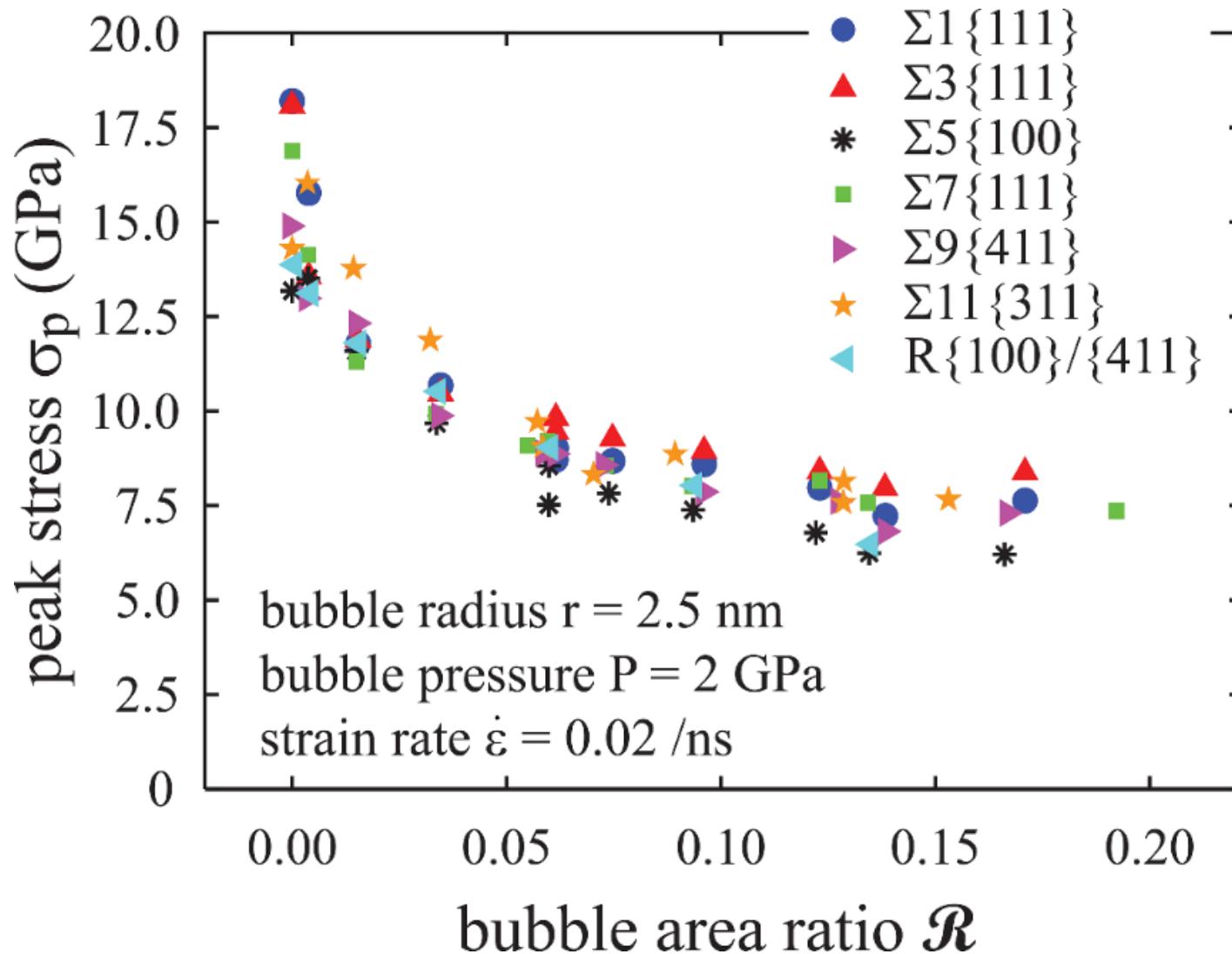


(b) a bubble with radius 2.5 nm



- $\Sigma 1\{111\}$  is weaker than  $\Sigma 11\{311\}$ , but the other cleavage planes are all stronger than GB or twin boundaries.
- The random GB R{100}/{411} has the lowest decohesion energy.

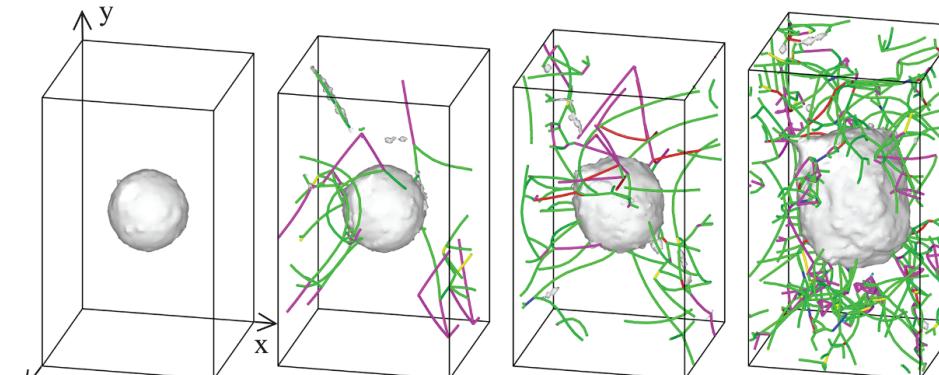
# Bubble Effects from All Data



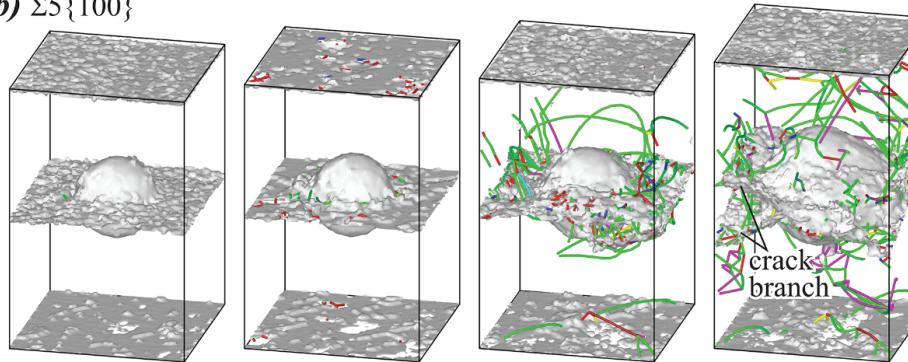
□ Peak stress is plotted as a function of areal coverage ratio from both the radius and dimension series for all GBs.

□ Peak stress monotonically decreases with areal ratio.

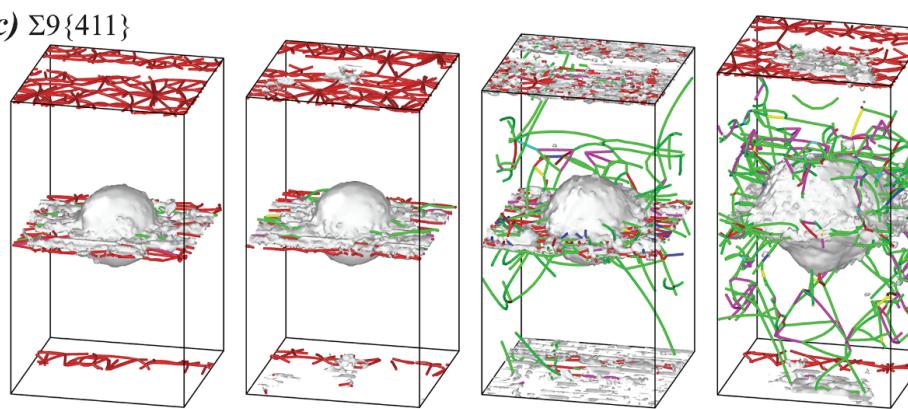
(a)  $\Sigma 1\{111\}$



(b)  $\Sigma 5\{100\}$



(c)  $\Sigma 9\{411\}$



$\varepsilon = 0.016$     $\varepsilon = 0.032$     $\varepsilon = 0.056$     $\varepsilon = 0.120$   
— :  $<110>/2$    — :  $<112>/6$    — :  $<110>/6$    — :  $<001>/3$    — :  $<111>/3$   
 $r = 3.0 \text{ nm}, P = 2 \text{ GPa}, T = 300 \text{ K}, \text{strain rate } \dot{\varepsilon} = 0.02 / \text{ns}$

# Mechanistic Studies

- $\Sigma 1\{111\}$  has an intermediate peak stress. Dislocation formation easier?
- Compared with  $\Sigma 9\{411\}$ ,  $\Sigma 5\{100\}$  has a higher integral energy but a lower decohesion energy. Why?
- We explored these by visualizing time evolution of atomic configurations.
- Indeed, the  $\Sigma 1\{111\}$  case forms dislocations early.
- The crack branches in the  $\Sigma 5\{100\}$  case causing it to have a high integral energy.

# Conclusions

- Fracture energy decreases with increasing bubble areal ratio, bubble pressure, temperature, and bubble radius.
- Initial bubble pressure has little impact on intergranular fracture because it quickly drops once dislocations move.
- The bubble areal ratio has the most important effect on fracture.
- Interface type sensitively impacts fracture. GB more likely causes fracture than cleavage plane. Random GB more likely causes fracture than coherent GB.

# Helium Equation of State

