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Molecular Dynamics Studies on Helium Bubble Effects on Grain Boundary Fracture in Fe₇₀Ni₁₁Cr₁₉-1%H Austenitic Stainless Steel

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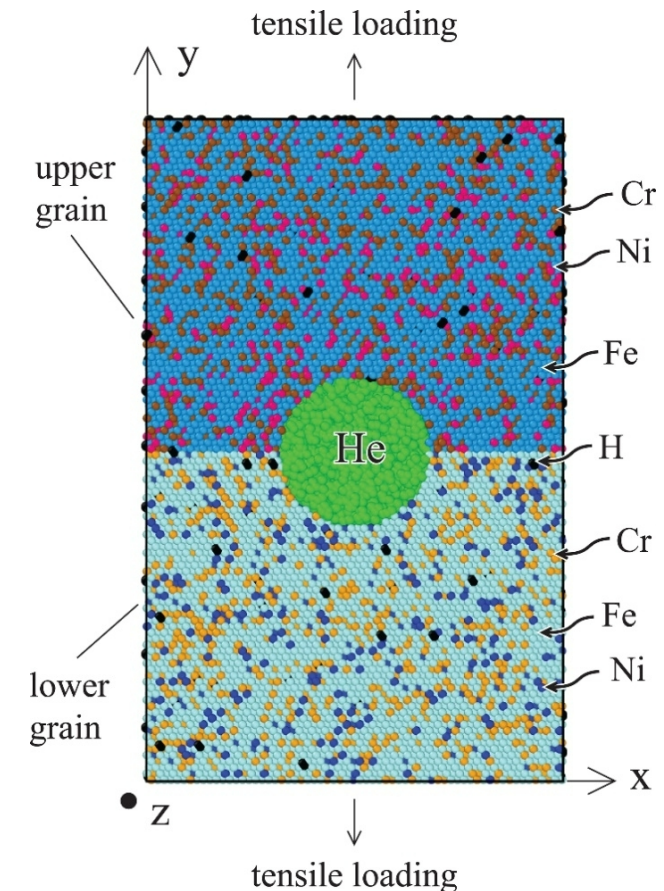
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Motivation

- ❑ Stainless steels for nuclear applications develop He bubbles.
- ❑ Bubbles promote brittle fracture especially at grain boundaries (GB).
- ❑ Improved applications require an understanding of effects on:
 - He bubble areal density on grain boundaries
 - Bubble pressure
 - Temperature
 - Bubble radius
 - Grain boundary types
- ❑ **We attempt to use molecular dynamics (MD) simulations to address these problems.**

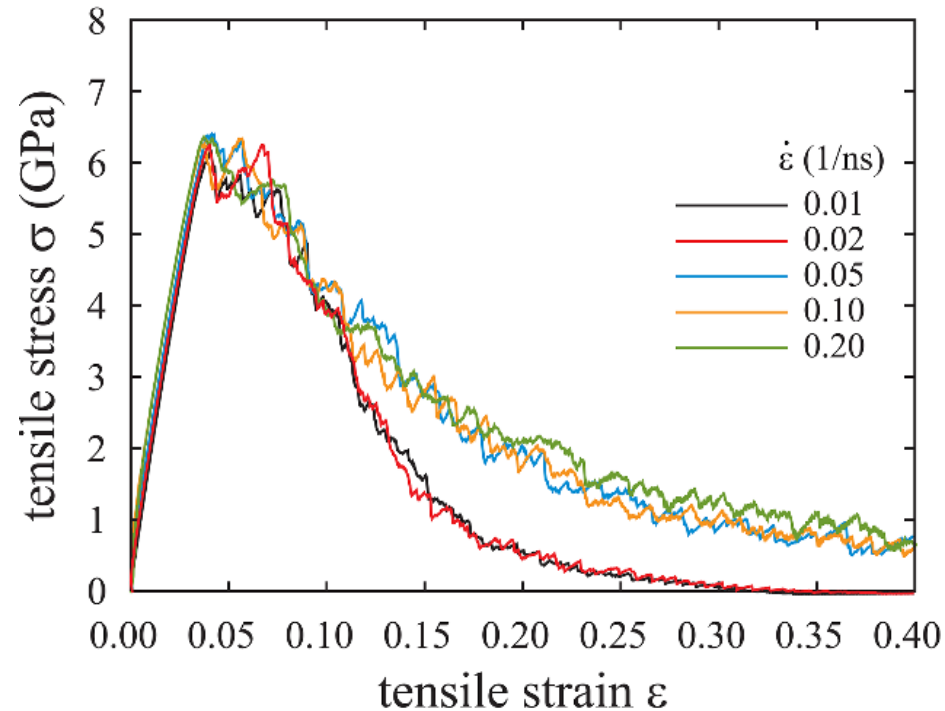
Approach

- ❑ Tensile tests of $\text{Fe}_{70}\text{Ni}_{11}\text{Cr}_{19}$ (304L)-1%H with a bubble on GB are simulated.
- ❑ Ten GB/cleavage planes are considered: $\Sigma 1\{111\}$, $\Sigma 3\{111\}$, $\Sigma 5\{100\}$, $\Sigma 7\{111\}$, $\Sigma 9\{411\}$, $\Sigma 11\{311\}$, $R\{100\}/\{411\}$, $\Sigma 1\{100\}$, $\Sigma 1\{311\}$, and $\Sigma 1\{411\}$.
- ❑ Periodic boundary conditions are used in all three directions.
- ❑ Strain controlled simulations with NVT ensemble are used.
- ❑ Strain is applied in segments to allow time-averaged energies and stresses to be calculated for each of the segments.
- ❑ Various system dimensions ranging from $\sim 200,000$ to $700,000$ atoms are explored.
- ❑ The Fe-N-Cr-H EAM potential in Inter. J. Hydro. Ener., 47, 651 (2022), the He-He and He-metal pair potentials in J. Nuc. Mater., 565, 153753 (2022) are used.

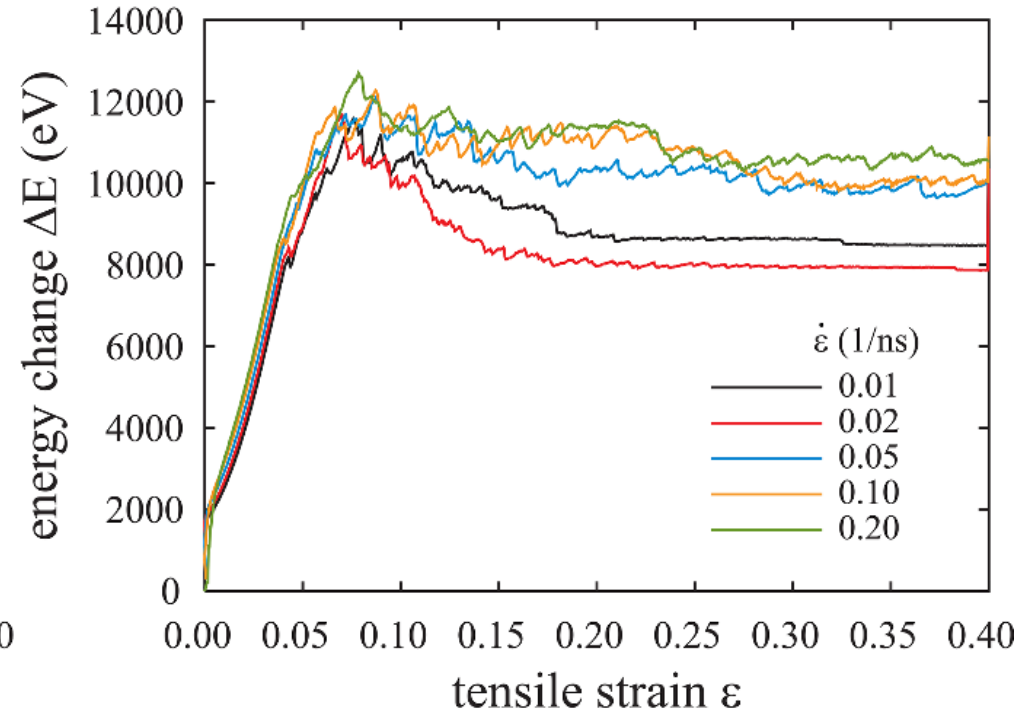


Effects of Accelerated MD Strain Rate

(a) σ vs. ϵ



(b) ΔE vs. ϵ



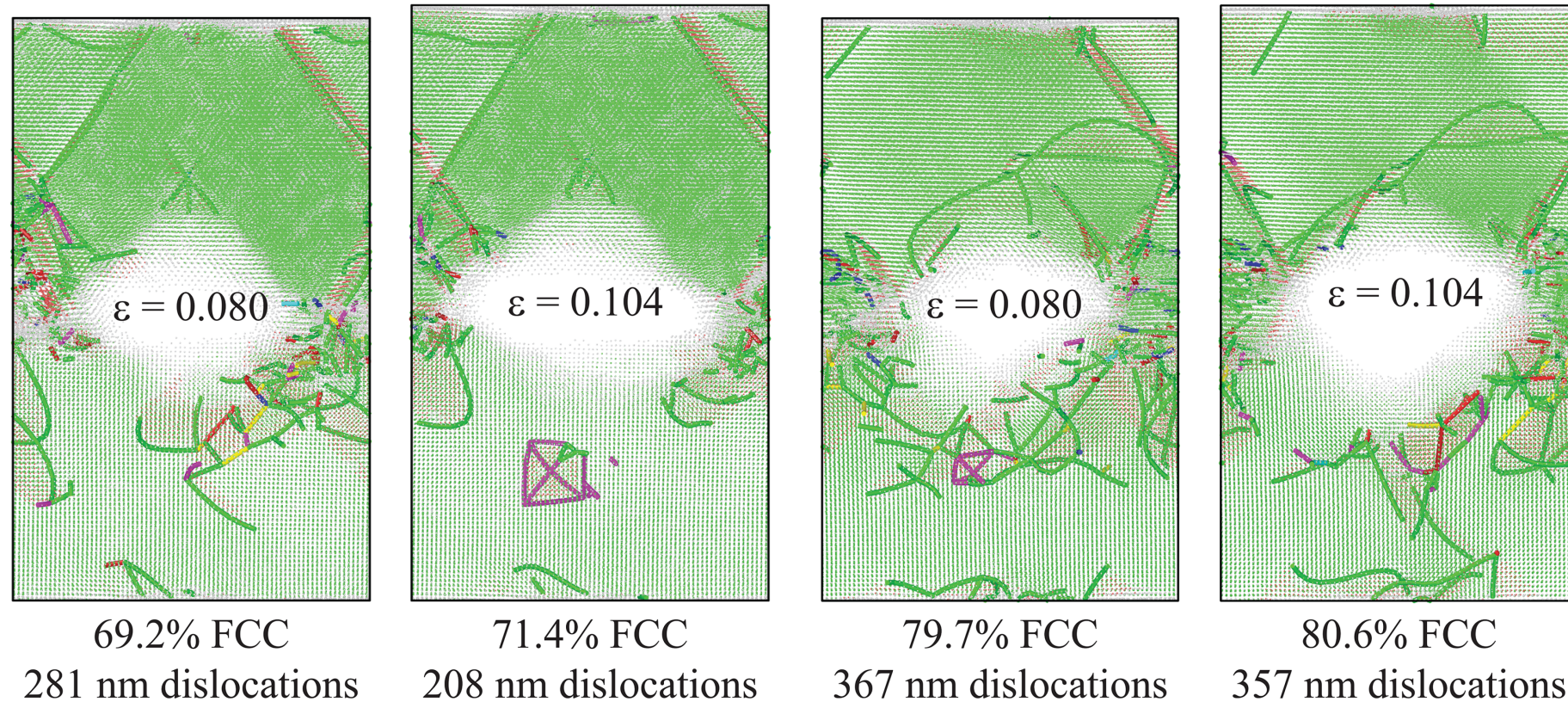
$\Sigma 5\{100\}$, system volume $V \sim 4600 \text{ nm}^3$, interfacial area $A \sim 210 \text{ nm}^2$
bubble radius $r = 3.0 \text{ nm}$, bubble pressure $P = 2 \text{ GPa}$, temperature $T = 300 \text{ K}$

Large strain rate overshoots stresses and energies. We will use $\dot{\epsilon} = 0.02 \text{ /ns}$.

Structures from Low and High Strain Rates

(a) low strain rate of 0.01 (1/ns)

(b) high strain rate of 0.20 (1/ns)



— : $\langle 110 \rangle / 2$ — : $\langle 112 \rangle / 6$ — : $\langle 110 \rangle / 6$ — : $\langle 001 \rangle / 3$ — : $\langle 111 \rangle / 3$ ■ : FCC ■ : HCP

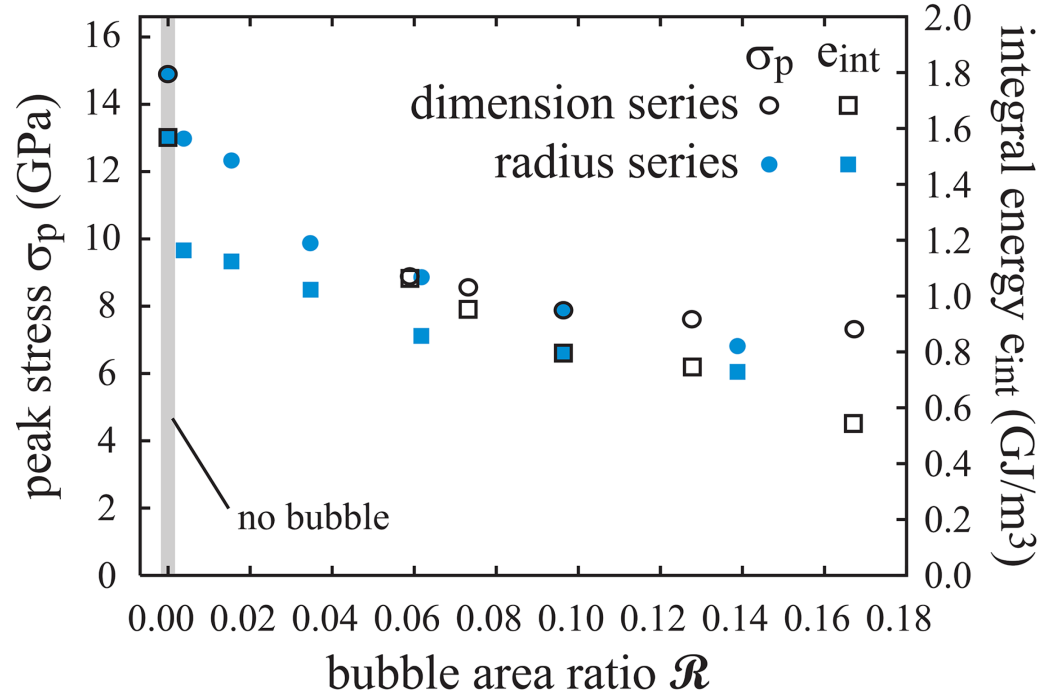
8 nm slice on x-y plane near bubble, $\Sigma 5 \{100\}$ grain boundary

bubble radius $r = 3.0$ nm, bubble pressure $P = 2$ GPa, temperature $T = 300$ K

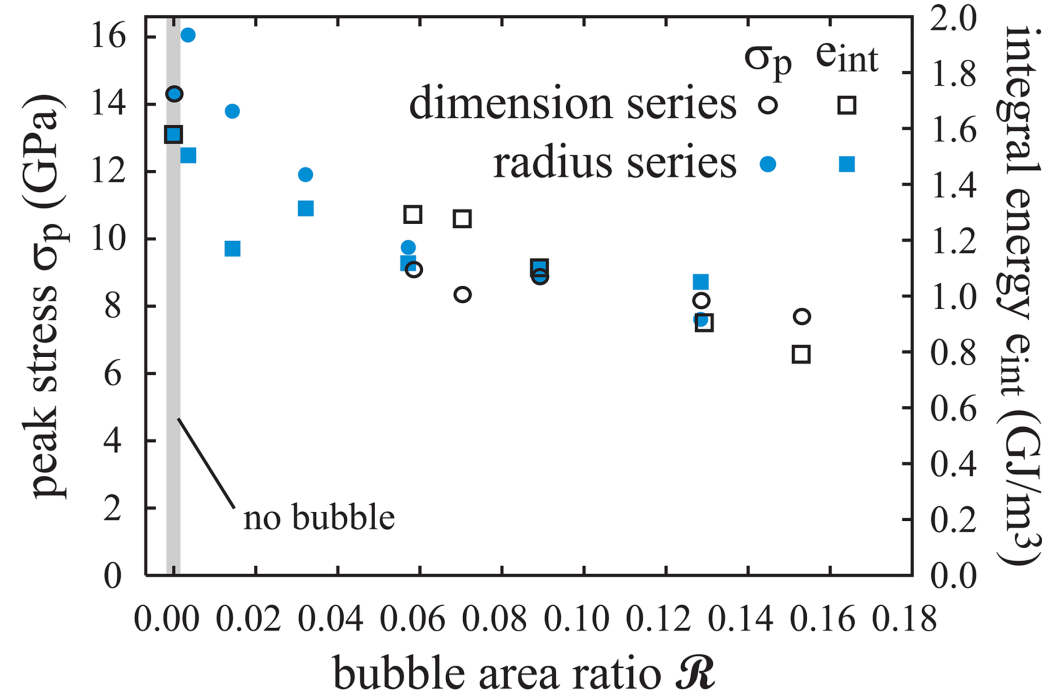
Large strain rate overshoots stresses and energies because dislocations do not have time to migrate and annihilate.

Areal Coverage Effects

(a) σ_p and e_{int} vs. \mathcal{R} for $\Sigma 9\{411\}$



(b) σ_p and e_{int} vs. \mathcal{R} for $\Sigma 11\{311\}$

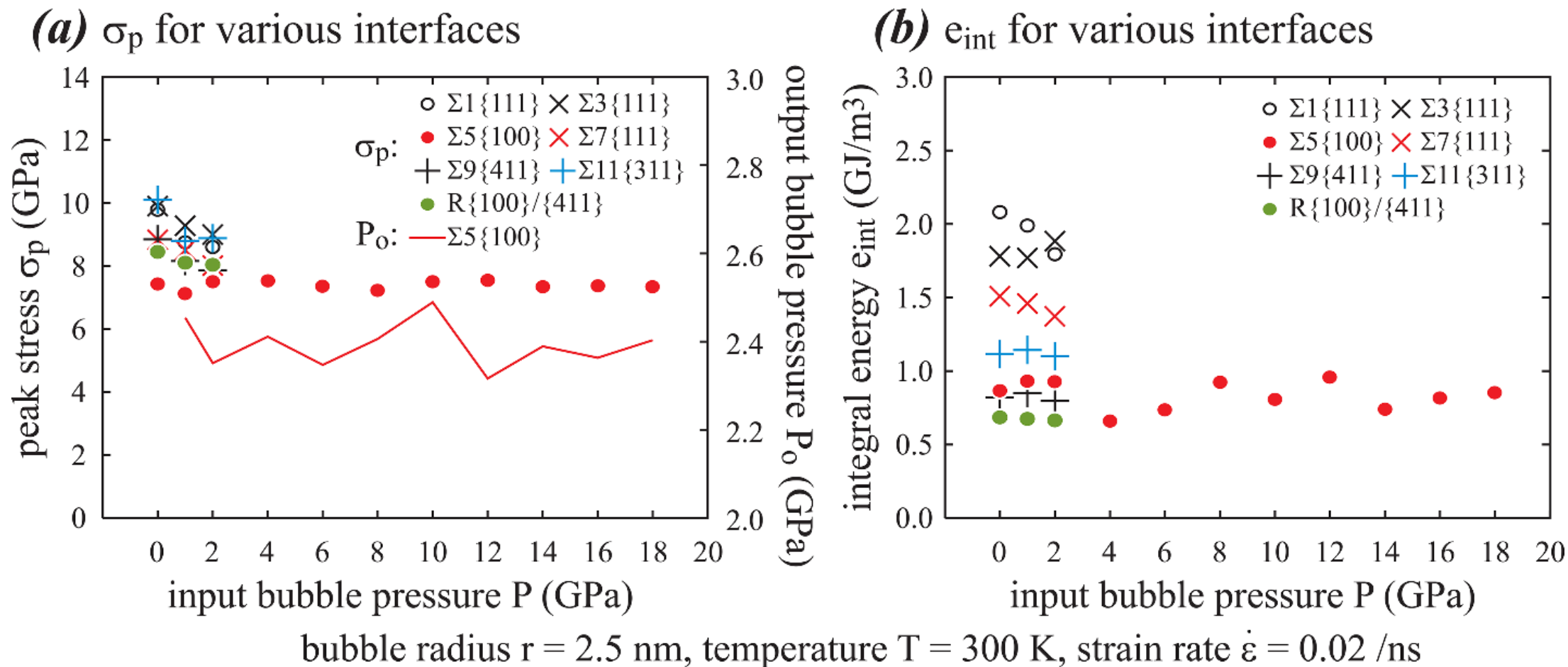


dimension series: bubble radius $r = 2.5$ nm; radius series: cross section area $\sim 15 \times 15$ nm²

bubble pressure $P = 2$ GPa, temperature $T = 300$ K, strain rate $\dot{\epsilon} = 0.02$ /ns

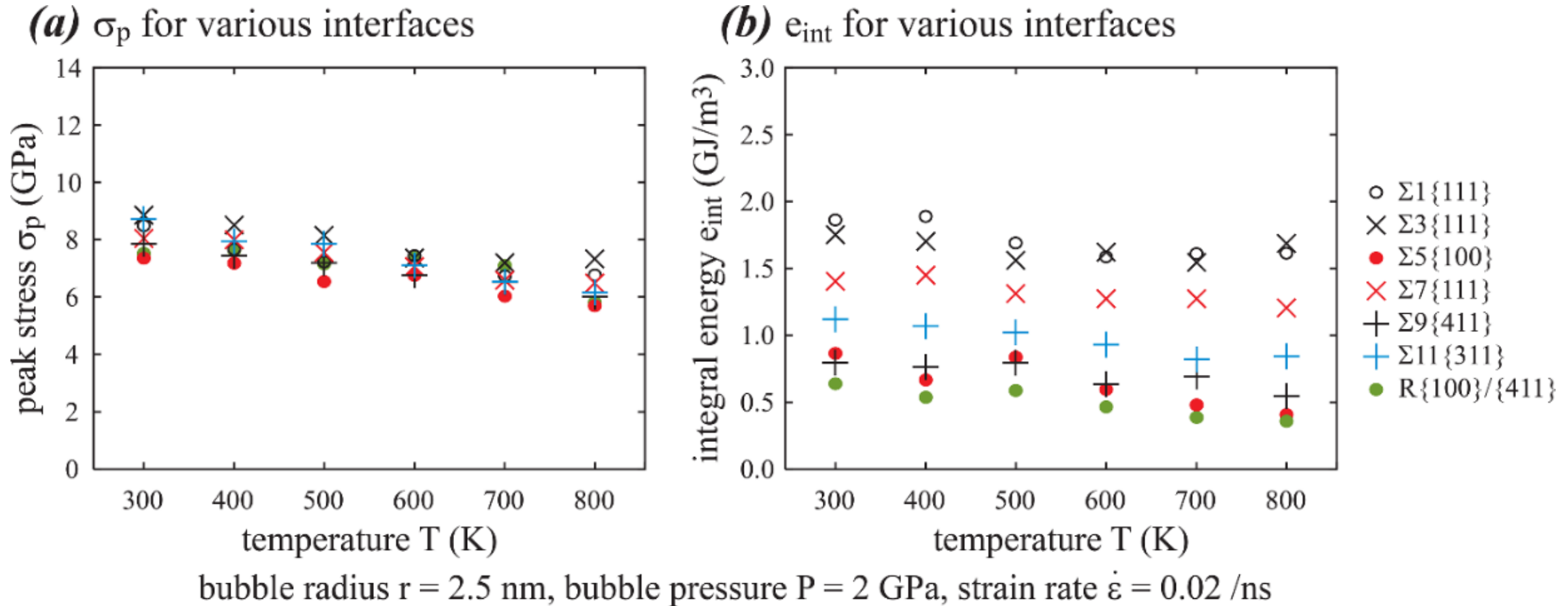
- ❑ Areal ratio can be changed by bubble radius or sample cross section area.
- ❑ The peak stress σ_p and integral energy e_{int} both decrease as bubble areal ratio increases.
- ❑ With the area effect understood, We will use cross section area $\sim 15 \times 15$ nm² below.

Bubble Pressure Effects



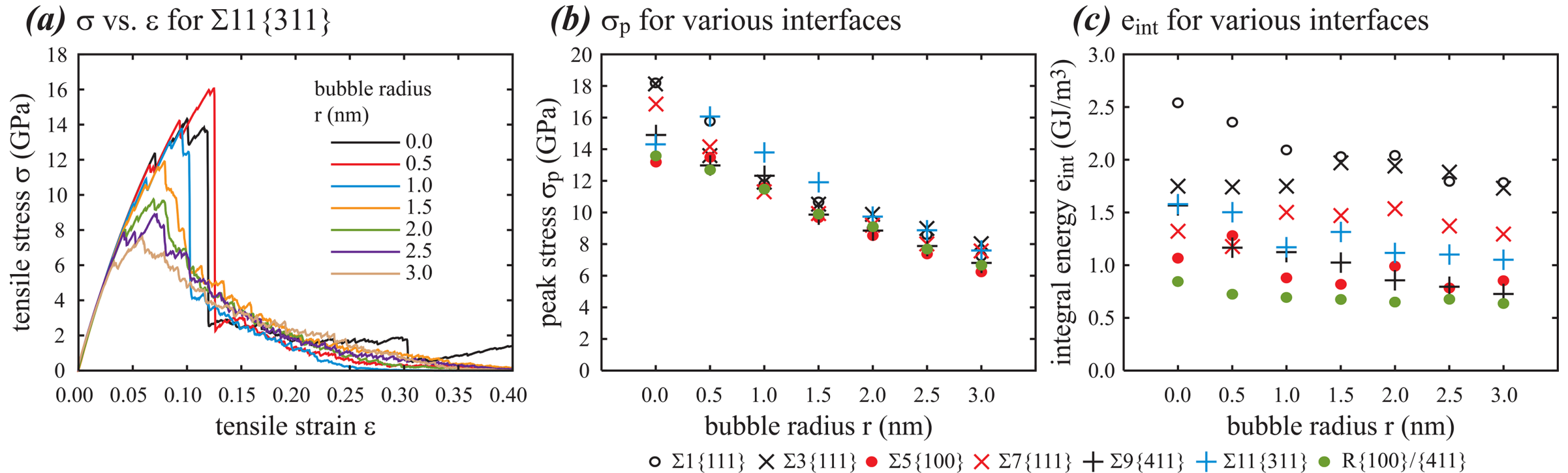
- ❑ Output pressure remains around 2.4 – 2.6 GPa in the input pressure range 0 – 20 GPa.
- ❑ Overall, increasing input pressure from 0 to 2 GPa decreases σ_p and e_{int} .

Temperature Effects



- Increasing temperature slightly reduces peak stress and integral energy.
- This is consistent with thermally activated nucleation and migration of dislocations.

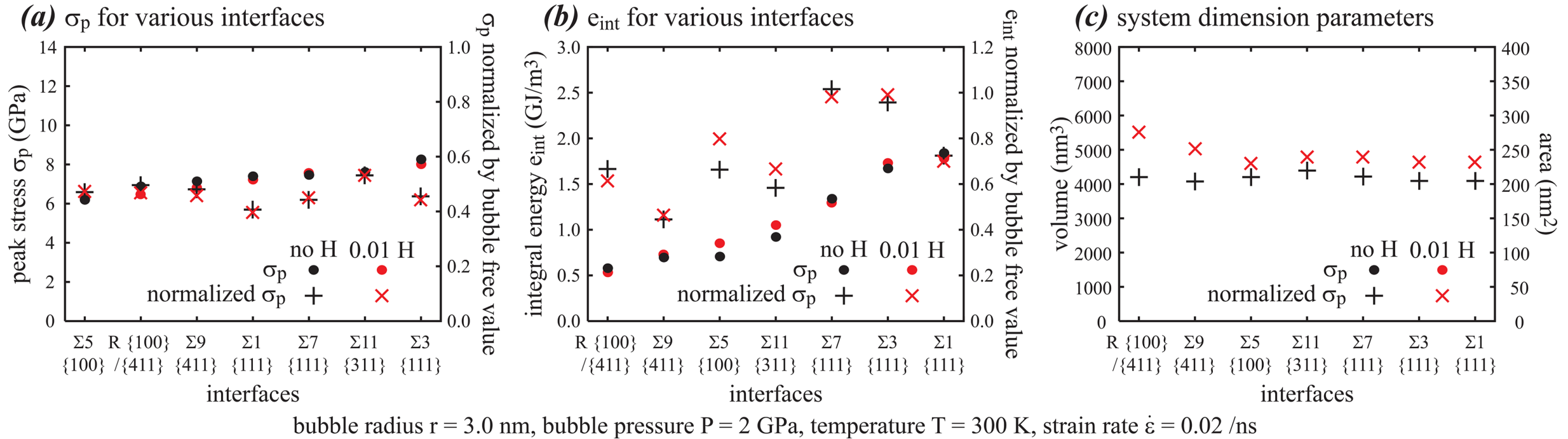
Bubble Radius Effects



bubble pressure $P = 2$ GPa, temperature $T = 300$ K, strain rate $\dot{\epsilon} = 0.02$ /ns

- Increasing bubble radius reduces peak stress and integral energy.
- Areal ratio seems to be more important than bubble radius.

Interface Type Effects

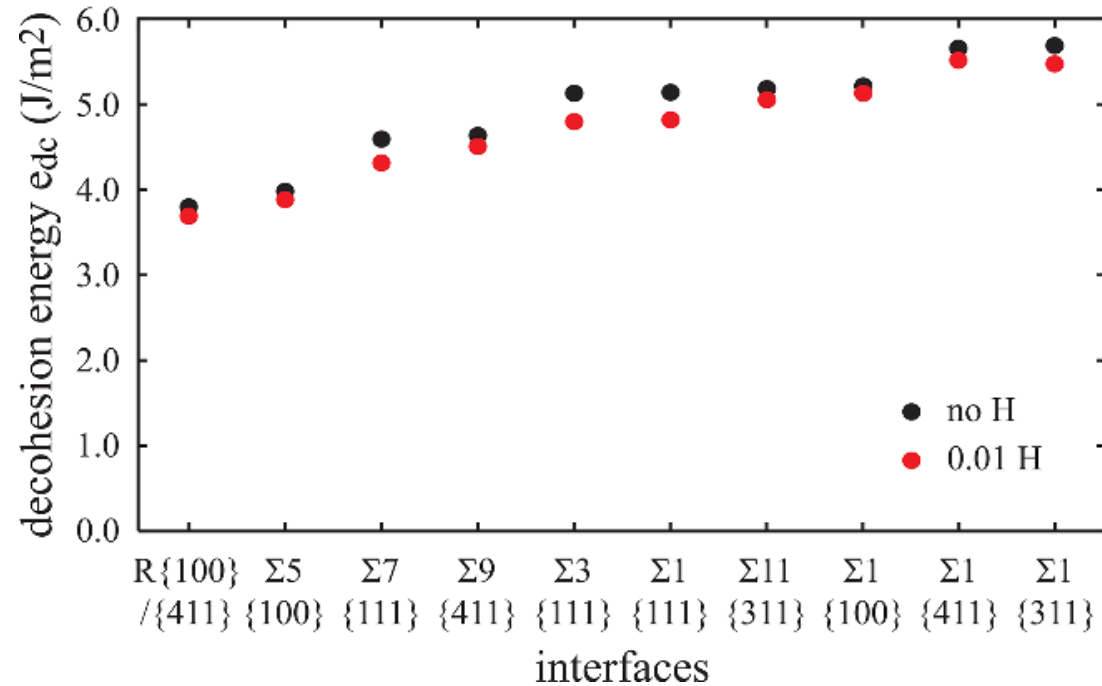


- ❑ σ_p and e_{int} trends are not the same, e_{int} is more reflective of fracture.
- ❑ Interface type more sensitively impacts e_{int} .

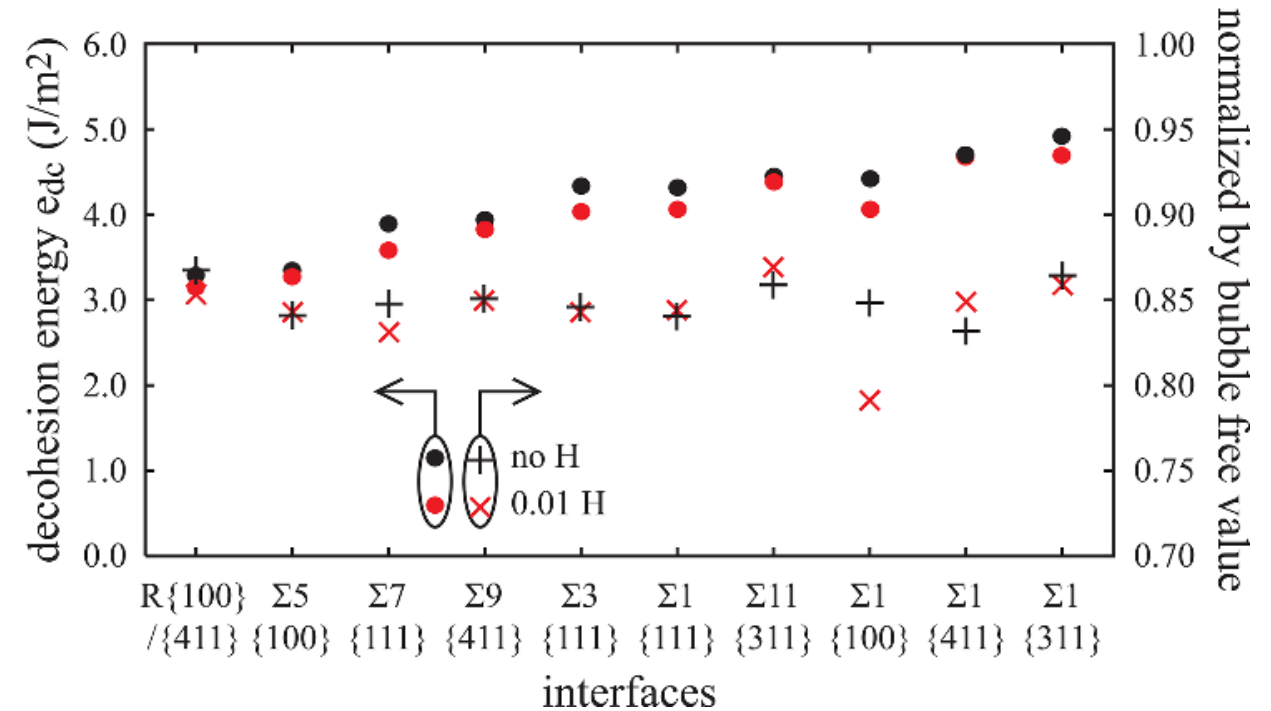
Decoherence Energies vs. Interfaces

(averaged over 40 ns)

(a) no bubble

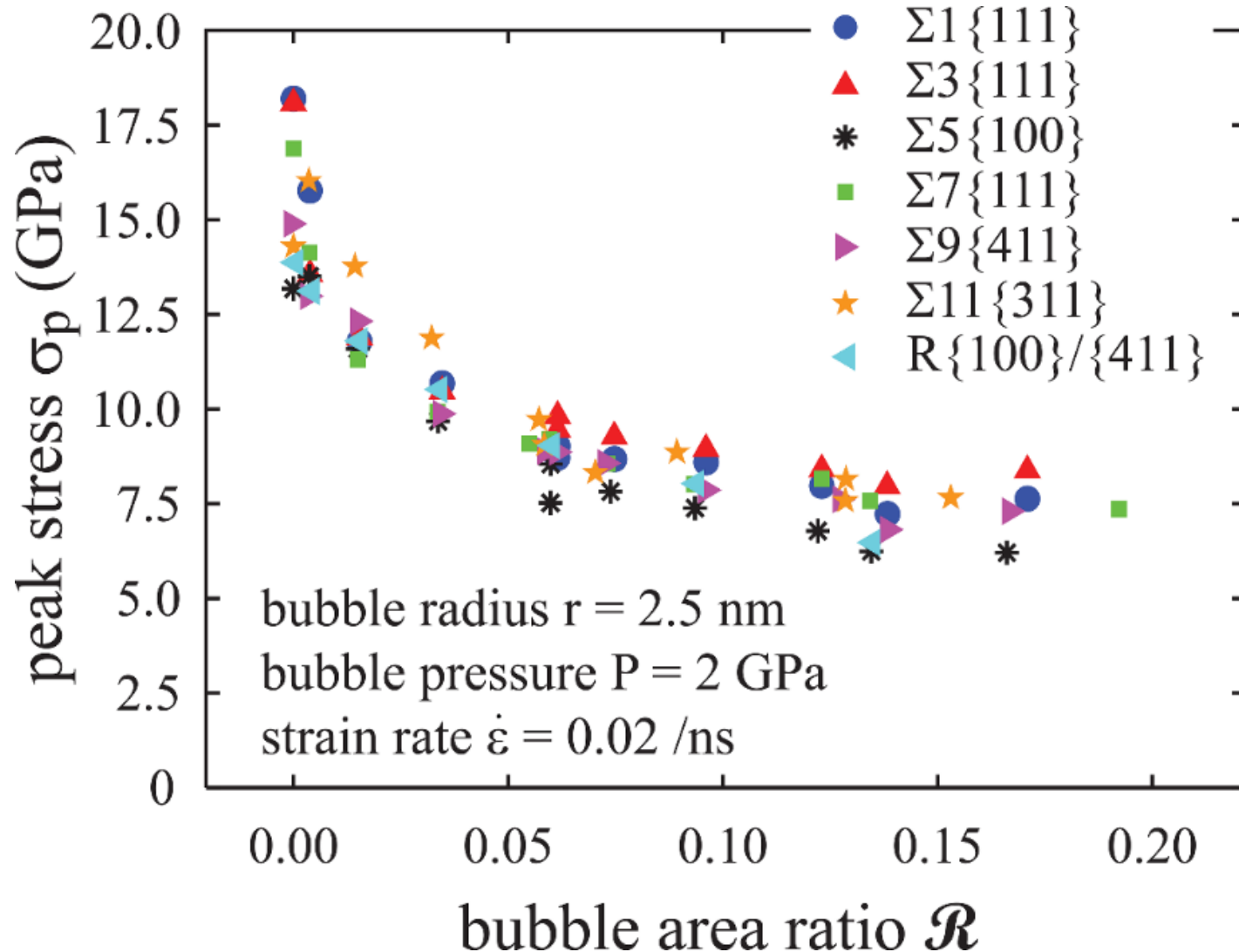


(b) a bubble with radius 2.5 nm



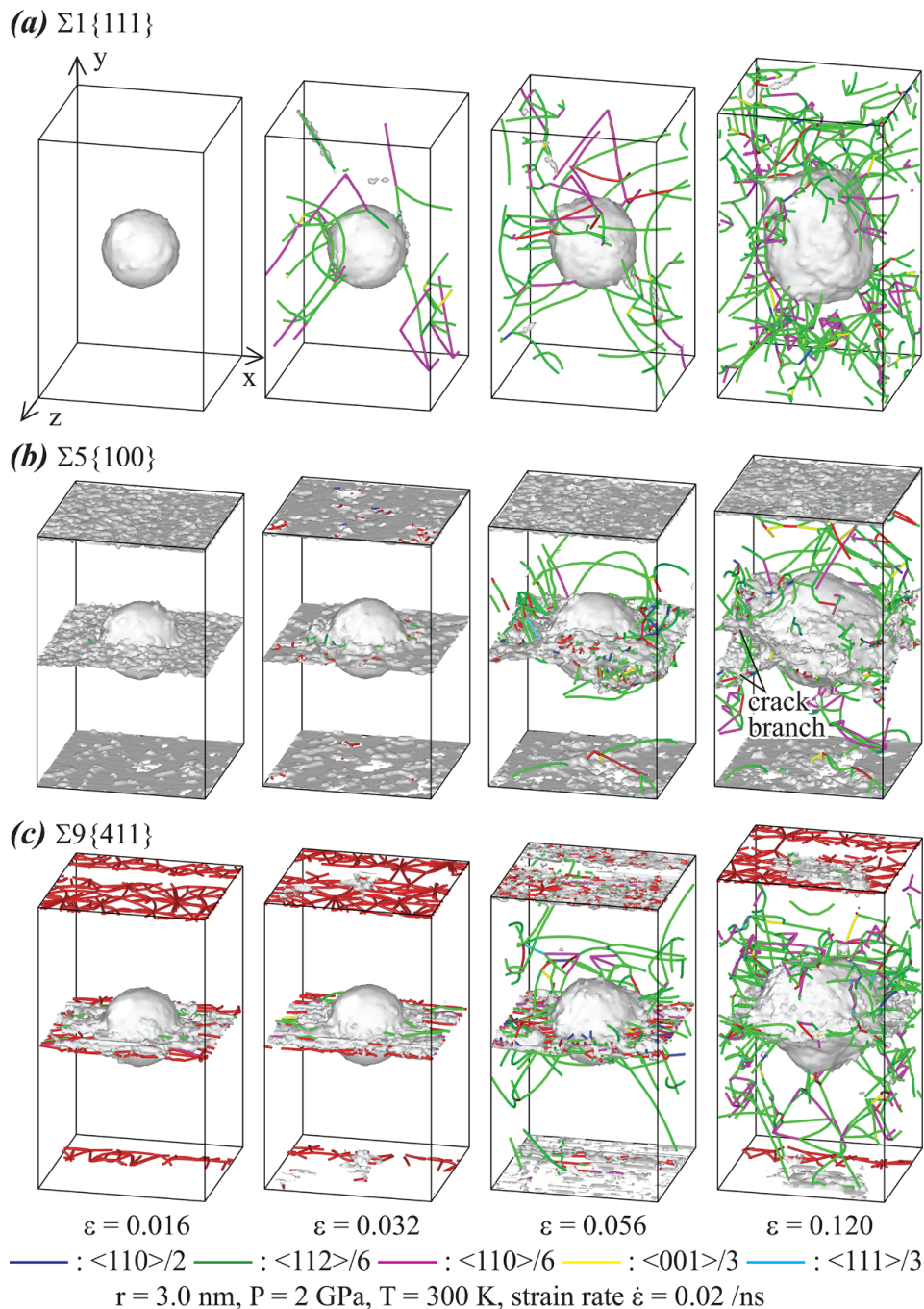
- ❑ $\Sigma 1 \{111\}$ is weaker than $\Sigma 11 \{311\}$, but the other cleavage planes are all stronger than GB or twin boundaries.
- ❑ The random GB $R\{100\}/\{411\}$ has the lowest decohesion energy.

Bubble Effects from All Data



- Peak stress is plotted as a function of areal coverage ratio from both the radius and dimension series for all GBs.
- Peak stress monotonically decreases with areal ratio.

Mechanistic Studies



- ❑ $\Sigma 1 \{111\}$ has an intermediate peak stress. Dislocation formation easier?
- ❑ Compared with $\Sigma 9 \{411\}$, $\Sigma 5 \{100\}$ has a higher integral energy but a lower decohesion energy. Why?
- ❑ We explored these by visualizing time evolution of atomic configurations.
- ❑ Indeed, the $\Sigma 1 \{111\}$ case forms dislocations early.
- ❑ The crack branches in the $\Sigma 5 \{100\}$ case causing it to have a high integral energy.

Conclusions

- ❑ Fracture energy decreases with increasing bubble areal ratio, bubble pressure, temperature, and bubble radius.
- ❑ Initial bubble pressure has little impact on intergranular fracture because it quickly drops once dislocations move.
- ❑ The bubble areal ratio has the most important effect on fracture.
- ❑ Interface type sensitively impacts fracture. GB more likely causes fracture than cleavage plane. Random GB more likely causes fracture than coherent GB.

Helium Equation of State

