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Detection of False Data Injection Attacks in Ambient Temperature-Dependent Battery Stacks

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Introduction

- Increased need for grid-scale energy storage systems
 - Battery Energy Storage Systems (BESSs)
 - Batteries are connected to meet voltage, current, and power requirements
- BESS employ a battery management system (BMS)
- State variable estimation and sensor measurements may be susceptible to cyber attacks

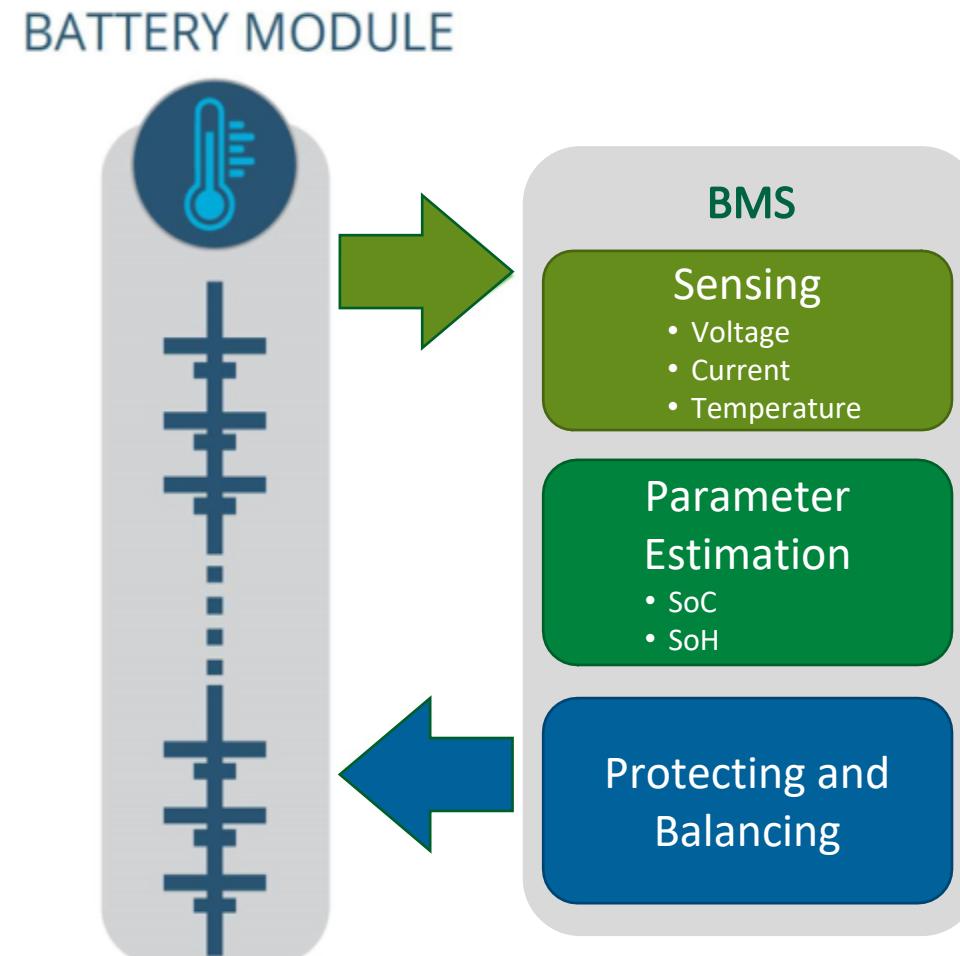


Figure 1. BMS functions

Problem Formulation

Goal: to increase battery cells' SoC estimation accuracy by incorporating ambient temperature dependent (ATD) models and by utilizing an Unscented Kalman Filter (UKF), then to detect FDIA in voltage sensors under various attack scenarios

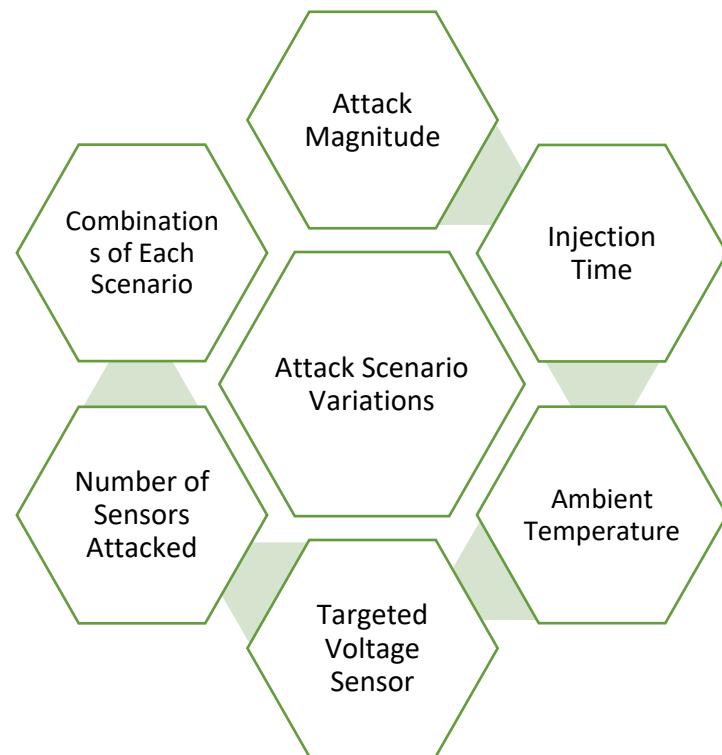


Figure 2. Tested Attack Scenario Variations

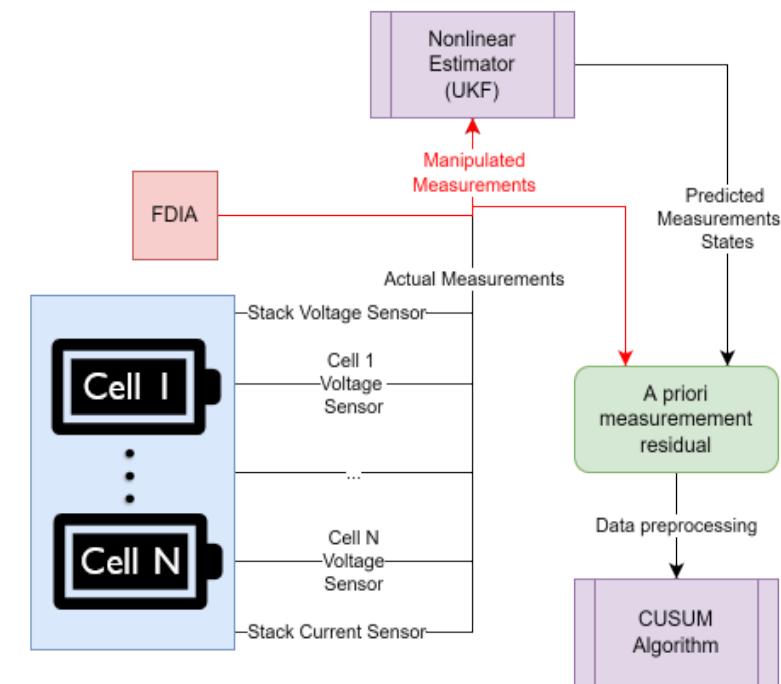


Figure 3. General process of SoC estimation and FDIA detection

False Data Injection Attacks (FDIAs)

- Possible Consequences:
 - Power outages
 - Damage to equipment / battery degradation
 - Thermal runaway events
 - Increased costs for utilities and consumers
- Bias attack:

$$y_a = y + \Delta y_a$$
 - Δy_a is the attack vector
 - y is the measurement vector
 - y_a is the manipulated measurement vector

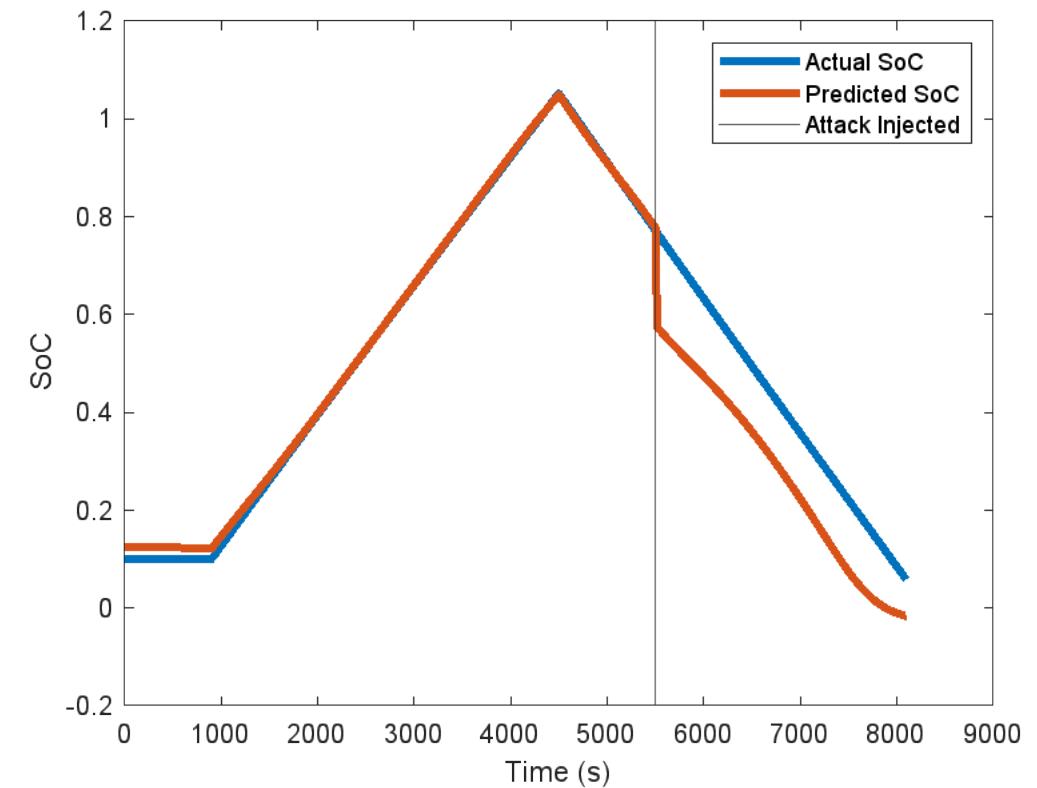


Figure 4. Cell 1 SoC when a 100 mV FDIA is Injected to the $v_{TOV,1}$ Measurement at 5500 s

Modeling Battery Dynamics

ATD Equivalent circuit model (ECM):

- Used to model dynamics of series-connected stacks of three batteries

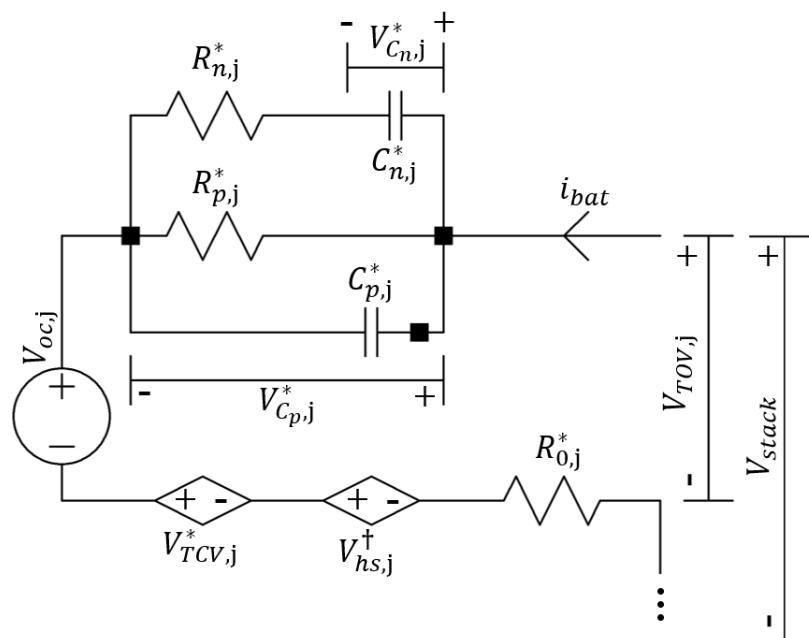


Figure 5. ECM for the j^{th} Cell in a Stack of N Batteries

State of Charge (SoC):

- Available capacity relative to total capacity
- Described by charge reservoir model (CRM)

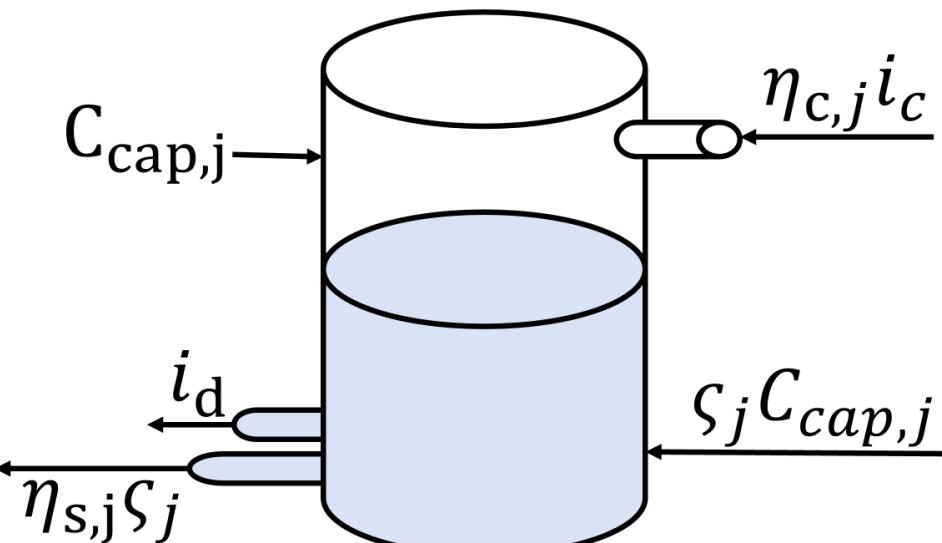


Figure 6. CRM for the j^{th} Cell in a Stack of N Batteries

Ambient Temperature Dependence

- Internal battery parameters vary with ambient temperature
- The battery parameters for Cell 2 and Cell 3 were generated by adding a random value to the parameters from Cell 1 (based on the variation between cells' parameters in [4]) and fitting a curve to the data

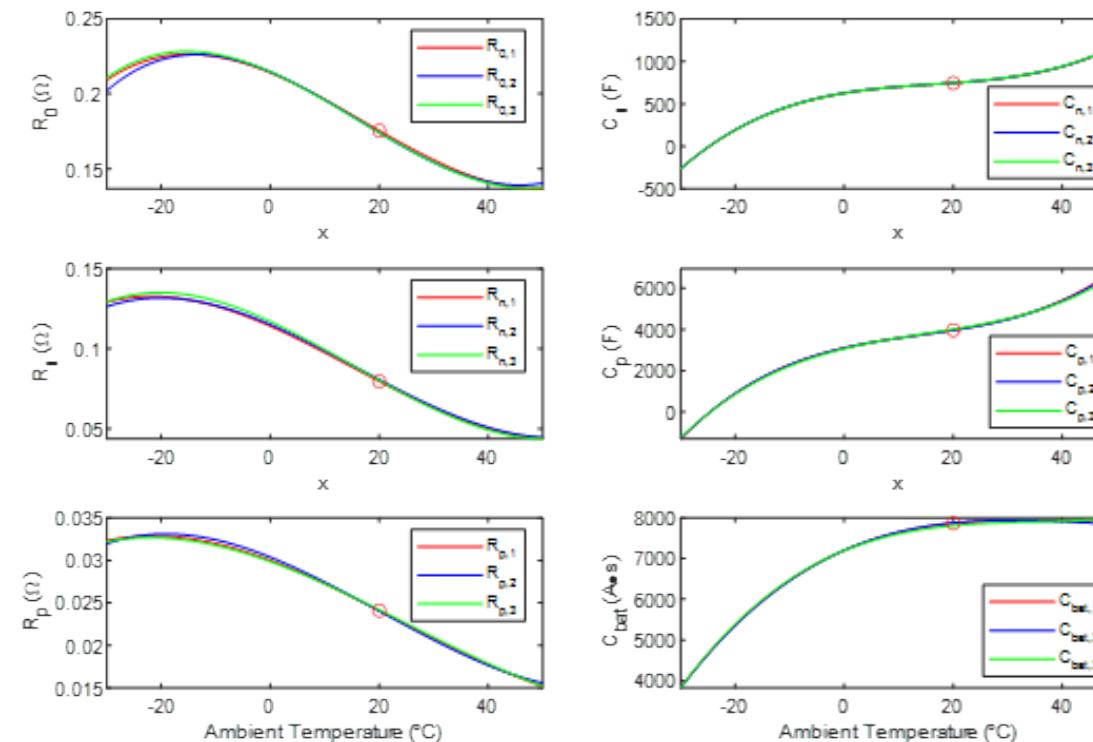


Figure 7. Internal battery parameter variation with ambient temperature [10]

Unscented Kalman Filter

- Typically more accurate for state estimation of nonlinear systems compared to the Extended Kalman Filter (EKF)
- Uses sigma points to represent the probability distribution of the nonlinear function



Figure 8. General steps of the UKF estimator

CUSUM Algorithm

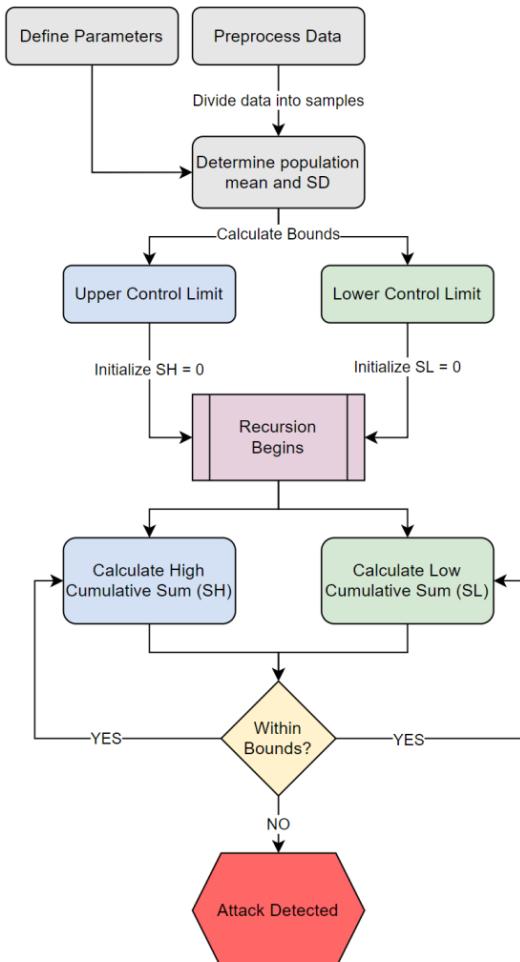


Figure 9. CUSUM Algorithm Flowchart

- Uses a priori residual with $\mu = 0$:

$$z[k|k-1] = y[k] - \hat{y}[k|k-1]$$

- Population Standard Deviation:

$$\sigma_z = \frac{A_3 \bar{s}}{3}$$

- Upper / Lower Control Limit:

$$UCL = h\sigma_z, LCL = -h\sigma_z$$

- High and Low CUSUM:

$$SH_i = \max(0, \bar{z}_i - \mu - k\sigma_z + SH_{i-1})$$

$$SL_i = \min(0, \bar{z}_i - \mu + k\sigma_z + SL_{i-1})$$

- Determine presence of attack:

$$SH_i > UCL \text{ or } SL_i < LCL \rightarrow \text{attack present}$$

$$SH_i \leq UCL \text{ and } SL_i \geq LCL \rightarrow \text{no attack}$$



Case Studies & Results

Case Study 1: Estimation Accuracy

- Goal: Compare the estimation accuracy of the UKF vs. the EKF
 - In terms of state and measurement estimation
 - Metrics: Maximum Absolute Error (MAE) and Root Mean Squared Error (RMSE)

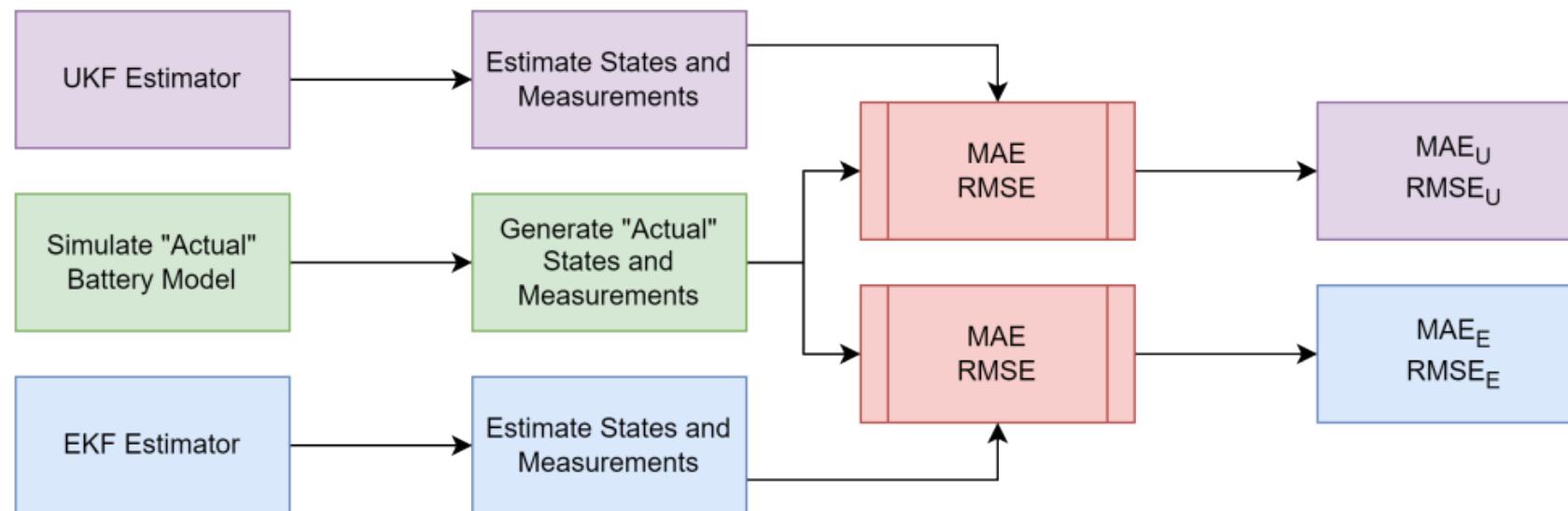


Figure 11. Estimation Accuracy Flowchart

Estimation Accuracy Results

- UKF vs. EKF error at various ambient temperatures

- Maximum Absolute Error (MAE):

$$MAE = \frac{1}{N} \sum_{i=1}^N |y_i - \hat{y}|$$

- Root Mean Squared Error (RMSE):

$$RMSE = \sqrt{\frac{1}{N} \sum_{i=1}^N (y_i - \hat{y})^2}$$

- UKF was more accurate estimating states and measurements in all cases compared to EKF

T (°C)	MAE _E	MAE _U
-10	0.0675	0.0295
0	0.0713	0.0360
10	0.0686	0.0364
20	0.0651	0.0358
30	0.0620	0.0354
40	0.0609	0.0355
50	0.0623	0.0377

T (°C)	RMSE _E	RMSE _U
-10	0.0936	0.0485
0	0.0964	0.0545
10	0.0931	0.0545
20	0.0892	0.0539
30	0.0859	0.0536
40	0.0836	0.0540
50	0.0835	0.0562

Case Study 2: CUSUM Detection

- Goals:
 - Determine the magnitude of the minimum detectable attack
 - Determine if CUSUM could detect attacks under each attack scenario variation
 - Minimize false positives

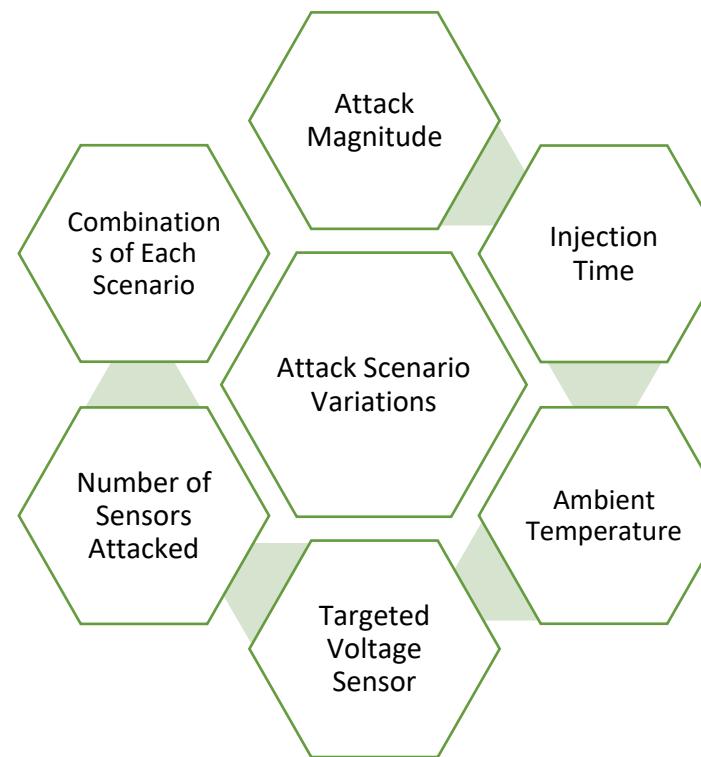
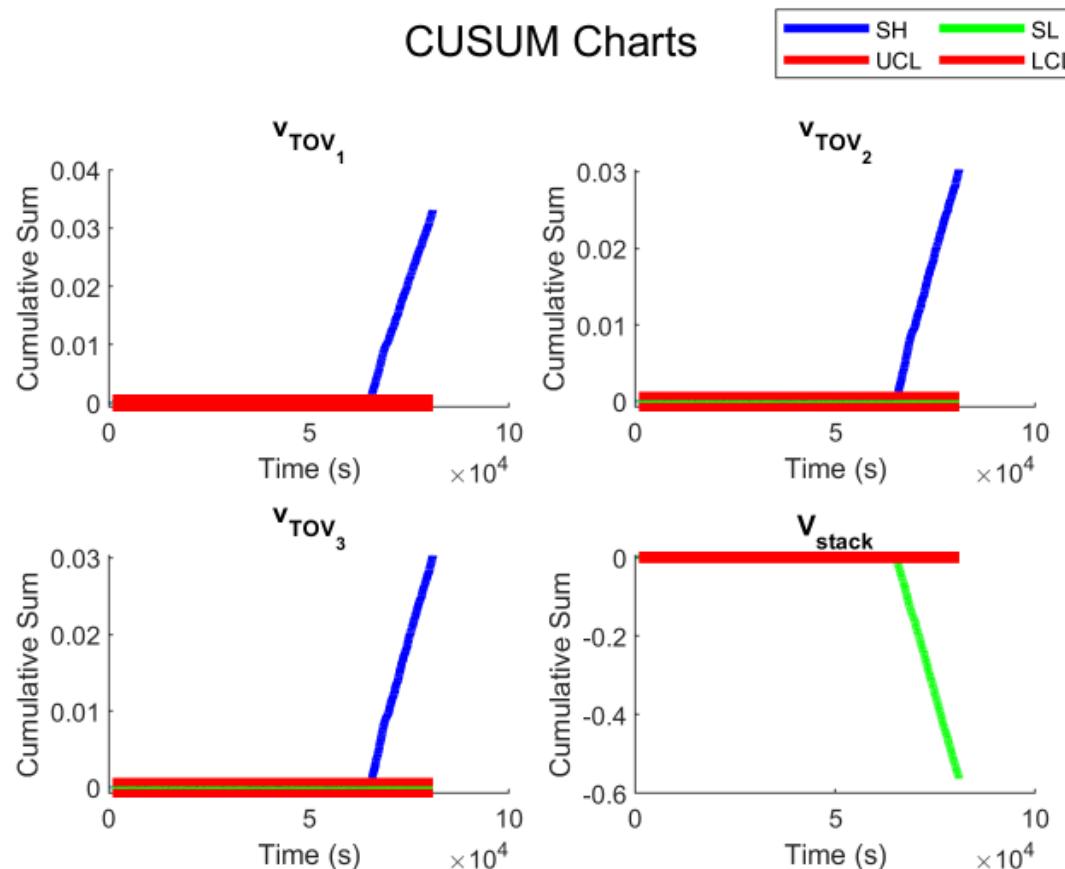


Figure 2. Tested Attack Scenario Variations

CUSUM Detection Results



- Attacks $\pm 1 \text{ mV}$ or greater were able to be detected
- Parameters that did not appear to have an impact on detectability:
 - Ambient temperature
 - Attack injection time
 - Targeted sensor
 - Number of sensors targeted
- No false positives

Figure 12. CUSUM Charts for a 1 mV Attack Injected to the v_{TOV_1} Sensor at a 6529 s and 39°C

Conclusions

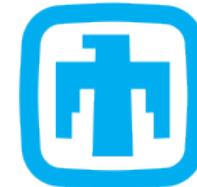
- The UKF was more accurate in estimating states and measurements in all cases compared to the EKF in terms of RMSE and MAE
- Attacks of $\pm 1 \text{ mV}$ or greater in voltage sensor(s) were able to be detected by the CUSUM algorithm
- The varying attack scenarios did not appear to have an impact on the CUSUM's ability to detect FDIs
- The CUSUM algorithm did not have any false positives when using the UKF or EKF

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Questions?

Thank you!

ATD ECM Governing Equations

$$\dot{V}_{C_{n,j}} = \frac{V_{C_{n,j}}}{R_{n,j}(T)C_{n,j}(T)} + \frac{V_{C_{p,j}}}{R_{n,j}(T)C_{n,j}(T)}$$

$$\dot{V}_{C_{p,j}} = -\frac{V_{C_{n,j}}}{R_{n,j}(T)C_{p,j}(T)} + \frac{i_{bat}}{C_{p,j}(T)} - \frac{V_{C_{p,j}}(R_{n,j}(T) + R_{p,j}(T))}{C_{p,j}(T)R_{n,j}(T)R_{p,j}(T)}$$

$$V_{hs,j} = p_{10}\zeta_j + p_{00}$$

$$V_{oc,j} = p_{30}\zeta_j^3 + p_{21}\zeta_j^2(T) + p_{20}\zeta_j^2 + p_{11}\zeta_j(T) + p_{10}\zeta_j + p_{01}(T) + p_{00}$$

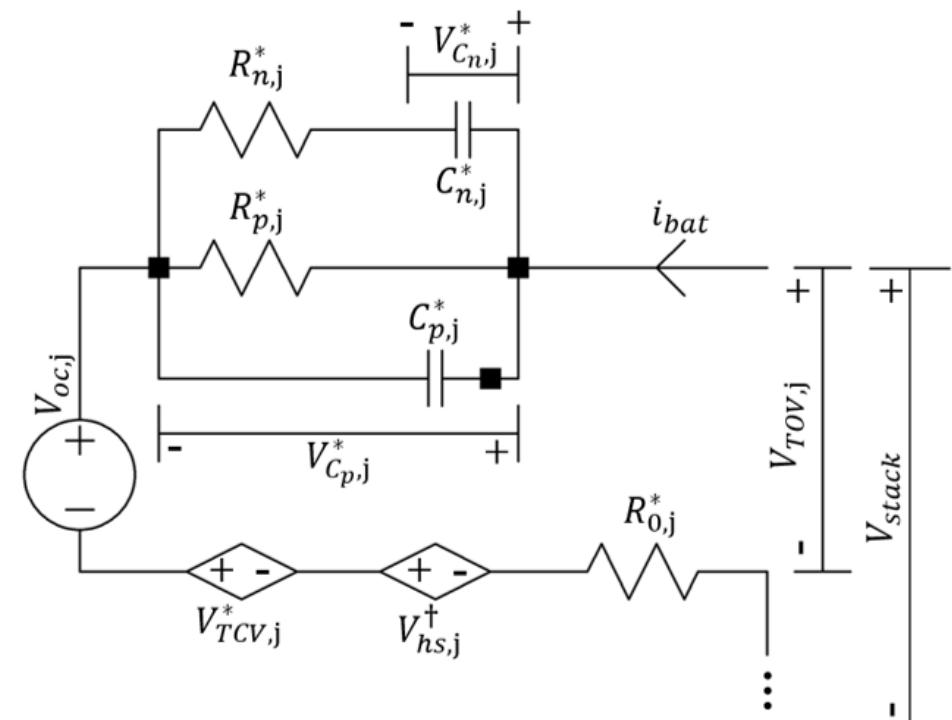
$$V_{TCV,j} = p_{02}(T)^2 + p_{01}(T) + p_{00}$$

$$V_{TOV,j} = V_{oc,j} + V_{C_{p,j}} + R_{0,j}(T)i_{bat} + V_{hs,j} + V_{TCV,j}$$

$$V_{stack} = V_{TOV,1} + \dots + V_{TOV,N}$$

$$i_{bat} = i_c + i_d$$

	p_{30}	p_{21} (10^{-3})	p_{20}	p_{11} (10^{-3})	p_{10} (10^{-2})	p_{02} (10^{-6})	p_{01} (10^{-3})	p_{00}
$V_{oc,1}$	1.36	-5	-1.917	7	8.79	-	-2	3.149
$V_{hs,1}$	-	-	-	-	-7.55	-	-	0.0755
$V_{TCV,1}$	-	-	-	-	-	-9.2	1.2	-0.097
$V_{oc,2}$	1.37	-5	-1.921	7.1	8.867	-	-2	3.149
$V_{hs,2}$	-	-	-	-	-7.27	-	-	0.07353
$V_{TCV,2}$	-	-	-	-	-	-9.98	1.242	-0.0964
$V_{oc,3}$	1.37	-5	-1.923	7.06	9.02	-	-2	3.149
$V_{hs,3}$	-	-	-	-	-7.869	-	-	0.077
$V_{TCV,3}$	-	-	-	-	-	-10.75	1.188	-0.0953



ATD Equations and Coefficients

$$P_{n,j} = p_{03}T^3 + p_{02}T^2 + p_{01}T + p_{00}$$

	p_{03}	p_{02}	p_{01}	p_{00}
$R_{0,1}$	$6.8 \cdot 10^{-7}$	$-3.5 \cdot 10^{-5}$	$-1.5 \cdot 10^{-3}$	0.214
$R_{p,1}$	$5.4 \cdot 10^{-8}$	$-3.8 \cdot 10^{-6}$	$-2.4 \cdot 10^{-4}$	0.03
$C_{p,1}$	0.04	-1.677	61.1	3100
$R_{n,1}$	$4.4 \cdot 10^{-7}$	$-2 \cdot 10^{-5}$	$-1.5 \cdot 10^{-3}$	0.114
$C_{n,1}$	$8 \cdot 10^{-3}$	-0.39	10.6	625
$C_{cap,1}$	0.012	-1.4652	57.6	7200
$R_{0,2}$	$8.373 \cdot 10^{-7}$	$-4.057 \cdot 10^{-5}$	$1.548 \cdot 10^{-3}$	0.2146
$R_{p,2}$	$7.461 \cdot 10^{-8}$	$-4.53 \cdot 10^{-6}$	$-2.56 \cdot 10^{-4}$	0.03
$C_{p,2}$	0.0397	-1.682	60.9	3099
$R_{n,2}$	$4.654 \cdot 10^{-7}$	$-2.232 \cdot 10^{-5}$	$-1.459 \cdot 10^{-3}$	0.1151
$C_{n,2}$	$8.17 \cdot 10^{-3}$	-0.39	10.5	628
$C_{cap,2}$	0.0112	-1.47	58.68	7198
$R_{0,3}$	$7.356 \cdot 10^{-7}$	$-3.565 \cdot 10^{-5}$	$-1.604 \cdot 10^{-3}$	0.2146
$R_{p,3}$	$4.779 \cdot 10^{-8}$	$-3.639 \cdot 10^{-6}$	$2.301 \cdot 10^{-4}$	0.02986
$C_{p,3}$	0.03483	-1.59	64.83	3066
$R_{n,3}$	$5.116 \cdot 10^{-7}$	$-2.346 \cdot 10^{-5}$	$-1.574 \cdot 10^{-3}$	0.1169
$C_{n,3}$	$8.04 \cdot 10^{-3}$	-0.39	10.6	626
$C_{cap,3}$	0.01435	-1.489	54.69	7192

UKF Equations

Step 1: Initialization

$$\hat{x}_{0|0} = \mathbb{E}[x_0]$$

$$P_{0|0} = P_0$$

Step 2: Prediction of States

$$\hat{x}_{k+1|k} = A\hat{x}_{k|k} + Bu_k$$

$$P_{k+1|k} = AP_{k|k}A^T + Q_k$$

Step 3: Generate the SPs and associated weights

$$\mathcal{X}_{0_{k+1|k}} = \hat{x}_{k+1|k}$$

$$\mathcal{X}_{i_{k+1|k}} = \hat{x}_{k+1|k} + \left(\sqrt{(n + \lambda)P_{k+1|k}} \right)_i$$

$$\mathcal{X}_{i+n_{k+1|k}} = \hat{x}_{k+1|k} - \left(\sqrt{(n + \lambda)P_{k+1|k}} \right)_i$$

$$W_{m_{k+1|k}}^0 = \frac{\lambda}{n + \lambda}$$

$$W_{c_{k+1|k}}^0 = W_{m_{k+1|k}}^0 + (1 - a^2 + b)$$

$$W_{m_{k+1|k}}^i = W_{c_{k+1|k}}^i = \frac{1}{2(n + \lambda)}$$

$$\lambda = a^2(n + \kappa) - n$$

Step 4: Correction

$$\hat{y}_{k+1|k} = \sum_{i=0}^{2n} W_m^i \cdot h(\mathcal{X}_{i_{k+1|k}})$$

$$P_{xy_{k+1|k}} = \sum_{i=0}^{2n} W_c^i \left(\mathcal{X}_{i_{k+1|k}} - \hat{x}_{k+1|k} \right) \cdot \left\{ h(\mathcal{X}_{i_{k+1|k}}) - \hat{y}_{k+1|k} \right\}^T$$

$$P_{yy_{k+1|k}} = \sum_{i=0}^{2n} W_c^i \left(h(\mathcal{X}_{i_{k+1|k}}) - \hat{y}_{k+1|k} \right) \cdot \left\{ h(\mathcal{X}_{i_{k+1|k}}) - \hat{y}_{k+1|k} \right\}^T$$

$$S_{k+1} = P_{yy_{k+1|k}} + R_{k+1}$$

$$K_{k+1} = P_{xy_{k+1|k}} \cdot S_{k+1}^{-1}$$

$$\hat{x}_{k+1|k+1} = \hat{x}_{k+1|k} + K_{k+1} \cdot (y_{k+1} - \hat{y}_{k+1|k})$$

$$P_{k+1|k+1} = P_{k+1|k} - K_{k+1} S_{k+1} K_{k+1}^T$$

Parameter	n	a	b	κ	λ
Value	9	0.1	2	0	-8.91

EKF Equations

$$\hat{x}[k|k-1] = f(\hat{x}[k-1|k-1], u[k-1], \mathbb{E}[w[k-1]])$$

$$P[k|k-1] = AP[k-1|k-1]A^T + Q$$

$$\hat{x}[k|k] = \hat{x}[k|k-1] + K[k](y[k] - \hat{y}[k|k-1])$$

$$\hat{y}[k|k-1] = g(\hat{x}[k|k-1], u[k], \mathbb{E}[e[k]])$$

$$\hat{y}[k|k] = g(\hat{x}[k|k], u[k], \mathbb{E}[e[k]])$$

$$P[k|k] = P[k|k-1] - K[k]CP[k|k-1]$$

$$K[k] = P[k|k-1]C^T(CP[k|k-1]C^T + R)^{-1}$$

$$A[k] = \frac{\partial f(x[k], u[k], w[k])}{\partial x[k]} \Big|_{x[k] = \hat{x}[k|k]}$$

$$C[k|k] = \frac{\partial g(x[k], u[k], v[k])}{\partial x[k]} \Big|_{x[k] = \hat{x}[k|k]}$$

$$C[k|k-1] = \frac{\partial g(x[k], u[k], v[k])}{\partial x[k]} \Big|_{x[k] = \hat{x}[k|k-1]}$$

UKF vs. EKF Characteristics

UKF

- Works well in all nonlinearities
- Uses sigma points to represent probability distribution of function
- Theoretically more accurate than EKF
- Examples of applications: power batteries, personal navigation

EKF

- Works well in systems represented by linear approximations
- Requires calculation of Jacobian matrix
- Examples of applications: electric vehicle batteries, temperature-dependent batteries