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Actuation Response of Glass-Ceramics

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Sandia National Laboratories

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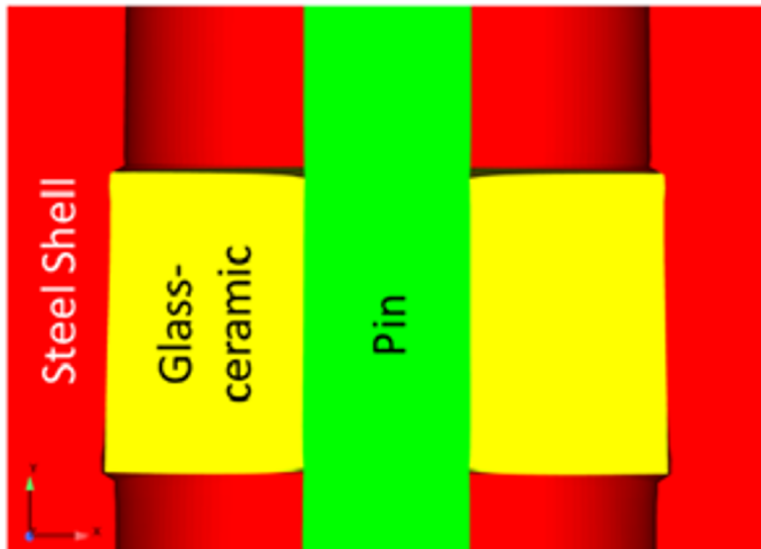
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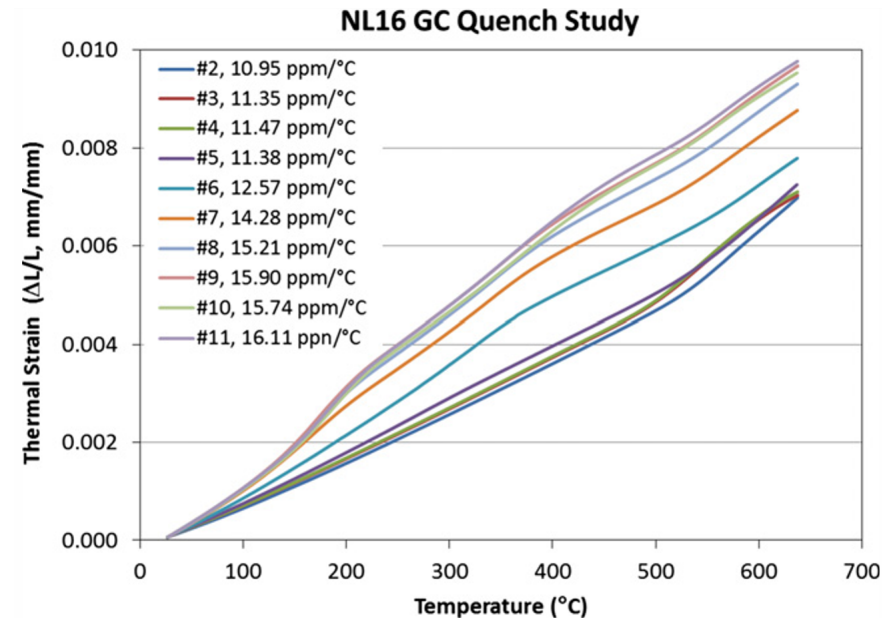


Glass-ceramic to Metal Seals (GcTMS)

- Variety of industrial applications for glass-ceramics
 - Hermetic glass-ceramic to metal seals (GcTMS)
 - Subject to complex thermomechanical histories



Dai *et al.*, 2017, *J Am Ceram Soc*, 100, pp.3652-3661

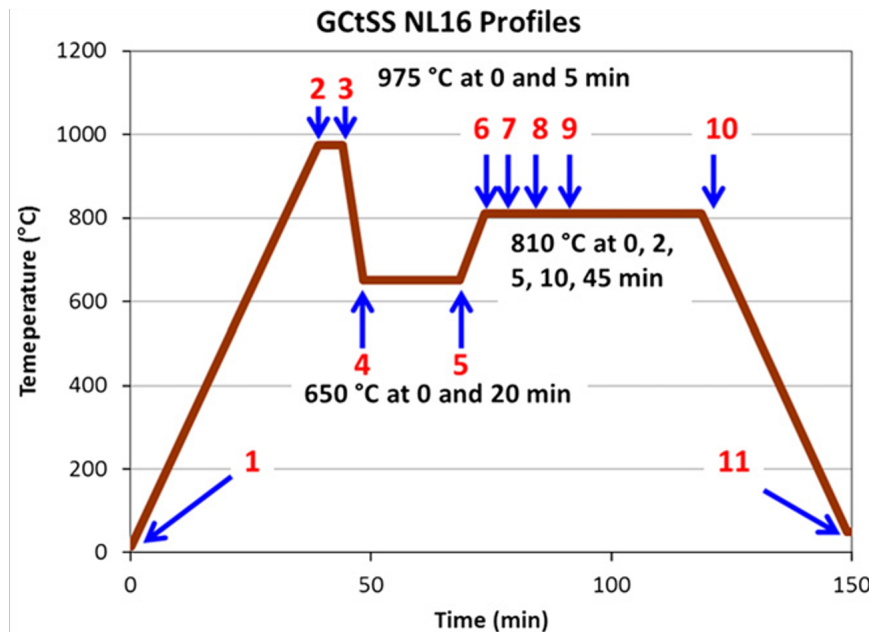


Dai *et al.*, 2016, *J Am Ceram Soc*, 99, pp.3719-3725



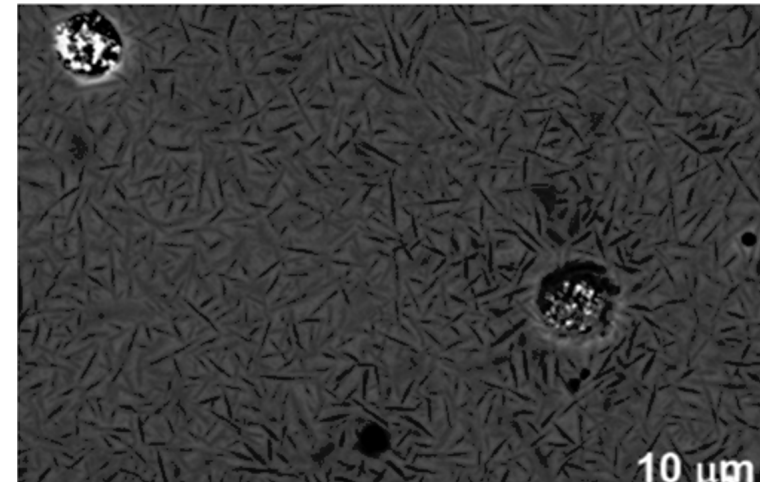
Glass-Ceramics - Microstructure

- Glass-ceramics are produced by inducing a ceramic phase(s) in an inorganic base glass
- Advantageous features arise from microstructure
 - Up to 5 constituents
 - Inelasticity from residual glass and silica polymorphs



Dai *et al.*, 2016, *J Am Ceram Soc*, 99 (11), pp.3719-3725

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Rodriguez *et al.*, 2016, *J Am Ceram Soc*, 99 (11), pp.3726-3733



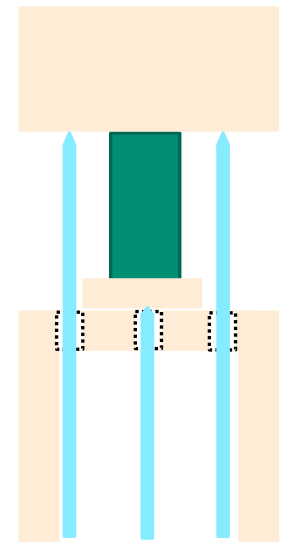
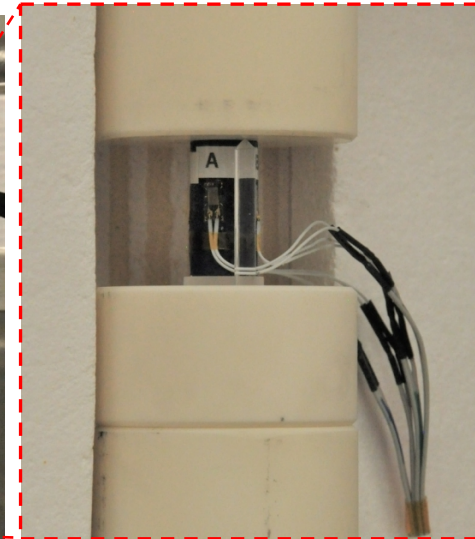
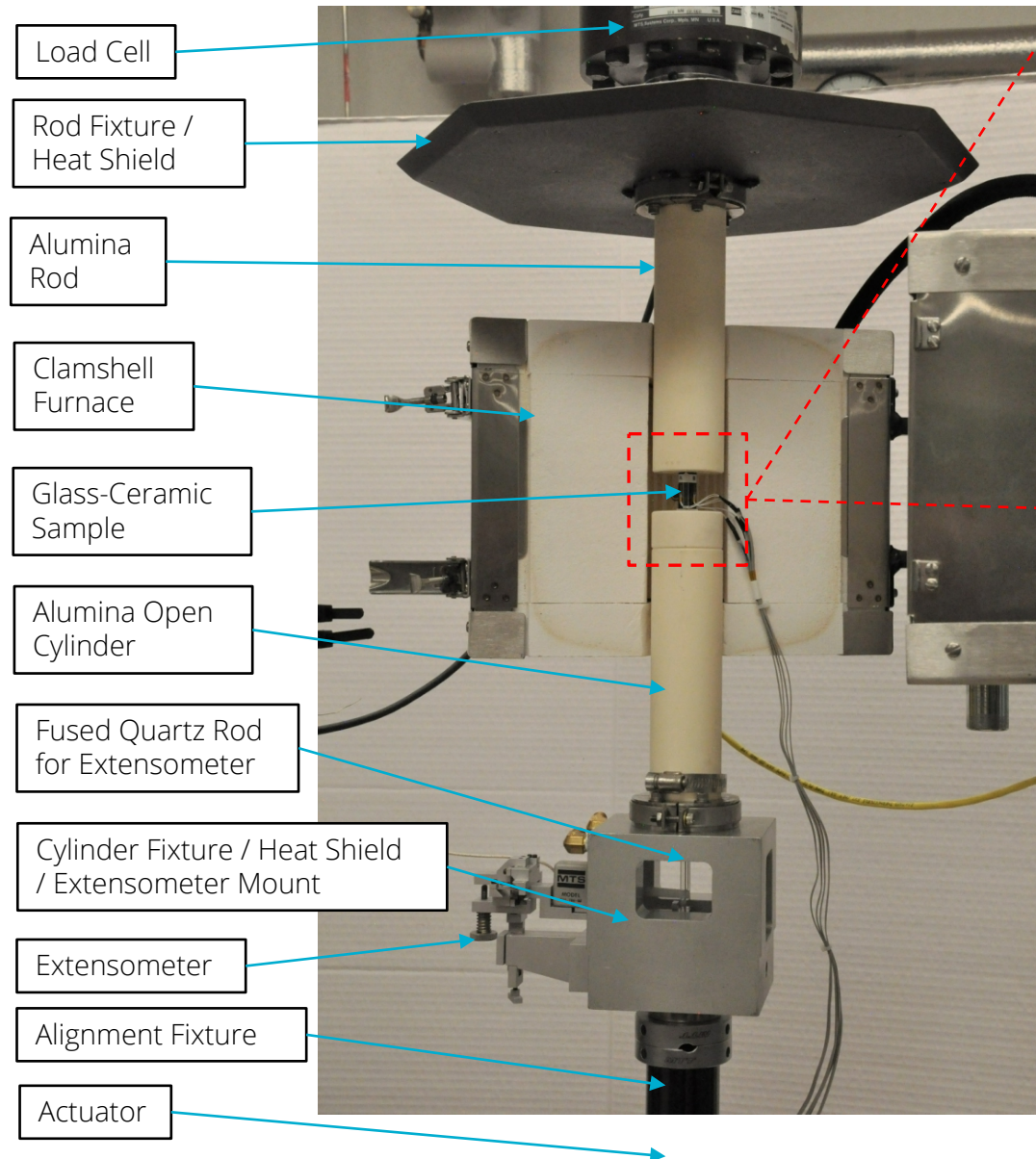
Objective

- Understanding actuation response essential for intended use
- Actuation not well understood experimentally or modeled
 - Experimental studies focused on other features (e.g. dilatometry, DMA)
 - Models leverage alternative phenomenologies
- Objective: Elucidate and enhance understanding of actuation response
 - Perform first of the kind experiments to characterize thermomechanical response
 - Develop new model capable of describing coupled phase-transformation and viscoelasticity



Experimental Set-up

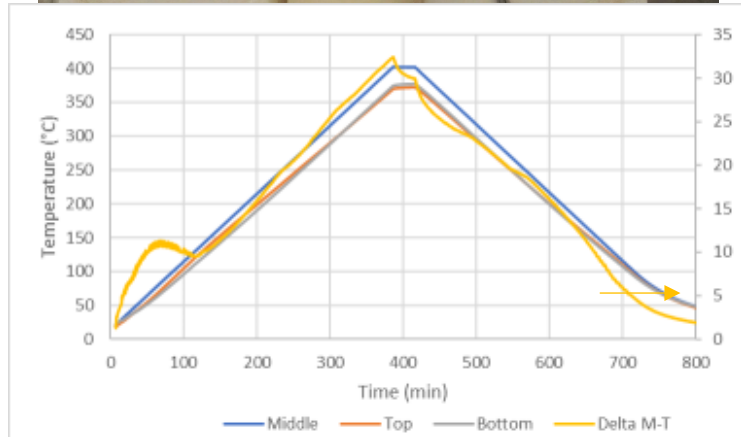
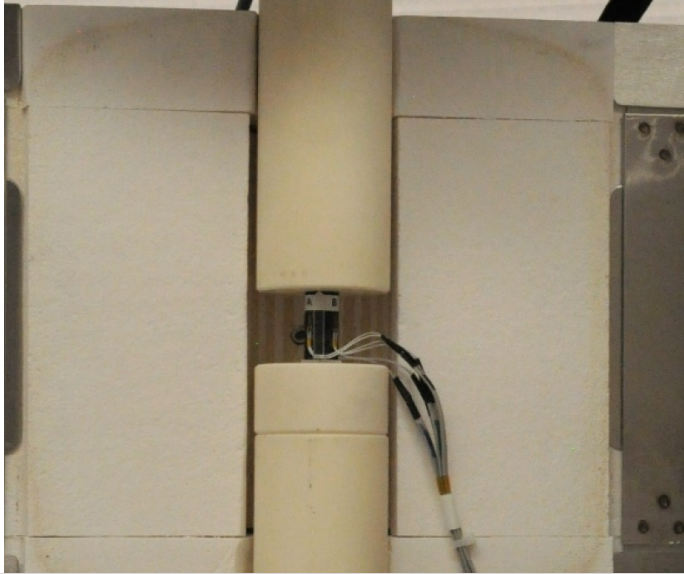
- Experimental challenges:
 - Thermal homogeneity
 - Precise strain measurement
 - Higher loads
- Developed novel thermomechanical test chamber
 - Novel extensometer and stage design
 - Clamshell furnace





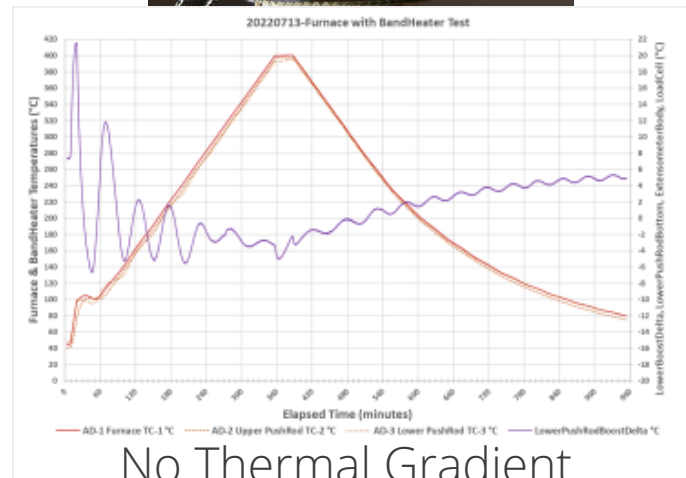
Experimental Thermal Control

Alumina Top and Bottom
No Band Heater



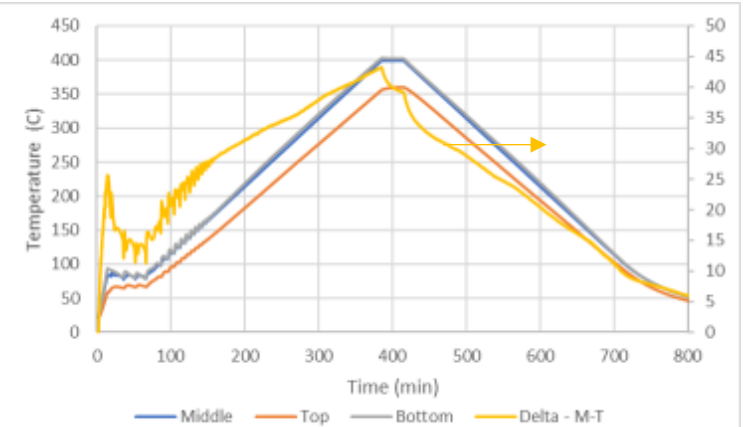
Thermal Gradient Across the Sample

Quartz Top Alumina Bottom
Band Heater



No Thermal Gradient

Alumina Top and Bottom
Band Heater

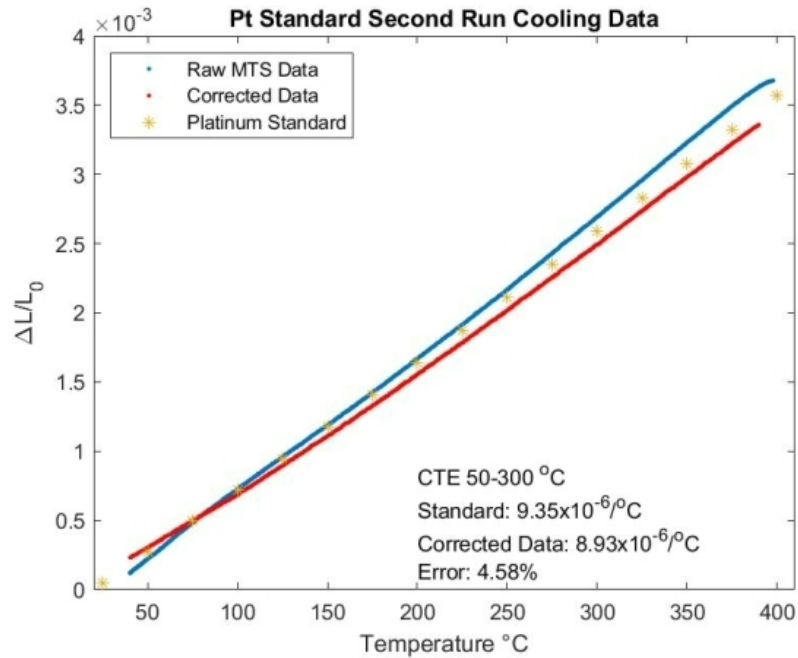


Minimal Thermal Gradient



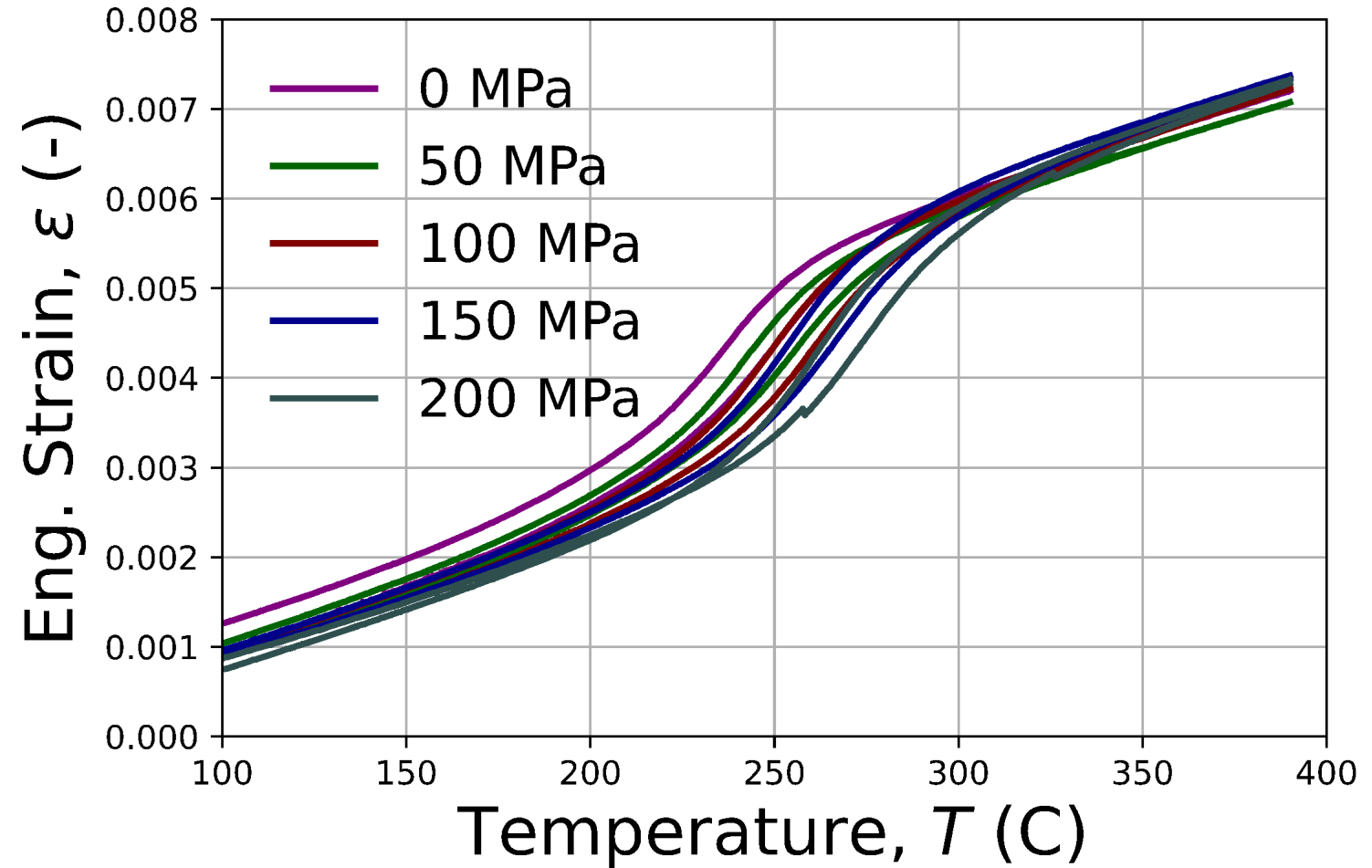
Experimental Results

- Obtained thermal strain data accounting for thermal issues



$$\frac{\Delta L}{L_0}(T)_{\text{Correction}} = \frac{\Delta L}{L_0}(T)_{\text{Raw Data Std.}} - \frac{\Delta L}{L_0}(T)_{\text{Known Standard}}$$

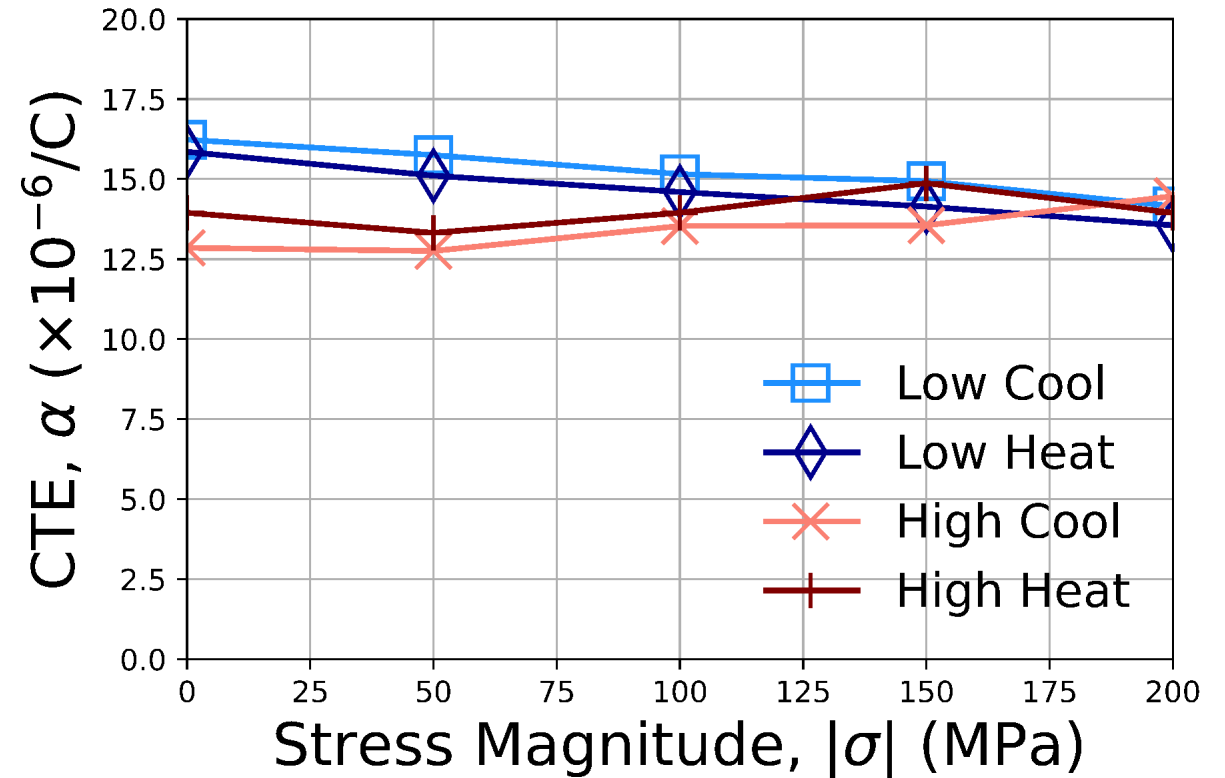
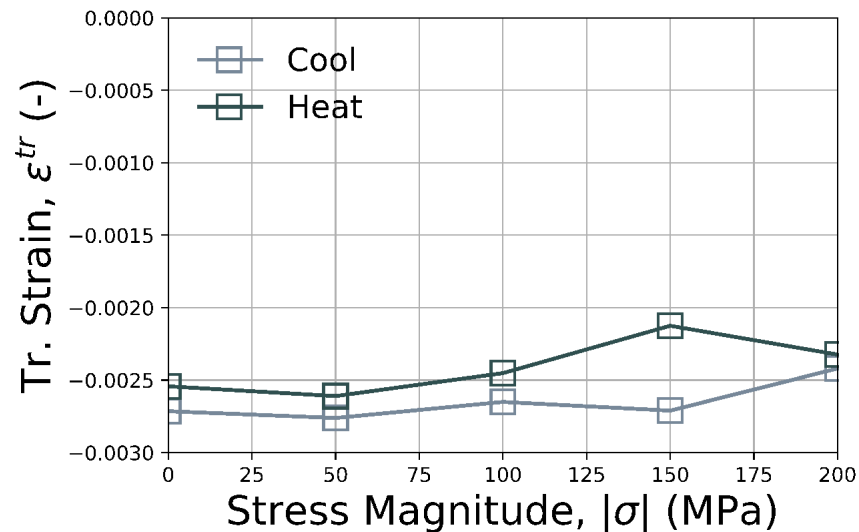
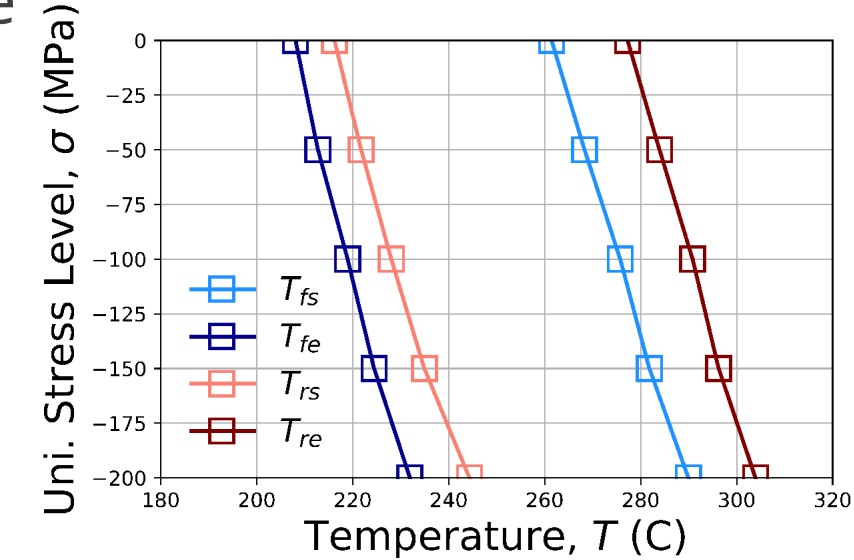
$$\frac{\Delta L}{L_0}(T)_{\text{Corrected Raw Data}} = \frac{\Delta L}{L_0}(T)_{\text{Raw Data}} - \frac{\Delta L}{L_0}(T)_{\text{Correction}}$$





Experimental Observations

- Able to obtain stress and thermomechanical dependencies of GCs for first time





Glass-Ceramic Model

- Seek macroscale representation of glass-ceramics via use of internal state variable/continuum thermodynamics theory
 - Thermoviscoelastic theory for response of glass
 - Utilize shape memory alloy (SMA) theory as basis (Lagoudas model) for phase transformations

$$G(\sigma_{ij}, T, t, \xi, \epsilon_{ij}^t; \delta^i) = G^{\text{te}}(\sigma_{ij}, T, \xi; \delta^i) + G^{\text{in}}(\sigma_{ij}, T, t, \xi, \epsilon_{ij}^t; \delta^i)$$

σ_{ij}, T, t

External State Variables

ξ, ϵ_{ij}^t

Internal State Variables

δ^i

Constituent Volume

Fractions

$$G^{\text{te}}(\sigma_{ij}, T, \xi; \delta^i) = \sum_{r=Q,LO,LM,A} \delta^r G^r(\sigma_{ij}, T) + \delta^C G^C(\sigma_{ij}, T, \xi)$$

$$G^{\text{in}}(\sigma_{ij}, T, t, \xi, \epsilon_{ij}^t) = G^{\text{in-t}}(\sigma_{ij}, \xi, \epsilon_{ij}^t) + G^{\text{neq}}(\sigma_{ij}, T, t)$$



Constitutive Behaviour

- Coleman-Noll and 2nd Law arguments produce:

- All constituents/phases assumed isotropic

$$\begin{aligned} \varepsilon_{ij} = & \frac{1}{2\bar{\mu}} \sigma'_{ij} + \frac{1}{9\bar{K}} \sigma_{kk} \delta_{ij} + g_\varepsilon \varepsilon_{ij}^t + \bar{\alpha} (T - T_0) \delta_{ij} - \\ & - g_v \frac{\Delta\mu}{2\mu^{\text{eq}} \mu^g} H_{ij}^2 - g_v \frac{\Delta K}{9K^{\text{eq}} K^g} H^1 \delta_{ij} + g_v \Delta\alpha H^3 \delta_{ij} \end{aligned}$$

- Transformation functions

- Utilize $J_2 - I_1$ model
- Combines parts of Qidwai & Lagoudas (IJP, 2000) and Lagoudas *et al.* (IJP, 2012)

$$f(X_{ij}, p) = [\phi(X_{ij}) - p]^2 - p_0^2$$

$$\phi(X_{ij}) = \gamma_1 (J_2) \sqrt{3J_2} - \gamma_2 I_1$$



Viscoelasticity

- Hereditary integral based formulation
 - Creep – not relaxation – spectra needed for use of Gibbs free energy
 - Shift-factor relates “material” and “laboratory” time

$$t^* = \int_0^t \frac{ds}{a(s)}$$

- Investigate impact of two shift factors
 - WLF – equilibrated shift factor

$$\log_{10} a = \frac{-C_1 (T - T_{\text{ref}})}{C_2 + (T - T_{\text{ref}})},$$

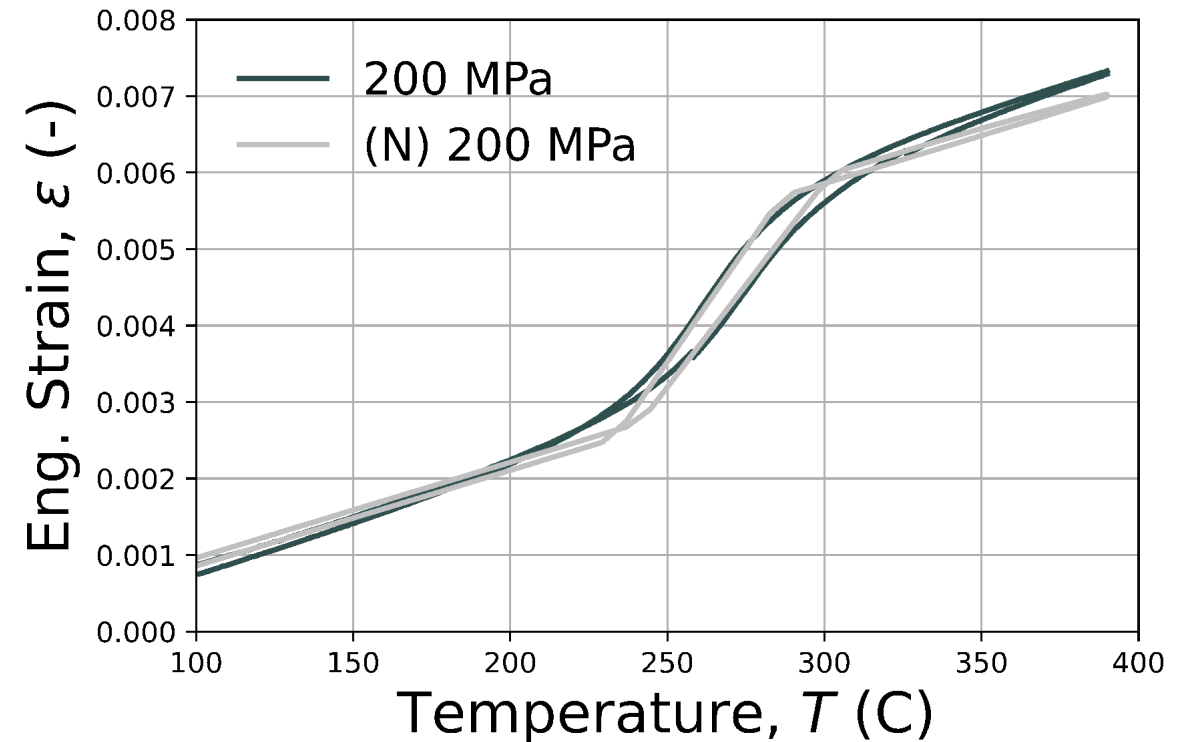
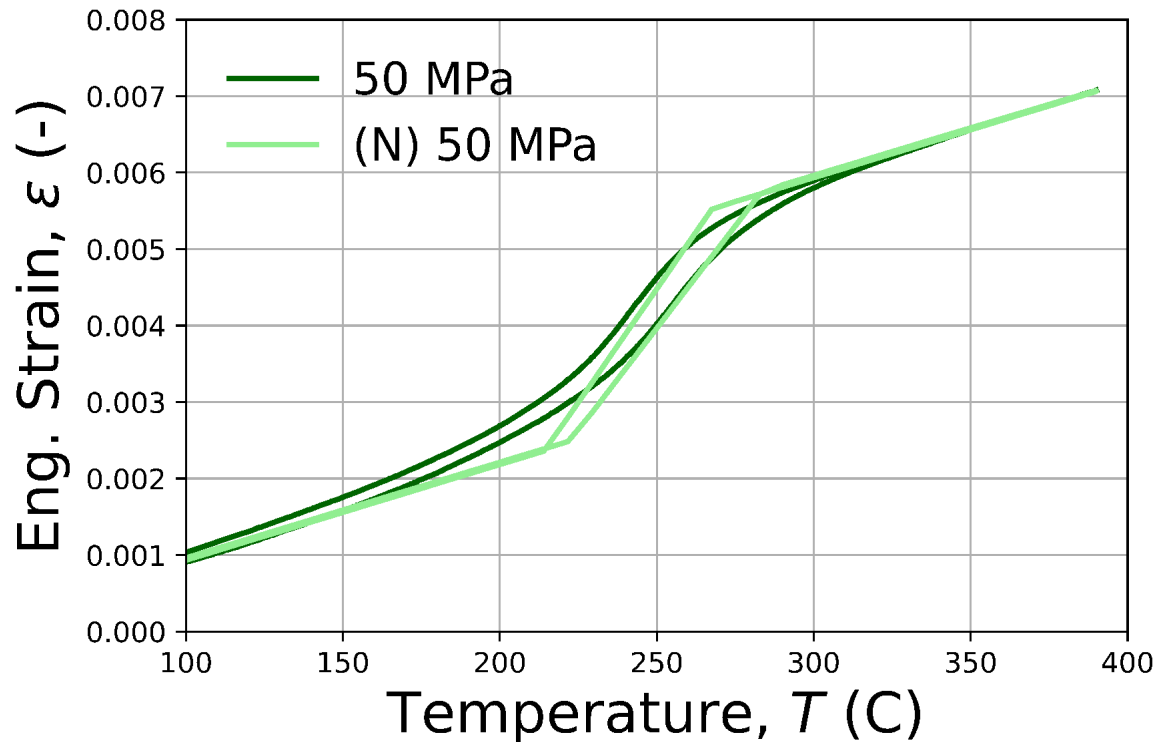
- WLF-Lag
 - Incorporate some history dependence
 - Sealing problem exhibits large temperature ranges of interest ($RT \ll T_g$)

$$\log_{10} a^{\text{WLF-Lag}} = \frac{-C_1 \left(T - T_{\text{ref}} - \int_0^t (1 - j_v(t^* - s^*, 0)) \frac{\partial T}{\partial s} ds \right)}{C_2 + \left(T - T_{\text{ref}} - \int_0^t (1 - j_v(t^* - s^*, 0)) \frac{\partial T}{\partial s} ds \right)}$$



Calibration and Exp. Simulation

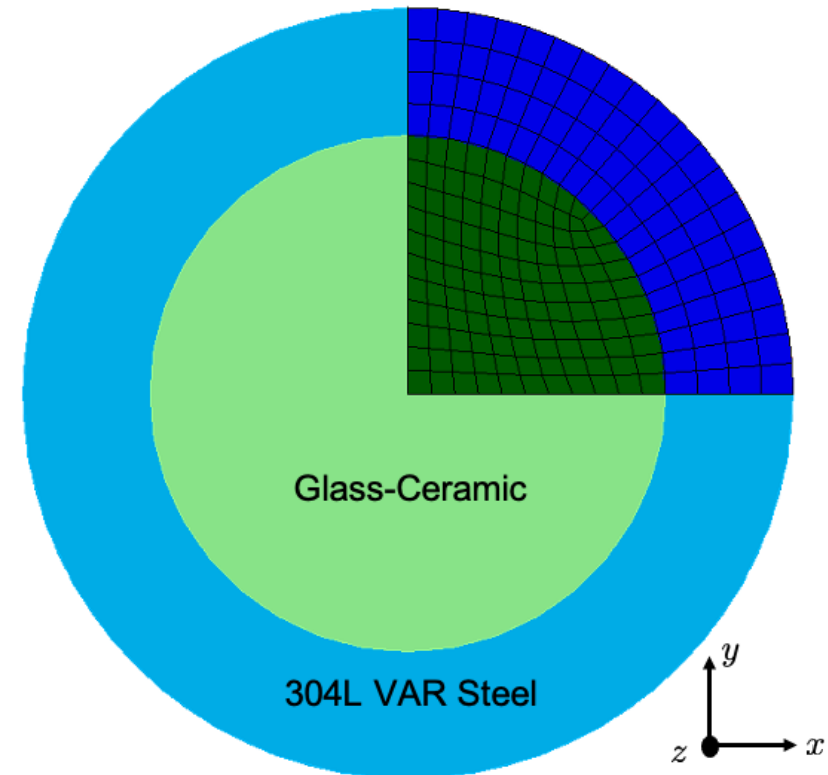
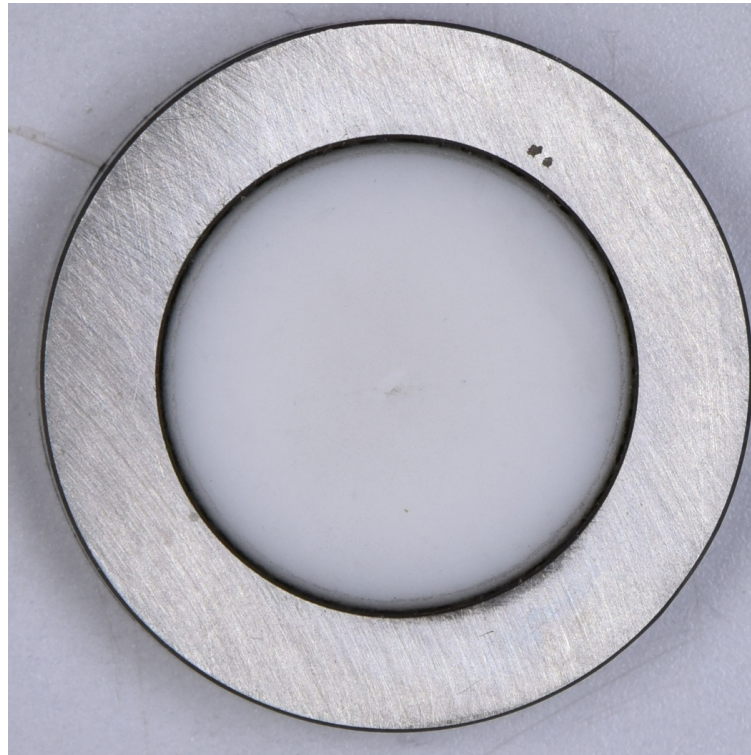
- Fit transformation terms to new actuation data
- Viscoelastic data from prior study
- Good agreement between experimental and simulation results observed





Example Problem – Simple Seal

- Simple seal used as representative example problem
 - Common test for prediction and measurement of residual stress
 - GC Seal enclosed in concentric metal (stainless steel) shell
 - Cooled from above T_g to RT

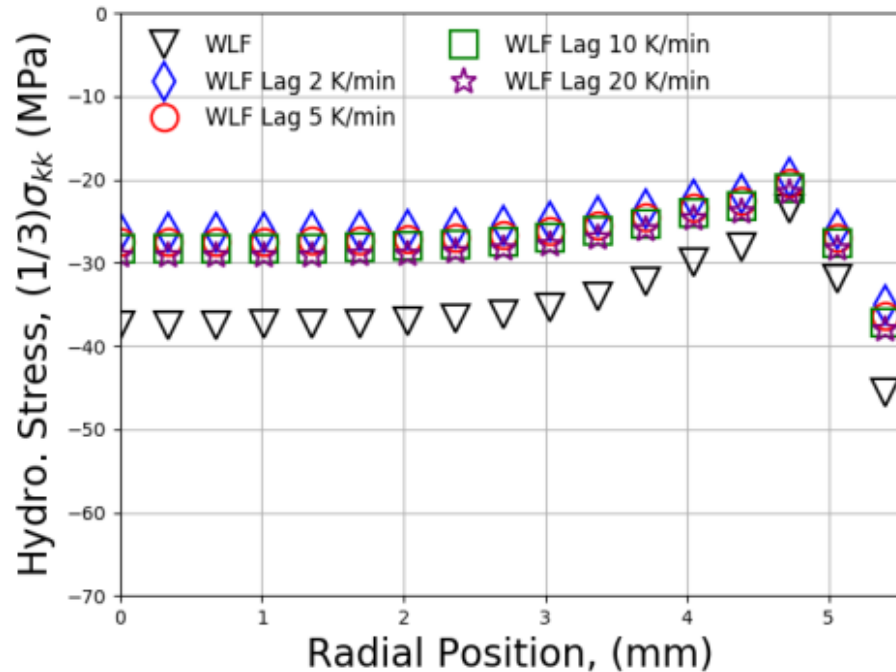




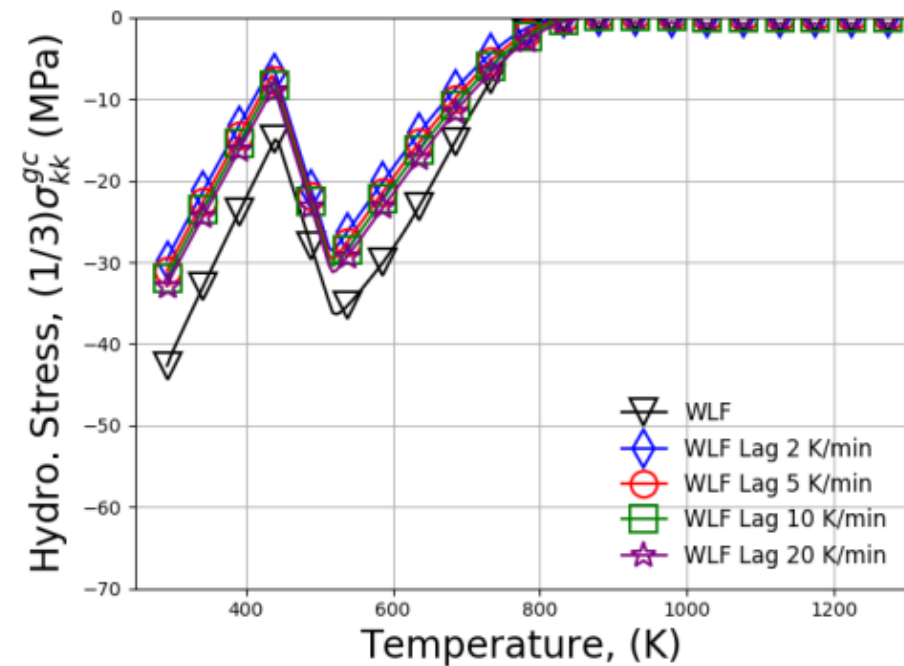
Impact of Heating Rate

- Investigate simple seal with multiple shift factor
 - WLF-Lag at different cooling rates
 - WLF cooled at 2 K/min
 - Purely volumetric flow rule $\gamma_1^0 = 0, \gamma_2^0 = \bar{\gamma}$

Hydrostatic stress along top seal surface



Volume averaged hydrostatic stress through cooling



- Impact of both viscoelastic and transformation mechanisms may be observed



Summary and Conclusions

- Actuation behavior of glass-ceramics explored for first time
 - Novel thermomechanical test chamber
 - New coupled constitutive model
- Have first measurements of stress dependence on different behaviors
 - Preparing second set of experiments to elucidate additional phenomenology
 - Used for updating model form
- Thermomechanical model demonstrated on representative problem
 - Examines coupling between different mechanisms
 - Essential tool for examining performance of engineered product



Acknowledgements

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The word "APPENDIX" is centered in white, uppercase letters within a dark blue diamond. This diamond is surrounded by a white border and is flanked by two diagonal lines that cross at the center. Each line is composed of several colored segments: cyan, purple, orange, green, and dark blue. The background is white with faint, light blue geometric patterns.

APPENDIX



Numerical Implementation

- 3D numerical implementation formulated and implemented
 - Sierra/SolidMechanics FE code constitutive library (LAMÉ)
 - Fully implicit integration, line-search augmented Newton-Raphson

Non-Linear Solve

$$\sigma_{ij}^{n+1} = \sigma_{ij}^n + \Delta t \dot{\sigma}_{ij}^{n+1}$$

$$\varepsilon_{ij}^{t(n+1)} = \varepsilon_{ij}^{t(n)} + \Delta t \dot{\varepsilon}_{ij}^{t(n+1)}$$

$$\xi^{n+1} \rightarrow f(\sigma_{ij}^{n+1}, T^{n+1}, \xi^{n+1}) = 0$$

Direct Solve

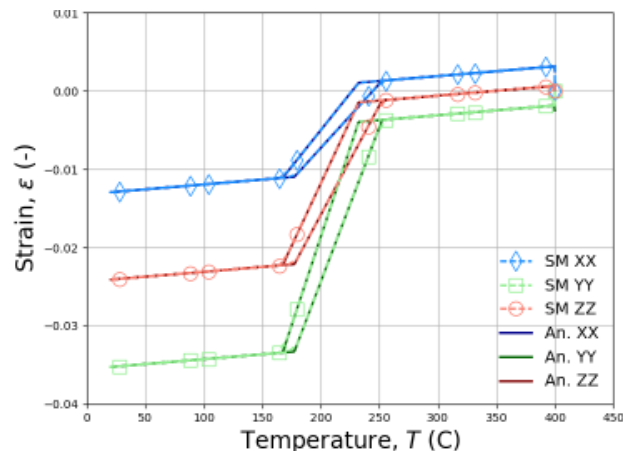
$$H_{n+1}^1 = H_n^1 + \Delta t \dot{H}_{n+1}^1$$

$$H_{ij}^{2(n+1)} = H_{ij}^{2(n)} + \Delta t \dot{H}_{ij}^{2(n+1)}$$

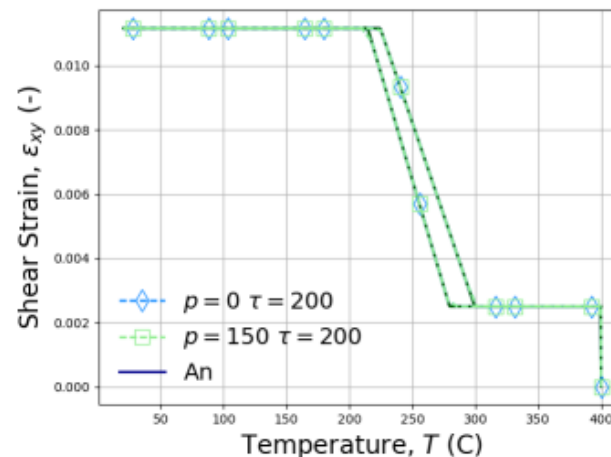
$$H_{n+1}^3 = H_n^3 + \Delta t \dot{H}_{n+1}^3$$

Example Verification Tests

Balanced Biaxial Thermal Sweep



Pure Shear w/ Pressure



Balanced Biaxial Creep

