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# Experimentally Informed Model Development of Glass- Ceramic Materials

32<sup>nd</sup> Rio Grande Symposium on Advanced  
Materials, Albuquerque, NM, October 24, 2022

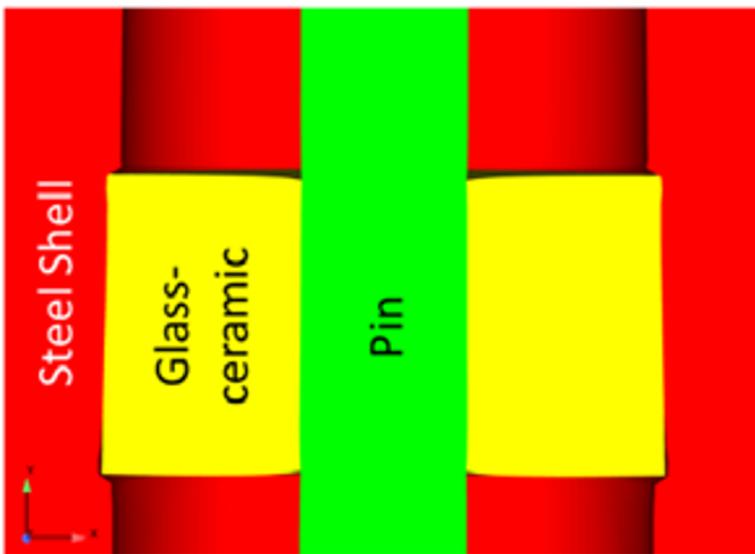
**B. T. Lester, K. Strong, T. Diebold, J. Laing, S.  
Dai, and K. Long**

Sandia National Laboratories

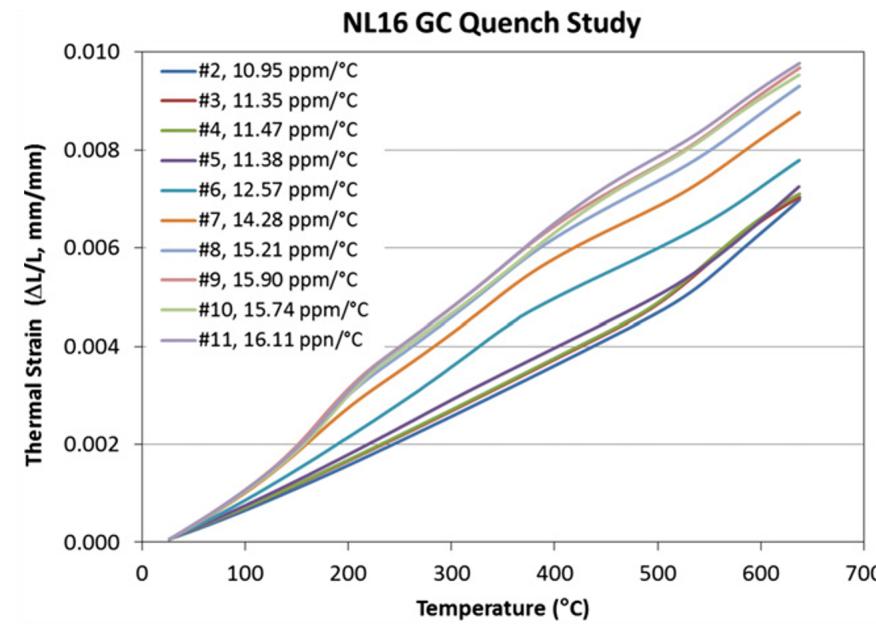
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# Glass-ceramic to Metal Seals (GcTMS)

- Variety of industrial applications for glass-ceramics
  - Hermetic glass-ceramic to metal seals (GcTMS)
  - Subject to complex thermomechanical histories



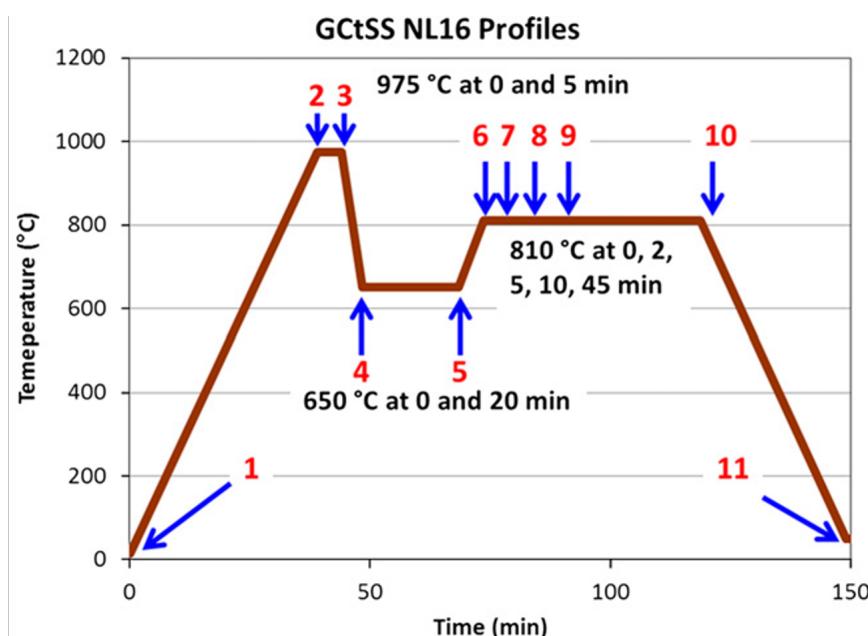
Dai *et al.*, 2017, *J Am Ceram Soc*, 100,  
pp.3652-3661



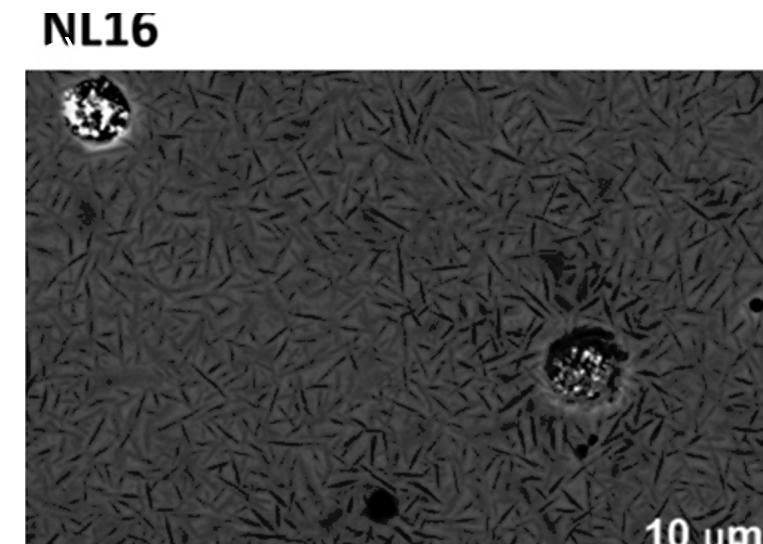
Dai *et al.*, 2016, *J Am Ceram Soc*, 99,  
pp.3719-3725

# Glass-Ceramics - Microstructure

- Glass-ceramics are produced by inducing a ceramic phase(s) in an inorganic base glass
- Advantageous features arise from microstructure
  - Up to 5 constituents
  - Inelasticity from residual glass and silica polymorphs



Dai et al., 2016, *J Am Ceram Soc*, 99 (11),  
pp.3719-3725



Rodriguez et al., 2016, *J Am Ceram Soc*,  
99 (11), pp.3726-3733

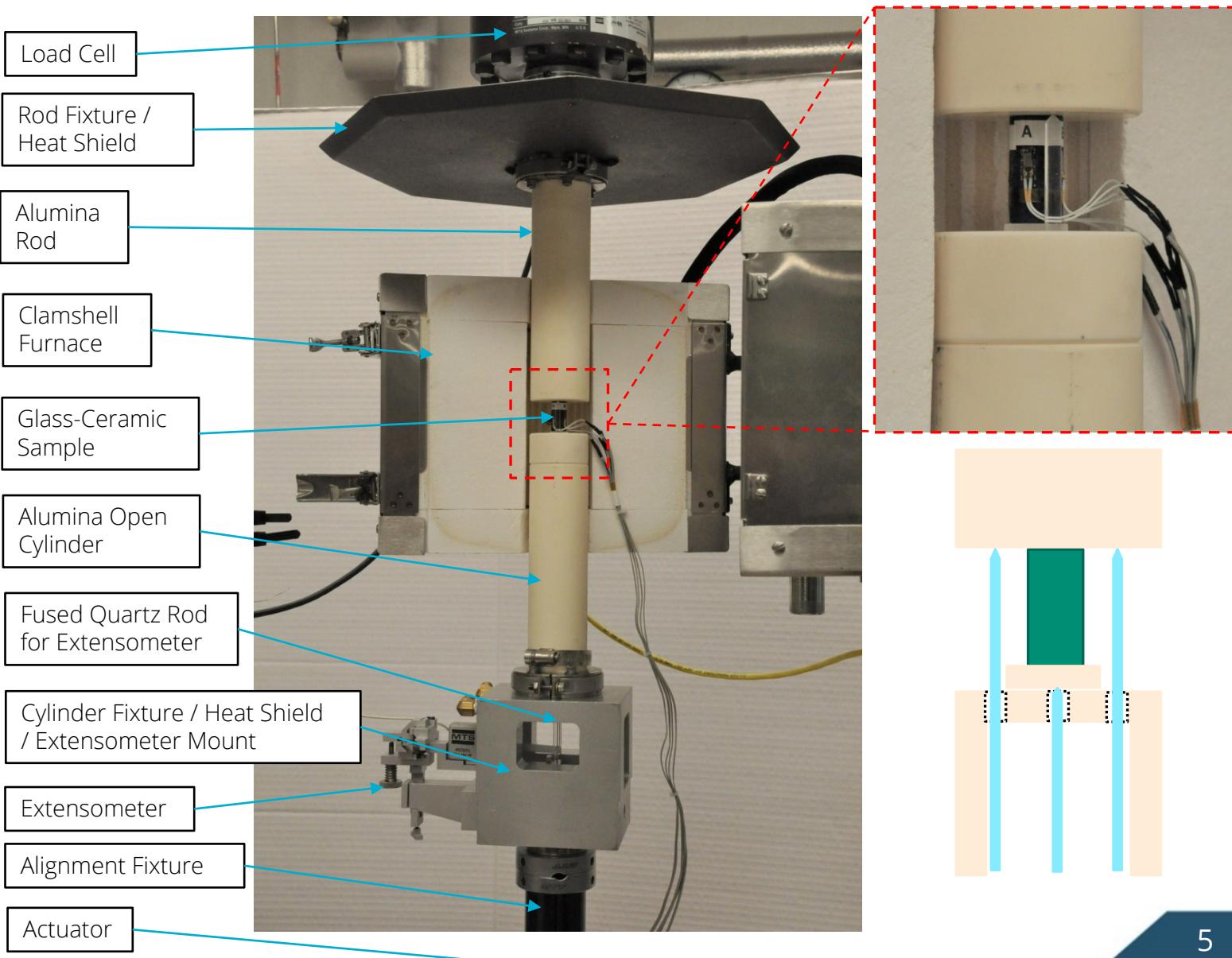


## Objective

- Understanding actuation response essential for intended use
- Actuation not well understood experimentally or modeled
  - Experimental studies focused on other features (e.g. dilatometry, DMA)
  - Models leverage alternative phenomenologies
- Objective: Elucidate and enhance understanding of actuation response
  - Perform first of the kind experiments to characterize thermomechanical response
  - Develop new model capable of describing coupled phase-transformation and viscoelasticity

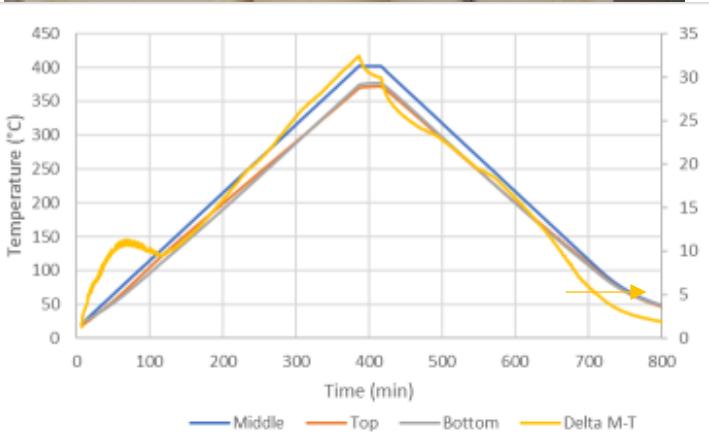
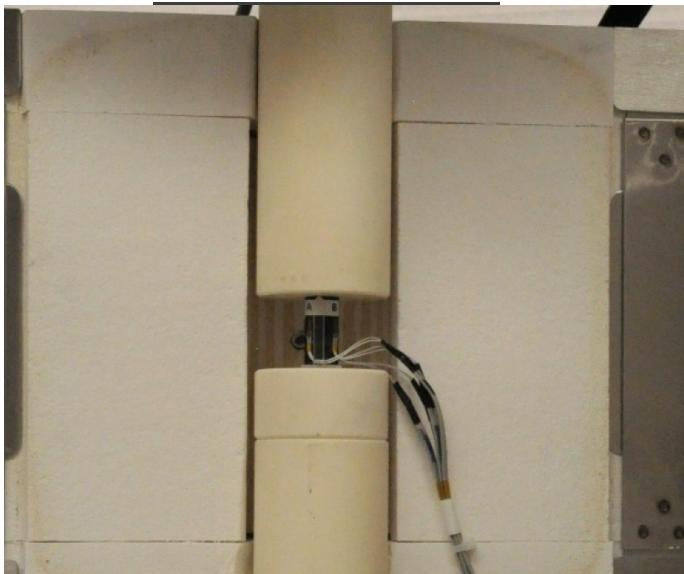
# Experimental Set-up

- Experimental challenges:
  - Thermal homogeneity
  - Precise strain measurement
  - Higher loads
- Developed novel thermomechanical test chamber
  - Novel extensometer and stage design
  - Clamshell furnace

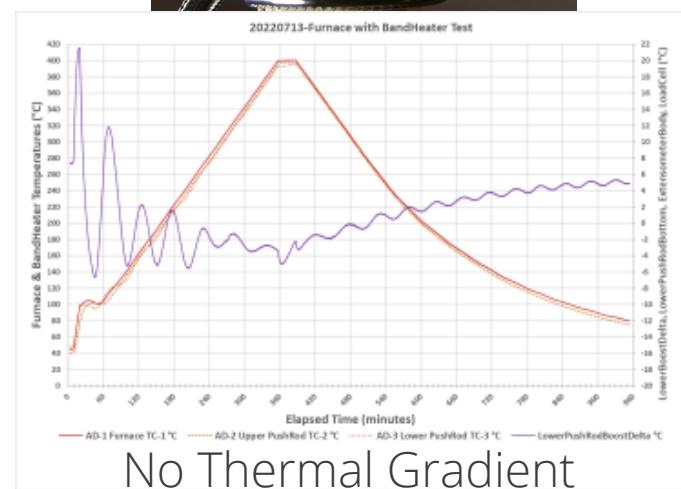


# Experimental Thermal Control

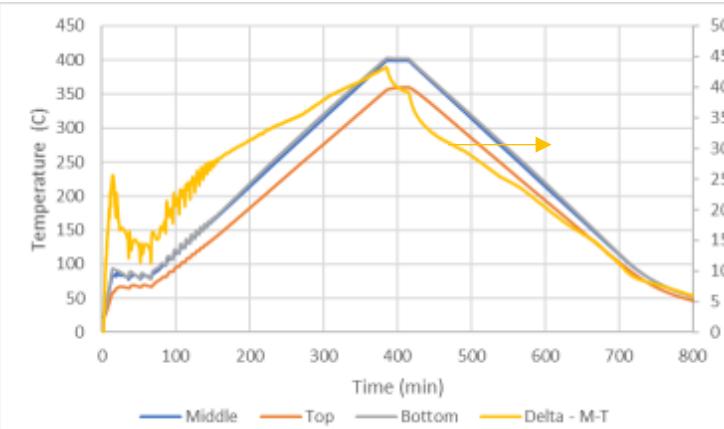
Alumina Top and Bottom  
No Band Heater



Quartz Top Alumina Bottom  
Band Heater



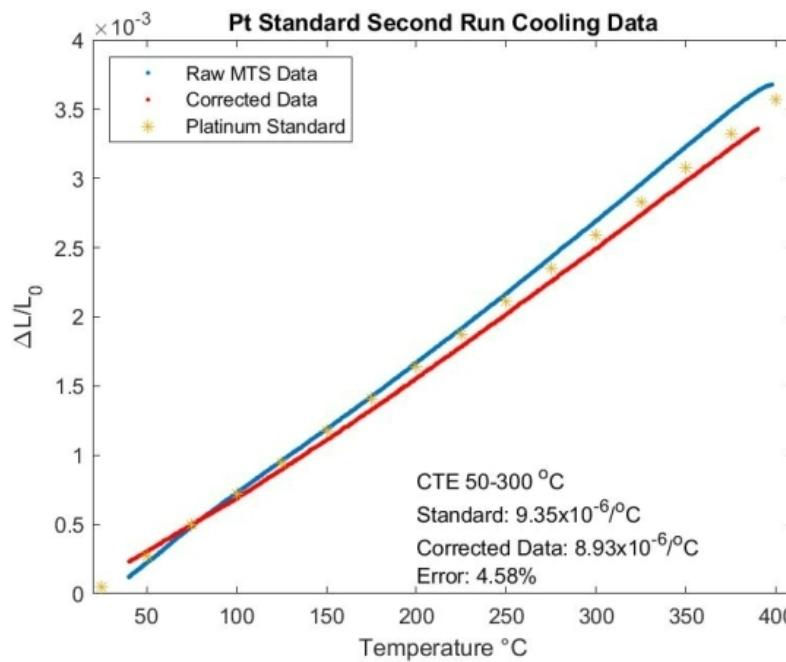
Alumina Top and Bottom  
Band Heater



Minimal Thermal Gradient

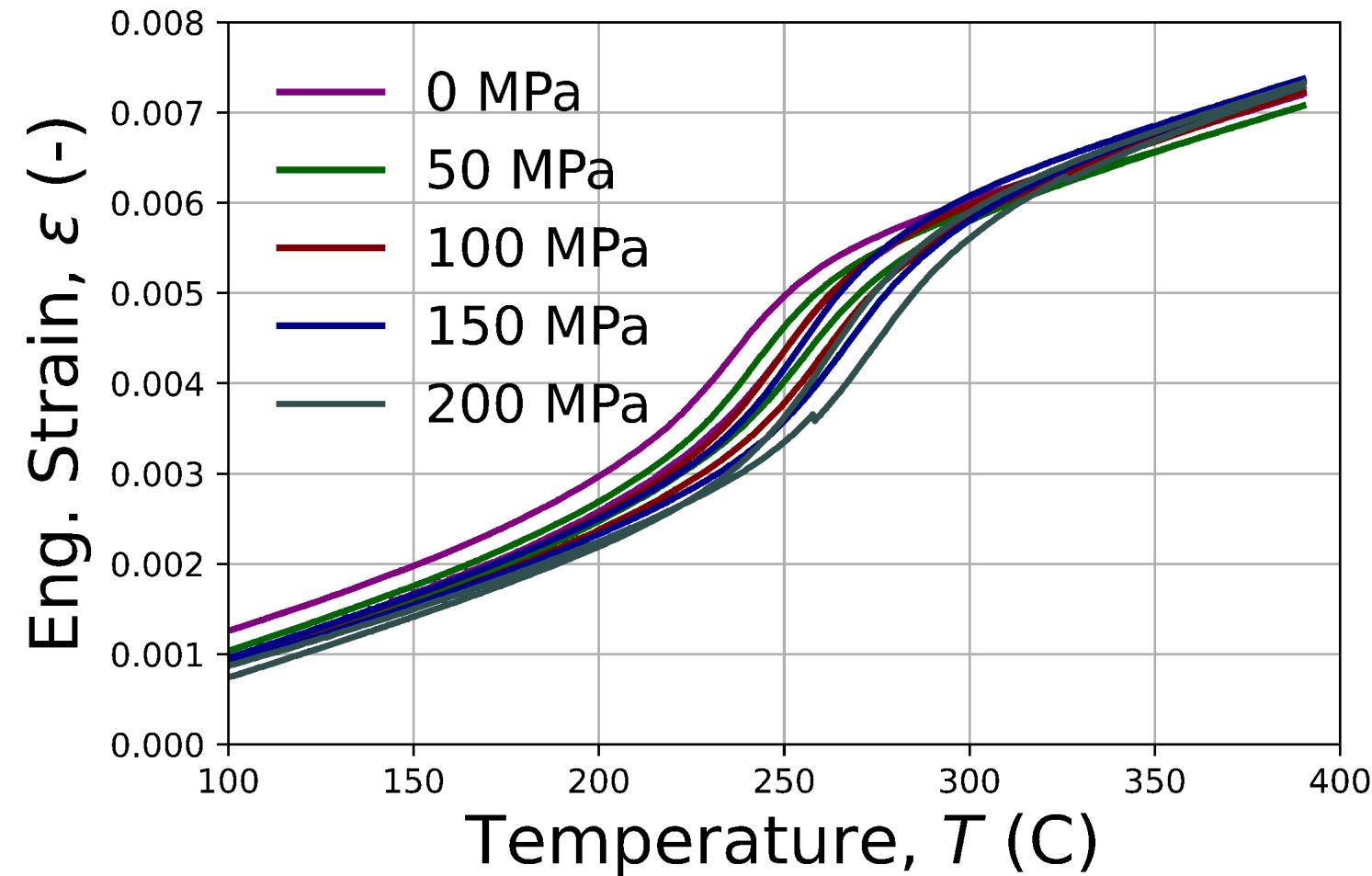
# Experimental Results

- Obtained thermal strain data accounting for thermal issues



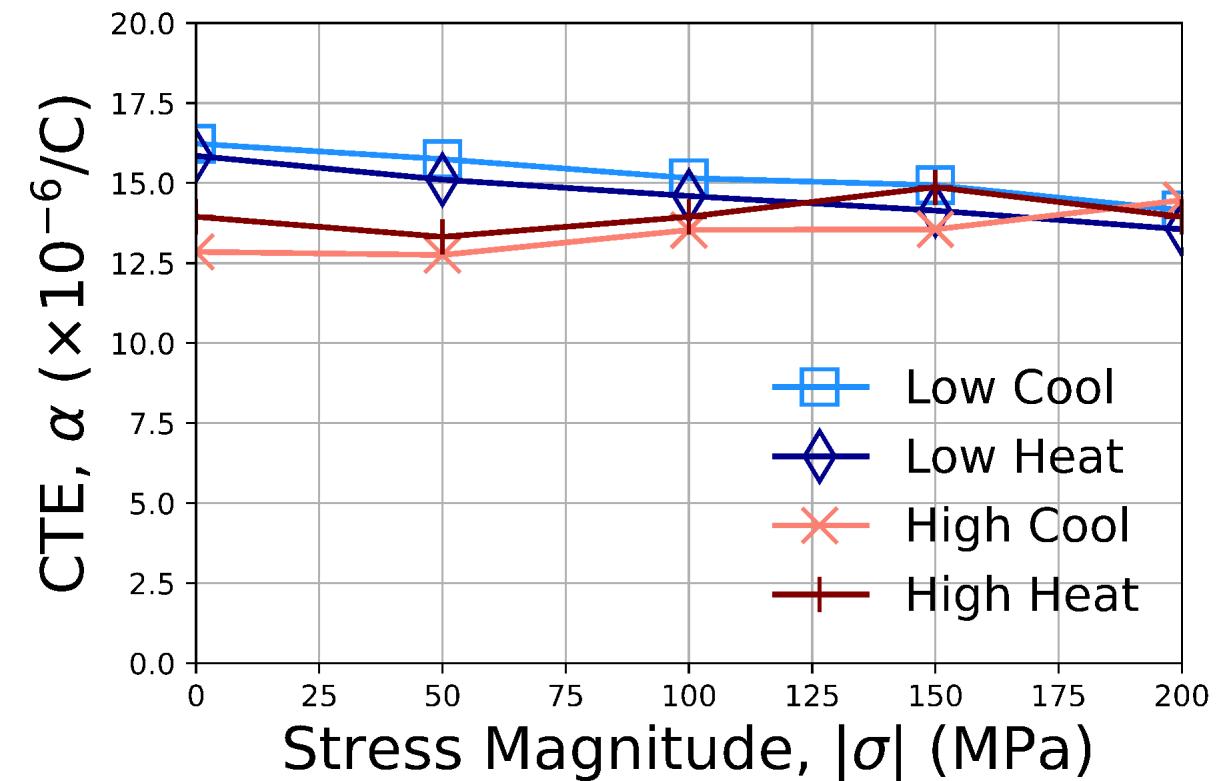
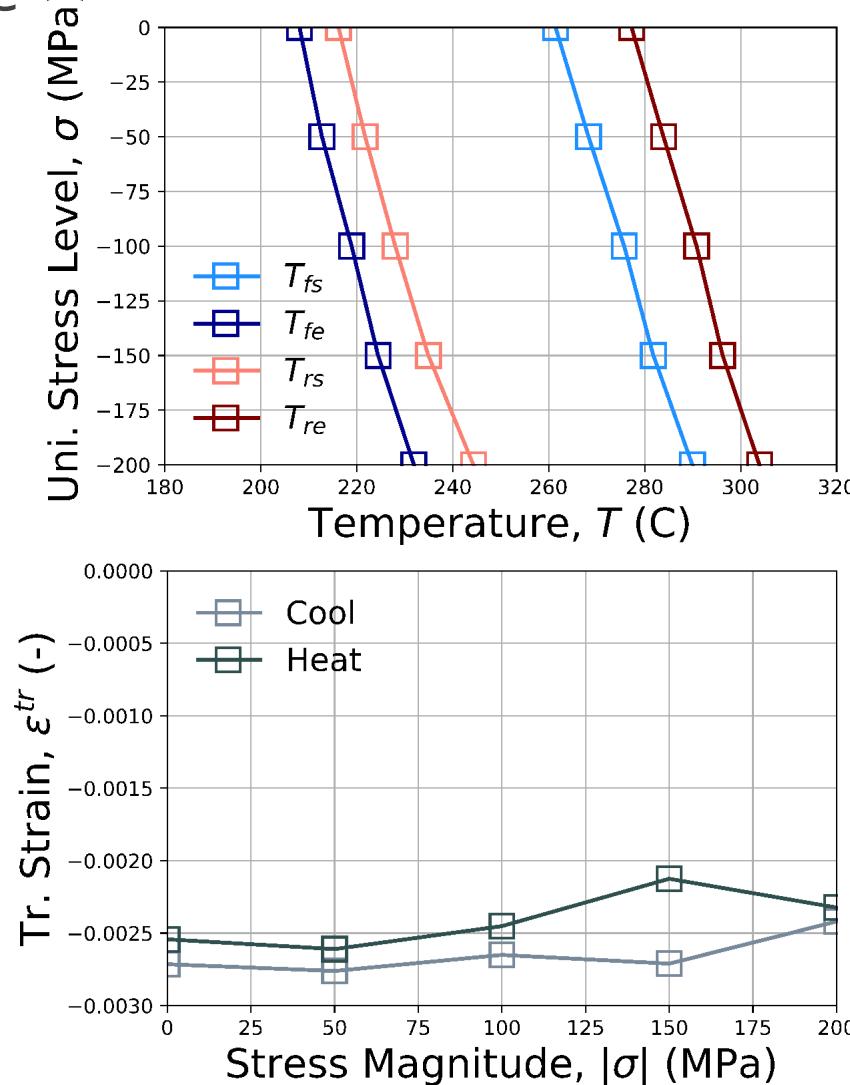
$$\frac{\Delta L}{L_0}(T)_{Correction} = \frac{\Delta L}{L_0}(T)_{Raw\ Data\ Std.} - \frac{\Delta L}{L_0}(T)_{Known\ Standard}$$

$$\frac{\Delta L}{L_0}(T)_{Corrected\ Data} = \frac{\Delta L}{L_0}(T)_{Raw\ Data} - \frac{\Delta L}{L_0}(T)_{Correction}$$



## Experimental Observations

- Able to obtain stress and thermomechanical dependencies of GCs for first time





## Glass-Ceramic Model

- Seek macroscale representation of glass-ceramics via use of internal state variable/continuum thermodynamics theory
  - Thermoviscoelastic theory for response of glass
  - Utilize shape memory alloy (SMA) theory as basis (Lagoudas model) for phase transformations
  - Details in Lester and Long, 2021, Mech Mat., 158, 103849

### Free Energy

$$G(\sigma_{ij}, T, t, \xi, \varepsilon_{ij}^t; \delta^i) = G^{\text{te}}(\sigma_{ij}, T, \xi; \delta^i) + G^{\text{in}}(\sigma_{ij}, T, t, \xi, \varepsilon_{ij}^t; \delta^i)$$

### Total Strain

$$\begin{aligned} \varepsilon_{ij} = & \frac{1}{2\bar{\mu}}\sigma'_{ij} + \frac{1}{9\bar{K}}\sigma_{kk}\delta_{ij} + g_\varepsilon \varepsilon_{ij}^t + \bar{\alpha}(T - T_0)\delta_{ij} - \\ & g_v \frac{\Delta\mu}{2\mu^{\text{eq}}\mu^{\text{g}}} H_{ij}^2 - g_v \frac{\Delta K}{9K^{\text{eq}}K^{\text{g}}} H^1 \delta_{ij} + g_v \Delta\alpha H^3 \delta_{ij} \end{aligned}$$

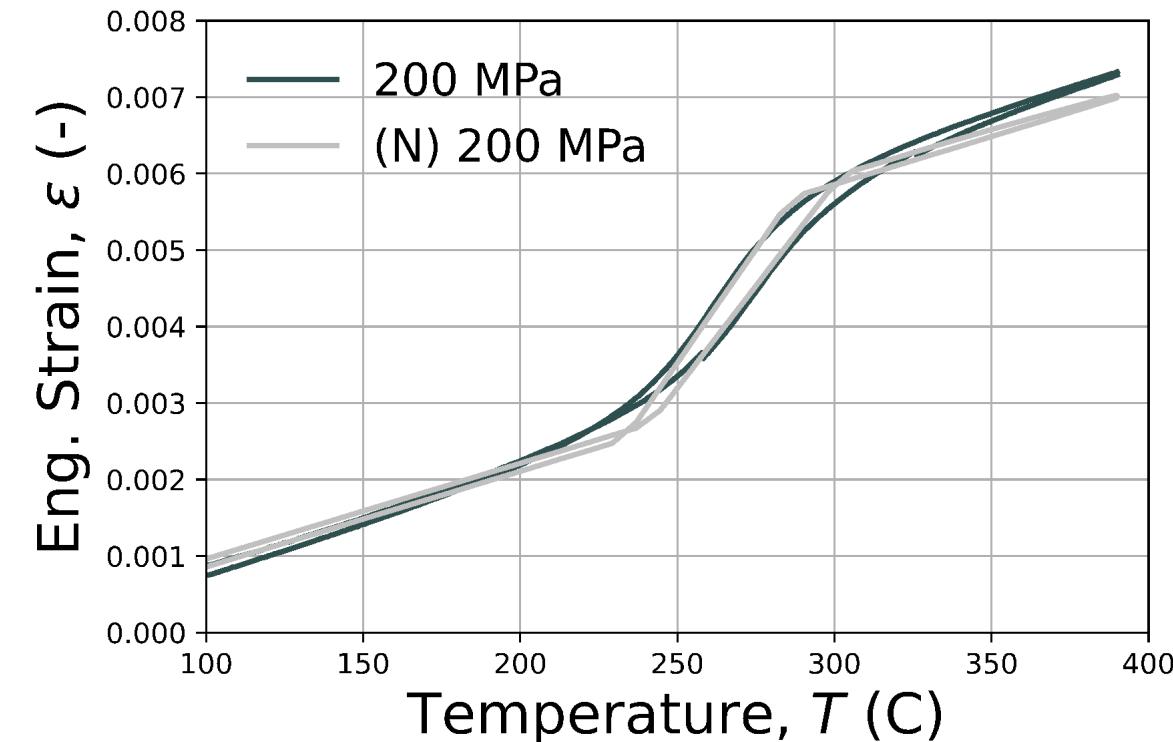
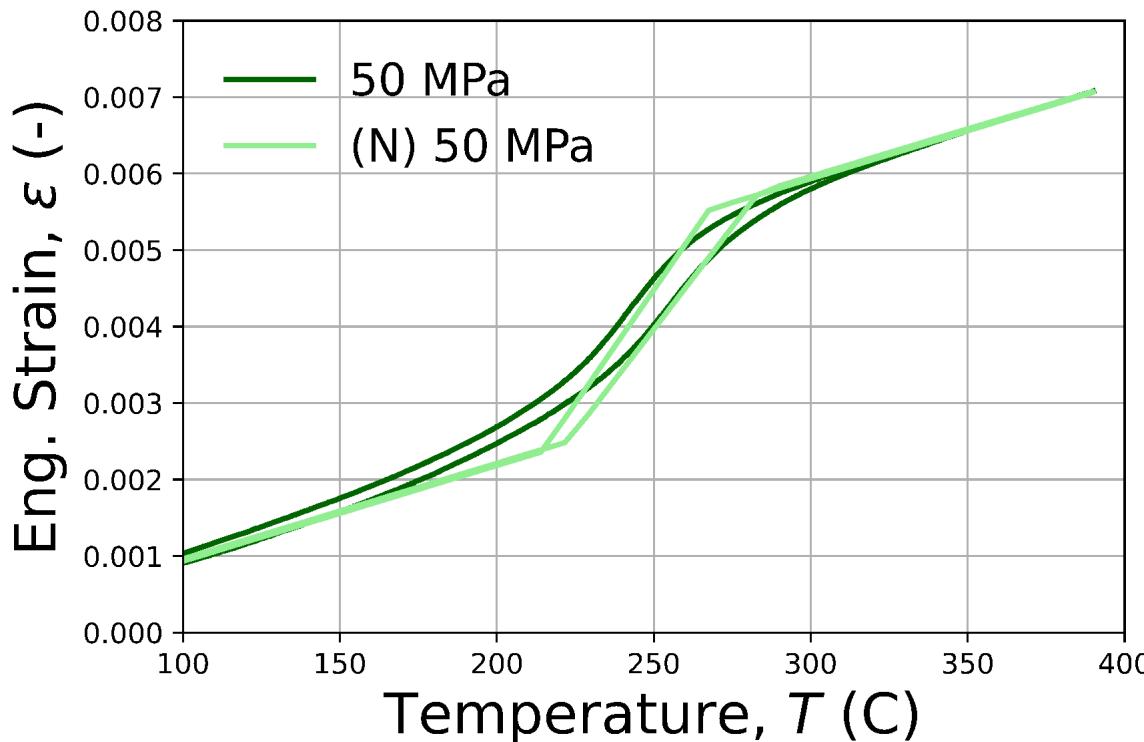
### Shift Factor

$$\log_{10} a = \frac{-C_1(T - T_{\text{ref}})}{C_2 + (T - T_{\text{ref}})},$$

$$\log_{10} a^{\text{WLF-Lag}} = \frac{-C_1 \left( T - T_{\text{ref}} - \int_0^t (1 - j_v(t^* - s^*, 0)) \frac{\partial T}{\partial s} ds \right)}{C_2 + \left( T - T_{\text{ref}} - \int_0^t (1 - j_v(t^* - s^*, 0)) \frac{\partial T}{\partial s} ds \right)}$$

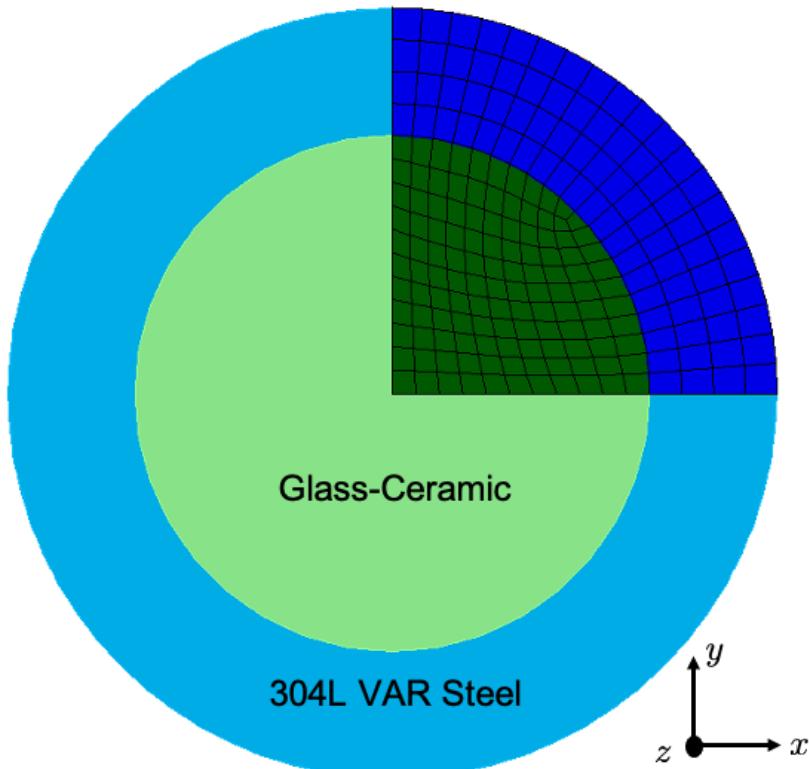
# Calibration and Exp. Simulation

- Fit transformation terms to new actuation data
- Viscoelastic data from prior study
- Good agreement between experimental and simulation results observed

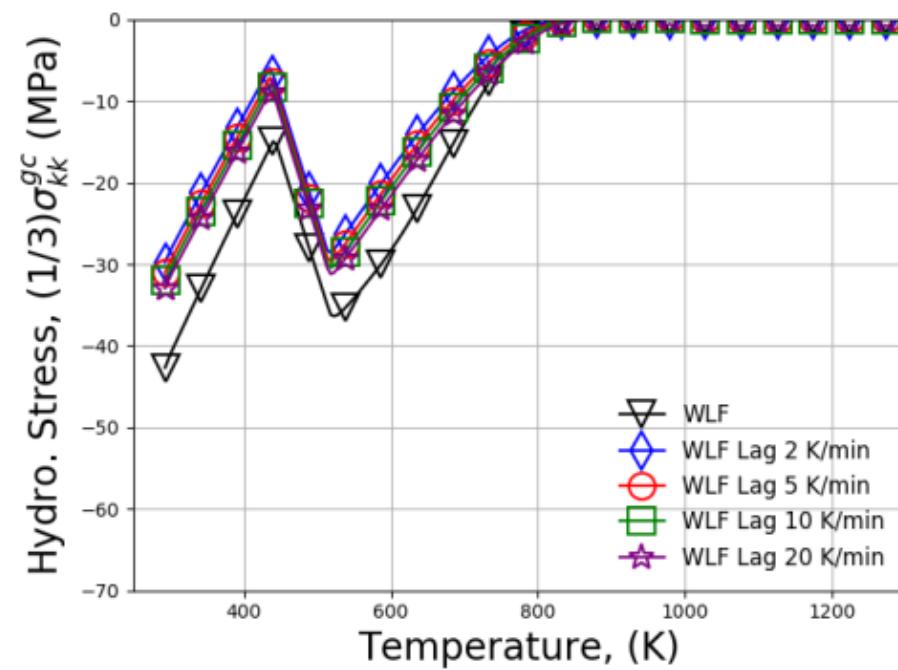


## Example Problem – Simple Seal

- Simple seal used as representative example problem
  - Common test for prediction and measurement of residual stress
  - GC Seal enclosed in concentric metal (stainless steel) shell
  - Cooled from above  $T_g$  to RT



Volume averaged hydrostatic stress through cooling





## Summary and Conclusions

- Actuation behavior of glass-ceramics explored for first time
  - Novel thermomechanical test chamber
  - New coupled constitutive model
- Have first measurements of stress dependence on different behaviors
  - Preparing second set of experiments to elucidate additional phenomenology
  - Used for updating model form
- Thermomechanical model demonstrated on representative problem
  - Examines coupling between different mechanisms
  - Essential tool for examining performance of engineered product



## Acknowledgements

- Sandia National Laboratories is a multimission laboratory managed and operated by National Technology and Engineering Solutions of Sandia, LLC, a wholly owned subsidiary of Honeywell International, Inc., for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-NA0003525. This paper describes objective technical results and analysis. Any subjective views or opinions that might be expressed in the paper do not necessarily represent the views of the U.S. Department of Energy or the United States Government



# APPENDIX

# Numerical Implementation

- 3D numerical implementation formulated and implemented
  - Sierra/SolidMechanics FE code constitutive library (LAMÉ)
  - Fully implicit integration, line-search augmented Newton-Raphson

*Non-Linear Solve*

$$\sigma_{ij}^{n+1} = \sigma_{ij}^n + \Delta t \dot{\sigma}_{ij}^{n+1}$$

$$\varepsilon_{ij}^{t(n+1)} = \varepsilon_{ij}^{t(n)} + \Delta t \dot{\varepsilon}_{ij}^{t(n+1)}$$

$$\xi^{n+1} \rightarrow f(\sigma_{ij}^{n+1}, T^{n+1}, \xi^{n+1}) = 0$$

*Direct Solve*

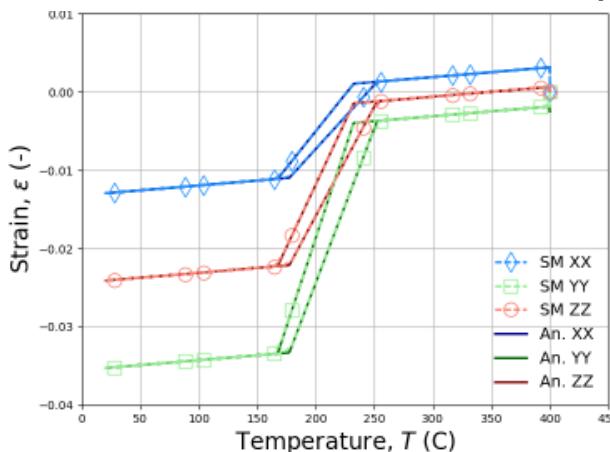
$$H_{n+1}^1 = H_n^1 + \Delta t \dot{H}_{n+1}^1$$

$$H_{ij}^{2(n+1)} = H_{ij}^{2(n)} + \Delta t \dot{H}_{ij}^{2(n+1)}$$

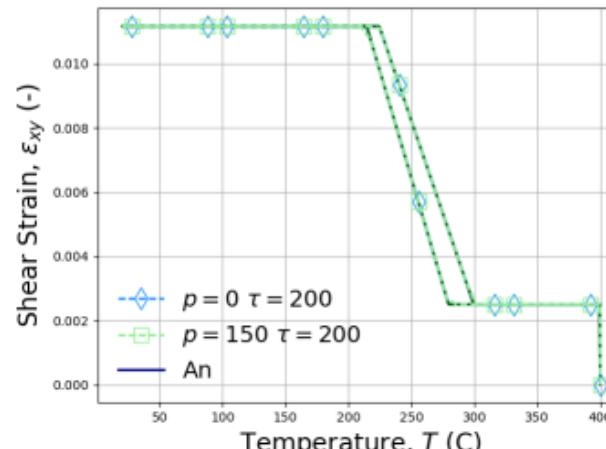
$$H_{n+1}^3 = H_n^3 + \Delta t \dot{H}_{n+1}^3$$

## Example Verification Tests

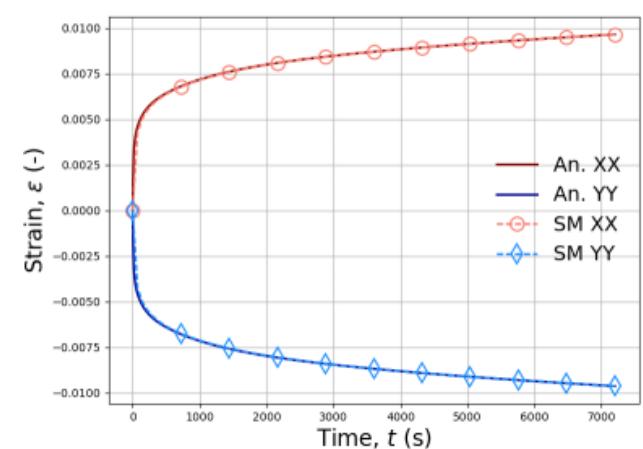
Balanced Biaxial Thermal Sweep



Pure Shear w/ Pressure



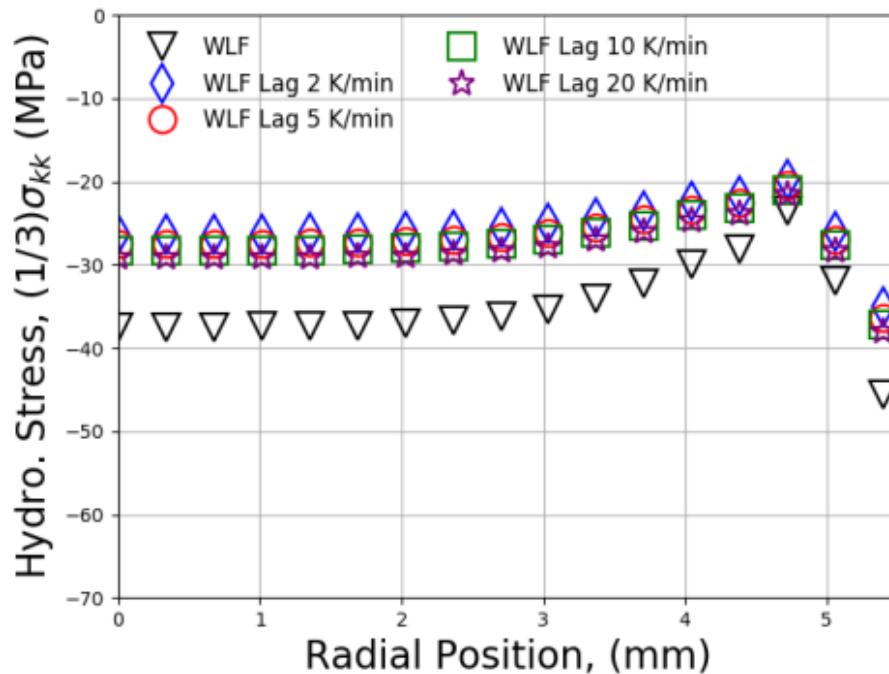
Balanced Biaxial Creep



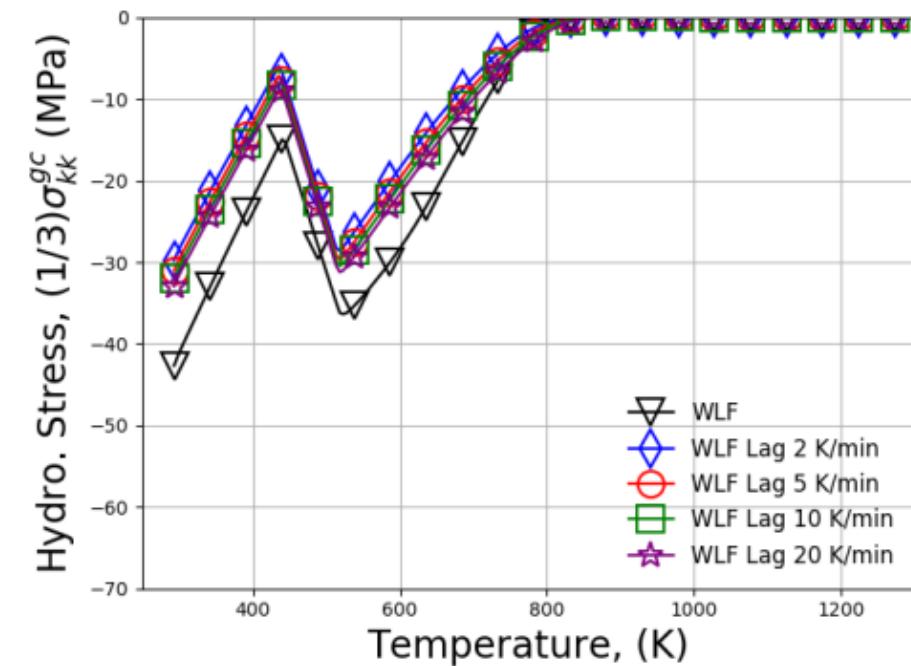
# Impact of Heating Rate

- Investigate simple seal with multiple shift factor
  - WLF-Lag at different cooling rates
  - WLF cooled at 2 K/min
  - Purely volumetric flow rule  $\gamma_1^0 = 0, \gamma_2^0 = \bar{\gamma}$

Hydrostatic stress along top seal surface



Volume averaged hydrostatic stress through cooling



- Impact of both viscoelastic and transformation mechanisms may be observed