

# Measurement of Infrasound Sensor Self-Noise

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**Cleared for release**

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# Infrasound-Sensor Intercomparison Exercise

Goal: Assess laboratory capabilities and equivalence for,

- (1) sensitivity and frequency-response measurement using primary or secondary means and
- (2) **self-noise measurement**

Frequency range: **0.01 to 10 Hz**

Sensor self-noise: The sensor output with input excitation reduced as low as possible; the noise power added to a measurement by the sensor.

Methods for self-noise measurement:

- (1) **Isolate from external excitation**
- (2) **Coherent-signal subtraction**
- (3) ~~Deactivate sense element~~

Importance: Is the noise-floor sufficiently low that the sensor can resolve acoustic events near the low-noise ambient background?

## The Exercise: PTSAVH.A-C1

PTSAVH.A-C1 was coordinated by the Provisional Technical Secretariat of the Comprehensive Nuclear Test-Ban Treaty Organization with LNE as the Pilot Lab, and it included the Participants listed below.

### Sensors:

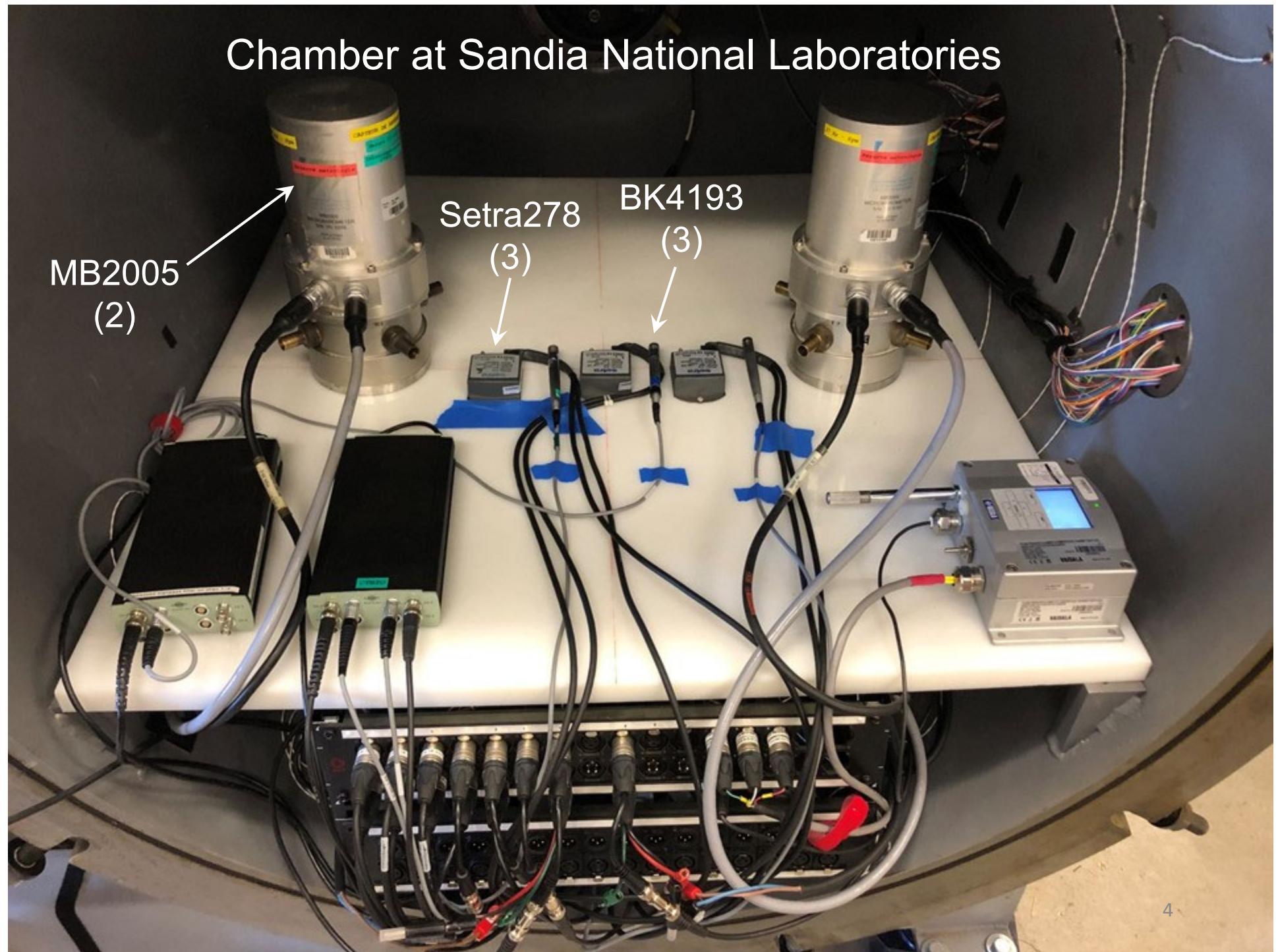
- Two Martec MB2005 microbarometers (MB)
- Two Brüel and Kjær 4193 infrasound microphones (BK)
- Two Setra 278 absolute pressure sensors (Se)

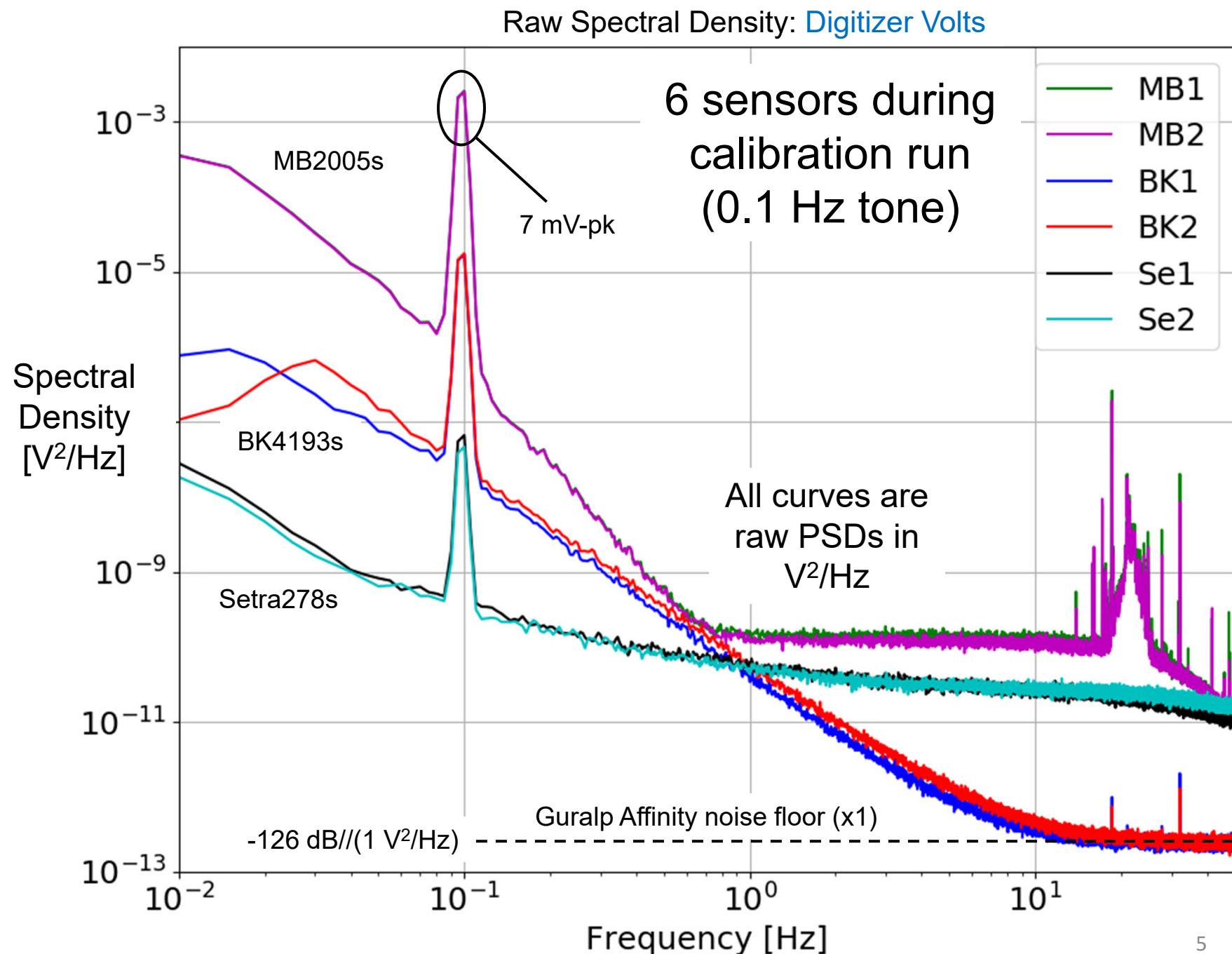
### Participants:

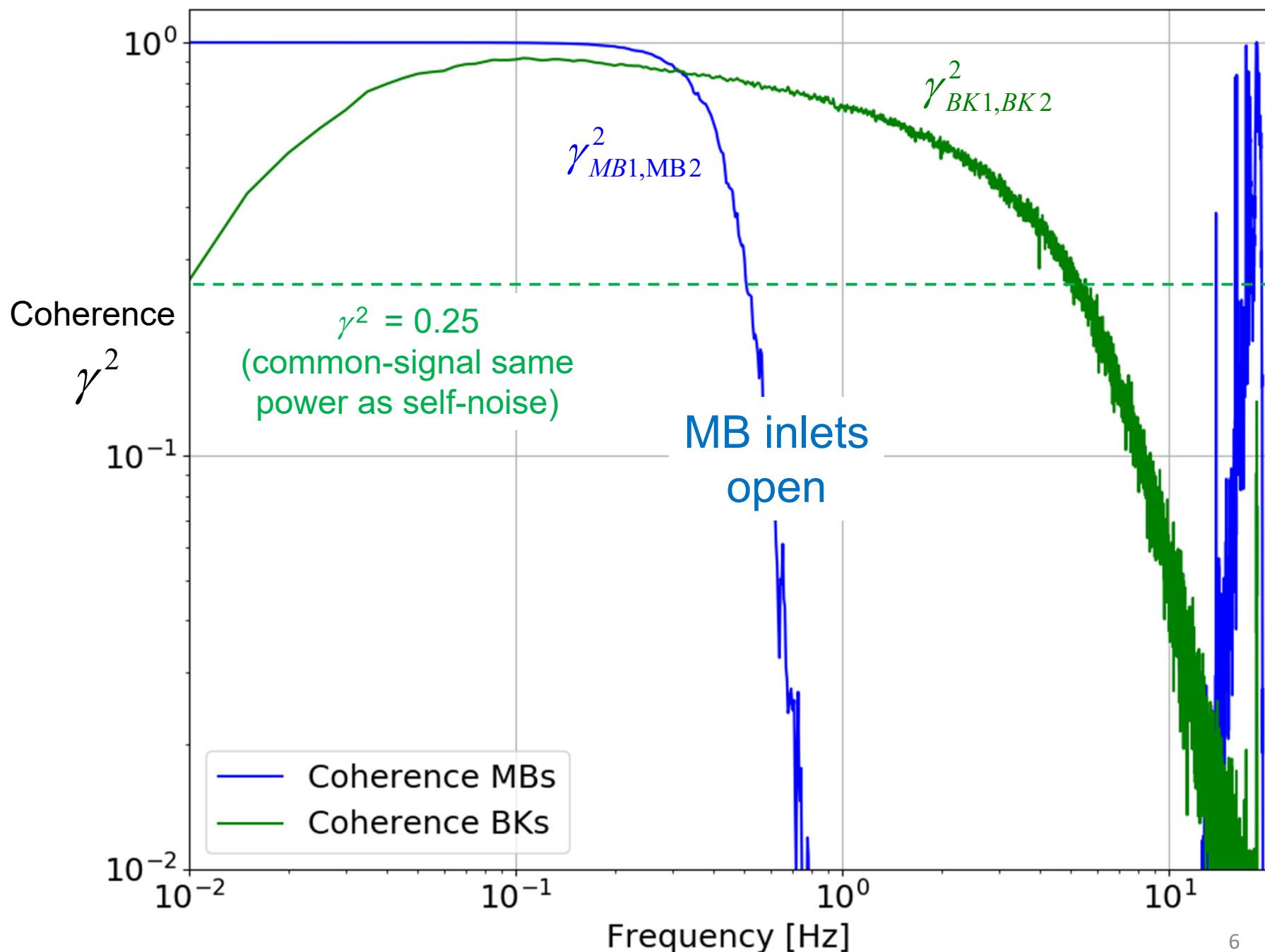
- LNE: Laboratoire National de métrologie et d'Essais
- CEA: Commissariat à l'énergie atomique et aux énergies alternatives
- PTS: Provisional Technical Secretariat
- SNL: Sandia National Laboratories
- NCPA: National Center for Physical Acoustics
- PSU: Penn State University

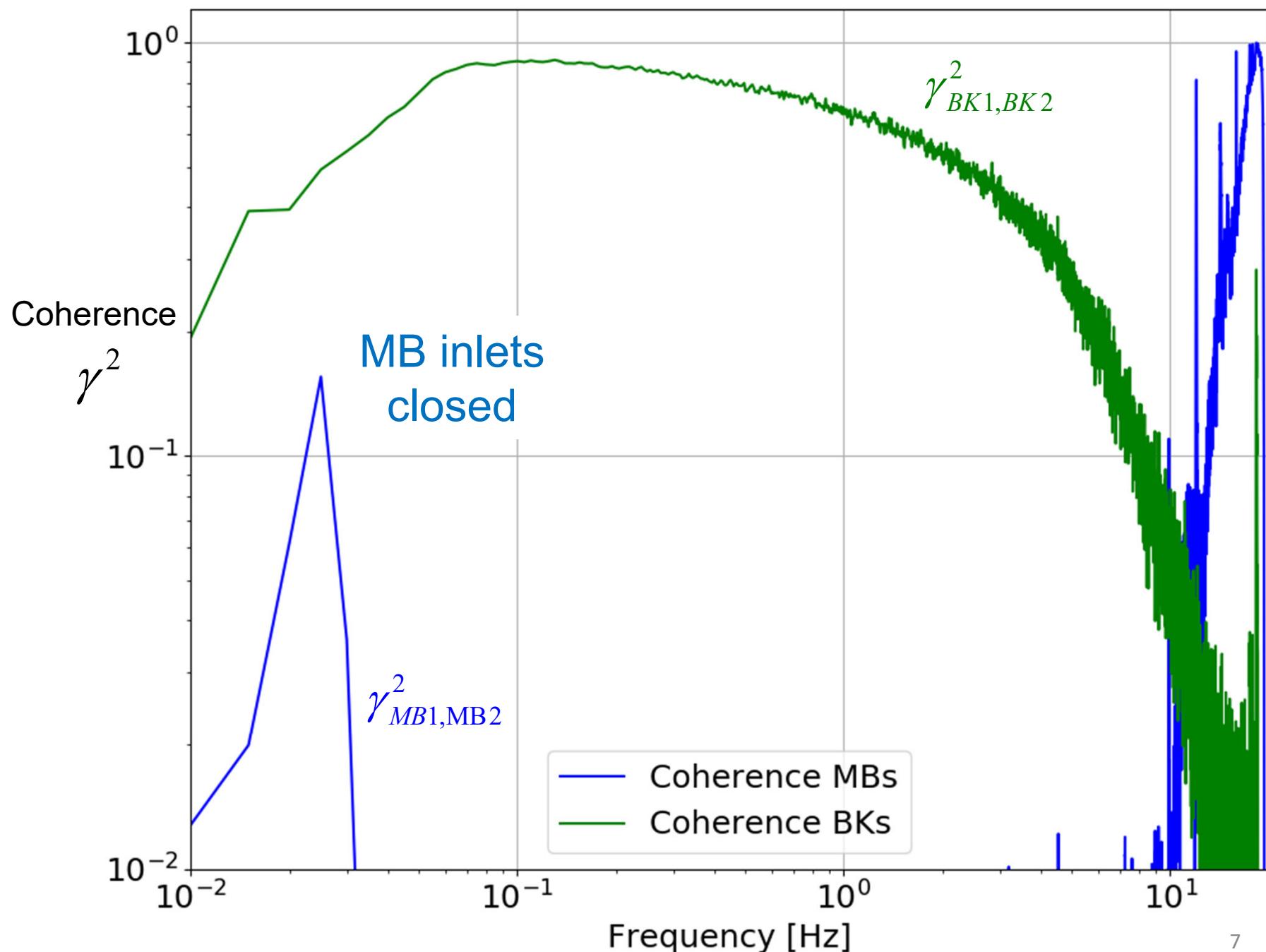
The infrasound sensors circulated from January 2020 to February 2021 in the following sequence: LNE, NCPA, PSU, SNL, CEA, PTS, LNE.

# Chamber at Sandia National Laboratories

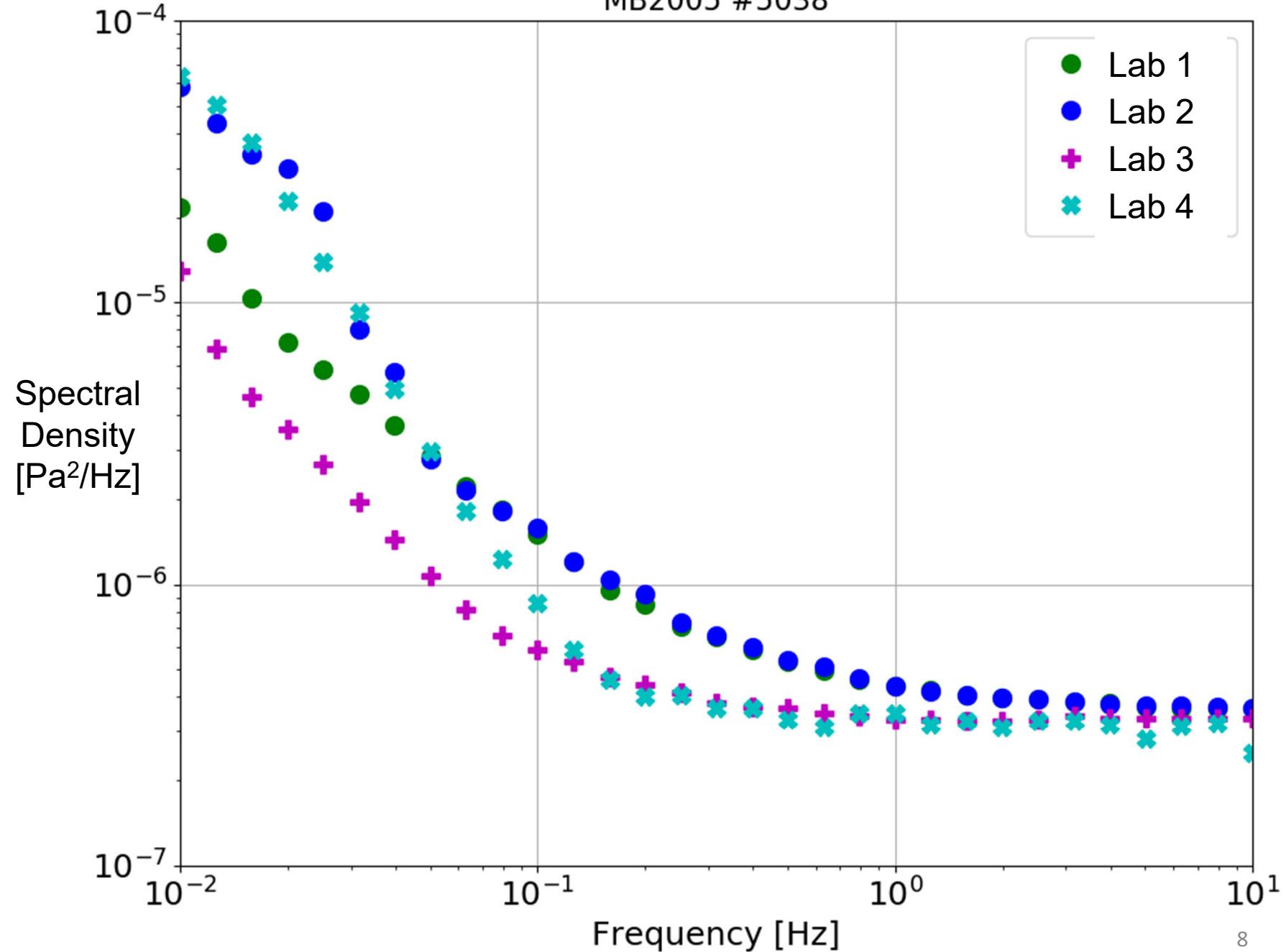




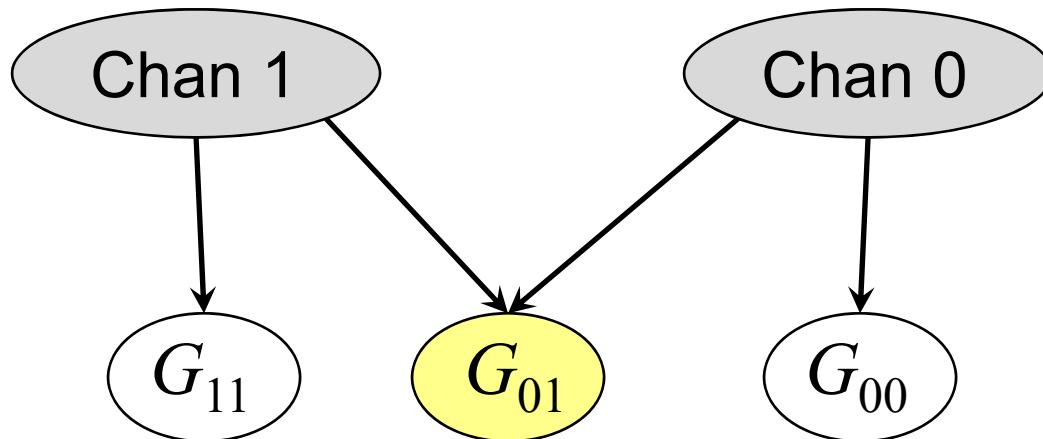




# MB2005 #5038



# Coherent-Signal Subtraction: Two-Channels Similar Sensors



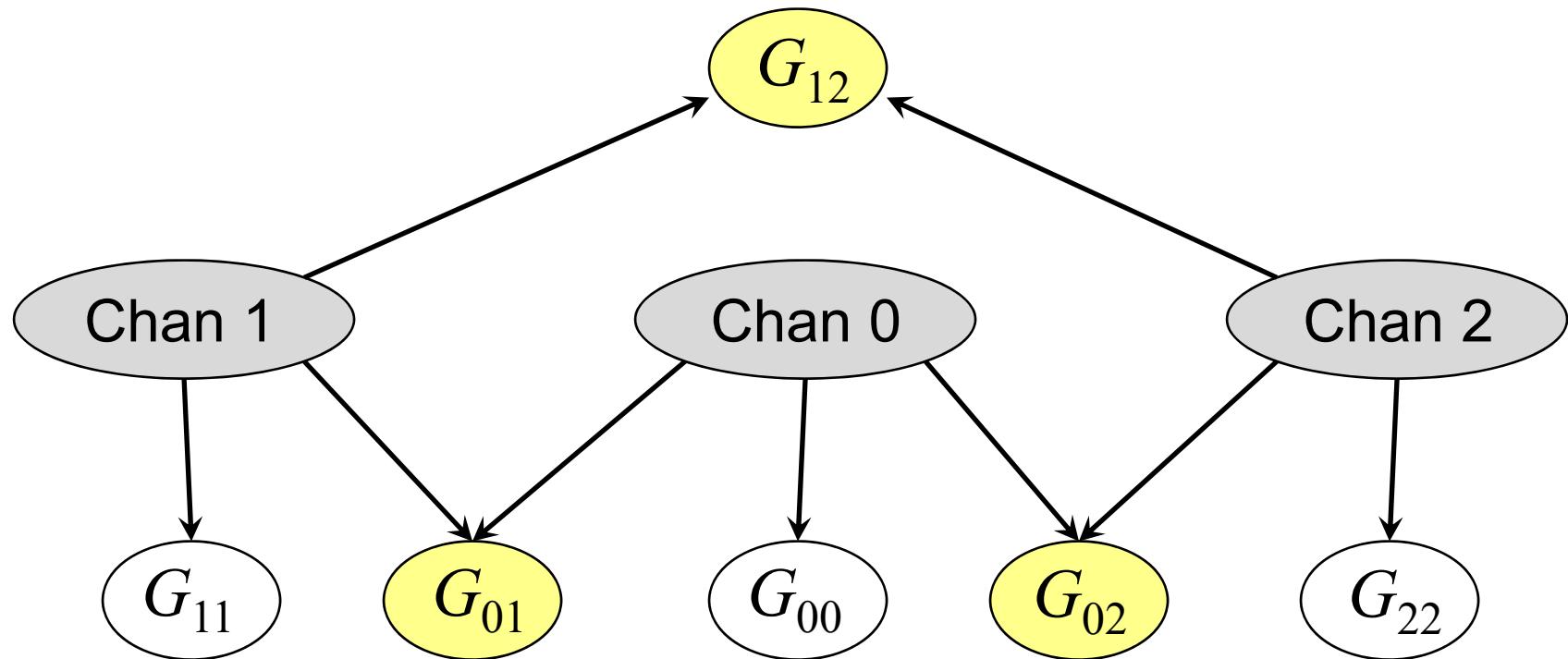
$$\tilde{N}_{00} = G_{00} \left[ 1 - \sqrt{\gamma_{01}^2} \right] \frac{1}{|H_0|^2}$$

$$\gamma_{01}^2 = \frac{G_{01}^* G_{01}}{G_{00} G_{11}}$$

$$\tilde{N}_{00} \text{ in } \frac{Pa^2}{Hz}; \quad G_{mn} \text{ in } \frac{V^2}{Hz}; \quad H_0 \text{ in } \frac{V}{Pa}$$

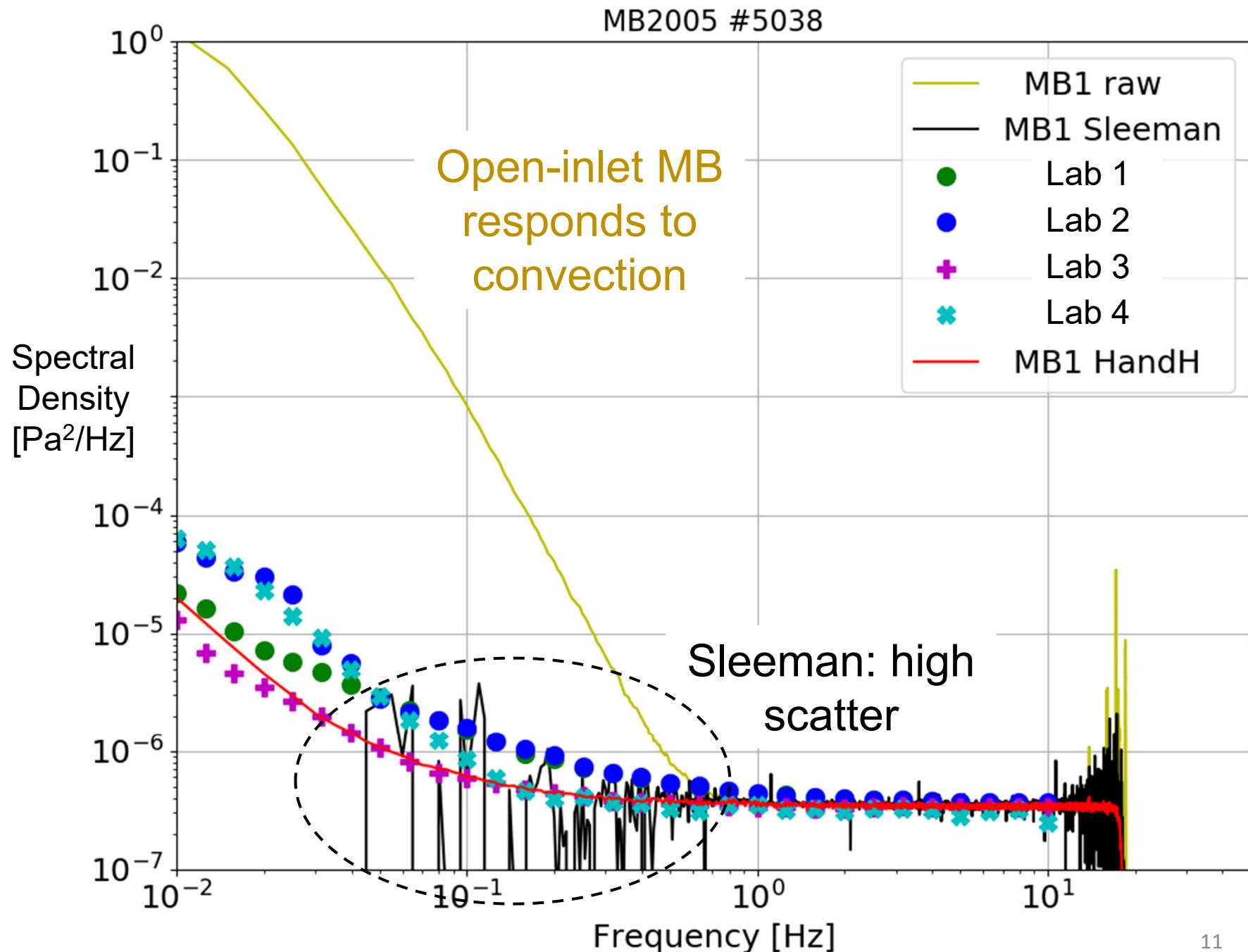
M. P. Horne and R. A. Handler, "Note on the cancellation of contaminating noise in the measurement of turbulent wall pressure fluctuations," *Experiments in Fluids* 12, pp. 136–139, 1991.

# Coherent-Signal Subtraction: Three-Channels

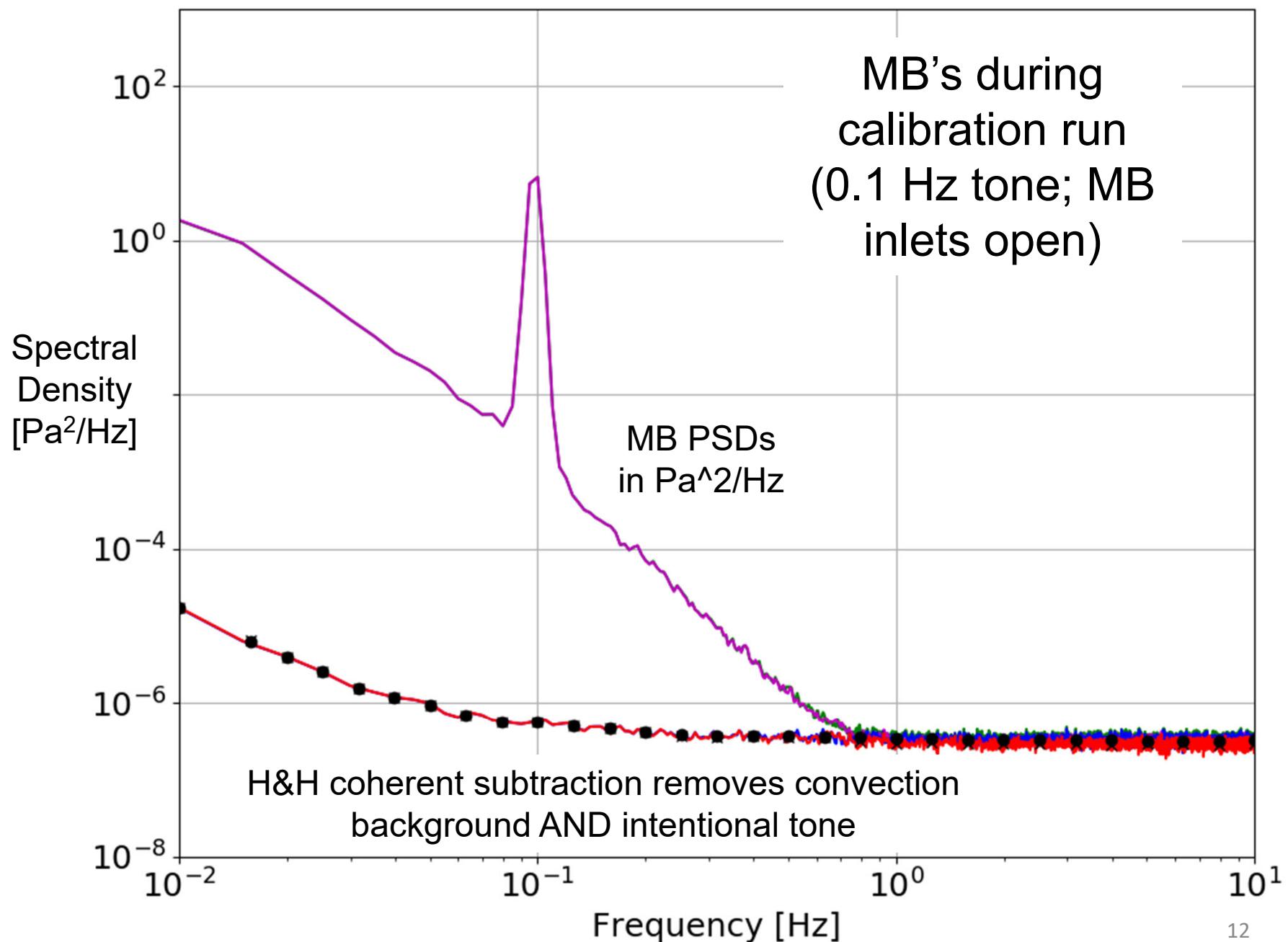


$$\tilde{N}_{00} = G_{00} \left[ 1 - \frac{G_{01} G_{20}}{G_{12}^* G_{00}} \right] \frac{1}{|H_0|^2}$$

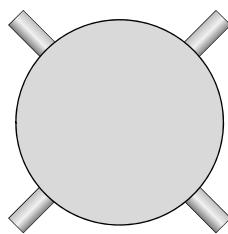
R. Sleeman, A. van Wettum, and J. Trampert, "Three-Channel Correlation Analysis: A New Technique to Measure Instrumental Noise of Digitizers and Seismic Sensors," *Bulletin of the Seismological Society of America*, Vol. 96, No. 1, pp. 258–271, February 2006. 10



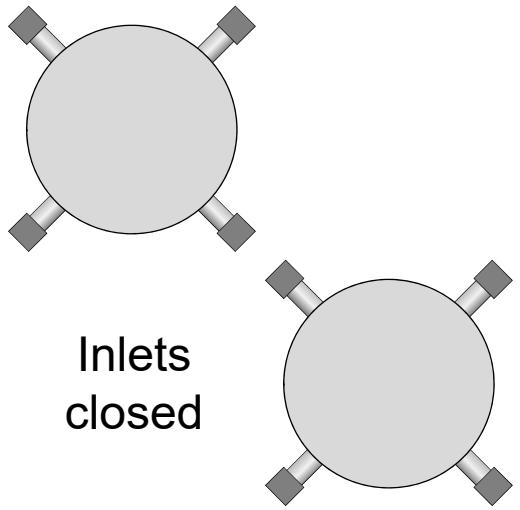
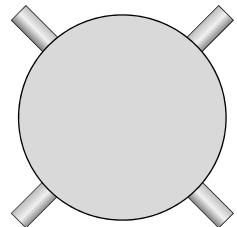
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# Sensors with Inlet Ports (MB2005)



Inlets open



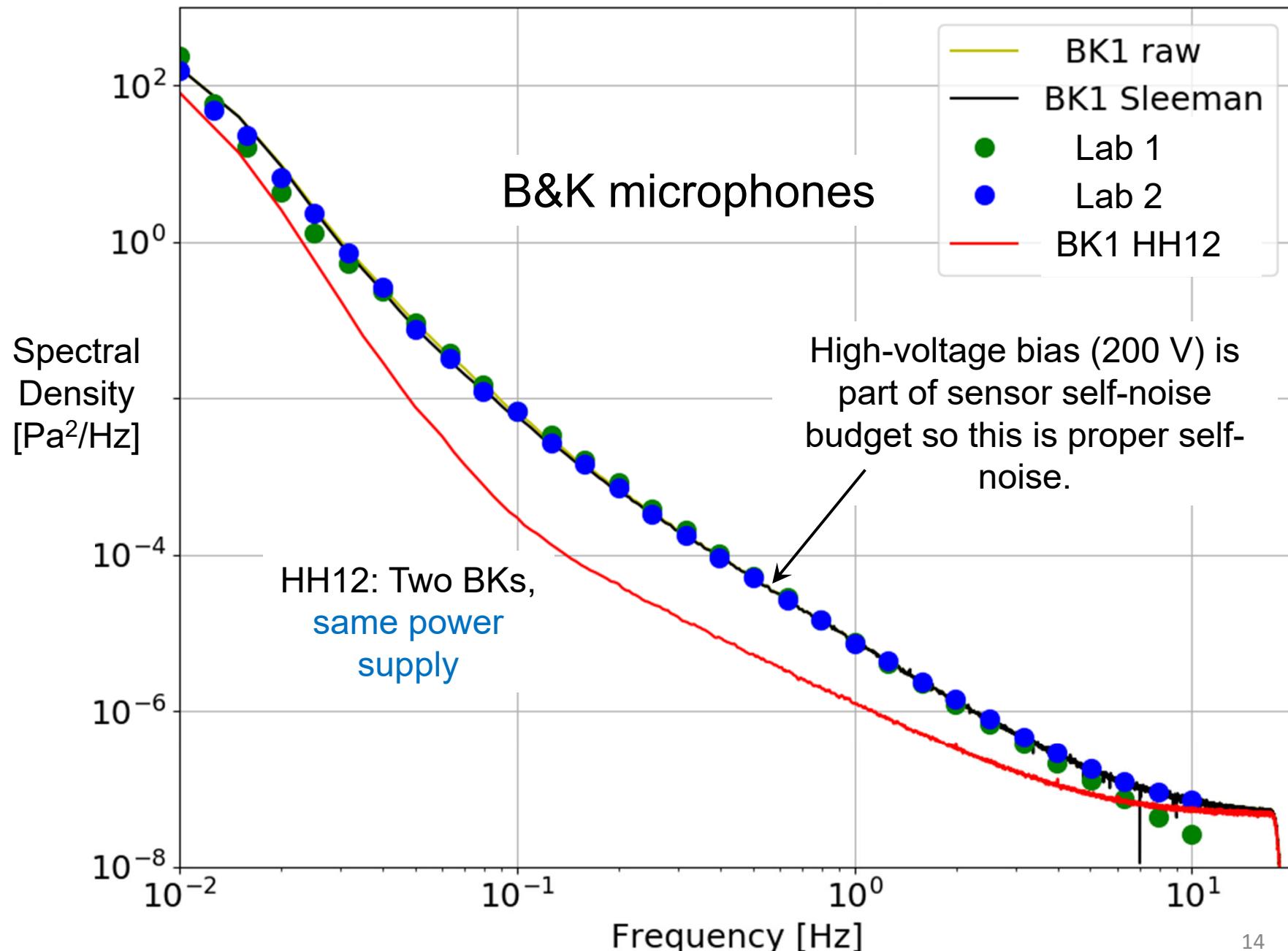
Inlets closed

Inlets coupled

- Potentially large common signal
- Common-signal subtraction OK but prone to differencing error

- Isolation
- Incoherent closed-volume components
- Common-signal subtraction ineffective

- Isolation
- Coherent closed-volume components
- Common-signal subtraction OK



# Recommendations

## Basic measurements

Use at least two sensors of each type

Plot the narrowband voltage spectral density ( $V^2/Hz$ )

List the parameters of process

    Sample rate, record length, overlap, window used,  
    number of averages

Plot the coherence

Assess the noise-floor of the digitizer

## Coherent-signal subtraction

Types

    Two-sensor (Horne and Handler)

    Three-sensor (Sleeman)

Anticipate errors associated with subtraction of large, nearly  
equal components

Check for unintended sensor coupling

    Electrical cross-talk

    Shared power

# Acknowledgements

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Yacine Sid Ahmed, Benoit Doury, Alfred Kramer (Provisional Technical Secretariat )

F. Larssonnier (Commissariat à l'énergie atomique et aux énergies alternatives)

Carrick Talmadge (National Center for Physical Acoustics)



# Back-up Slides

# Outline

Definition of self-noise

Measurement approaches

- isolation from ambient

  - in a chamber/box

  - plug inlet

  - find a quiet place

- subtraction of coherent components

  - de-activation of active element

Diagnostics

- Raw voltage spectral density ( $V^2/Hz$ )

- Coherence

- Noise-floor of DAQ

Problems

- isolation

- coherence

- spurious response (e.g., temperature fluctuations)

Coherent-signal subtraction

- types

- potential for problems

Recommendations

# Sensor Self-Noise

**Definition of Self-noise:** the irreducible output of the sensor; the output of the sensor with negligible excitation. Accomplish by isolation and/or coherent-signal subtraction.

Use at least two sensors of the same type.

Use coherence to verify “good” noise-floor measurement.

Report narrowband spectral density, record length, time-domain window, overlap, sample rate, digitizer, digitizer gain.

Minimum (?) for narrowband estimation in 0.01 to 10 Hz range: 200 s records ( $df = 0.005$  Hz, ignore  $0*df$  and  $1*df$  bins); 50% overlap, Hann window; 100 averages (total time = 2.8 hours).

Incomplete isolation from ambient introduces a bias (over-estimate); this error is not a zero-mean random uncertainty.

Measure noise floor of acquisition system to verify that it's sufficiently below sensor noise floor (challenging for B&K microphones); need noise floor of everything after sensor ( $V^2/Hz$  useful presentation).

Decibel reference:  $1.0 \text{ Pa}^2/\text{Hz}$  and  $10*\log_{10}(\text{spectral density})$ .

## Sensor Self-Noise: Special Cases

Microbarometers generate heat and, in closed chambers, produce **convection**, which produces turbulence. Two factors confound coherent-signal subtraction: coherent levels much larger than self-noise levels and potential for turbulence scales to be shorter than distance between inlet ports over some range of frequencies.

Capping microbarometers can isolate from chamber convection; however, **capping “adds” another noise source**: pressure fluctuations caused by temperature fluctuations in the fore-volume.

Possible method if sensor test must be done inside chamber: port all microbarometers together while capped with respect to interior of chamber. (Some evidence that Horne and Handler coherent subtraction may work with inlets open.)

Possible method if measurement can be done at local ambient pressure: Cluster three or more sensors indoors/outdoors (but not inside a chamber) and use Sleeman for quiet overnight period.

B&K power-supply noise common to all connected microphones; use separate power supply for each microphone, if possible.

**Injection of signal: don’t do it** unless trying to characterize nonlinearity and spurious lines; then use high-purity (?) sine wave, not broadband

# Basic Parameters for Self-Noise Measurement (examples)

## Case 1

Sample frequency,  $fs = 200$  S/s

# usable records, record length = 330, 100 s

File length = 5.7 hours

Window, Overlap: Hann, 50%

## Case 2

Sample frequency,  $fs = 40$  S/s

# usable records, record length = 700, 200 s

File length = 19.4 hours

Window, Overlap: Hann, 50%

## Digitizer [Example: Guralp Affinity]

<https://www.osti.gov/servlets/purl/1564039>

G.W. Slad, Guralp Affinity Evaluation for SNL Infrasound Testbed, Sandia National Laboratories Report SAND2019-10947, Sept 2019.

<https://doi.org/10.2172/1564039>

Standard set up

Gain = x1

Full scale = +/-20 V (40 V range)

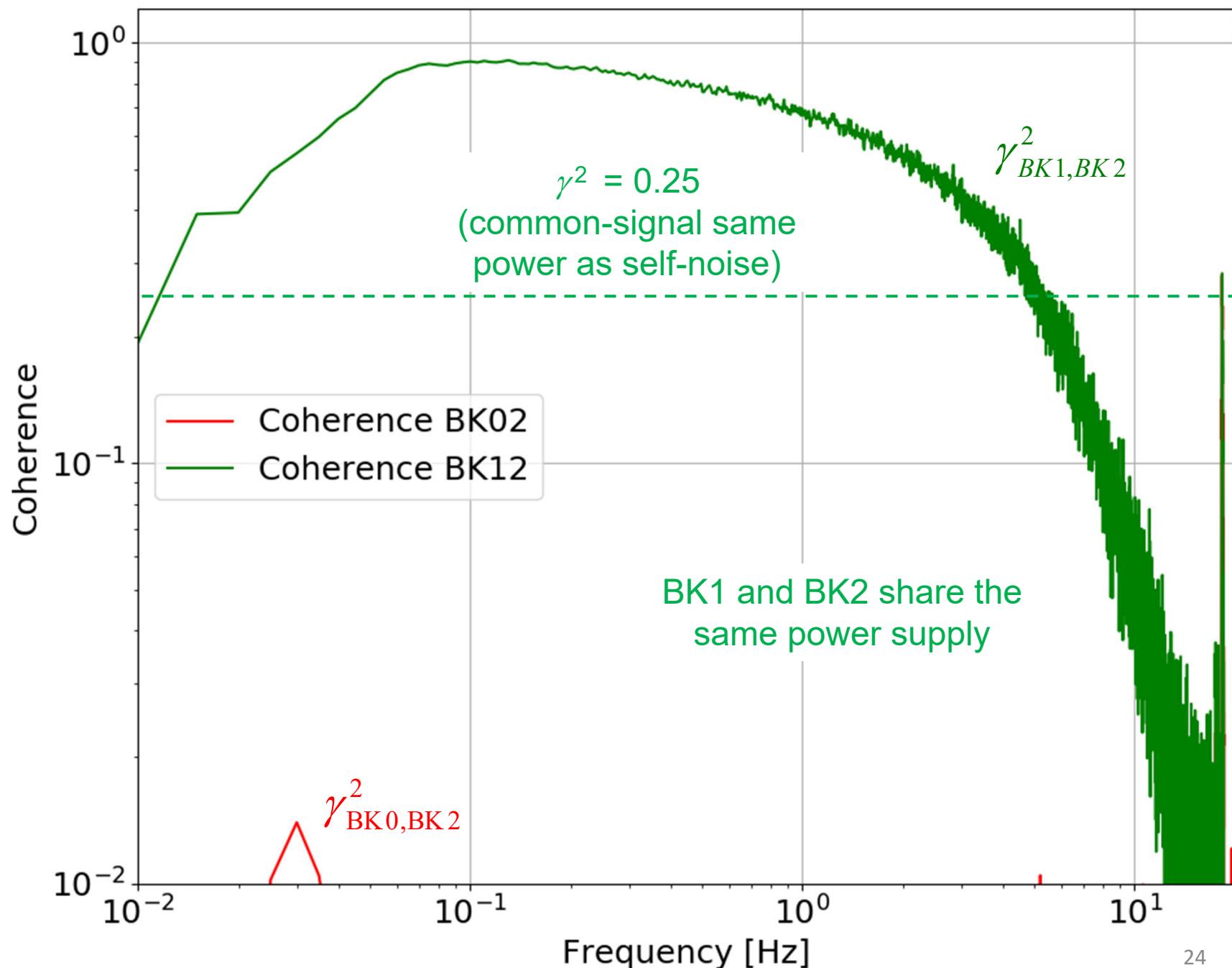
Noise floor (for  $f_s = 200$  S/s and x1 gain)

-126 dB/V<sup>2</sup>/Hz; 2.5e-13 V<sup>2</sup>/Hz; 500 nV/ $\sqrt{\text{Hz}}$ ; 21 bits effective

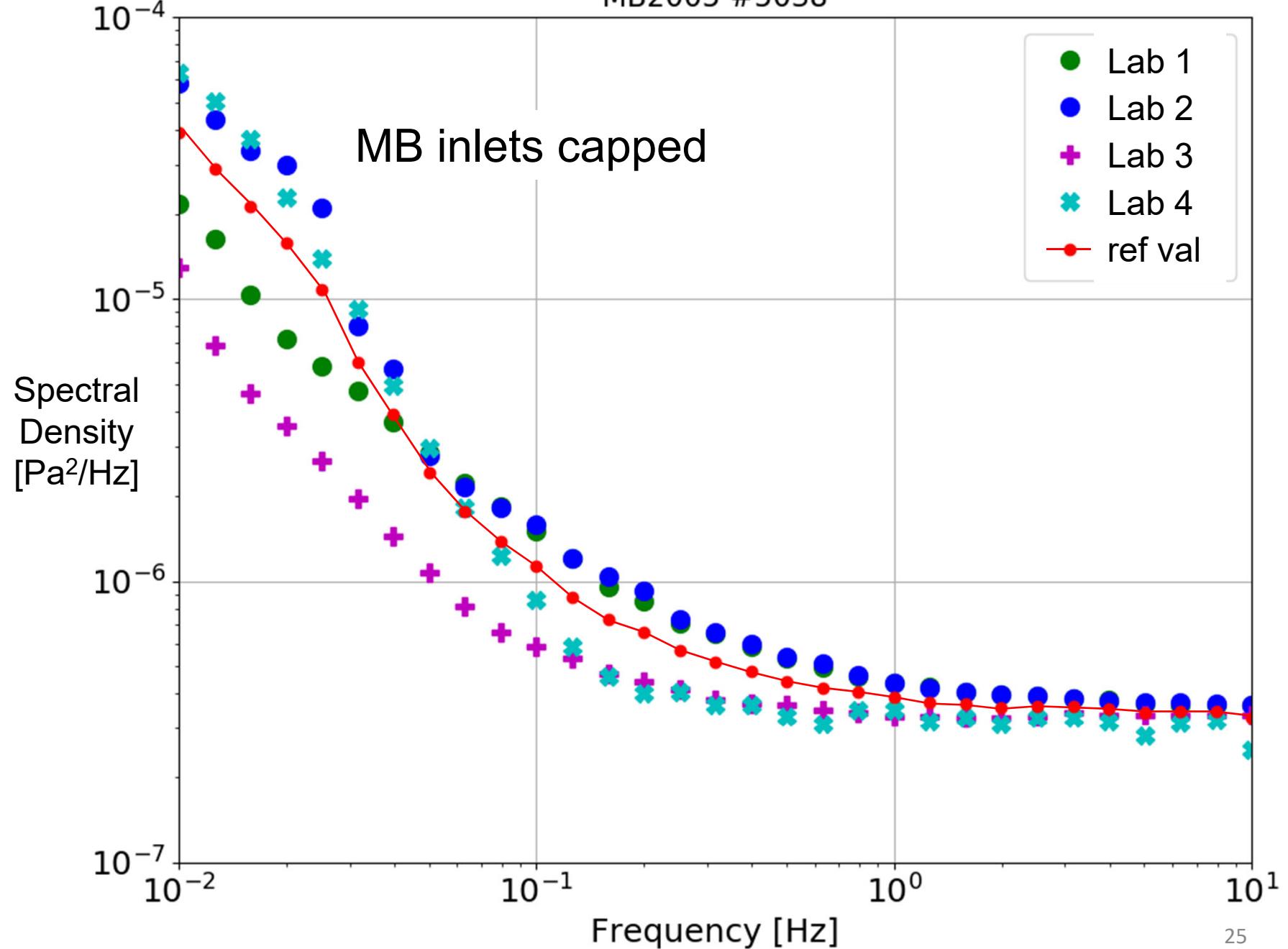
[100-ohm resistor termination for noise-floor measurement:

Resistor noise = 1.6e-18 V<sup>2</sup>/Hz; 1.3 nV/ $\sqrt{\text{Hz}}$ ]

Nominal bit weight = 1.000  $\mu\text{V}/\text{count}$



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## Outdoor Self-Noise Measurement

