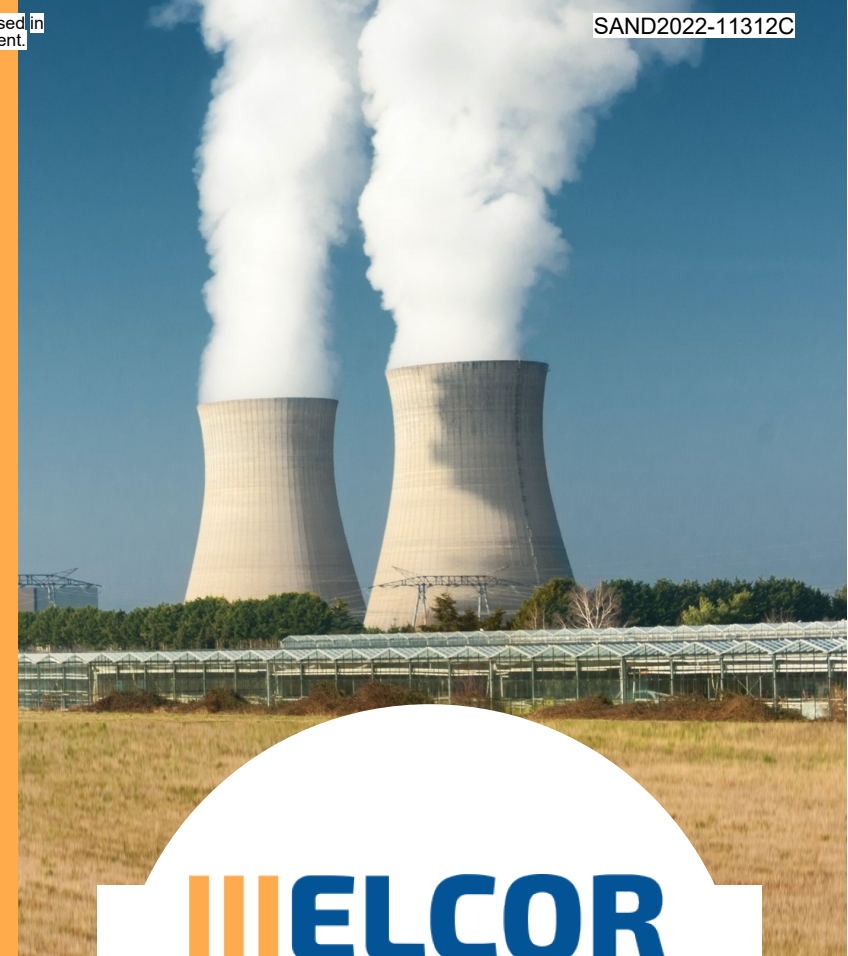




Sandia
National
Laboratories

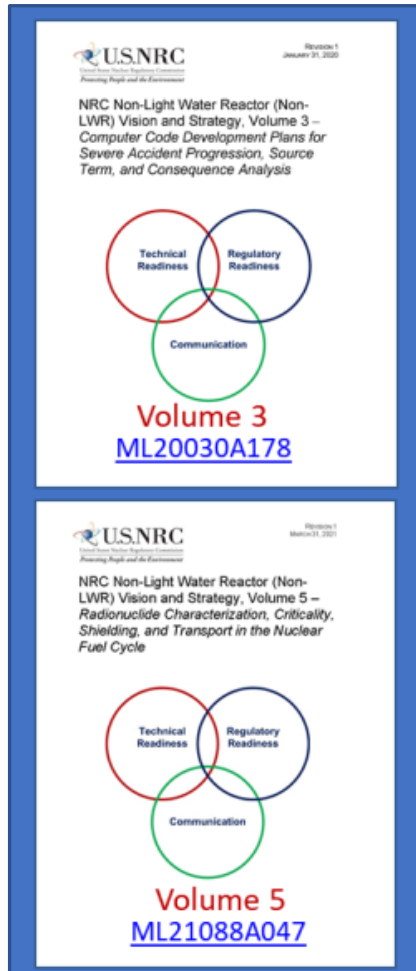
Securing the future of Nuclear Energy



MELCOR Integrated Non-LWR Accident Progression and Source Term Analysis

David L. Luxat
Nuclear Energy Safety Modeling and Analysis (8852)

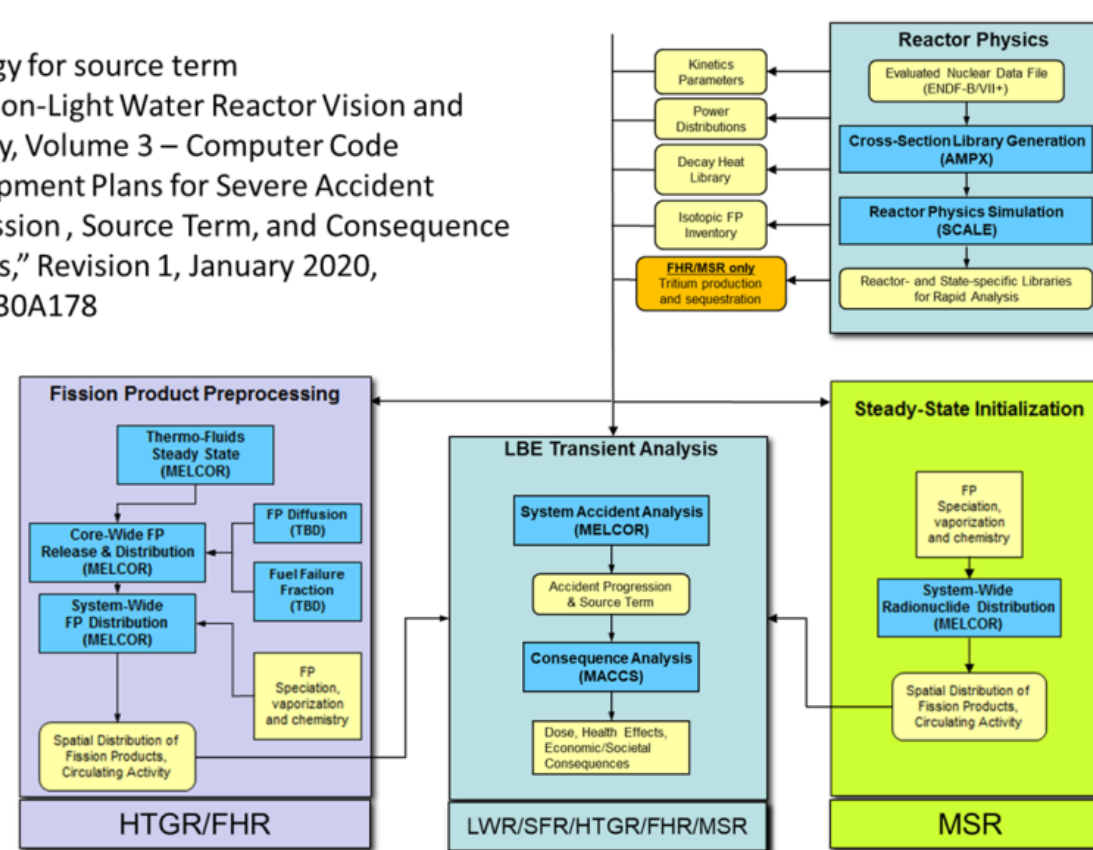
NRC strategy for severe accident analysis



Evaluation Model and Suite of Codes

Code strategy for source term

“NRC Non-Light Water Reactor Vision and Strategy, Volume 3 – Computer Code Development Plans for Severe Accident Progression, Source Term, and Consequence Analysis,” Revision 1, January 2020, ML20030A178



MELCOR Non-LWR Public Demonstrations

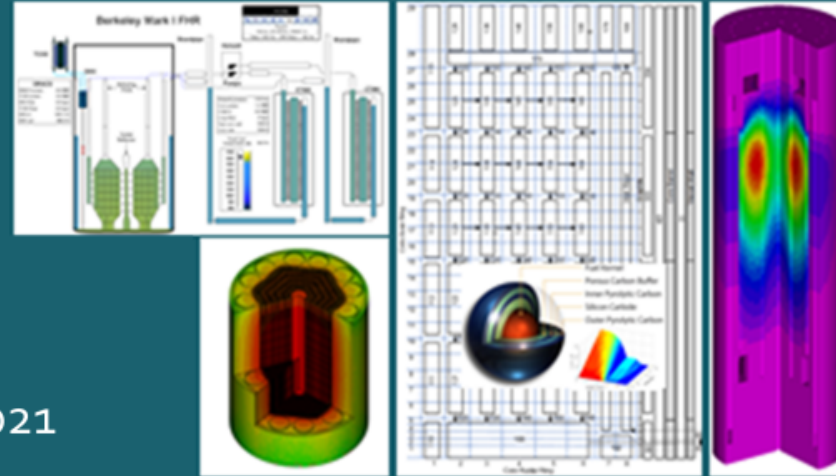


Public Workshop: SCALE/ MELCOR Non LWR Source Term Demonstration Project

Heat pipe reactor – June 29, 2021

Gas cooled reactor – July 20, 2021

Pebble bed molten-salt-cooled reactor – Sept 14, 2021

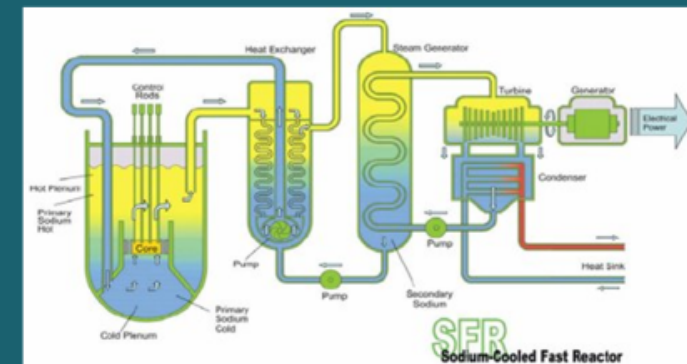
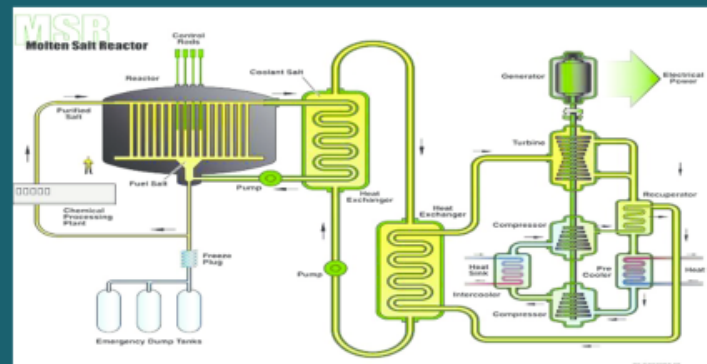


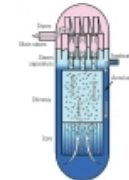
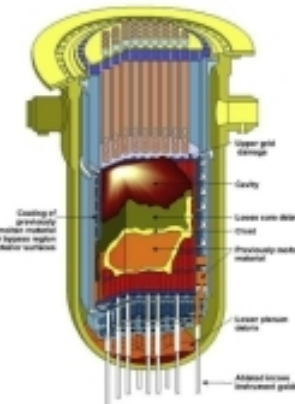
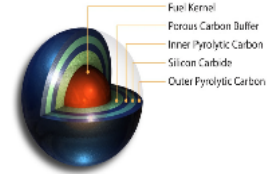
For More
Information



Coming in 2022

Molten-salt fueled reactor
Sodium-cooled fast reactor





MELCOR Pedigree – Leveraging Collaboration

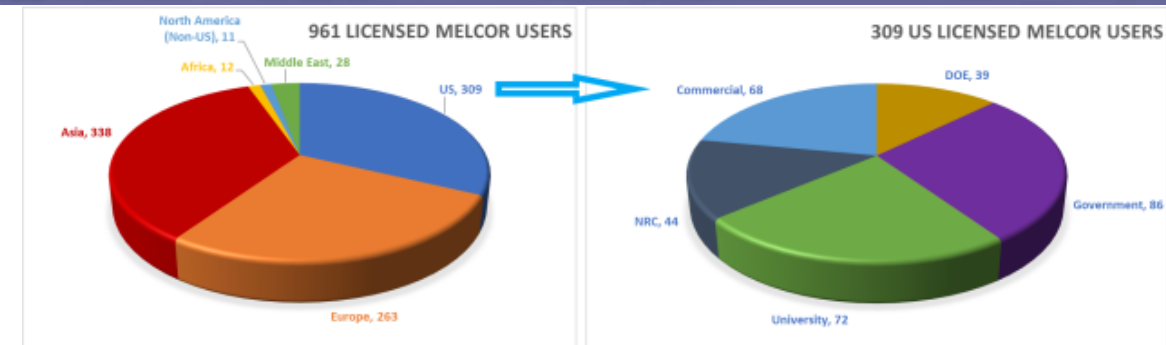


Validated physical models

- International Standard Problems, benchmarks, experiments, and reactor accidents
- Beyond design basis validation will always be limited by model uncertainty that arises when extrapolated to reactor-scale

Cooperative Severe Accident Research Program (CSARP) is an NRC-sponsored international, collaborative community supporting the validation of MELCOR

International LWR fleet relies on safety assessments performed with the MELCOR code



MELCOR Non-LWR Modeling



Hydrodynamic modeling

Generalized working fluid treatment

Conduction heat transfer within working fluids (under development)

Generalized convection and flow models to capture flow through new core geometries (e.g., pebble beds)

Core models

TRISO pebble and compact core components

Heat pipe reactor core component

Graphite oxidation

Intercell and intracell conduction

Fast reactor core degradation (under development)

Fission product release

Generalized release modeling for metallic fuels

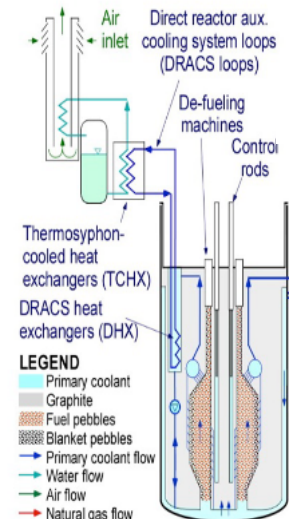
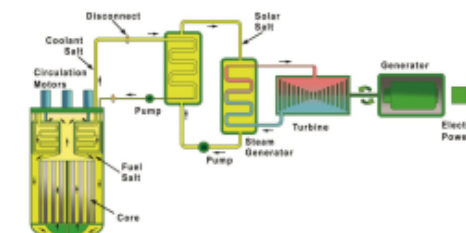
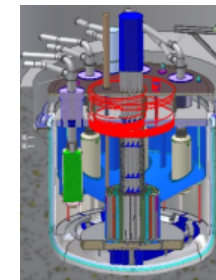
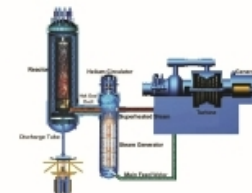
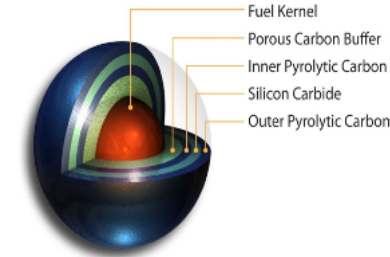
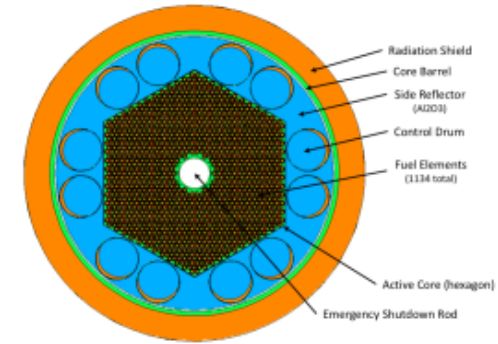
Radionuclide transport and release from TRISO particles, pebbles and compacts

Generalized Radionuclide Transport and Retention (GRTR) model (under development)

Simplified neutronic modeling

Solid fuel core point kinetics

Fluid point kinetics (liquid-fueled molten salt reactors)



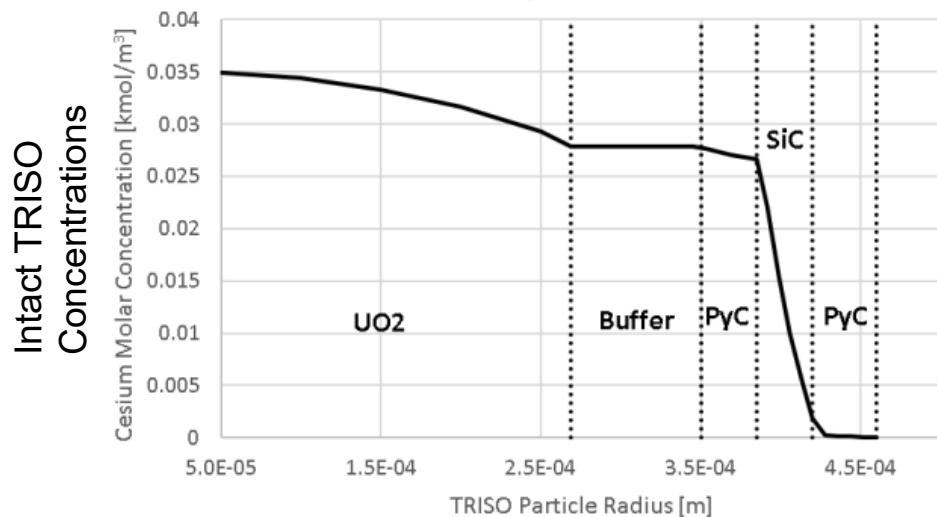
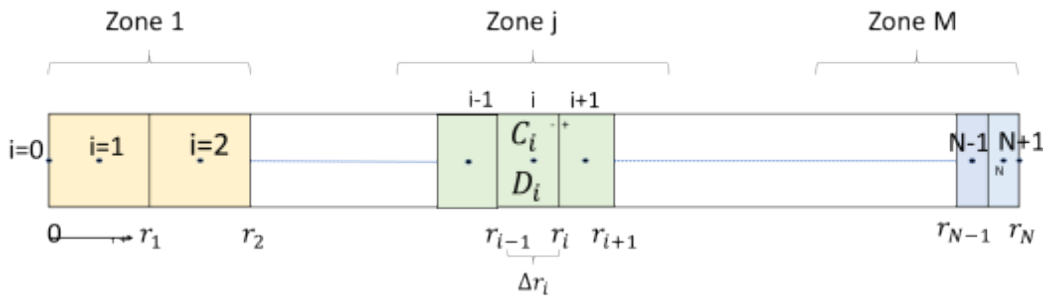
TRISO Radionuclide Diffusion Release Model



Intact TRISO Particles

- One-dimensional finite volume diffusion equation solver for multiple zones (materials)
- Temperature-dependent diffusion coefficients (Arrhenius form)

$$\frac{\partial C}{\partial t} = \frac{1}{r^n} \frac{\partial}{\partial r} \left(r^n D \frac{\partial C}{\partial r} \right) - \lambda C + \beta \quad D(T) = D_0 e^{-\frac{Q}{RT}}$$



Diffusivity Data Availability

Radionuclide	UO ₂	UCO	PyC	Porous Carbon	SiC	Matrix Graphite	TRISO Overall
Ag	Some	Not investigated	Some	Not found	Extensive	Some	Extensive
Cs	Some		Some		Extensive	Some	Some
I	Some		Some		Some	Not found	Not found
Kr	Some		Some		Not found	Some	Some
Sr	Some		Some		Extensive	Some	Some
Xe	Some		Some		Some	Some	Not found

Data used in the demo calculation

[IAEA TECDOC-0978]

Layer	FP Species							
	Kr		Cs		Sr		Ag	
	D (m ² /s)	Q (J/mole)	D (m ² /s)	Q (J/mole)	D (m ² /s)	Q (J/mole)	D (m ² /s)	Q (J/mole)
Kernel (normal)	1.3E-12	126000.0	5.6-8	209000.0	2.2E-3	488000.0	6.75E-9	165000.0
Buffer	1.0E-8	0.0	1.0E-8	0.0	1.0E-8	0.0	1.0E-8	0.0
PyC	2.9E-8	291000.0	6.3E-8	222000.0	2.3E-6	197000.0	5.3E-9	154000.0
SiC	3.7E+1	657000.0	7.2E-14	125000.0	1.25E-9	205000.0	3.6E-9	215000.0
Matrix Carbon	6.0E-6	0.0	3.6E-4	189000.0	1.0E-2	303000.0	1.6E00	258000.0
Str. Carbon	6.0E-6	0.0	1.7E-6	149000.0	1.7E-2	268000.0	1.6E00	258000.0

Iodine assumed to behave like Kr

CORSOR-Booth LWR scaling used to estimate other radionuclides

Heat Pipe Reactor Modeling

Release from fuel to reactor vessel

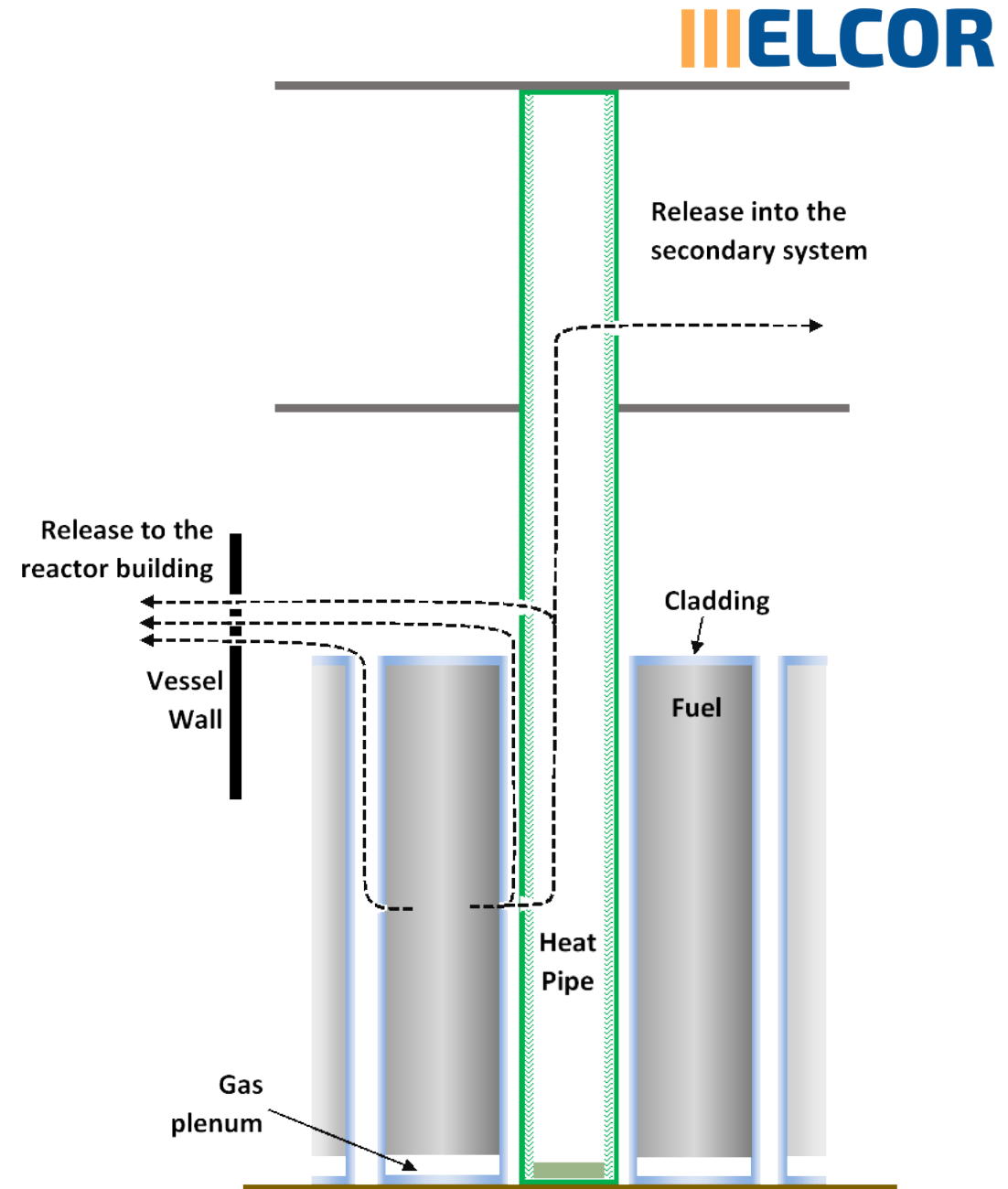
- Stainless-steel cladding failure at 1650 K

Release from reactor vessel to reactor building

- Assumed reactor vessel leakage

Heat-pipe release path

- Requires heat-pipe wall failure in two places
 - Creep rupture followed by melting
- Creep rupture failure in the heat-pipe condenser region (secondary system region) could lead to reactor building bypass



MELCOR Generalized Radionuclide Transport and Retention (GRTR) Model



Model Scope

Define 5 radionuclide physico-chemical forms in liquid pool

- Soluble fission products
- Insoluble fission products suspended in working fluid
- Insoluble fission products deposited on structures
- Insoluble fission products at liquid-gas interface
- Fission product gases

Generalized Gibbs Energy Minimization approach

- Fission product solubility
- Fission product vapor pressure

Model generically applies to range of non-LWR working fluids

- Molten salt systems
- Liquid metal systems

Fission Product Forms	Soluble FPs (salt-seeking) Form 1	Insoluble FP suspension Form 2	Salt liq./gas Interface Form 3	Insoluble FP deposits on structures Form 4	FPs Vapor/NCG Form 5	
Equilibrium	Soluble & Volatile FP	Insoluble FP suspension			Gas Bubbles	
Transport within GRTR	Soluble & Volatile FP	Insoluble FP suspension	Salt gas/liq. Interface	Deposits on heat structures	Deposits on core	Gas Bubble Rise
Gas space Release	Volatile Vapor and Eventual Aerosol	No Release	Bubble Film Rupture Aerosol	No Release	Gas Release (Kr, Xe, T)	

MELCOR Generalized Radionuclide Transport and Retention (GRTR) State Modeling



Fission products characterized in terms of...

Isotopic state

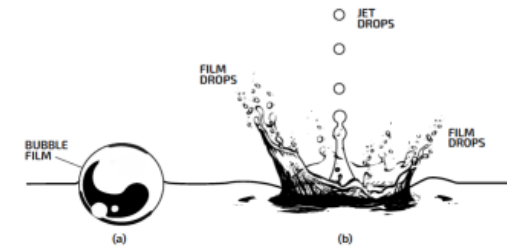
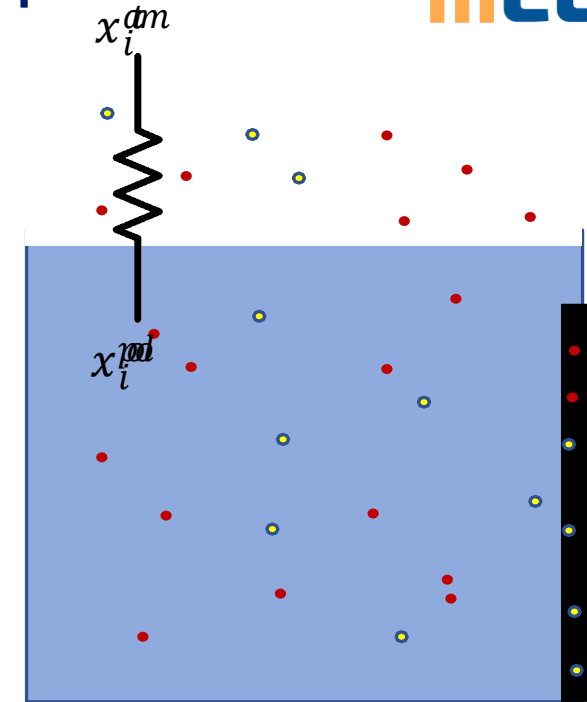
- Fission product decay

Distribution of fission products in reactor system

- Hydrodynamic flows moving fission products within system

Physico-chemical form and ability of fission products to be transported out of liquid pool

- Deposition on structures from liquid pool
- Vaporization into gas atmospheres from liquid pools
- Attachment to gas bubbles in liquid pool or surface interface between liquid pool and gas atmosphere
- Aerosolization of fission products into gas atmosphere through bursting of bubbles



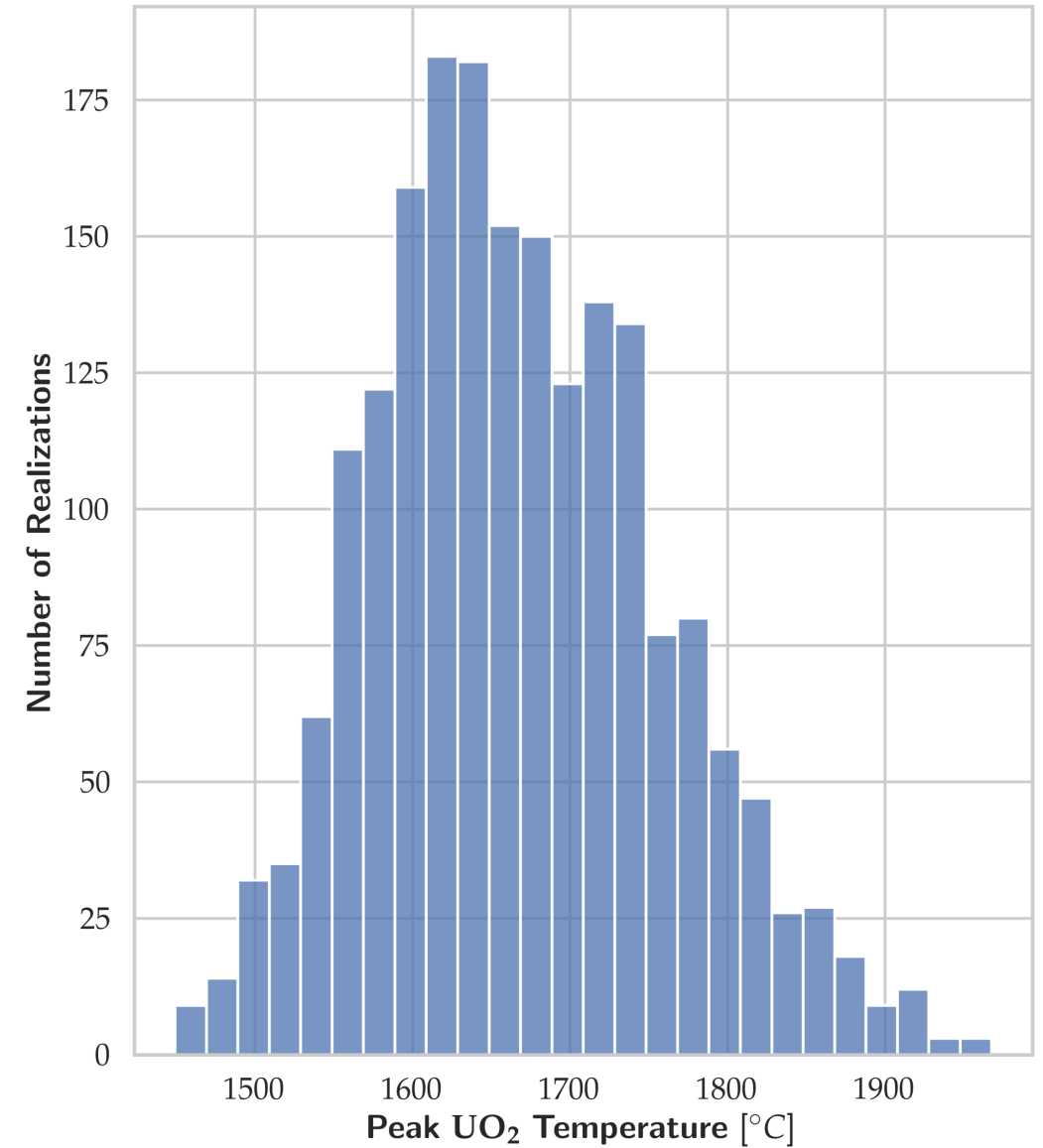
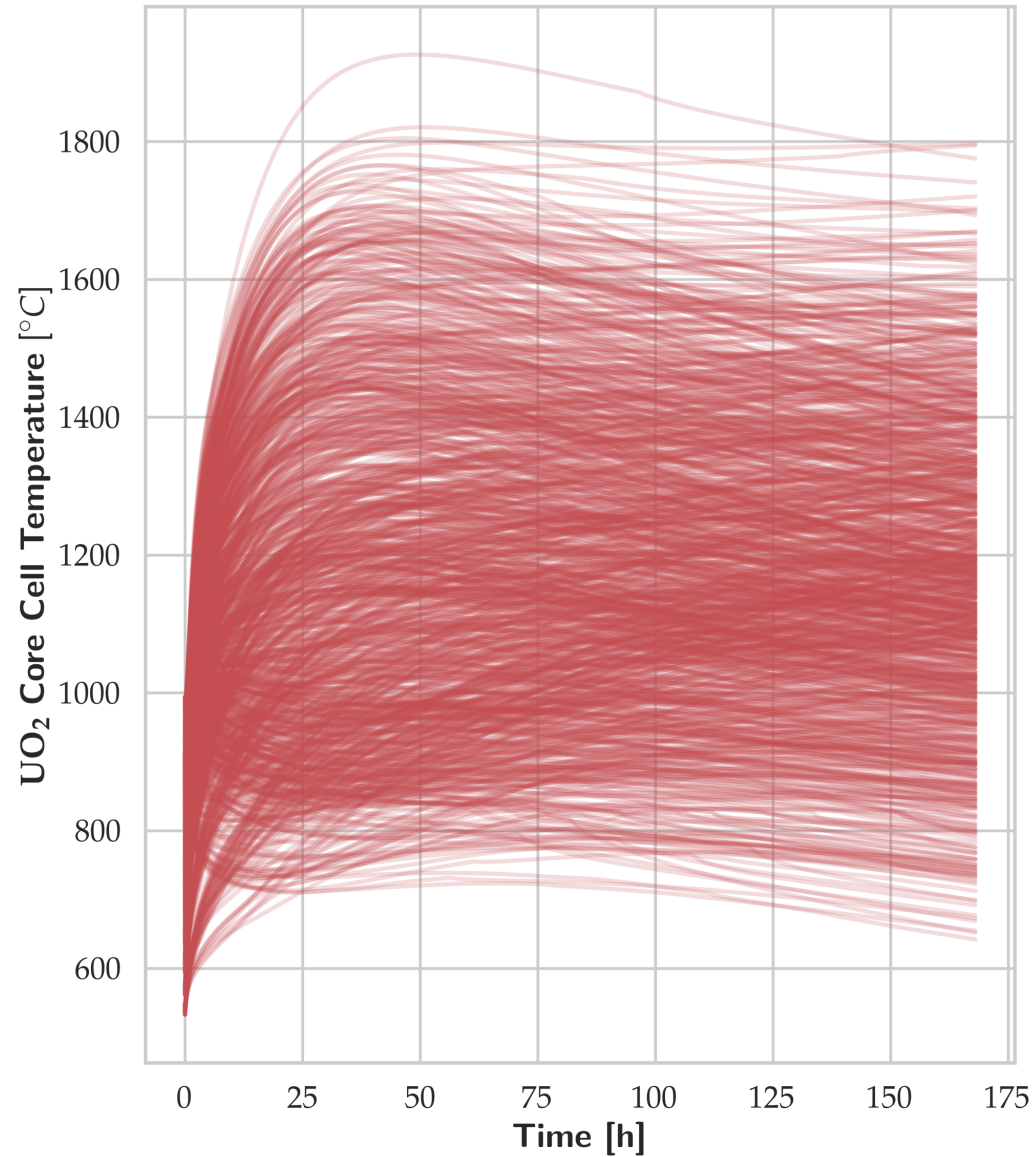
Note: MELCOR considers soluble, bulk colloid, interfacial colloid, and vapors as distinct physico-chemical states

MELCOR can be used to explore the variability of the results to uncertainties

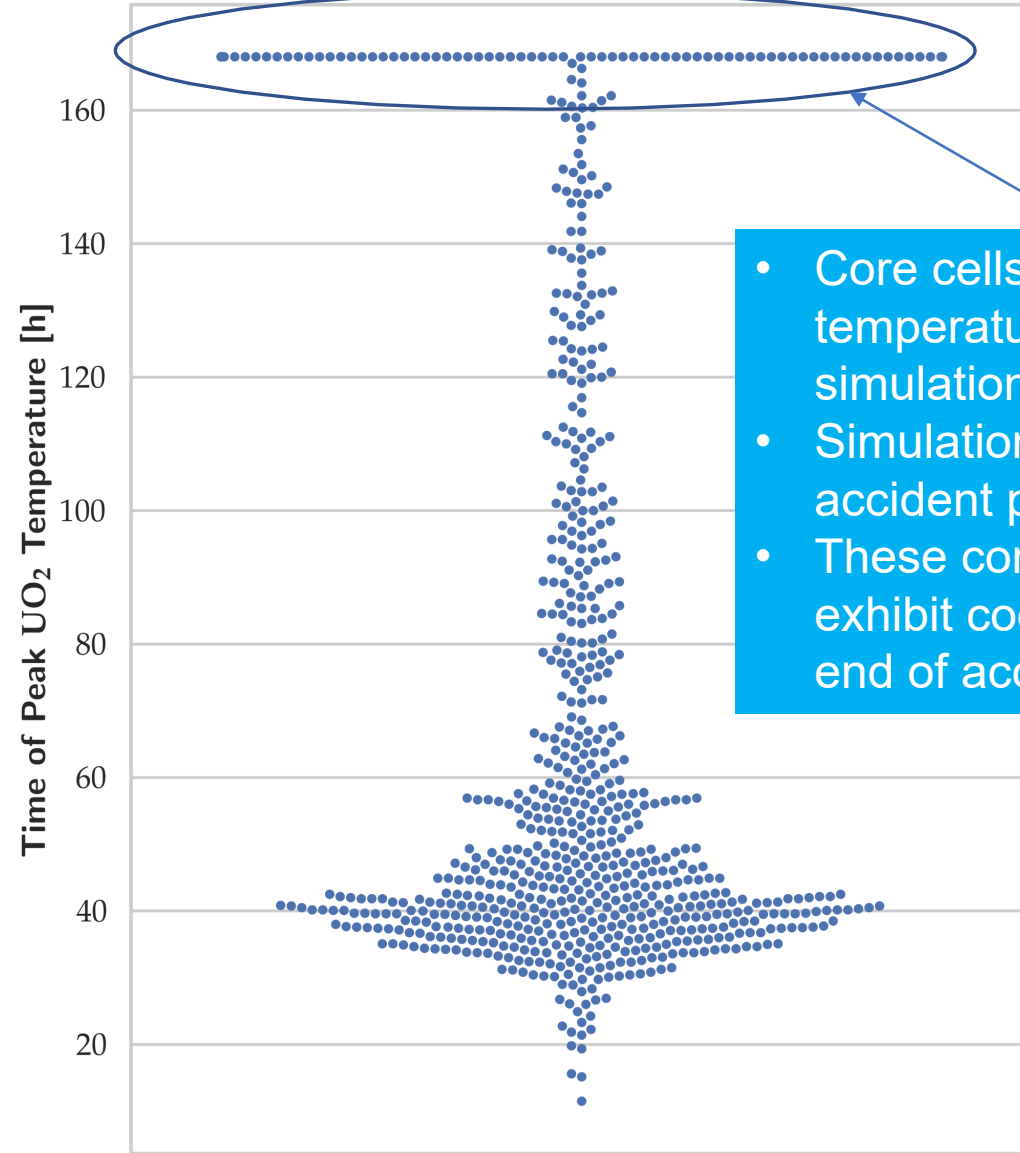
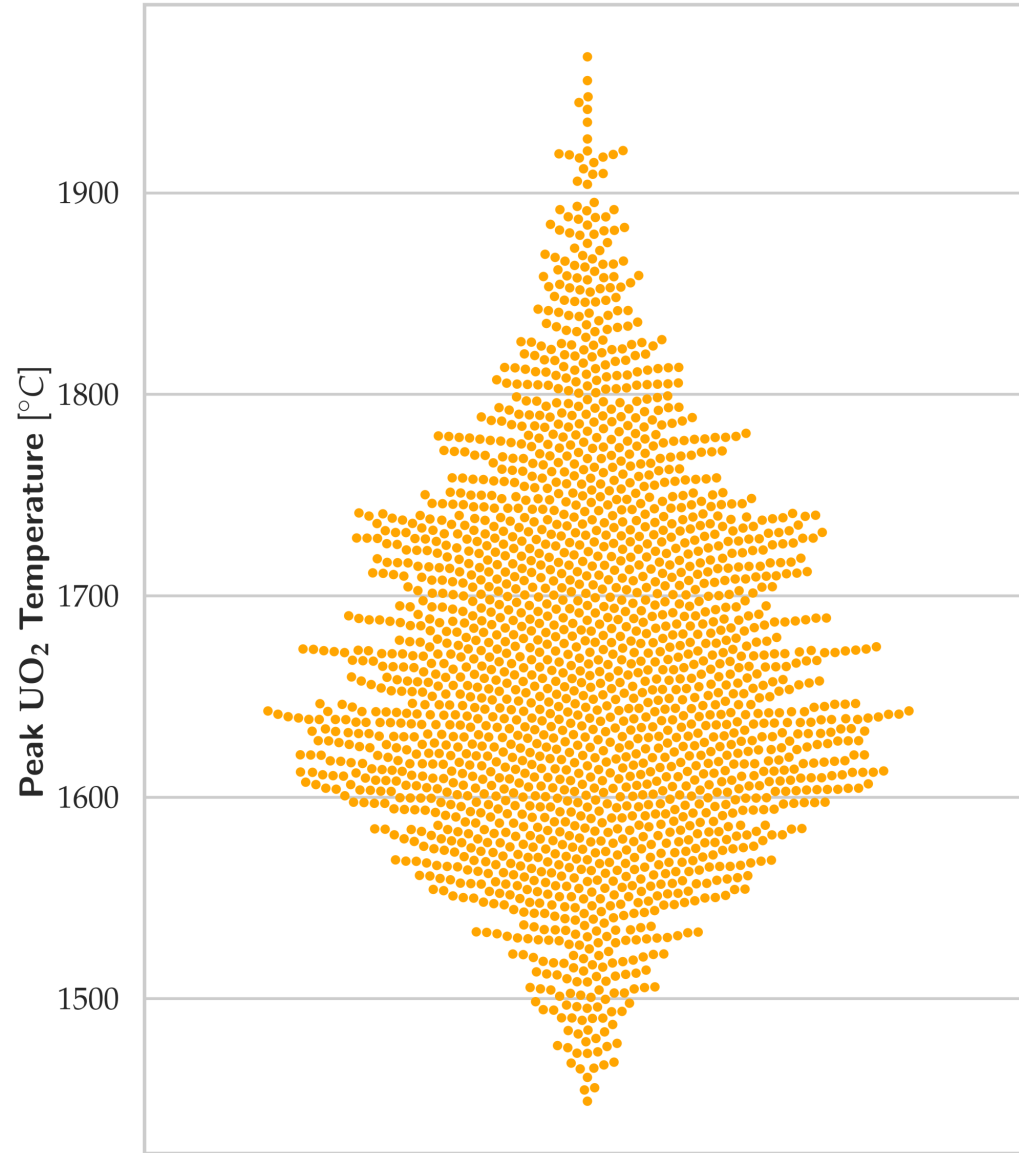


Model	Parameter	Distribution	Range
TRISO Model Parameters	Initial TRISO Failure Fraction (fraction of inventory)	Log uniform	$10^{-5} - 10^{-3}$
	TRISO Failure Rate Multiplier (-)	Log uniform	0.1 – 10.0
	Intact TRISO Diffusivity Multiplier (-)	Log uniform	0.001 – 1000.0
	Failed TRISO Diffusivity Multiplier (-)	Log uniform	0.001 – 1000.0
	Matrix Diffusivity Multiplier (-)	Log uniform	0.001 – 1000.0
	TRISO Pebble Emissivity (-)	Uniform	0.5 – 0.999
	TRISO Pebble Bed Porosity (-)	Uniform	0.3 – 0.5
	TRISO recoil fraction (-)	Uniform	0 – 0.03
Radionuclide Model Parameters	Shape Factor (-)	Uniform	1.0 – 5.0
	Gaseous Iodine Multiplier (Base = 5% I ₂)	Uniform	0.02 – 1.0
Design Parameters	Graphite Conductivity Multiplier (-)	Uniform	0.5 – 1.5
	Decay Heat Multiplier (-)	Uniform	0.9 – 1.1
	RCCS Blockage Multiplier (-)	Log uniform	0.001 – 1.0
	RCCS Emissivity (-)	Uniform	0.1 – 1.0
	Reactor Building Leakage Multiplier (-)	Log uniform	0.1 – 100.0
	Wind speed (m/s)	Uniform	0 - 10

UO₂ Thermal Response



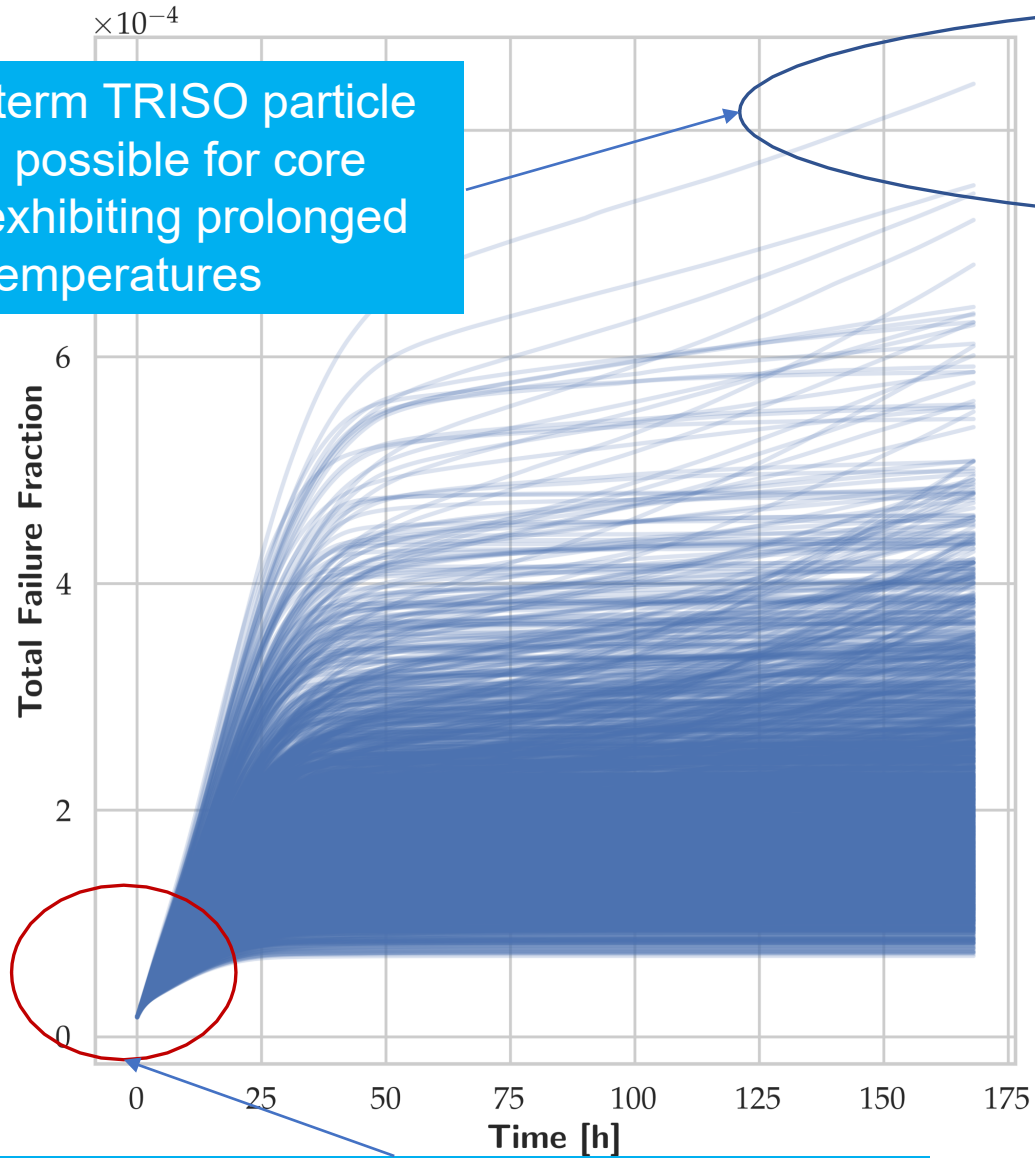
UO₂ Thermal Transient Evolution



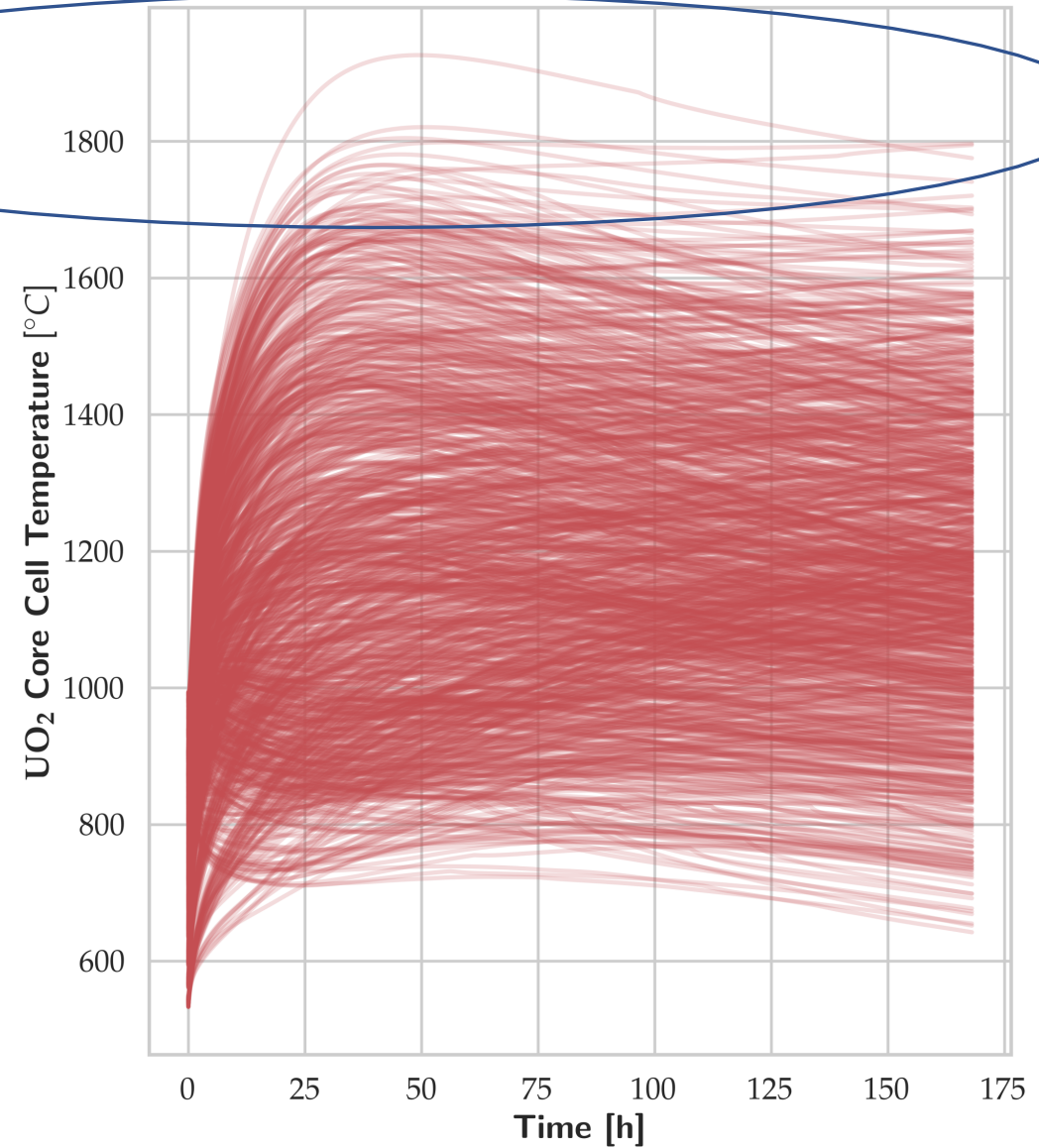
- Core cells with peak fuel temperatures at end of simulation
- Simulation time denoted as accident phase
- These core cells do not exhibit cooldown prior to end of accident phase

TRISO Particle Failure

Long-term TRISO particle failure possible for core cells exhibiting prolonged over-temperatures

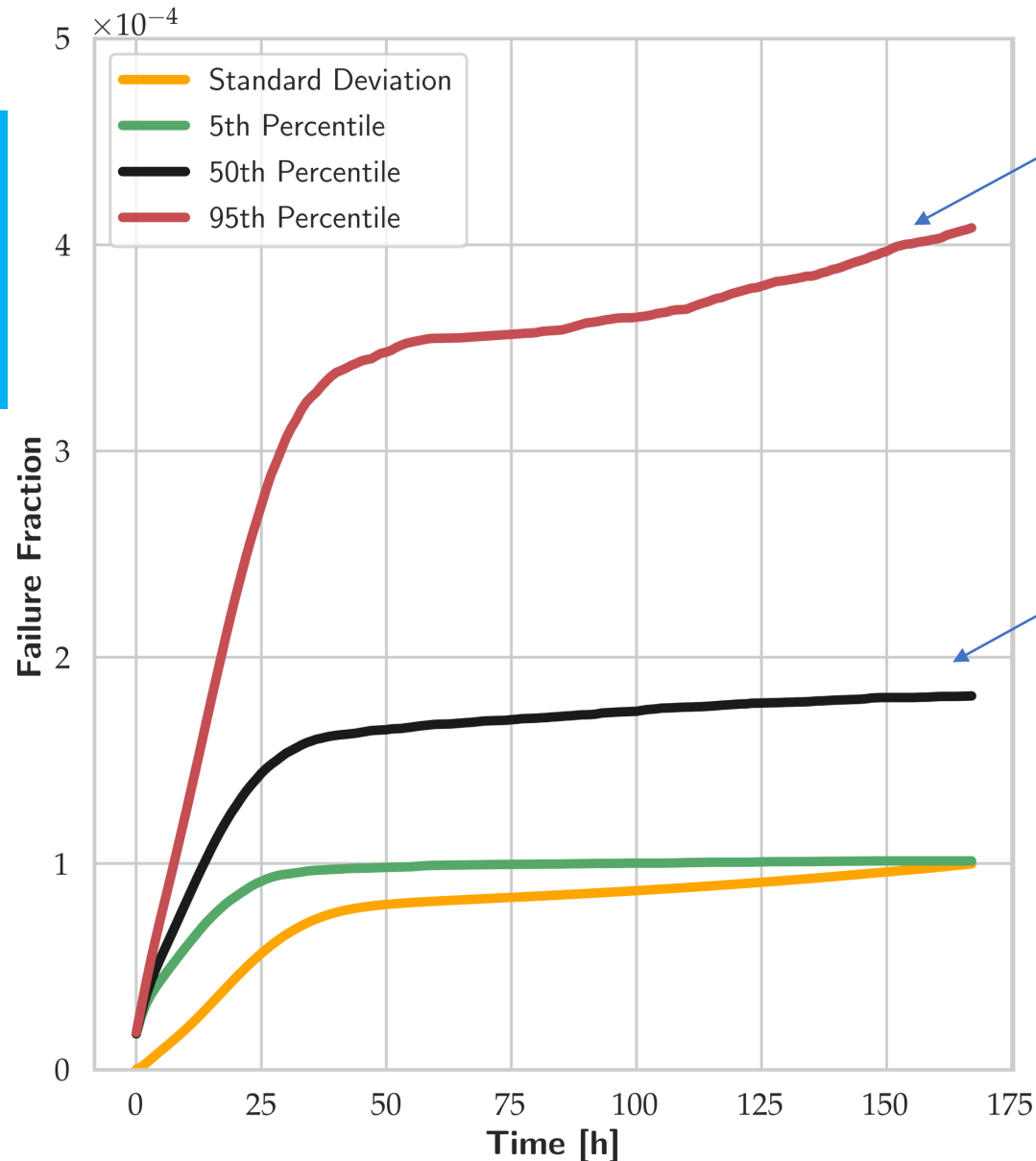


Initial distribution of failed TRISO particles



Evolution of TRISO Particle Failures

Long-term failures of TRISO particles at lower rate but driven by prolonged period of elevated fuel temperature



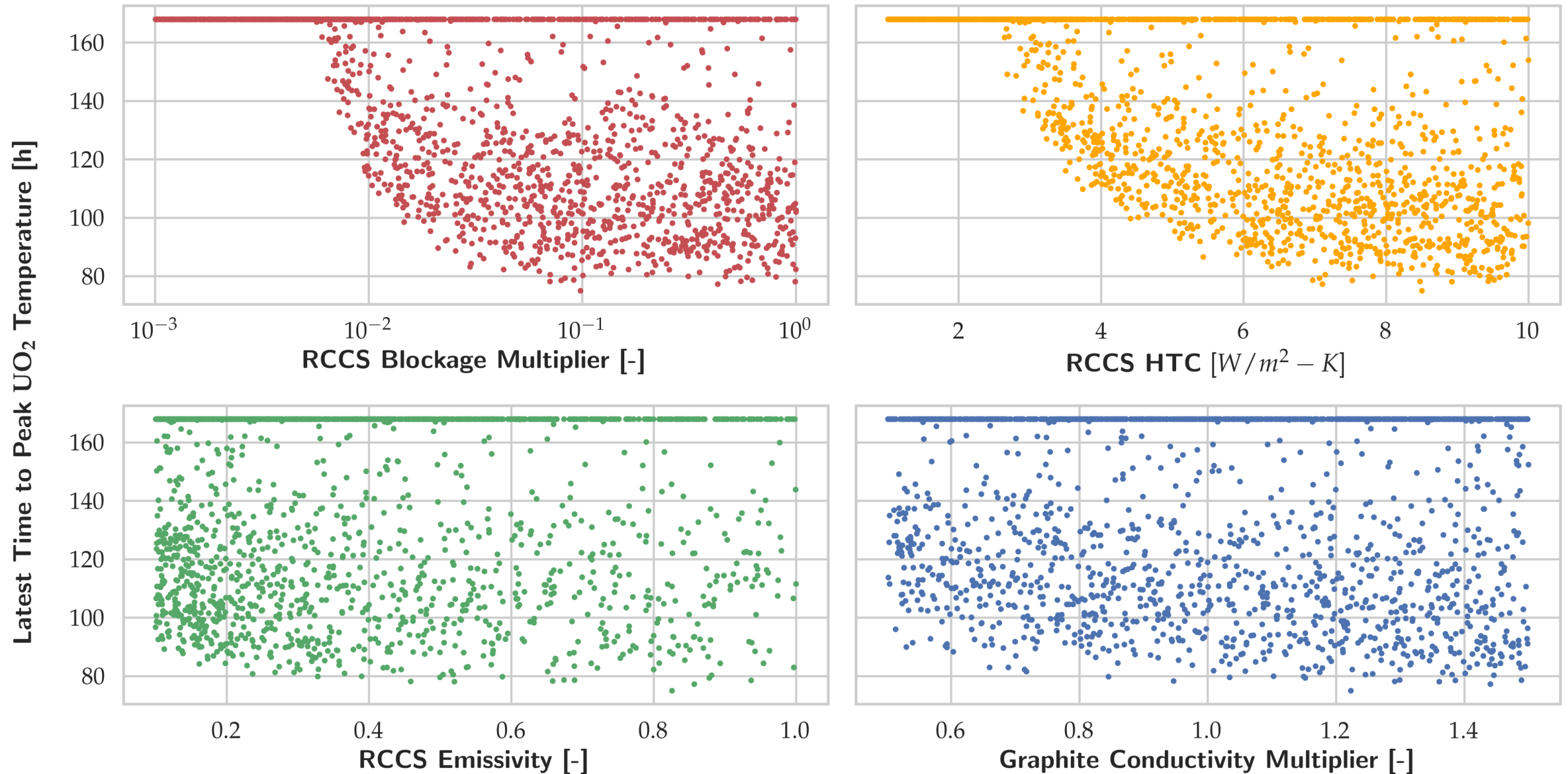
Tails of realizations contributing to longer term growth of TRISO particle failures

50th percentile reasonably stable in the long-term

Rapid growth in failure fraction driven by the early temperature excursion

Lower rates of failure entirely driven by early temperature excursion
Variability in peak fuel temperature and cooldown transient dominates higher failure rate realizations

Role of Decay Heat Rejection – Latest Time to Peak Fuel Temperature



Role of Decay Heat Rejection – Peak Fuel Temperature

