

Slip Transmission and Voiding during Slip Band Intersections in $\text{Fe}_{70}\text{Ni}_{10}\text{Cr}_{20}$ Stainless Steels



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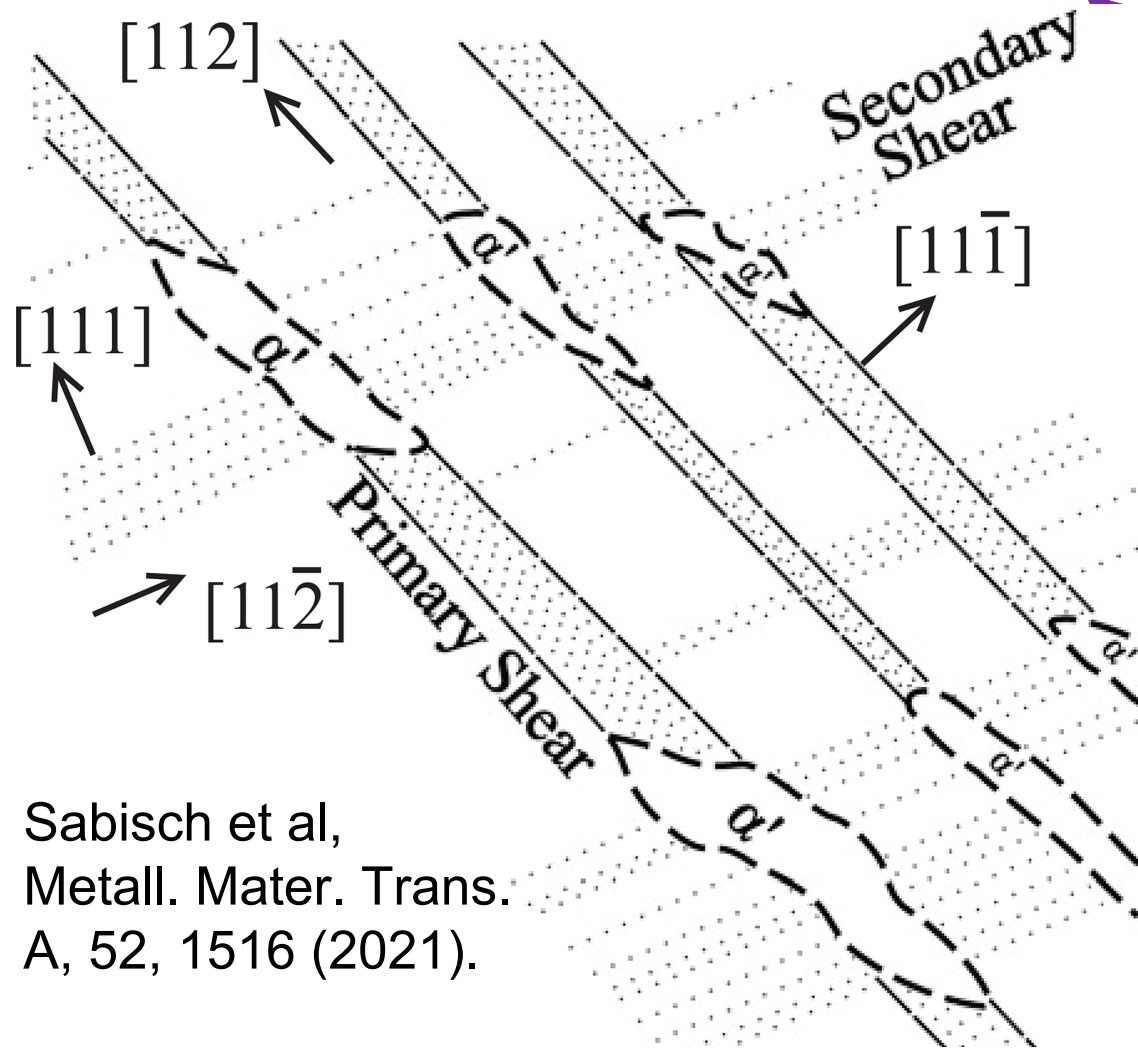
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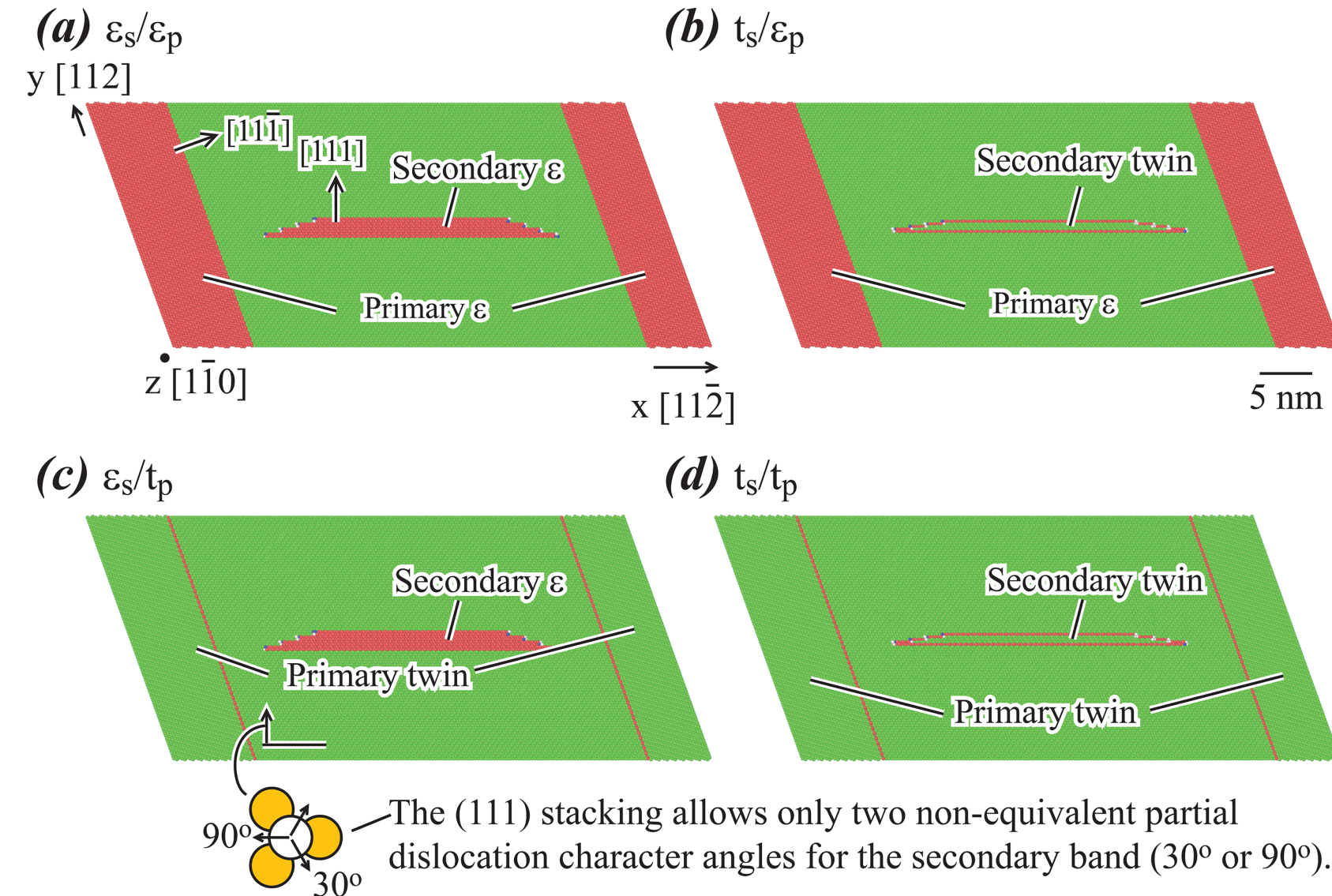
Experimental Observations in Fe-Ni-Cr Stainless Steels



- ☐ Deformation features slip
- ☐ bands
- ☐ hydrogen promotes ϵ -

- ☐ Slip bands contain twins / ϵ -
- ☐ martensite
- ☐ martensite at band

Eight Possible Band Intersections



- Four band combinations ϵ_s/ϵ_p , t_s/ϵ_p , ϵ_s/t_p , and t_s/t_p exist, where α_s/β_p represents secondary band α_s hitting primary band β_p ($\alpha, \beta = \epsilon$ or t for twin);
- Each secondary band has 30° and 90° dislocation character angles;

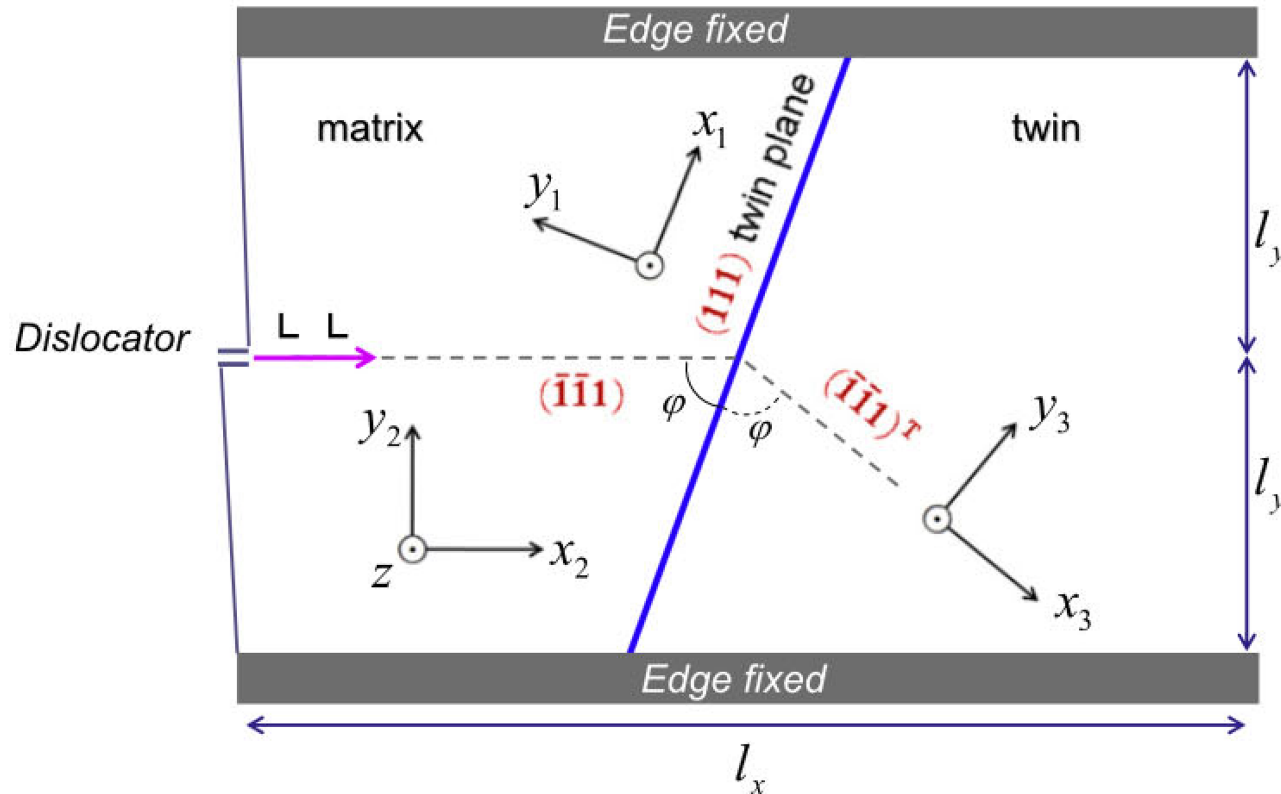
Questions

- ❑ What is the slip transmission propensity order for the eight band intersection processes?
- ❑ What is the voiding propensity order for the eight band intersection processes?
- ❑ Why the ε -martensite becomes α' -martensite when a secondary band penetrates an ε -band?
- ❑ We perform molecular dynamics (MD) simulations to answer these questions.

Literature MD Simulations

Single Dislocation / Twin Interaction

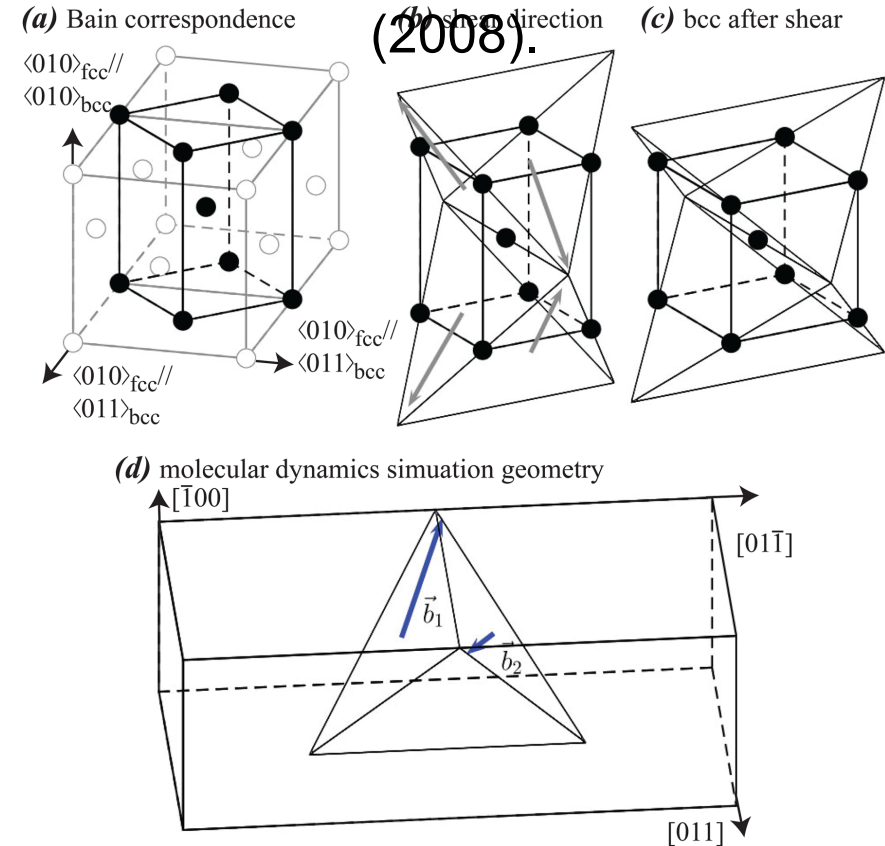
Jin et al, Acta Mater. 56, 1126
(2008).



- ❑ Do not study slip band intersections;

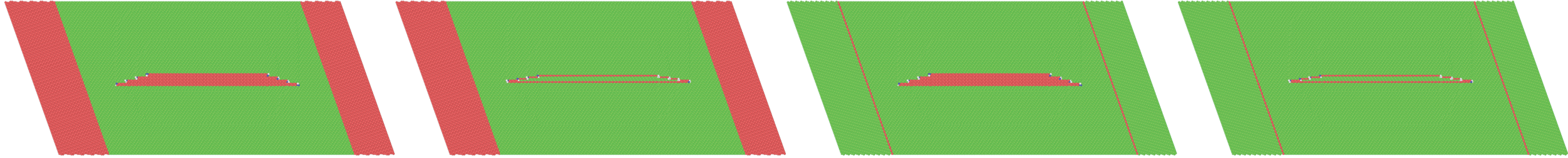
α' (bcc) Formation

Sinclair et al, Acta Mater. 56, 4160
(2008).



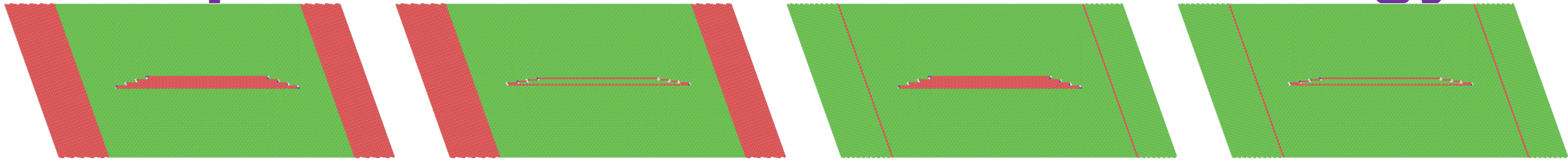
- ❑ Enforce artificial shear;
- ❑ Predict wrong orientation

Unique Features of Our MD Simulations



- ❑ Use non-orthogonal cells to enforce fully periodic boundary conditions to eliminate artificial surface effects that are present in previous studies;
- ❑ Explore all eight possible slip band intersections;
- ❑ Identify propensity of both slip transmission and interfacial voiding;
- ❑ Predict α' formation without manual constraints.

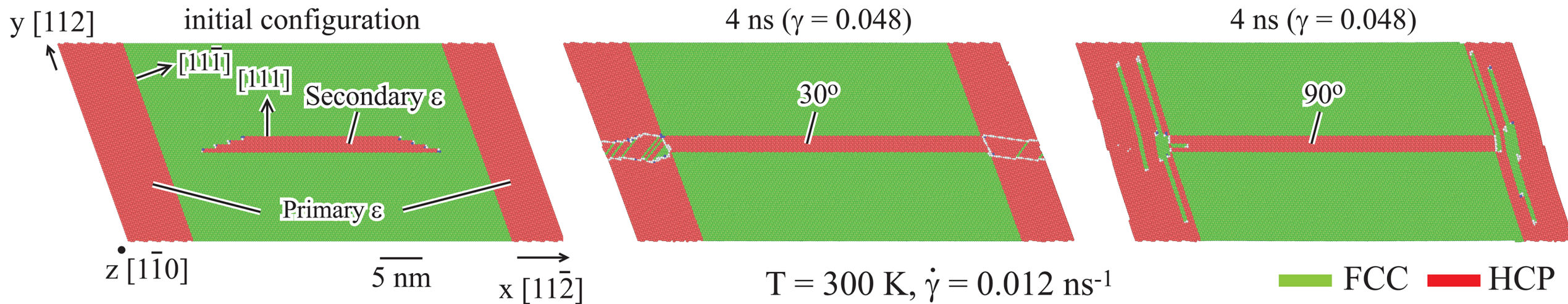
Slip Transmission MD Methodology



- ❑ Use NVT (constant volume) ensemble;
- ❑ Perform simulations at 300 K for 8 ns;
- ❑ Apply shear strain-controlled method at a shear strain rate of 0.012 /ns with the shear direction parallel to the Burgers vector;
- ❑ The shear strain rate is modeled in segments: a 0.00192 instantaneous shear strain is applied every 0.16 ns to enable time-averaged shear stress to be calculated for each segment;

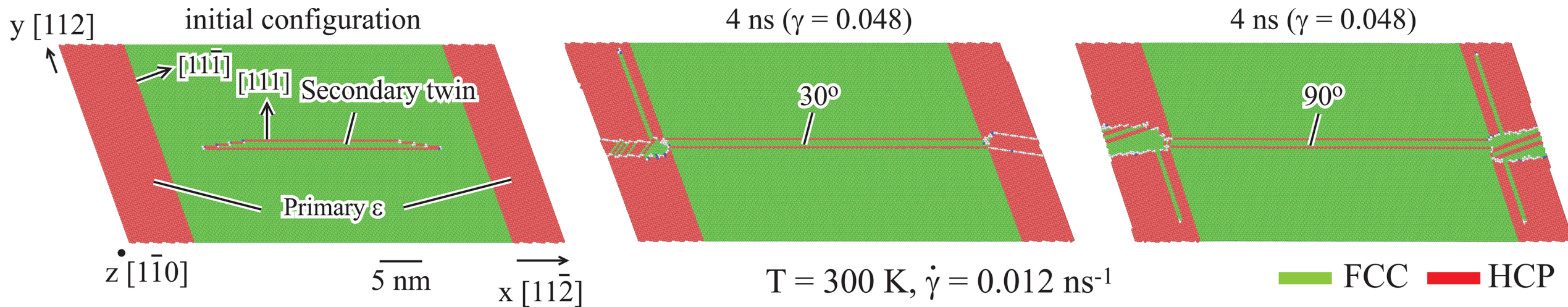
❑ All data are collected and analyzed using the LAMMPS software.

ϵ -to- ϵ Transmission



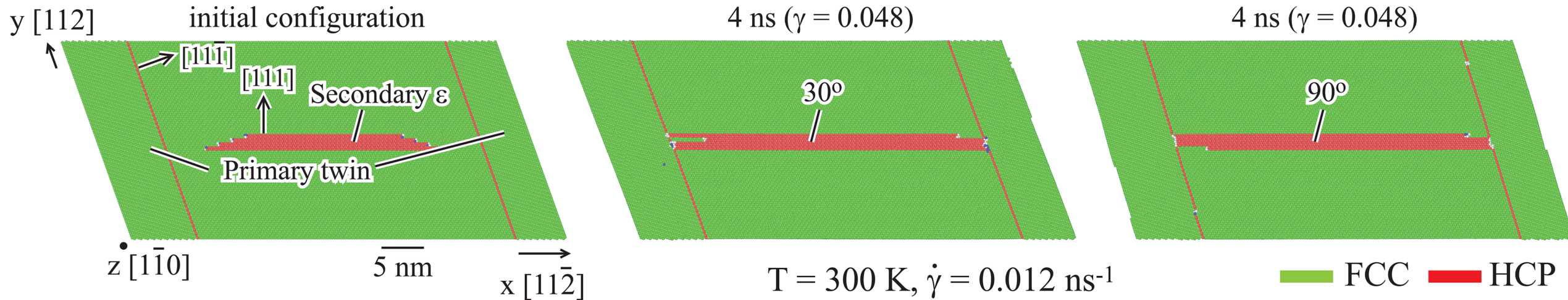
- Our MD algorithm is able to capture the expansion of the secondary ϵ -band and its collision with the primary ϵ -band;
- Regardless of the character angle (30° , 90°), the secondary ϵ -band is seen to transmit into the primary ϵ -band at a shear strain of 0.048;
- The transmission mode depends on the character angle

Twin-to- ϵ Transmission



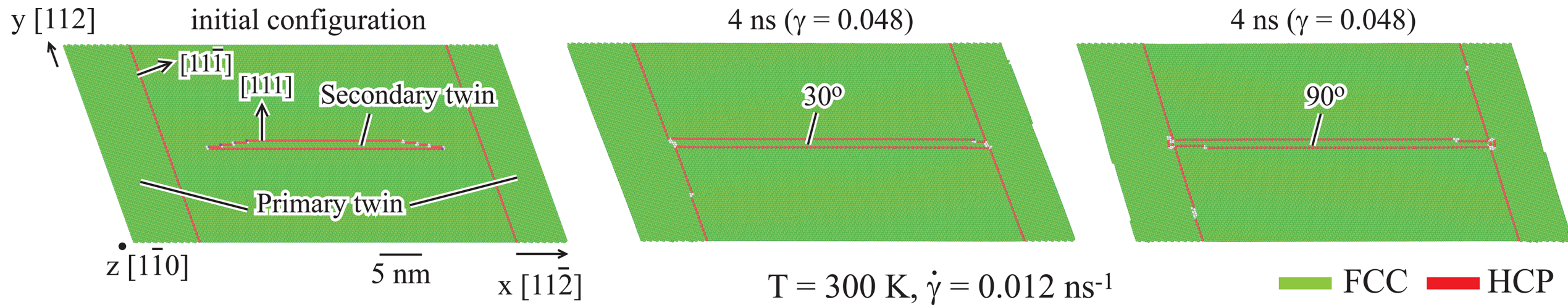
- ❑ Our MD algorithm is able to capture the expansion of the secondary twin-band and its collision with the primary ϵ -band;
- ❑ Regardless of the character angle (30°, 90°), the secondary twin-band is seen to transmit into the primary ϵ -band at a shear strain of 0.048;
- ❑ The transmission mode depends on the character angle

ϵ -to-Twin Transmission



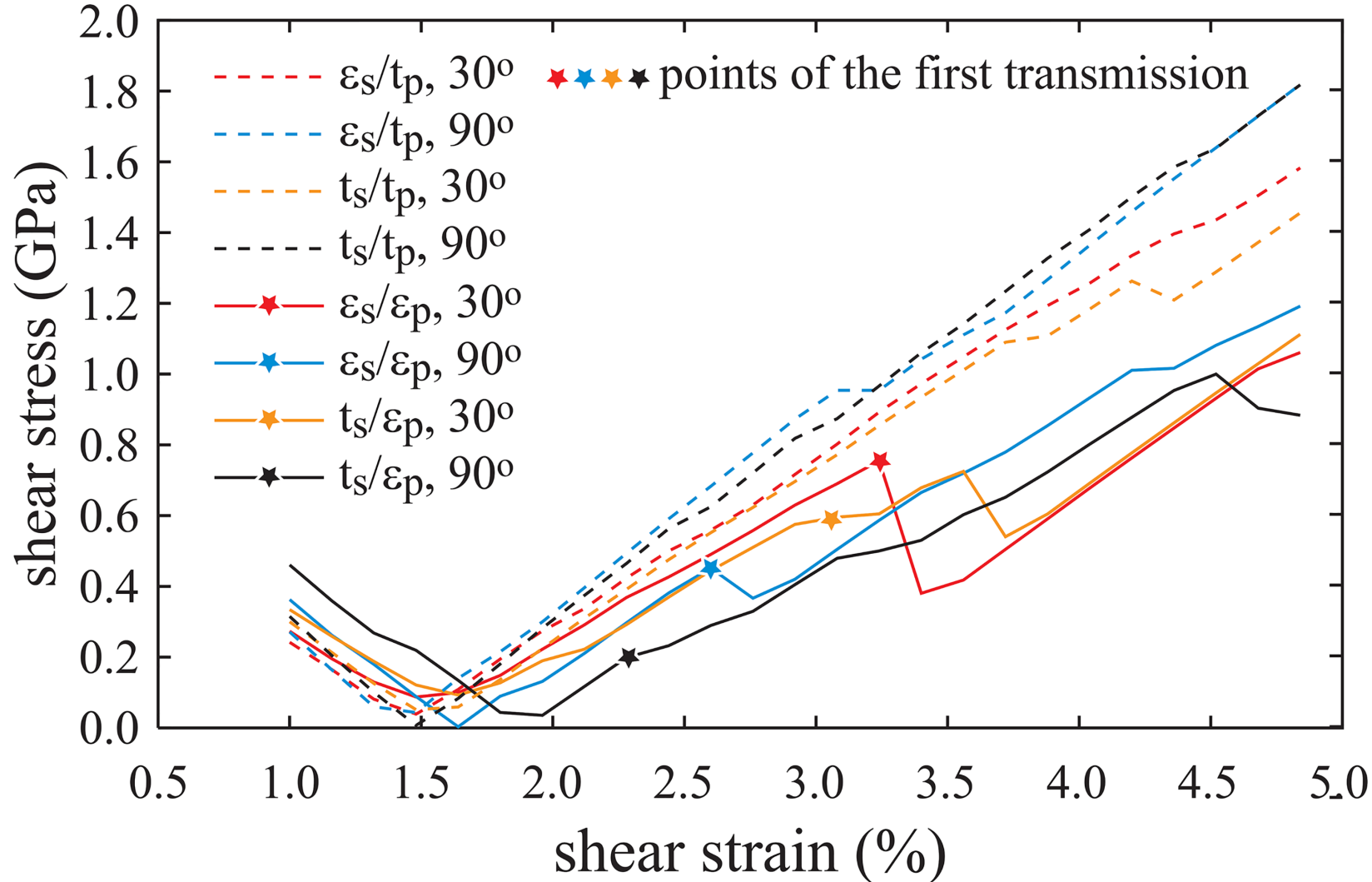
- ❑ Our MD algorithm is able to capture the expansion of the secondary ϵ -band and its collision with the primary twin-band;
- ❑ Regardless of the character angle (30°, 90°), the secondary ϵ -band is seen to be unable to transmit into the primary twin-band at the shear strain of 0.048.

Twin-to-Twin Transmission



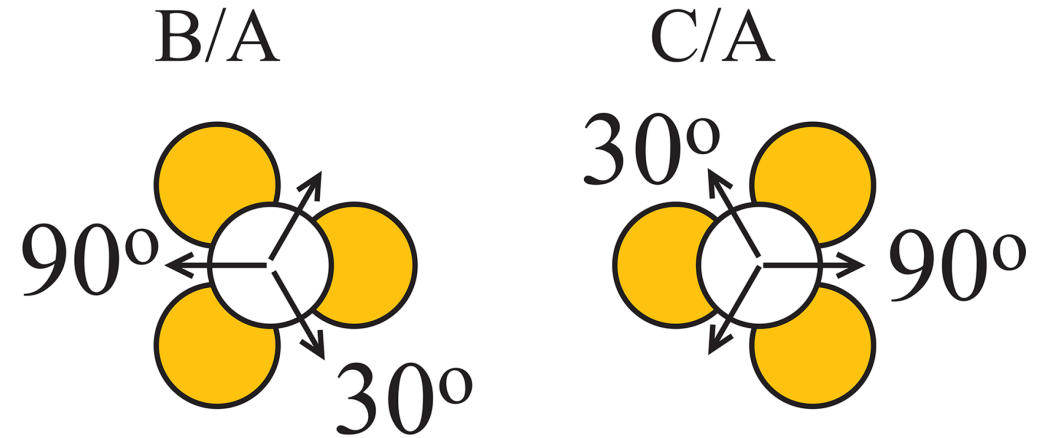
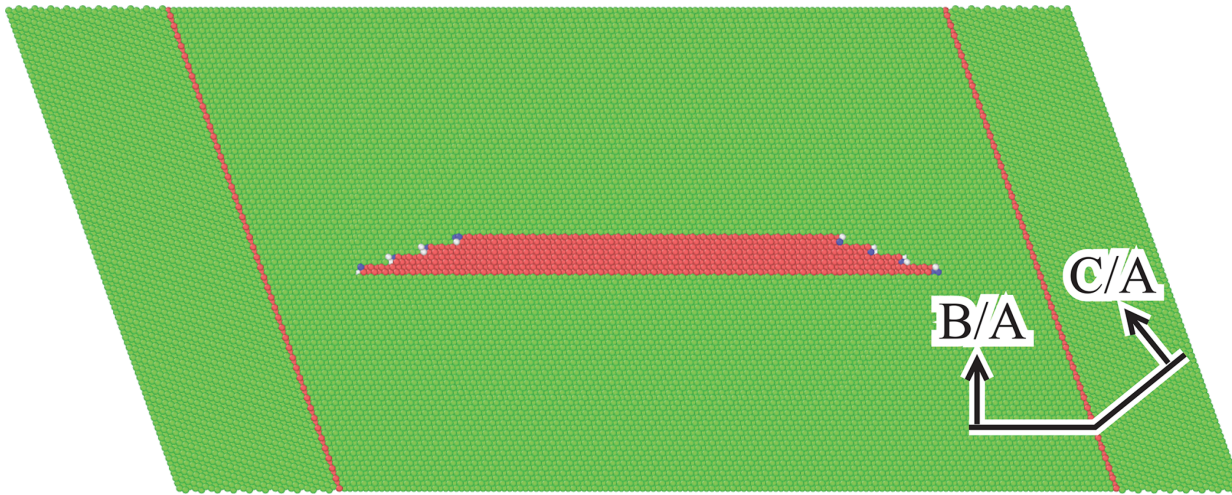
- ❑ Our MD algorithm is able to capture the expansion of the secondary twin-band and its collision with the primary twin-band;
- ❑ Regardless of the character angle (30° , 90°), the secondary twin-band is seen to be unable to transmit into the primary twin-band at the shear strain of 0.048.

Stress-Strain Curves for all 8 Intersections



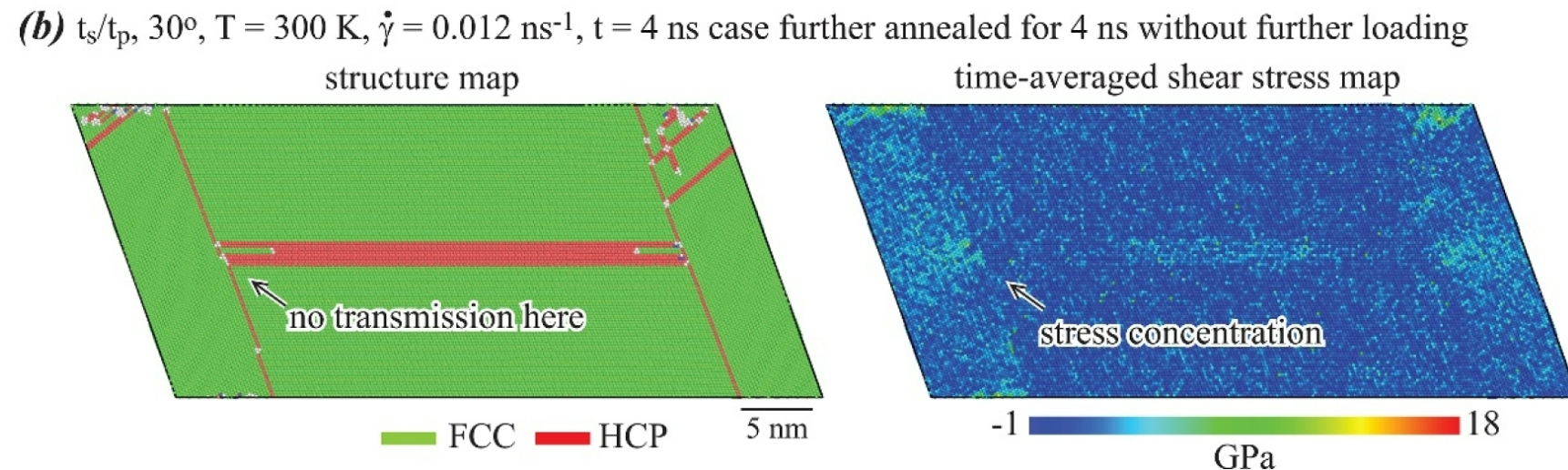
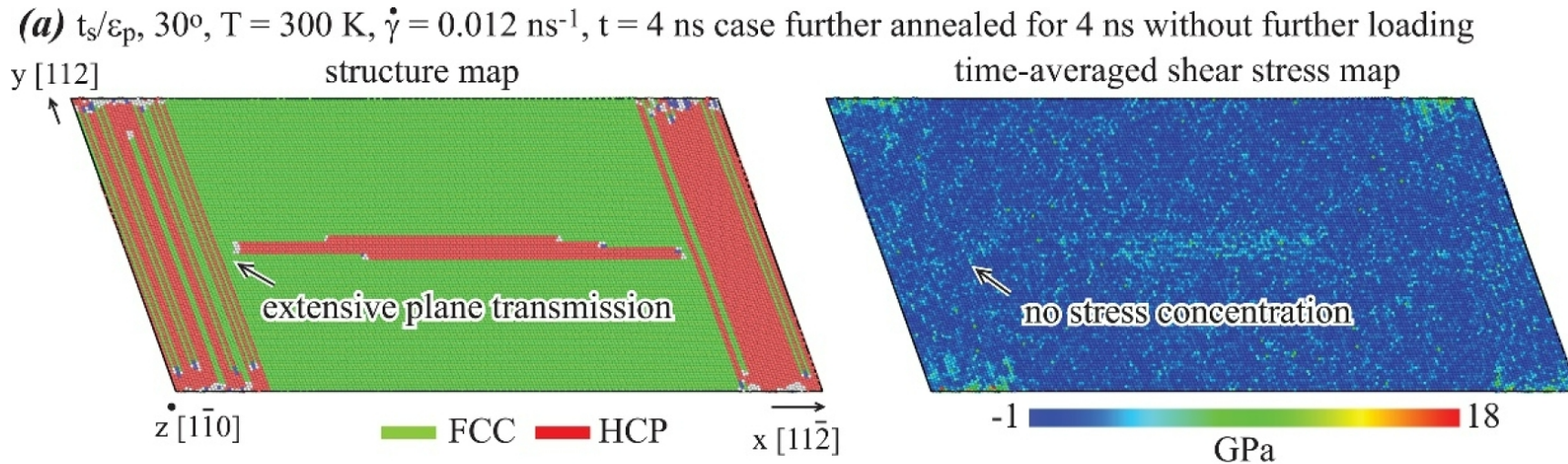
- Regardless of the secondary band type, intersection with ϵ -band produces lower stresses;
- The stress drops correlate well with transmission events;
- Transmission into ϵ -band is easier than into t -band;

Transmission Pathways into twin



- ❑ The $\{111\}$ stacking in matrix and twin regions is B-on-A (B/A) or C-on-A (C/A) respectively;
- ❑ Top-views of stackings indicate that the Burgers vectors of partial dislocations in B/A and C/A stackings are anti-aligned;
- ❑ The lack of more aligned slip pathways accounts for the difficulties to transmit into twin-bands.

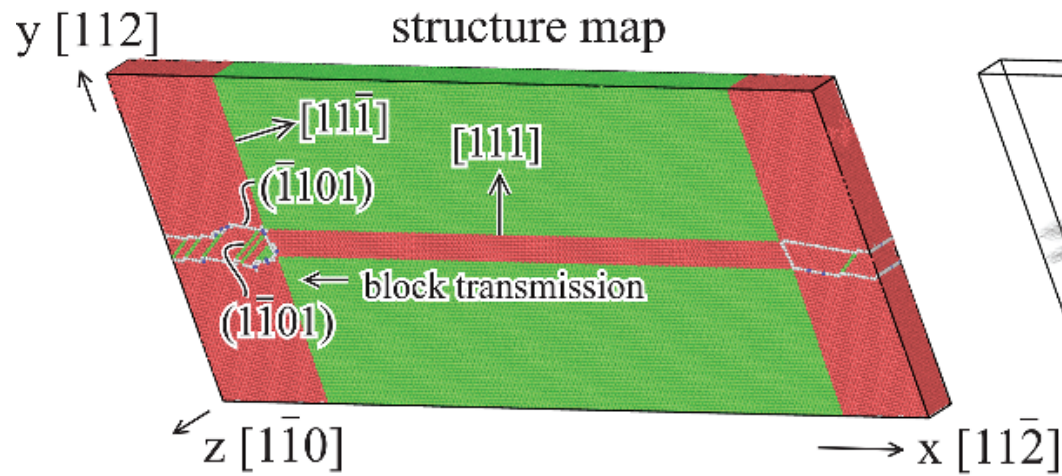
Stress Concentration



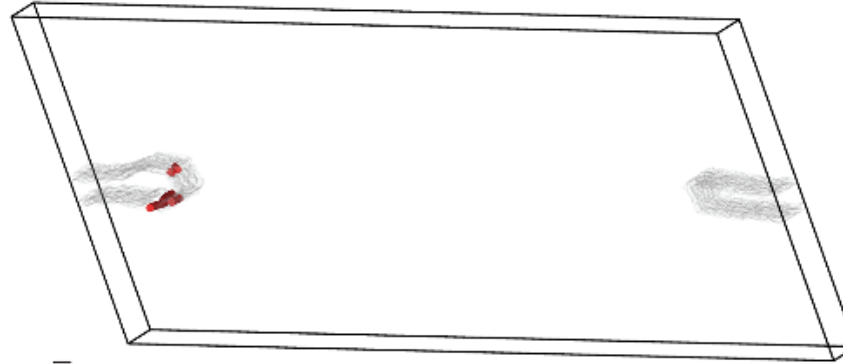
- ☐ Hitting ε bands causes no stress concentration;
- ☐ Hitting twin bands causes stress concentration;
- ☐ These agree with slip pile-ups and transmission.

Transmission Mechanisms

(a) ϵ_s/ϵ_p 30° at 300 K, 2.56 ns ($\dot{\gamma} = 0.012 \text{ ns}^{-1}$) showing block transmission



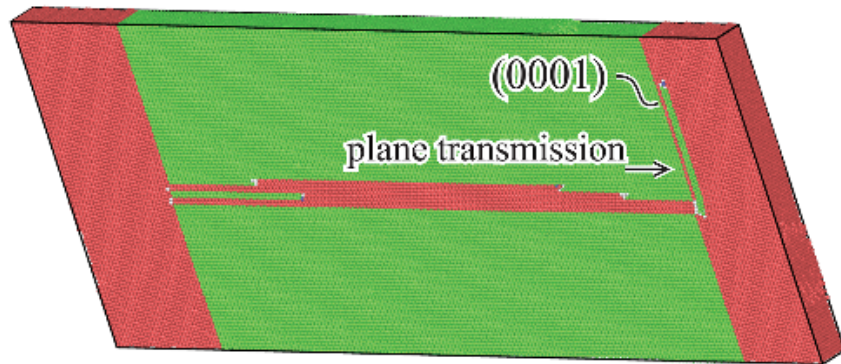
HCP dislocation map



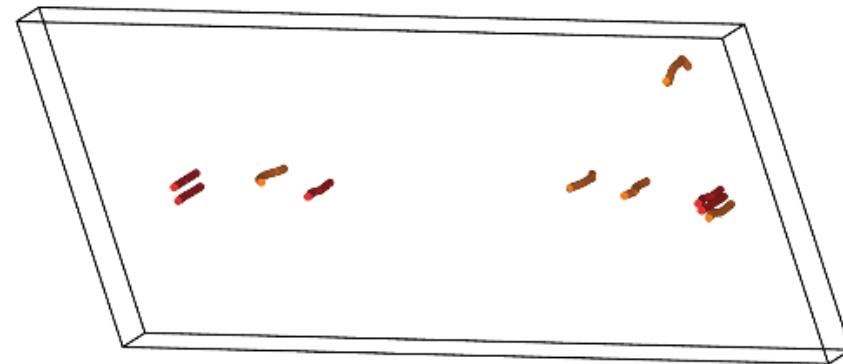
□ Slip transmission occurs through plane and block mechanisms;

(b) ϵ_s/ϵ_p 90° at 300 K, 1.12 ns ($\dot{\gamma} = 0.012 \text{ ns}^{-1}$) showing slip transmission

structure map



HCP dislocation map



□ Both mechanisms involve migration of dislocation;

■ FCC ■ HCP

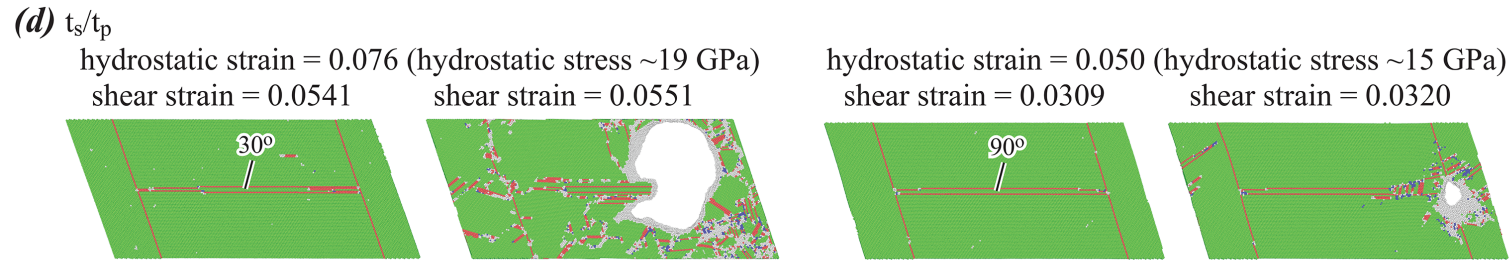
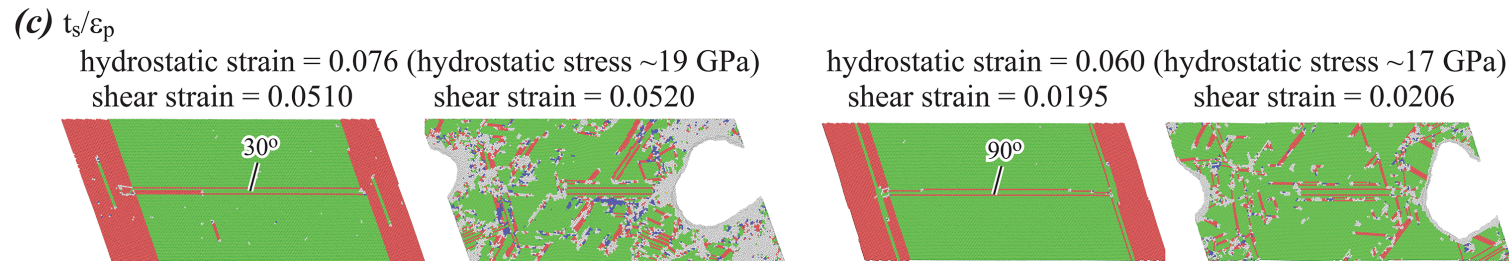
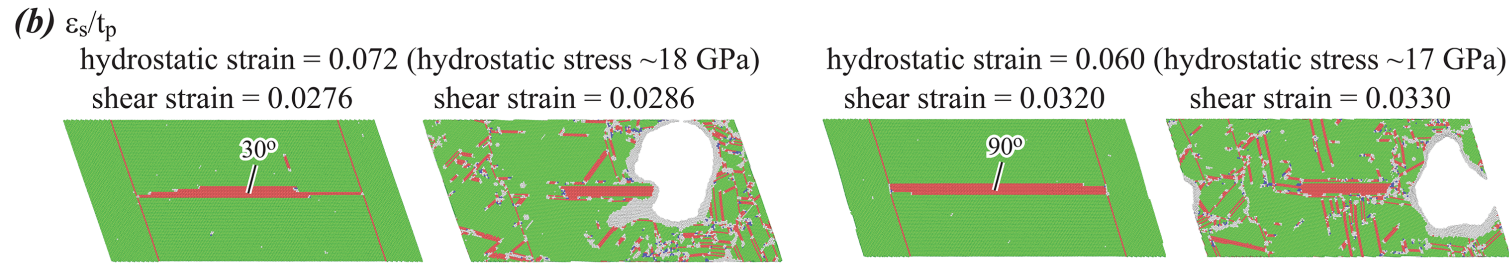
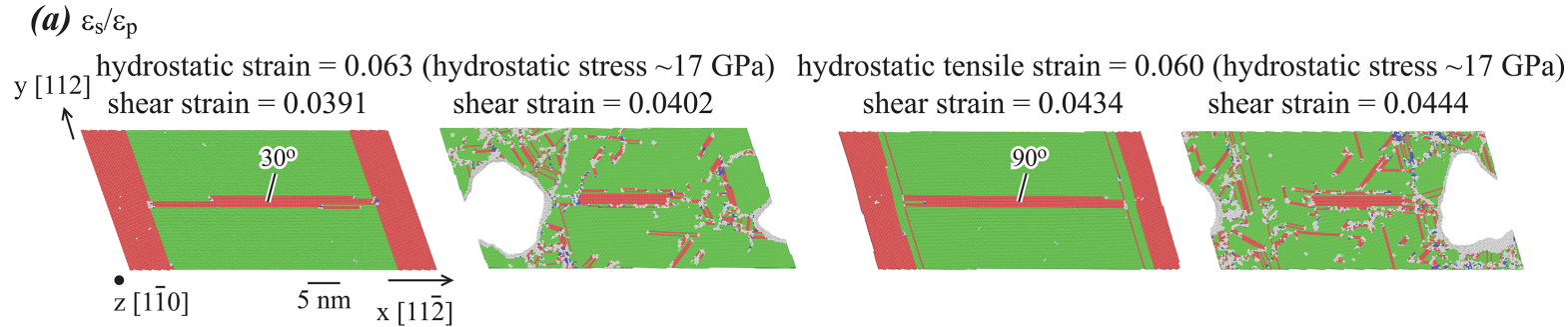
— $b = \langle 1\bar{1}00 \rangle / 3$ — unidentified

□ Block

Voiding MD Methodology

- ❑ MD time/length scales do not allow simulation of voiding under realistic conditions;
- ❑ Instead, we focus on identifying relative voiding propensities for the eight slip band intersection processes;
- ❑ The same shear straining simulations as used in transmission studies are used here except at a reduced strain rate of 0.006875 /ns;
- ❑ A constant hydrostatic tensile strain is added during the shear simulations to help voiding. If voiding does not occur, the tensile strain is progressively increased in small increments;
- ❑ The combination of tensile / shear strains for the onset of voiding is used to rank the relative voiding propensities.

Voiding MD Results



— FCC — HCP

$T = 300 \text{ K}, \dot{\gamma} = 0.006875 \text{ ns}^{-1}$

less difficult \longleftrightarrow more difficult

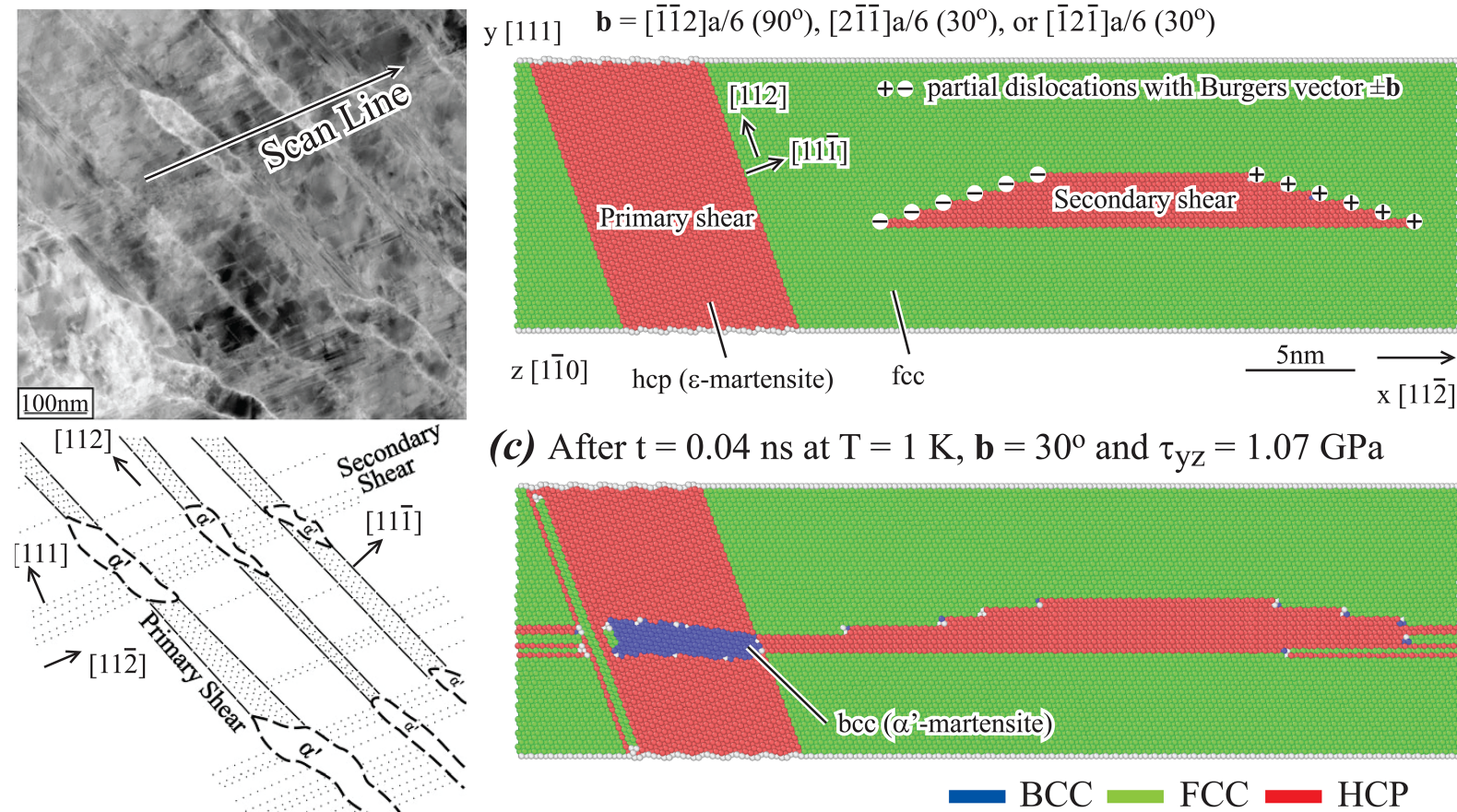
t_s/t_p-90° ϵ_s/t_p-90° $\epsilon_s/\epsilon_p-30^\circ$ t_s/ϵ_p-30°
 t_s/ϵ_p-90° $\epsilon_s/\epsilon_p-90^\circ$ ϵ_s/t_p-30° t_s/t_p-30°

❑ All voiding occurs at the band intersection interfaces;

❑ Voiding more easily occurs when the secondary band has edge dislocations.

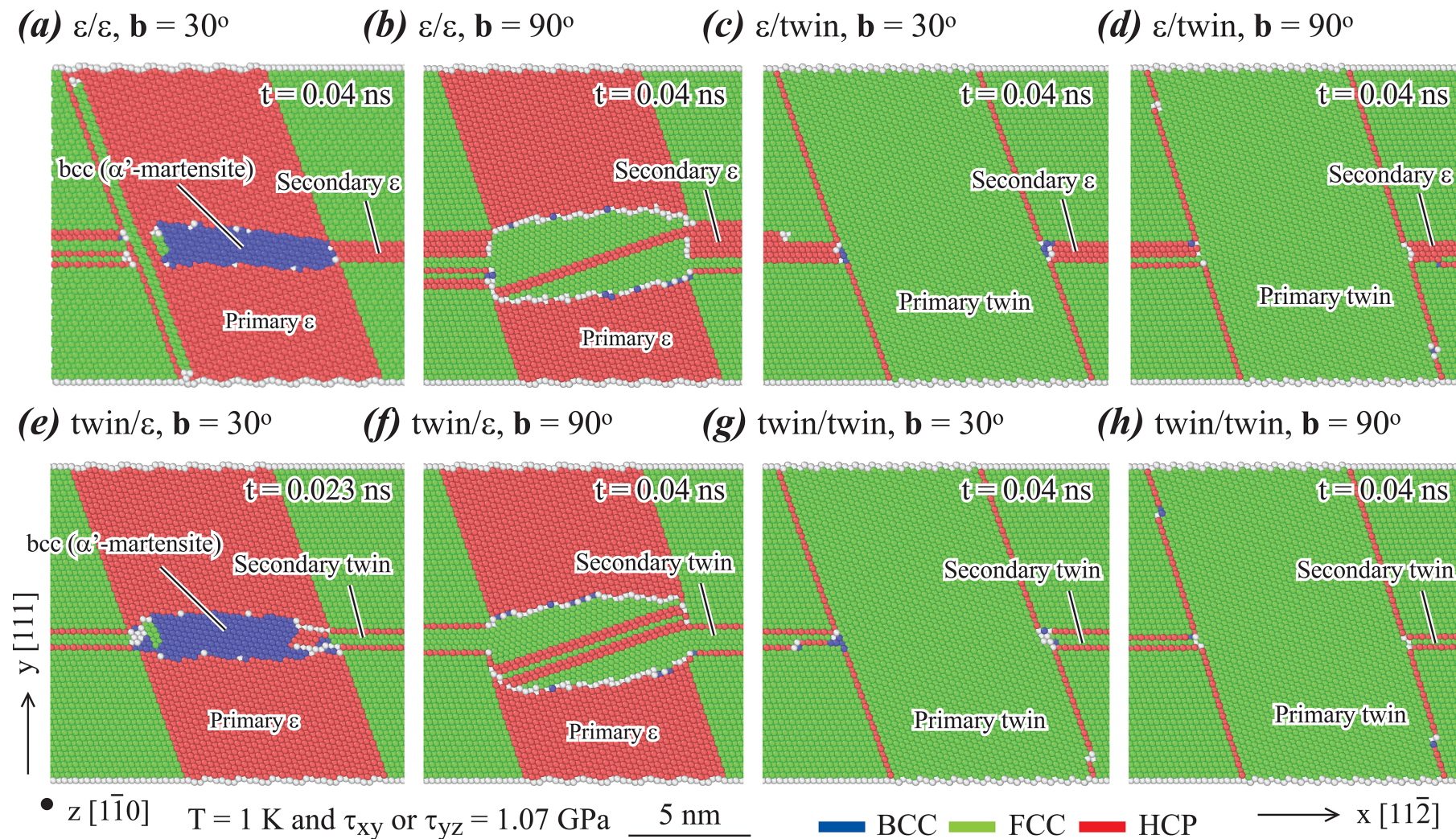
MD Prediction of α' Formation in ϵ -primary band

(a) Experimental α' formation (b) Initial MD geometry



- ❑ Other than the two slip bands inserted, our simulations do not have any constraints;
- ❑ We predict the formation of α' at ϵ_s/ϵ_p intersections;
- ❑ We find $[11\bar{1}]_\gamma // [0001]_\epsilon$
 $// [1\bar{1}0]_{\alpha'}$, $[1\bar{1}0]_\gamma // [11\bar{2}0]_\epsilon$
 $// [111]_{\alpha'}$, in agreement with experiments.

MD Prediction of α' Formation in All Eight Band Intersections



- ☐ α' always forms if the primary band is ϵ ;
- ☐ α' does not form if the primary band is not ϵ ;
- ☐ We are studying the reason for this phenomenon

SUMMARY

1. MD simulations have been used to study all eight slip band intersections in $\text{Fe}_{90}\text{Ni}_{10}\text{Cr}_{20}$ stainless steels;
2. Slip is found to transmit into ε -bands more easily than twin-bands. This is because twin bands do not provide transmission pathways;
3. Voiding always occurs at the slip intersection regions;
4. Voiding more easily occurs when the impinging (secondary) band is associated with edge dislocations rather than the 30° dislocations;
5. MD predicts α' formation when slip penetrates ε -bands. No α' formation is observed when slip penetrates twin-bands;
6. The predicted orientation relations between α' , γ , and ε agree with experiments.