

An Optimal Sensor Placement Approach for Damage Detection Under Frequency-Domain Structural Dynamics

EMI Conference 2022

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DOE-NEUP Project 19-16391: GuArDIAN: General Active Sensing for condition Assessment

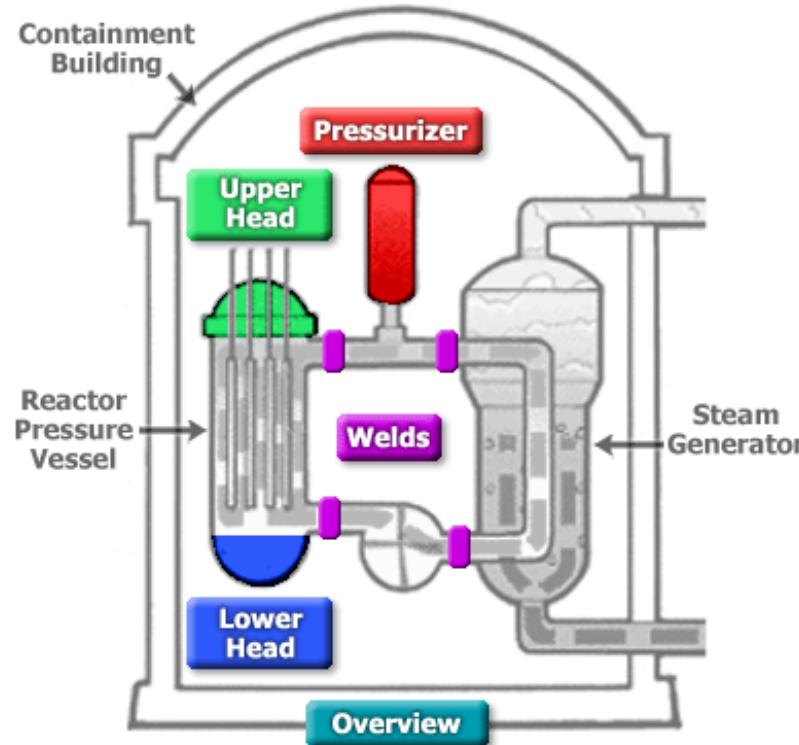
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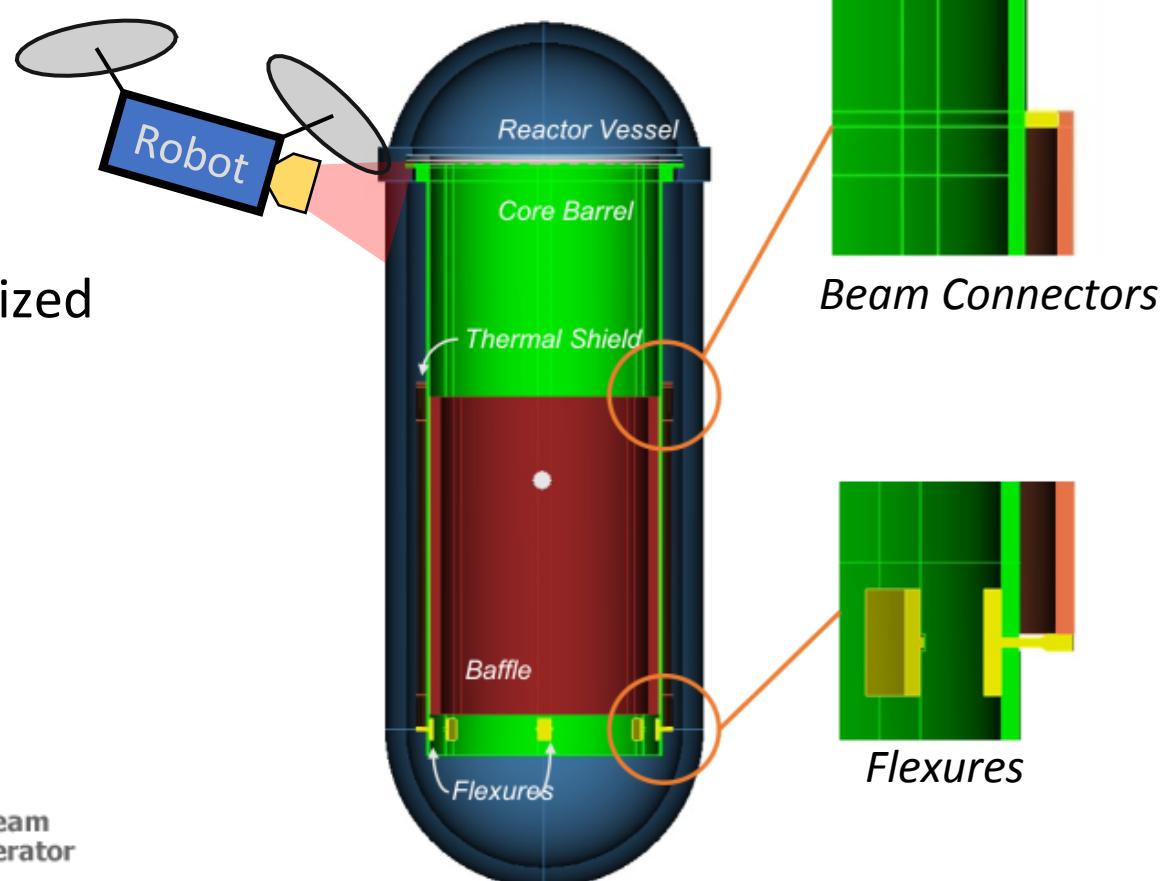
Academic Collaborators: Kavinayan Sivakumar, Michael Zavlanos, Wilkins Aquino (*Duke*)

Motivation

- Monitoring/Qualification of Pressurized Water Reactors



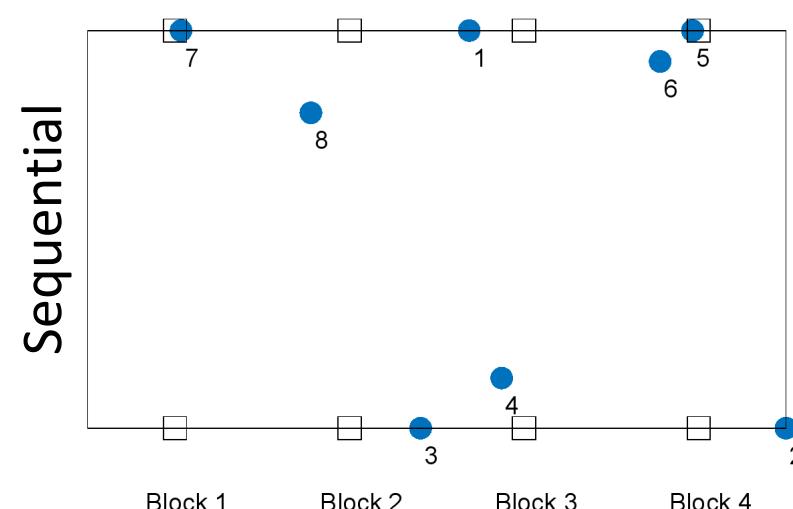
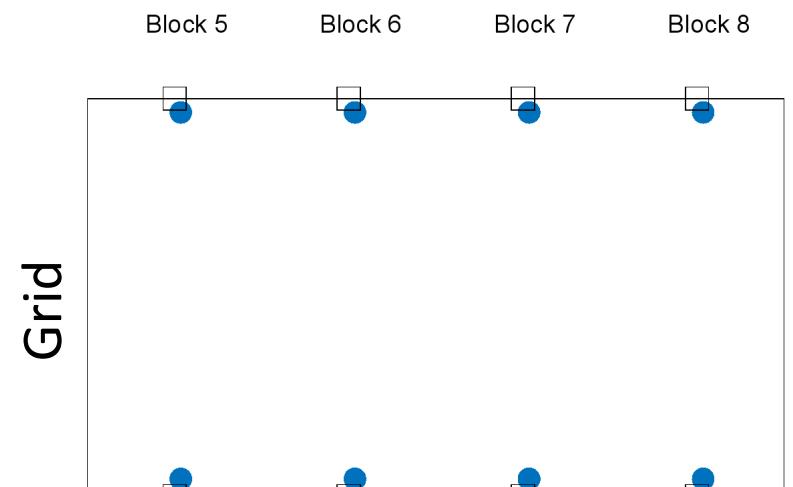
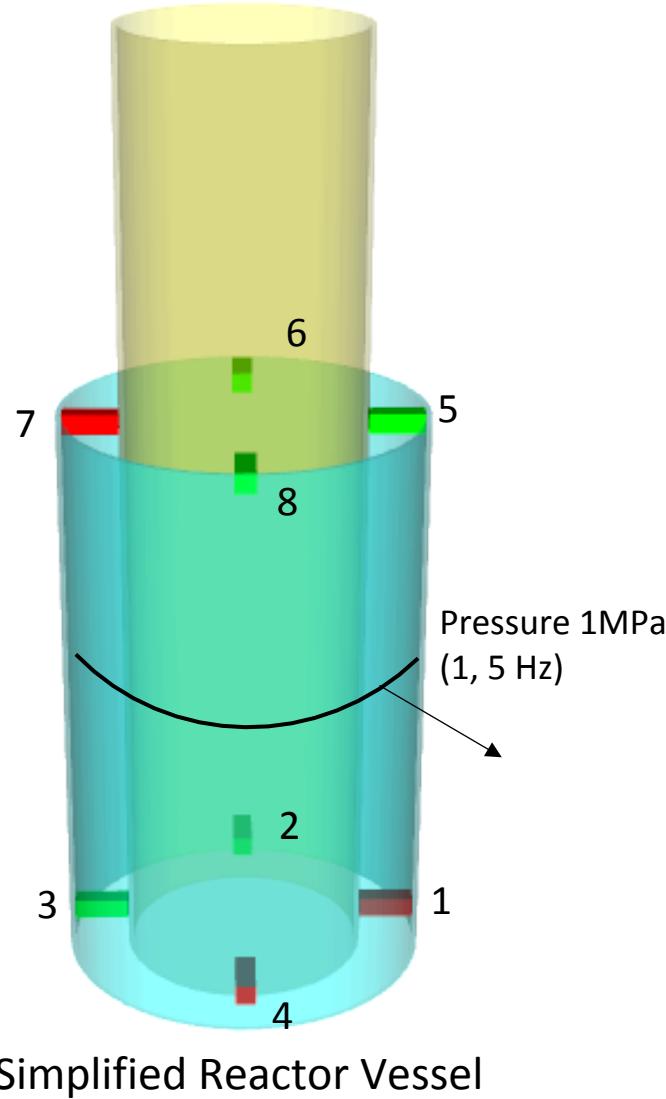
Pressurized Water Reactor (NRC.gov)



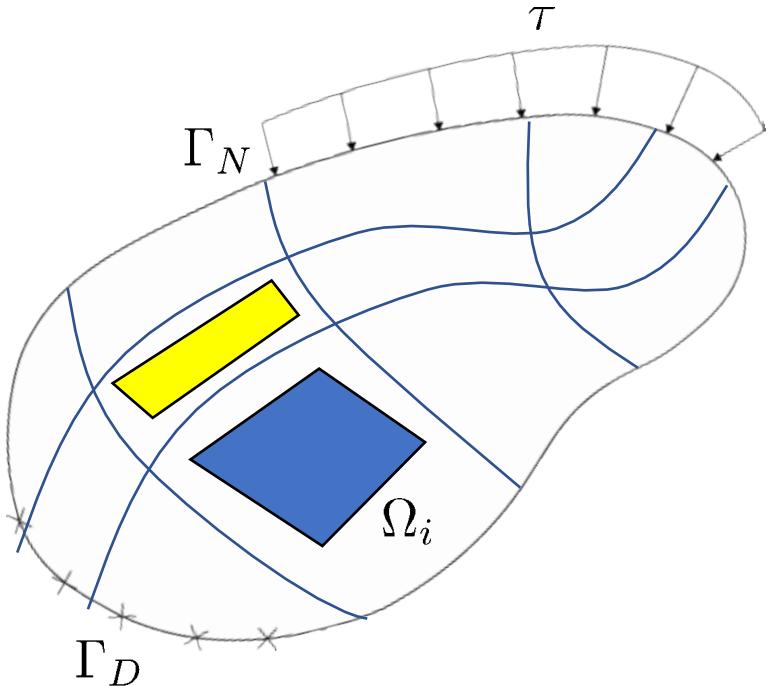
Key Components:

- Structure Modeling (forward)
- Damage Estimator (inverse)
- Optimal Experimental Design (OED)

Reactor Vessel Internals



Modeling Reactor Vessel (Forward)



Component Modeling:

$$\Omega = \bigcup_{i=1}^m \Omega_i$$

- Assume linear elasticity (frequency domain) governing PDE
- Assume simple isotropic material penalty parameter

Damage Parameter: $\theta \in [0, 1]$

Forward System:

$$\begin{aligned}[K(\theta) - \omega^2 M(\theta)]\mathbf{u} &= \mathbf{f} \\ \implies [H(\theta)]\mathbf{u} &= \mathbf{f}\end{aligned}$$

Obtaining a Damage Estimator (Inverse)

Data Model: $\mathbf{y} = H(\boldsymbol{\theta})^{-1}\mathbf{f} + \boldsymbol{\epsilon}, \quad \epsilon_i \sim \mathcal{N}(0, \sigma_i^2)$

Notation:

$\mathbf{u}, \mathbf{y}, \boldsymbol{\epsilon}, \mathbf{d} \in \mathbb{R}^n$

Observations: $Q(\mathbf{d}) = \text{diagonal matrix}; \quad d_i \in \{0, 1\}$

$Q, H \in \mathbb{R}^{n \times n}$

$\boldsymbol{\theta} \in \mathbb{R}^m$

$$\hat{\boldsymbol{\theta}} = \operatorname{argmin}_{\boldsymbol{\theta}} \frac{1}{2} \|Q(\mathbf{d})(\mathbf{u} - \mathbf{y})\|^2 + \mathcal{R}(\boldsymbol{\theta})$$

$$s.t. \quad \mathbf{g}(\mathbf{u}, \boldsymbol{\theta}) = H(\boldsymbol{\theta})\mathbf{u} - \mathbf{f} = \mathbf{0}$$

$$\boldsymbol{\theta} \in [0, 1]$$

(Aquino 2019)

Linearizing the Damage Estimation Problem

$$\begin{aligned}\hat{\boldsymbol{\theta}} &= \underset{\boldsymbol{\theta}}{\operatorname{argmin}} \frac{1}{2} \|Q(\mathbf{d})(\mathbf{u} - \mathbf{y})\|^2 + \mathcal{R}(\boldsymbol{\theta}) \\ s.t. \quad \mathbf{g}(\mathbf{u}, \boldsymbol{\theta}) &= H(\boldsymbol{\theta})\mathbf{u} - \mathbf{f} = \mathbf{0}\end{aligned}\quad \text{(Nonlinear IP)}$$

Jacobian Matrix: $\mathbf{J}(\boldsymbol{\theta})_{ij} := \frac{\partial u_i}{\partial \theta_j}$

$$\begin{aligned}\boldsymbol{\theta} &= \boldsymbol{\theta}_0 + \boldsymbol{\delta\theta} \\ \mathbf{y} &= \mathbf{y}_0 + \boldsymbol{\delta\mathbf{y}}\end{aligned}\quad \boldsymbol{\delta\mathbf{y}} = \mathbf{J}(\boldsymbol{\theta}_0)\boldsymbol{\delta\theta}$$

$$\hat{\boldsymbol{\theta}}(\boldsymbol{\theta}, \mathbf{y}) = \boldsymbol{\theta}_0 + \underset{\boldsymbol{\theta} \in \mathcal{Z}}{\operatorname{argmin}} \frac{1}{2} \|Q(\mathbf{d})(\boldsymbol{\delta\mathbf{y}} - \mathbf{J}(\boldsymbol{\theta}_0)\boldsymbol{\delta\theta})\|^2 + \frac{1}{2} \|B(\boldsymbol{\theta}_0 + \boldsymbol{\delta\theta})\|^2$$

(Linearized IP)

Least-Squares Solution: $\boldsymbol{\delta\theta} = (\mathbf{J}^T Q \mathbf{J} + B^T B)^{-1} (\mathbf{J}^T Q \boldsymbol{\delta\mathbf{y}} - B^T B \boldsymbol{\theta}_0)$

Optimal Experimental Design

- Control the **variance** in our parameters; define the Fisher Information Matrix (FIM):

$$\mathbf{FIM} := \mathbf{J}^T Q \mathbf{J}$$

- Consider an unregularized least-squares solution:

$$\text{Var}[\boldsymbol{\delta\theta}] = \text{Var}[(\mathbf{FIM})^{-1} \mathbf{J}^T Q \boldsymbol{\delta y}] = \sigma^2 \mathbf{FIM}^{-1}$$

- Employ Various Optimality Criteria: A, D, E criteria
(Tenorio 2010)

$$\begin{aligned} \operatorname{argmin}_d \quad & \lambda_{\max}[\mathbf{FIM}(\mathbf{d})^{-1}] \\ \text{s.t.} \quad & 0 \leq d_i \leq 1 \\ & \mathbf{1}^T \mathbf{d} = 1 \end{aligned}$$

Sequential OED (SOED) Algorithm

Algorithm 1 Sequential Optimal Experimental Design

```
procedure SOED
2:    $k \leftarrow 0$ 
       $\epsilon_k \leftarrow 1e6, \theta_k \leftarrow \theta_0, d_k \leftarrow 0$                                  $\triangleright$  Initialize parameters
4:   while  $k < \text{MAX ITER}$  and  $\epsilon_k > \text{TOL}$  do
       $k \leftarrow k + 1$ 
6:    $d_k \leftarrow OED(\theta_{k-1})$                                                $\triangleright$  Solve OED problem
       $\theta_k \leftarrow IP(d_k)$                                                $\triangleright$  Solve Inverse problem
8:    $\epsilon_k \leftarrow \frac{\|\theta_k - \theta_{k-1}\|_2}{\|\theta_{k-1}\|_2}$                                  $\triangleright$  Stopping criterion
return  $d_k, \theta_k$ 
```

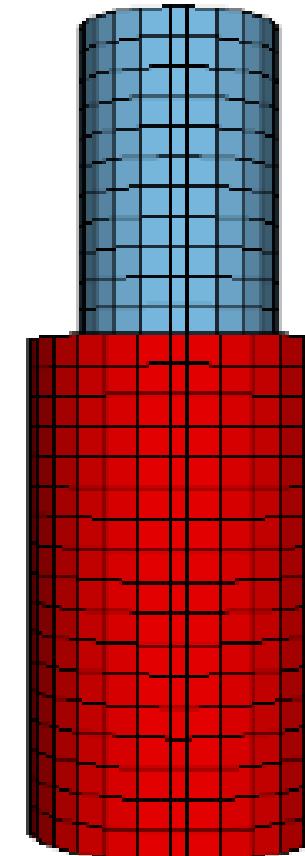
- θ_k : (estimated) damage parameters per iteration
- d_k : sensor locations (observations) per iteration

Numerical Example: Two Cylinders

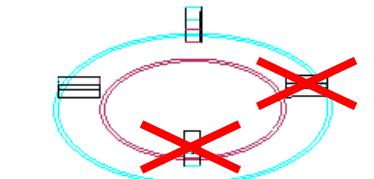
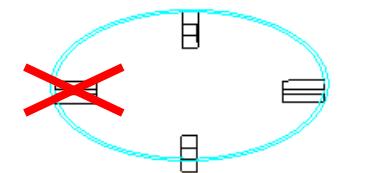
- Pressure applied on outer surface at **1 Hz**
- Inner bottom cylinder fixed; 1% Gaussian noise added
- Parameters:
 - Regularization: Double Well Potential
 - Budget: 20 Sensors
 - Number of MC trials: 30
- Metrics:

$$\text{Relative Iter Difference} := \frac{\|\theta_i - \theta_{i-1}\|_2}{\|\theta_{i-1}\|_2}$$

$$\text{Relative Solution Error} := \frac{\|\theta_i - \theta_{true}\|_2}{\|\theta_{true}\|_2}$$



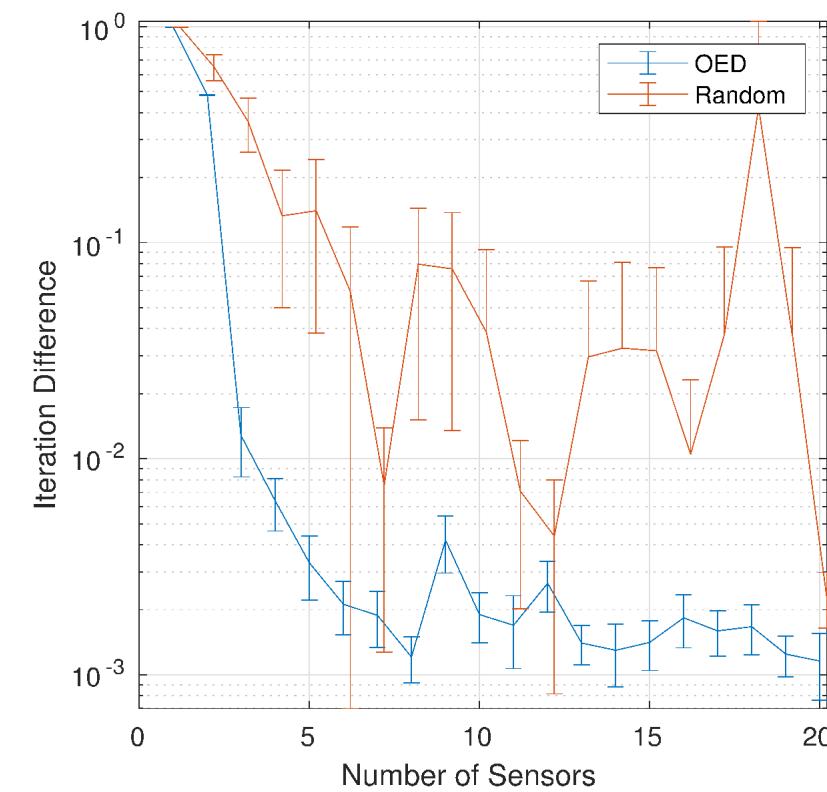
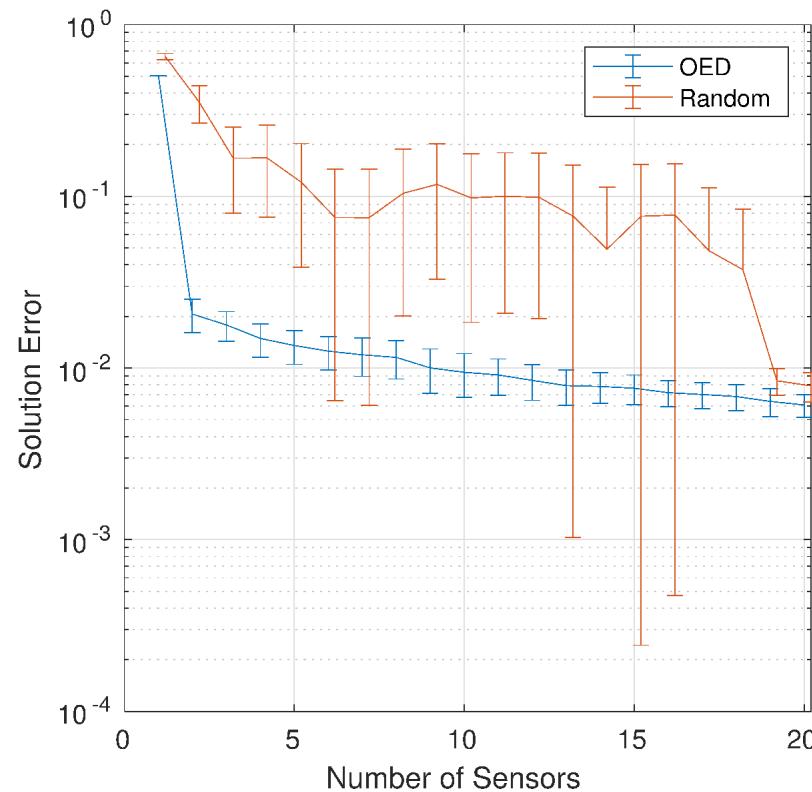
Cylinder Mesh



Example damage case

SOED Results

- Compare SOED with a random-walk sensor placement scheme



Modified Error in Constitutive Equations

- Helmholtz-type problems contain singularities (e.g. at natural frequencies) which can force damage parameter estimators to be at local minima
- Goal: Convexify the damage ID problem

$$(\mathbf{u}^*, \boldsymbol{\sigma}^*; \mathbf{C}^*) = \operatorname{argmin}_{(\mathbf{u}, \boldsymbol{\sigma}, \mathbf{C}) \in \mathcal{U} \times \mathcal{S} \times \mathcal{C}} \underline{\Pi(\mathbf{u}, \boldsymbol{\sigma}; \mathbf{C})} + \underline{\kappa \Gamma(\mathbf{u}, \boldsymbol{\sigma})}$$

Model Error: $\Pi(\mathbf{u}, \boldsymbol{\sigma}; \mathbf{C}) := \frac{1}{2} \int_{\Omega} (\boldsymbol{\sigma} - \mathbf{C} : \boldsymbol{\varepsilon}[\mathbf{u}]) : \mathbf{C}^{-1} : \overline{(\boldsymbol{\sigma} - \mathbf{C} : \boldsymbol{\varepsilon}[\mathbf{u}])} d\Omega$

Data Misfit: $\Gamma(\mathbf{u}, \boldsymbol{\sigma}) := \frac{1}{2} \|\mathbf{u} - \mathbf{y}\|^2$ (Banerjee 2013)

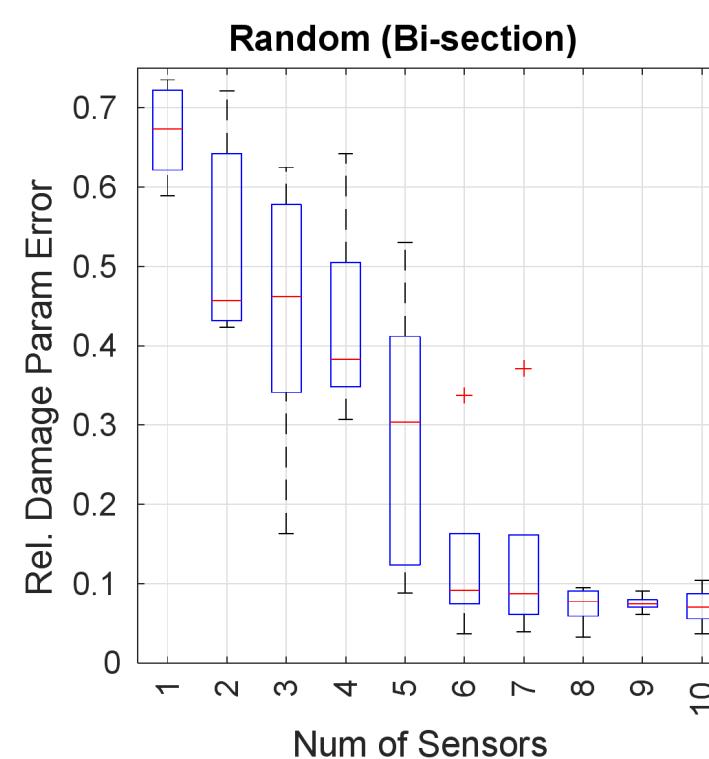
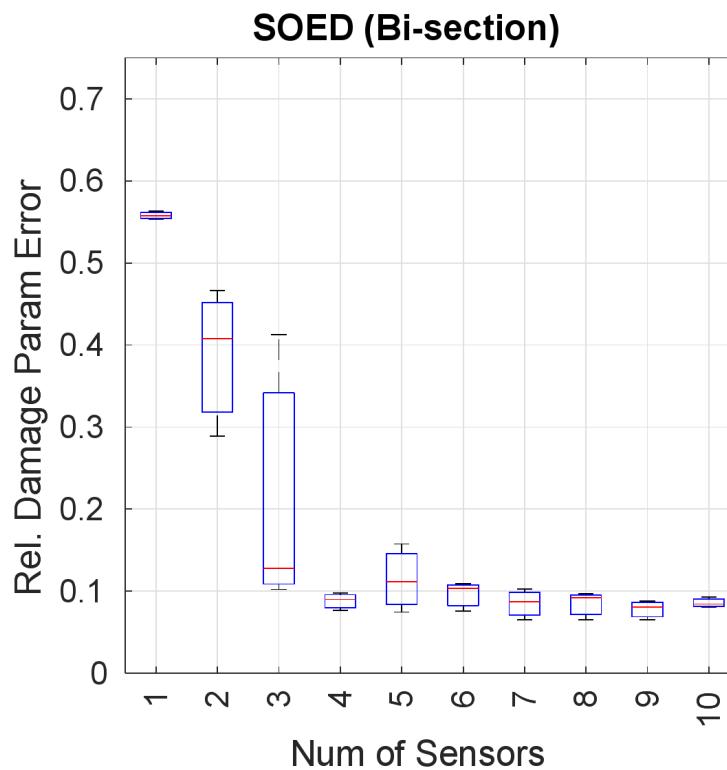
Sequential OED (SOED) Algorithm with MECE

Algorithm 2 Sequential Optimal Experimental Design with MECE

```
procedure SOED
2:    $k \leftarrow 0$ 
3:    $\epsilon_k \leftarrow 1e6, \theta_k \leftarrow \theta_0, d_k \leftarrow \mathbf{0}$                                 ▷ Initialize parameters
4:   while  $k < \text{MAX\_ITER}$  and  $\epsilon_k > \text{TOL}$  do
5:      $k \leftarrow k + 1$ 
6:      $d_k \leftarrow OED(\theta_{k-1})$                                               ▷ Solve OED problem
7:      $\theta_k \leftarrow IP\_MECE^\dagger(d_k)$                                          ▷ Solve Inverse problem (MECE)
8:      $\epsilon_k \leftarrow \frac{\|\theta_k - \theta_{k-1}\|_2}{\|\theta_{k-1}\|_2}$                                 ▷ Stopping criterion
9:   return  $d_k, \theta_k$ 
```

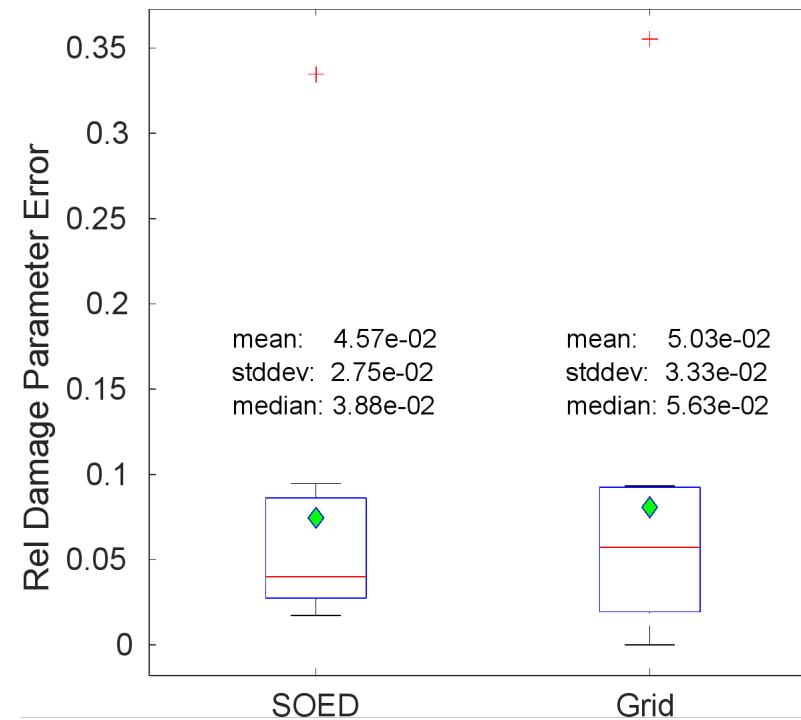
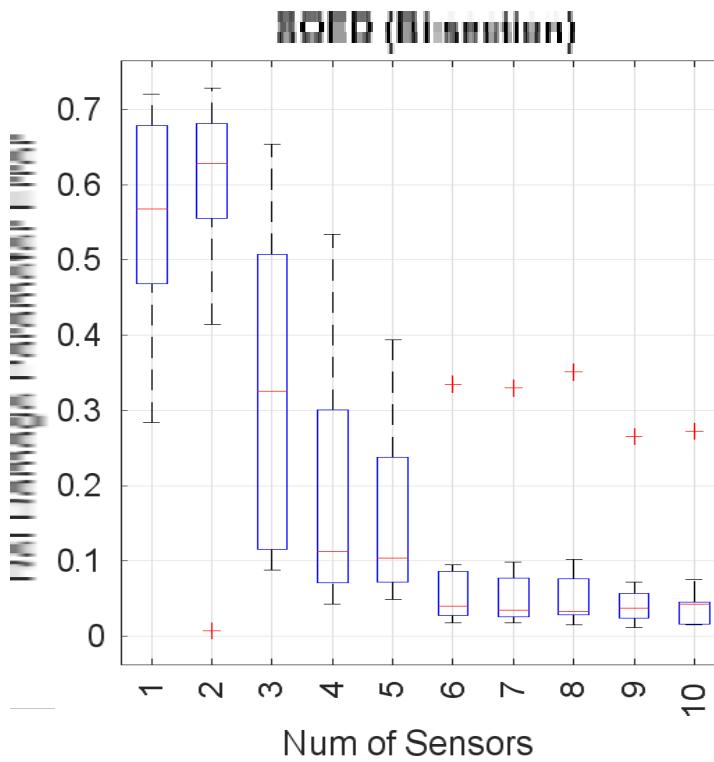
- θ_k : (estimated) damage parameters per iteration
- d_k : sensor locations (observations) per iteration
- \dagger : MECE penalty parameter chosen by bisection or continuation

SOED with MECE Performance Comparison



- Compare performance of SOED against ergodically-placed sensors
- Operating Frequency: 5Hz
- Noise Level: 5% Gaussian

SOED Performance (Multiple Damage Cases)



- 10 Damage Cases
- 5Hz Frequency
- 5% Noise
- SOED: 6 sensors
- Grid: 8 sensors at damage locations

Concluding Remarks

- Formulated a linearized damage estimator inverse problem and used a linear optimal experimental design framework (E-optimality). Created a sequential OED framework
- Enhanced the damage estimator using the Modified Error in Constitutive Equation functional
- Evaluated the sequential OED framework by considering number of needed sensors and damage estimator error
- Demonstrated that sequential OED can perform model-specific damage localization

Acknowledgements and Selected References

- DOE-NEUP Project 19-16391: GuArDIAN: General Active Sensing for condition AssessmeNt
- Chandler Smith (Sierra/Inverse) and the Sierra/SD Team for code development support
- Aquino, Wilkins, et al. ``A gradient-based optimization approach for the detection of partially connected surfaces using vibration tests." *Computer Methods in Applied Mechanics and Engineering* 345 (2019): 323-335.
- Banerjee, Biswanath, et al. "Large scale parameter estimation problems in frequency-domain elastodynamics using an error in constitutive equation functional." *Computer methods in applied mechanics and engineering* 253 (2013): 60-72.
- Horesh, Lior, Eldad Haber, and Luis Tenorio. "Optimal experimental design for the large-scale nonlinear ill-posed problem of impedance imaging." *Large-Scale Inverse Problems and Quantification of Uncertainty* (2010): 273-290.