



Rensselaer

why not change the world?®

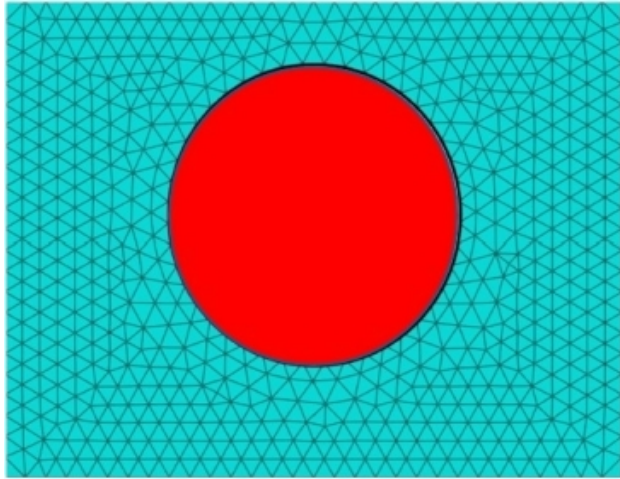
Mesh Convergence for Coupled Problems using Immersed Methods

Chen Shen¹, Scott Miller², Jesse Thomas², Lucy T. Zhang¹

¹ Department of Mechanical Aerospace and Nuclear Engineering, Rensselaer Polytechnic Institute, 12180 NY, USA

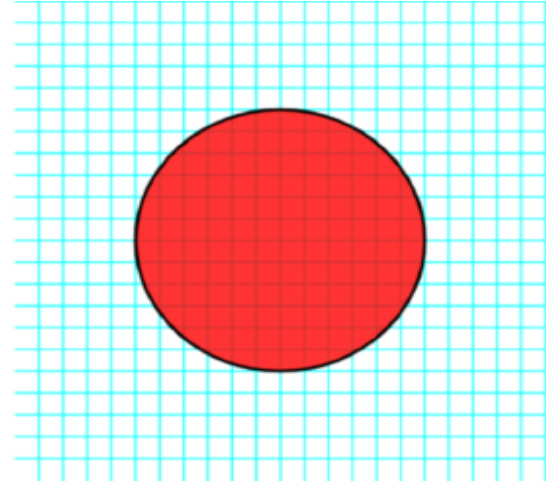
² Sandia National Laboratories, Albuquerque, 87185 NM, USA

Conforming vs non-conforming meshing techniques



Conforming mesh method:

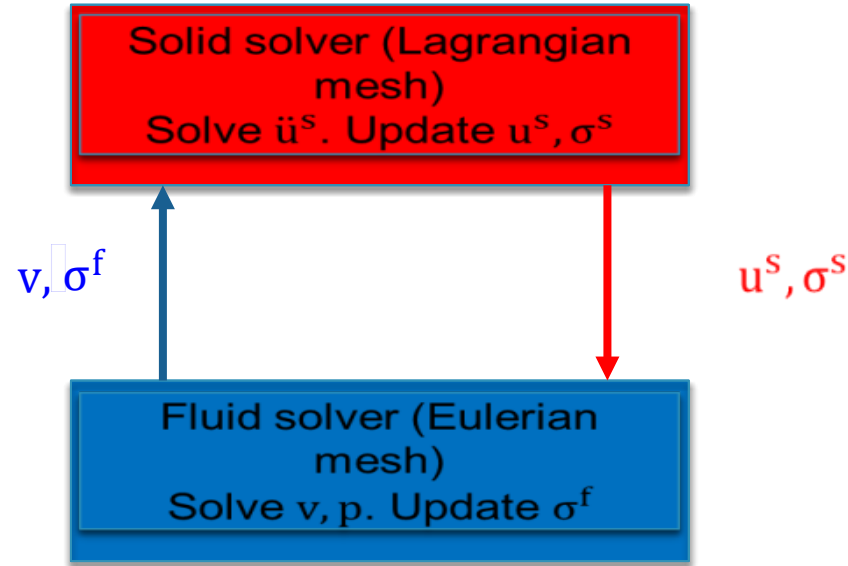
- Mesh conforming at interface
- Mesh movement incorporated into governing equations
- Needs remeshing



Non-conforming mesh method:

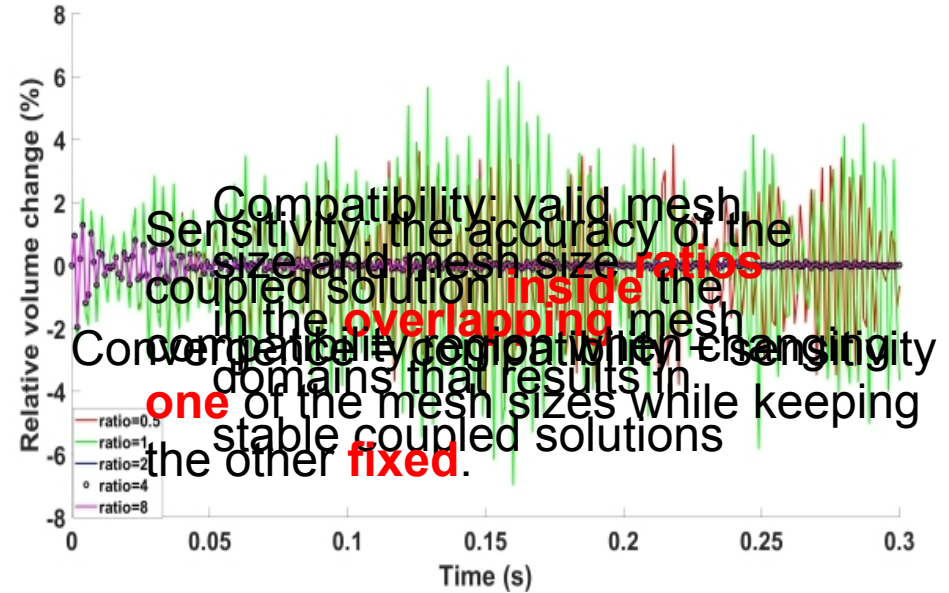
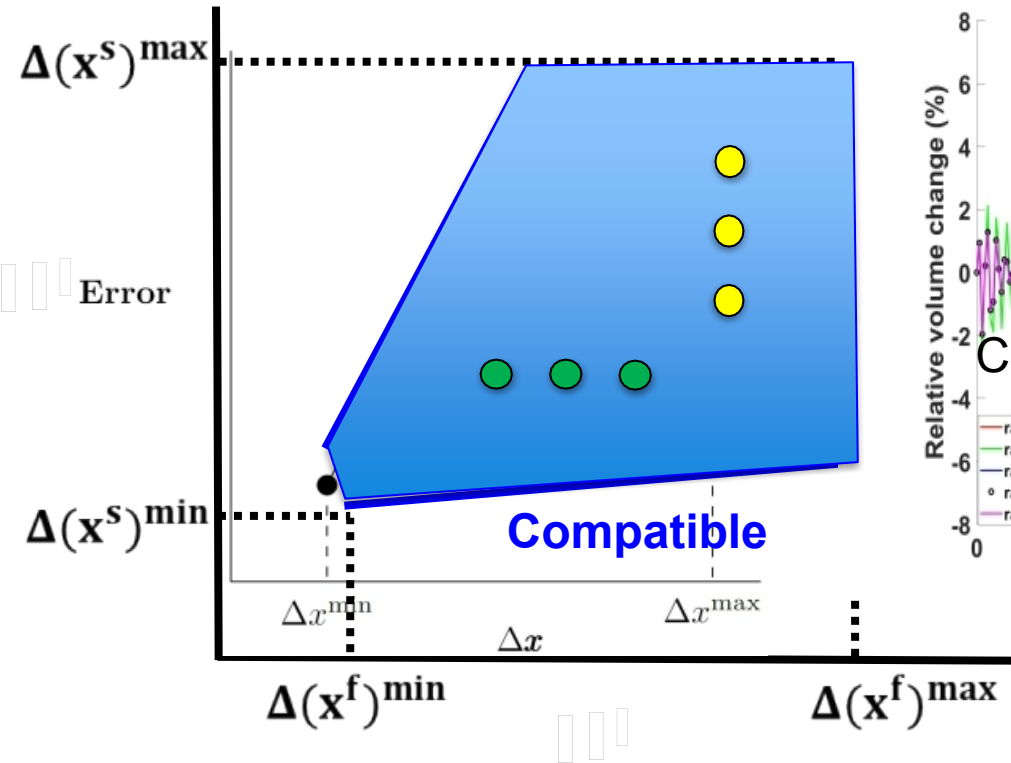
- Two independent meshes
- Data exchange through interpolation
- No remeshing, inexact interface representation

A generic algorithm for fully-coupled non-boundary-fitted meshing FSI methods



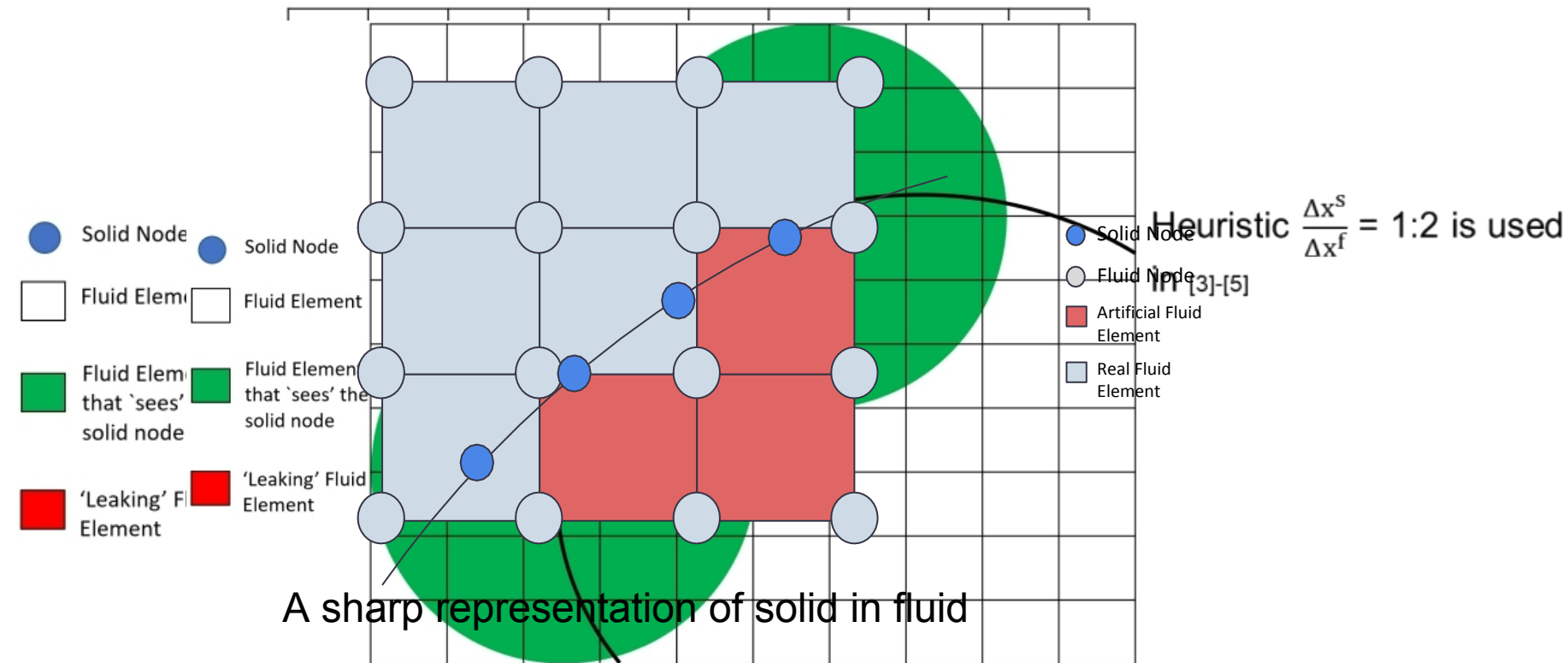
Hypothesis: Mesh size **ratio** is the dominant factor for convergence

Definition of mesh convergence for immersed methods



Check the solid volume/area conservation [1-3]

Explicit solid representation



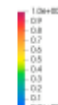
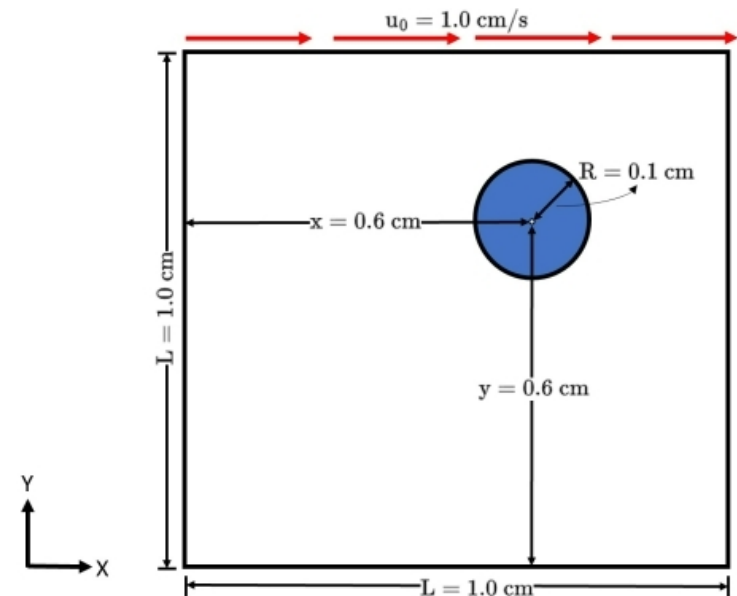
Numerical Example I: 2-D deformable solid disk driven by cavity flow^[6]

- **Fluid** (incompressible) constant velocity on the top, no-slip and no penetration on the other boundaries
- **Solid** (Neo-Hookean) free of constraints

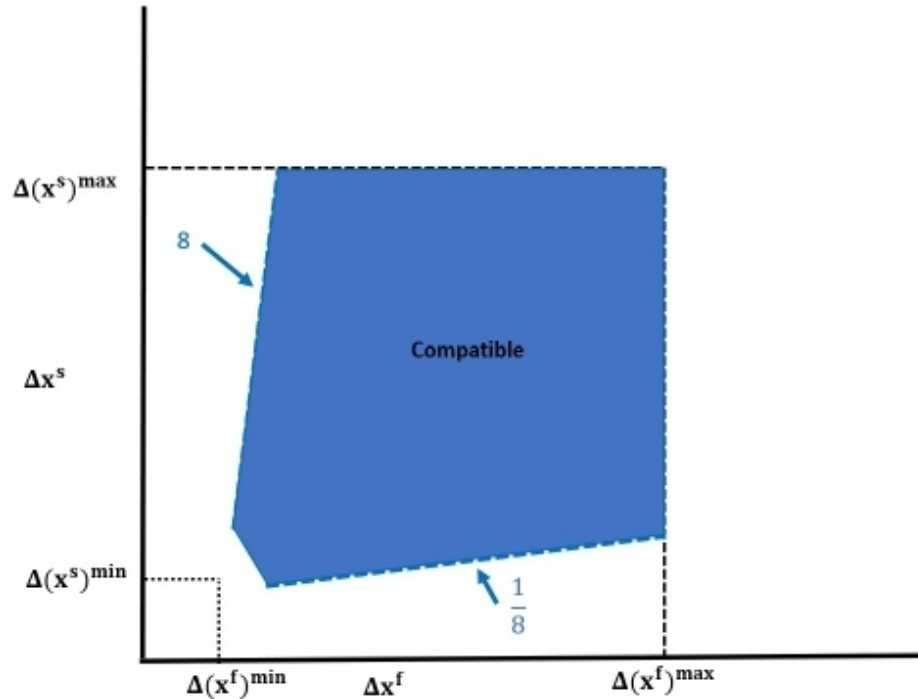
Material properties

Fluid	ρ^f (g/cm ³)	1
	μ^f (dyne/(cm · s))	1
Solid	ρ^s (g/cm ³)	1
	C (dyne/cm ²)	1.72×10^4
	K (dyne/cm ²)	3.33×10^5

Time: 0.000000



Numerical Example I: 2-D deformable solid disk driven by cavity flow



Fluid sensitivity tests	Solid sensitivity tests	Pure fluid tests
fluid velocity	fluid velocity	fluid velocity
solid KE over time	solid KE over time	
solid displacement	solid displacement	

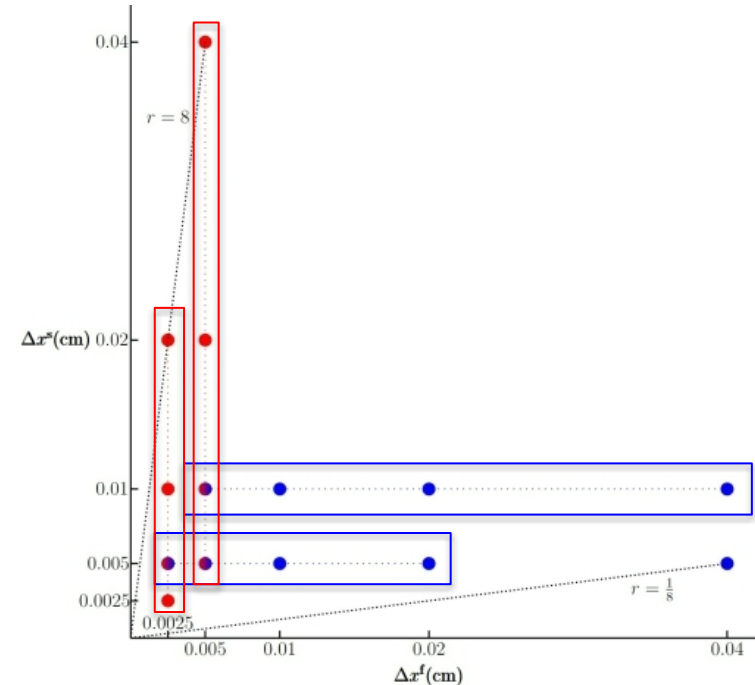
Avg solid solution difference using half time step: 0.33%
 Avg fluid solution difference using half time step: 0.22%

Extrapolation order of convergence using existing solutions [7]:

$$p = \frac{\ln(\frac{f_3 - f_2}{f_2 - f_1})}{\ln(r)} \quad r \text{ is the mesh refinement ratio}$$

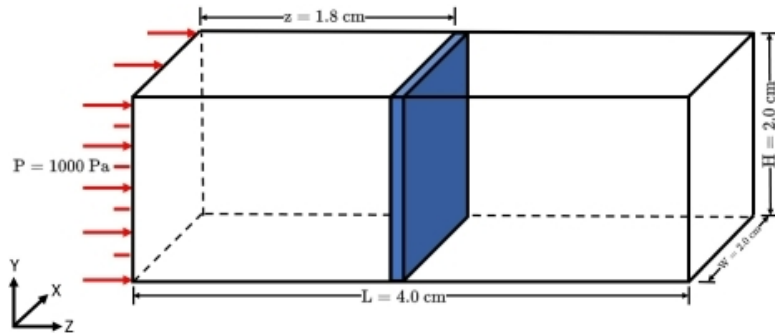
Numerical Example I: 2-D deformable solid disk driven by cavity flow

Fluid/solid sensitivity studies	Measurement	Convergence rate coarse mesh combinations (L1/L2/LInf)	Convergence rate fine mesh combinations (L1/L2/LInf)	pure fluid tests
fluid	fluid velocity	1.24/1.22/1.07 (0.97)	1.39/1.41/1.29 (0.87)	3.71/3.86/3.88/ (4.23)
fluid	solid displacement	1.31/1.34/1.66 (0.76)	1.28/1.28/1.36 (0.93)	N/A
fluid	solid KE	1.47 (time-avg) (1.16)	1.39 (time-avg) (1.01)	N/A
solid	fluid velocity	2.05/1.98/1.60 (1.66)	2.22/2.27/2.11 (2.18)	N/A
solid	solid displacement	1.86/1.90/2.00 (1.49)	1.90/1.92/2.01 (1.35)	N/A
solid	solid KE	2.25 (time-avg) (2.46)	2.22 (time-avg) (1.83)	N/A



Mesh size ratio dominates the convergence

Numerical Example II: 3-D elastic block under pressure wave

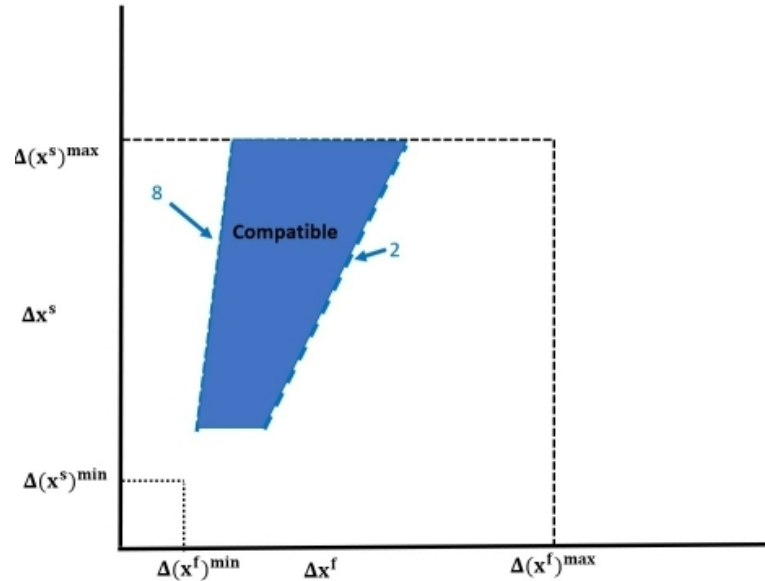


- **Fluid** (slightly compressible) constant pressure on the left, outflow on the right, no-slip on others
- **Solid** (Neo-Hookean) fully constrained on top and bottom, constrained in X on left and right surfaces, free for front and back surfaces

Material properties

Fluid	$\rho^f \text{ (g/cm}^3\text{)}$	1.3×10^{-3}
	$\mu^f \text{ (dyne/(cm} \cdot \text{s))}$	1.8×10^{-4}
Solid	$\rho^s \text{ (g/cm}^3\text{)}$	1
	$C \text{ (dyne/cm}^2\text{)}$	1.72×10^4
	$K \text{ (dyne/cm}^2\text{)}$	3.33×10^5

Numerical Example II: 3-D elastic block under pressure wave

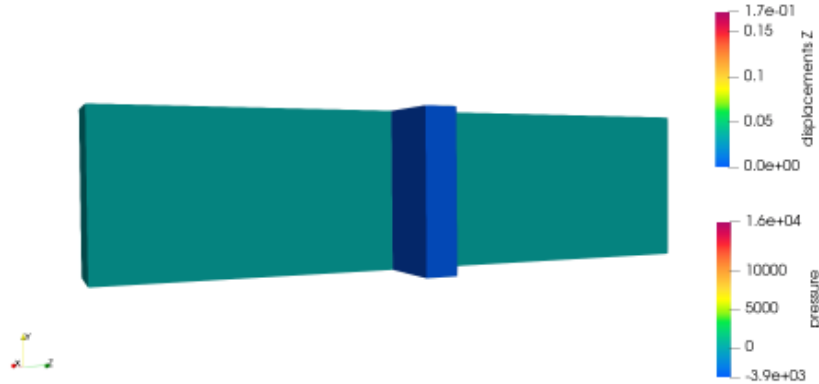


Solid mesh size	Fluid mesh size	Convergence steps
0.1	0.1	3790
0.05	0.05	2970
0.025	0.025	1710

Observation: refine the mesh for incompatible mesh size ratios will accelerate the failure

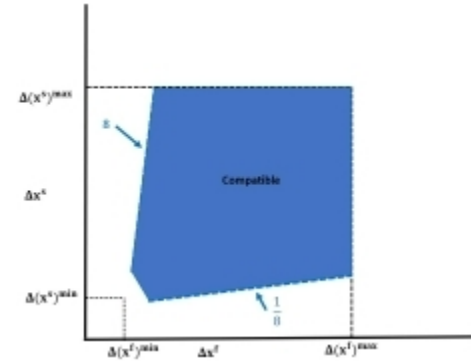
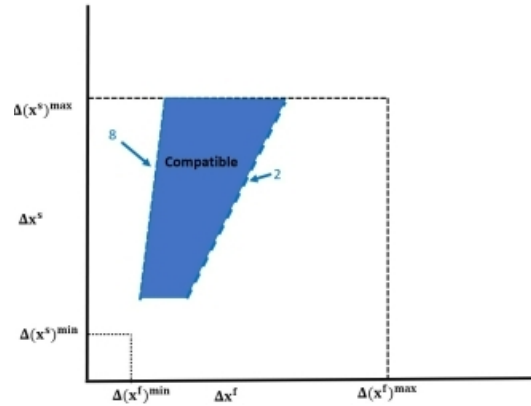
Numerical Example II: 3-D elastic block under pressure wave

Time: 0.000000



Fluid/solid sensitivity studies	Measurement	convergence rate (L1/L2/LInf)
fluid	fluid velocity	1.46/1.60/1.11 (1.05)
fluid	solid displacement	0.98/1.02/0.83 (0.81)
fluid	solid KE	1.33 (time-avg) (1.40)
solid	fluid velocity	1.82/1.77/1.88 (1.72)
solid	solid displacement	1.34/1.13/1.42 (1.45)
solid	solid KE	1.47 (time-avg) (1.53)

Summary of mesh convergence studies



- ❑ Compatible mesh size **ratios** are **pre-requisite** to a convergence coupled solution
- ❑ FSI interpolation method, solid geometry, B.C., and deformation affect the **range** of the compatible mesh size ratios
- ❑ The mesh size ratio **dominates** the accuracy of the coupled FSI solutions

Summary

- Two-dimensional **mesh convergence** definition
- The need for the **mesh compatibility** study
- The dominant effect of the **mesh size ratio** on coupled solution convergence

References

- [1] L. Heltai, S. Roy, and F. Costanzo, “A fully coupled immersed finite element method for fluid structure interaction via the deal. ii library,” arXiv preprint arXiv:1209.2811, 2012.26
- [2] Griffith, B. E. and X. Luo (2012) “Hybrid finite difference/finite element version of the immersed boundary method,” Submitted in revised form.
- [3] X. Wang and L. T. Zhang, “Interpolation functions in the immersed boundary and finiteelement methods,”Computational Mechanics, vol. 45, no. 4, p. 321, 2010
- [4]C. S. Peskin, “The immersed boundary method,” Acta numerica, vol. 11, pp. 479–517, 2002
- [5] W. K. Liu, Y. Liu, D. Farrell, L. Zhang, X. S. Wang, Y. Fukui, N. Patankar, Y. Zhang,C. Bajaj, J. Lee,et al., “Immersed finite element method and its applications to biological systems,”Computer methods in applied mechanics and engineering, vol. 195, no. 13-16,pp. 1722–1749, 2006
- [6] Jie Cheng, Feimi Yu, Lucy T. Zhang ‘OpenIFEM: A High Performance Modular Open-Source Software of the Immersed Finite Element Method for Fluid-Structure Interactions’
- [7] Patricj J Roache, ‘Verification and Validation in Computational Science and Engineering’



Rensselaer

why not change the world?®