



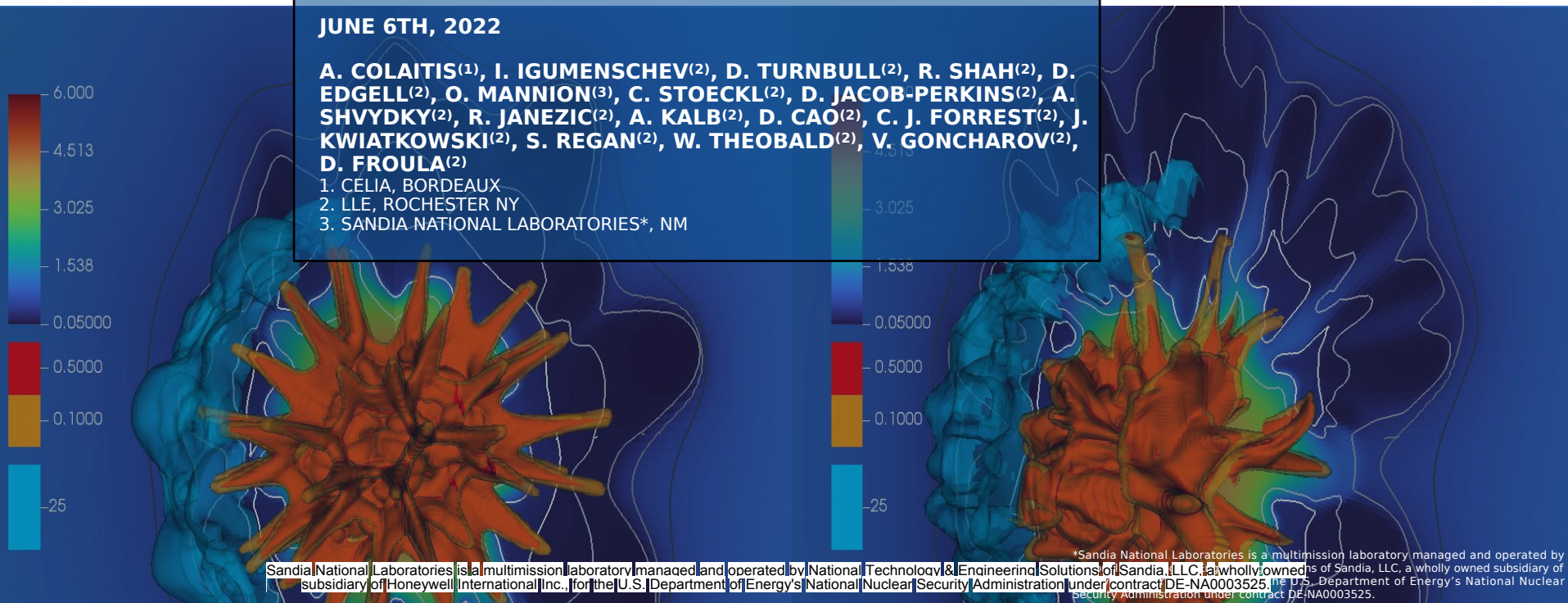
# 3D SIMULATIONS CAPTURE THE PERSISTENT LOW MODE ASYMMETRIES EVIDENT IN LASER-DIRECT-DRIVE IMPLOSIONS ON OMEGA

ANOMALOUS ABSORPTION CONFERENCE 2022

JUNE 6TH, 2022

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- 1. CELIA, BORDEAUX
- 2. LLE, ROCHESTER NY
- 3. SANDIA NATIONAL LABORATORIES\*, NM

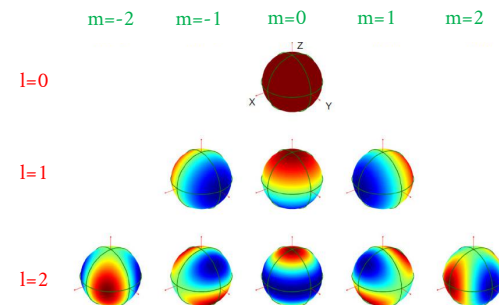


# BEST-SETUP EXPERIMENTS ON OMEGA IN 2019-2020 EXHIBIT SYSTEMATIC FLOW ANOMALIES

Database of 111 shots conducted in 2019-2020 on OMEGA

=> down-selection of 12 shots with:

- 60 beams, full SSD
- good ice thickness uniformity ( $<1\%$   $l=1$ )
- good ice surface roughness
- low pointing error ( $<2\%$   $l=1$ ,  $<2\%$   $l=2$  to  $<1\%$   $l=1$ )
- low power imbalance
- low target offset ( $<5$  microns to  $<1$  micron)



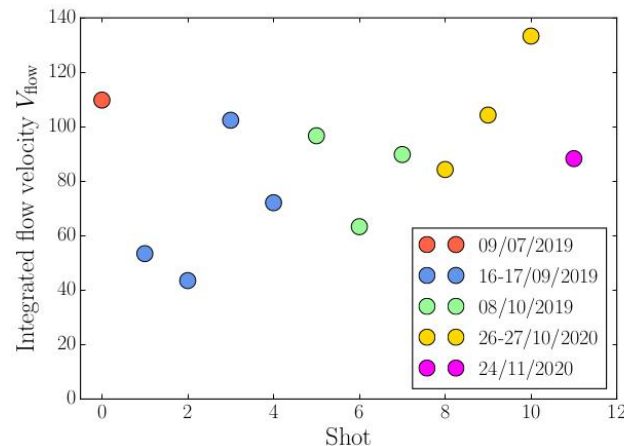
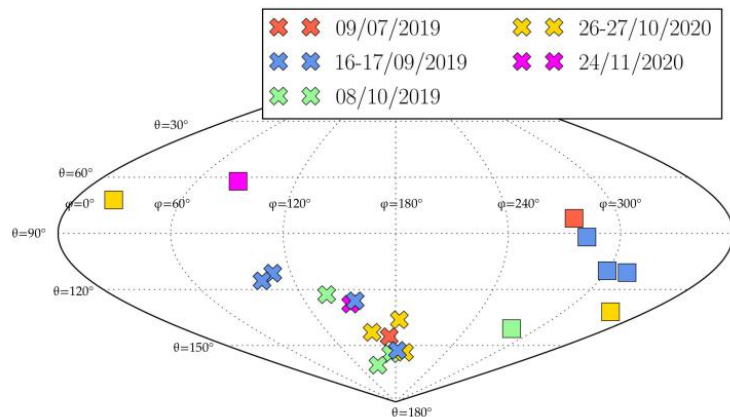
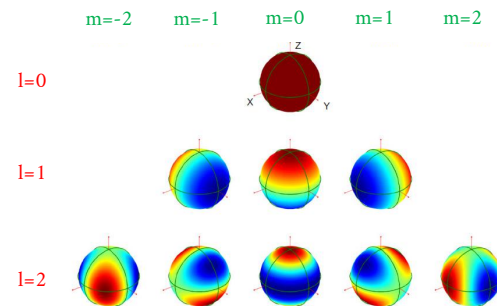
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... there remain a significant mode 1 assymetry in the DT flow at stagnation, that does not seem correlated to mispointing error, cryo/warm, or shot-day anomalies



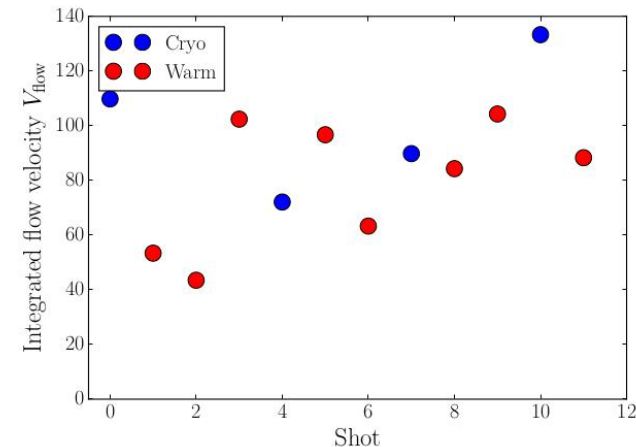
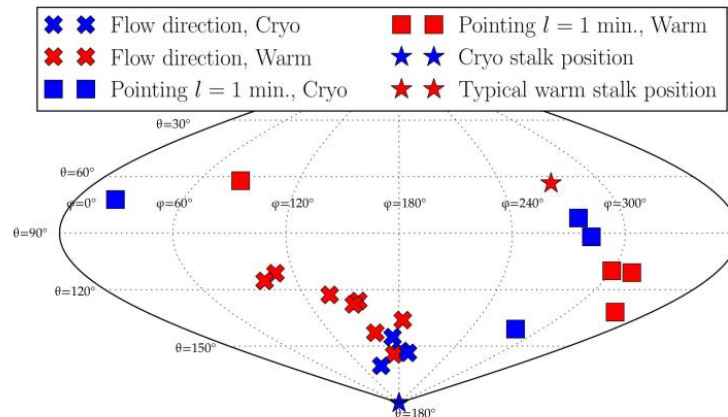
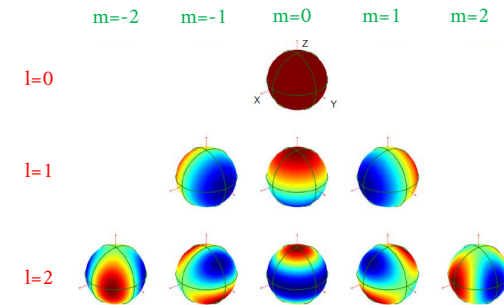
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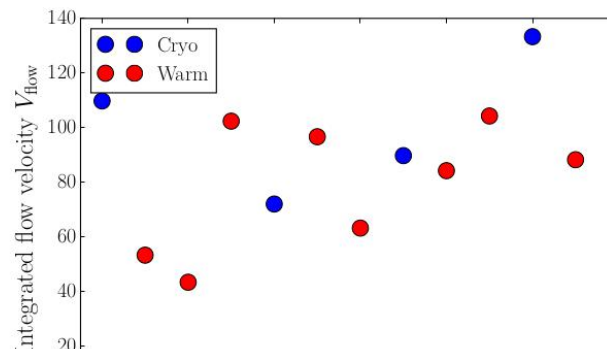
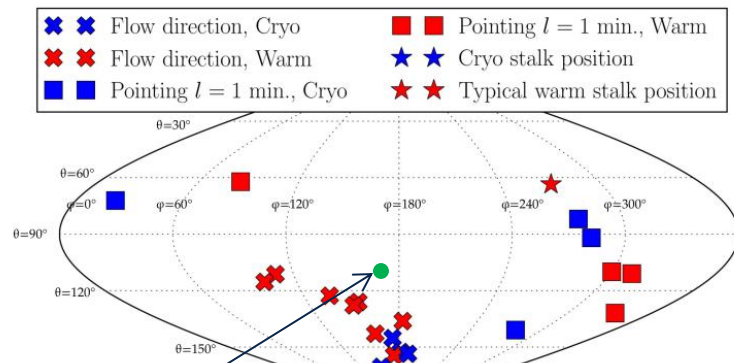
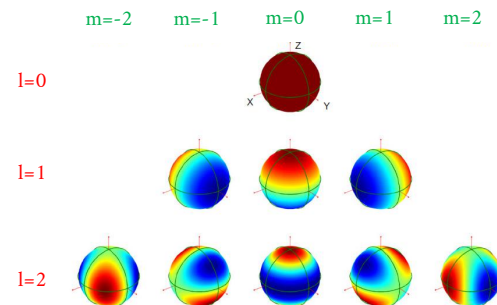


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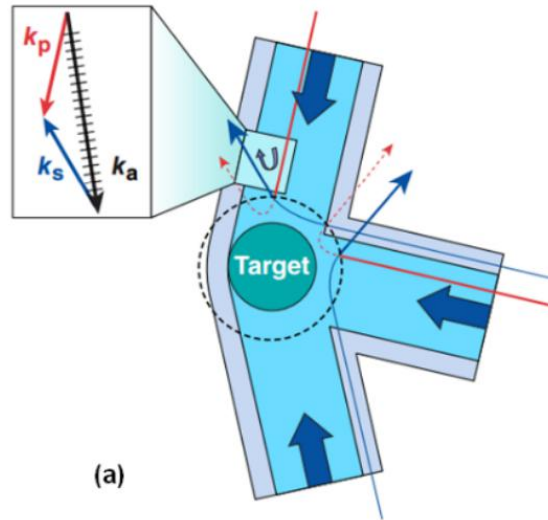


- Is the polarization effect of CBET responsible for the systematic anomaly ?
- If including most sources of low modes, can the modeling reproduce the experimental data for neutron data ?
- What is the relative contribution of these sources to yield degradation ?
- How to mitigate low modes ?
- Polarization anomaly on NIF ?

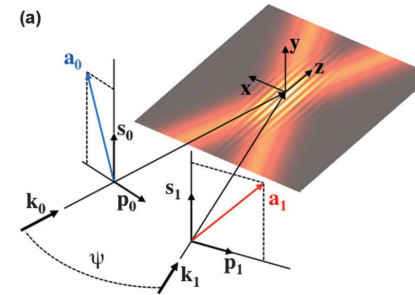
# UNPOLARIZED CBET FROM A SYMMETRIC BEAM PATTERN PRODUCES A SYMMETRIC IRRADIATION

Why would the polarization effect matter ... ?

Cross Beam Energy Transfer (CBET) transfers energy between beams through a shared IAW grating



[A. K. Davis et al. PoP (2016)]



[P. Michel et al. PoP 17 (2010)]

In direct-drive, reflected beams “steal” energy from incident beams

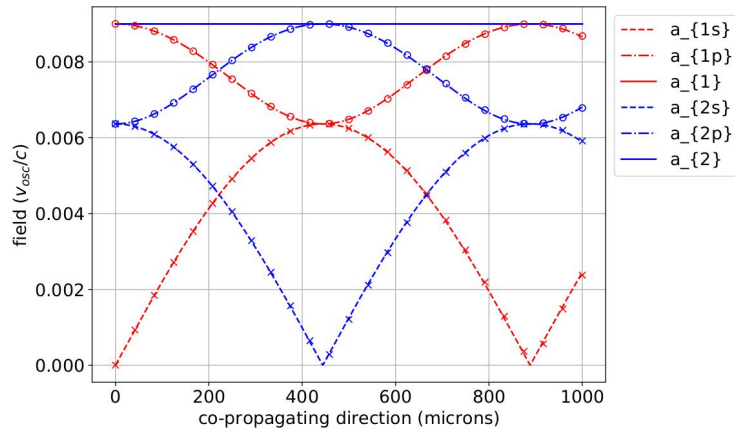
If the laser configuration is **perfectly symmetric**, the unpolarized CBET also remains symmetric



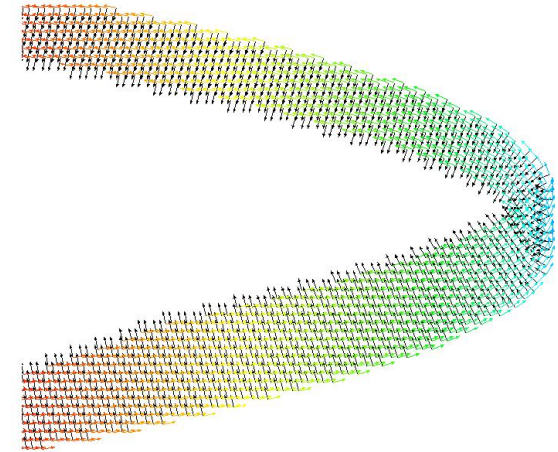
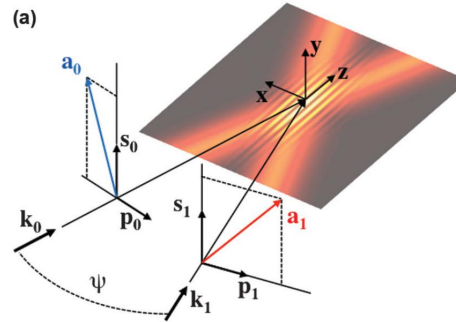
# POLARIZATION EFFECTS CONTRIBUTE TO THE DETAILS OF CBET AMPLIFICATION

Why would the polarization effect matter ... ?

- Ellipticity induced from propagation in a bi-refringent medium formed by the IAW grating
- Probe beam polarization rotation toward that of the pump
- Polarization transport through refraction



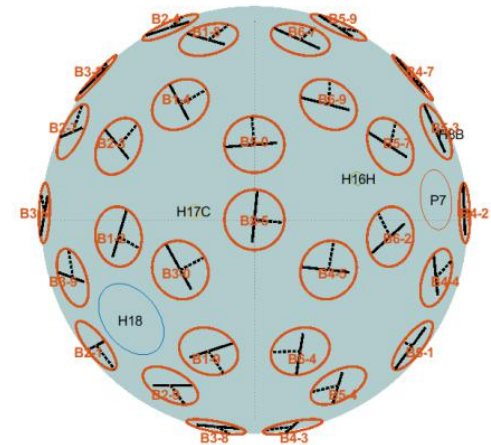
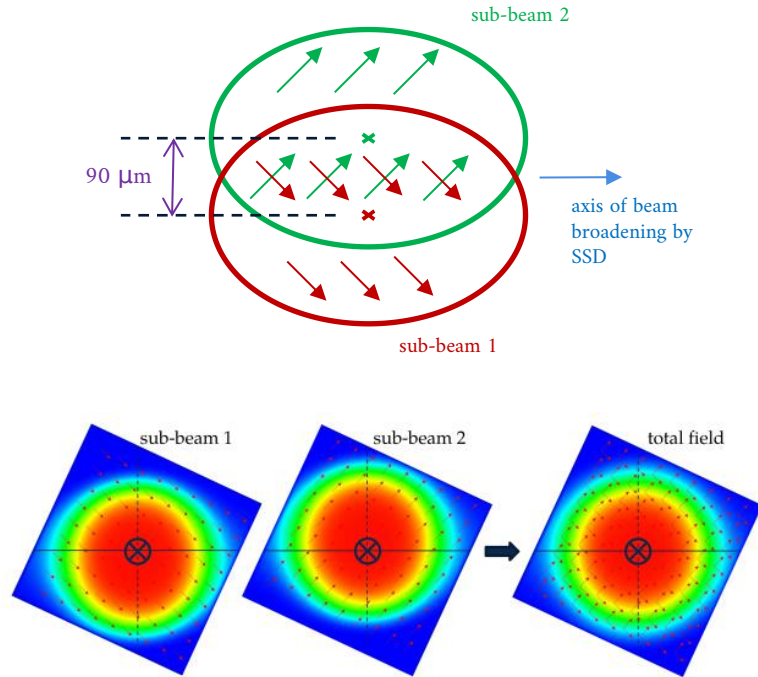
Beams interacting in a medium with  
 $\text{Im}(K) = 0$  and  $\text{Re}(K) > 0$





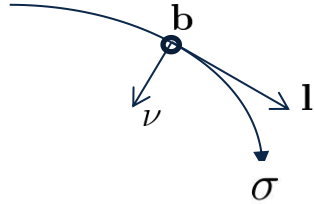
# THE POLARIZATION CONFIGURATION ON OMEGA IS NON-SYMMETRIC

Why would the polarization effect matter ... ?



# INLINE MODELING OF POLARIZED CBET RELIES ON DECOMPOSITION OF THE FIELD ON THE FRENET FRAME OF RAYS

Frenet reference frame



$$\boldsymbol{\nu} = \frac{1}{2\mathcal{K}\epsilon'} \nabla_{\perp} \epsilon'$$

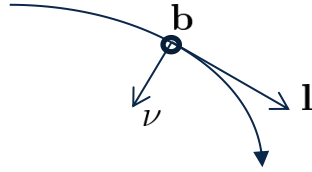
$$\mathcal{K} = \frac{1}{2} \left| \frac{\nabla \epsilon'}{\epsilon'} \times \mathbf{l} \right|$$

$$\frac{d\boldsymbol{\nu}}{d\sigma} = -\mathcal{K}\mathbf{l} + \kappa\mathbf{b}$$

$$\kappa = \mathbf{b} \cdot \frac{d\boldsymbol{\nu}}{d\sigma}$$

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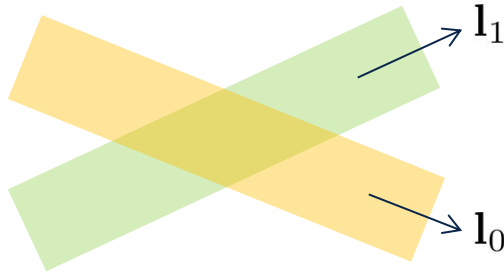
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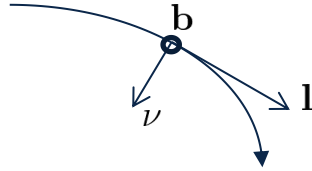
$$\frac{\partial \mathbf{a}_1}{\partial \mathbf{l}_1} = \frac{i}{8k_1} K_{10} k_{b,10}^2 (\mathbf{a}_0^* \cdot \mathbf{a}_1) \mathbf{a}_0$$

$$\frac{\partial \mathbf{a}_0}{\partial \mathbf{l}_0} = \frac{i}{8k_0} K_{01} k_{b,01}^2 (\mathbf{a}_0 \cdot \mathbf{a}_1^*) \mathbf{a}_1$$



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Complex s/p components in the Frenet frame

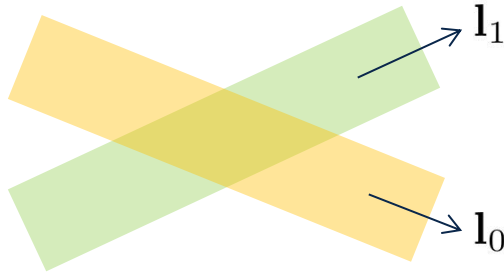
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$$\frac{\partial}{\partial \mathbf{l}_n} \begin{pmatrix} a_{n,\nu_n} \\ a_{n,b_n} \end{pmatrix} = \underline{\underline{\mathcal{D}_n}} \cdot \begin{pmatrix} a_{n,\nu_n} \\ a_{n,b_n} \end{pmatrix}$$

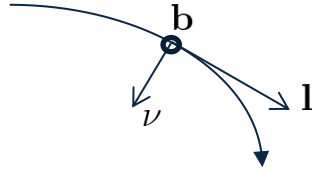
$$\underline{\underline{\mathcal{D}_n}} = \frac{i}{8k_n} \sum_{\substack{m \in \text{beams, sheets} \\ m \neq n}}^N K_{nm}^* k_{b,nm}^2 \underline{\underline{\mathbf{M}_{nm}}}$$

Complex kinetic plasma response  
Langdon and Dewandre effect  
Real part: induces **ellipticity**  
Imaginary part: depletion or gain



# INLINE MODELING OF POLARIZED CBET RELIES ON DECOMPOSITION OF THE FIELD ON THE FRENET FRAME OF RAYS

Frenet reference frame



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Complex s/p components in the Frenet frame

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→

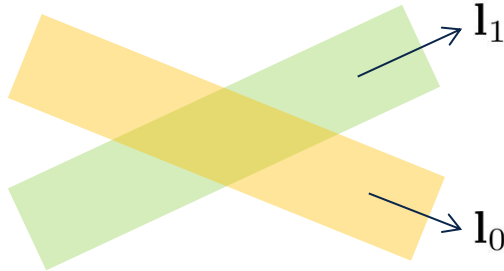
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$$\underline{\underline{\mathbf{M}_{nm}}} = \begin{pmatrix} a_{m,\nu_n}^2 & a_{m,b_n}^* a_{m,\nu_n} \\ a_{m,b_n} a_{m,\nu_n}^* & a_{m,b_n}^2 \end{pmatrix}$$

Matrix responsible for  
polarization rotation  
and ellipticity

“Usual” coupling

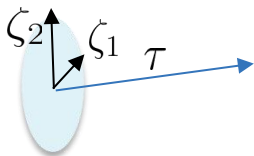


# REASONABLE NUMERICAL EFFICIENCY IS OBTAINED BY LEVERAGING INVERSE RAY TRACING

$$u = A \exp[ik_0\psi] ,$$

$$\psi''(\tau) = \int_0^\tau \epsilon''(\mathbf{r}(\hat{\tau})) d\hat{\tau} / 2 ,$$

$$A(\tau) = A(0) \left| \frac{D(0)}{D(\tau)} \right|^{1/2} ,$$



Step 1; manifold geometry

- compute the mapping from phase space  $(\zeta_1, \zeta_2)$  to real space  $(x, y)$
- compute the geometric part of the laser field
- compute the Airy Integral that gives the caustic field
- compute the full Frenet frame for each sheet of each beam at each gridpoint

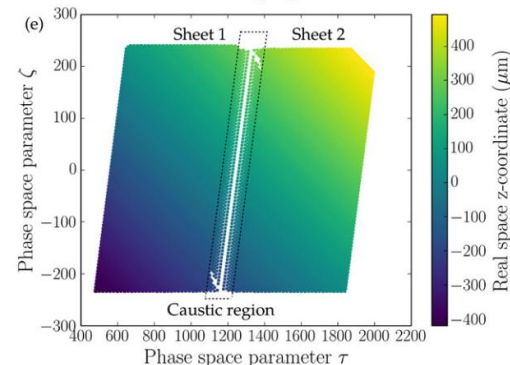
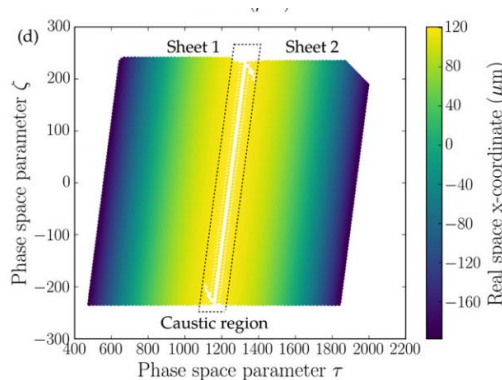
=> these are **geometric** factors stemming from the ray mapping fixed during one timestep

ne/nc

z

x

plane wave  
at an angle

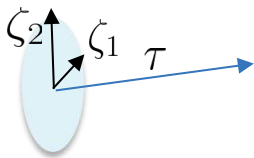


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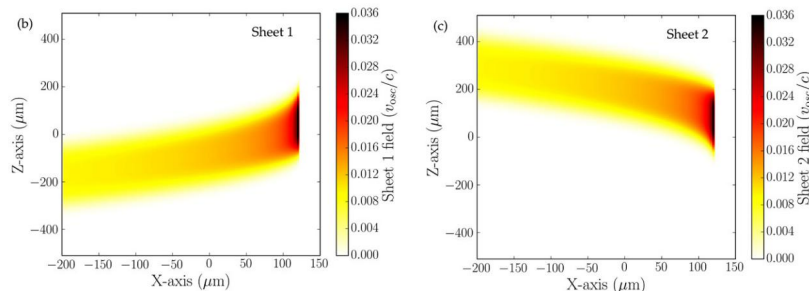
=> these are **geometric** factors stemming from the ray mapping fixed during one timestep

Step 2; fields

- compute the phase contribution to the fields
- compute the Langdon effect coefficient and the polarized CBET coupling term

$$\begin{pmatrix} \epsilon_{i,j,\nu_n} \\ \epsilon_{i,j,b_n} \end{pmatrix} = [\epsilon'_i + i(\epsilon''_{0,i} f_L + \underline{\underline{D_{i,j}}})] \cdot \begin{pmatrix} 1 \\ 1 \end{pmatrix}$$

Fixed point iteration with damping until convergence



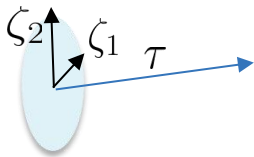


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## Unpolarized CBET

- Track the incident and reflected field of each beam
- Use an angle-dependant “unpolarized” coefficient for the interaction

Step 1; manifold geometry

- compute the mapping from phase space ( $\zeta_1, \zeta_2$ ) to real space (x, y)
- compute the geometric part of the laser field
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- compute the full Frenet frame for each sheet of each beam at each gridpoint

=> these are **geometric** factors stemming from the ray mapping fixed during one timestep

Step 2; fields

- compute the phase contribution to the fields
- compute the Langdon effect coefficient and the polarized CBET coupling term

Fixed point iteration with damping until convergence

## Polarized CBET

- Transport the Frenet basis of the rays that rotates due to refraction
- Track 2 complex polarizations + the incident and reflected components of each beam
- For DPR modeling: split each beam into two sub-beams

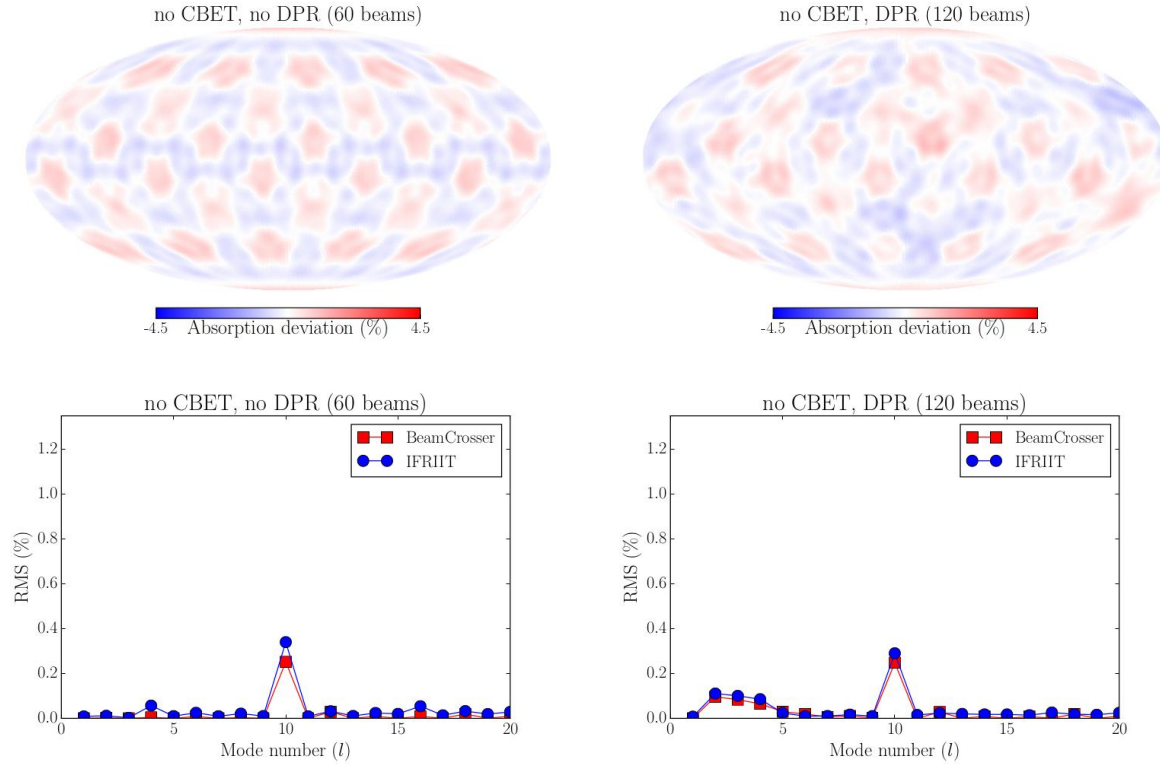


CBET coefficients: 60 beams x 2 fields x N\_gridpoints

=> CBET coefficients: 60 beams x 2 fields x 2 sub-beams x 2 components x 2 x N\_gridpoints

# THE UNPOLARIZED CBET ON OMEGA INDUCES NO SIGNIFICANT ASSYMETRY ON THE ENERGY DEPOSITION

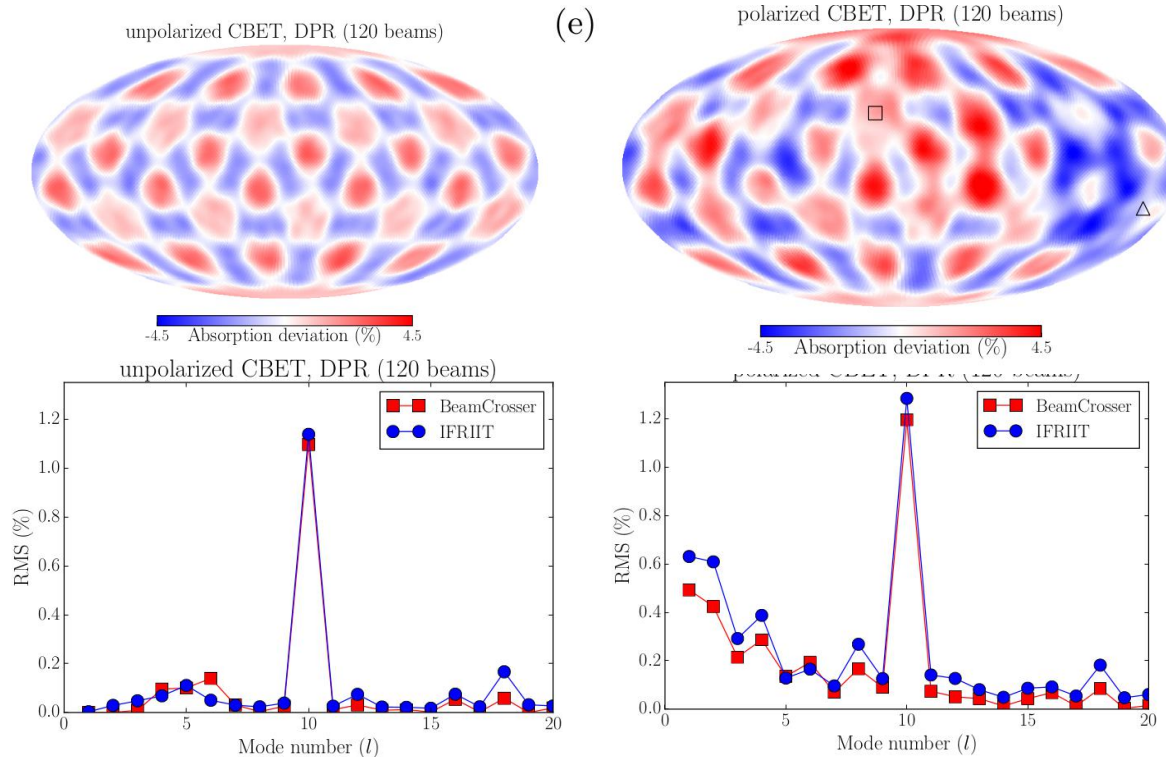
Heat source calculated in a 1D hydro profile - no CBET



The DPR system itself induces slight low modes, small effect

# THE POLARIZED CBET INDUCES A NON-NEGLIGIBLE LOW MODE ANOMALY ON THE ENERGY DEPOSITION PATTERN

Heat source calculated in a 1D hydro profile - CBET



The polarization effect induces significant low modes

Consistent with results from D. Edgell obtained using BeamletCROSSER postprocessor

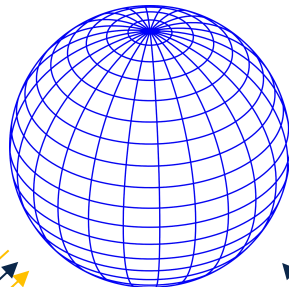
What is the compound effect accounting for hydrodynamics feedback and other low mode sources ?

# THE ASTER+IFRIIT COUPLED CODE WAS DEVELOPPED TO STUDY ICF IMPLOSIONS CONSIDERING MOST LOW MODE SOURCES

## ASTER+IFRIIT code coupling

[A. Colaitis, I. V. Igumenshchev et al. JCP (2021)]

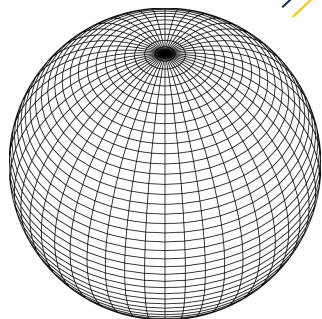
aster mesh  
typical size: 20-500M nodes



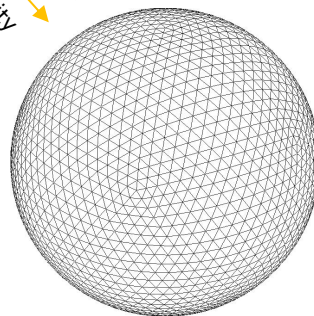
initial permittivity,  
 $T_e, T_i, n_e$  fractions,  $v$   
nodes coordinates,  
EM energy density

nodes coordinates  
initial permittivity

Langdon permittivity perturbation  
CBET permittivity per-sheet  
perturbations



observation mesh  
typical size: 0.5-1.5M nodes



raytracing mesh  
typical size: 1-10M nodes, 5-50M tetras

## ASTER 3-D radiative hydrodynamics code

- Eulerian spherical moving grid
- EOS, heat transport, radiation, hydro...
- High resolution, block-decomposed MPI

[I. V. Igumenshchev et al. PoP (2016),  
I. V. Igumenshchev et al. PoP (2017)]

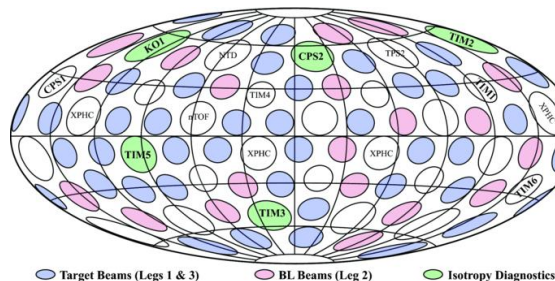
## IFRIIT 3-D laser propagation code

- Inverse Ray Tracing for fast and low noise field computations
- Caustic modeling with Etalon Integrals
- CBET with many physics models, including polarization
- Adaptive resolution, domain-duplicated MPI/OpenMP

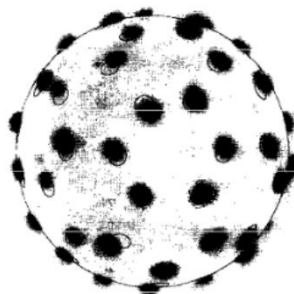
[A. Colaitis et al., PoP 26(3) (2019),  
A. Colaitis et al., PoP 26(7) (2019)]

# WE STUDY 4 SHOTS CONSIDERING MOST LOW MODE SOURCES

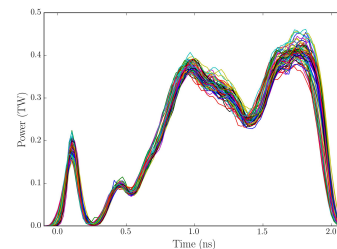
Shot number	Date	Type	$E_{\text{las}}$ (kJ)	$D_t$ ( $\mu\text{m}$ )	Offset magnitude ( $\mu\text{m}$ )	Pointing shot	Pointing	Balance $l = 1$ (% RMS)		
							$l = 1$ (% RMS)	picket	early drive	late drive
94343	09/07/2019	cryo	27.7	982	3.5	94336	1.26	2.58	0.48	1.45
94712	09/08/2019	cryo	28.4	961.4	7.0*	94708	5.94	4.52	0.35	1.34
98768	27/10/2020	cryo	28.4	1012	3.2	98762	1.08	1.72	0.43	1.7
98755	26/10/2020	warm	27.9	978.2	1.3	98754/98757	0.64/1.0	0.71	0.79	0.92



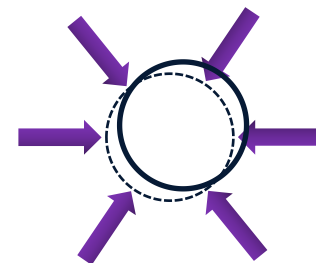
OMEGA detailed beam geometry  
120 DPR-split beams



XPC H7 View  
Measured beam pointing  
(from beginning and/or  
end of shot day)



Measured pulse shapes

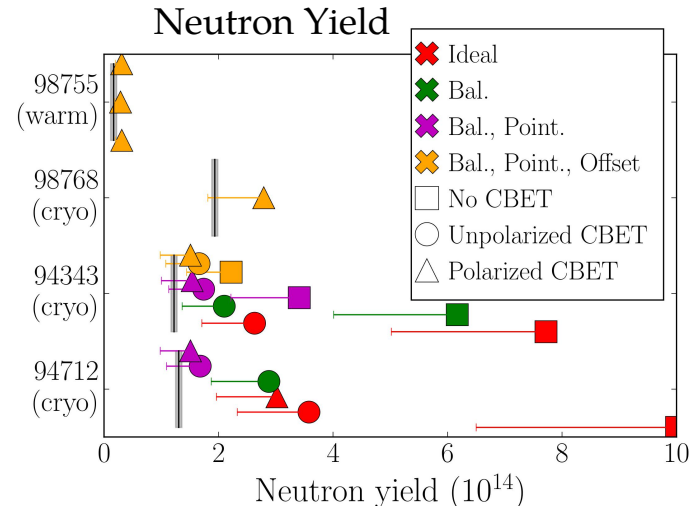
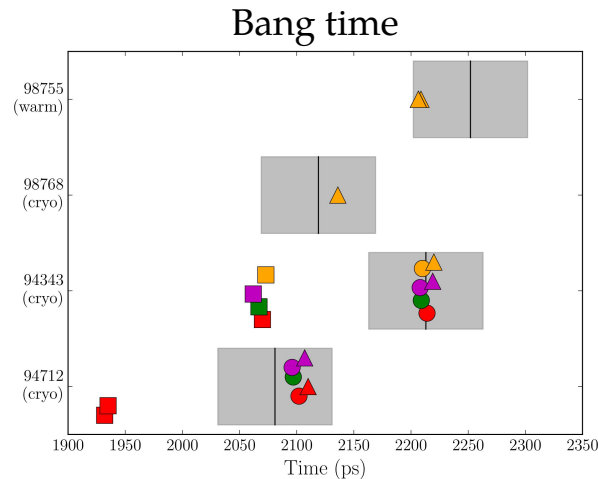


Measured offset (if  
available)

# THE 3D MODELING REPRODUCES THE EXPERIMENTALLY MEASURED BANG TIME AND NEUTRON YIELD

Simulation results presented for 4 shots are studied ; 3 cryogenic and one « warm » shot

Total ~ 60M CPU hours of computation



- The modeling reproduces bang time (time of peak convergence) as long as CBET is modeled
- Experimentally measured neutron yields are also reproduced in simulations that account for system-induced low modes and CBET

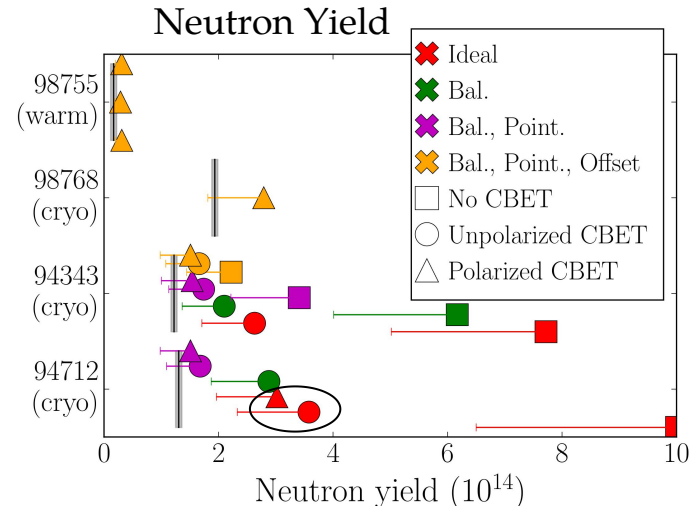
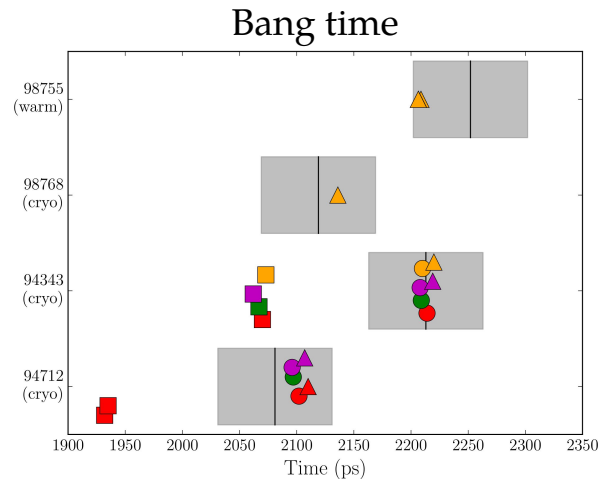
Note:

- experimental yields are corrected for fuel aging
- simulated yield include a “range” accounting for some of the high modes contributions

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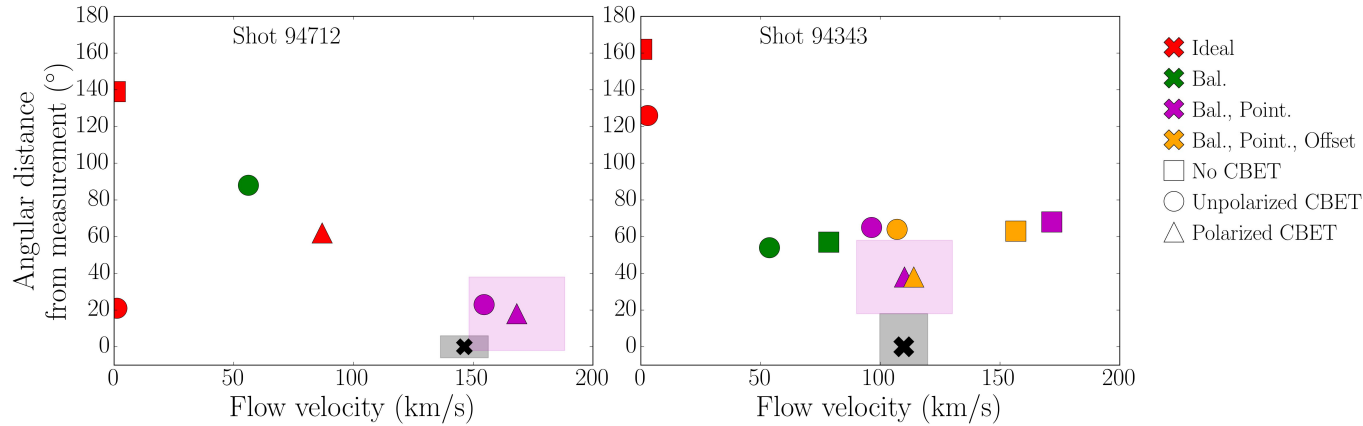
- The modeling reproduces bang time (time of peak convergence) as long as CBET is modeled
- Experimentally measured neutron yields are also reproduced in simulations that account for system-induced low modes and CBET
- Polarization alone, in the ideal case, causes a 15% yield drop wrt. unpolarized

Note:

- experimental yields are corrected for fuel aging
- simulated yield include a “range” accounting for some of the high modes contributions

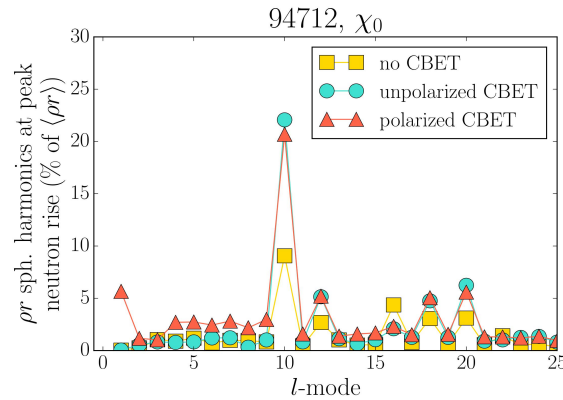
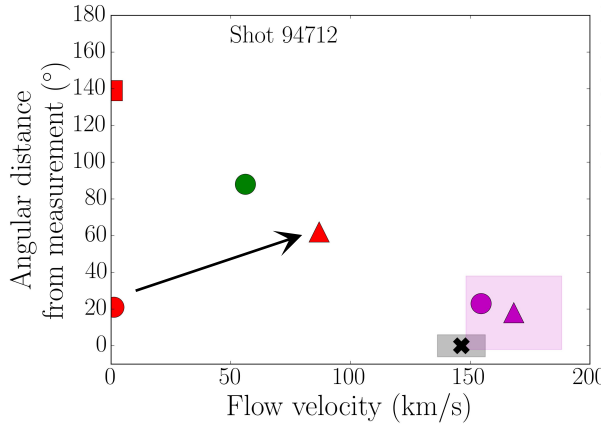


# THE 3D MODELING ALSO APPROACHES WELL THE FLOW VELOCITY MAGNITUDE AND DIRECTION



The modeling is also able to reproduce the measured flow velocity and direction, once again only if all system low modes are accounted for and if polarized CBET is account for

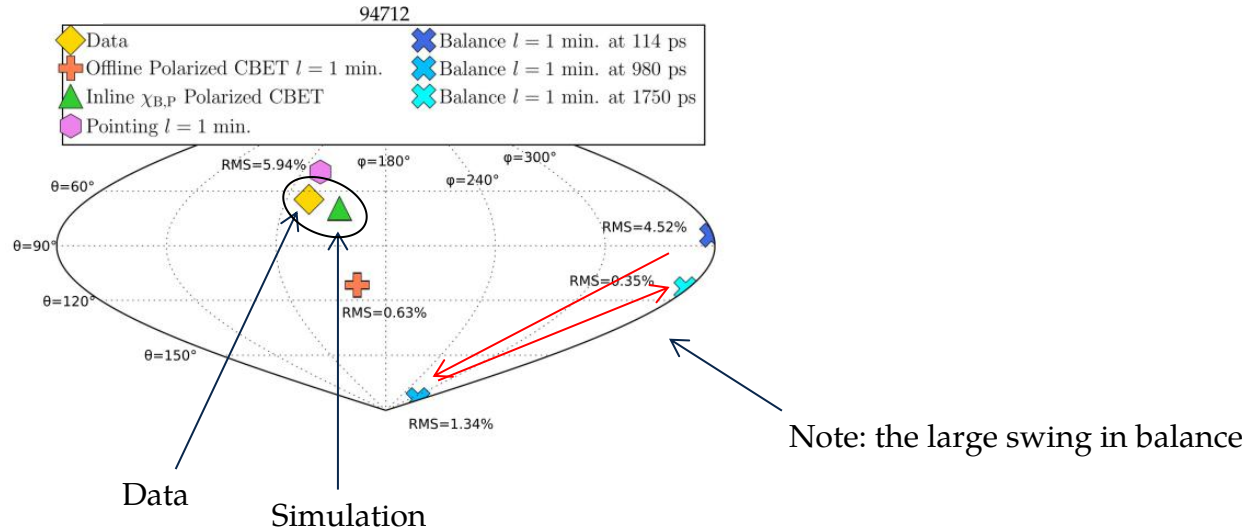
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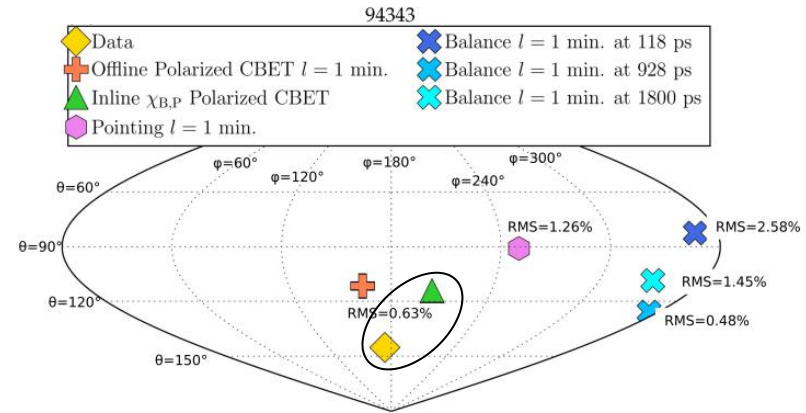
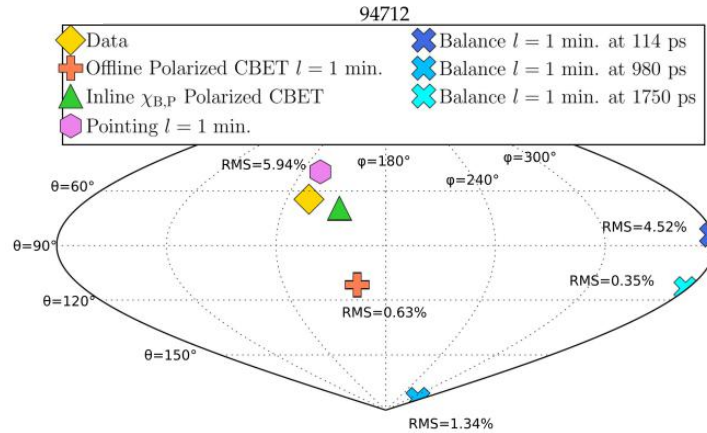
Note the single effect of polarized CBET, that induces a  $\sim 80$  km/s flow in the ideal case

# THE MODELING SYSTEMATICALLY APPROACHES THE MEASURED FLOW DIRECTION



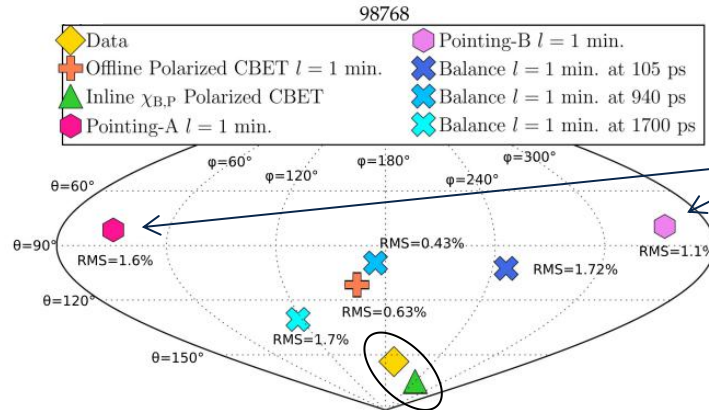
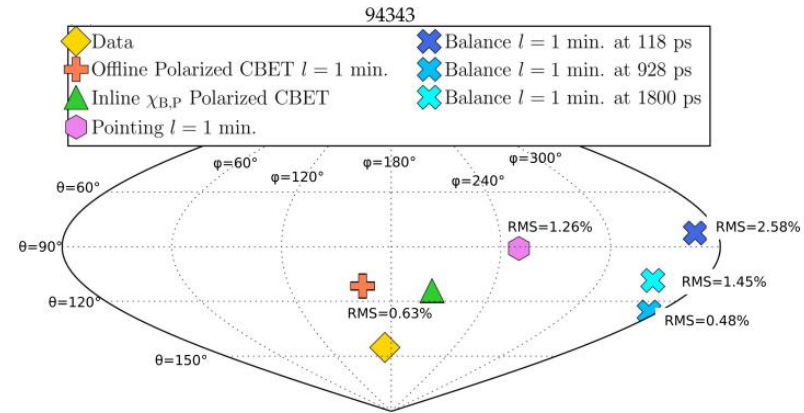
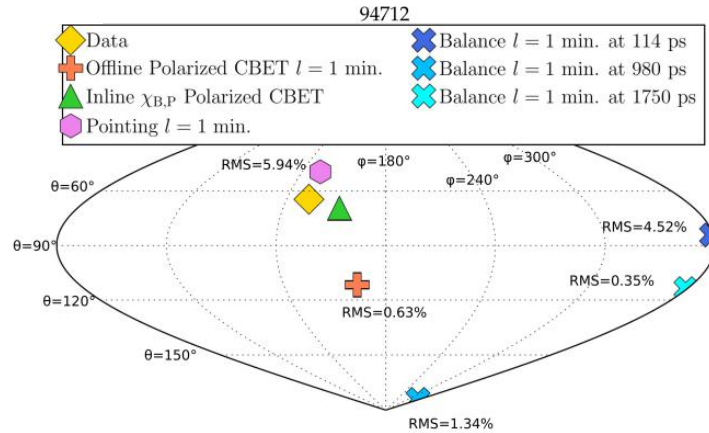
94712 was dominated by pointing:  
result is close to pointing anomaly

# THE MODELING SYSTEMATICALLY APPROACHES THE MEASURED FLOW DIRECTION



94343 had balanced low mode sources; the results is a non-trivial combination of those

# THE MODELING SYSTEMATICALLY APPROACHES THE MEASURED FLOW DIRECTION



Note: 53° between two pointing analysis of the same pointing shot

For this shot, the simulation underestimates the flow velocity (72 km/s vs 133 km/s measured)

# THE KNOWLEDGE OF THE ACTUAL POINTING MODES IS LIMITING OUR AGREEMENT WITH THE DATA

Note:

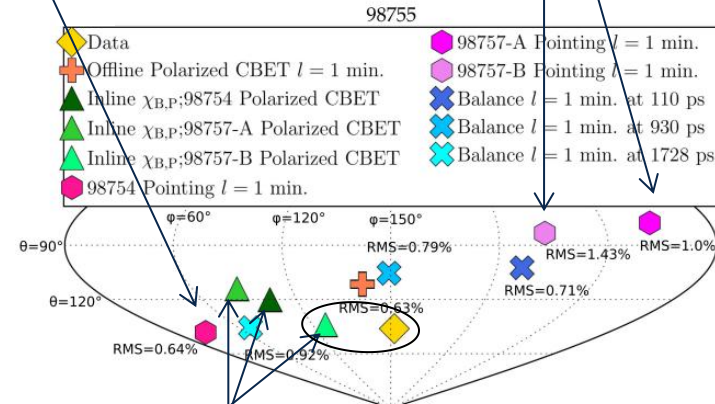
- 80 to 100° difference between the morning and afternoon pointing shots despite no TIM transaction

For this shot, the simulations underestimate the flow velocity (50 km/s vs 84 km/s measured)

=> Knowledge of pointing limitates our predictability of flow direction

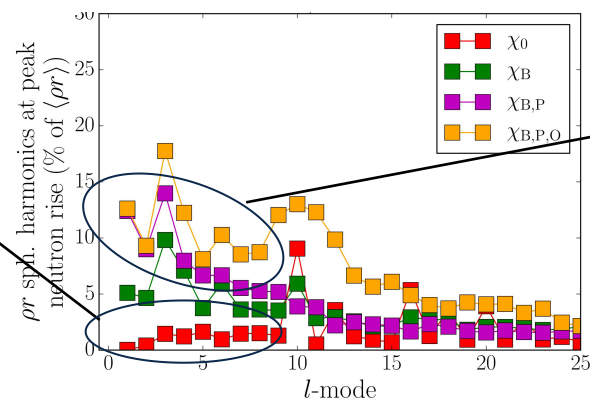
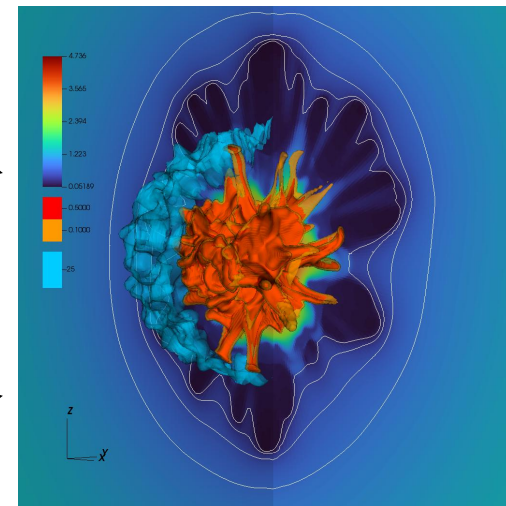
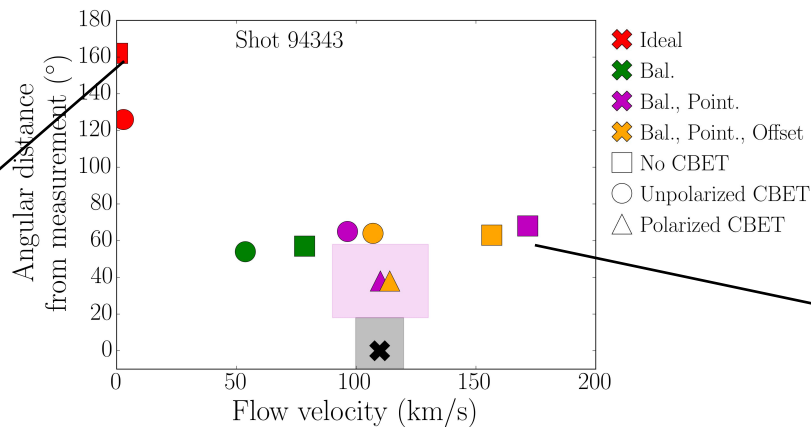
Morning pointing shot

Afternoon pointing shot



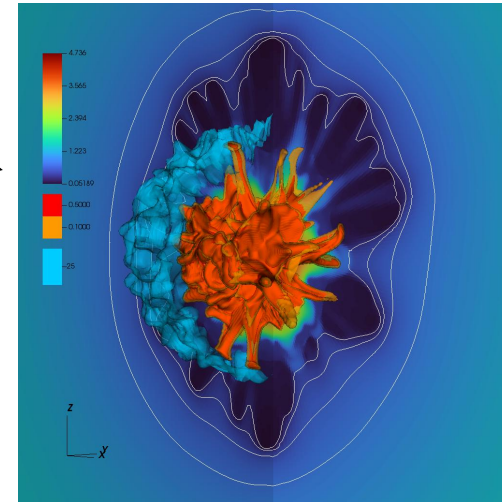
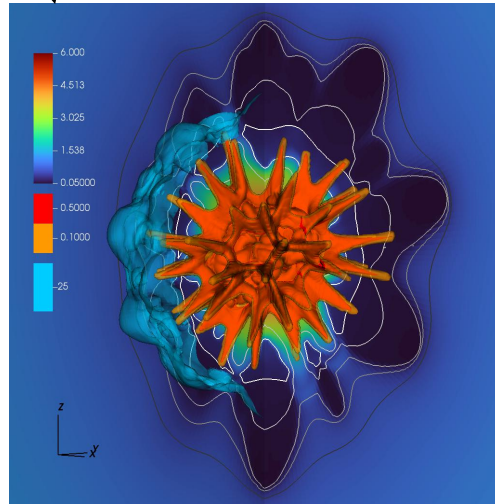
Three simulations with three pointings

# THE CURRENT BEST PERFORMANCES OF THE LASER SYSTEM CAN STILL CAUSE HIGHLY SIGNIFICANT FLOW ANOMALIES

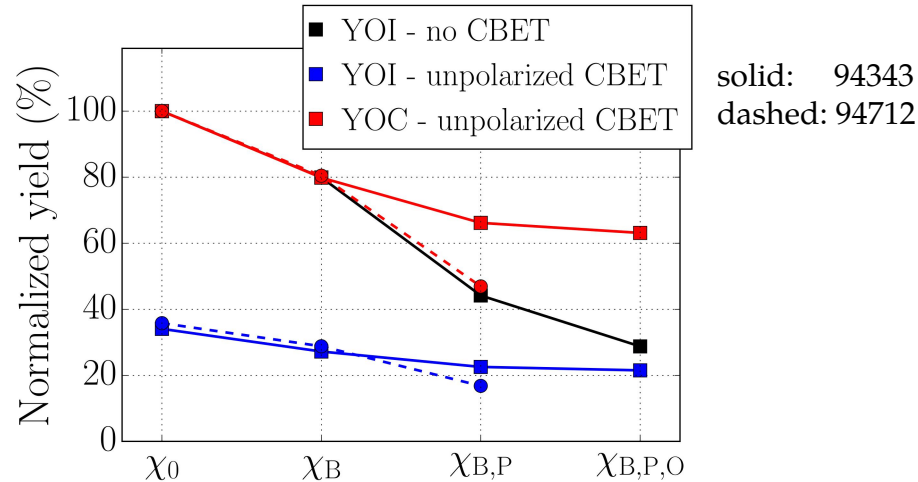


Without CBET, best levels of pointings, balance and offset introduce significant low modes at stagnation, with DT flows that can reach up to 170 km/s





# TOTAL ENERGY COUPLING IS STRONGLY DRIVEN BY CBET AND SYSTEM LOW MODES



- **CBET alone reduces neutron yields by ~60 % in the ideal case** → a realistic fusion driver must remove CBET
- **System-induced low modes are mitigated by CBET** → designs without CBET must be made more robust to low modes

=> How to mitigate low modes ? We can explore two mitigation strategies (current and envisioned)

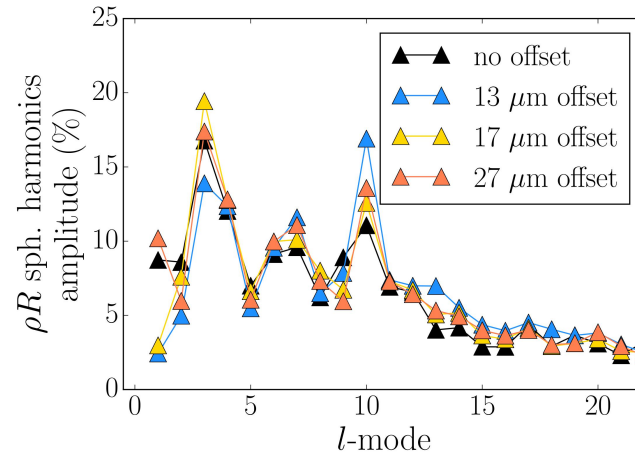
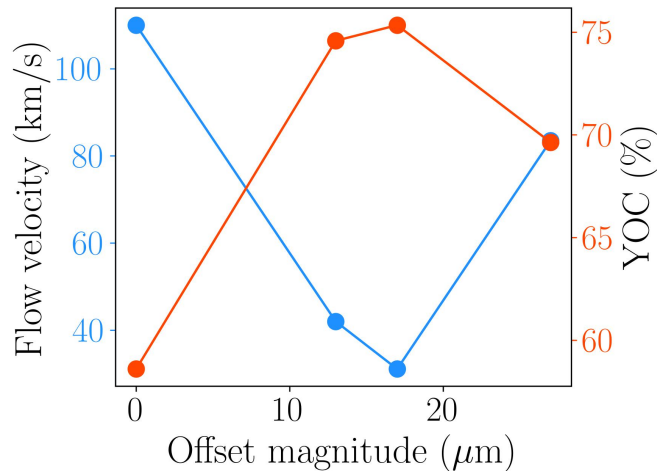
# MITIGATION OF LOW MODES BY TARGET OFFSET CAN ONLY RECOVER A FINITE AMOUNT OF YIELD

## Strategy 1 : offset mitigation

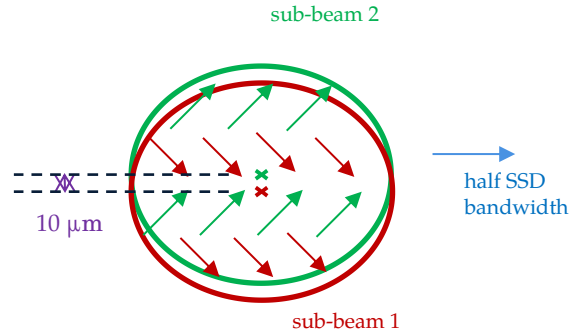
- In experiments, the target can be offset opposite to the direction of the measured flow anomaly (this is used routinely to improve yields)

Pros : Simple to implement, allows to recover ~15 % in yield at maximum here

Cons : The method rapidly reaches a maximum efficacy due to it mitigating only  $l=1$ . In particular, even in the ideal case, polarized CBET introduces other modes than  $l=1$ . It is also a post-hoc method.



# A RE-DESIGN OF THE OMEGA DPR SYSTEM IS A MORE VIABLE LONG TERM STRATEGY TO IMPROVE IMPLOSION PERFORMANCE



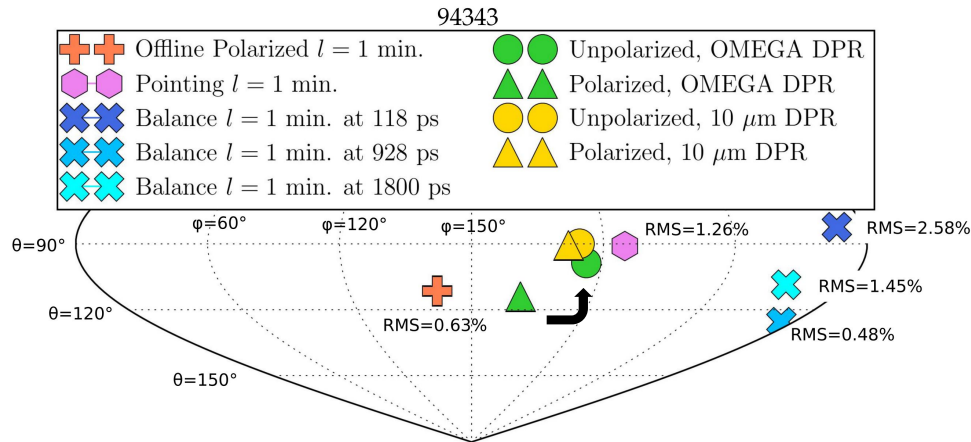
Strategy 2 :

- Re-design the DPR system on OMEGA to reduce the offset between polarizations

Pros : Allows to recover the unpolarized CBET result, effectively mitigating this source of low modes

Cons : difficult to implement, also requires to half the SSD bandwidth...

However, this anomaly does need to be corrected in the long run ...

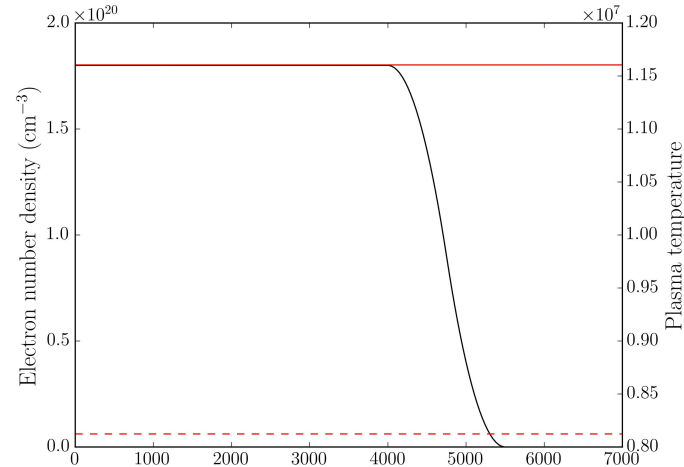
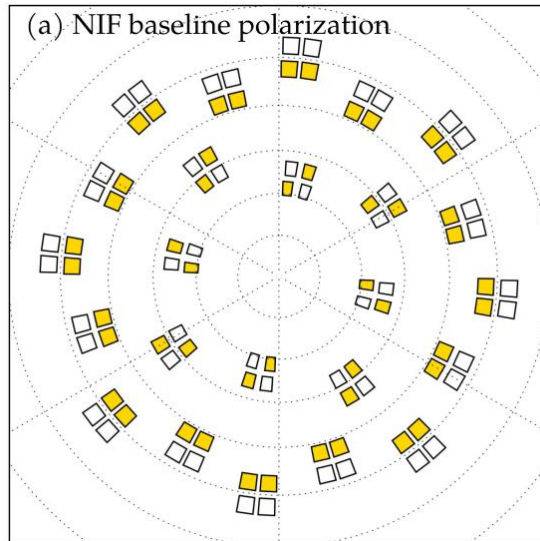


# THE POLARIZED CBET MODEL HAS BEEN APPLIED TO OFFLINE ESTIMATIONS OF CBET FOR NIF

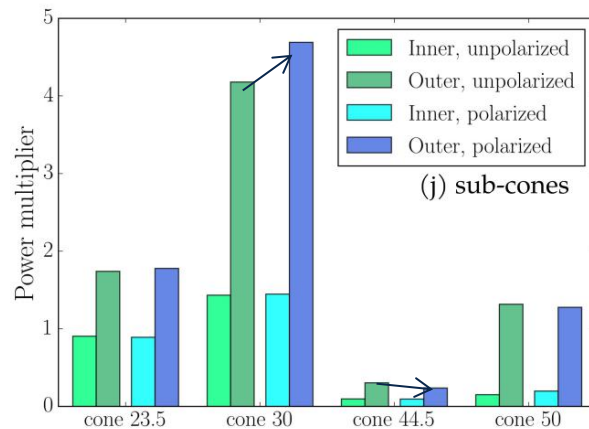
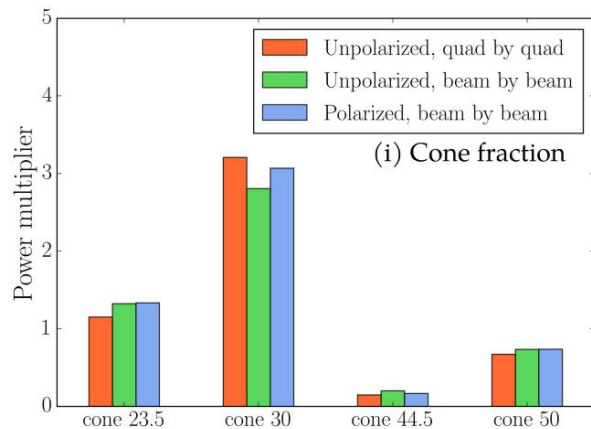
What about the polarization effect on the NIF?

Half hemisphere (96 beams) pointed at TCC, interacting in a spherical plasma with upward flow velocity at  $c/1000$

Comparing: unpolarized quad-by-quad, unpolarized beam-by-beam, polarized beam-by-beam

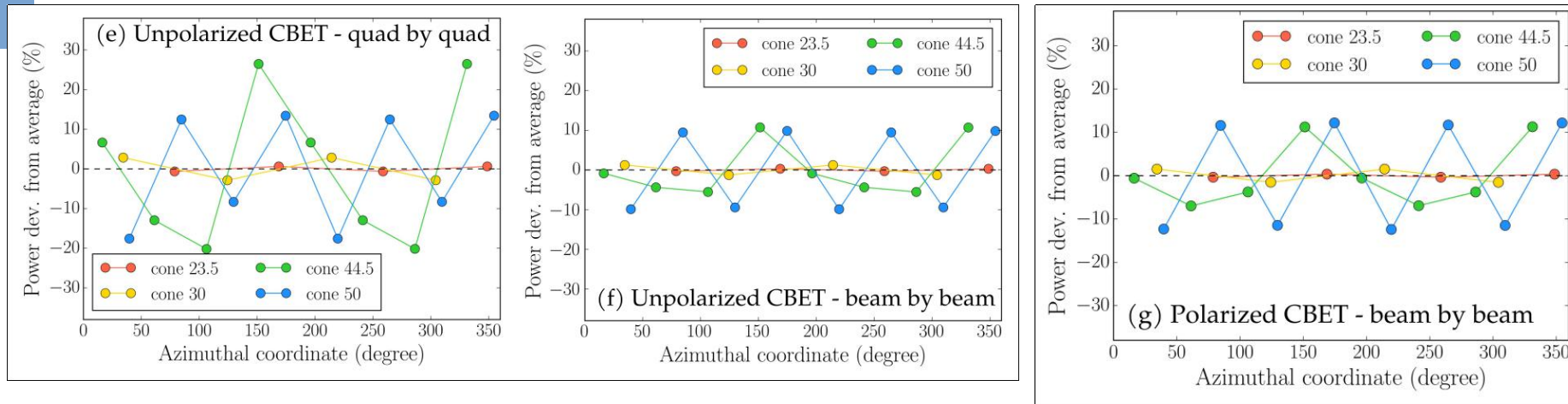


# THE POLARIZATION EFFECT HAS ONLY A MODEST EFFECT ON CONE FRACTION



- Cone-wise, there is little effect of polarization
- In more details; polarization effect leads to more energy transfer to outer beams in cone 30 and less to outer beams in cone 44.5

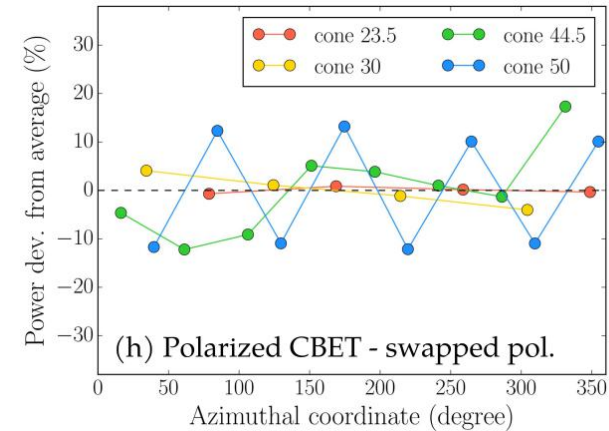
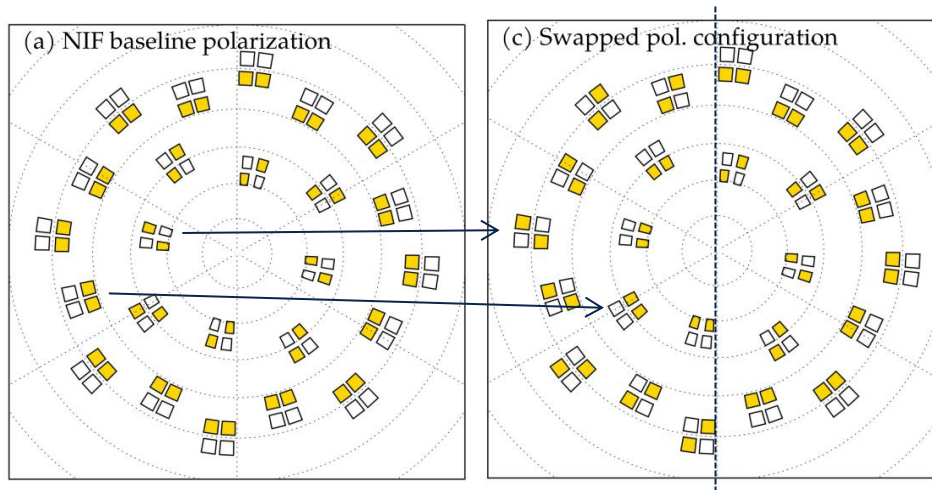
# THE LARGEST EFFECT ON THE DETAILS OF CBET IS THAT OF BEAM-BY-BEAM CALCULATION VS UNPOLARIZED QUADS



- Cone-wise, there is little effect of polarization
- In more details; polarization effect leads to more energy transfer to outer beams in cone 30 and less to outer beams in cone 44.5
- Computing the CBET beam by beam instead of quad by quad leads to less azimuthal variability in power amplification (polarized or unpolarized)



# THE POLARIZATION CONFIGURATION STILL MATTERS FOR SYMMETRY



- Cone-wise, there is little effect of polarization
- In more details; polarization effect leads to more energy transfer to outer beams in cone 30 and less to outer beams in cone 44.5
- Computing the CBET beam by beam instead of quad by quad leads to less azimuthal variability in power amplification (polarized or unpolarized)
- ...but, polarization matters ! If the polarization configuration was not symmetric, the azimuthal power amplification would be non-symmetric

# CONCLUSIONS AND PERSPECTIVES

- Improving laser models in a consistent 3D inline framework is a strategy that pays off
- Direct-drive simulations for OMEGA with ASTER/IFRIIT are now able to reproduce most experimental results related to large scale dynamics: neutron quantities, low modes... some limitations remain (stalk, high mode modeling coupled to CBET)
- Polarized CBET, in addition to current low modes, explains the observed anomaly of the last 2 years of OMEGA shots
- CBET must ultimately be mitigated altogether in a fusion driver. However, this will make current designs more vulnerable to system errors -> we also need schemes more robust to those

## Perspectives:

- CBET code validation at ignition scale (see D. Viala's talk)
- Use of CBET modeling to optimize illumination (see D. Barlow's talk)
- Modeling of foam for new designs (see R. Liotard's talk)
- Stalk ... ?