



Analysis of Element Size on Failure Model Performance

Introduction

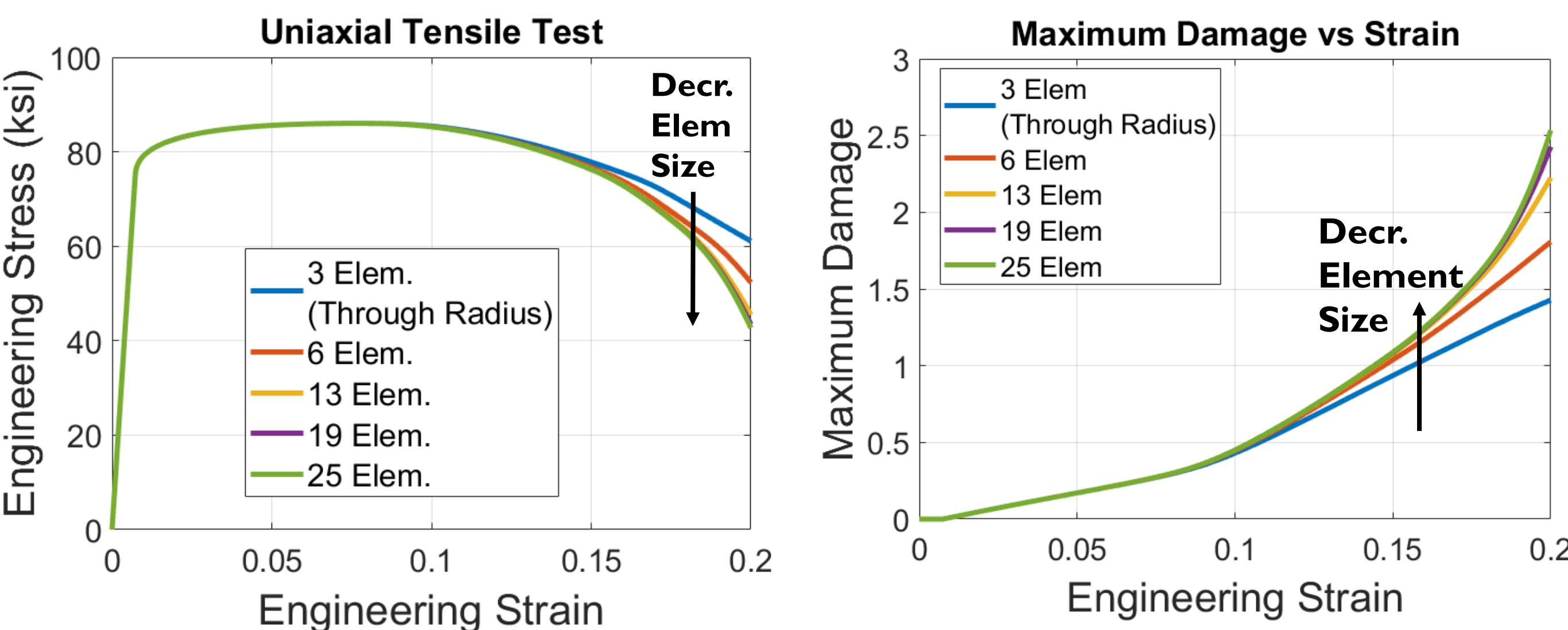
- For finite element simulations, minimum element size is often dictated by considerations like computation time, which makes very fine meshes impractical.
- Predictions of failure models are highly sensitive to element size.**
- 3 models of increasing complexity were studied to understand the effect of element size on failure predictions
- All models were constructed using 8 node hexahedral elements and used a J_2 plasticity constitutive model with power-law hardening, and Wilkins failure model.

$$\bar{\sigma} = \left(A(T) + B(T) \epsilon_{pl}^{n(T)} \right) \left(1 + C(T) \ln \left(\frac{\dot{\epsilon}}{\dot{\epsilon}_0} \right) \right)$$

$$D = \frac{1}{D_{crit}} \int_0^t \frac{(2-A)^\beta * \dot{\epsilon}^P}{\left(1 - \frac{P}{B} \right)^\alpha (1 + D_4 \ln \dot{\epsilon}^*) (1 + D_5 T^*)} dt$$

Example 1: Tensile Test (Quasi-static isothermal)

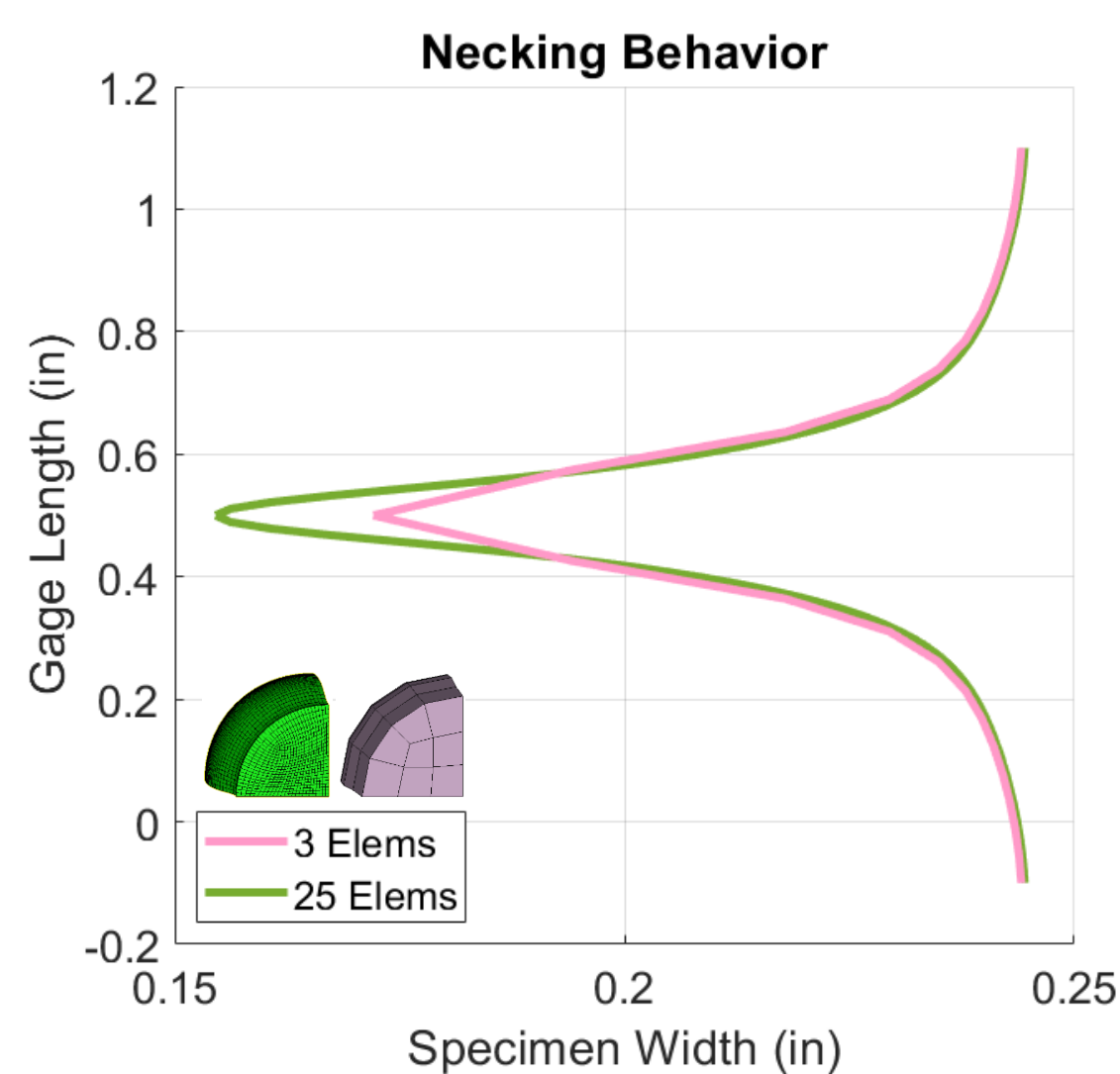
- Tensile specimens of varying element sizes were simulated to quantify the trend of damage for a simple stress state.



- Prior to ultimate, all perform the same
- Beyond ultimate, as element size decreases ↓:
 - Stress post-peak decreases ↓
 - Maximum damage increases ↑
- Necking phenomenon is captured better with smaller elements.

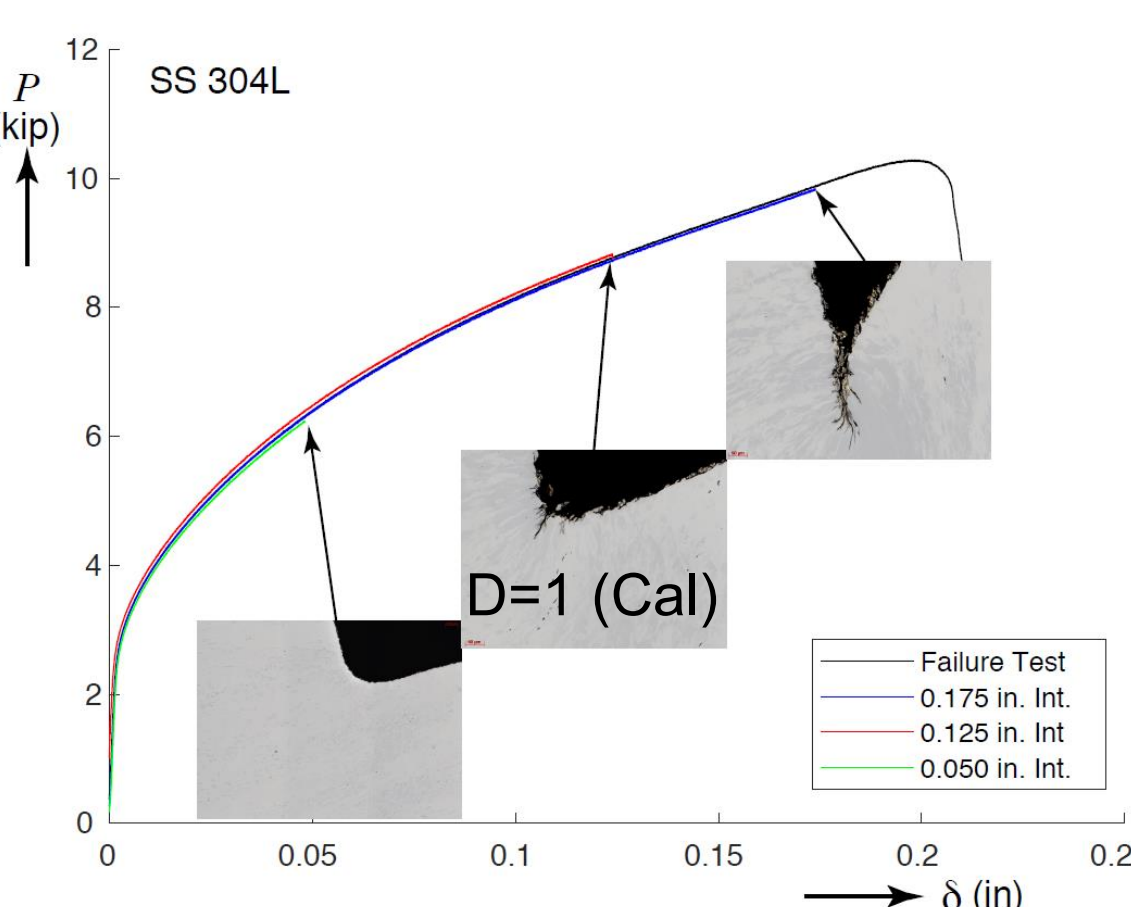
❖ **Higher geometric fidelity captures more localization.**

❖ **As element size decreases, maximum damage increases.**

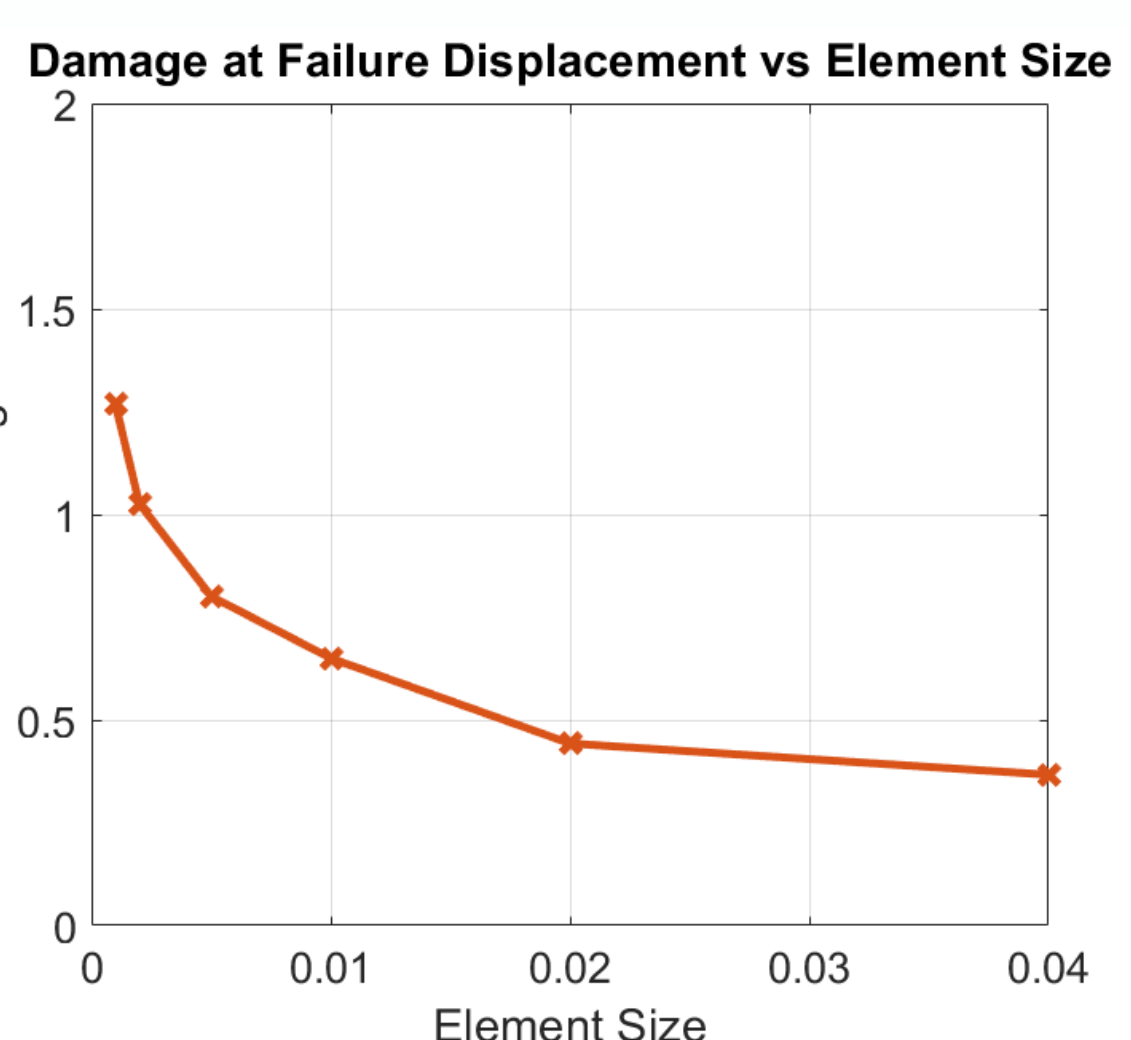


Example 2: Compression Hat (Quasi-static, isothermal)

- Interrupted shear failure test where crack growth was imaged at different displacements.
- Simulations of varying element size were conducted to understand the trend of damage for a model with large stress concentrators.
- ❖ Maximum damage decreases with increasing element size
- ❖ Smaller elements capture stress concentrations better.

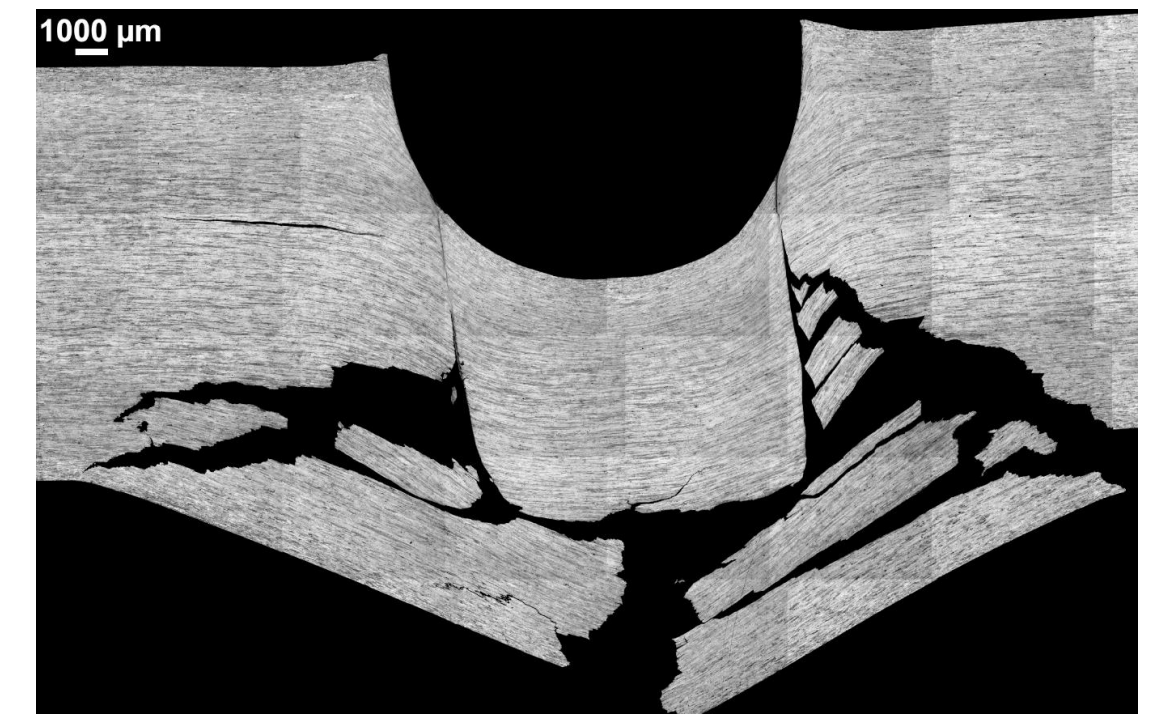


*Experiments performed by Amanda Jones [SNL]

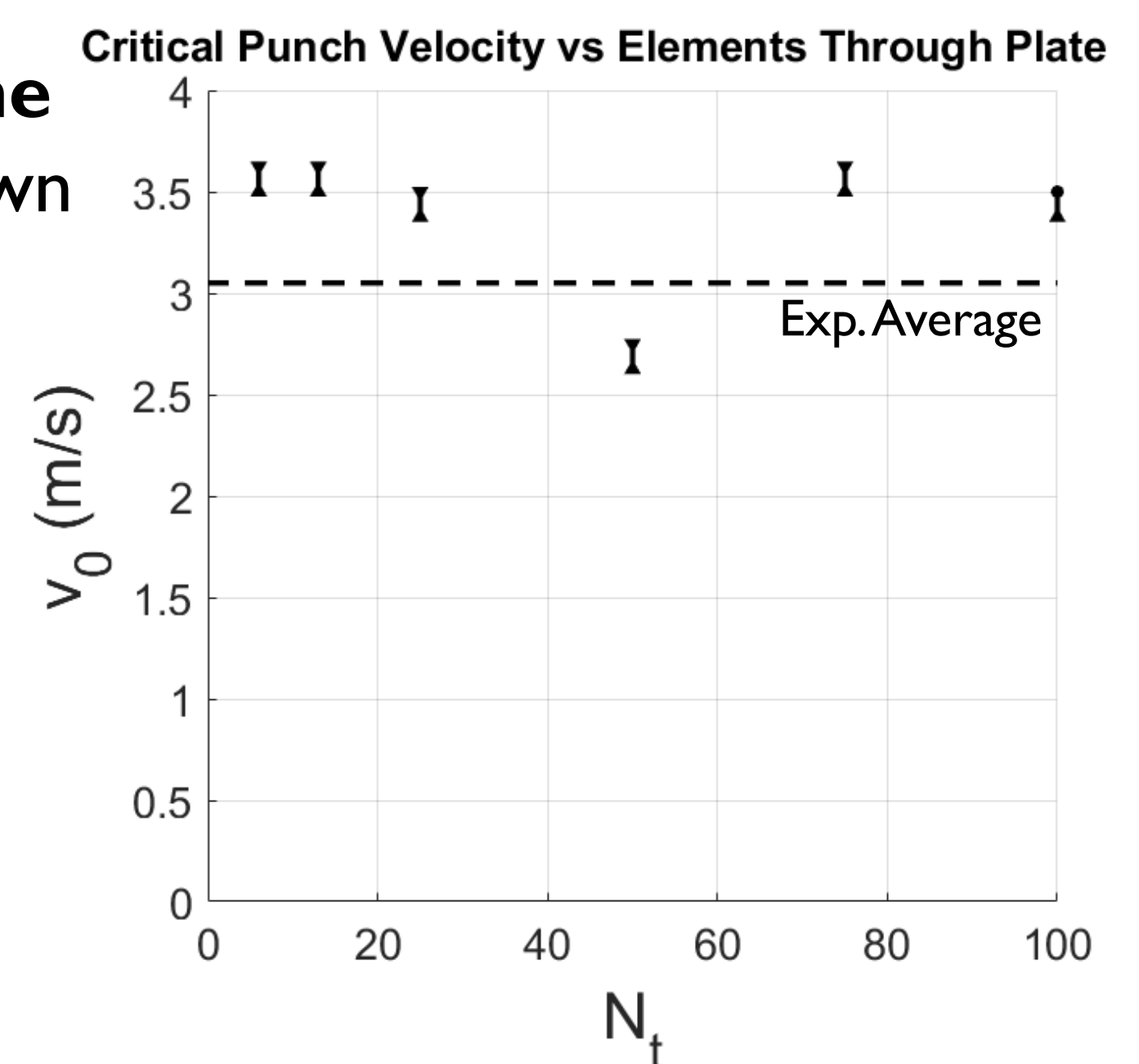


Example 3: Puncture Problem (Dynamic, adiabatic)

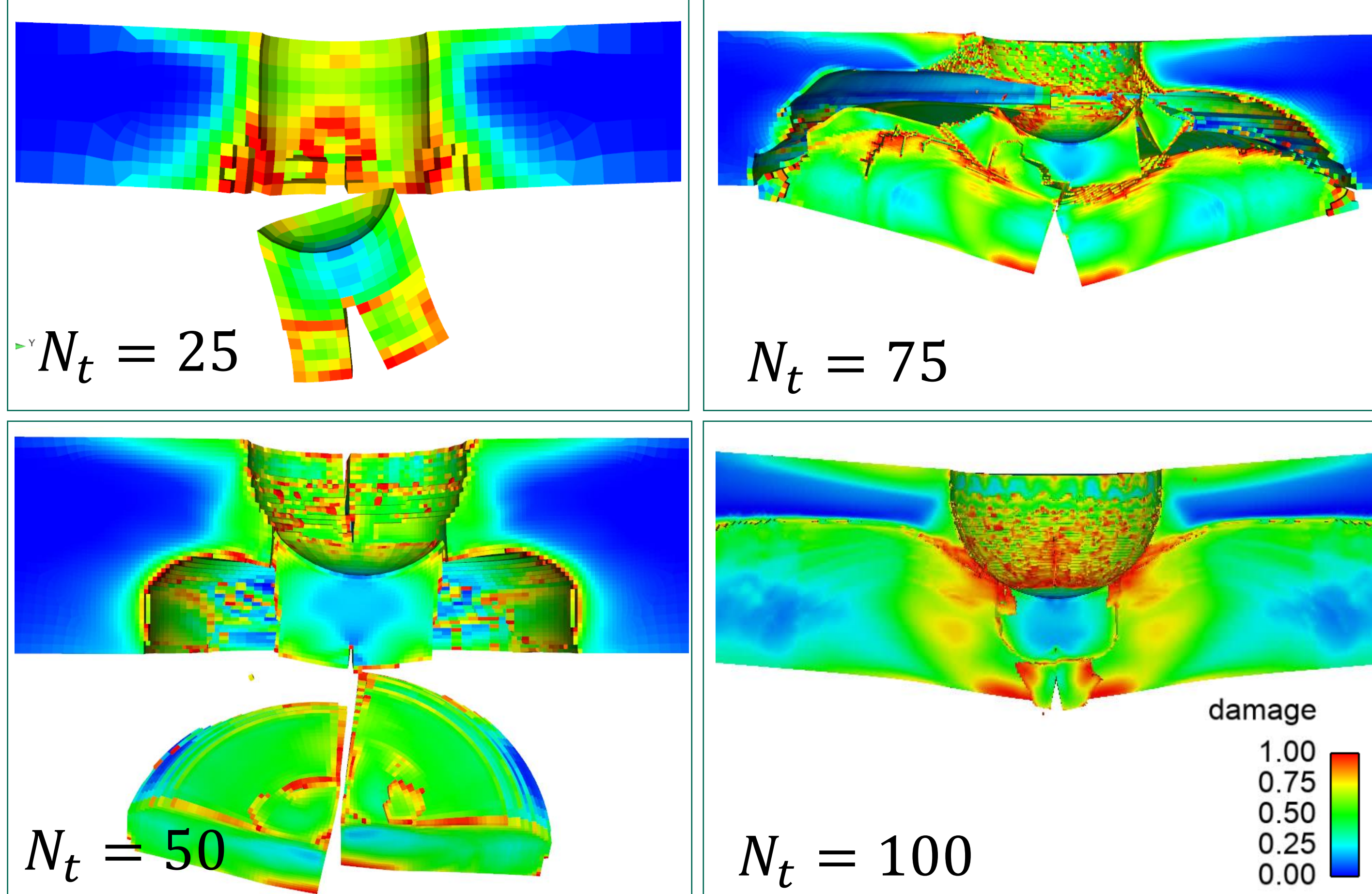
- 1/2 inch hemispherical punch attached to a falling mass, which contacts a 1/2 inch aluminum plate. Failure propagation was modeled by element death although the model was not calibrated for this.
- Critical punch velocity is the minimum velocity needed for breach where a bracket between breach and no breach was measured.
- Critical punch velocity was relatively mesh insensitive but not convergent.
- Experiments showed plugging failure with scabbing.
- As element size decreases the mode of failure changes (shown below)**
 - 25 Elements, no scabbing occurred
 - 50 elements, matches test.
 - 75 elements mostly scabbing occurred.
 - 100 elements, nonphysical behavior on contact.



*Experiments performed by Matt Spletzer [formerly SNL]



❖ **Problems requiring damage propagation may require fracture propagation calibrations that account for element size.**



Conclusions

- For failure initiation as element size decreases maximum damage increases.
- Using failure initiation criteria can lead to difficulties if failure propagation plays a role.
- Failure propagation likely requires further investigation.
- Analysts should use caution when modeling failure and making associated design decisions.

References

- [1] Johnson, G. R., and W. H. Cook. "Fracture Characteristics of Three Metals Subjected to Various Strains, Strain Rates, Temperatures and Pressures." *Eng. Fract. Mech.* 21, no. 1 (1985): 31–48.
- [2] Wilkins, M.L., R.D. Streit, and J.E. Reaugh. "Cumulative-Strain-Damage Model of Ductile Fracture," *LLNL* (1980). UCRL-53058
- [3] Corona, E., and C. Fietek. "Effects of Finite Element Discretization and Model Simplification on Calculations of Ductile Failure Initiation." *SNL* (2021). SAND2021-10905R