



GBCs and the conjugate basis for both element-based and element-free solution of PDEs

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Workshop on Generalized Barycentric Coordinates in Computer Graphics
and Computational Mechanics, June 1-4, 2022, Ascona, Switzerland

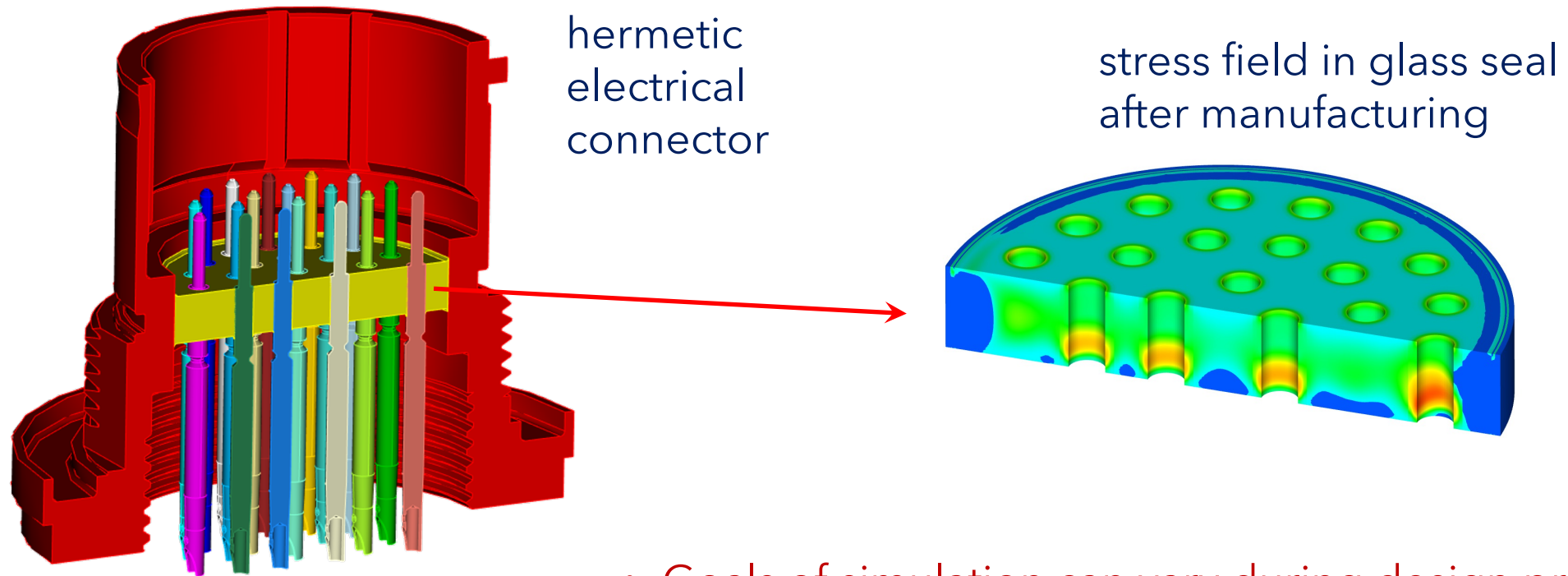
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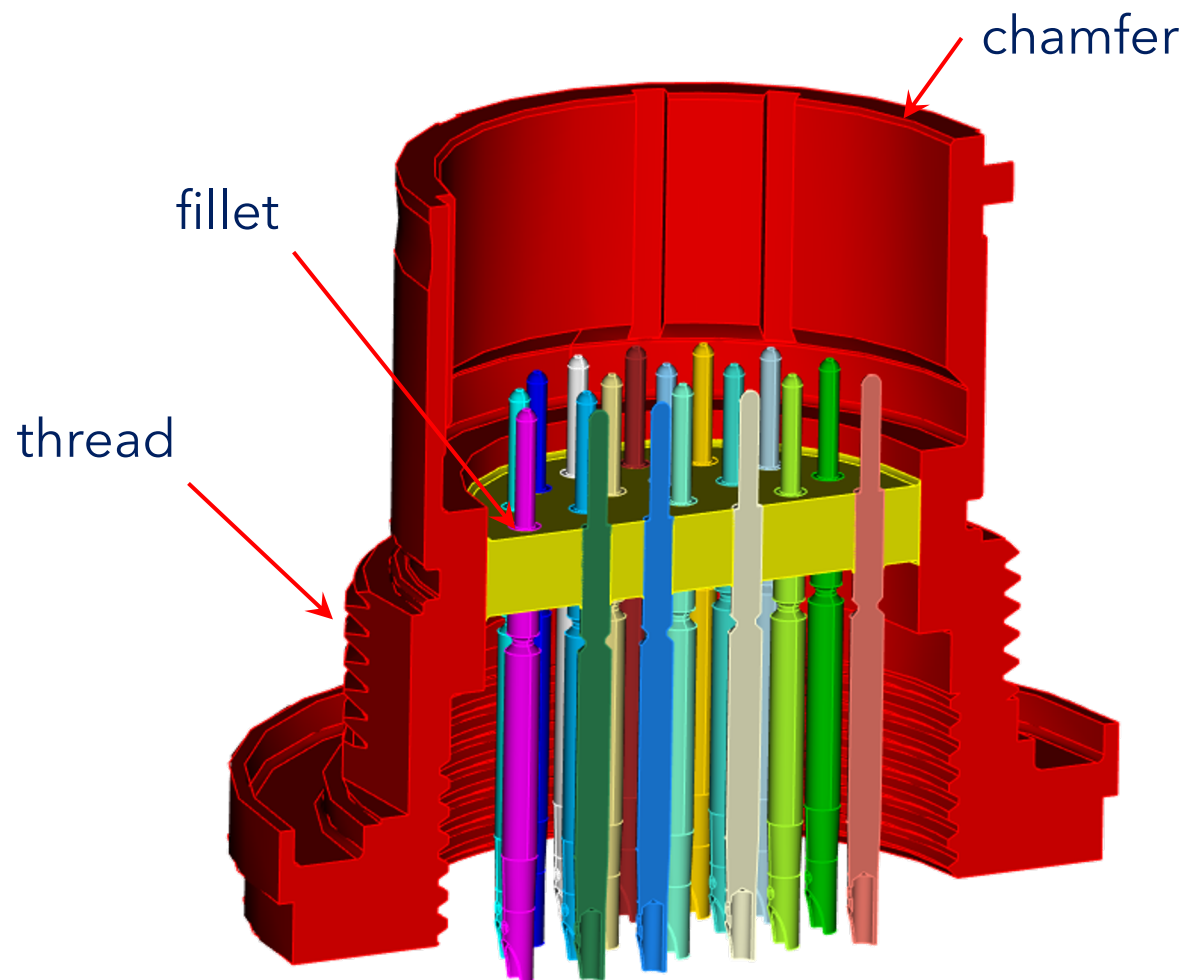
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Motivation: Agile simulation of complex assemblies



- Goals of simulation can vary during design process.
- Heuristics are often used to defeature geometry.
- Heuristics are used to construct finite element mesh.

Motivation: Typical domain (geometry) features



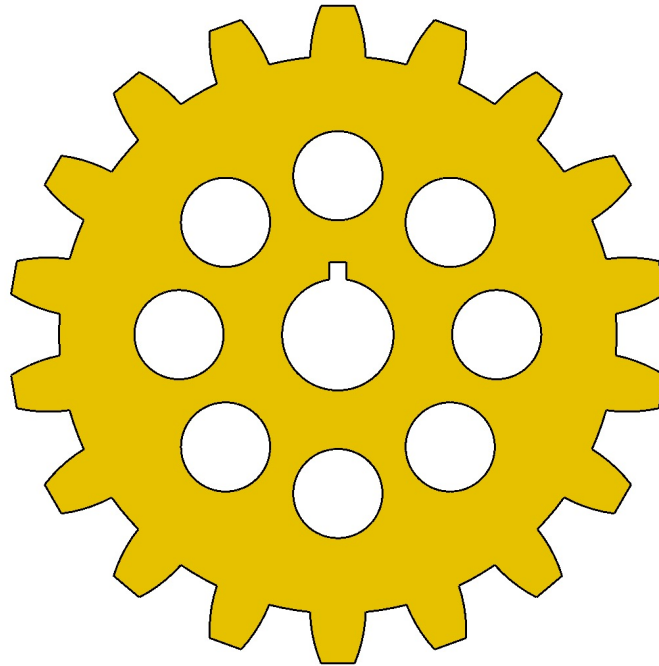
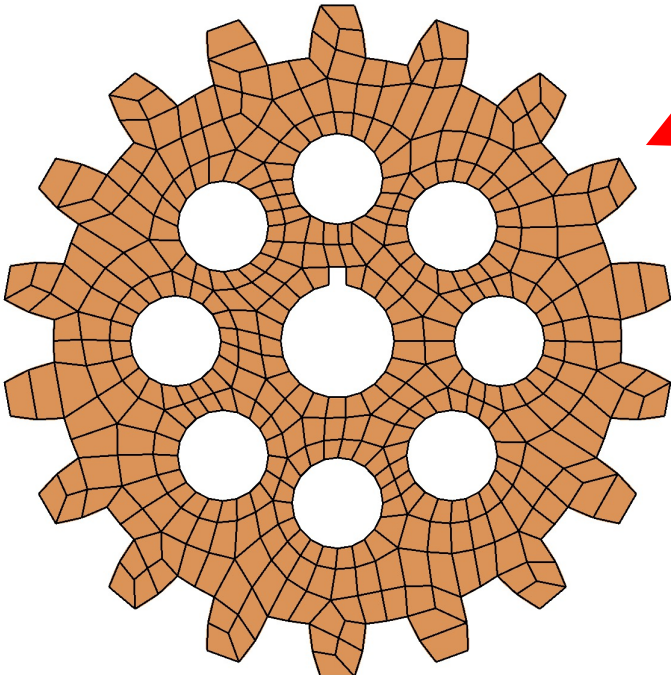
In engineering applications, domains typically contain numerous geometric features that are unimportant for the goals of the simulation.

Motivation

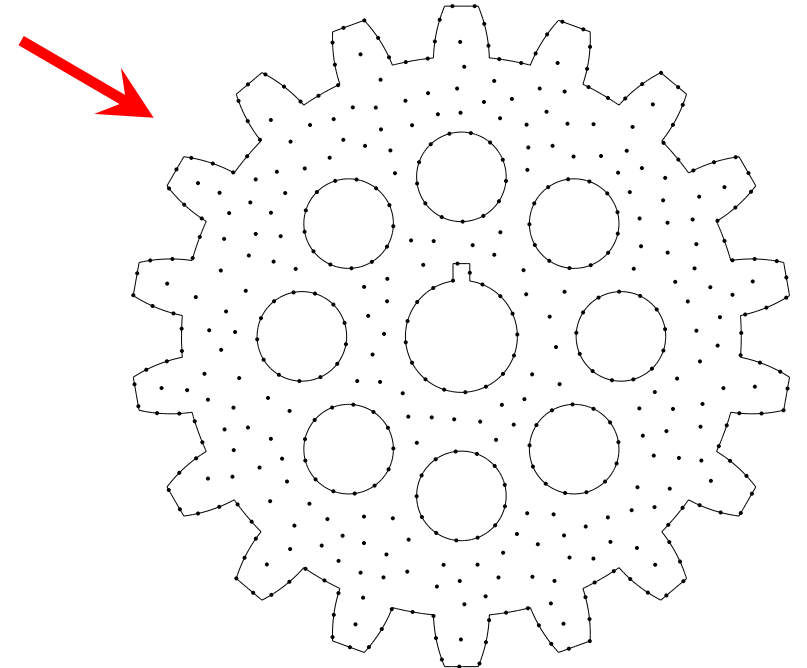


- GBCs provide framework for broad class of discretizations, both element based and element free.
- Can unify both classes of discretizations.

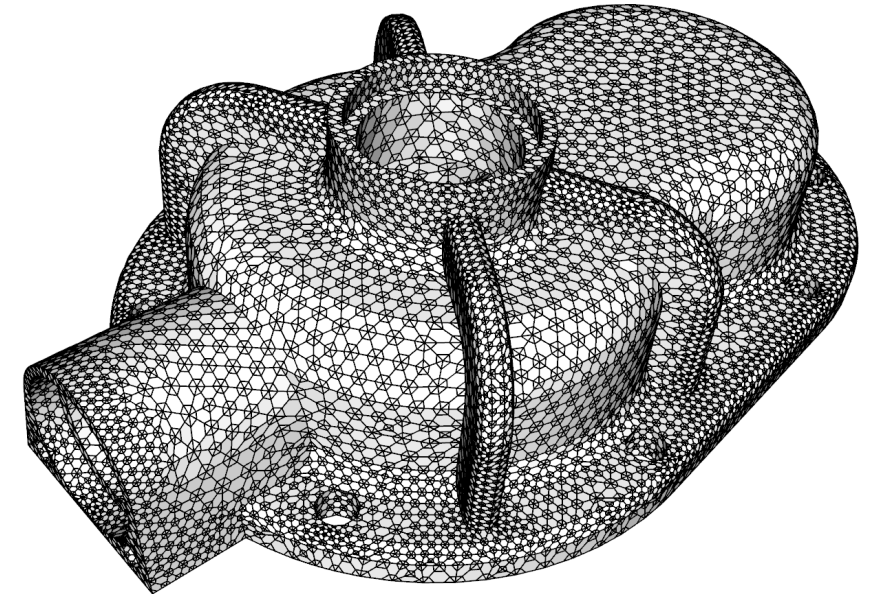
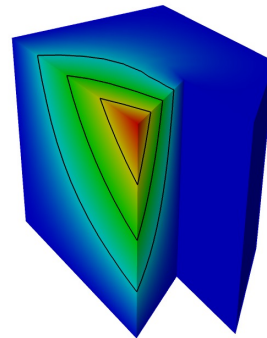
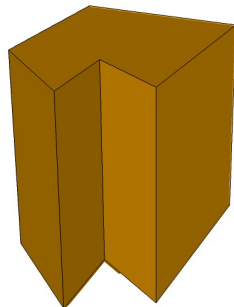
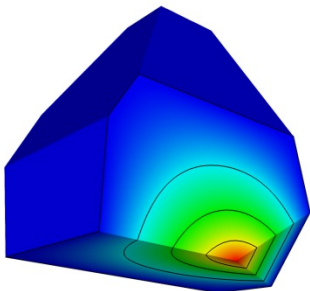
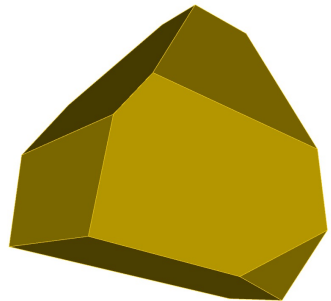
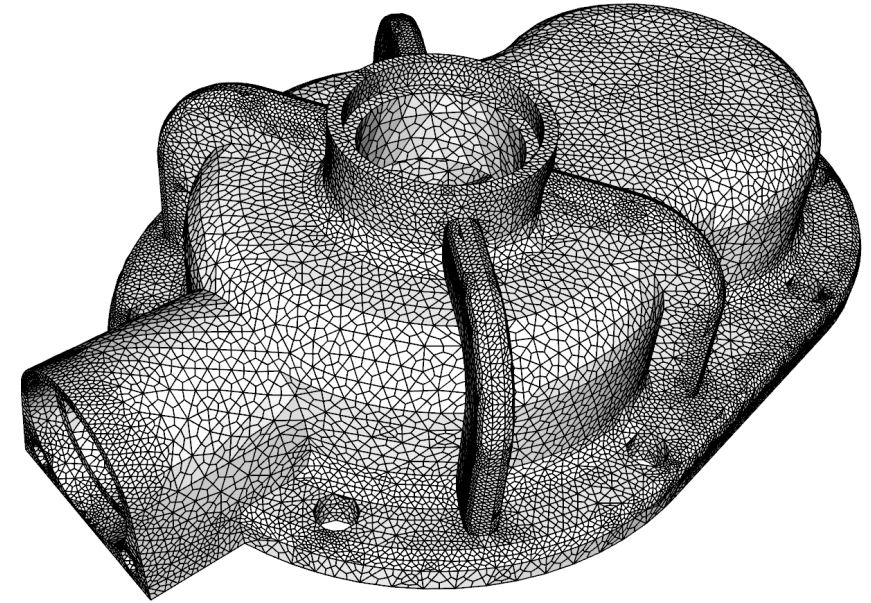
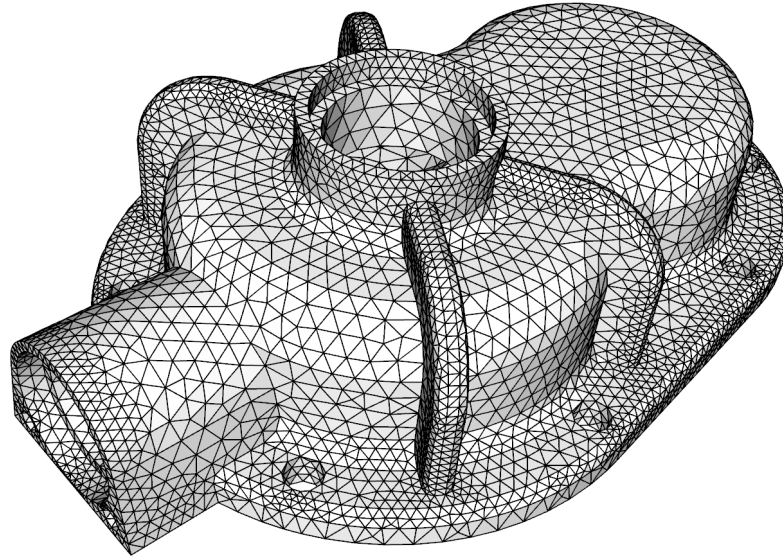
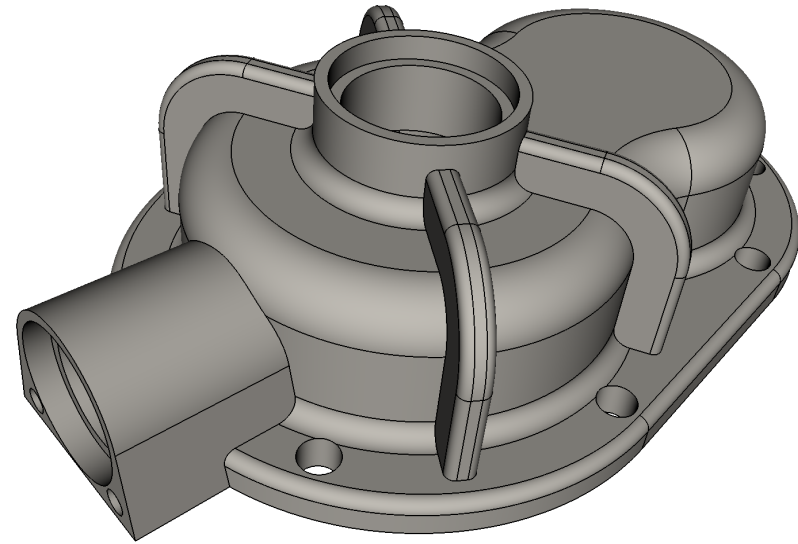
element based



element free



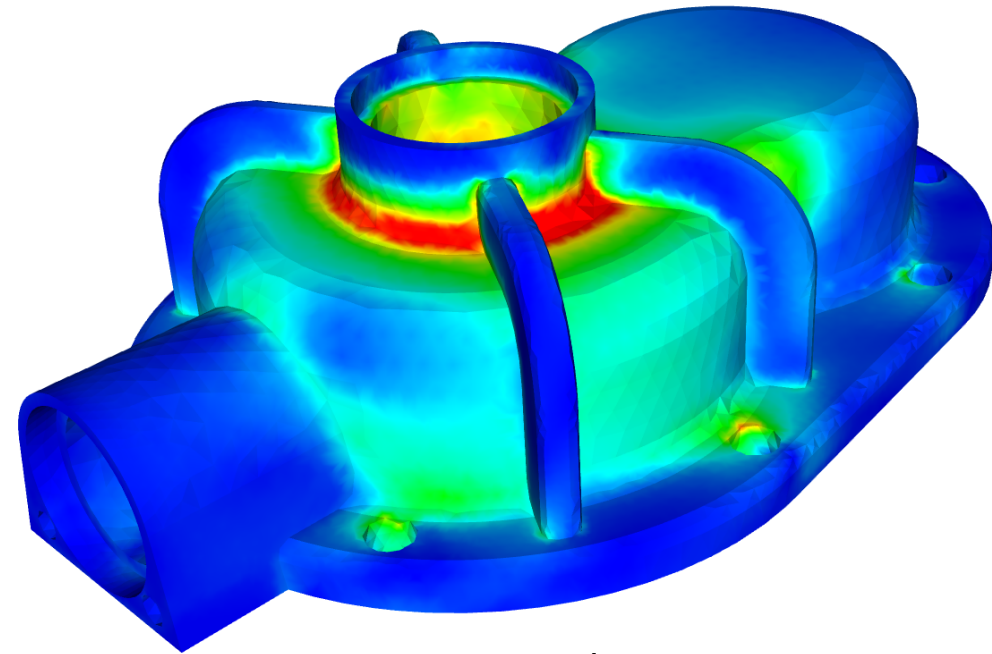
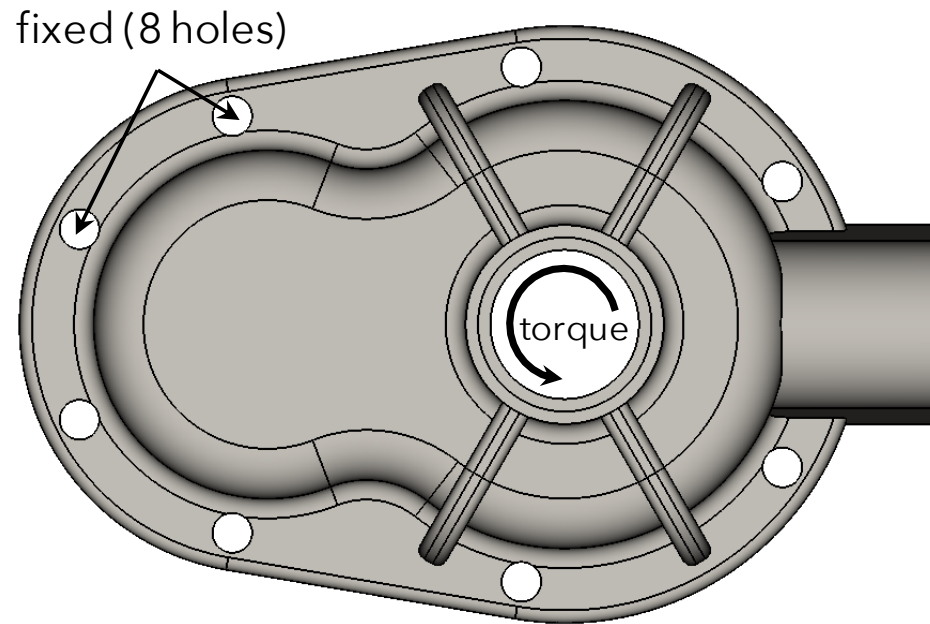
Motivation: element-based polyhedral discretizations



Motivation: element-based polyhedral discretizations



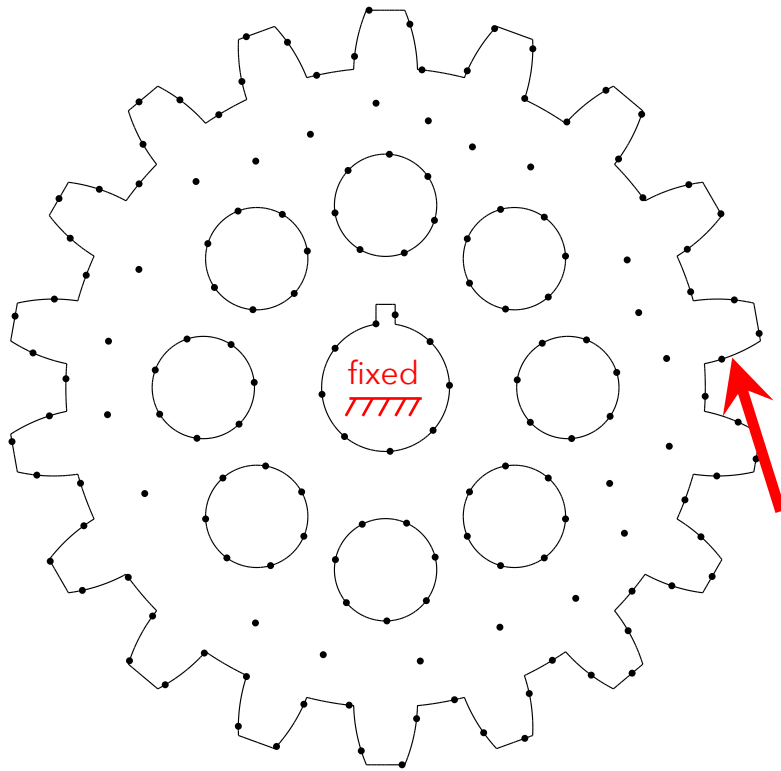
von Mises stress field



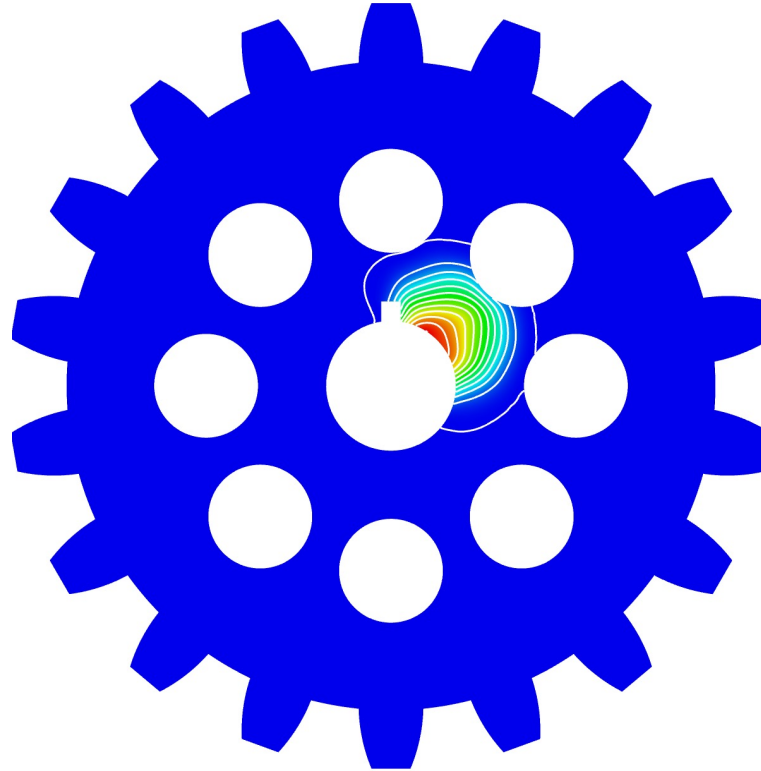
Motivation: element-free discretizations



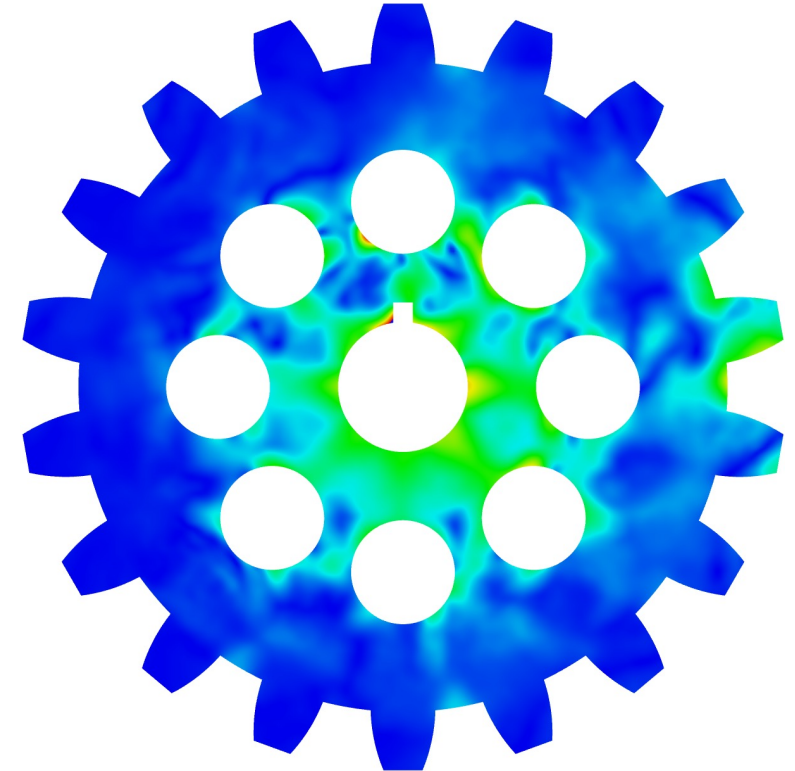
nodes



basis functions



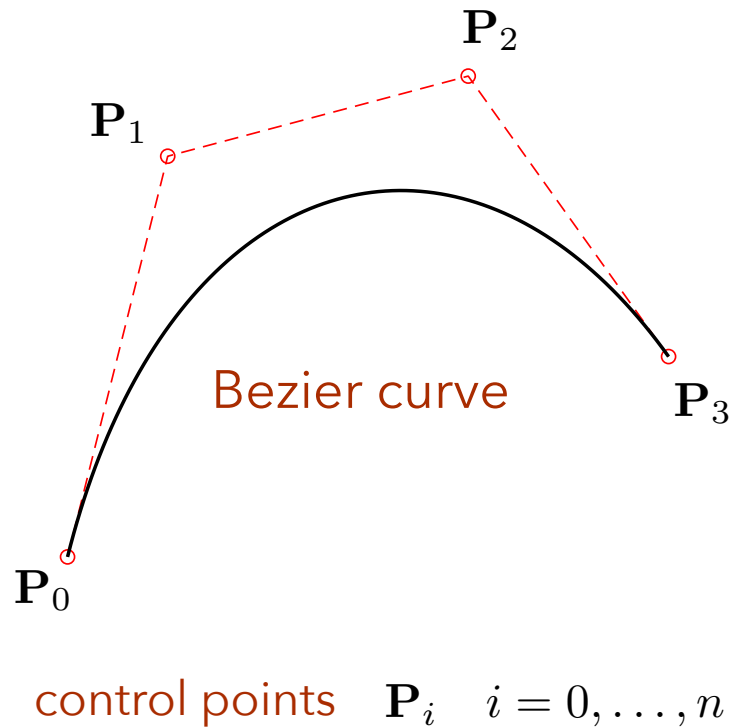
stress field (vm)



Outline

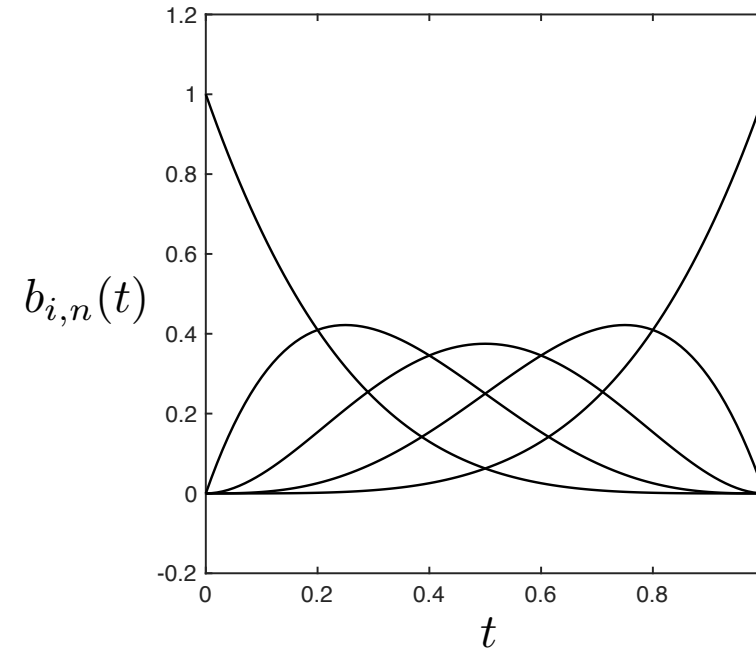
1. motivation
2. GBC approximation
3. GBC application to quadrature
4. conjugate basis
5. element-based applications
6. element-free applications (weight functions using manifold geodesics)
7. summary

Geometry to function approximation



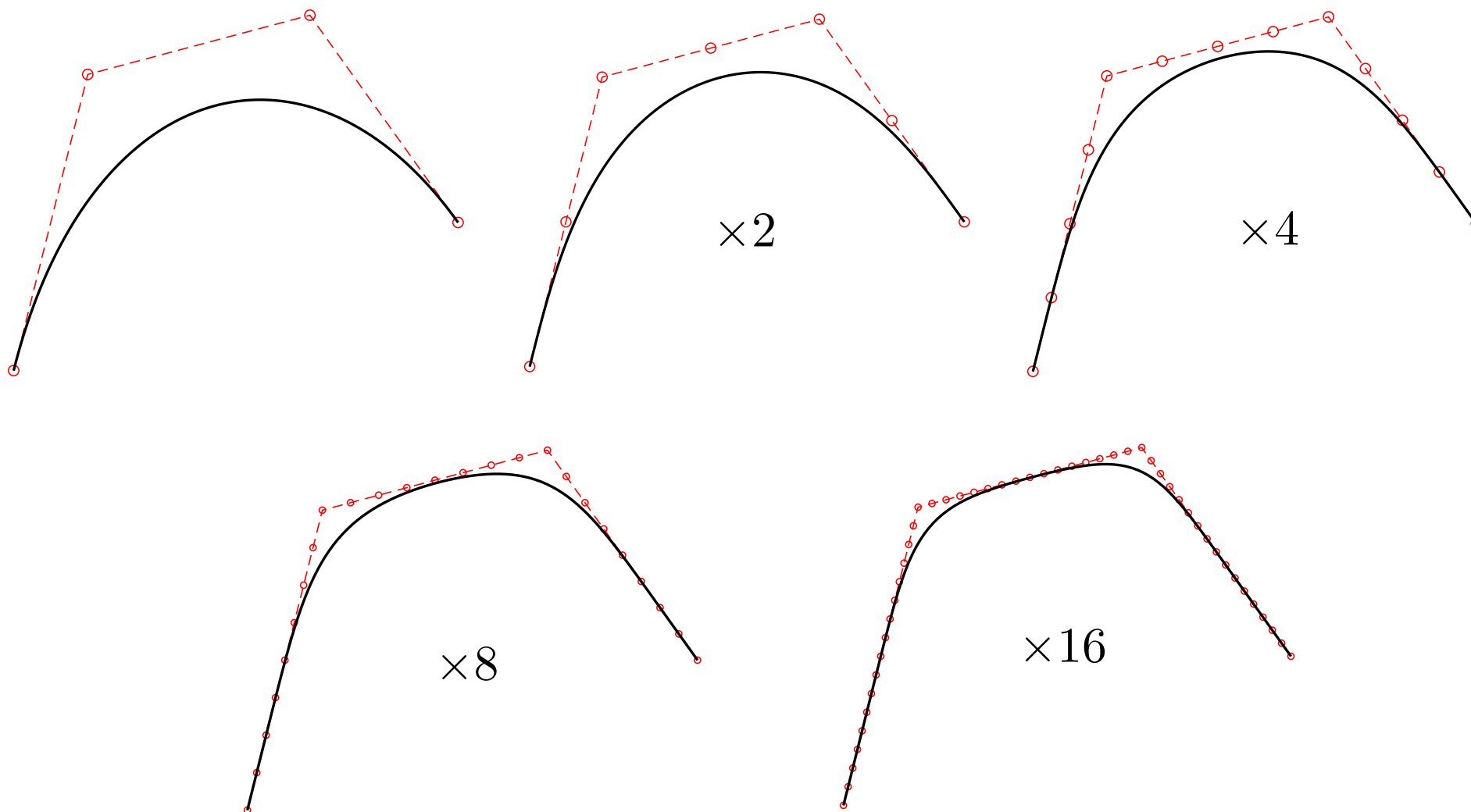
$$\mathbf{B}(t) := \sum_{i=0}^n \mathbf{P}_i b_{i,n}(t)$$

Bernstein polynomial $b_{i,n}(t)$



provide affine invariance (scaling, rotation)

Geometry to function approximation



Bernstein polynomial, a GBC-type approximation



Bernstein polynomial $B_n(t) := \sum_{i=0}^n \beta_n b_{i,n}(t)$

Bernstein basis polynomials of degree n

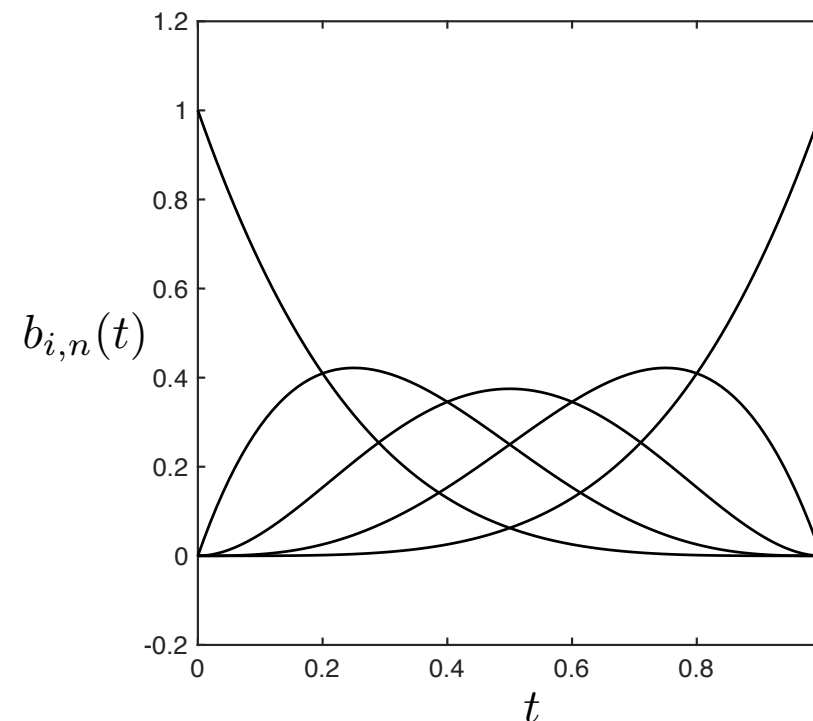
$$b_{i,n}(t) := \binom{n}{i} t^i (1-t)^{n-i}, \quad i = 0, \dots, n$$

$$\sum_{i=0}^n b_{i,n} = 1 \quad \text{partition of unity}$$

$$\sum_{i=0}^n \frac{i}{n} b_{i,n} = t \quad \text{linear reproduction}$$

affine invariance

Bernstein polynomial $b_{i,n}(t)$



Note that $b_{i,n}(t)$ are not interpolating except at endpoints.

Function approximation using Bernstein polynomials



Weierstrass approximation theorem: constructive proof that polynomials are dense in $C[0,1]$.

Theorem: Let f be a continuous function on the interval $[0,1]$. Then the Bernstein polynomial $B_n(f)(x)$ given by

$$B_n(f)(x) := \sum_{i=0}^n f\left(\frac{i}{n}\right) b_{i,n}(x)$$

converges uniformly to $f(x)$ on the interval $[0,1]$.

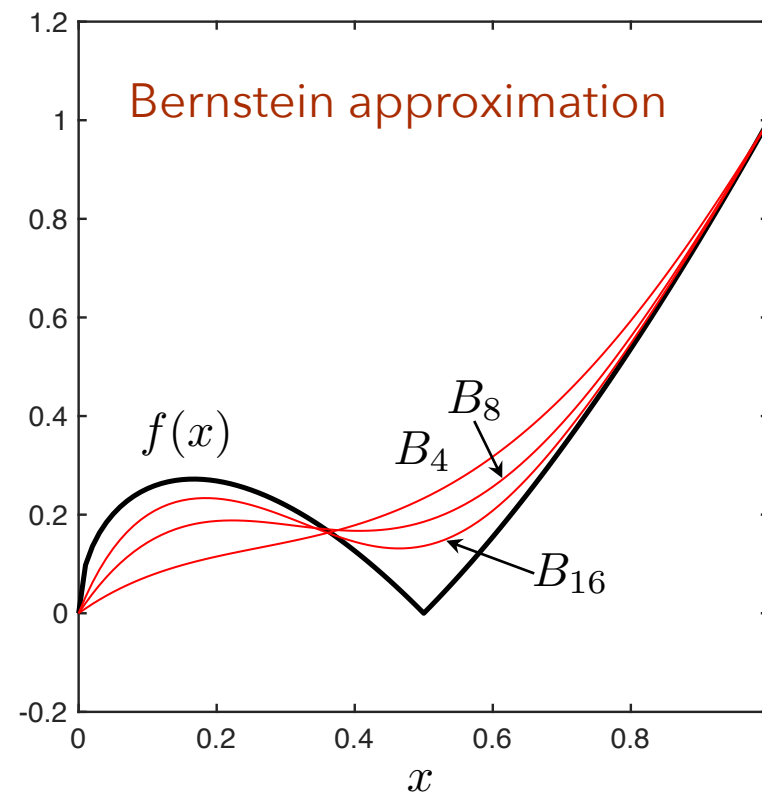
$$\lim_{n \rightarrow \infty} B_n(f)(x) = f(x)$$

convergence is uniform

Example: Function approximation using Bernstein polynomials

Let $f(x) = |2x - 1|\sqrt{x}$

$$B_n(x) := \sum_{i=0}^n f\left(\frac{i}{n}\right) b_{i,n}(x)$$



Key observations:

- Bernstein basis polynomials have global support.
- Bernstein polynomials are not interpolatory, but still converge because of linear consistency.
- Approximation involves product of functional and basis.
- Can we generalize to any GBC? (yes!)

Example: Function approximation using moving-least-squares basis

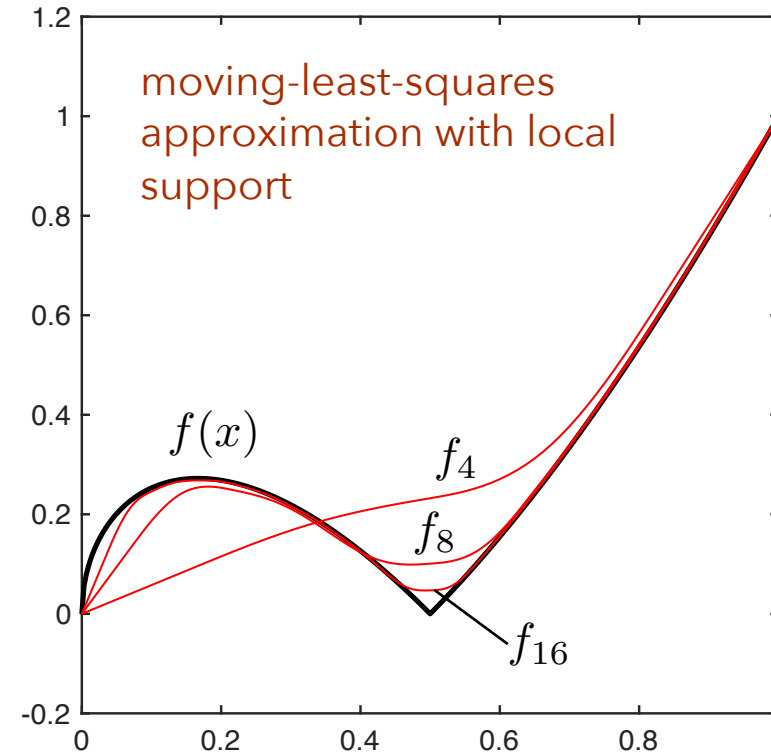
$$f(x) = |2x - 1|\sqrt{x}$$

$$f_N = \sum_{K=1}^N f(x_K)\phi_K(x)$$

$\phi_K(x)$ are MLS basis functions
with local support

Observations:

- Approximation still converges uniformly.
- Convergence is faster with local support.



Function approximation using GBCs on general domains

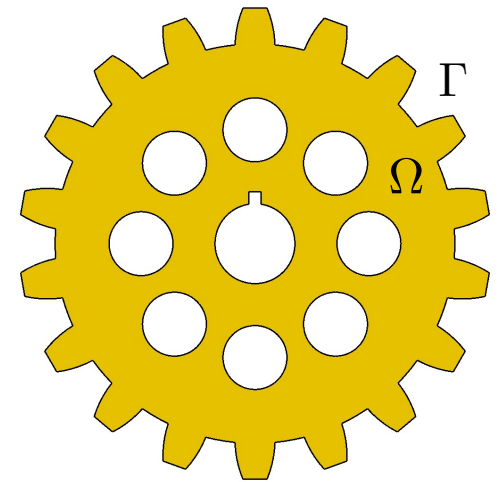


Theorem:

Let f be a continuous function on the domain Ω . Suppose $\{\phi_K(\mathbf{x}), K = 1, \dots, N\}$ forms a partition of unity and each function ϕ_K has local support of size h . Then the GBC approximation $f_h(\mathbf{x})$ given by

$$f_h(\mathbf{x}) := \sum_K f(\mathbf{x}_K) \phi_K(\mathbf{x})$$

converges uniformly to $f(\mathbf{x})$ on $\bar{\Omega}$.



$$\lim_{h \rightarrow 0} f_h(x) = f(x)$$

convergence is uniform

GBC application to quadrature

Will be used in applications to PDE solution.

Application to quadrature



Since $\lim_{h \rightarrow 0} f_h(x) = f(x)$ uniformly, it follows that $\int_{\Omega} f_h(\mathbf{x}) d\Omega \rightarrow \int_{\Omega} f(\mathbf{x}) d\Omega$

with $\left| \int f_h(\mathbf{x}) d\Omega - \int f(\mathbf{x}) d\Omega \right| \leq \int |f_h(\mathbf{x}) - f(\mathbf{x})| d\Omega \leq \int \varepsilon d\Omega = V \cdot \varepsilon$

Can obtain rates of convergence using Taylor's theorem.

$$f_h(\mathbf{x}) := \sum_K f(\mathbf{x}_K) \phi_K(\mathbf{x})$$

then $\int f_h(\mathbf{x}) d\Omega = \sum_K f(\mathbf{x}_K) \underbrace{\int \phi_K(\mathbf{x}) d\Omega}$

Define quadrature weight as $w_K = \int_{\Omega} \phi_K(\mathbf{x}) d\Omega$

$$\int f_h(\mathbf{x}) d\Omega = \sum_K w_K f(\mathbf{x}_K) \approx \int f(\mathbf{x}) d\Omega$$

$$w_K = \int_{\Omega} \phi_K(\mathbf{x}) d\Omega$$



Note that
$$\sum_K w_K = \sum_K \int_{\Omega} \phi_K(\mathbf{x}) d\Omega = \int_{\Omega} \sum_K \phi_K(\mathbf{x}) d\Omega = \int_{\Omega} 1 d\Omega = V$$

Also, since
$$\sum_K \mathbf{x}_K \phi_K(\mathbf{x}) = \mathbf{x}$$

then
$$\sum_K w_K \mathbf{x}_K = \sum_K \int_{\Omega} \phi_K(\mathbf{x}) \mathbf{x}_K d\Omega = \int_{\Omega} \sum_K \mathbf{x}_K \phi_K(\mathbf{x}) d\Omega = \int_{\Omega} \mathbf{x} d\Omega$$

Now have a second-order integration scheme that can integrate linear functions exactly.

$$\sum_K w_K = V$$

$$\sum_K w_K \mathbf{x}_K = \int_{\Omega} \mathbf{x} d\Omega$$

Can extend to higher-order integration using higher-order reproducing conditions.

Quadrature example in 1D



For Bernstein approximation:

recall $B_n(x) := \sum_{i=0}^n f\left(\frac{i}{n}\right) b_{i,n}(x)$

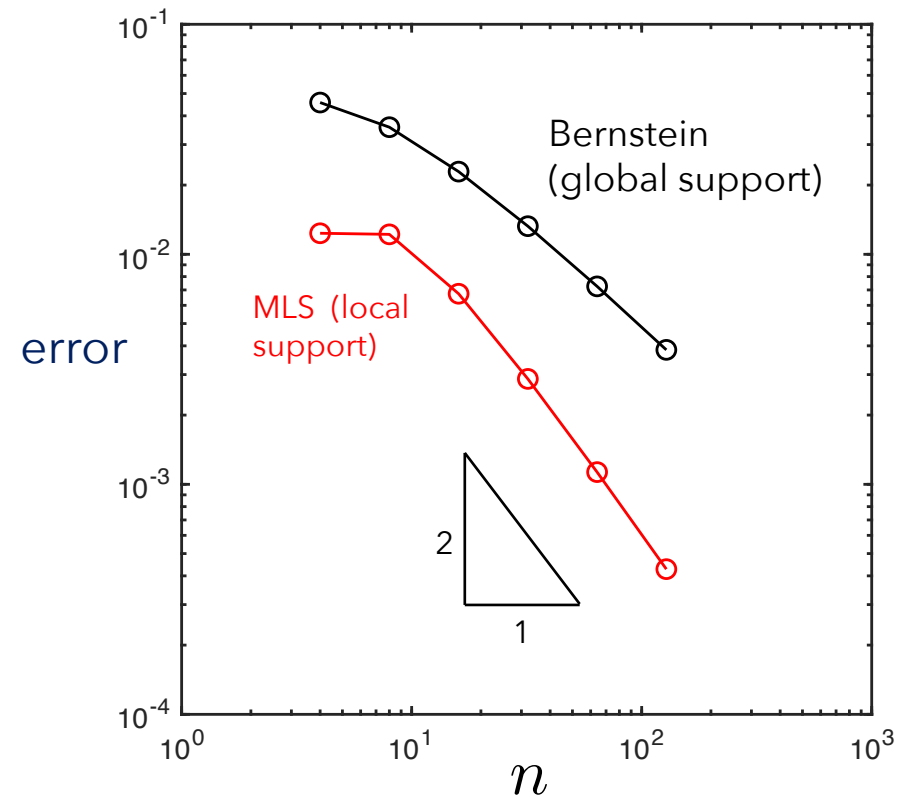
$$\int_0^1 b_{i,n}(x) dx = \frac{1}{n+1} = w_i$$

$$\int_0^1 f(x) dx \approx \int_0^1 B_n(f)(x) dx = \frac{1}{n+1} \sum_{i=0}^n f\left(\frac{i}{n}\right)$$

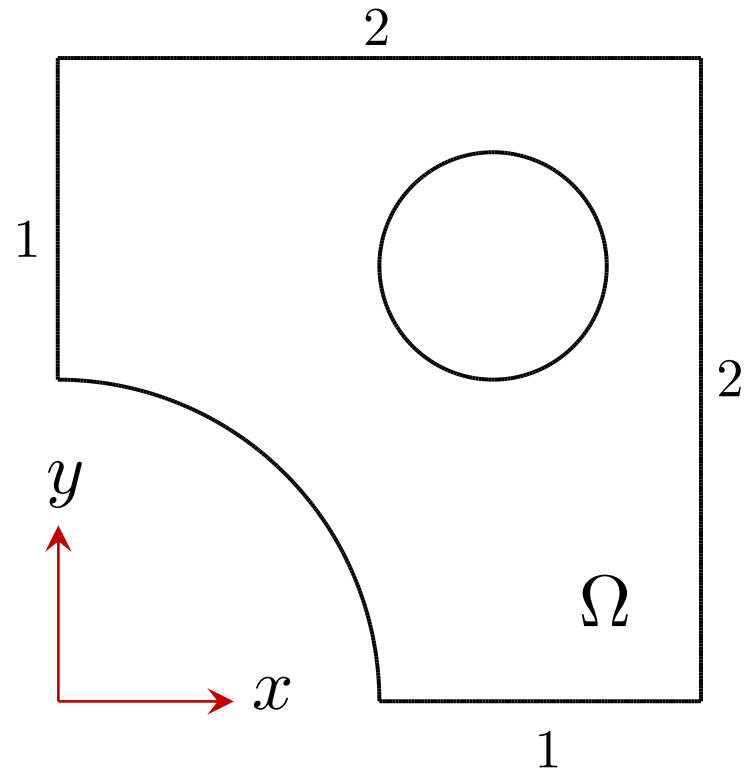
~ midpoint rule

Of course, Gauss rules are much more efficient, but are not generalizable to arbitrary domains.

Let $f(x) = |2x - 1|\sqrt{x}$



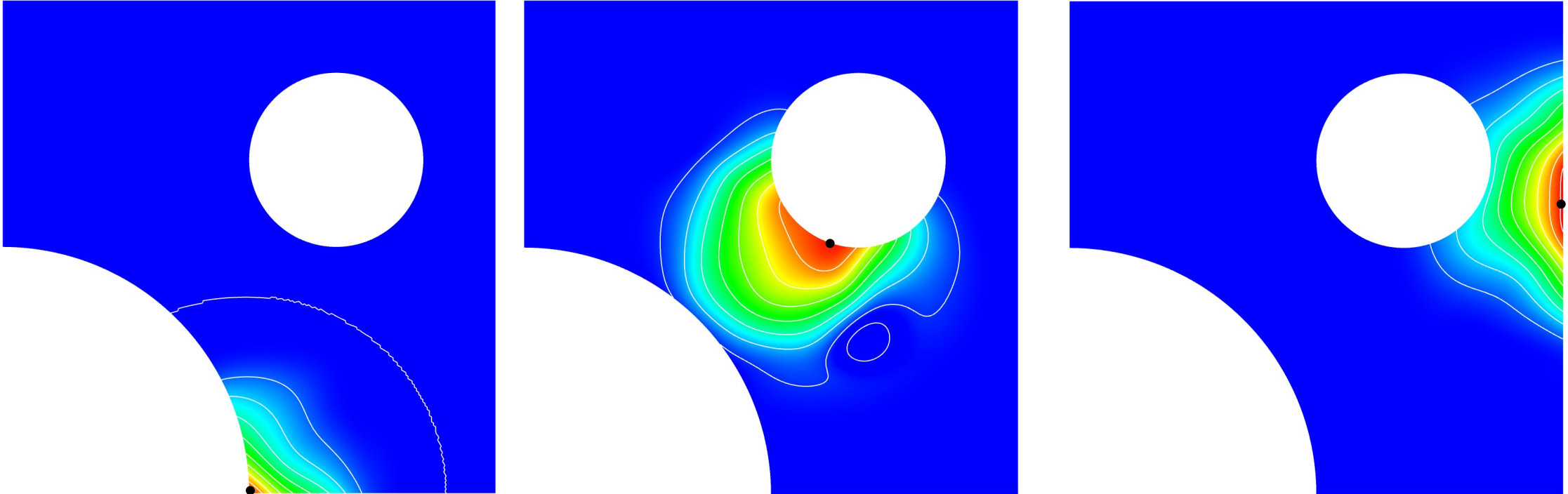
Quadrature example in 2D



$$f(x, y) = \sin(\pi x/2) \sin(\pi y)$$

$$\text{error} := \left| \sum_K w_K f(\mathbf{x}_K) - \int_{\Omega} f d\Omega \right|$$

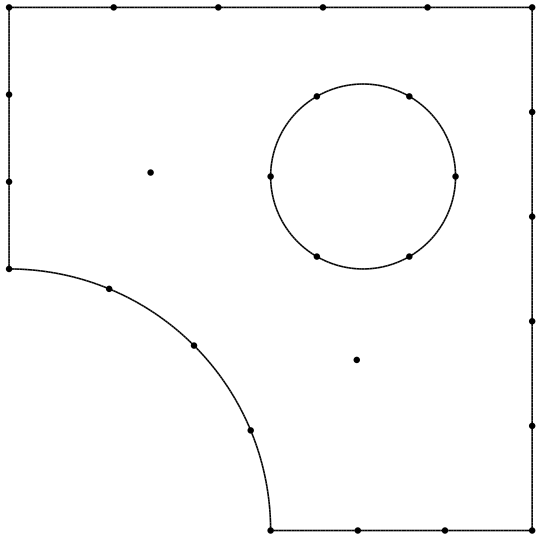
GBC element-free basis functions



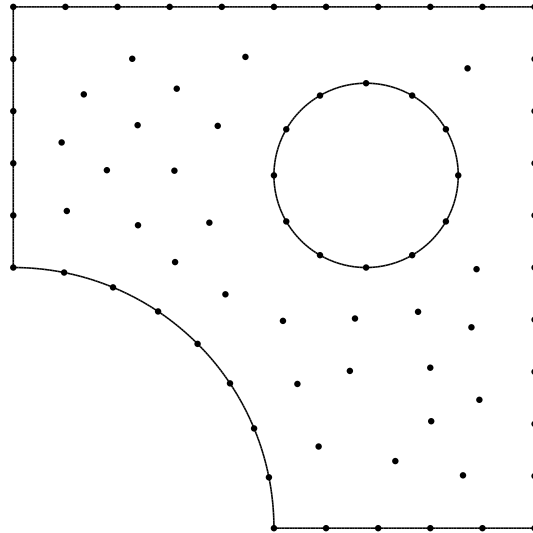
Quadrature example



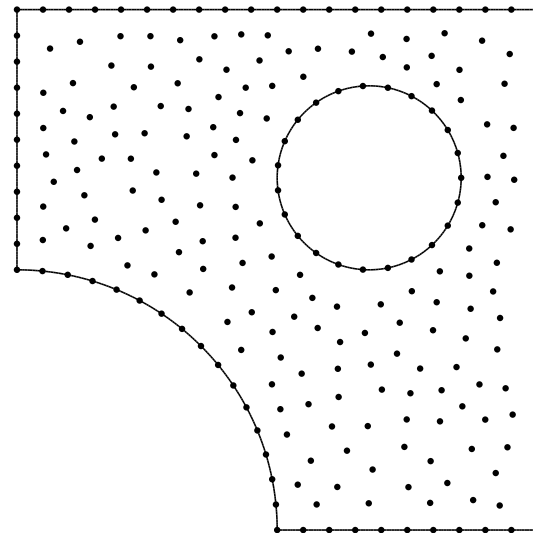
$H = 0.4$



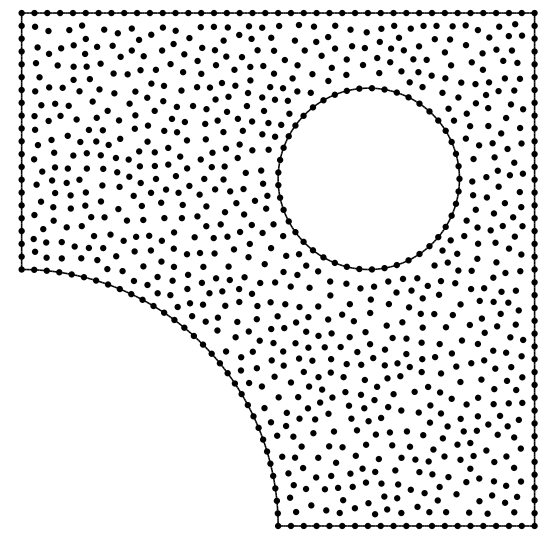
$H = 0.2$



$H = 0.1$



$H = 0.05$

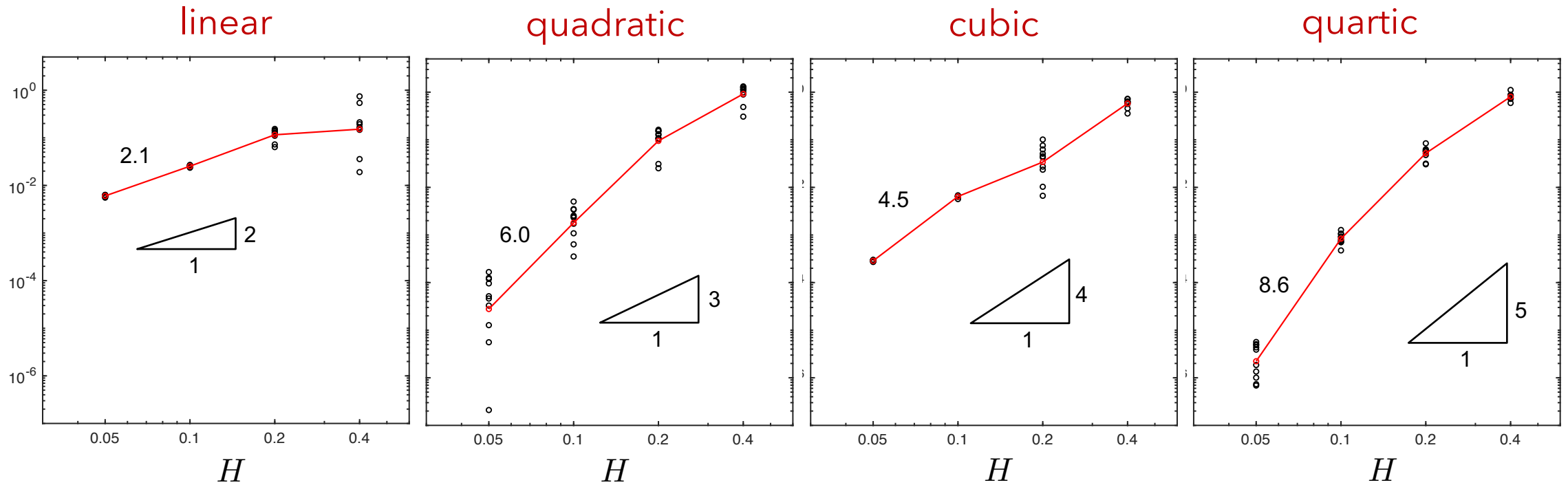


Evaluate error for 10 realizations.

Quadrature convergence



$$\text{error} := \left| \sum_K w_K f(\mathbf{x}_K) - \int_{\Omega} f d\Omega \right|$$



Note: seeing convergence rates greater than $p + 1$

Conjugate (dual) basis

Will be used in applications to PDE solution.

Conjugate basis



Consider a set of linearly independent GBCs $\{\Phi_I\}$

It will be useful in the formulation of both element-based and element-free solutions of PDEs to project function gradients to this basis.

The projection can be written in terms of the conjugate (dual) basis $\{\Phi^J\}$

$$(\Phi_I, \Phi^J) = \delta_I^J \quad \text{bi-orthogonal}$$

Define G_{IJ} as the Gram matrix for the basis

$$G_{IJ} := \int_{\Omega} \Phi_I \Phi_J d\Omega$$

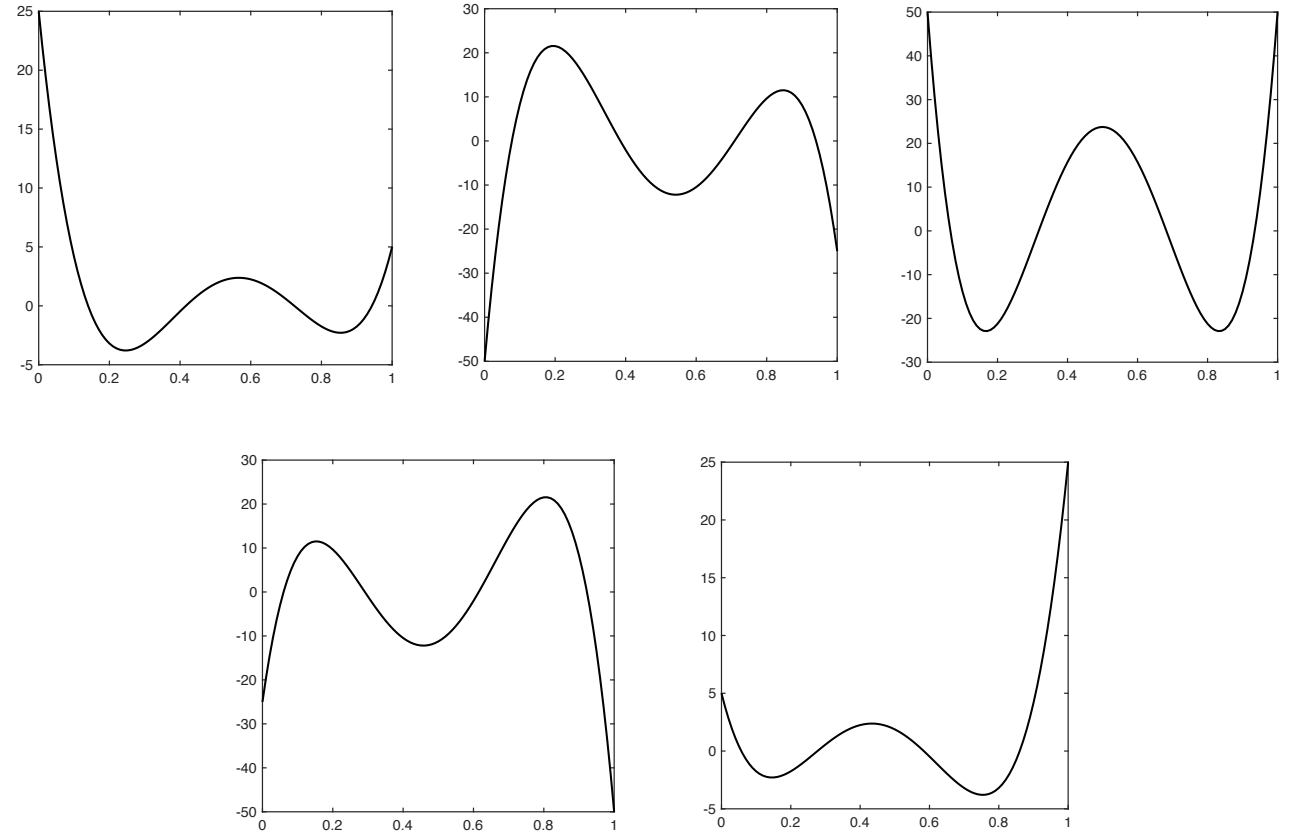
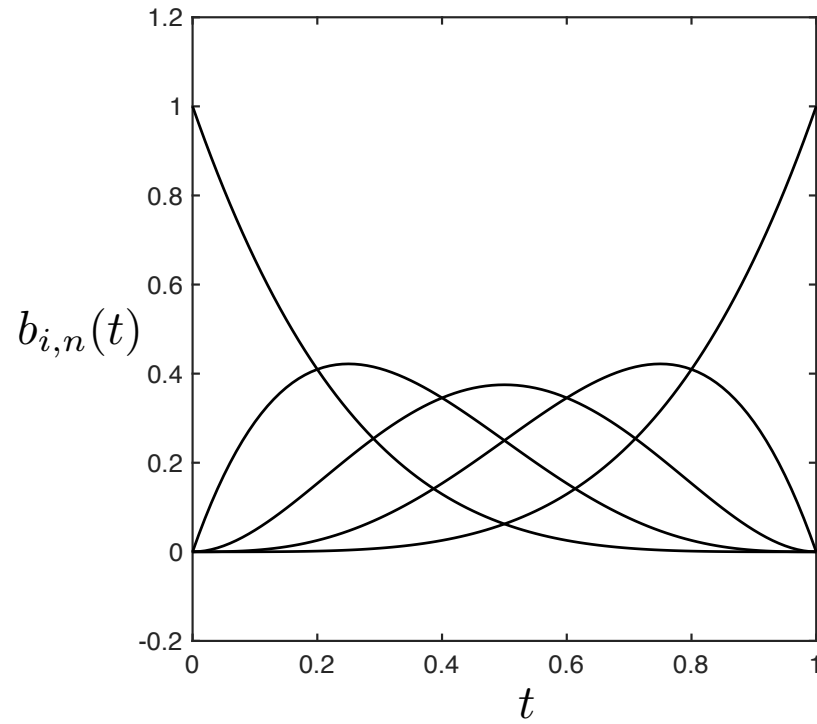
Can show that $\Phi^I = G^{IJ} \Phi_J$ and $\Phi_I = G_{IJ} \Phi^J$ where $G^{IJ} = (G_{IJ})^{-1}$

Conjugate basis example: Bernstein



conjugate functions

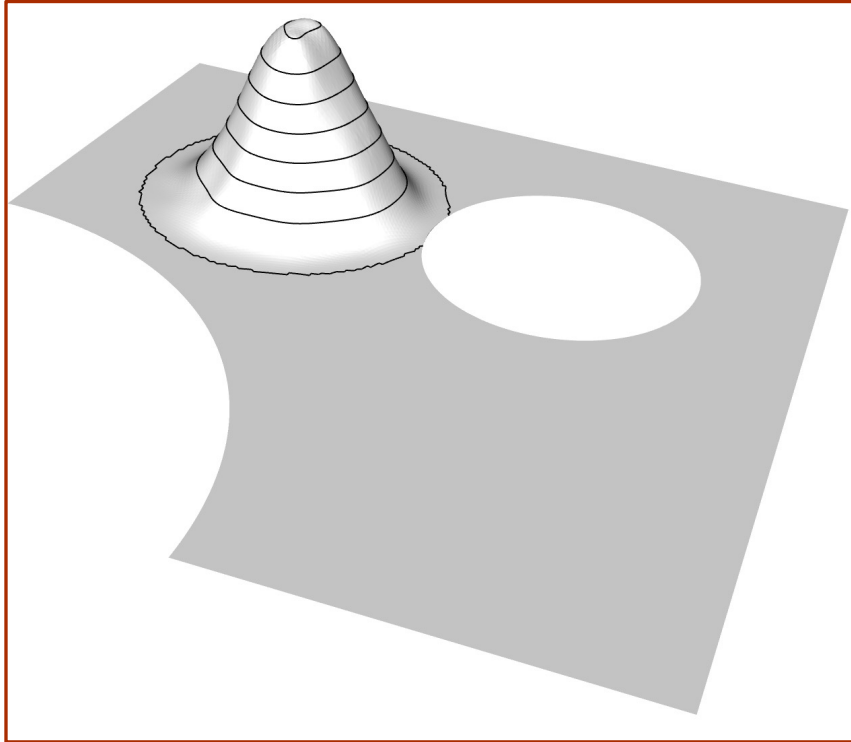
Bernstein polynomial $b_{i,n}(t)$



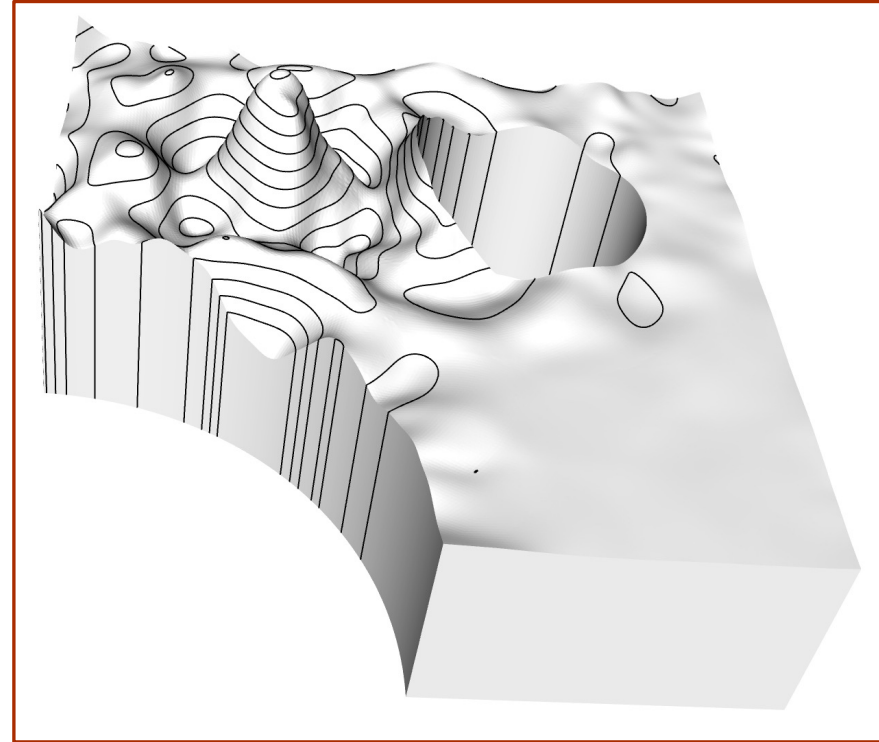
Conjugate basis example: element free



basis vector Φ_K



dual basis vector Φ^K



$$(\Phi_K, \Phi^J) = \delta_K^J \text{ bi-orthogonal}$$

Note: Φ_K has local support, but Φ^K has global support

Application to PDEs (solid mechanics)

Also applicable to formulations in $H(\text{div})$ and $H(\text{curl})$?

Governing equations (total-Lagrangian formulation)

strong form

$$\frac{\partial \mathbf{P}}{\partial \mathbf{X}} : \mathbf{I} = \rho_0 \ddot{\mathbf{u}}$$

$$\mathbf{u} = \bar{\mathbf{u}} \quad \text{on} \quad \Gamma_0^u \quad \text{and} \quad \mathbf{P} \cdot \mathbf{N} = \mathbf{t}_0 \quad \text{on} \quad \Gamma_0^t$$

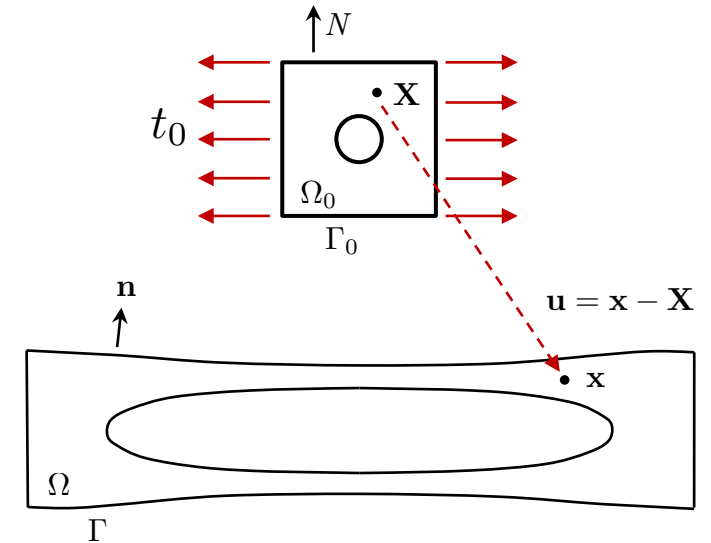
\mathbf{P} is first Piola-Kirchhoff stress tensor

weak form

find the trial functions $\mathbf{u} \in \mathbf{H}^1(\Omega_0)$ such that

$$\int_{\Gamma_0^t} \mathbf{t}_0 \cdot \mathbf{v} \, dS - \int_{\Omega_0} \mathbf{P} : (\partial \mathbf{v} / \partial \mathbf{X}) \, d\mathbf{X} = \int_{\Omega_0} \rho_0 \ddot{\mathbf{u}} \cdot \mathbf{v} \, d\mathbf{X}$$

for all test functions $\mathbf{v} \in \mathbf{H}_0^1(\Omega_0)$



Governing equations for linear elasticity

strong form $\frac{\partial \boldsymbol{\sigma}}{\partial \mathbf{x}} : \mathbf{I} + \mathbf{f} = \mathbf{0} \quad \mathbf{u} = \bar{\mathbf{u}} \text{ on } \Gamma_u \text{ and } \boldsymbol{\sigma} \mathbf{n} = \mathbf{t} \text{ on } \Gamma_t$

$\boldsymbol{\sigma} = \mathbb{C} \boldsymbol{\epsilon}$, where $\boldsymbol{\epsilon} := \text{sym}(\nabla \mathbf{u})$ *(linear elastic)*

$\exists \alpha_l, \alpha_u > 0$ such that $\alpha_l \boldsymbol{\epsilon} : \boldsymbol{\epsilon} \leq \boldsymbol{\epsilon} : (\mathbb{C}(\mathbf{x}) \boldsymbol{\epsilon}) \leq \alpha_u \boldsymbol{\epsilon} : \boldsymbol{\epsilon} \quad \forall \boldsymbol{\epsilon}$ *(uniform ellipticity)*

weak form find the trial functions $\mathbf{u} \in \mathbf{H}^1(\Omega_0)$ such that

$$\int_{\Omega} \boldsymbol{\sigma} : (\partial \mathbf{v} / \partial \mathbf{x}) d\Omega = \int_{\Omega} \mathbf{f} \cdot \mathbf{v} d\Omega + \int_{\Gamma_t} \mathbf{t} \cdot \mathbf{v} d\Gamma$$

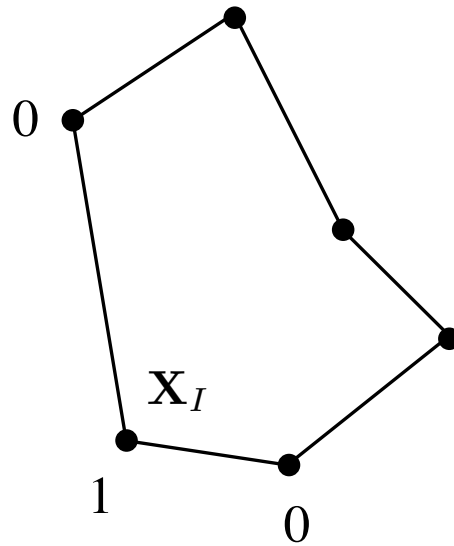
for all test functions $\mathbf{v} \in \mathbf{H}_0^1(\Omega_0)$

Show bilinear form?

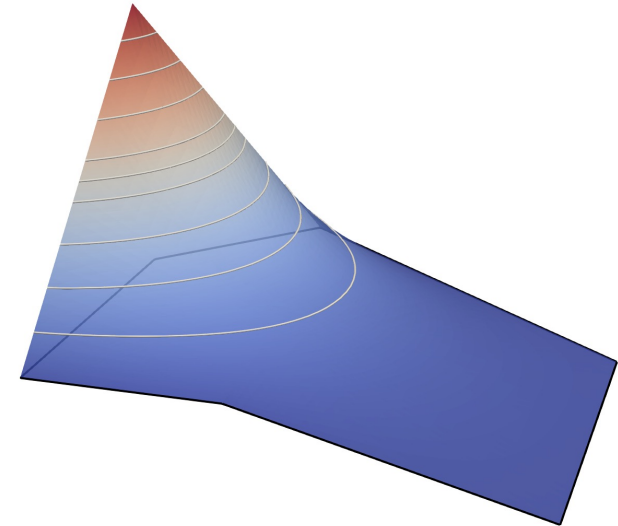
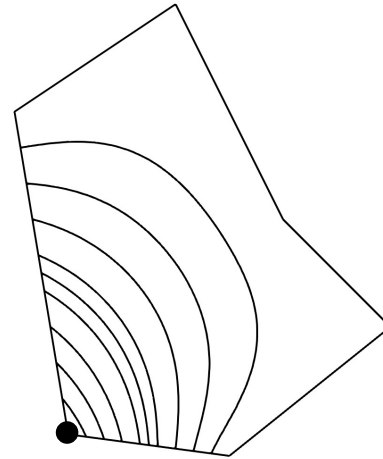
$$a(u, v) = \int_{\Omega_e} \nabla u : \mathbb{C} \nabla v d\Omega$$

Element-based discretizations (polyhedra)

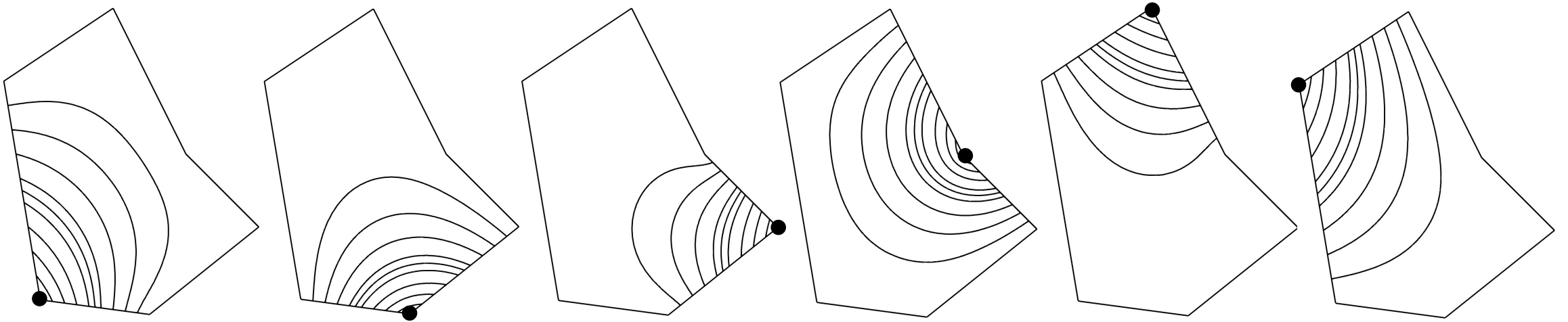
Harmonic shape functions



$$\nabla^2 \phi_I = 0$$



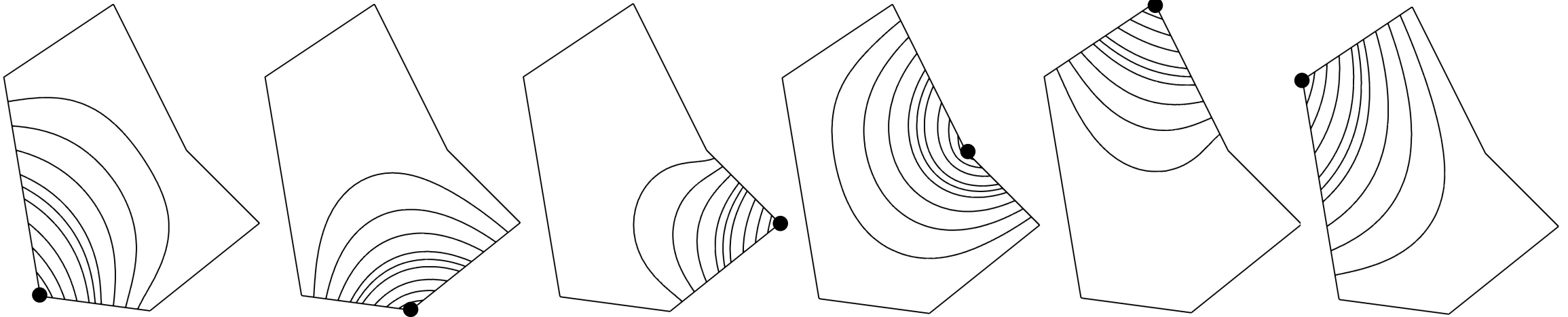
Harmonic shape functions



$$\sum_I \phi_I(\mathbf{x}) = 1 \quad \text{partition of unity}$$

$$\sum_I \mathbf{x}_I \phi_I(\mathbf{x}) = \mathbf{x} \quad \text{linear reproducibility}$$

Quadrature weights



$$\frac{w_1}{A} = 0.201$$

$$\frac{w_2}{A} = 0.147$$

$$\frac{w_3}{A} = 0.110$$

$$\frac{w_4}{A} = 0.196$$

$$\frac{w_5}{A} = 0.138$$

$$\frac{w_6}{A} = 0.209$$

A = area

quadrature weights

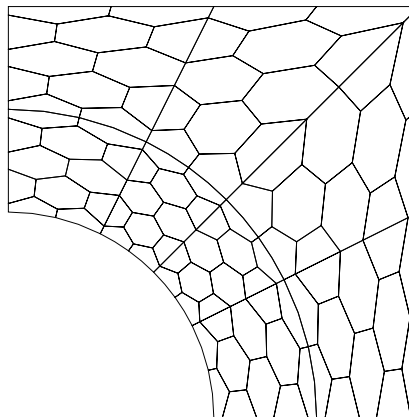
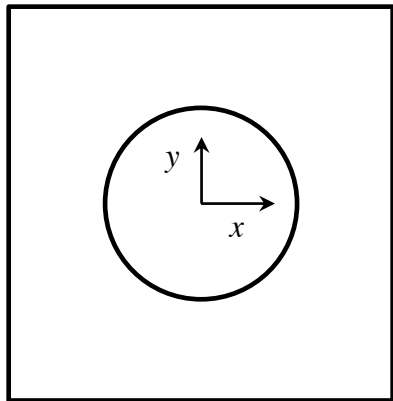
$$\sum_K w_K = A$$

$$w_K = \int_{\Omega_e} \phi_K(\mathbf{x}) d\Omega$$

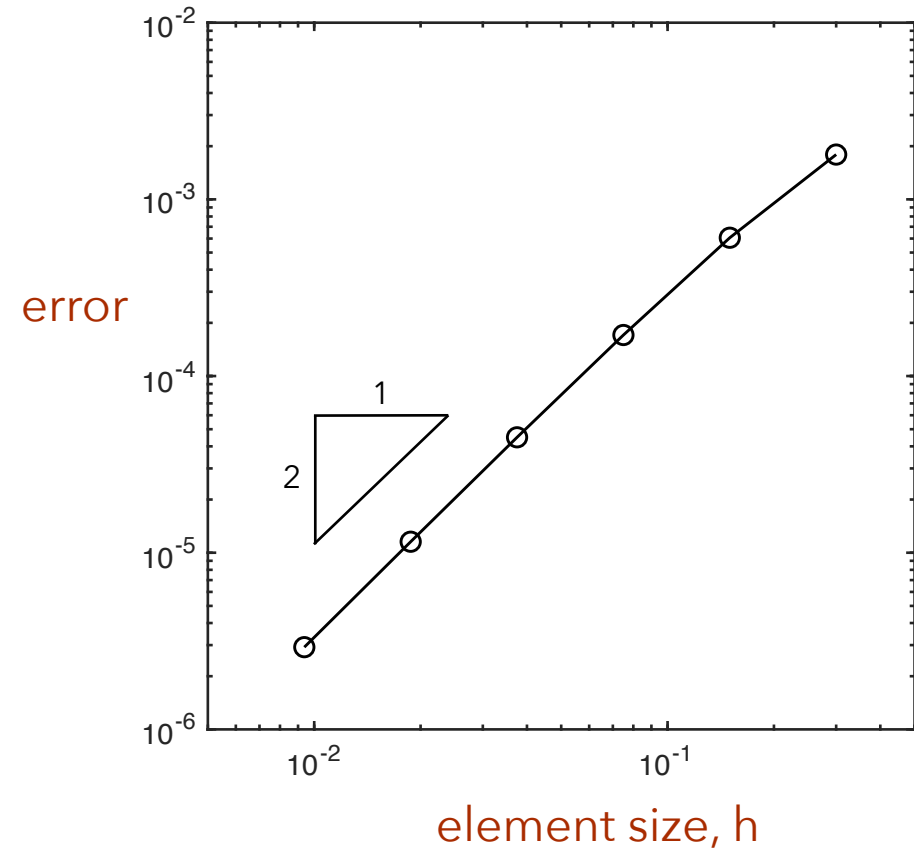
Quadrature

$$\text{error} = \left| \int f - \sum_i w_i f_i \right|$$

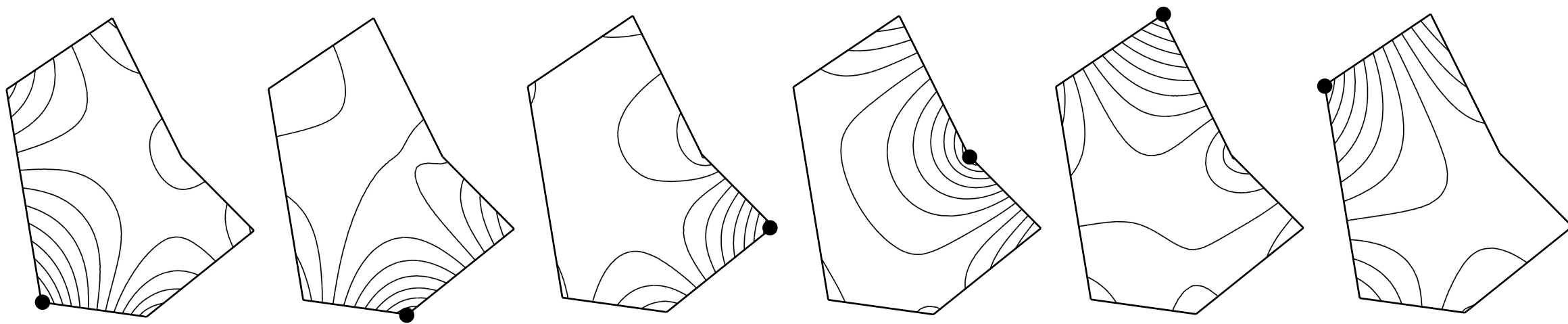
$$f(x, y) = \left[1 - \left(\frac{2x}{L_x} \right)^2 \right] \left[1 - \left(\frac{2y}{L_y} \right)^2 \right]$$



quadrature error



Conjugate functions



$$(\Phi_I, \Phi^J) = \delta_I^J \text{ bi-orthogonal}$$

Consistency of discrete form (integration)

- For convergence of discrete approximation, need to ensure consistency of discrete and continuous bilinear forms.
- Requires polynomial consistency of shape-function gradients (including quadrature).
- To obtain quadrature consistency, project the DoF shape function gradients to the subspace of quadrature shape functions.
- Only performed once in a pre-processing step.

$\{\phi_I, I = 1, \dots, N\}$ *DoF basis (shape functions)*

$\{\Phi_K, K = 1, \dots, M\}$ *Quadrature basis (shape functions)*

$$\bar{\nabla} \phi_I := \arg \min \int_{\Omega} \left(\nabla \phi_I - \sum_{K=1}^M a^K \Phi_K \right)^2 d\Omega \quad (L_2 \text{ projection})$$

The projection can be written in terms of the dual or conjugate basis $\{\Phi^J\}$

$$(\Phi_K, \Phi^J) = \delta_K^J \quad \text{bi-orthogonal}$$

$$\bar{\nabla} \phi_I = \sum_K \underbrace{(\nabla \phi_I, \Phi_K)}_{\text{covariant components}} \Phi^K = \sum_K \underbrace{(\nabla \phi_I, \Phi^K)}_{\text{contravariant components}} \Phi_K$$

Can prove polynomial consistency up to the order of the precision of $\{\Phi_K\}$

$$\text{Theorem: } \int_{\Omega} \mathbf{p} \bar{\nabla} \phi_I d\Omega = \int_{\Omega} \mathbf{p} \nabla \phi_I d\Omega \quad \text{for all } \mathbf{p} \in \mathbb{P}_k(\Omega)$$

This ensures satisfaction of the patch test.

Replace the original bilinear form $a(u, v) = \int_{\Omega} \nabla u : \mathbb{C} \nabla v \, d\Omega$

with this modified bilinear form $\bar{a}(u, v) = \int_{\Omega} \bar{\nabla} u : \mathbb{C} \bar{\nabla} v \, d\Omega$ *Note: This modified bilinear form is still symmetric (Bubnov-Galerkin).*

$$\bar{a}(u, v) = \int_{\Omega} \left[\sum_I (\nabla u, \Phi_I) \Phi^I \right] \mathbb{C} \left[\sum_J (\nabla v, \Phi_J) \Phi^J \right] d\Omega$$

$$\bar{a}(u, v) = \sum_{I, J} (\nabla u, \Phi_I) \mathbb{C} (\nabla v, \Phi_J) \underbrace{\int_{\Omega_e} \Phi^I \Phi^J \, d\Omega}_{G^{IJ}}$$

Can show that $G^{IJ} = (G_{IJ})^{-1}$

where $G_{IJ} = \int_{\Omega_e} \Phi_I \Phi_J d\Omega$ is the Gram matrix for the basis $\{\Phi_K\}$

Can show that $\Phi^I = G^{IJ} \Phi_J$ and $\Phi_I = G_{IJ} \Phi^J$

$$\bar{a}(u, v) = \sum_{I, J} G^{IJ} (\nabla u, \Phi_I) \mathbb{C} (\nabla v, \Phi_J) = \sum_K (\nabla u, \Phi^K) \underbrace{\mathbb{C} (\nabla v, \Phi_K)}_{\text{Looks like a sum over quadrature points.}}$$



Replace G_{IJ} with row-sum lumped version: $G_{IJ}^L := \sum_J G_{IJ} = \text{diag}\{w_K\}$

where recall $w_K = \int_{\Omega} \phi_K(\mathbf{x}) d\Omega$

Then $\bar{a}(u, v) \rightarrow \bar{a}^L(u, v) = \sum_K \frac{1}{w_K} (\nabla u, \Phi_K) \mathbb{C} (\nabla v, \Phi_K)$ where $(G_{IJ}^L)^{-1} = \text{diag}\left\{\frac{1}{w_K}\right\}$

Can write $\bar{a}^L(u, v)$ as

$$\bar{a}^L(u, v) = \sum_K w_K (\bar{\nabla} u)_K : \mathbb{C} (\bar{\nabla} v)_K$$

where

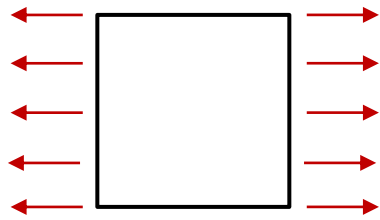
$$(\bar{\nabla} u)_K := \frac{1}{w_K} \int_{\Omega} (\nabla u) \Phi_K d\Omega$$

which has the form of a discrete derivative at a quadrature point K .

Our discrete bilinear form is now "sparse."

Verification: elasticity patch test

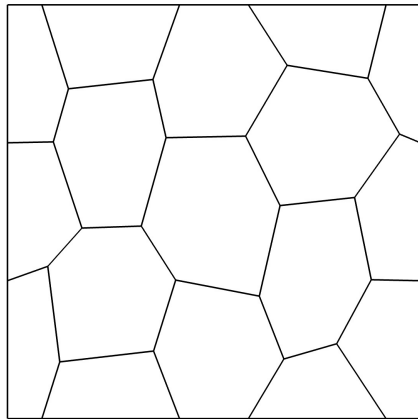
uniaxial tension



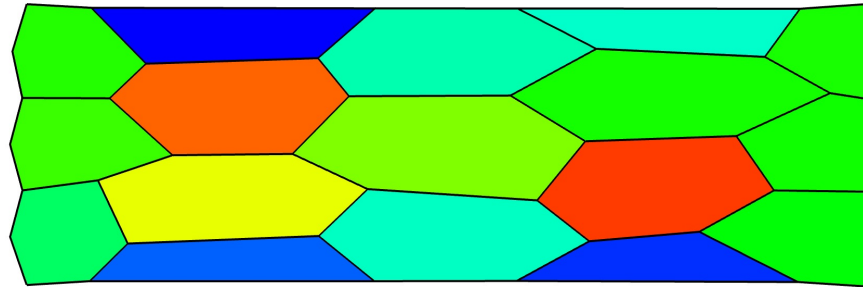
$$E = 1.0$$

$$\nu = 0.3$$

hexagon mesh

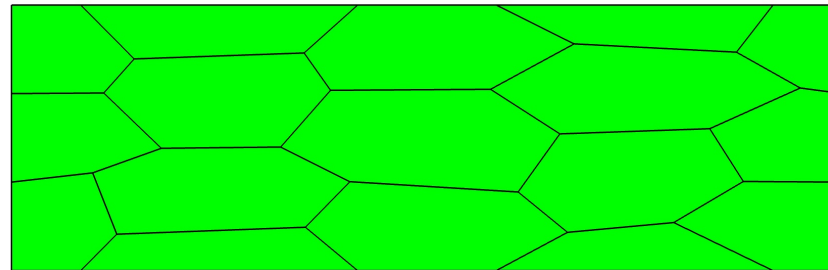


subtriangle quadrature



max stress error = 2%

projection based quadrature

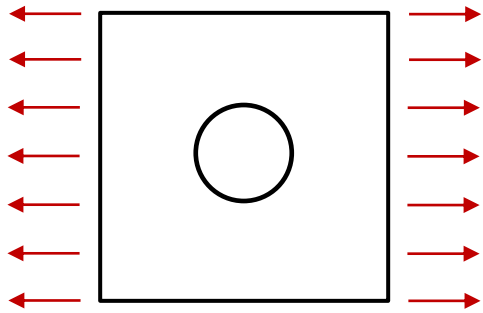


max stress error = 3×10^{-15}

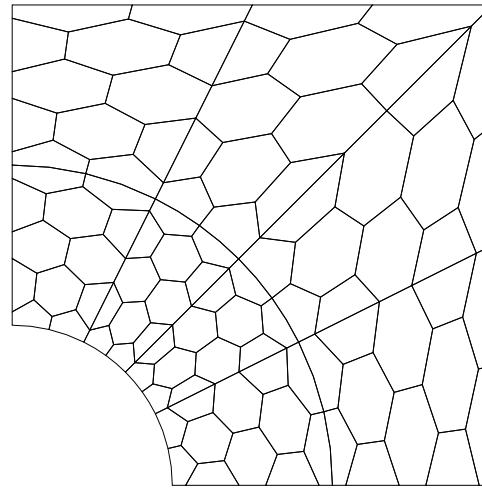
Verification: elasticity, hole-in-plate tension



uniaxial tension



mapped hexagon mesh

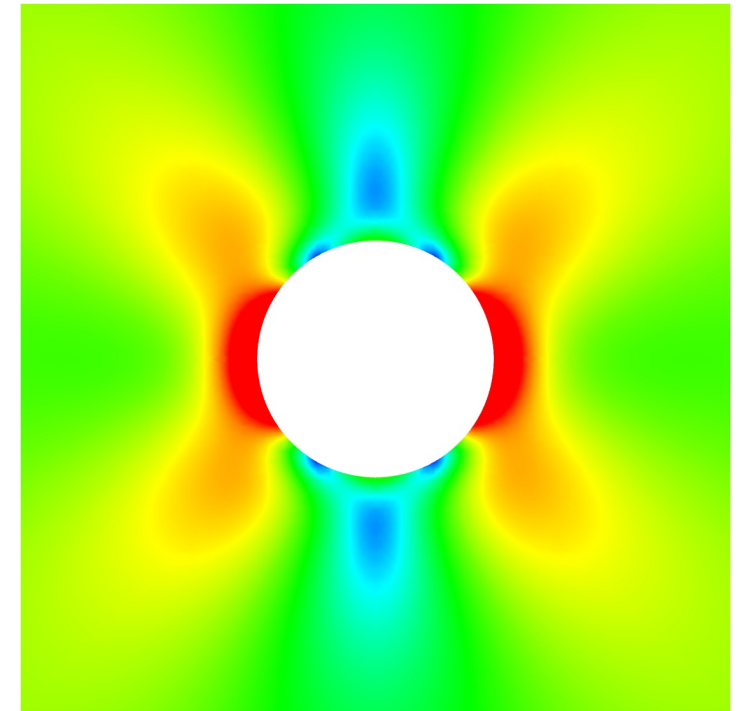


- exact tension prescribed corresponding to infinite plate
- plane strain
- quarter symmetry model used

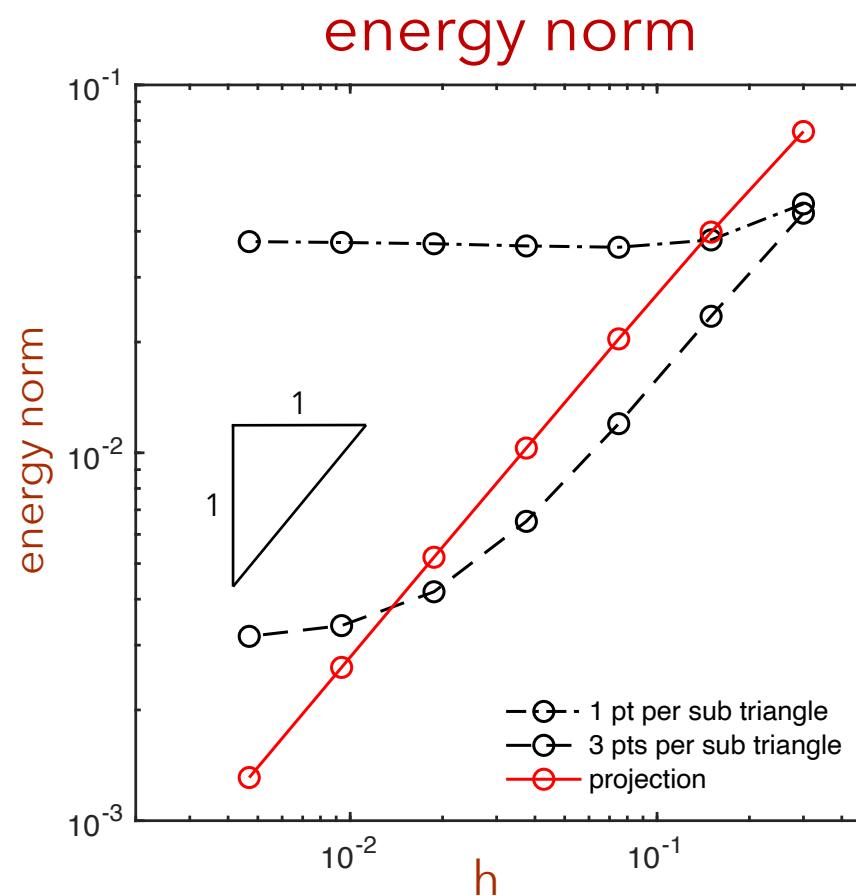
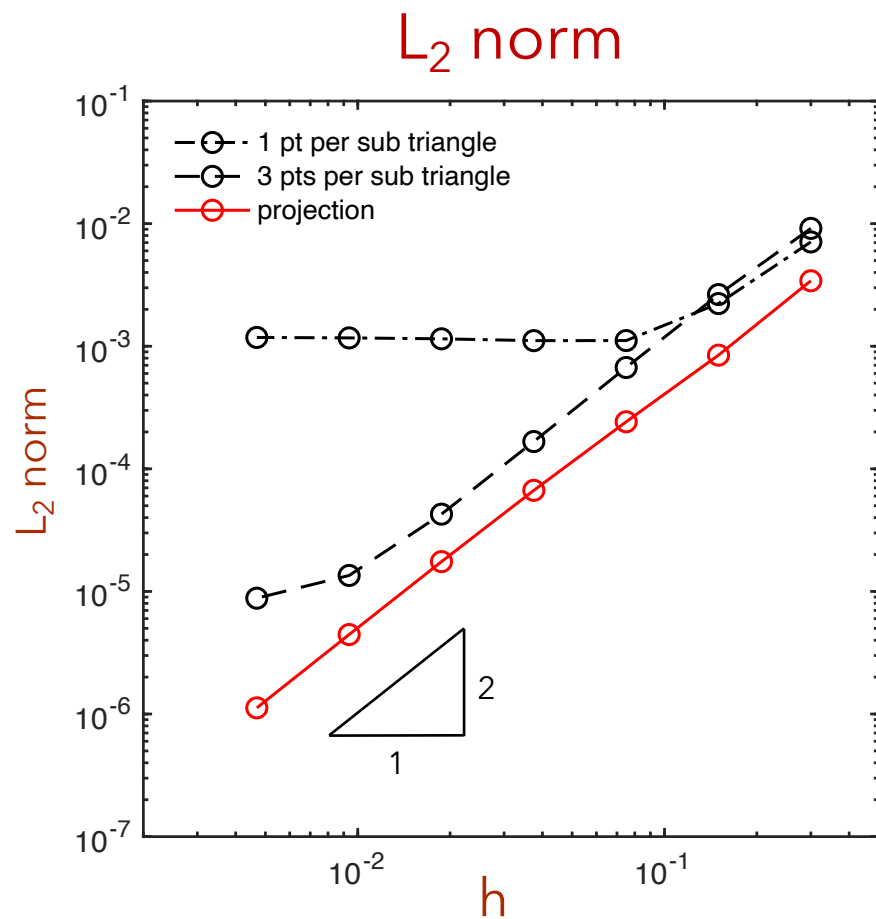
$$E = 1.0$$

$$\nu = 0.3$$

von Mises stress invariant



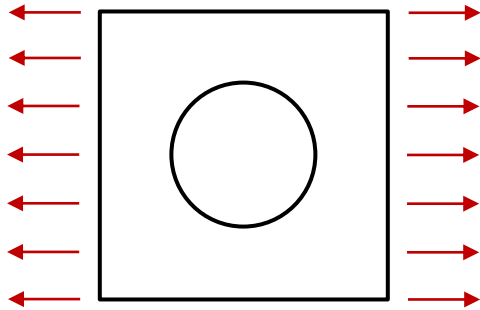
Verification: elasticity, hole-in-plate tension



Optimal rates of convergence

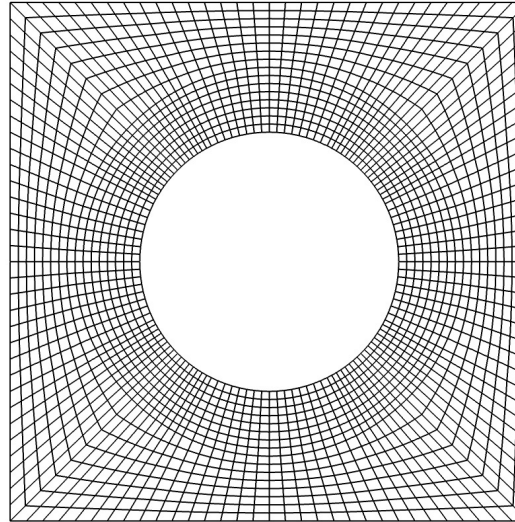
Application example: hyperelastic, hole-in-plate

uniaxial extension

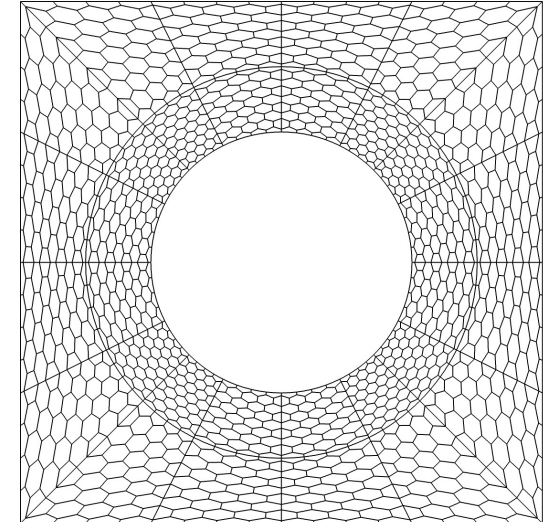


- plane strain
- quarter symmetry model used

quad mesh



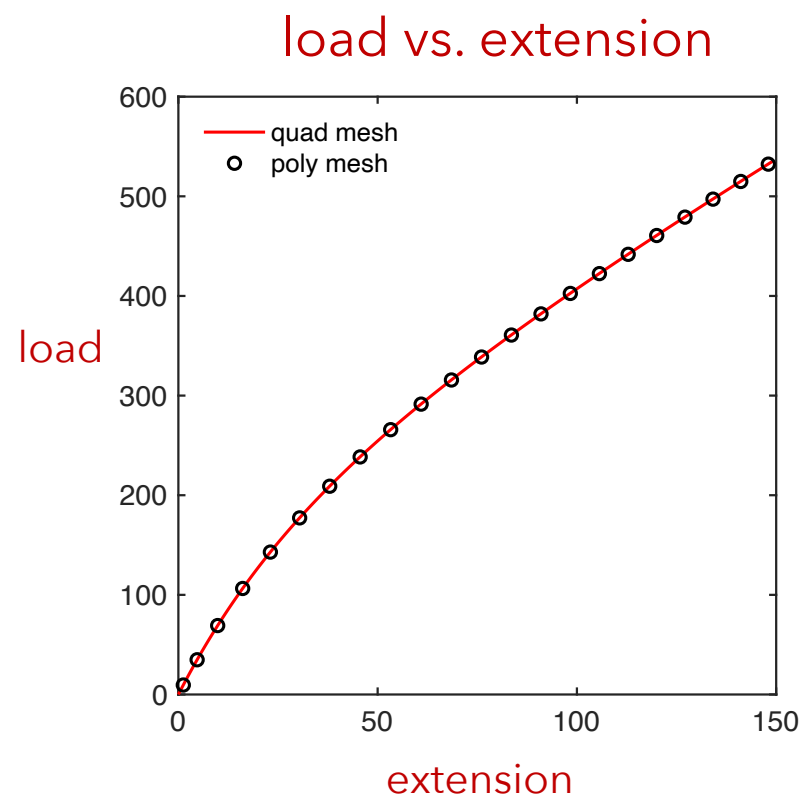
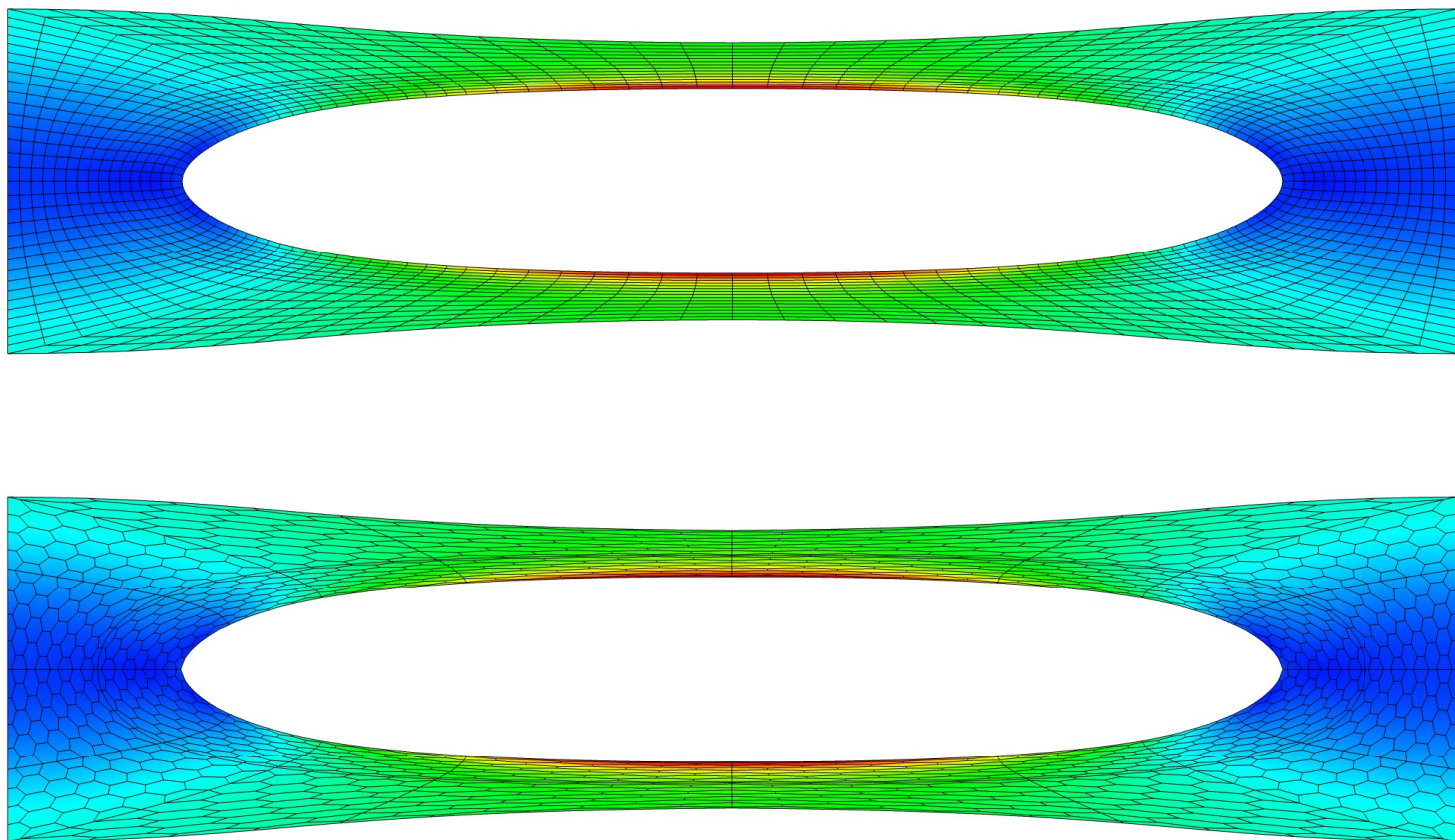
mapped hexagon mesh



compressible neo-Hookean material

$$\boldsymbol{\sigma} = \frac{\mu}{J}(\mathbf{F}\mathbf{F}^T - \mathbf{I}) + \frac{\lambda}{\ln J}\mathbf{I}$$

$$J = \det \mathbf{F} \quad \mathbf{F} = \frac{\partial \mathbf{x}}{\partial \mathbf{X}}$$



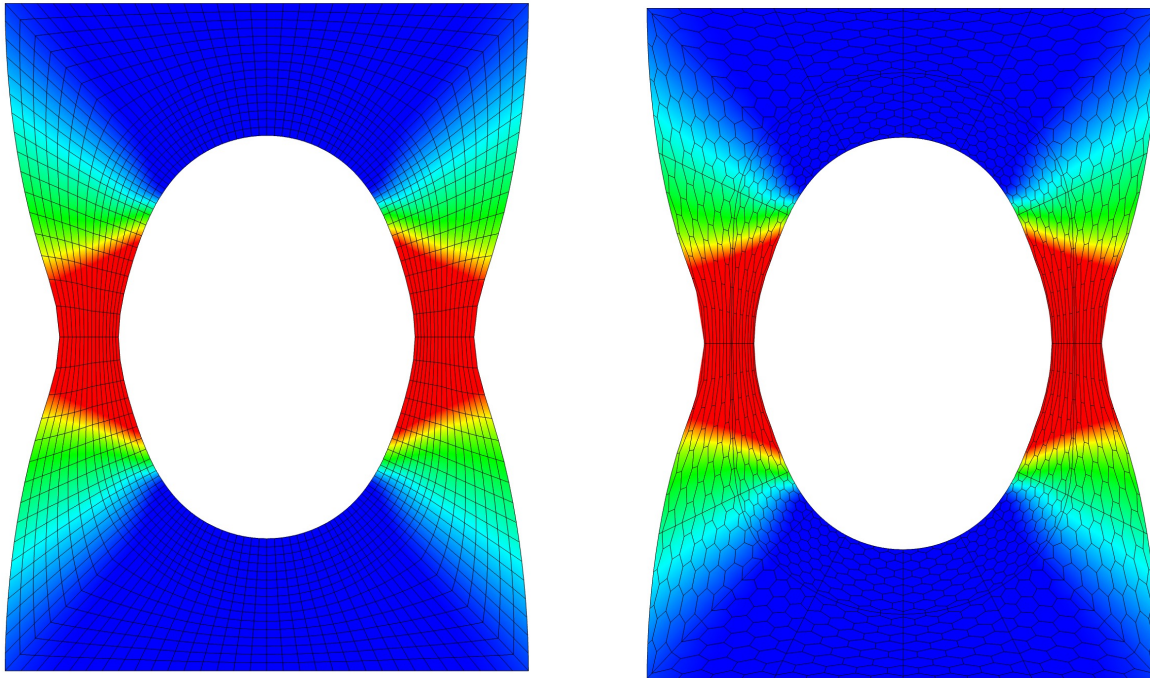
Application example: elastic-plastic, hole-in-plate



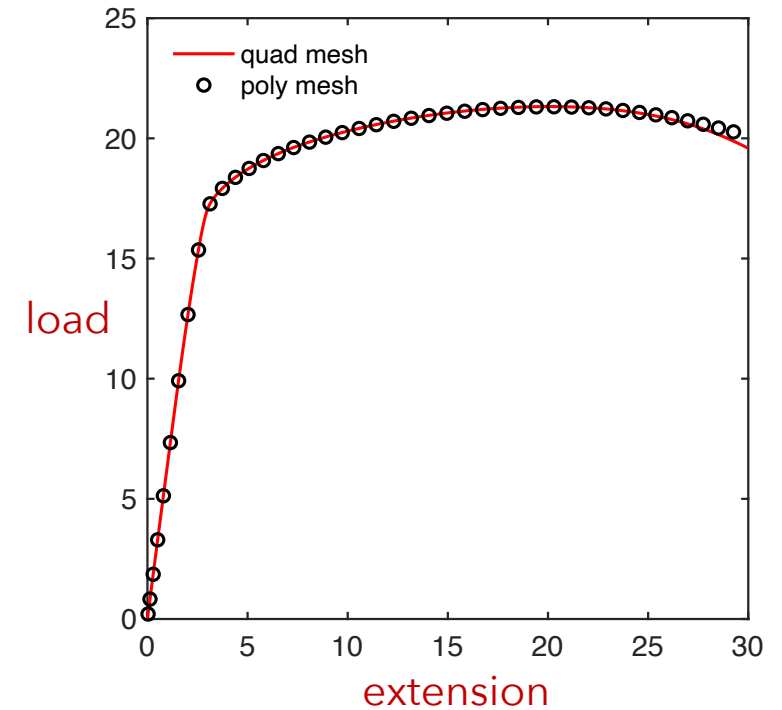
yield surface $f(\sigma, \bar{\epsilon}^p) = \phi(\sigma) - \sigma_y(\bar{\epsilon}^p) = 0$

$$\phi(\sigma) = \left\{ \frac{1}{2} (|\sigma_1 - \sigma_2|^2 + |\sigma_1 - \sigma_3|^2 + |\sigma_2 - \sigma_3|^2) \right\}^{1/2}$$

plastic strain field



load vs. extension



(Use F-bar methods for inf-sup stability.)

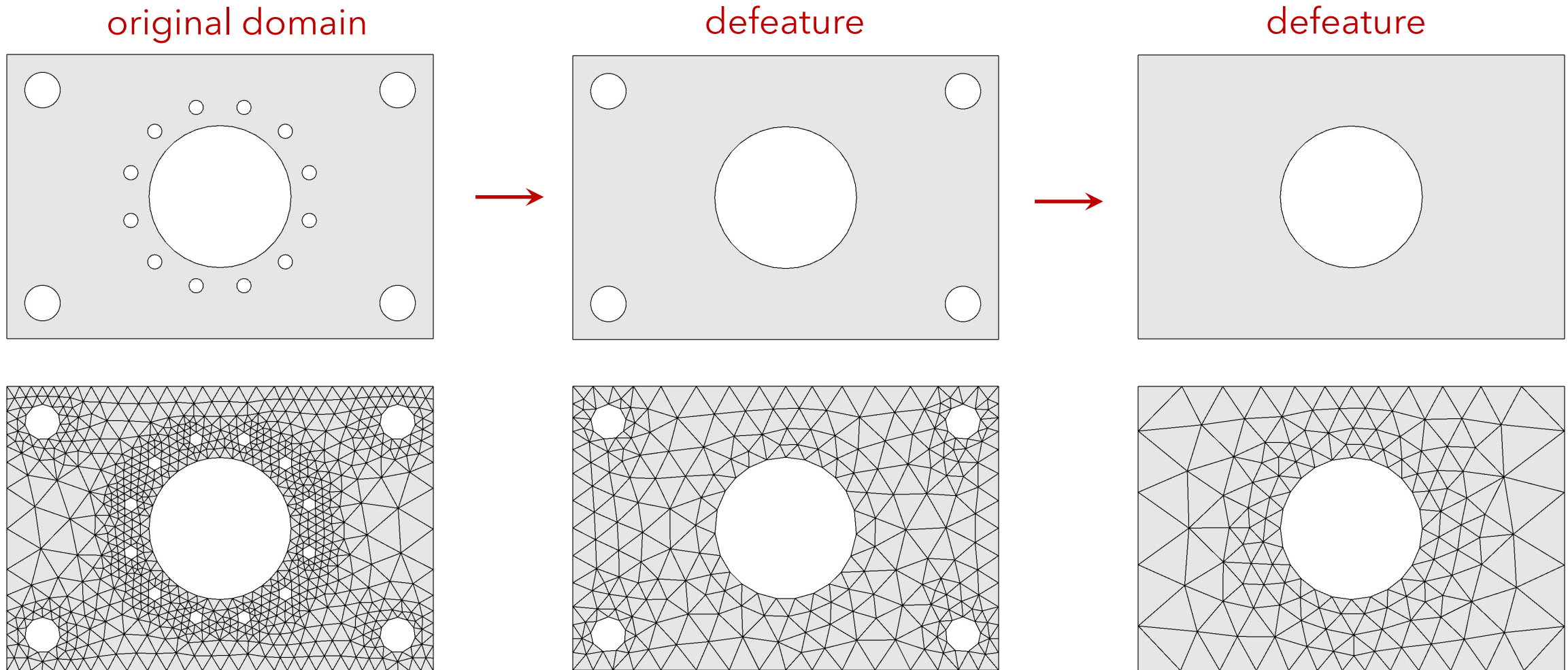
Calculation of $(\nabla \phi_I, \phi_K)$



- Currently solving for derivative projection using a sub-triangulation and FEA.
- Can also use Green's identities to calculate these if shape functions are harmonic.

Element-free discretizations

Motivation: Separate domain discretization from solution discretization



Impact of domain defeaturing? depends on goals of simulation

Motivation: Separate domain discretization from solution discretization



- Domain defeaturing is needed to control FEA discretization quality, size, and critical time step (explicit dynamics)
- Domain defeaturing typically requires human intervention (heuristics).
- For FEA, domain discretization and solution discretization are synonymous (isoparametric).
- Geometric features can require a fine local discretization while solution does not.
- Heuristics are often used in domain defeaturing and mesh design.
- Meshes are typically designed with goal in mind, thus making it cumbersome to reuse.
- Adaptivity requires going back to domain model (geometry).

A hybrid element-free approach



finite-element approach

- defeature domain geometry based on goals
- create a mesh based on goals
- mesh discretizes domain and solution
- quadrature of weak form is easy
- visualization of results using mesh
- adaptivity of mesh is hard

mesh-free approach

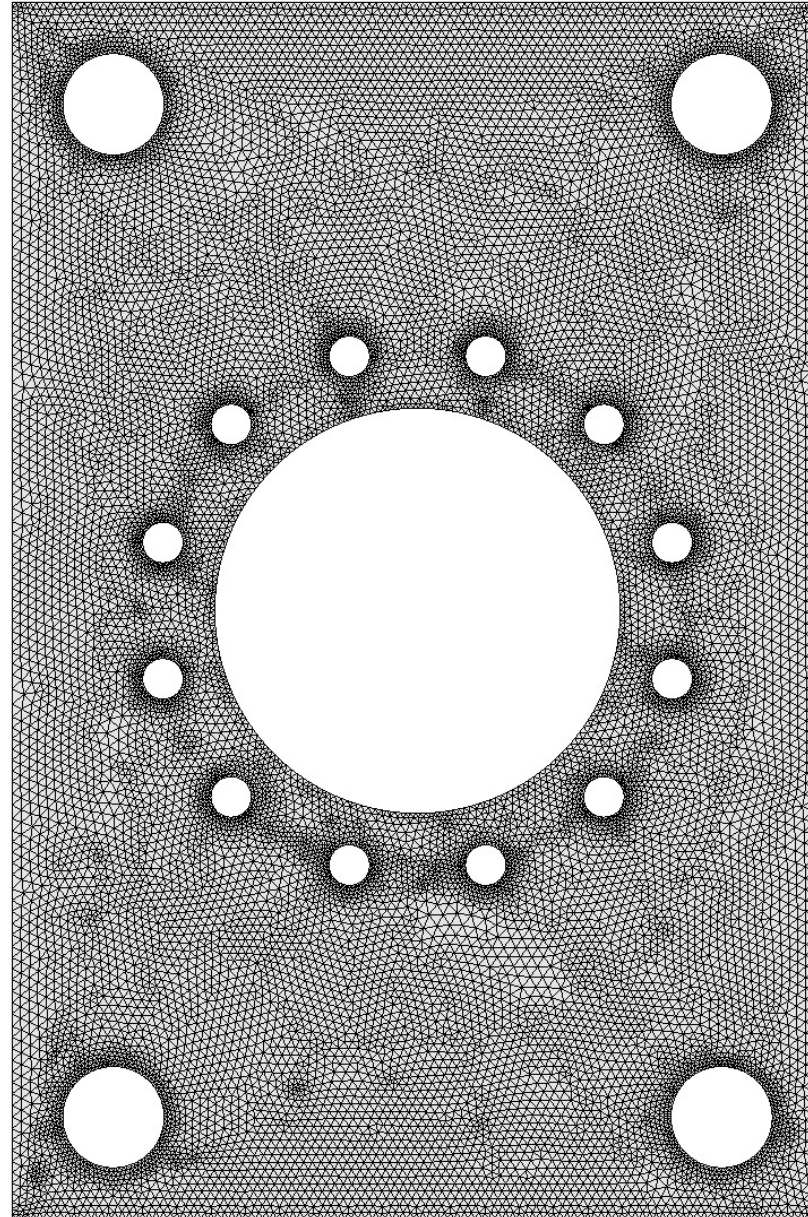
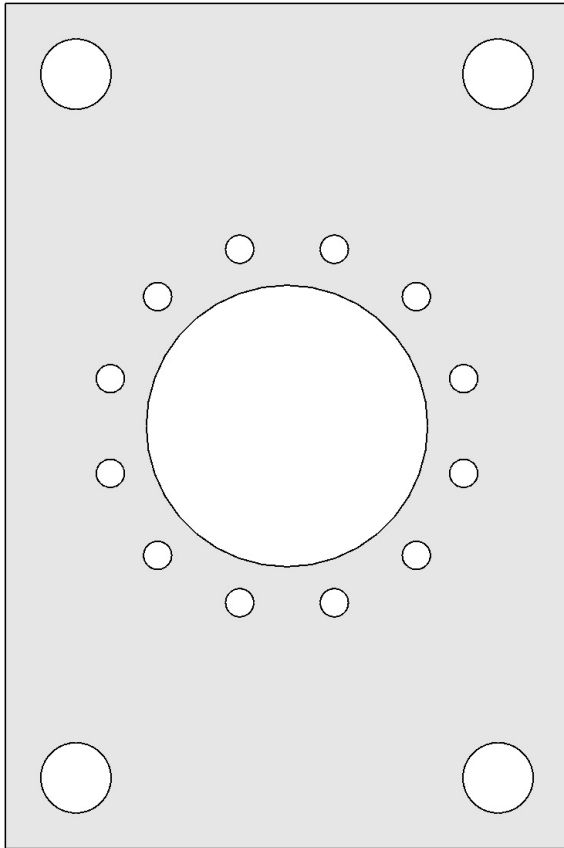
- no defeaturing of domain geometry
- no discretization of domain
- connectivity of domain is undefined (need computational geometry)
- quadrature of weak form is very hard
- visualization of results is cumbersome

Alternative hybrid approach: separate domain discretization and solution approximation using an element-free formulation.

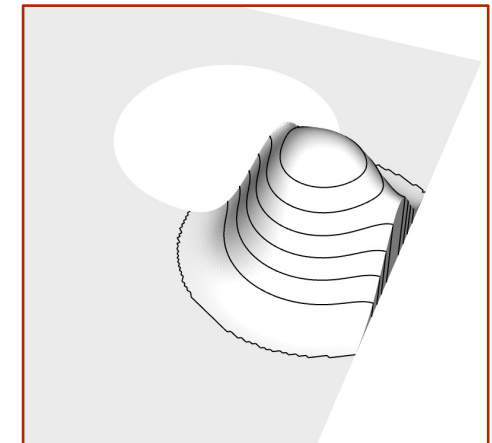
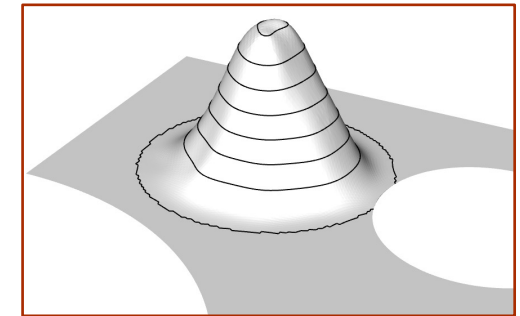
Hybrid approach: fine-scale triangulation



original domain

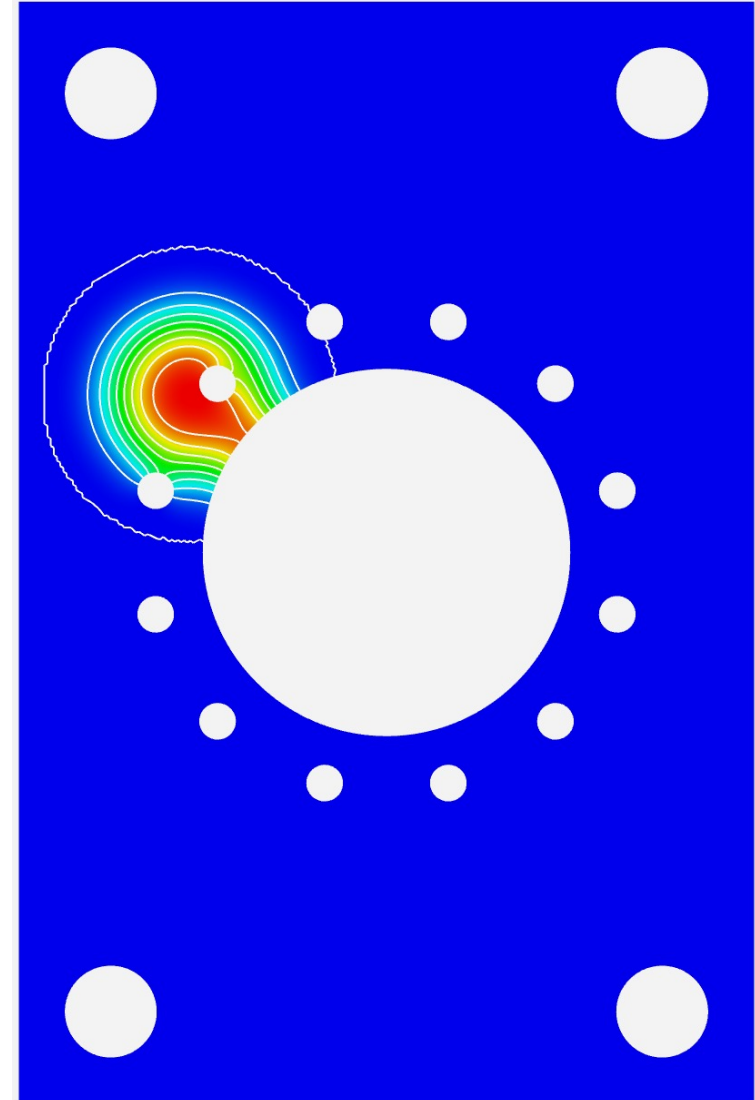


- Use a fine-scale triangulation to discretize domain.
- Define element-free basis using this triangulation.



Element-free basis functions

- Element-free basis functions automatically include geometric features at all scales.
- Solution discretization is separate from domain discretization.
- No need to defeature domain.



Hybrid element-free approach

- no defeaturing of domain
- discretize domain using fine-scale triangulation (a mesh, but poor quality is okay)
- use hp-cloud to define solution discretization (GBC, RK)
- use second hp-cloud to define quadrature and ensure coercivity
- projection of solution gradient to obtain polynomial consistency
- visualization of results using fine-scale mesh

pros

- symmetric, Galerkin
- linear or nonlinear
- implicit or explicit dynamics
- can do higher order
- can do direct or mixed formulation
- adaptivity is seamless
- can use poor quality tet mesh
- adaptivity is facilitated
- should work for $H(\text{div})$ and $H(\text{curl})$ spaces
- reduced order modeling through coarse discretizations

cons

- constant material properties within a domain
- material interfaces: have to use weak enforcement such as mortar method
- less sparse

INTERNATIONAL JOURNAL FOR NUMERICAL METHODS IN ENGINEERING, VOL. 37, 229–256 (1994)

ELEMENT-FREE GALERKIN METHODS

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The Technological Institute, Northwestern University, Evanston IL 60208-3109, U.S.A.*

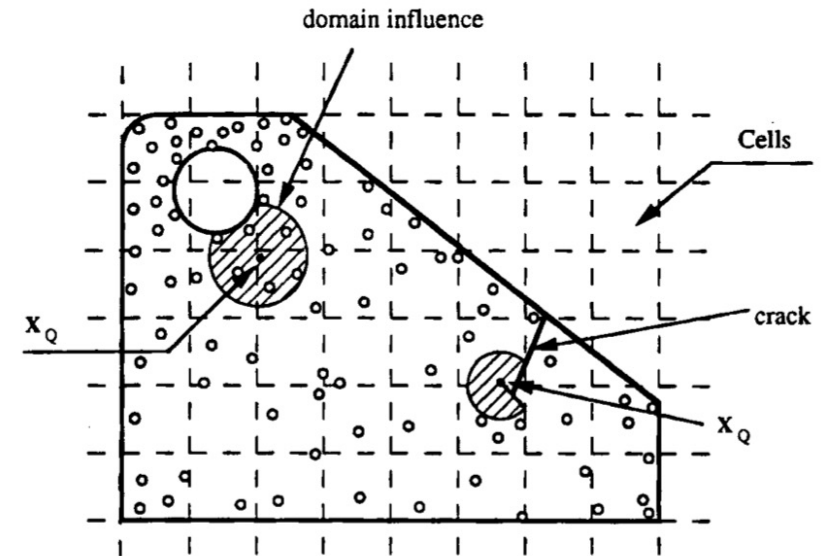


Figure 1. Cell structure for quadrature in EFGM and domains of quadrature point

Moving Least Squares (Reproducing Kernel)



The MLS shape functions $\phi_I(\mathbf{X})$ are defined as a spatial modulation of the nodal weight functions.

$$\phi_I(\mathbf{X}) = c_I(\mathbf{X})w_I(\mathbf{X})$$

where the modulation function $c_I(\mathbf{X})$ is found through a least square minimization process resulting in

$$c_I(\mathbf{X}) = \mathbf{g}^T(\mathbf{X})\mathbf{A}^{-1}(\mathbf{X})\mathbf{g}(\mathbf{X}_I)$$

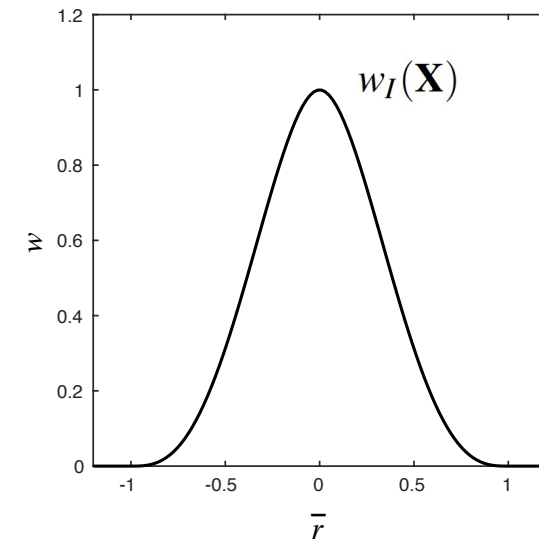
where

$$\mathbf{A}(\mathbf{X}) = \sum_{I \in \mathcal{N}} w_I(\mathbf{X})\mathbf{g}(\mathbf{X}_I)\mathbf{g}^T(\mathbf{X}_I) \quad (\text{sum over neighbors})$$

$$\mathbf{g}^T(\mathbf{X}) = \{ 1 \ X_1 \ X_2 \} \quad (\text{linear reproducibility})$$

Note: shape function construction is algebraic.

nodal weight function

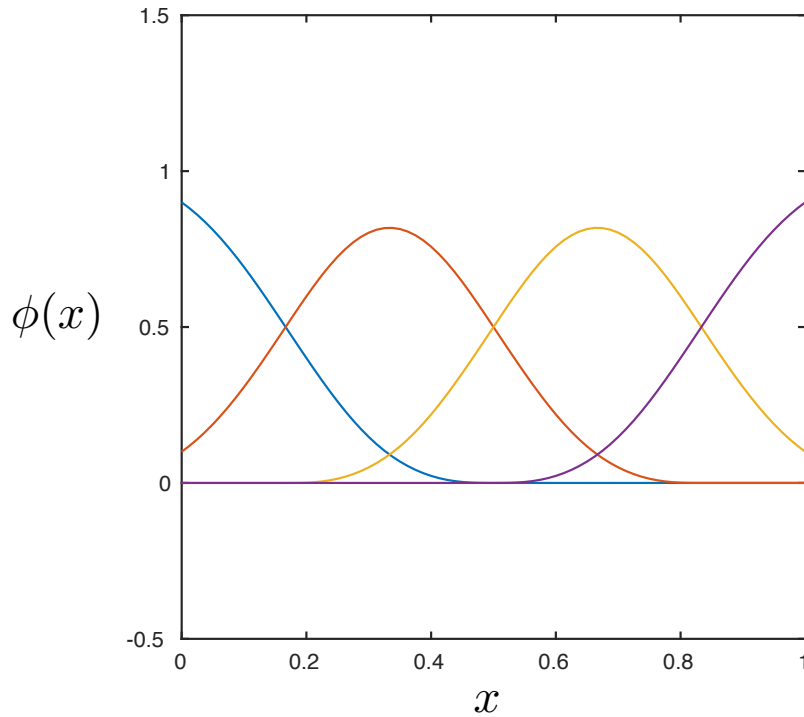


circular or rectangular support

Moving Least Squares

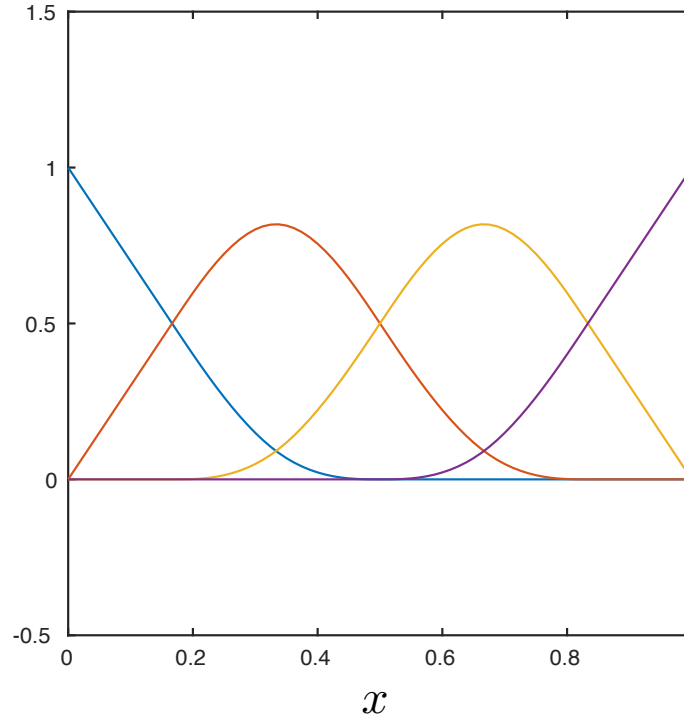


$$\sum_K \phi_K(x) = 1$$



$$\sum_K \phi_K(x) = 1$$

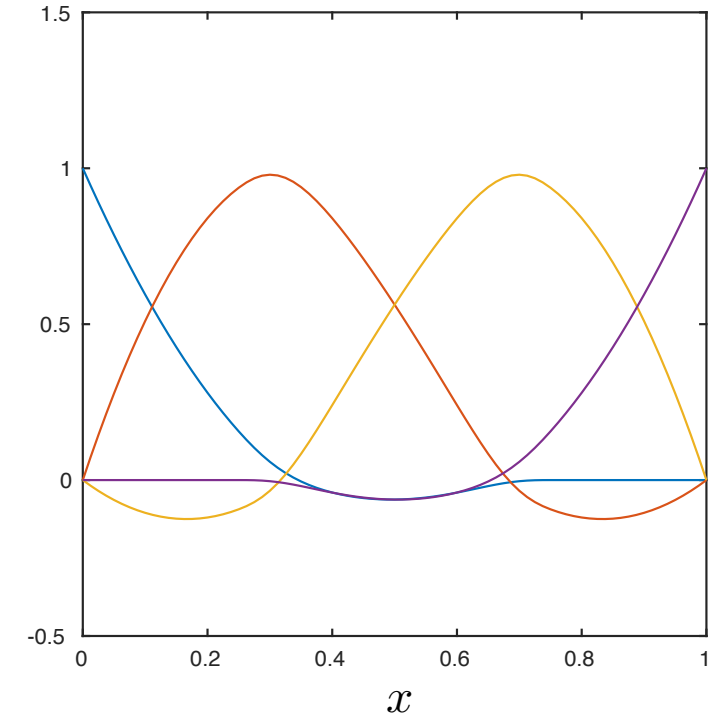
$$\sum_K x_K \phi_K(x) = x$$



$$\sum_K \phi_K(x) = 1$$

$$\sum_K x_K \phi_K(x) = x$$

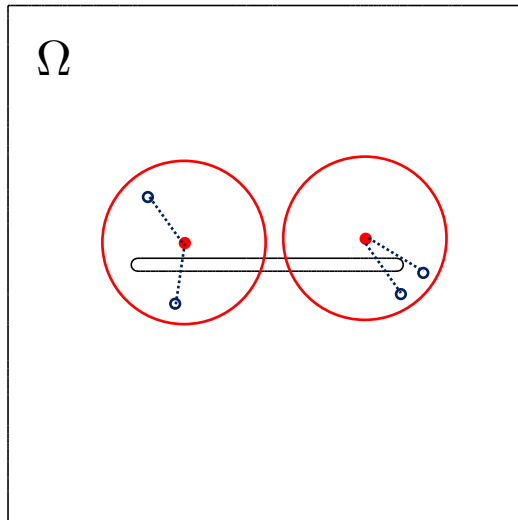
$$\sum_K x_K^2 \phi_K(x) = x^2$$



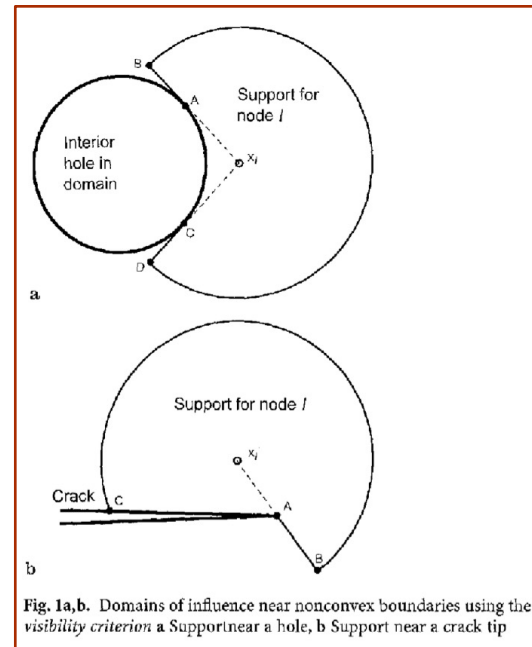
Continuous meshless approximations for nonconvex bodies by diffraction and transparency

D. Organ, M. Fleming, T. Terry, T. Belytschko

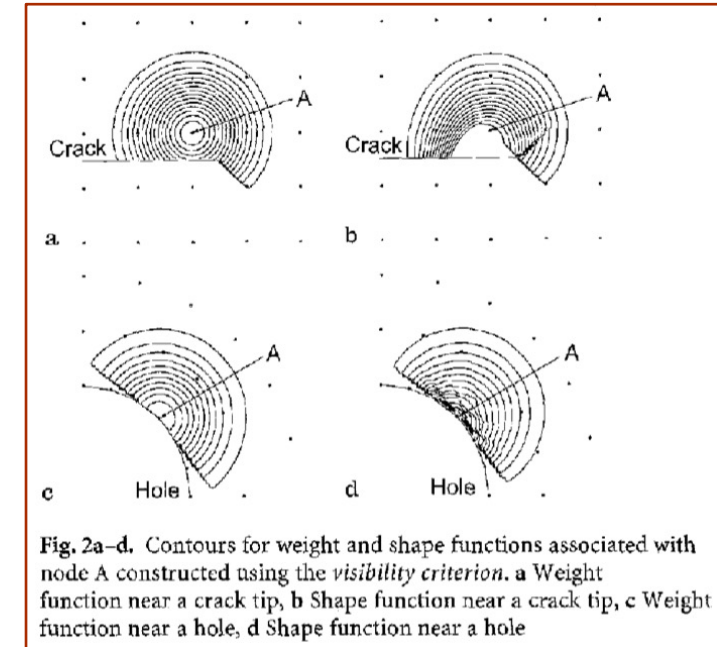
domain
with slot



visibility criterion



visibility criterion





Continuous meshless approximations for nonconvex bodies by diffraction and transparency

D. Organ, M. Fleming, T. Terry, T. Belytschko

diffraction method

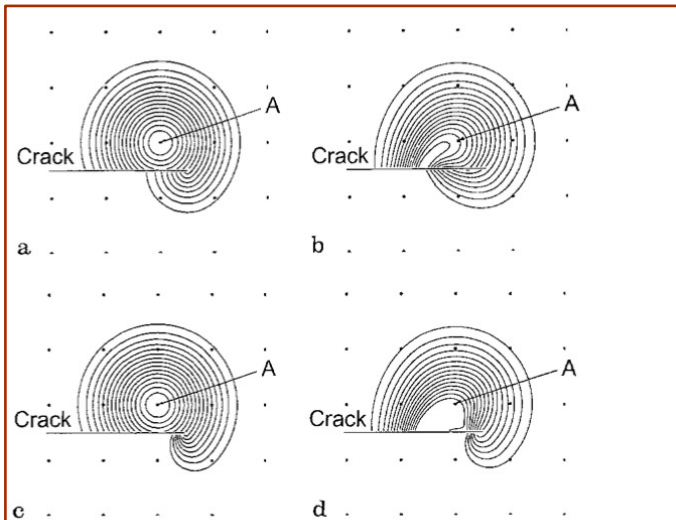


Fig. 5a–d. Contours for weight and shape functions associated with node A near a crack tip constructed using the *diffraction method*. The quartic weight function in (2.18b) was used with $d_{max} = 2.01$ a Weight function for $\lambda = 1$, b Shape function for $\lambda = 1$, c Weight function for $\lambda = 2$, d Shape function for $\lambda = 2$

transparency method

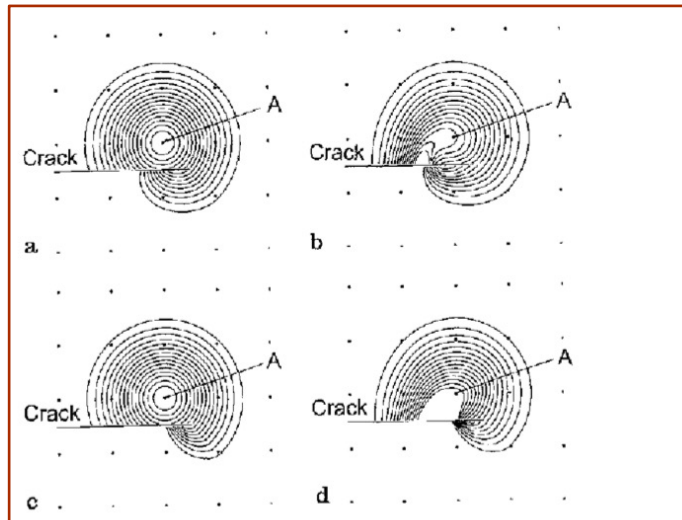


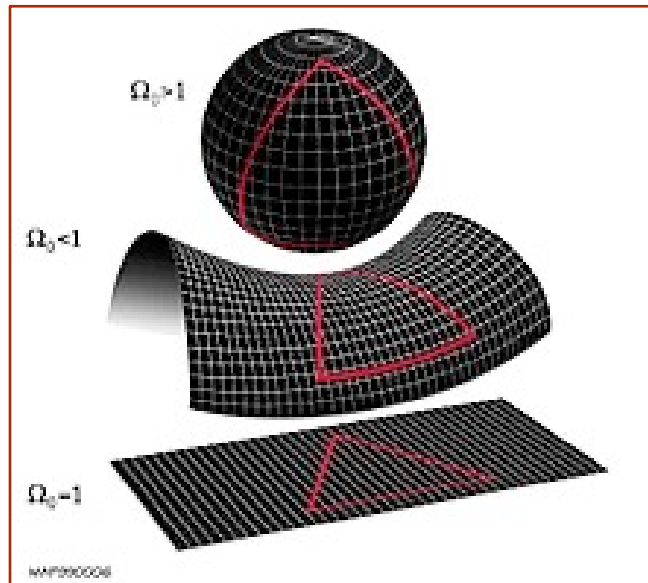
Fig. 8a–d. Contours for weight and shape functions associated with node A near a crack tip constructed using the *transparency method*. The quartic weight function in (2.18b) was used with $d_{max} = 2.01$. a Weight function for $\kappa = 1.0$, b Shape function for $\kappa = 1.0$, c Weight function for $\kappa = 0.5$, d Shape function for $\kappa = 0.5$

All these methods (visibility, transparency, diffraction) require use of computational geometry.

Manifold geodesic

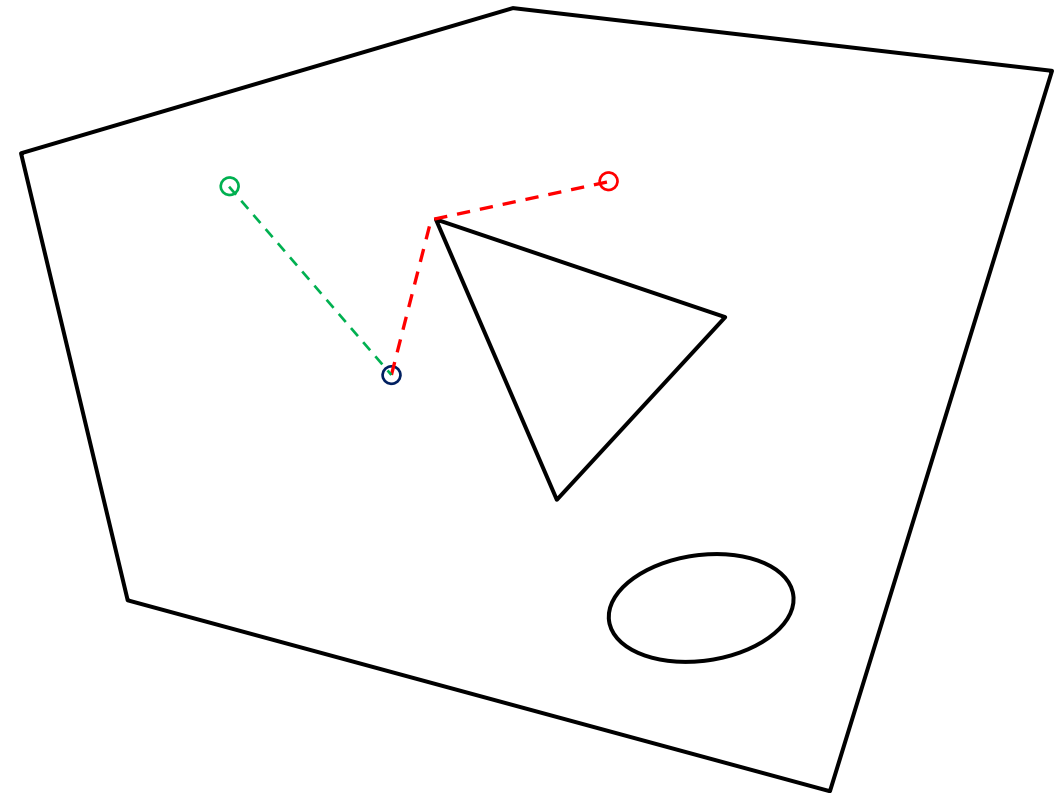


Geodesic: path that provides the shortest distance along a manifold



<https://en.wikipedia.org/wiki/Geodesic>

Euclidean manifold with boundary



Geodesics in Heat: A New Approach to Computing Distance Based on Heat Flow

KEENAN CRANE

Caltech

and

CLARISSE WEISCHEDEL and MAX WARDETZKY,

University of Göttingen

ACM Trans. Graph. 2013 Vol. 32 Issue 5 Pages Article 152

ALGORITHM 1: The Heat Method

- I. Integrate the heat flow $\dot{u} = \Delta u$ for some fixed time t .
 - II. Evaluate the vector field $X = -\nabla u / |\nabla u|$.
 - III. Solve the Poisson equation $\Delta \phi = \nabla \cdot X$.
-

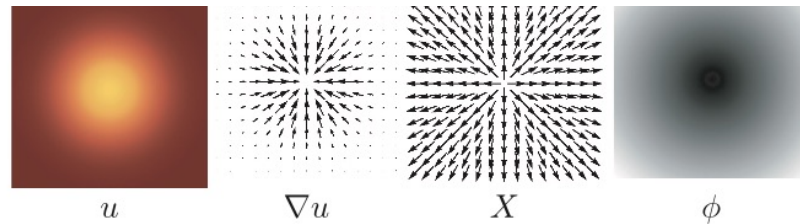


Fig. 5. Outline of the heat method. (I) Heat u is allowed to diffuse for a brief period of time (*left*). (II) The temperature gradient ∇u (*center left*) is normalized and negated to get a unit vector field X (*center right*) pointing along geodesics. (III) A function ϕ whose gradient follows X recovers the final distance (*right*).

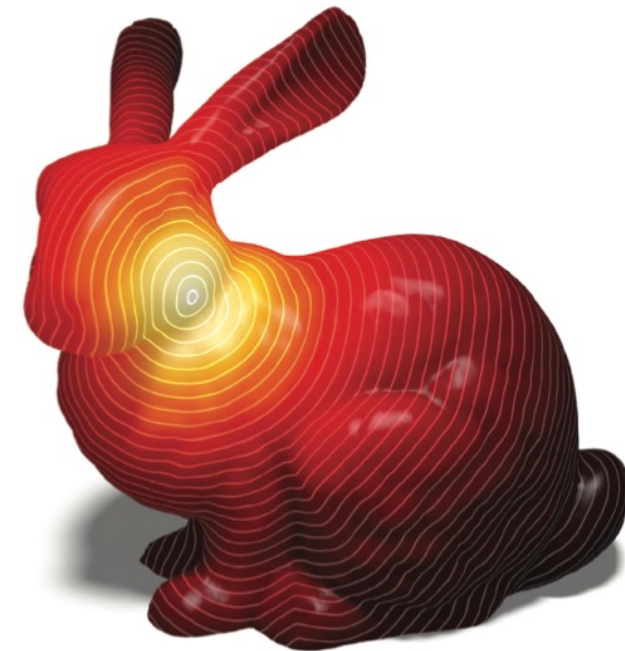
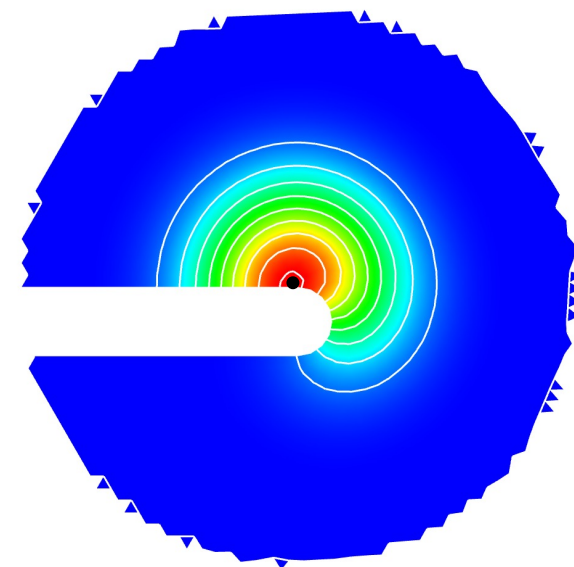
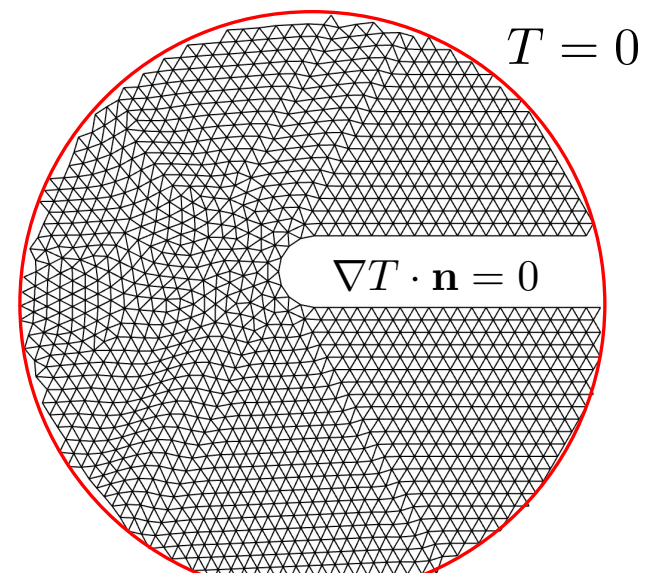
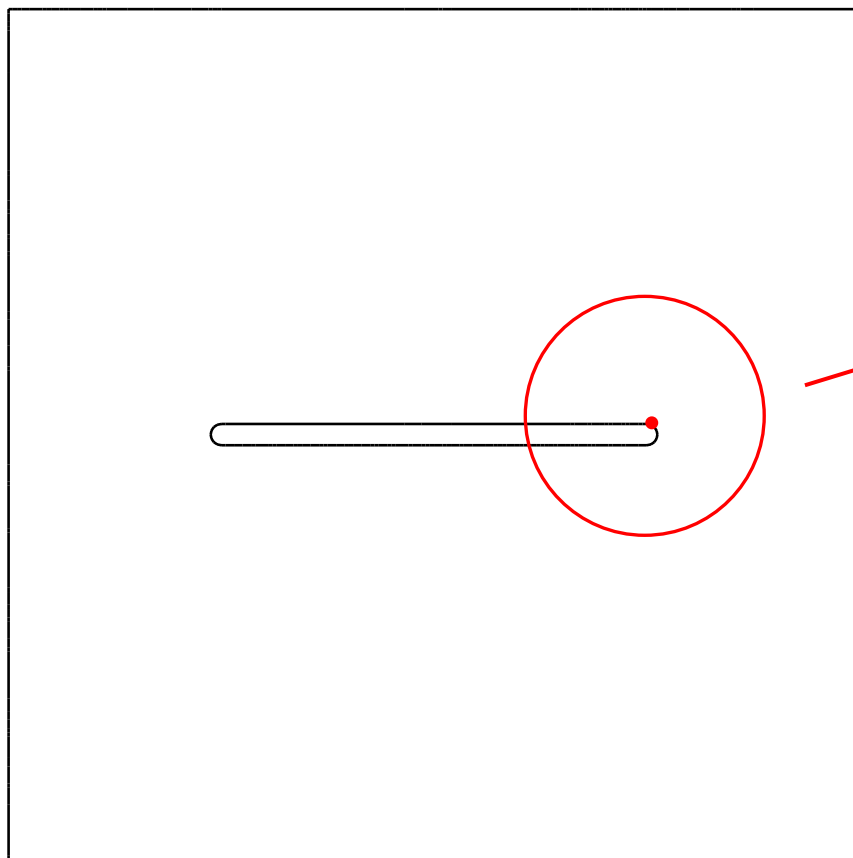
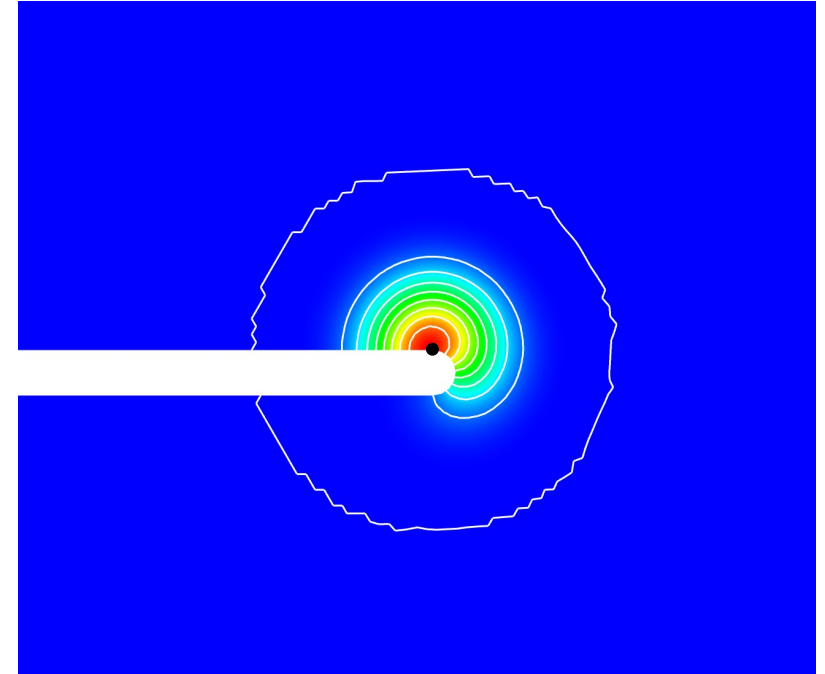
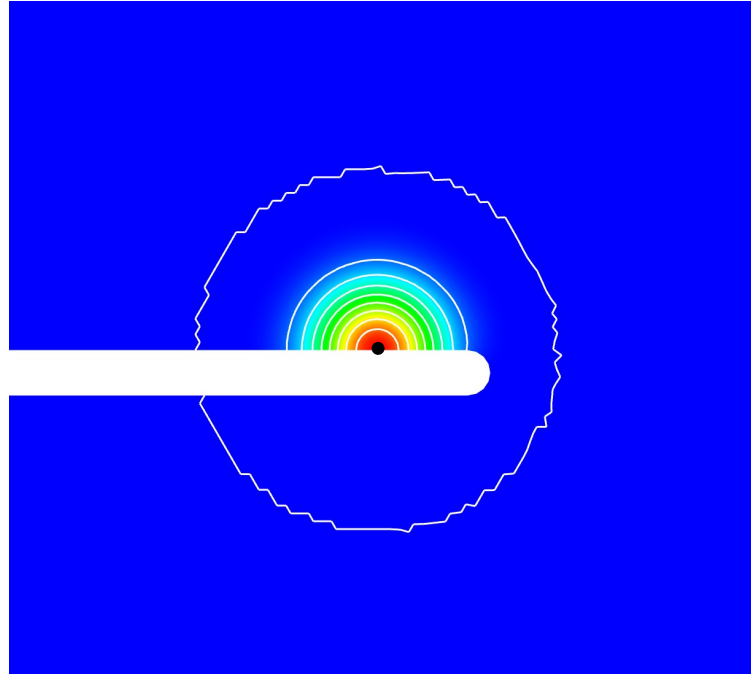
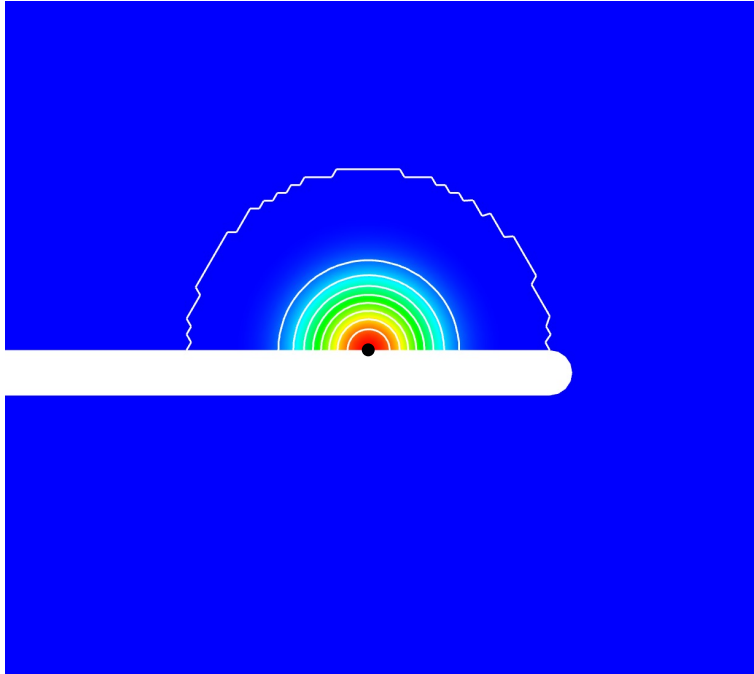


Fig. 1. Geodesic distance from a single point on a surface. The heat method allows distance to be rapidly updated for new source points or curves.

Weight functions using heat flow

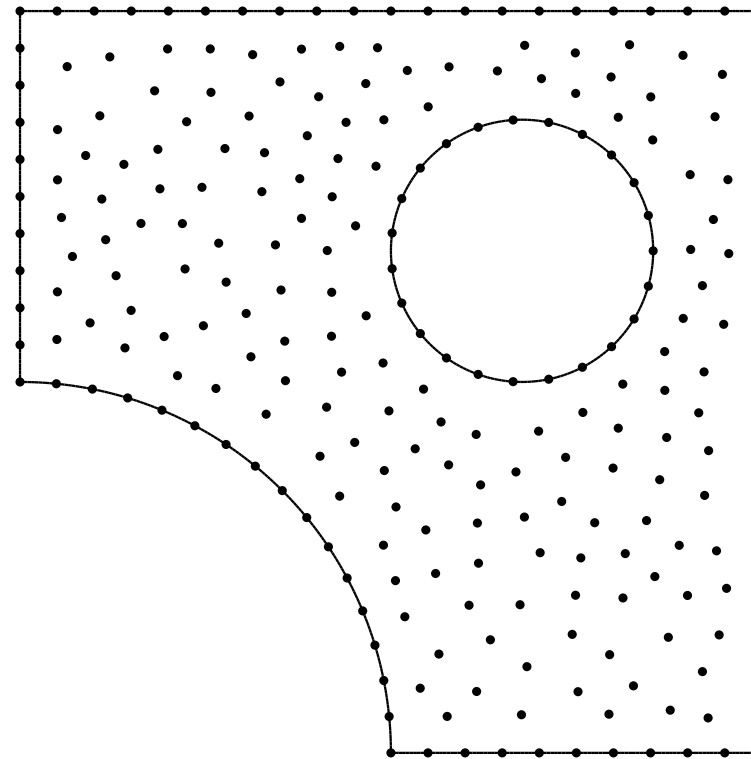
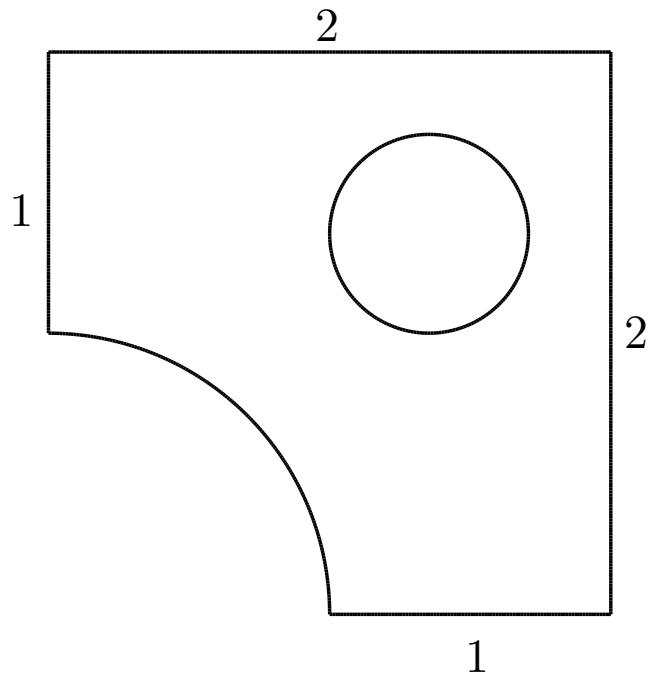


Weight functions using heat flow



"Point" placement

- uniform on boundary
- random close packing on interior (maximal Poisson sampling)



packing size:

$$H = 0.1$$

Weight function support size



packing size: $H = 0.1$

$R = 2H$

linear

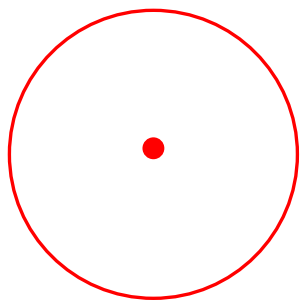
$R = 3H$

quadratic

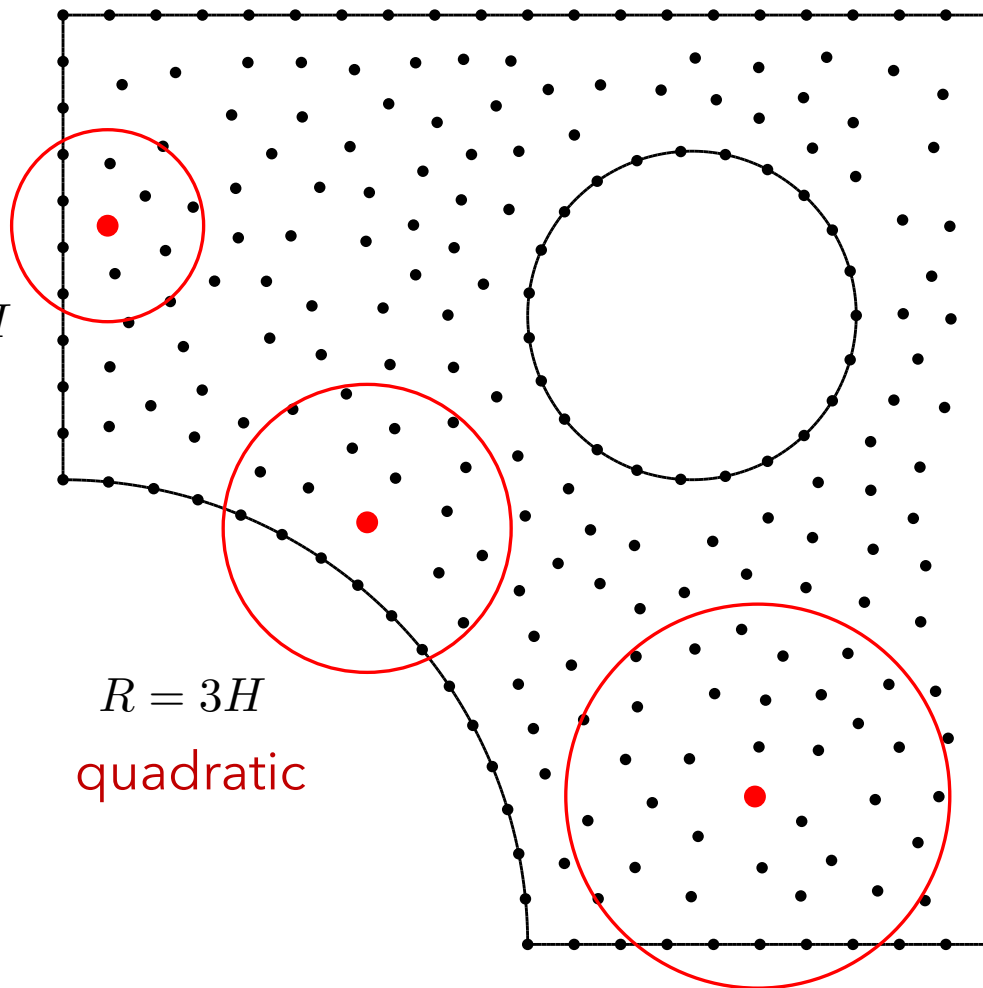
$R = 4H$

cubic

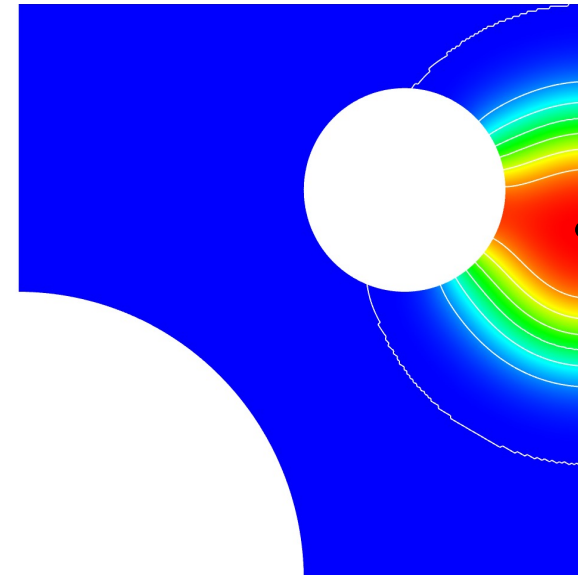
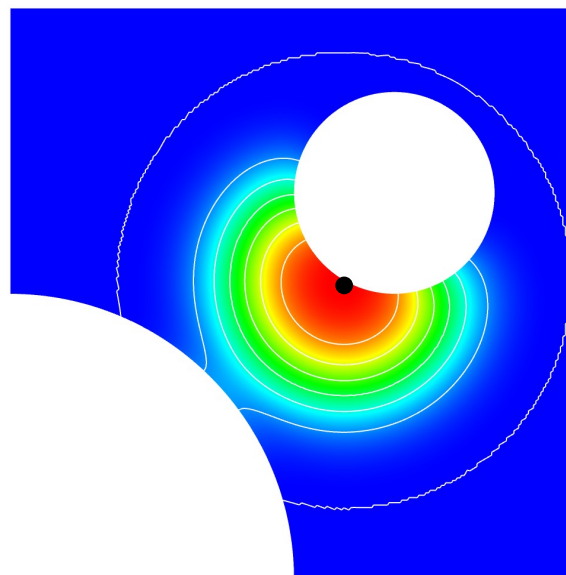
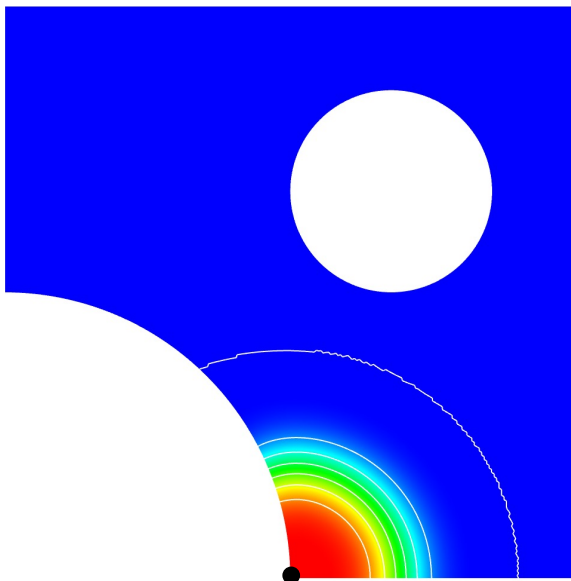
support size



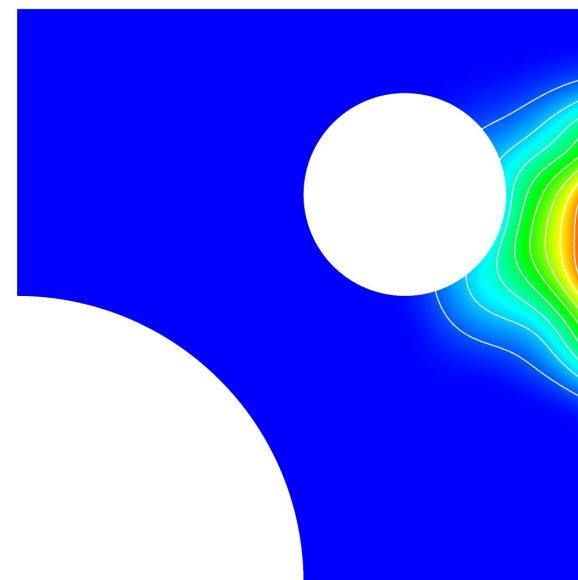
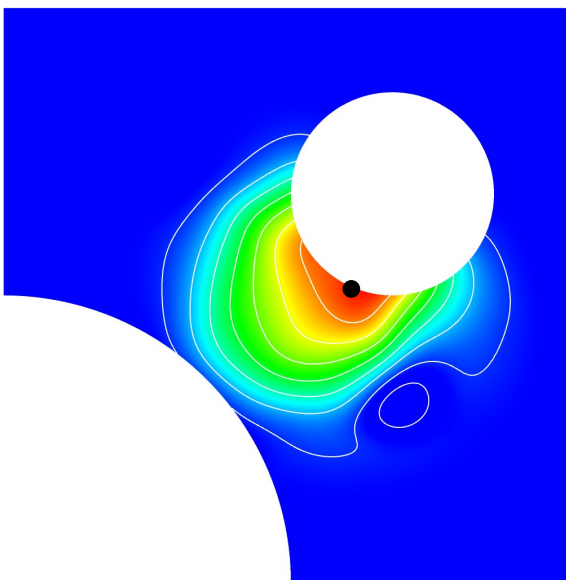
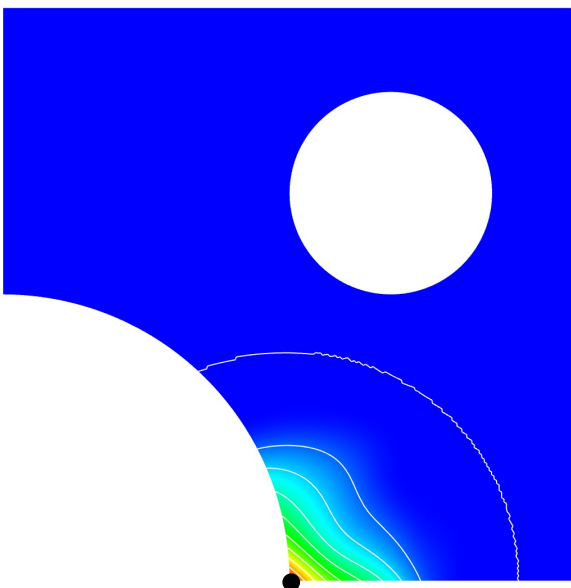
encloses underlying tri mesh



weight
functions



shape
functions
(basis)

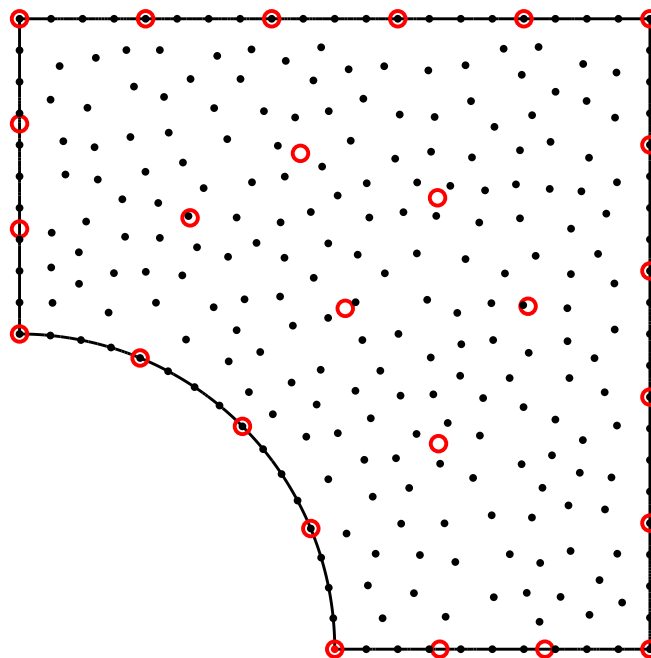


Element-free approach to solve BVPs



Use two meshfree clouds: one for solution discretization (DoF) and one for quadrature.

- DoF node
- quadrature nodes



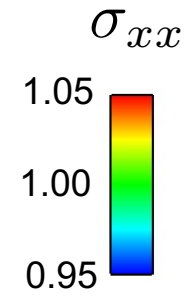
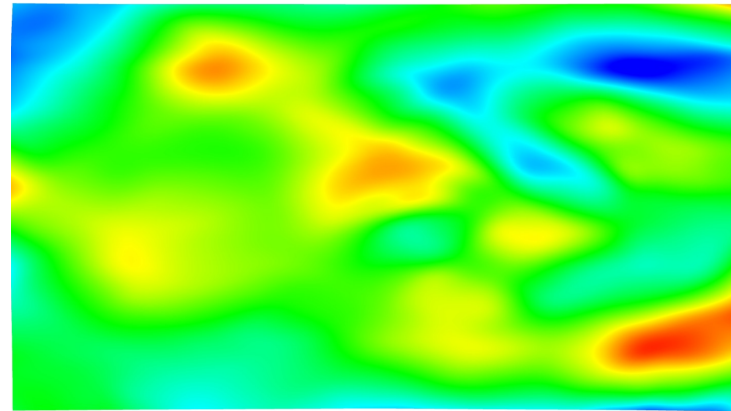
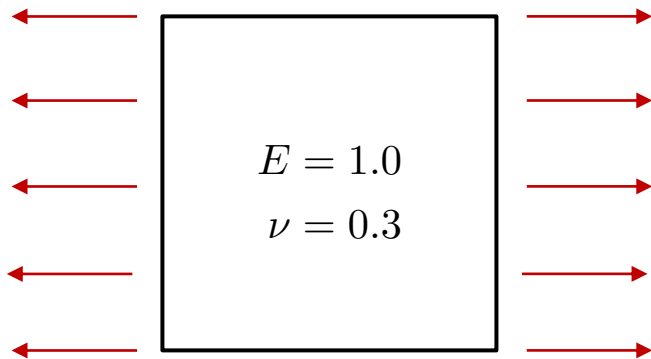
quad-to-dof ratio = 4^2

What ratio of quad nodes to dof nodes is needed for stability (coercivity of bilinear form)?

Patch test (linear consistency)



uniaxial tension



error > 5%

Consistency of discrete form (integration)

- For convergence of discrete approximation, need to ensure consistency of discrete and continuous bilinear forms.
- Requires polynomial consistency of shape-function gradients (including quadrature).
- To obtain quadrature consistency, project the DoF shape function gradients to the subspace of quadrature shape functions.
- Only performed once in a pre-processing step.

$\{\phi_I, I = 1, \dots, N\}$ *DoF basis (shape functions)*

$\{\Phi_K, K = 1, \dots, M\}$ *Quadrature basis (shape functions)*

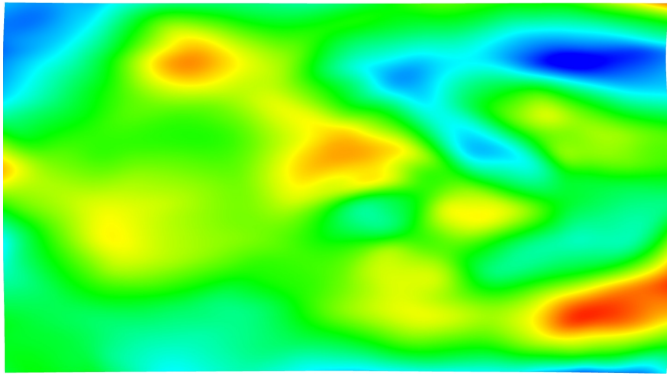
$$\bar{\nabla} \phi_I := \arg \min \int_{\Omega} \left(\nabla \phi_I - \sum_{K=1}^M a^K \Phi_K \right)^2 d\Omega \quad (L_2 \text{ projection})$$

Patch test (linear consistency)

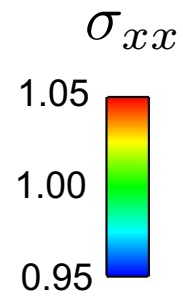


uniaxial tension

no projection



error $> 5\%$

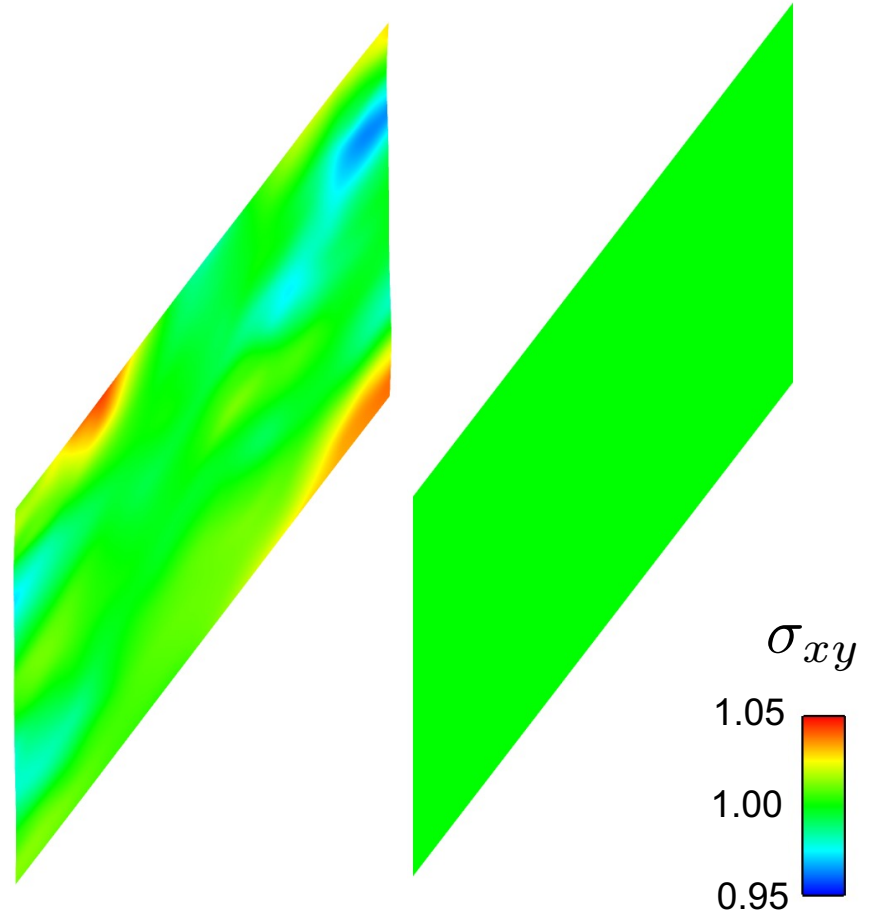


with projection

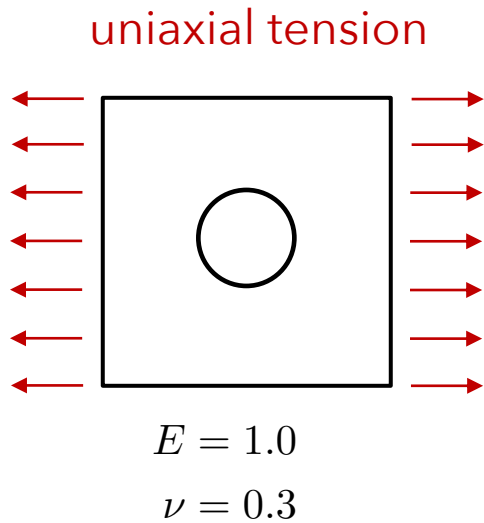


error $< 10^{-13}$

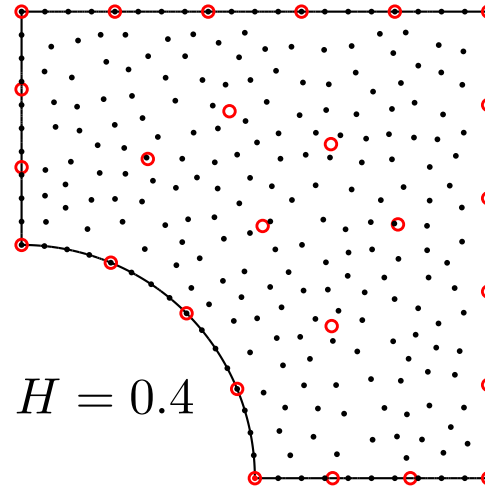
pure shear



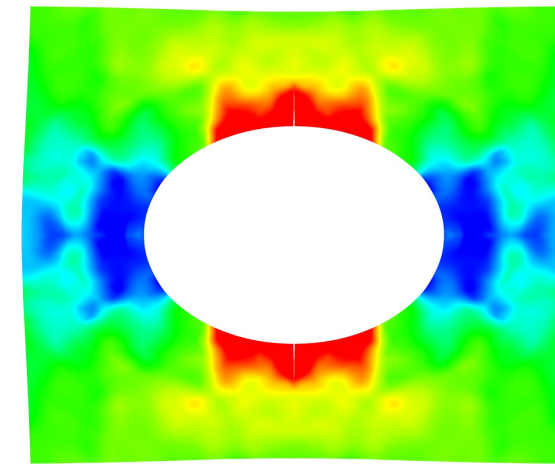
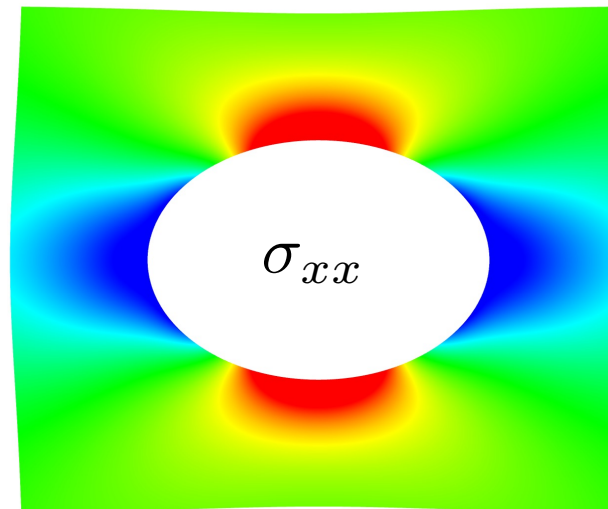
Example: plate with hole



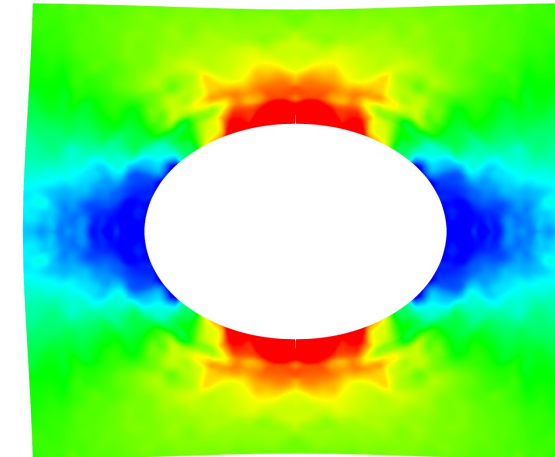
- plane strain
- quarter symmetry



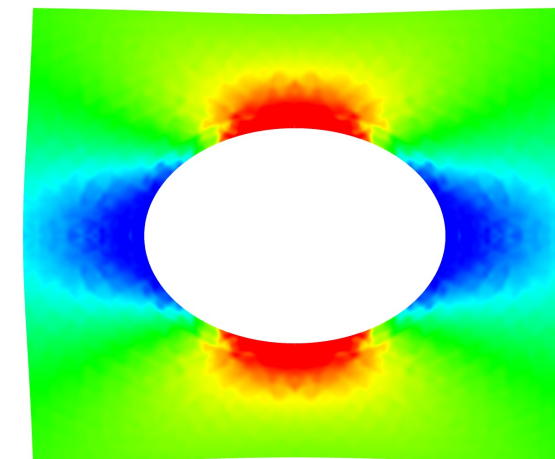
exact



$H = 0.4$



$H = 0.2$

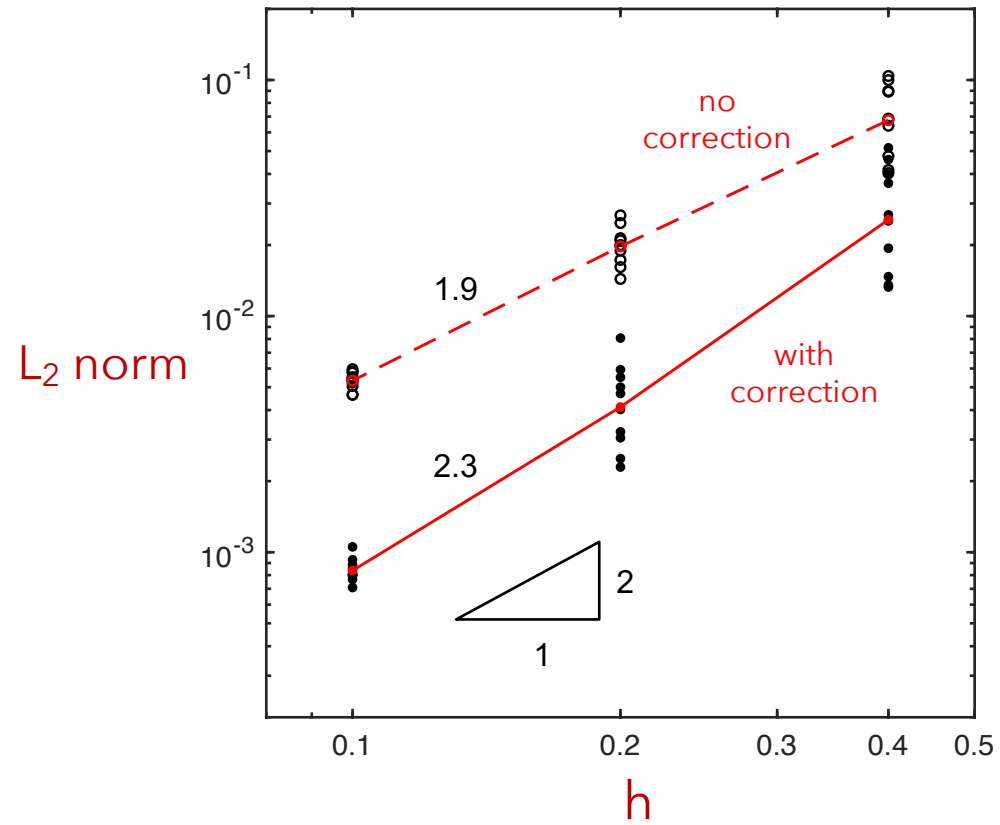


$H = 0.1$

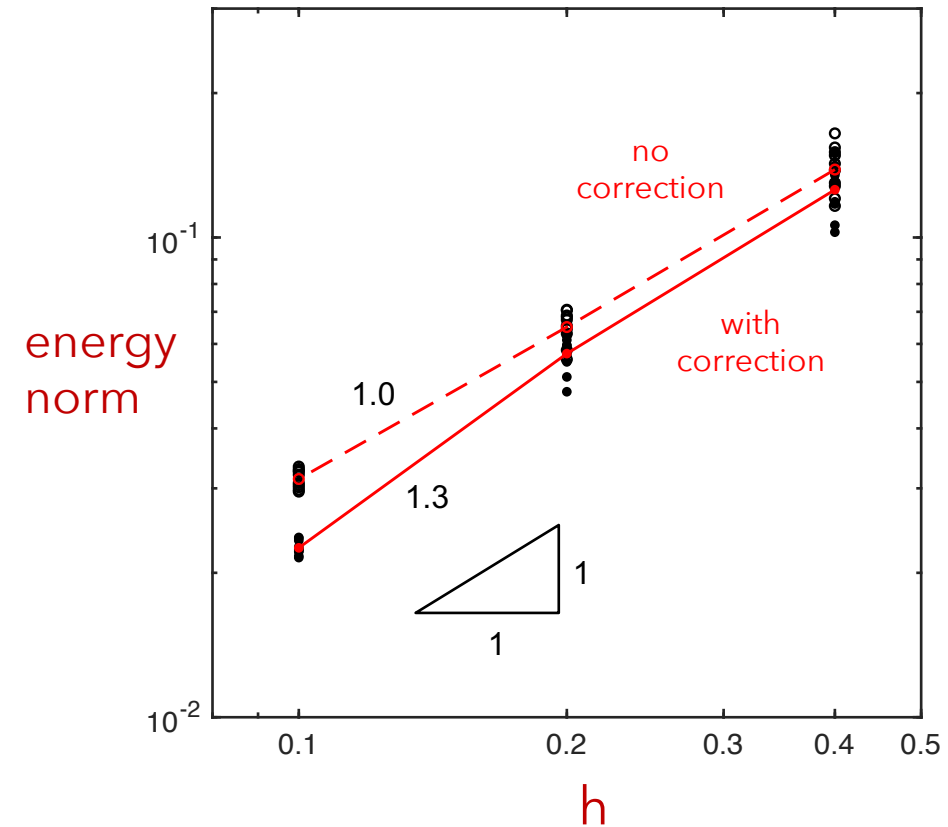
Example: plate with hole



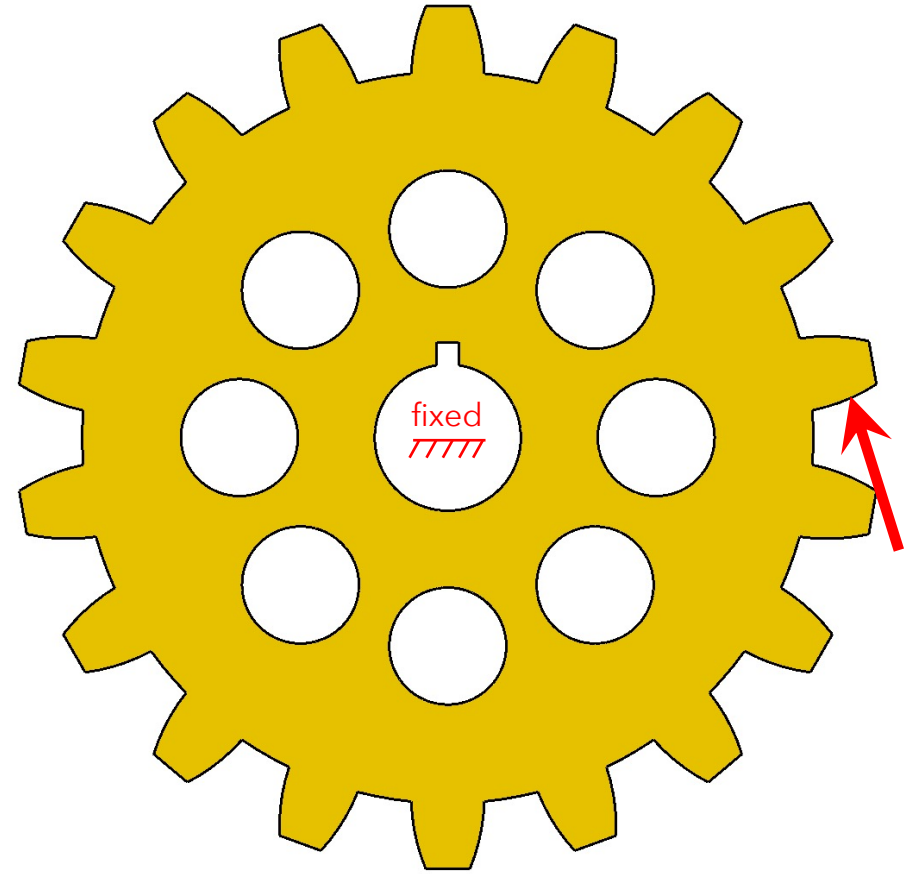
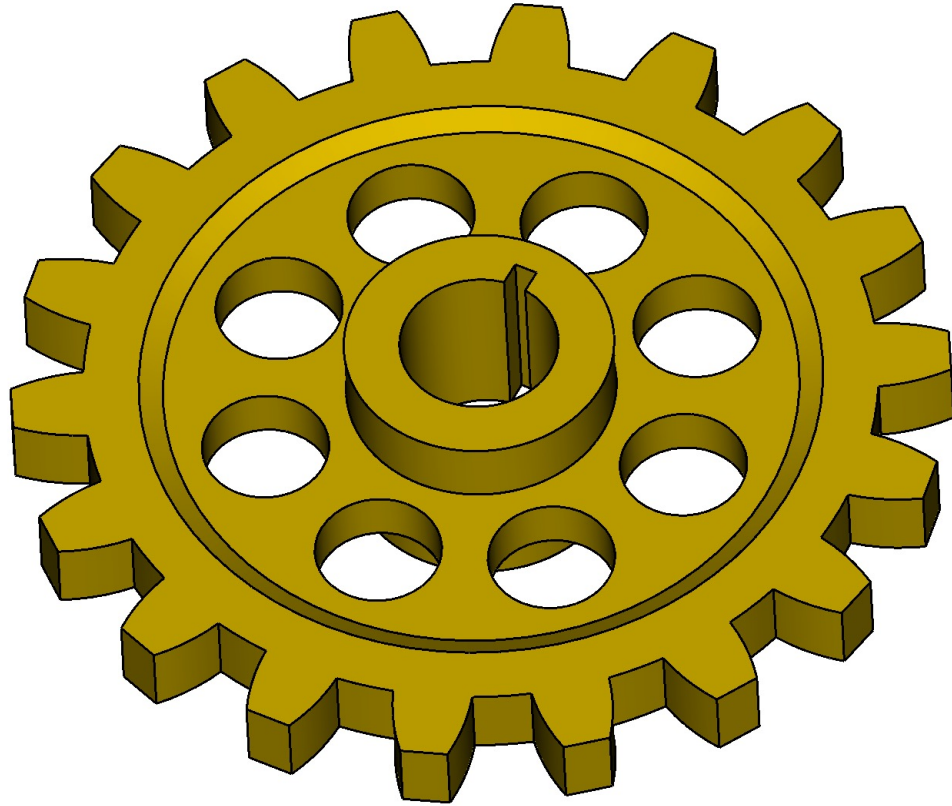
L_2 norm



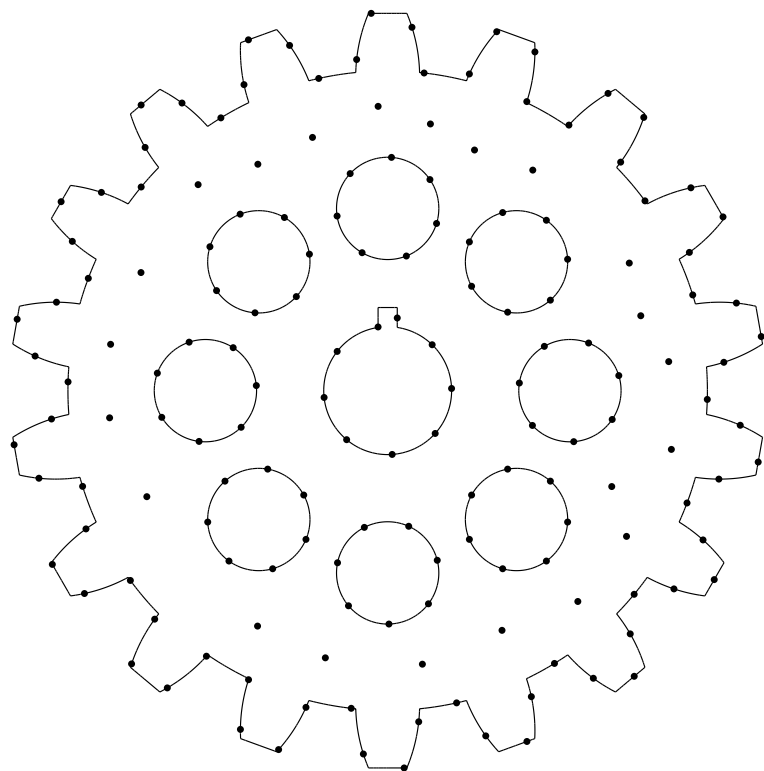
energy norm



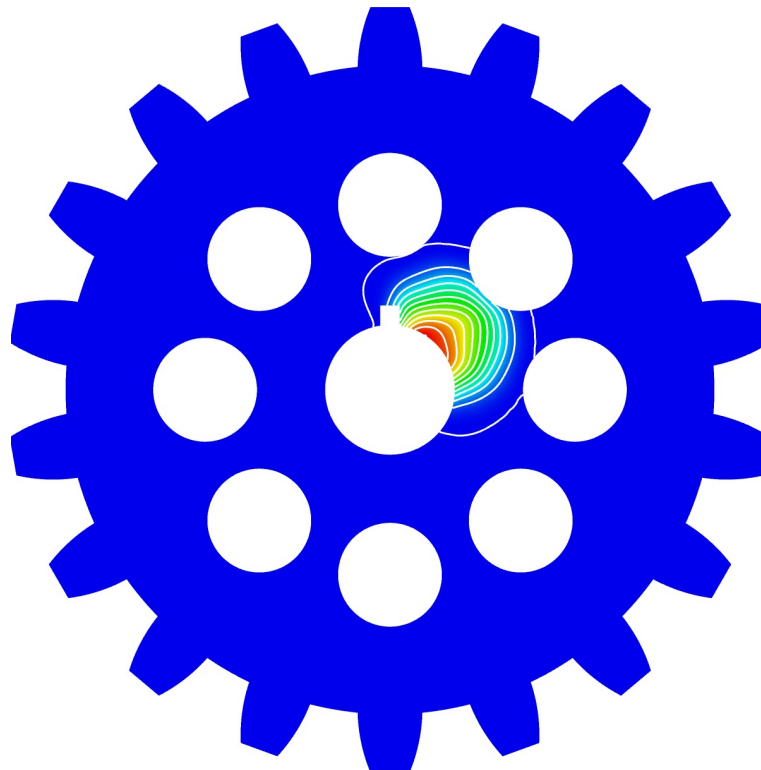
Example



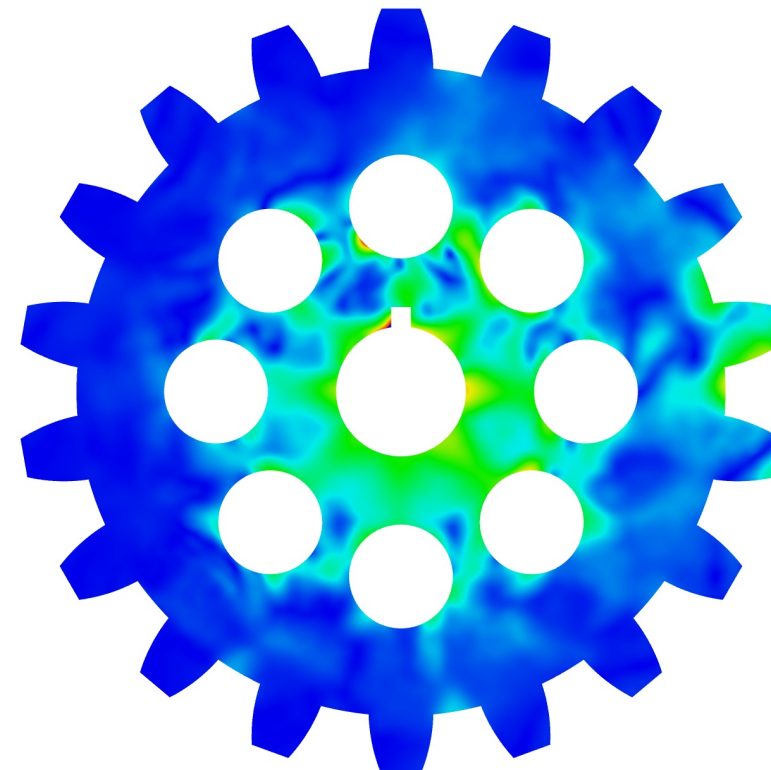
dof nodes

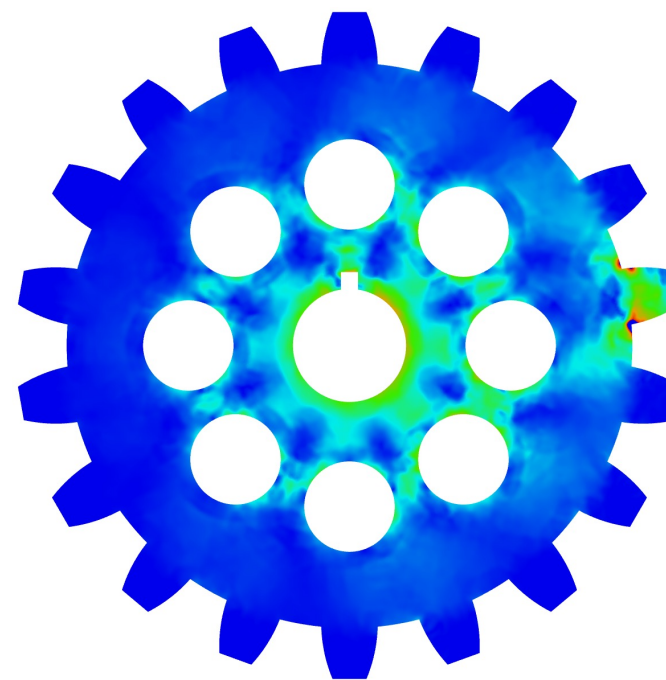
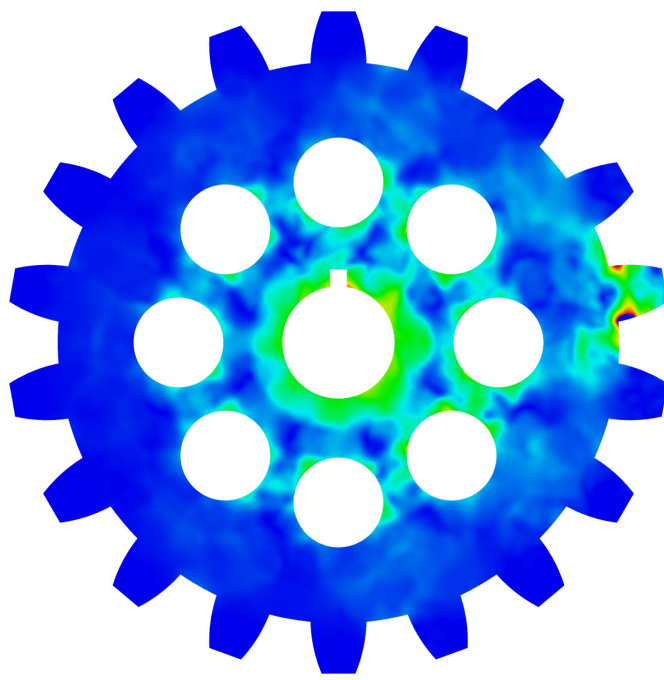
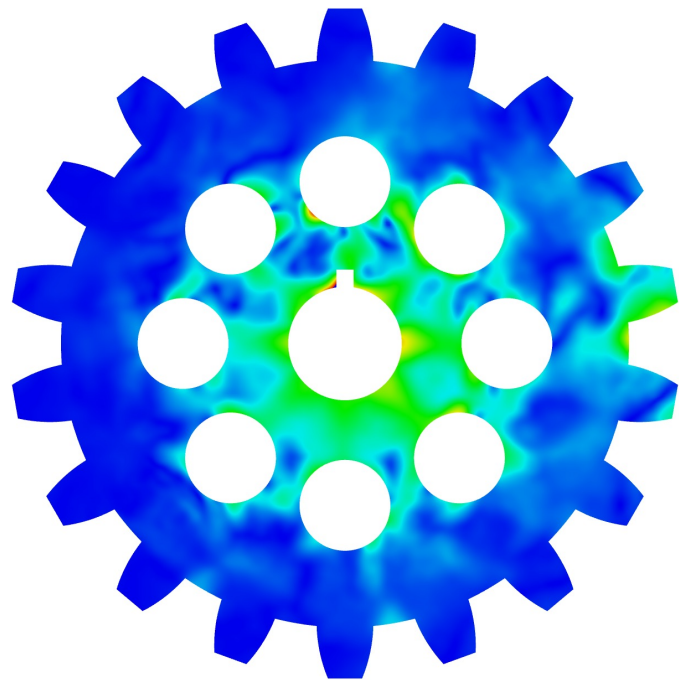
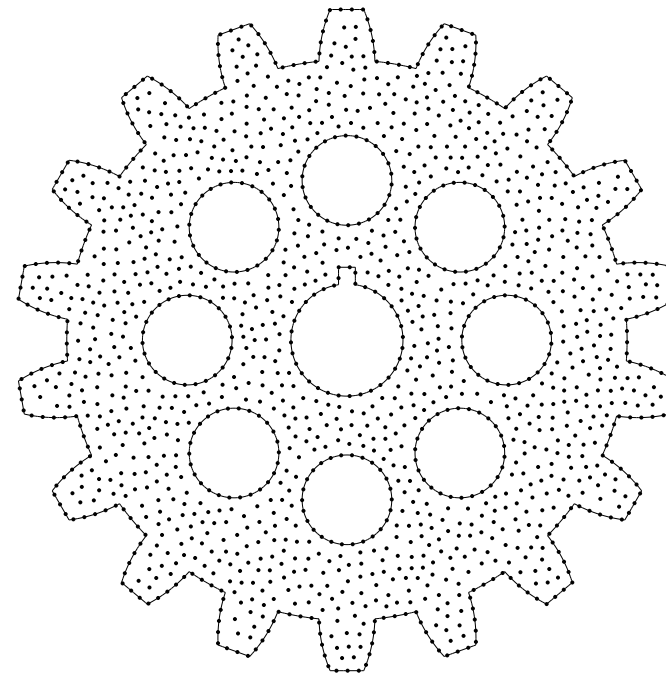
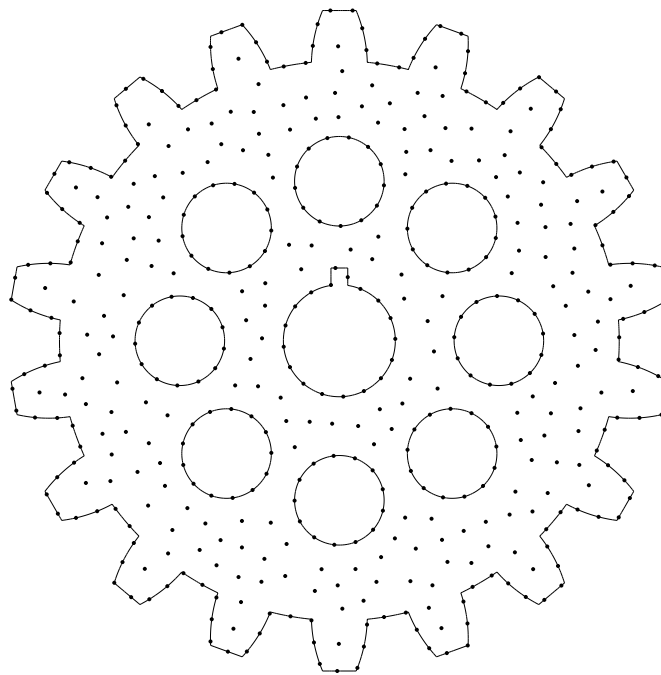
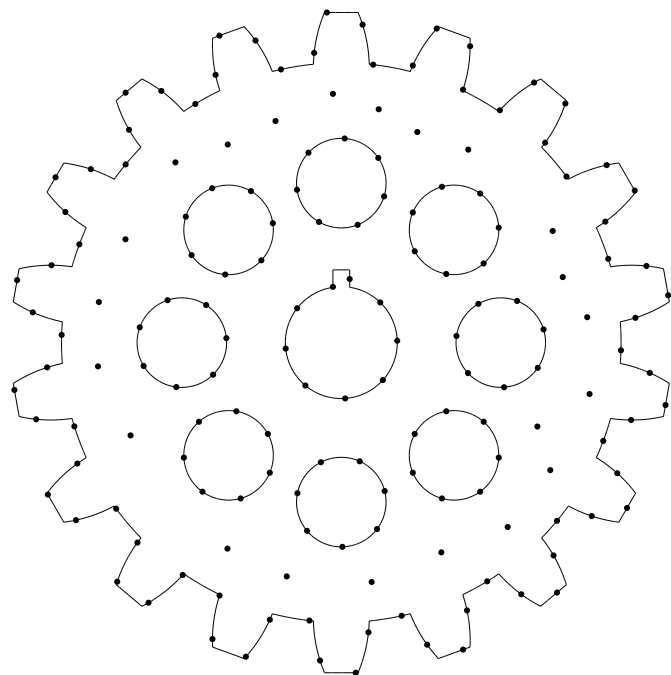


basis functions



stress field (vm)

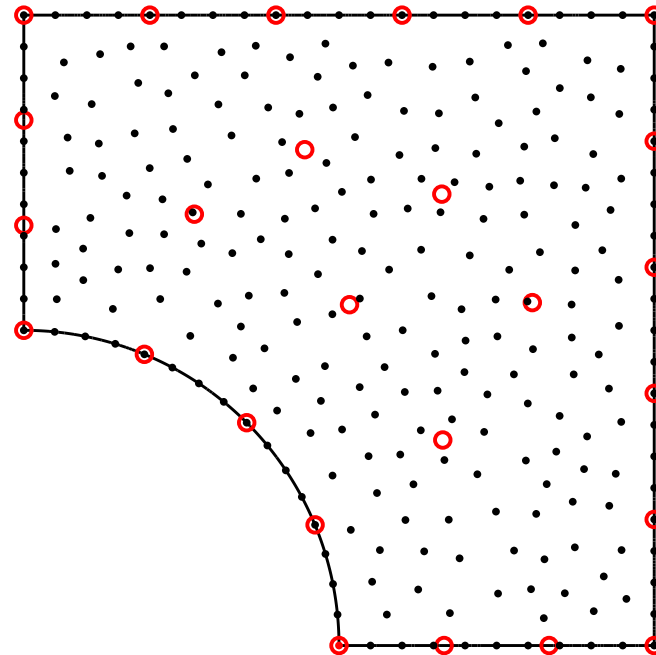




Nearly incompressible limit



- Can extend approach to handle nearly incompressible materials
- Use a “generalized” B-Bar/F-bar approach.
- Project dilatational portion of deformation gradient to smaller subspace, e.g. use original DOF points as quadrature basis.



- DoF node and dilatational quadrature node
- deviatoric quadrature node

Summary



1. Showed applications of GBCs to both element-based and element-free PDE discretizations
2. GBCs enable formulation of a diverse set of polyhedral discretizations.
3. GBCs enable element-free discretization on complex **disconnected** domains without resource to computational geometry.
4. Element-free weight function used manifold geodesic (heat map)
5. GBCs also induce quadrature schemes for both element-based and element-free methods.
6. GBCs facilitate gradient projection schemes for PDE consistency.
7. Applications to multiresolution (wavelet) on complex shapes?