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Development of C-Ring Geometry to Explore Fatigue Crack Extension and Verification in High-Pressure Vessels

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ASME 2022 Pressure Vessels & Piping Conference

July 17-22nd, 2022

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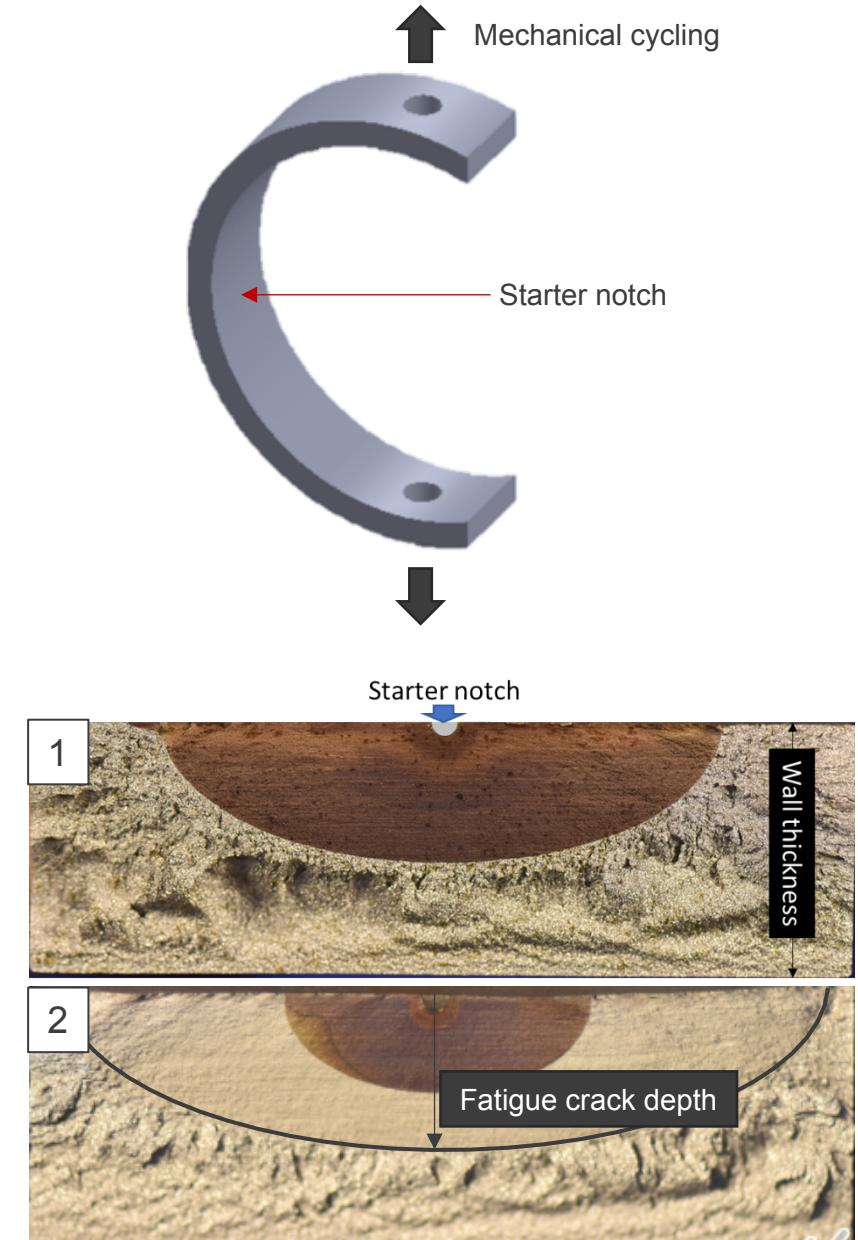
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Outline

- Background and motivation
- Sample design and test methods
- Experimental results and comparison with simulated crack growth
- Summary and conclusions

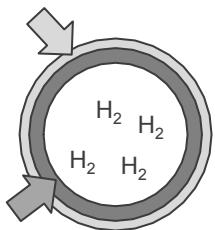




Motivation: Avenues for Life Extension of Pressure Vessels

- High pressure hydrogen storage vessels, such as those used at hydrogen refueling stations, are retired upon reaching their designed number of pressure cycles
 - Design cycle life is defined in User's Design Specification (UDS) based on pressure range
- One avenue for extending the life of hydrogen vessels is recertification through non-destructive evaluation (NDE)
 - Currently no commercially available means to perform NDE on Type 2 vessels, therefore vessels are retired

Hoop wrapped carbon fiber



Steel liner

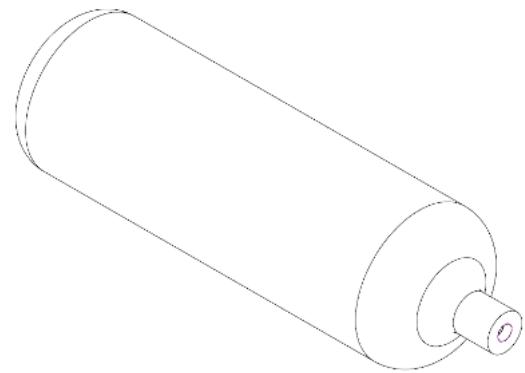


Type 2 vessels are commonly used at Hydrogen Refueling Stations (HRS)



Motivation: Avenues for Life Extension of Pressure Vessels

- Goal: Development of a representative NDE sample/methodology that can:
 - Develop fatigue cracks to prescribed depths
 - Provide NDE calibration data based on sharp fatigue cracks (as opposed to machined notches)
 - Provide a testing platform to simulate compressive residual stresses induced by autofrettage or proof testing
- The scope of this paper includes the development and analysis of a representative NDE sample from a type 1 pressure vessel
 - NDE validation and calibration is planned but not discussed in this presentation



Schematic of type 1 pressure vessel (above) and ring section extracted from a type 1 vessel (below)



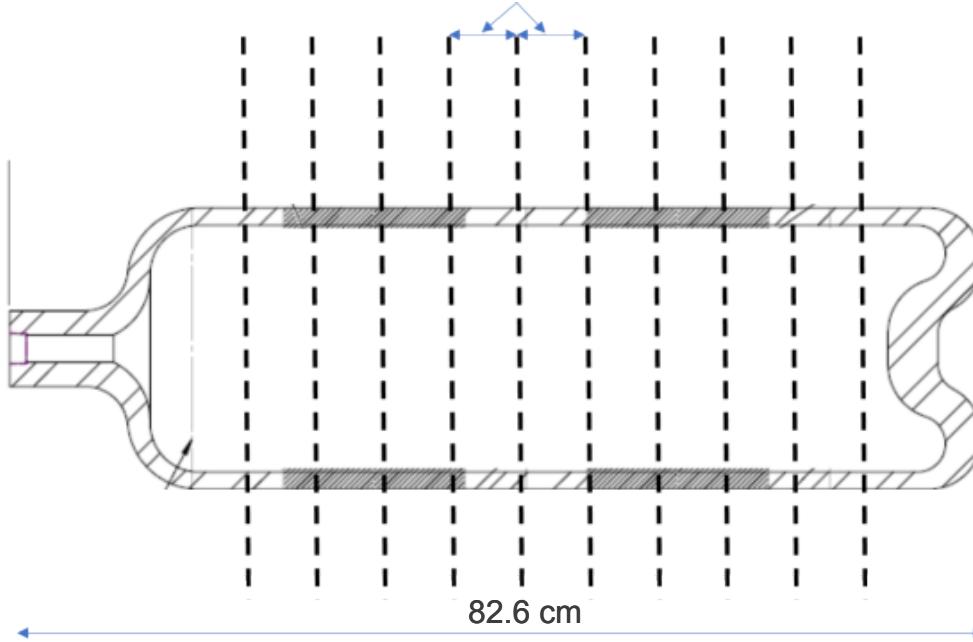
OD = 238mm
t = 14.5mm



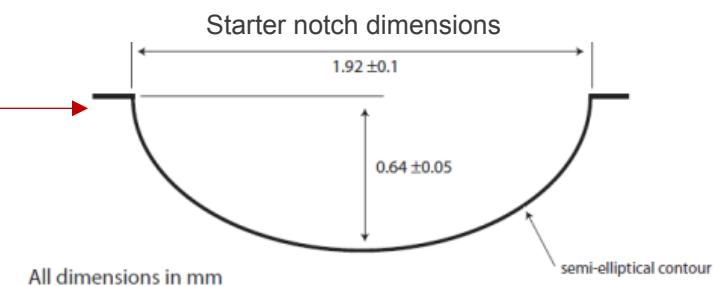
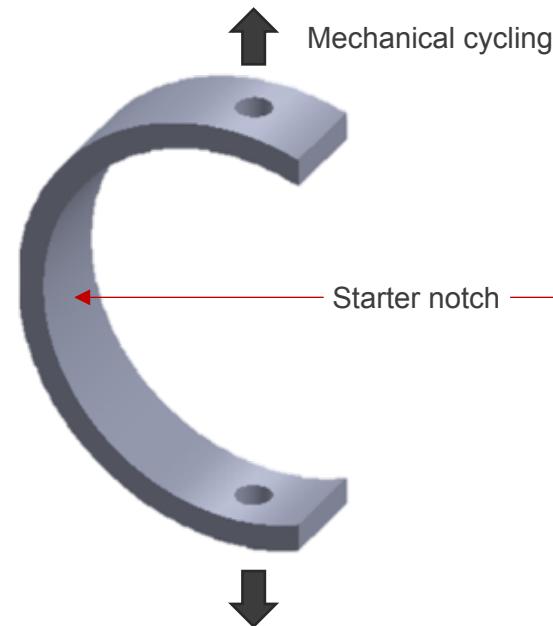
Material and C-ring Sample Design

Type 1 Pressure Vessel

50.8 mm wide ring sections



C-ring Sample Geometry

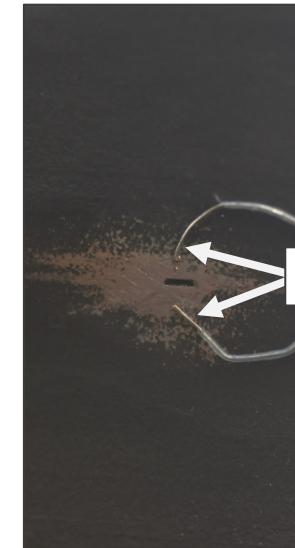


- C-ring samples were machined by extracting ring sections from an all-steel transportable pressure vessel (type 1)
 - Sides of the ring sections were removed (giving the sample a “C” shape) and $\frac{3}{4}$ ” bolt holes were added to allow for mechanical cycling or static loading during NDE
- Starter notches were added (plunge EDM) to ensure crack growth initiated at the center of the C-ring samples

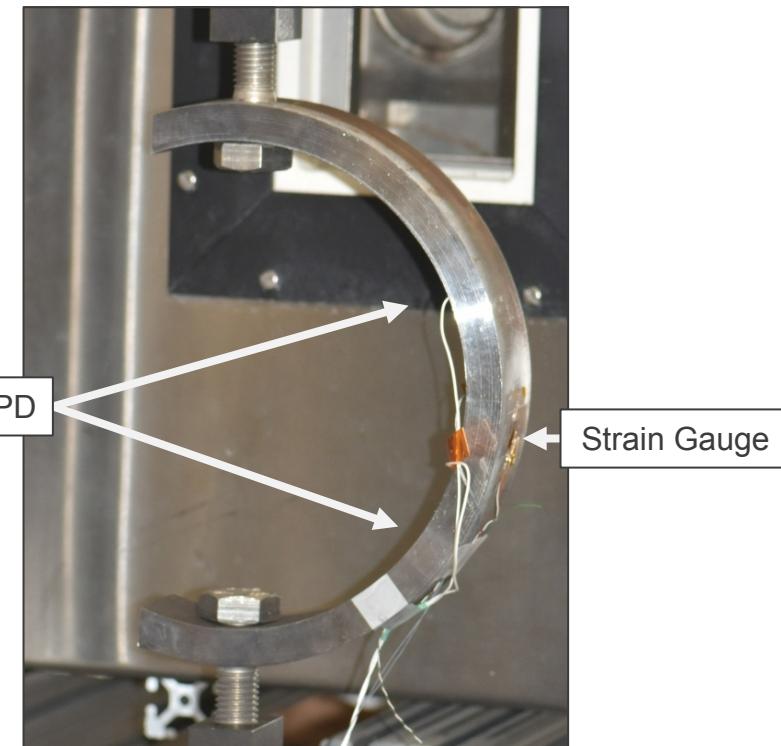
Crack Growth Monitoring through DCPD and Backface Strain

- To monitor crack growth, C-ring samples were instrumented with:
 - Direct current potential difference (DCPD)
 - Backface strain gauge
- Post-fatigue, samples were submerged in LN₂ and fractured open
- Heat tinting (275°C / 30 min) was utilized to mark fatigue crack growth at specific stages of the test

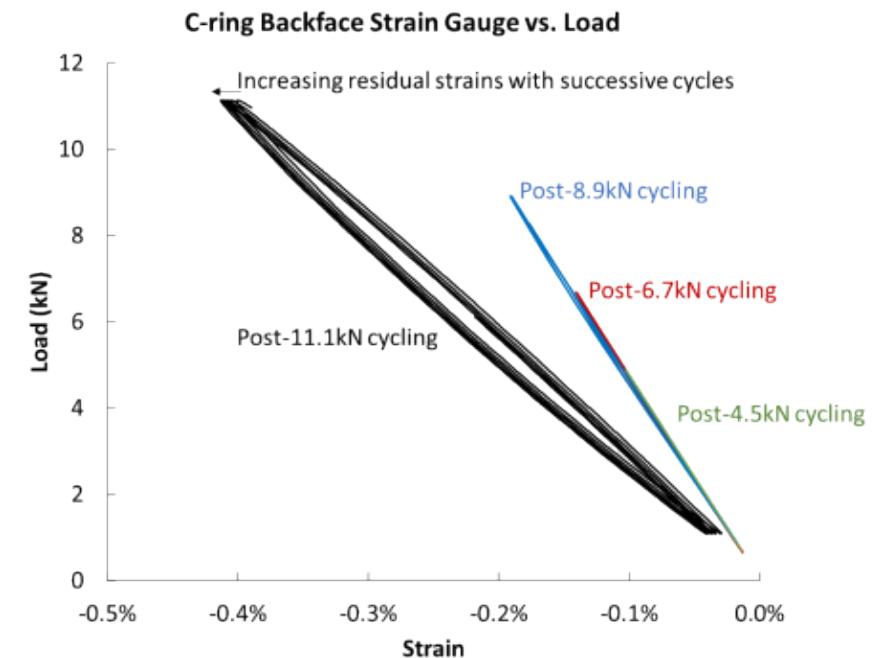
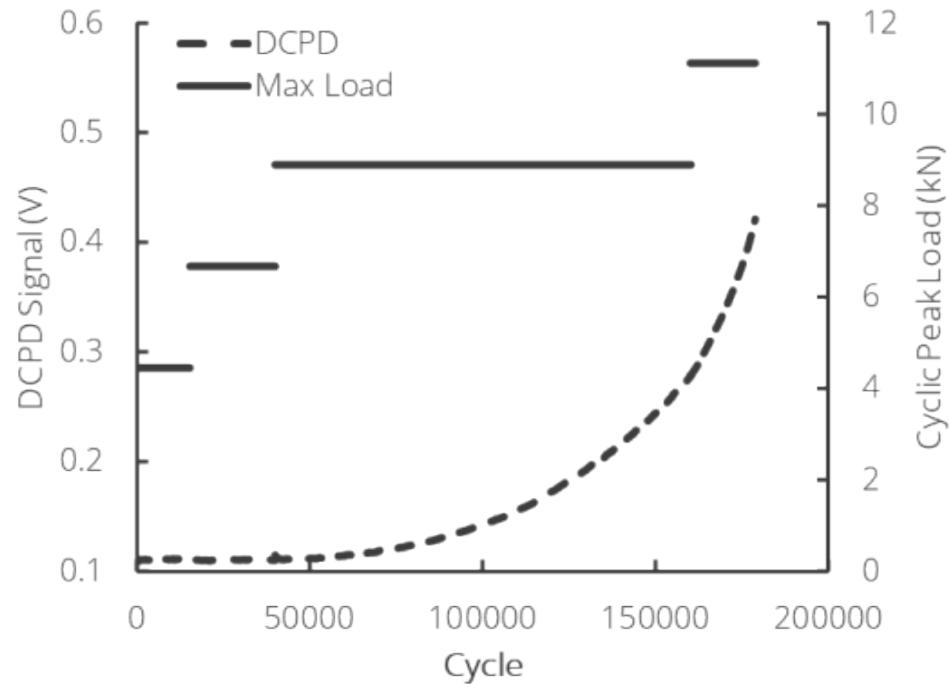
DCPD and Starter Notch on Sample 1



C-ring Sample 1 on Load Frame



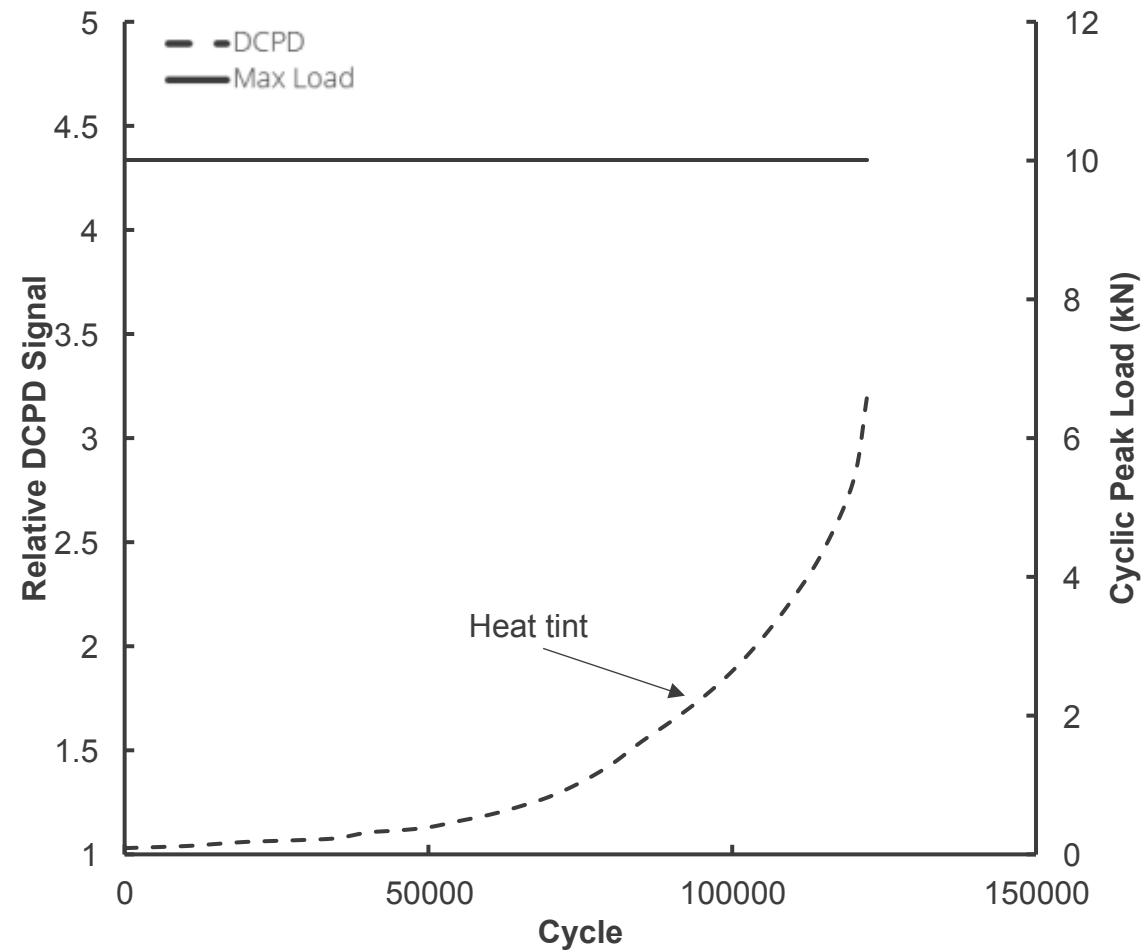
Fatigue Cycling at Increasing Maximum Loads



- Two C-ring samples were mechanically cycled to induce fatigue crack growth
 - $R = 0.1$ (Min/Max load)
 - Both DCPD and backface compliance (slope of the load-strain curve) monitored throughout tests
- Loads below 8.9kN (2000 lbf) had minimal effect on the measured compliance and DCPD
- Higher loads resulted in crack propagation, as indicated by the increasing DCPD and compliance

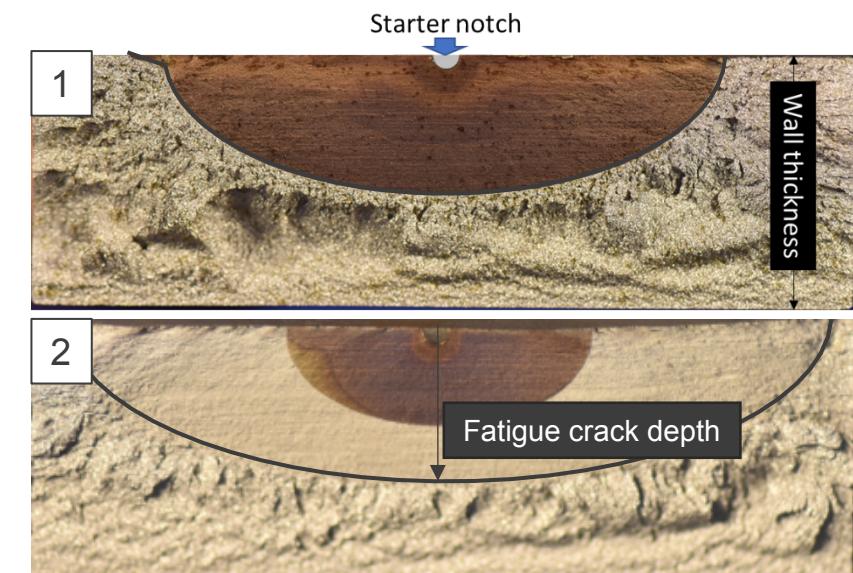
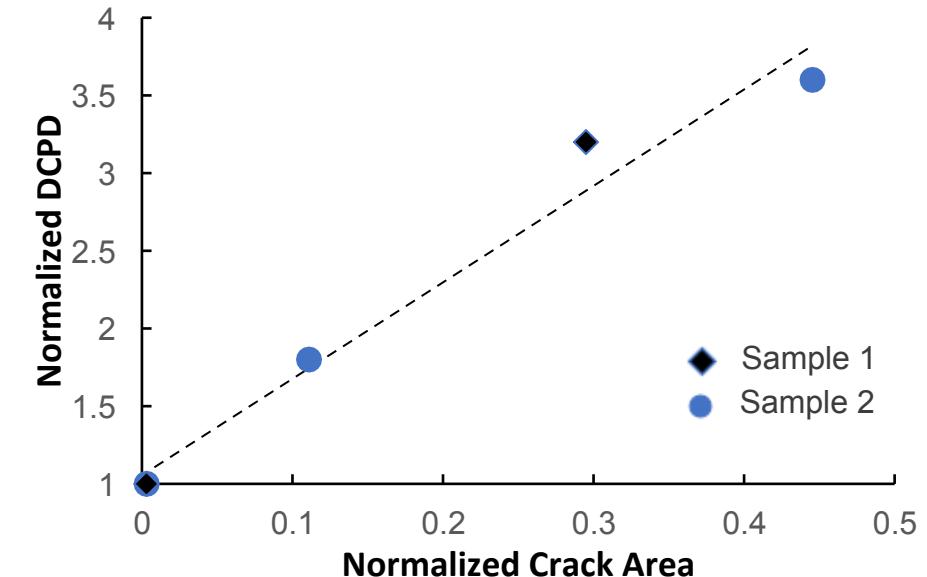
Fatigue Crack Growth at Constant (10kN) Max Load

- A second C-ring sample was cycled with a peak load of 10kN (2250 lbf) and $R = 0.1$
- The measured DCPD can be seen to increase at the beginning of the test, indicating the immediate onset of crack growth
 - The test was interrupted for heat tinting after the relative DCPD (measured/initial) reached a value of 2, which happened after $\sim 100,000$ cycles



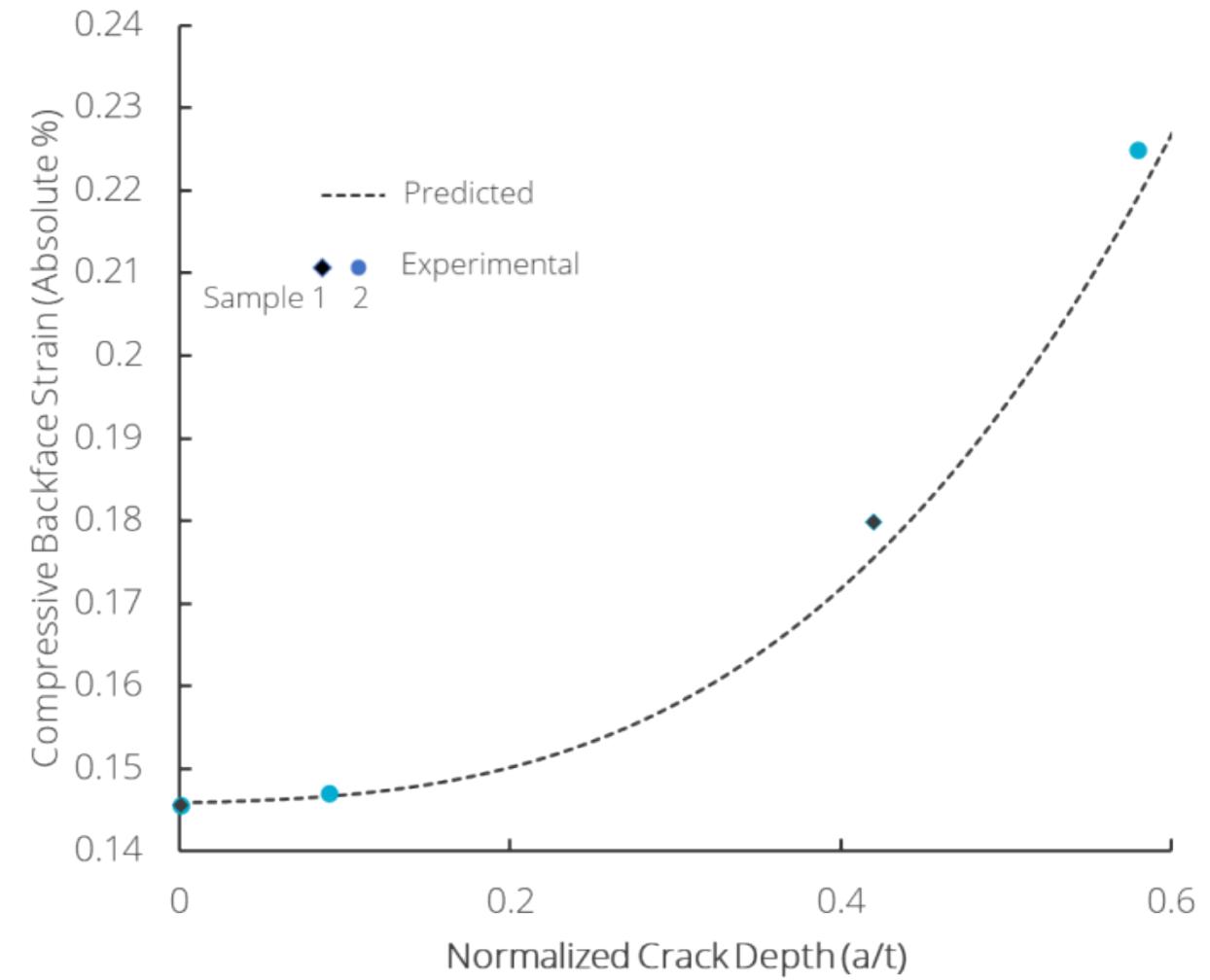
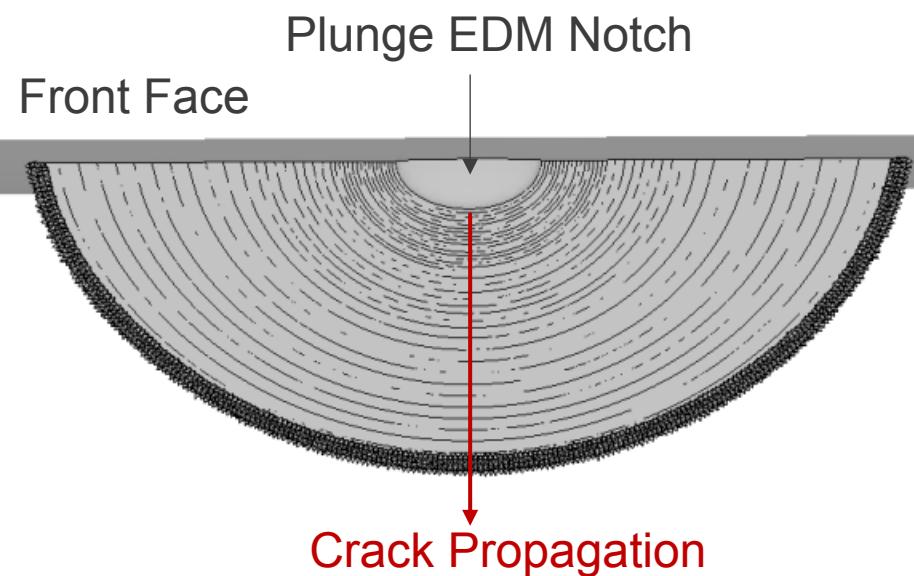
Linear Trend Observed between DCPD and Crack Area

- The DCPD (normalized by the initial measurement) was found to increase approximately linearly for increasing crack areas (normalized by cross-sectional area)
 - The linear estimation (dashed line) is fit to experimental data from both samples
 - Heat tinting during testing of sample 2 allowed for the collection of an additional data point



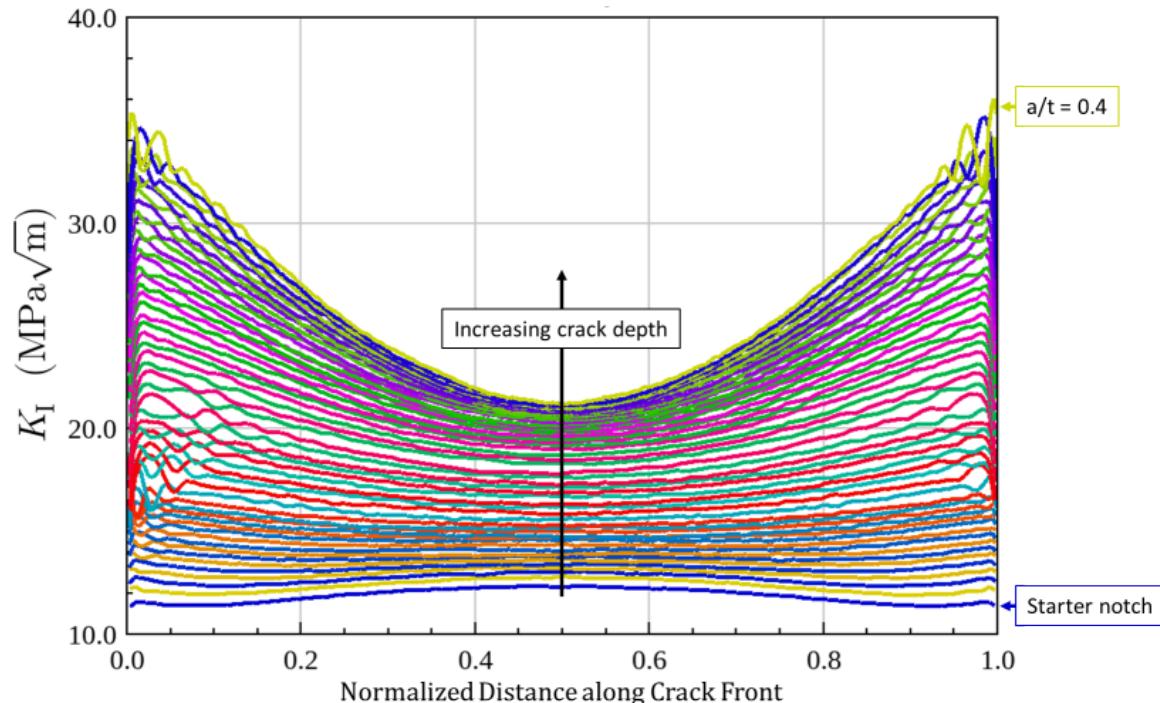
Comparison of Modeling and Experimental Backface Strains

- Simulations were performed to better understand the crack propagation and provide a relationship between the crack depth (a/t) and the measured strain on the backface of the C-ring samples
 - Simulations performed with Sierra/SM and FRANC3D

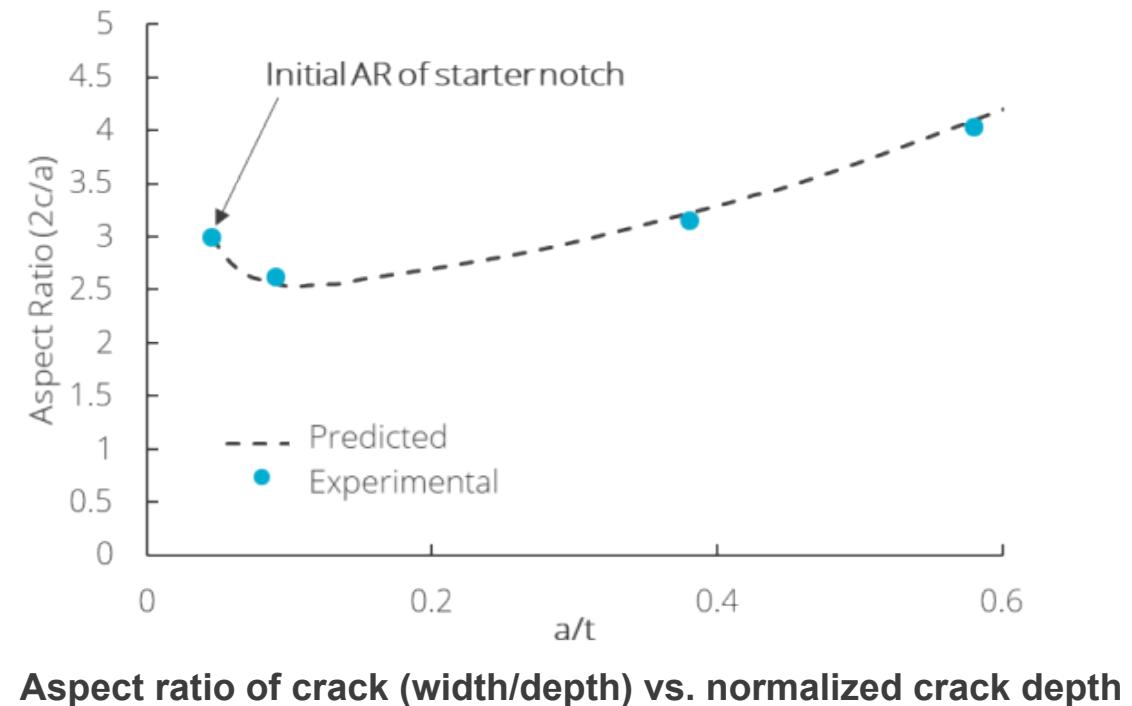


Compressive backface strain at a load of 6.7kN vs. crack depth

Model Predicts Evolution of Crack Geometry



K_I vs. position along crack front at a load of 6.7kN

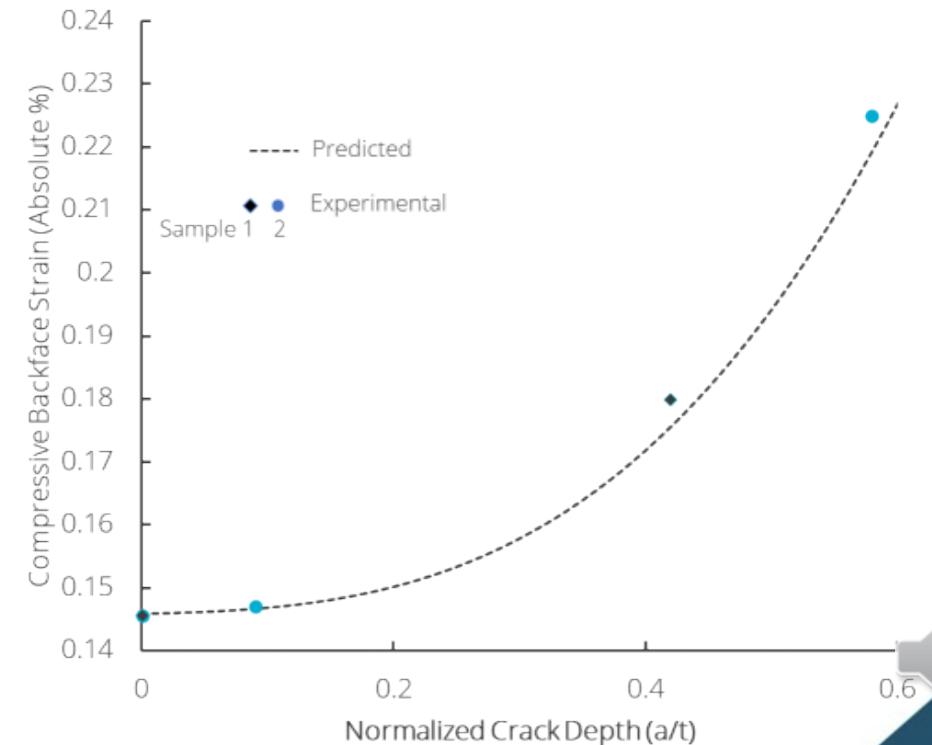
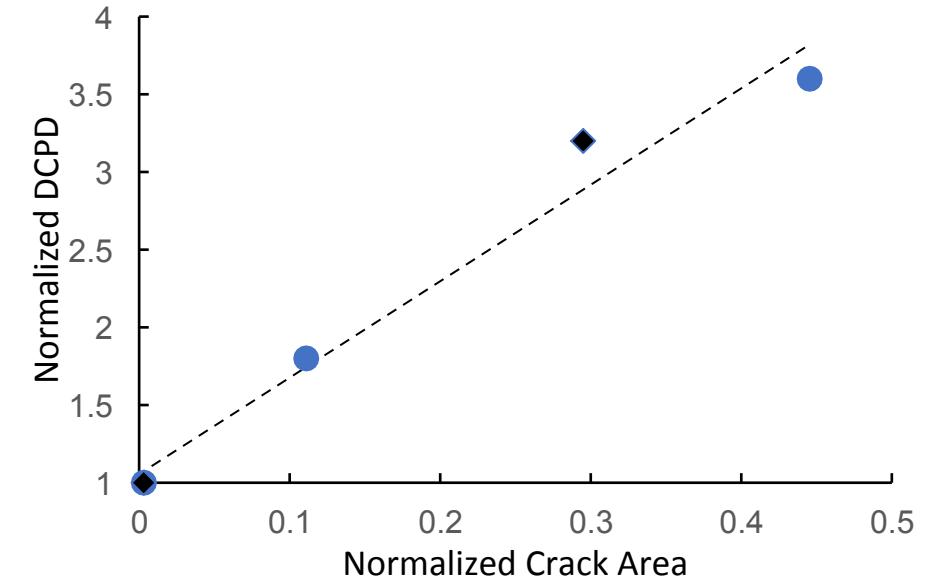


Aspect ratio of crack (width/depth) vs. normalized crack depth

- Initially, the maximum stress intensity factor (K_I) is located at the center (deepest portion) of the crack
- As the crack propagates deeper into the sample, the stress intensity factor becomes higher on the edges
 - This is due to the bending nature of the applied mechanical load, which induces compressive stresses at the backface

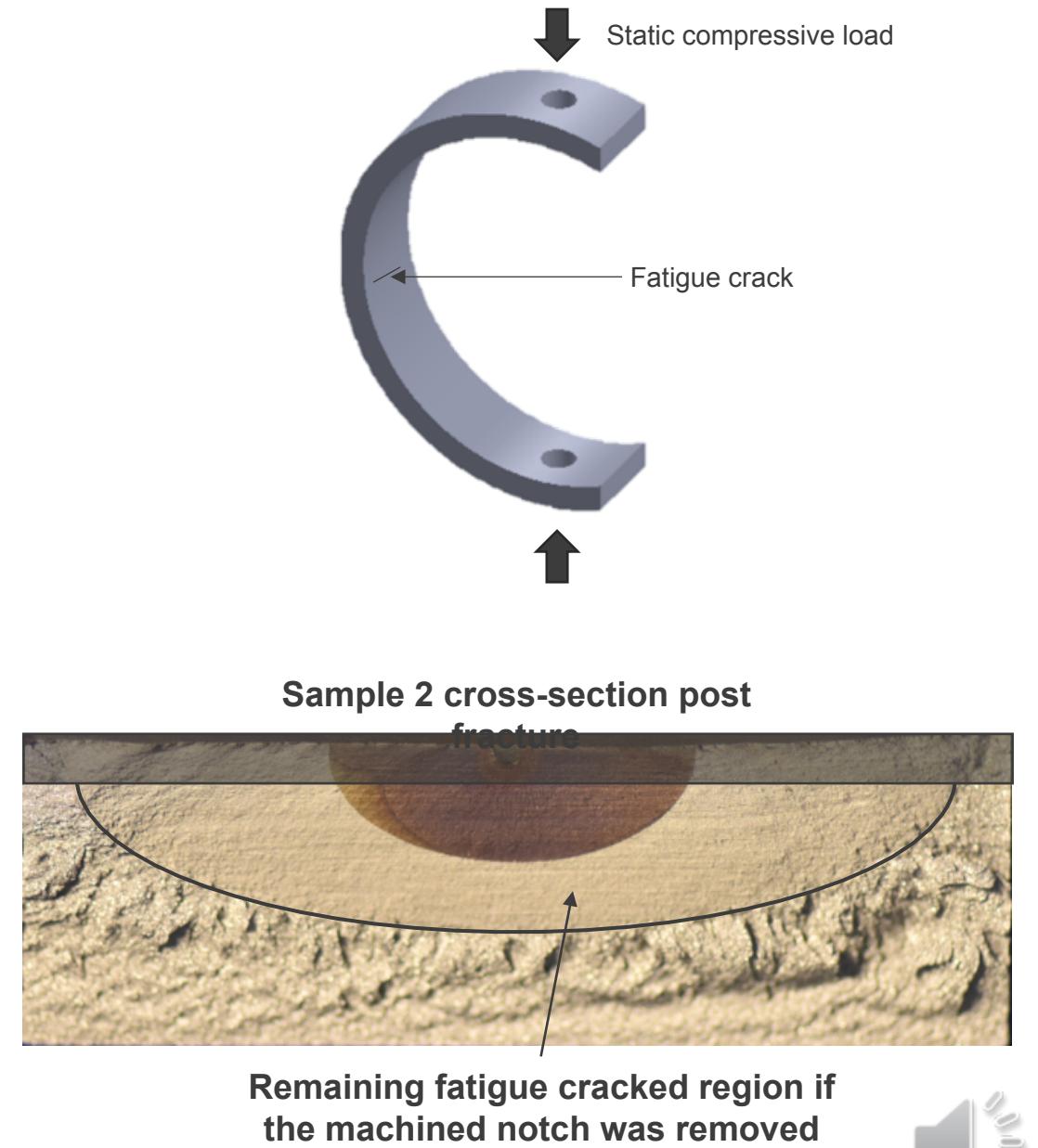
Summary and Conclusions

- C-ring specimens were extracted from a type 1 pressure vessel and mechanically cycled to induce fatigue crack growth
- Both DCPD and backface strain were found to be good indicators of crack area and depth (respectively)
 - The measured DCPD varied approximately linearly with crack area



Summary and Conclusions

- Using this C-ring geometry, cracks could be extended to prescribed flaw depths, which could then be inspected via NDE methods (e.g., eddy current)
 - The machined notch could be removed via grinding or polishing so that only the fatigue crack remains
 - After NDE, the C-ring can be heat tinted and fractured open to calibrate the NDE measurements with the true crack size
- The unique nature of the C-ring allows for either static compressive or tensile loading such that flaws could be scanned concurrent with applied stresses
 - Such as those that represent residual stresses from proof testing or autofrettage





Thank you for your attention!

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