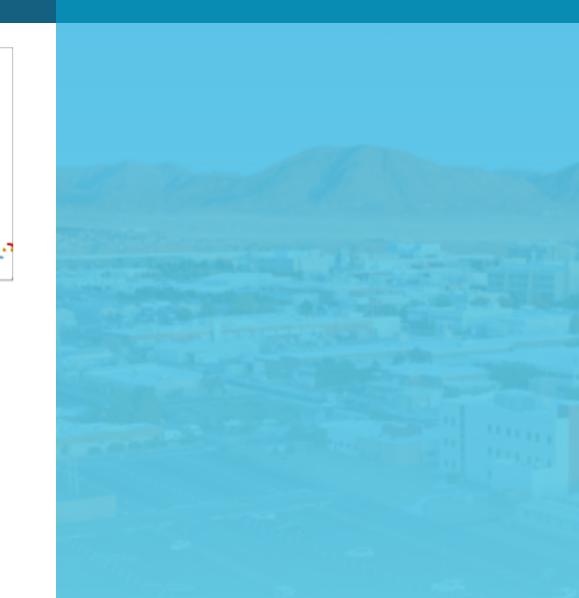
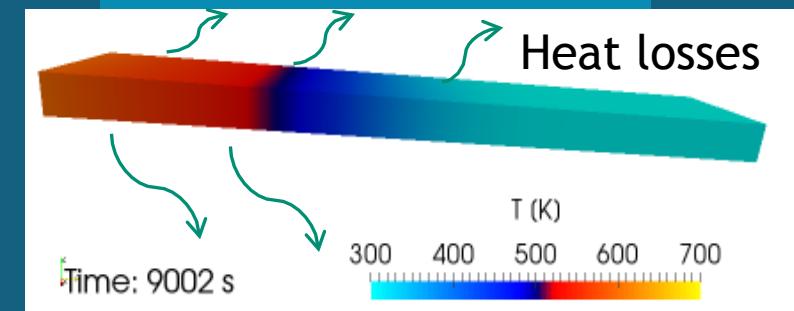
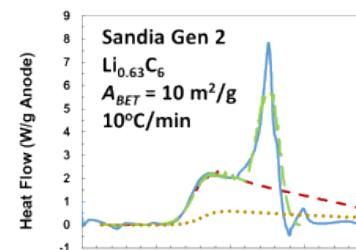
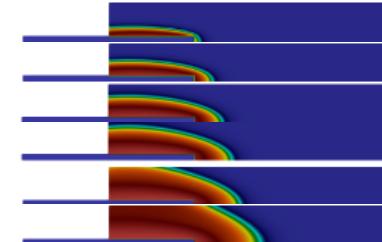
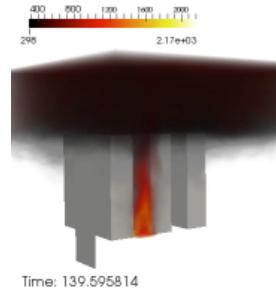




Sandia
National
Laboratories

Intra-Particle Diffusion-Limited Thermal Runaway Predictions in Lithium-Ion Systems



Presented by

Andrew Kurzawski, Randy Shurtz, Loraine
Torres-Castro, and John Hewson

Materials Research Society Spring Meeting and
Exhibit, May 5, 2022



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Thermal runaway and cascading failure



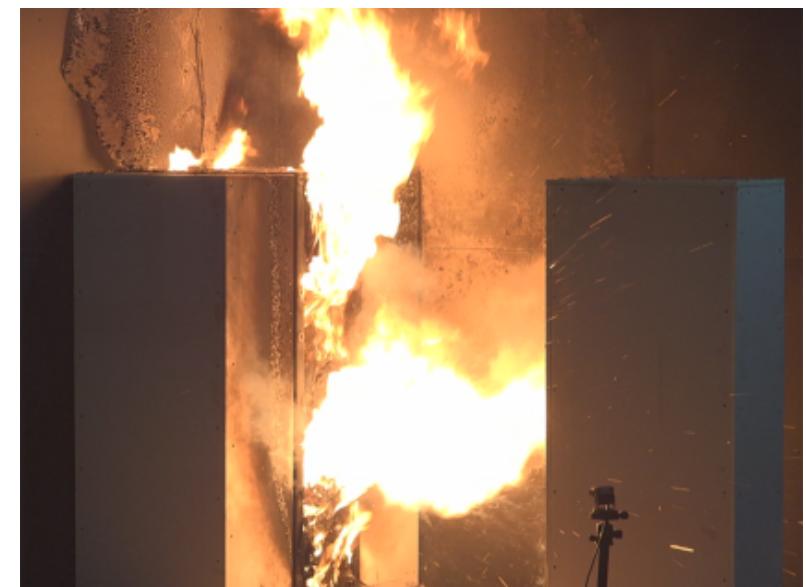
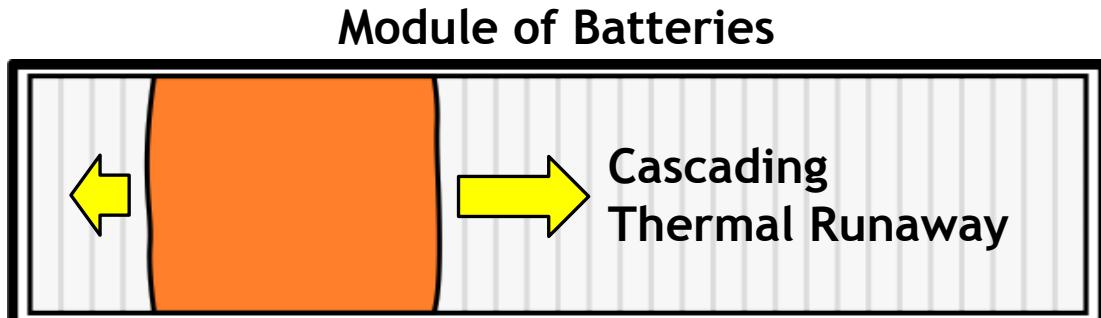
Cascading failure poses a risk to energy storage systems, electric vehicles, and first responders.

The current approach is to test our way into safety.

- Large system (>1MWh) testing is difficult and costly.

We supplement testing with **predictions** of challenging scenarios and optimization of mitigation.

A key to designing safe systems at larger scales is understanding cascading thermal runaway.



Source: (top) <https://cmte.ieee.org/pes-essb/wp-content/uploads/sites/43/2019/06/2019-SM-UL-9540A-IEC-Lithium-Test-Summary.pdf>
(bottom) <https://www.ul.com/news/ul-9540a-battery-energy-storage-system-ess-test-method>

Cascading failure testing with passive mitigation



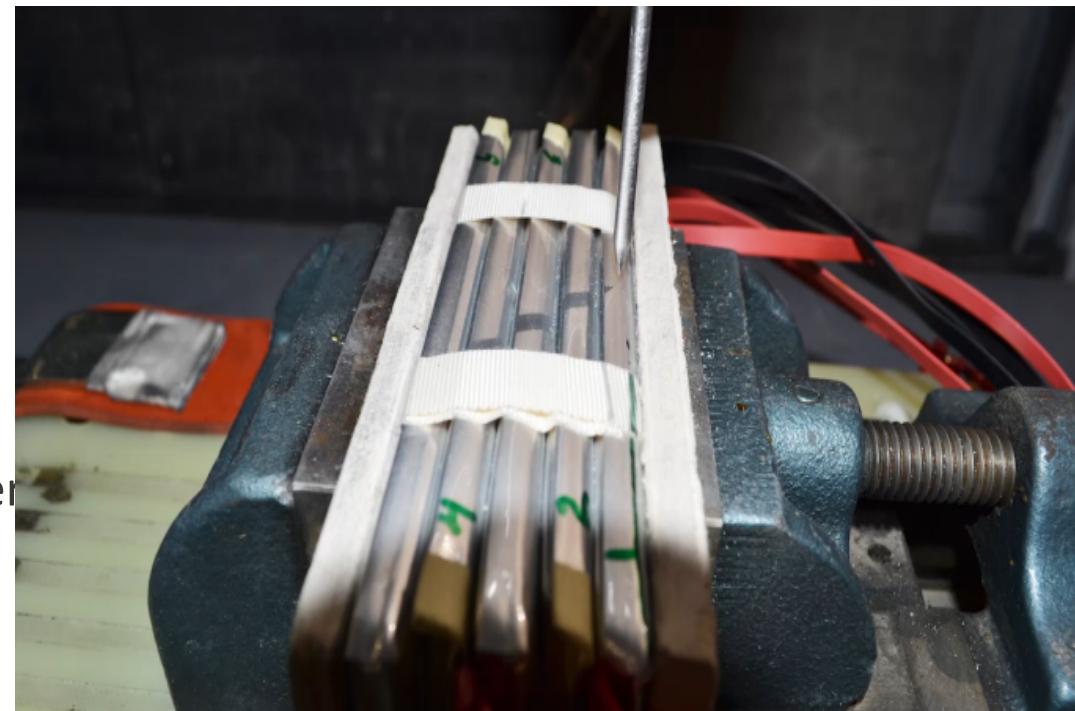
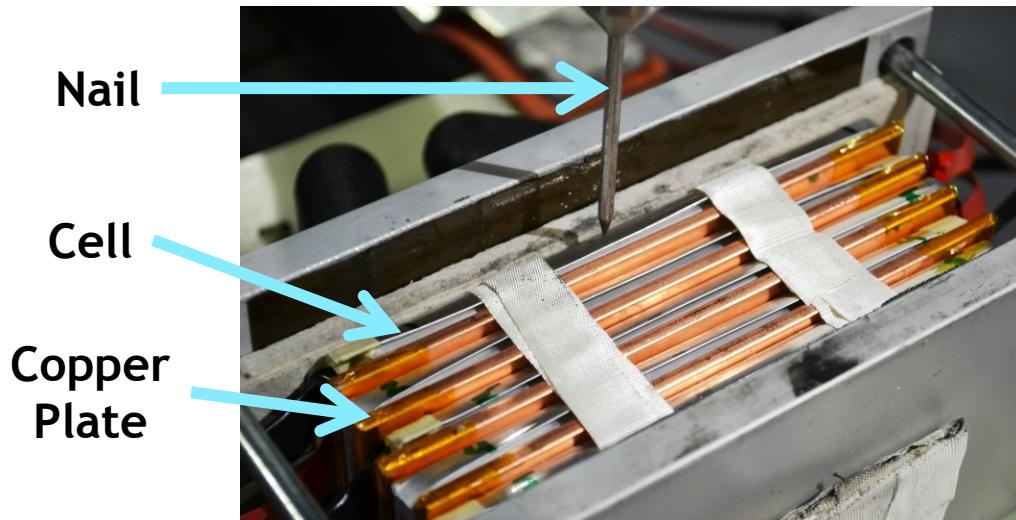
LiCoO₂ 3Ah pouch cells

5 closely packed cells with/without aluminum or copper spacer plates

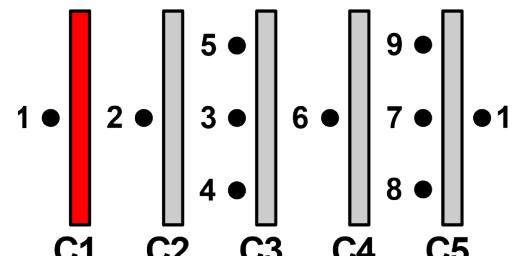
- Spacer thicknesses between 0.8 mm and 3.2 mm
- State of charge (SOC) between 50% and 100%

Failure initiated by a mechanical nail penetration in the outer cell (cell 1)

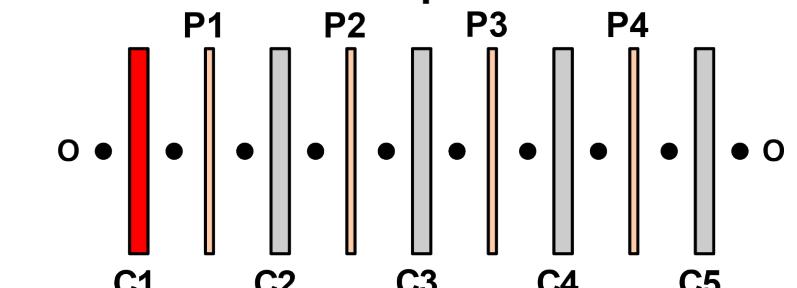
Thermocouples (TC) between cells and spacers (if present)



**Thermocouple Locations
without spacers**



**Thermocouple Locations
with spacers**



Finite element model for Li-ion cells in thermal runaway



Model: SIERRA/Aria

Discretization in one direction (x)

Modeled as a quasi 1-D domain of thin hexahedron elements

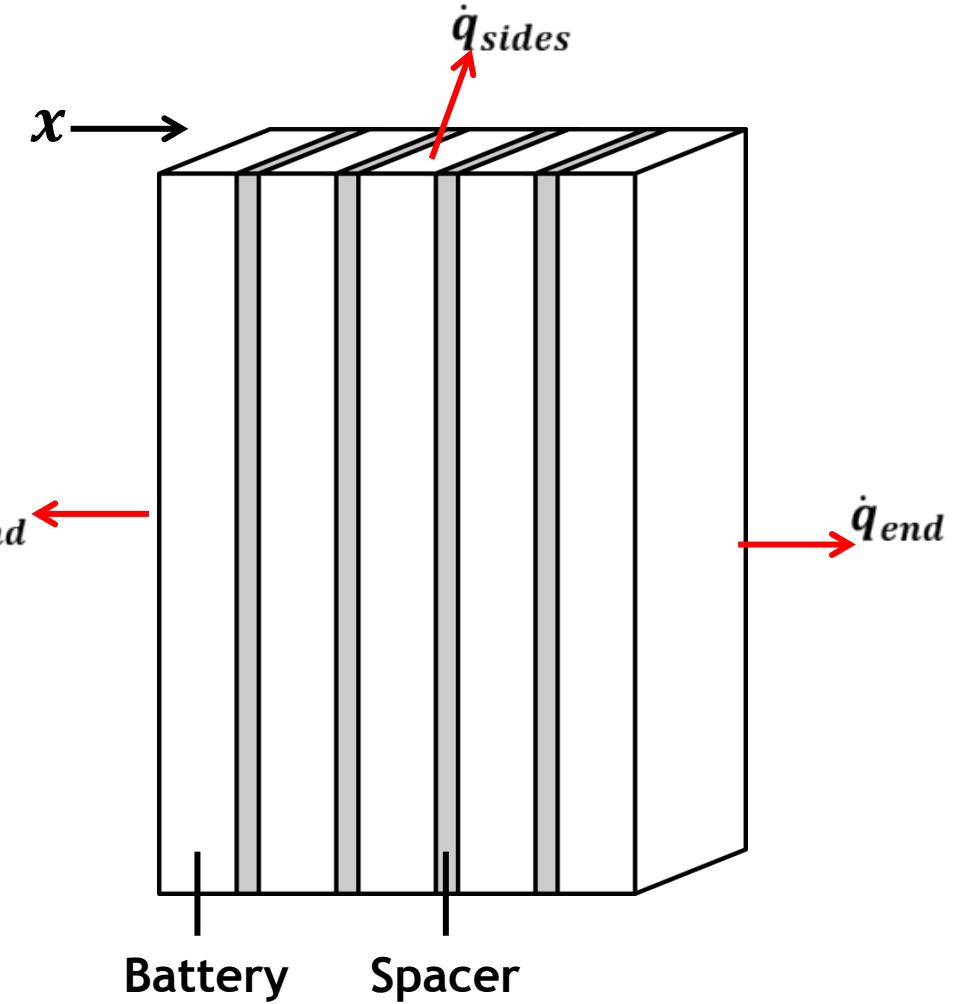
- $k_x \ll k_{yz}$

Multi-layered system

- Lumped battery material
- Spacers
- End block insulators

Convective heat transfer to surroundings
(scaled by surface area to volume ratio for thin domain)

Heat conduction with chemical sources inside
battery material



Finite element model equations



Energy conservation:

$$\rho c_p \frac{\partial T}{\partial t} = \nabla \cdot (K \nabla T) + \dot{q}'''$$

Mass conservation for species i with N_r reactions:

$$\frac{\partial \rho_i}{\partial t} = \sum_{j=1}^{N_r} (\nu_{ij}'' - \nu_{ij}') r_j$$

Energy source:

$$\dot{q}''' = - \sum_{j=1}^{N_r} \Delta H_j r_j$$

Chemical source terms for thermal runaway



Li-ion batteries contain a metal and oxidizer that can react with each other or alkyl carbonate electrolyte to release energy

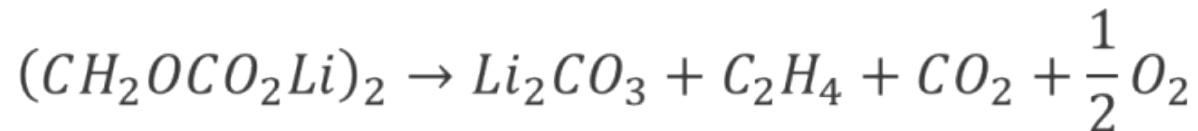
These reactions occur at sub-grid scales and can be approximated as pre-mixed

Empirical chemical reactions:

- Short-circuit



- SEI decomposition (Richard 1999)



- Anode-electrolyte (Shurtz 2018)



- Cathode-electrolyte (Hatchard 2001, Shurtz 2020)

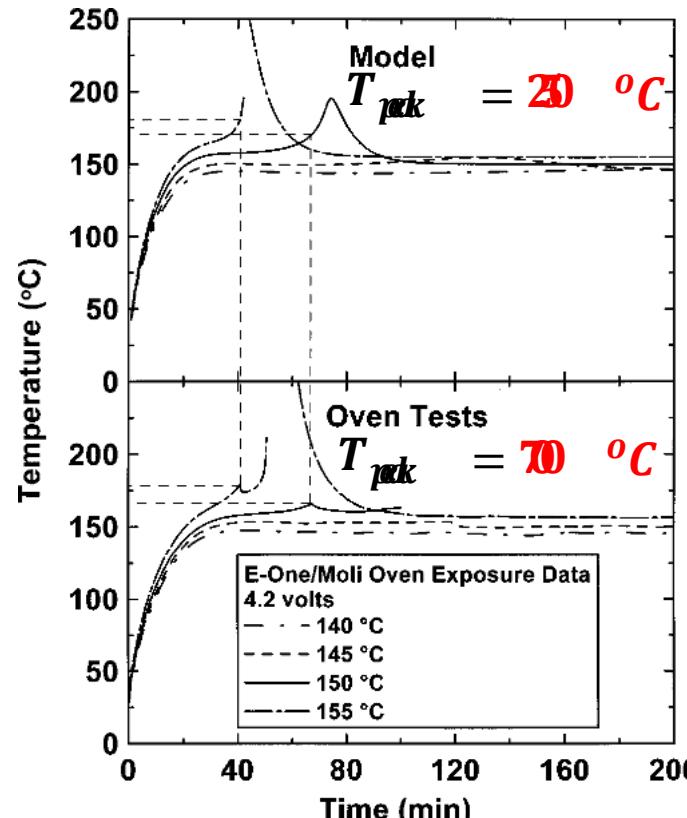


Chemical source terms for thermal runaway



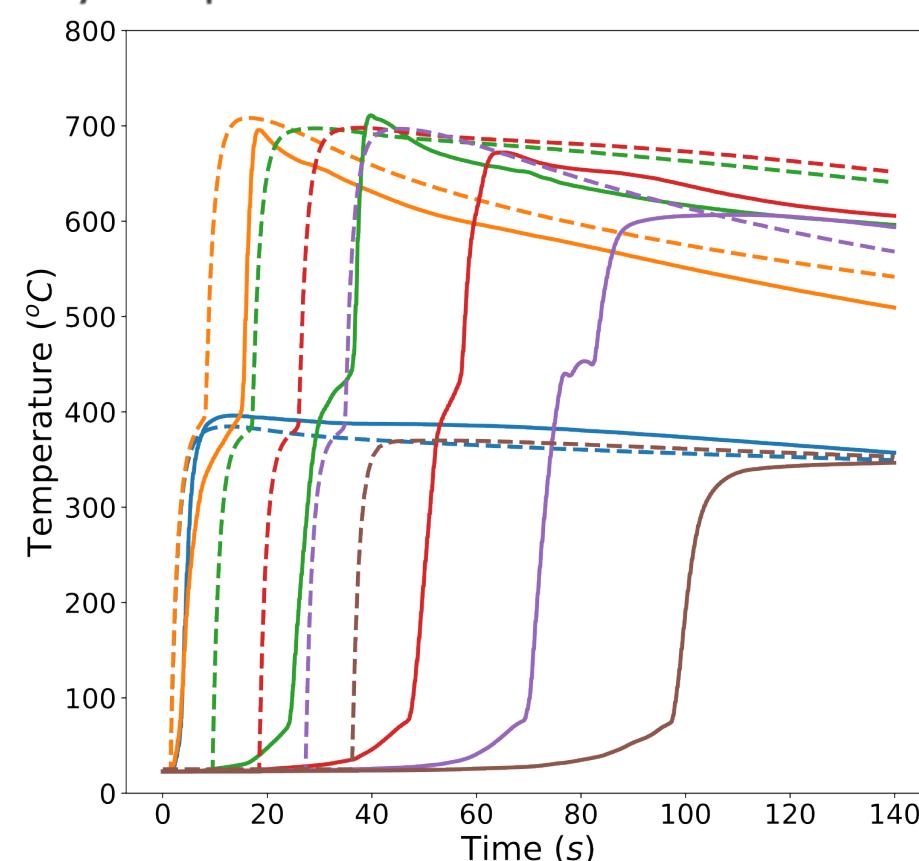
Preliminary chemistry models from literature

- Based on Dahn group (1999-2001)
- Calibrated for onset, but under-predicts peak temperature due to incomplete thermodynamics



Extrapolating literature models to cell-scale with updated thermodynamics

- Reaction rates at propagation temperature ($\sim 700^\circ\text{C}$) are over-predicted
- Velocity of a premixed flame: $v \approx \sqrt{\dot{\omega}\alpha}$



Species transport in electrode particles



Thermal runaway is analogous to very fast degradation

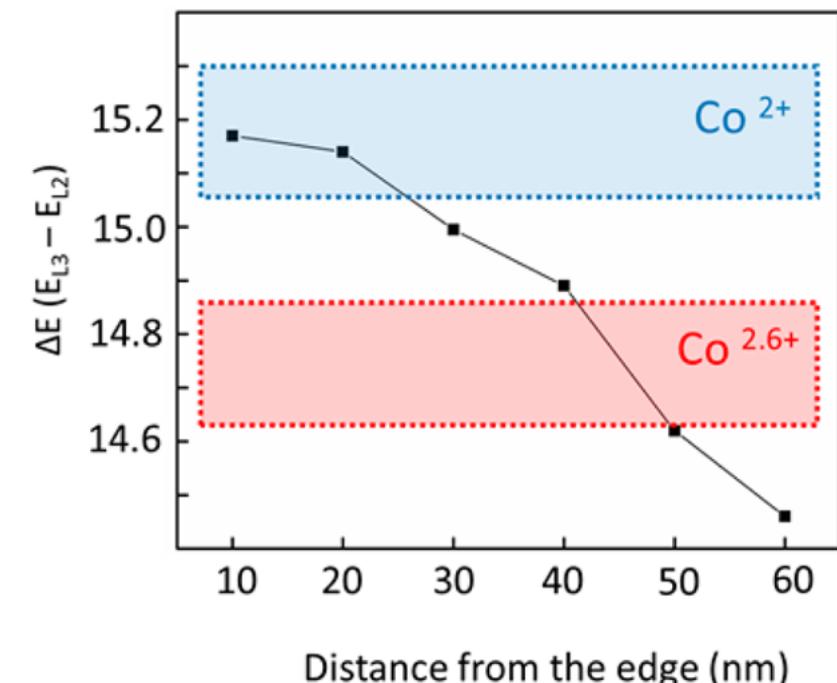
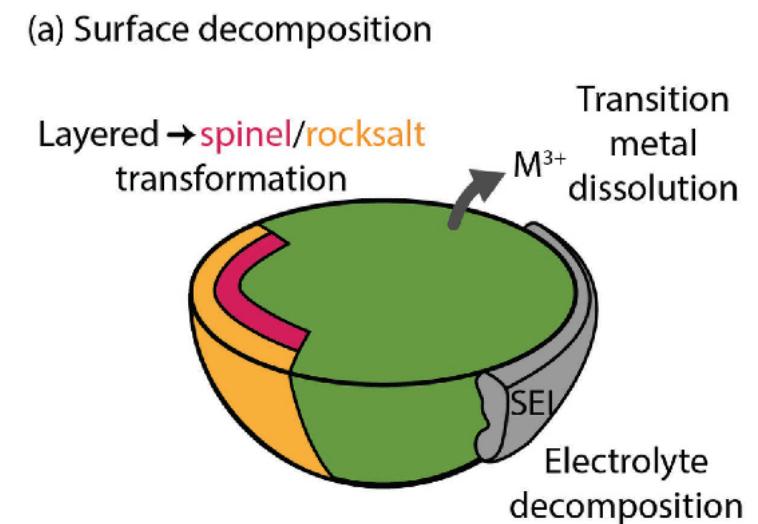
Radin et al. describe three cathode degradation methods that affect transport of Li and O₂ transport

- Surface decomposition, bulk transformations to spinel, mechanical degradation

Sharifi-Asl et al. observed oxygen release occurs at the surface of cathodes where spinel (M₃O₄) and rock salt (MO) begin formation.

The phases grow from the surface towards the core of the particles, leaving O₂ behind to diffuse to the surface.

Similarly in the anode, Li must diffuse through the graphite particle to react with electrolyte at the exposed surface.



Figures:

(top) Radin et al. (2017). *Advanced Energy Materials*, 7, 1602888

(bottom) Sharifi-Asl et al. (2017). *Nano Letters*, 17, 2165-2171.

Model for solid-state particle diffusion limit



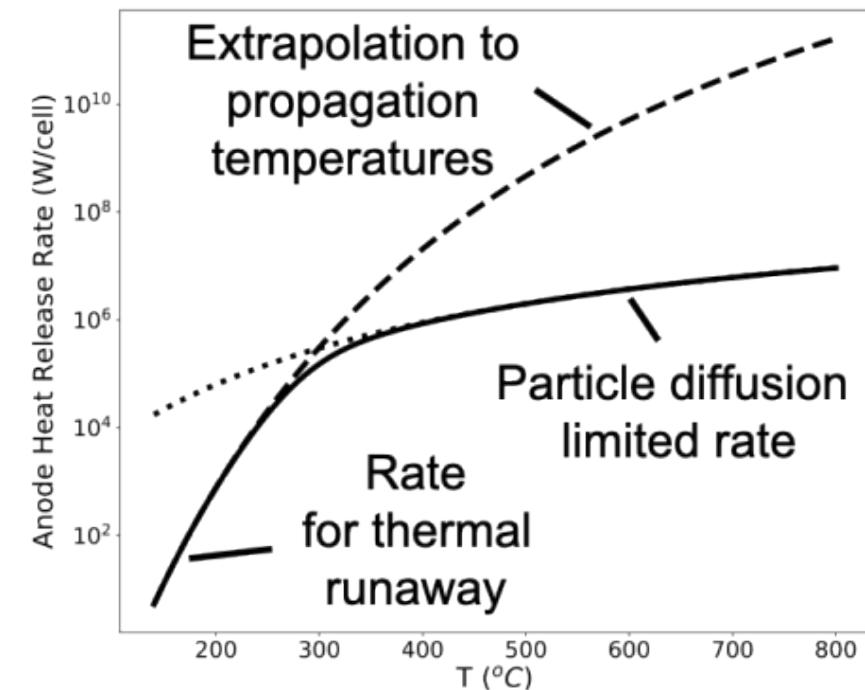
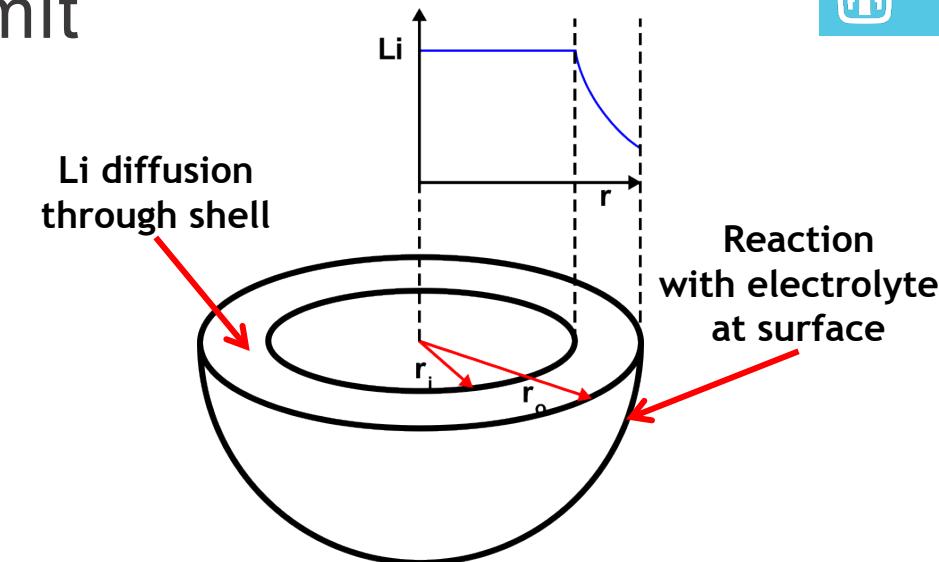
Challenge: Calorimetry measurements only at lower temperatures

- Lithium and oxygen must diffuse to the particle surface to react with the electrolyte.
- Serial reactions are corrected with the “Damköhler limited” form.

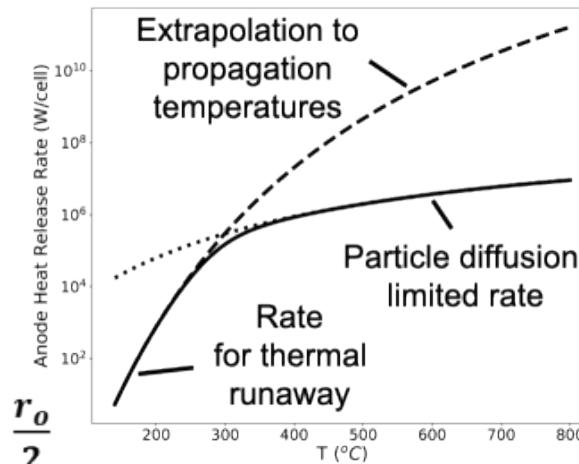
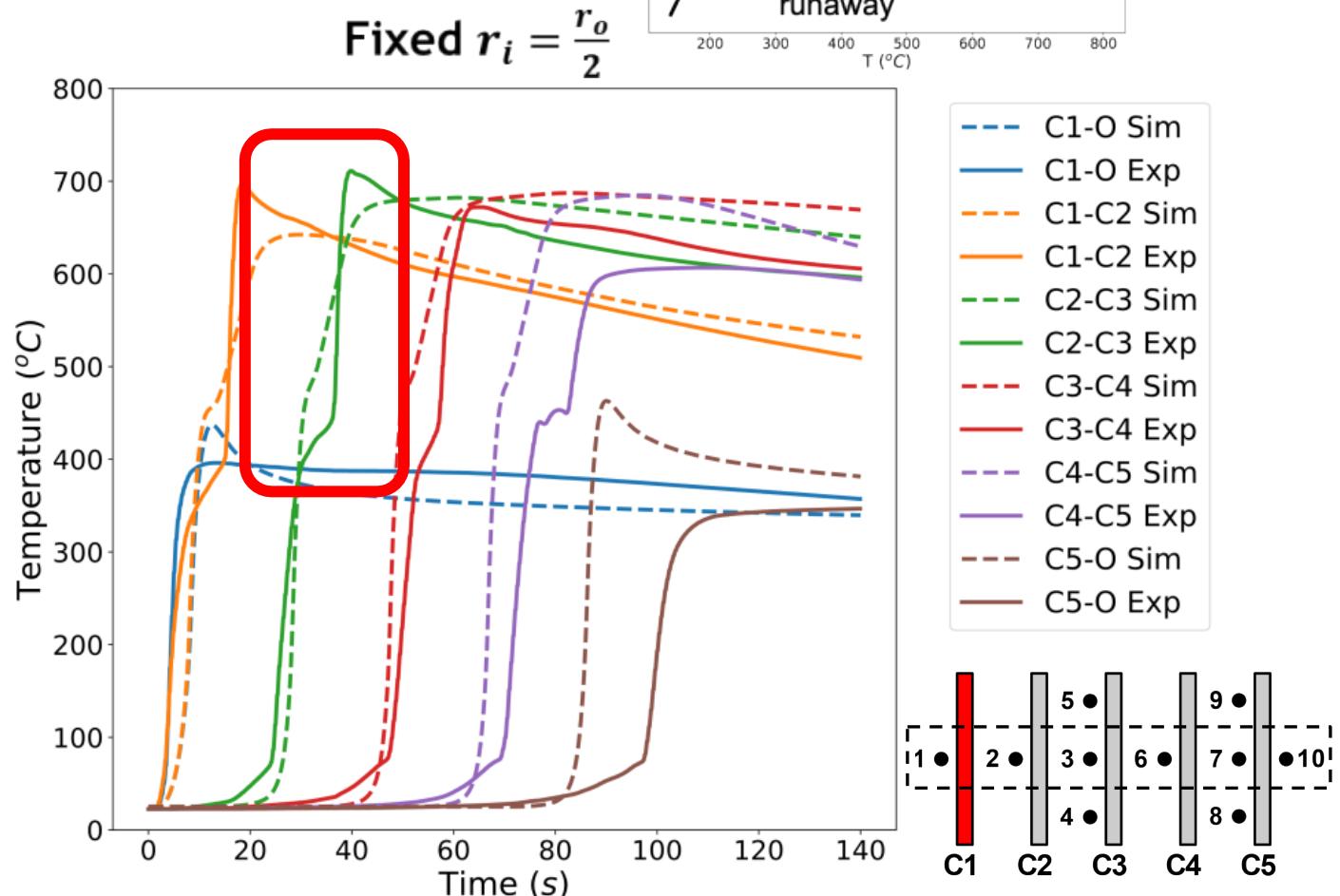
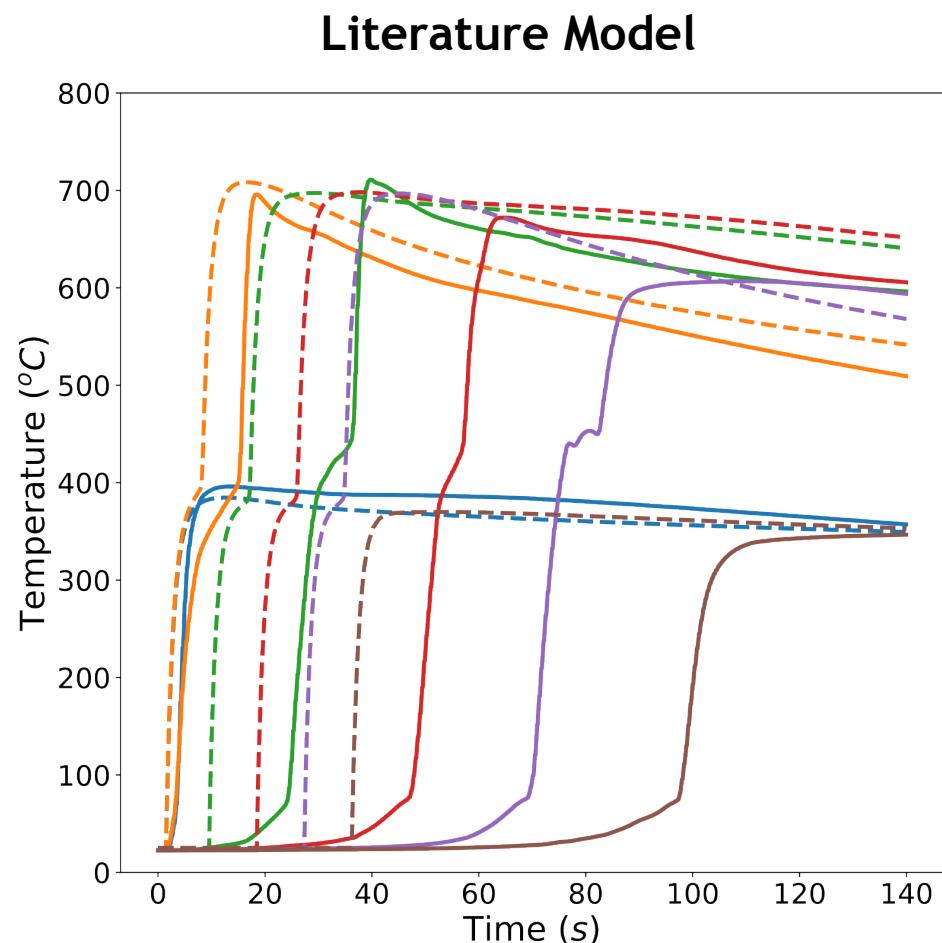
$$k' = \frac{k}{1 + Da}$$

- The Damköhler number is ratio of surface reaction rate to the rate of diffusion between an inner radius (r_i) and outer radius (r_o).

$$Da = \frac{A \exp\left(-\frac{E}{RT}\right)}{a_e \rho D_o \exp\left(-\frac{E_D}{RT}\right)} \frac{(r_o - r_i)r_o}{r_i}$$



Five cell stack results: 100% SOC



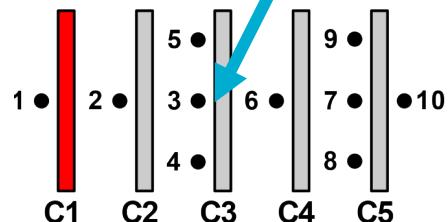
Model for solid-state particle diffusion limit



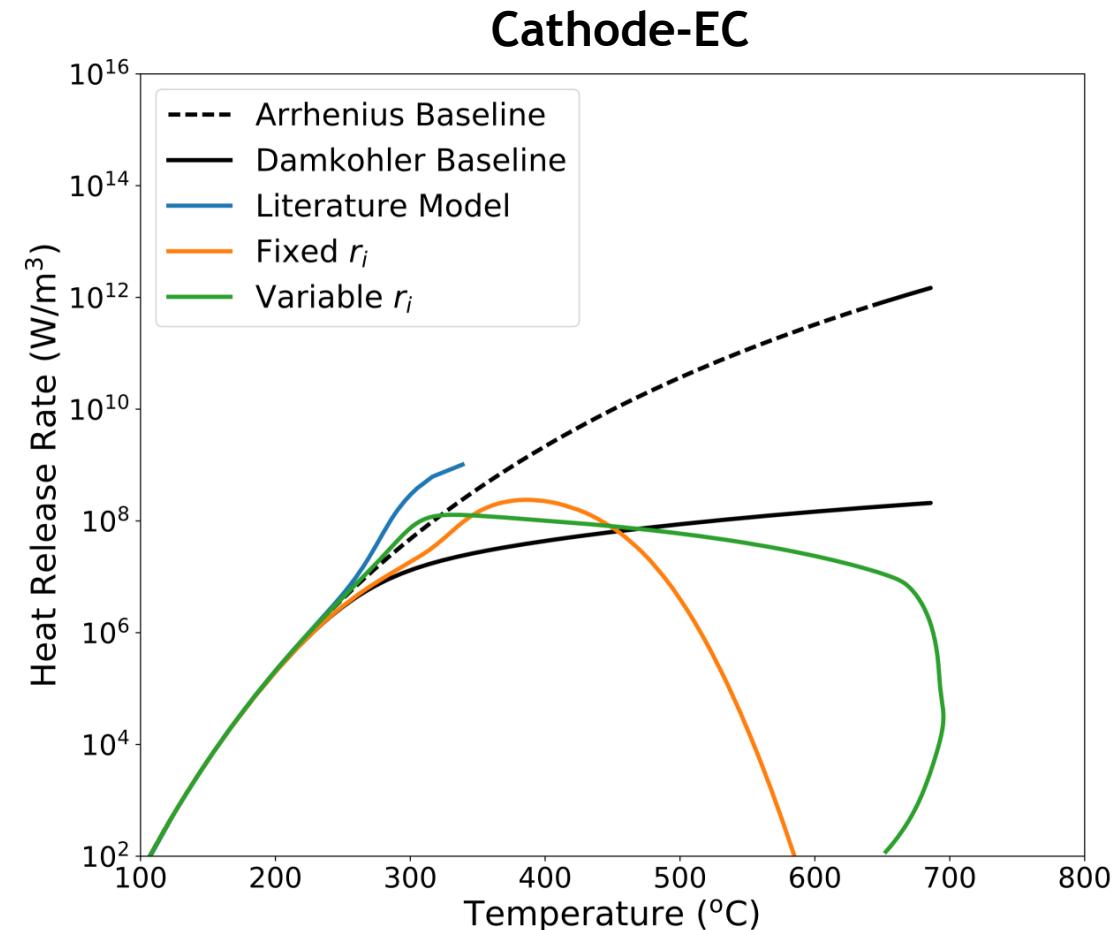
The inner radius as a function of species concentration (ρ_s).

$$\frac{r_i}{r_o} = \left(\frac{\rho_s}{\rho_{s,o}} \right)^{1/3}$$

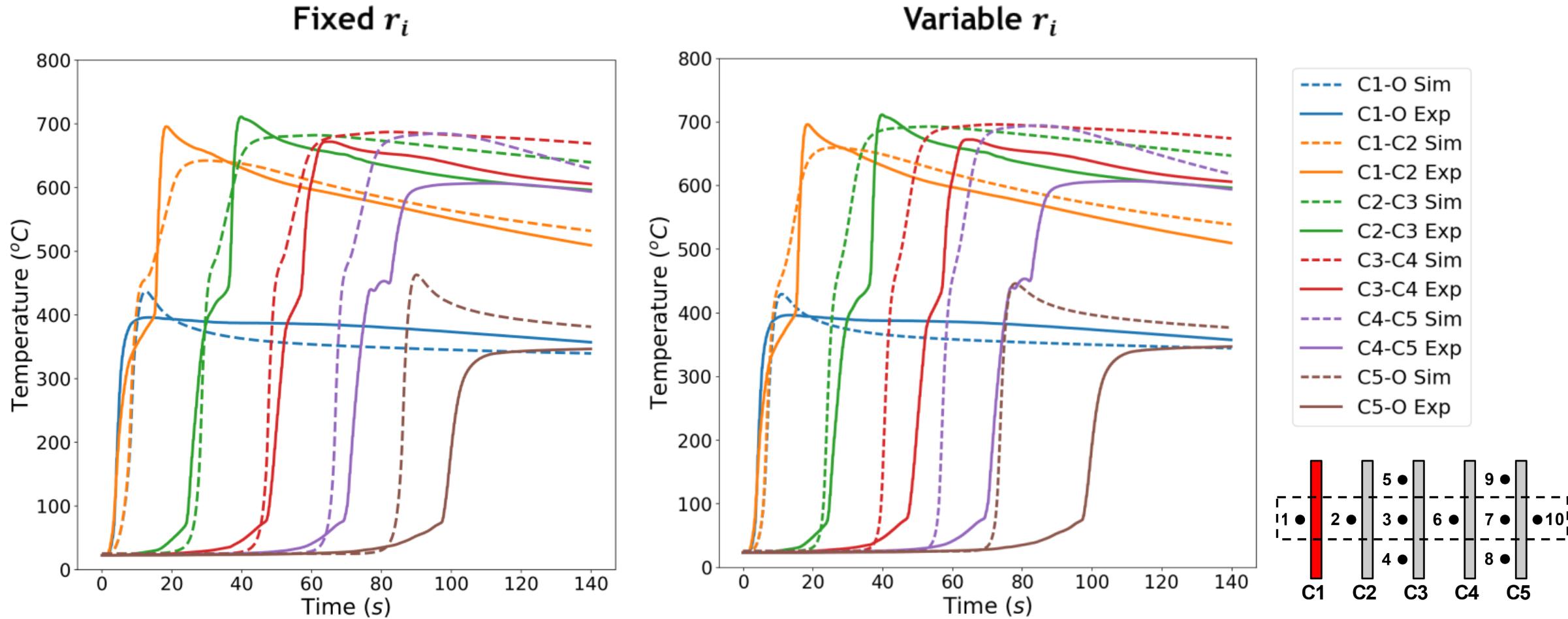
Ex: heat release rate shown at the edge of Cell 3 closest to Cell 2.



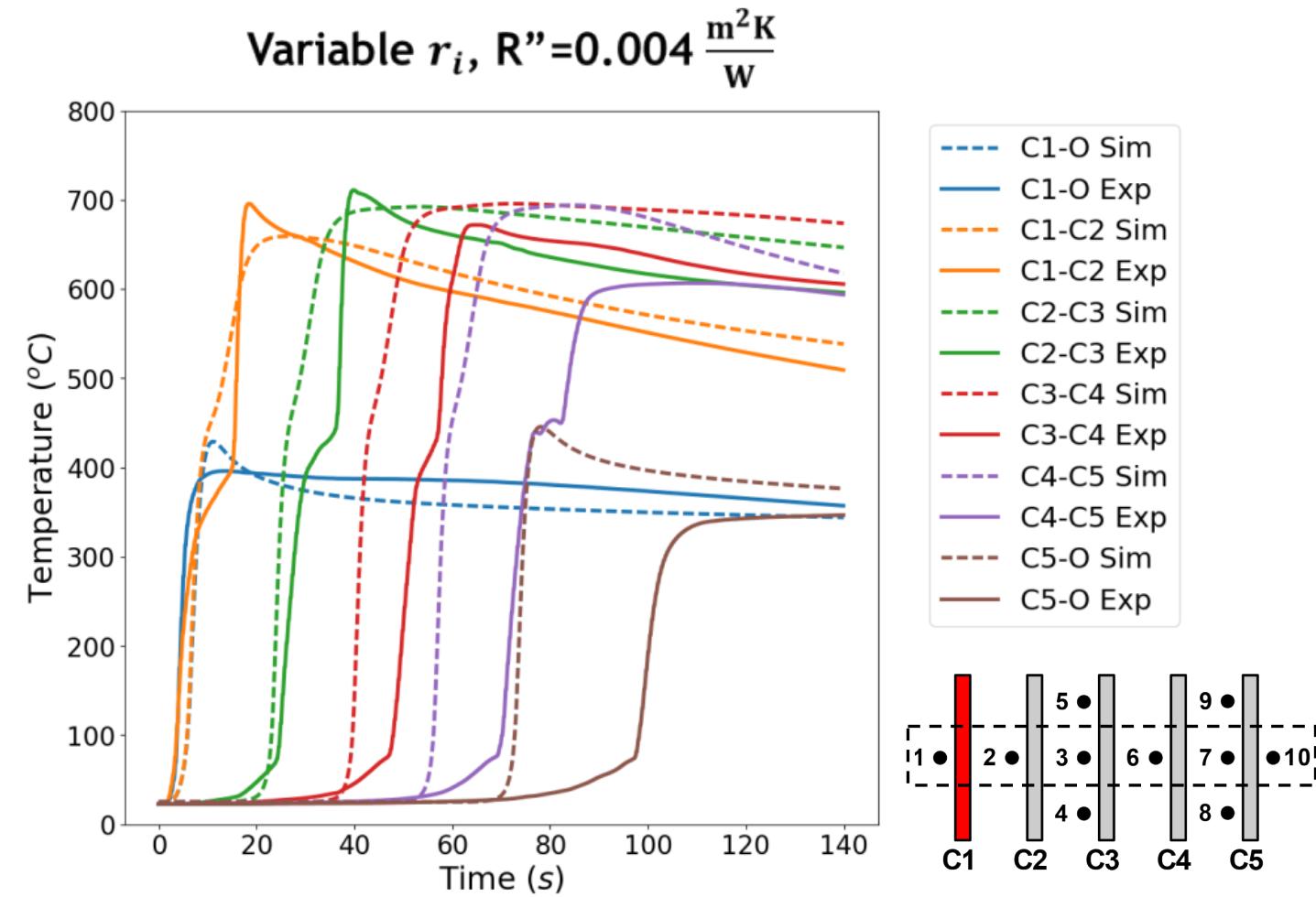
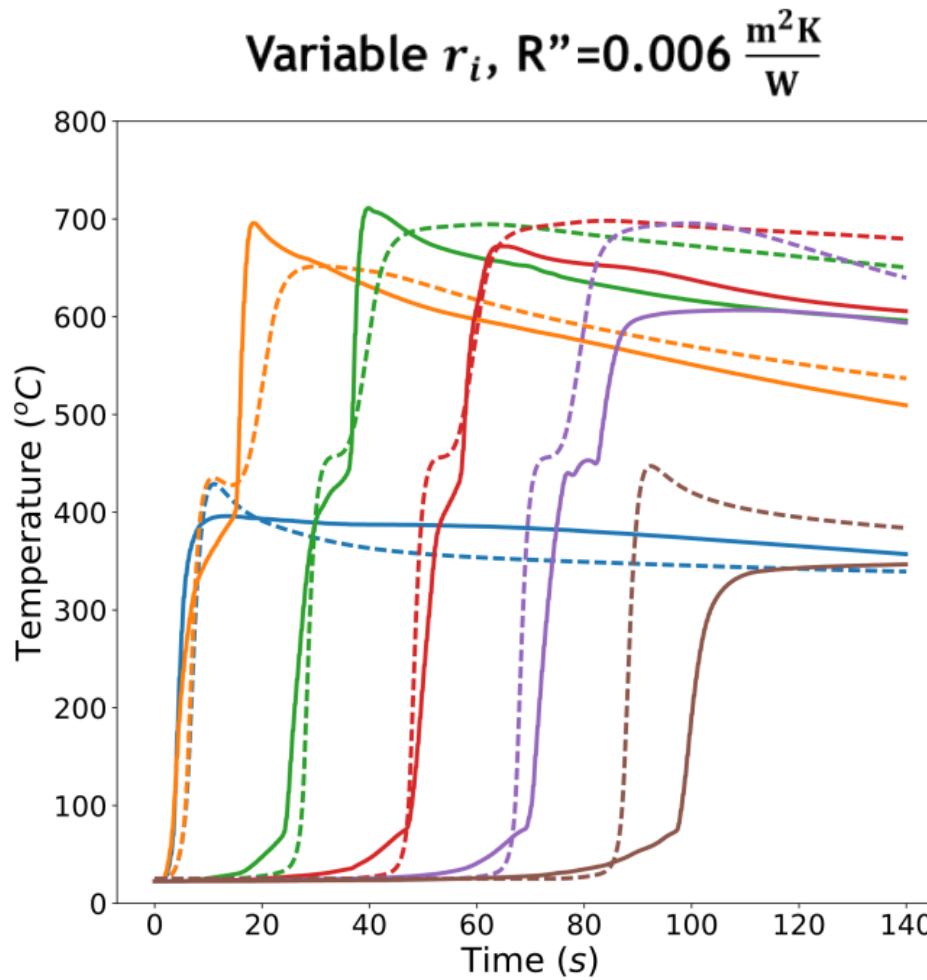
- Baseline rates exclude concentration dependence.
- Literature models propagate too fast.
- Fixed $r_i = 0.5r_o$ resulted in good bulk propagation predictions, but the initial rate is slow relative to experiments.
- Variable r_i model include concentration dependence for anode and cathode particles, r_o values from Guo 2002.



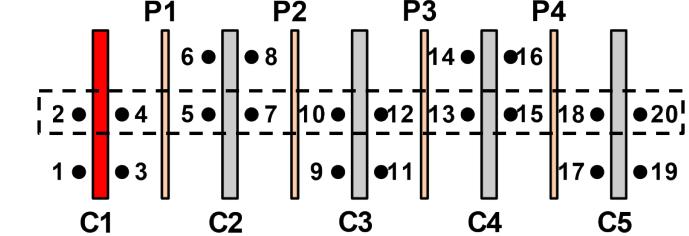
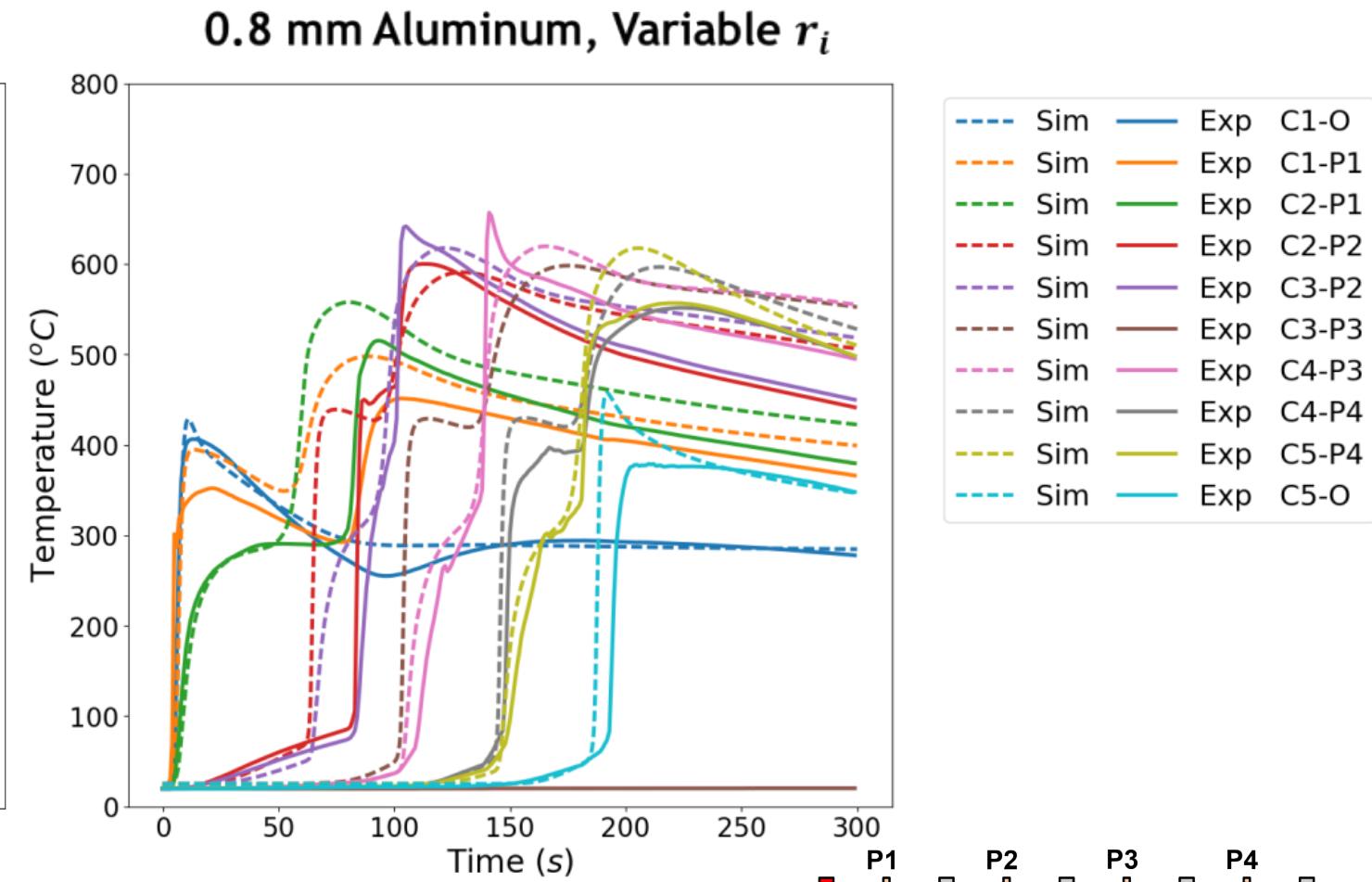
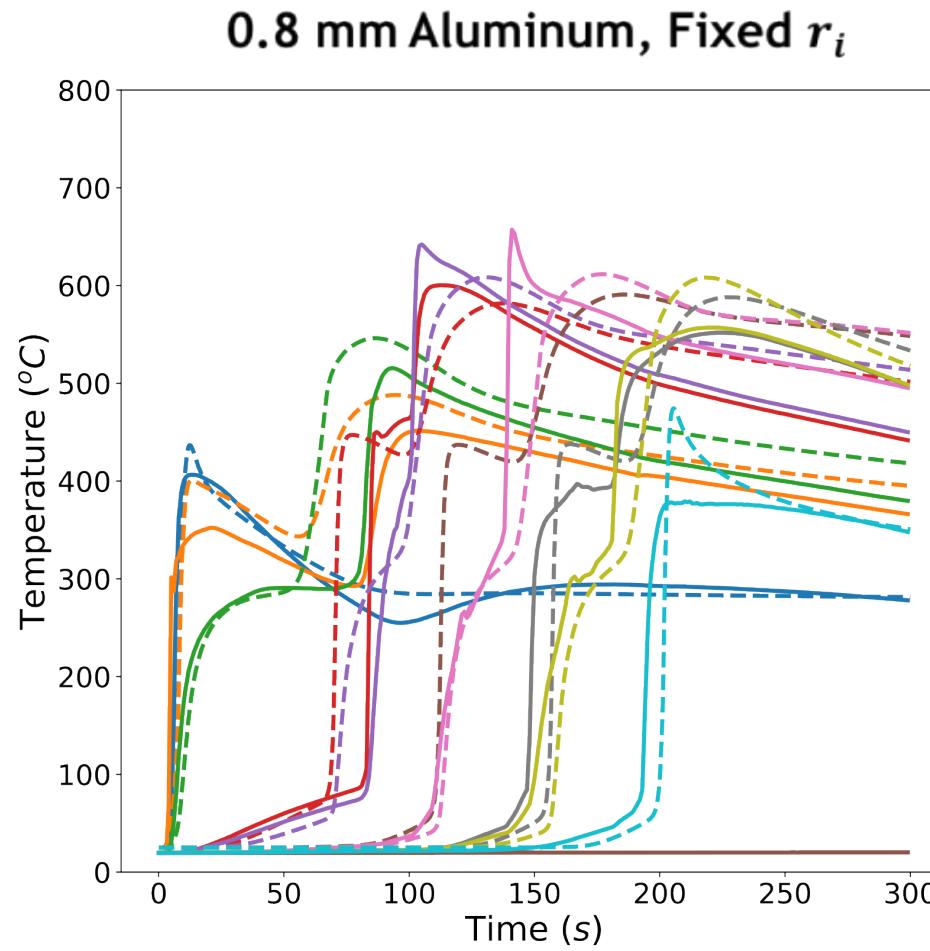
Five cell stack results: 100% SOC, no spacers



Five cell stack results: 100% SOC, no spacers



Results: 100% SOC, metallic spacers



Summary



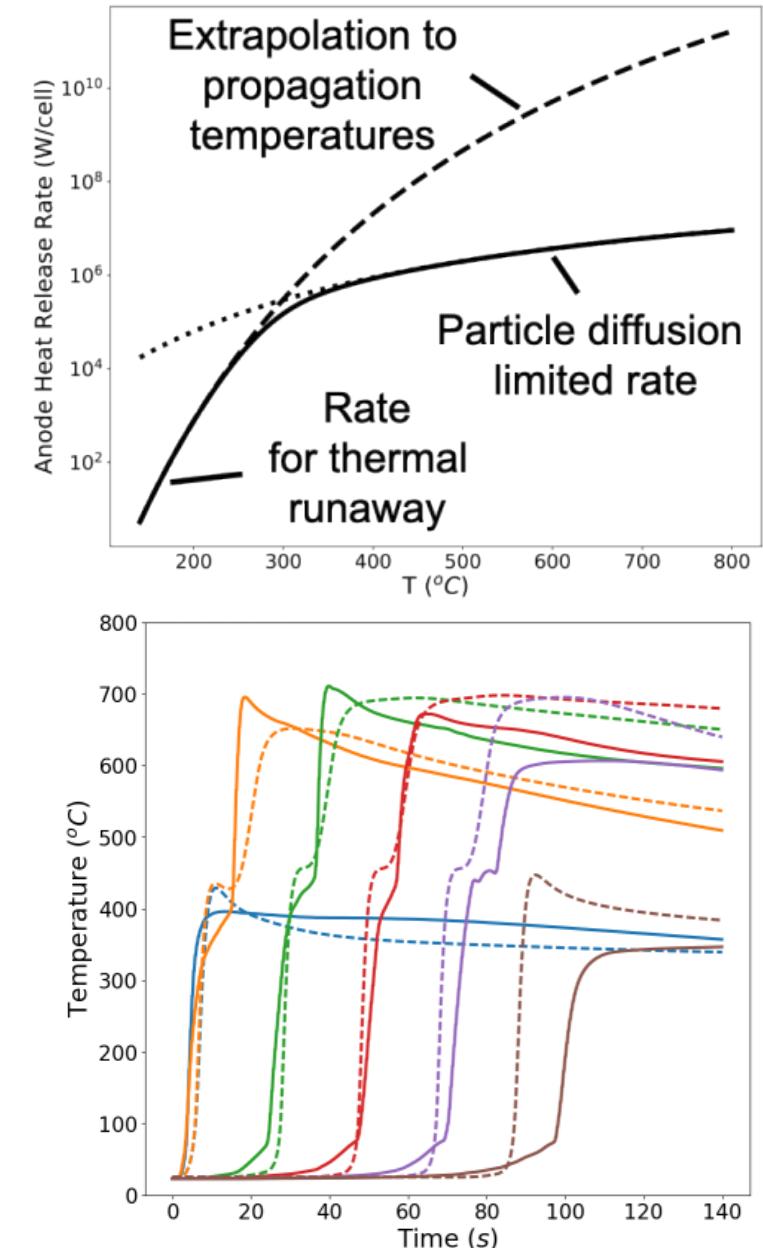
Using legacy chemistry source terms predicts onset of thermal runaway, but extrapolating this to higher temperature over-predicts cell-scale propagation speeds.

Results suggest that inclusion of intra-particle diffusion limits (or a similar change in the kinetics) becomes important for higher temperature cell-scale propagation.

Predictions of fixed and variable internal particle radius formulations were tested on a range of conditions with variable state-of-charge and passive mitigation spacers.

These results represent an extension of prediction capabilities to predict propagation and its limits over a range of thermal “dilution” conditions.

Understanding mitigation boundaries is important for designing safe energy storage systems.



Acknowledgements



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