

Chemical gradients to control stability and mechanical behavior in nanostructured Pt-Au

PRESENTED BY

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Abdeljawad

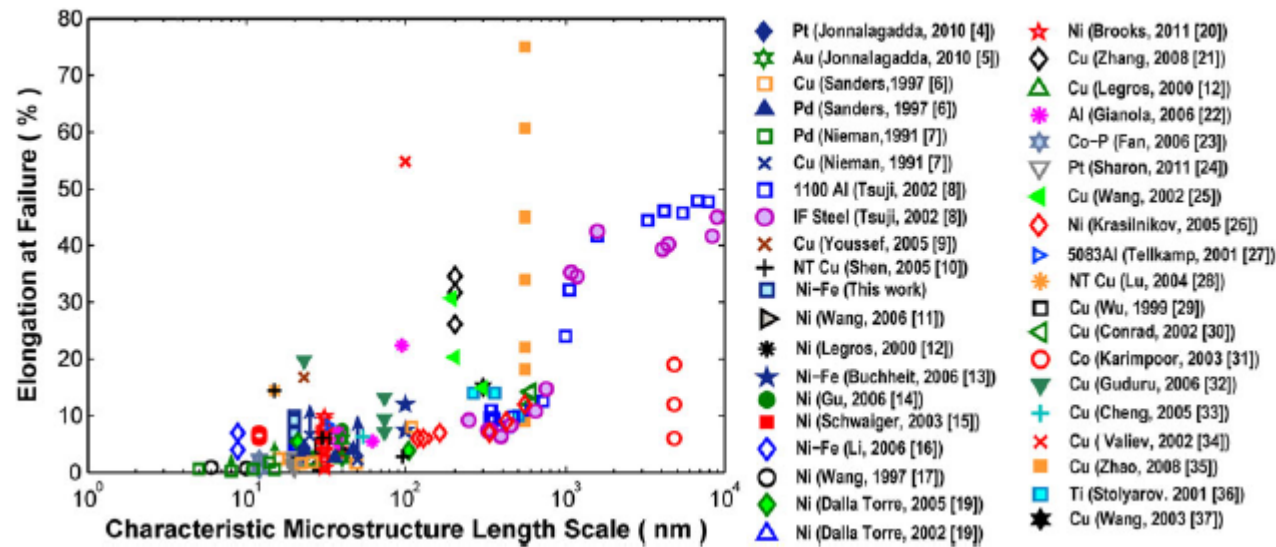


This work was performed, in part, at the Center for Integrated Nanotechnologies, an Office of Science User Facility operated for the U.S. Department of Energy (DOE) Office of Science. Sandia National Laboratories is a multimission laboratory managed and operated by National Technology & Engineering Solutions of Sandia, LLC, a wholly owned subsidiary of Honeywell International Inc., for the U.S. DOE's National Nuclear Security Administration under contract DE-NA-0003525. The views expressed in the article do not necessarily represent the views of the U.S. DOE or the United States Government.



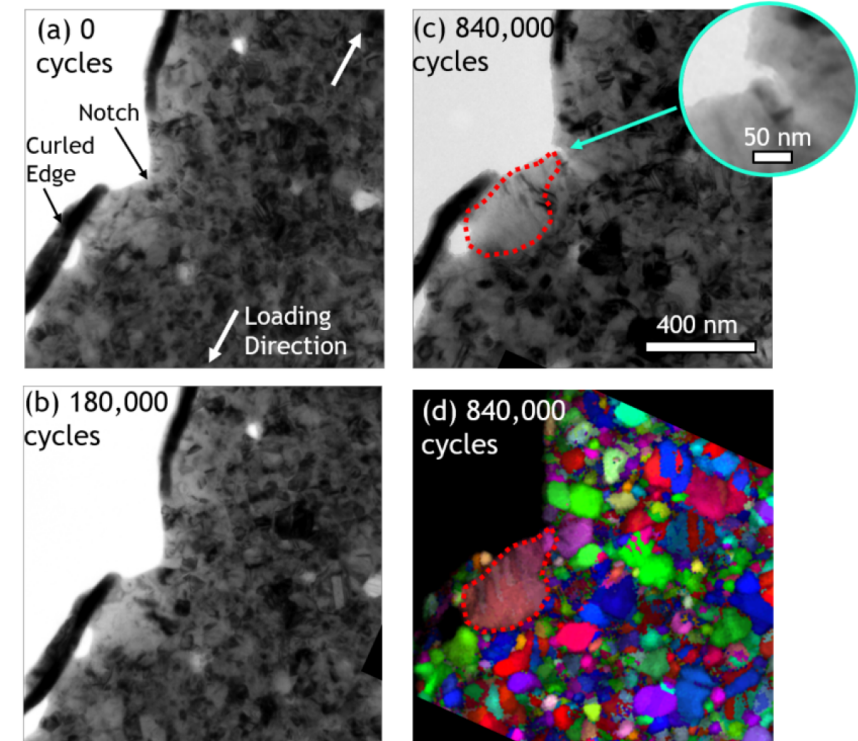
The limitations of pure nanocrystals

Ductility/toughness



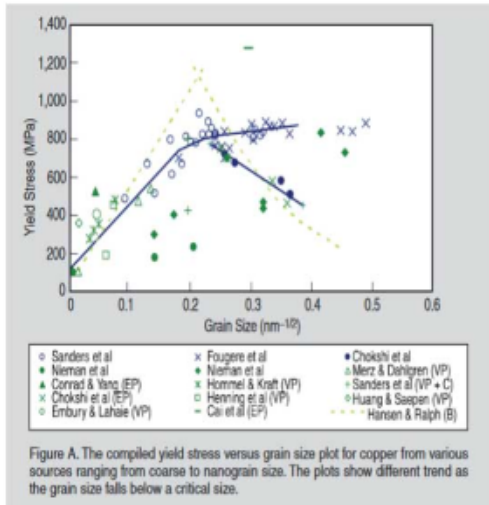
Sharon, Padilla, Boyce, *J. Mater. Res.*, 2013

Stability

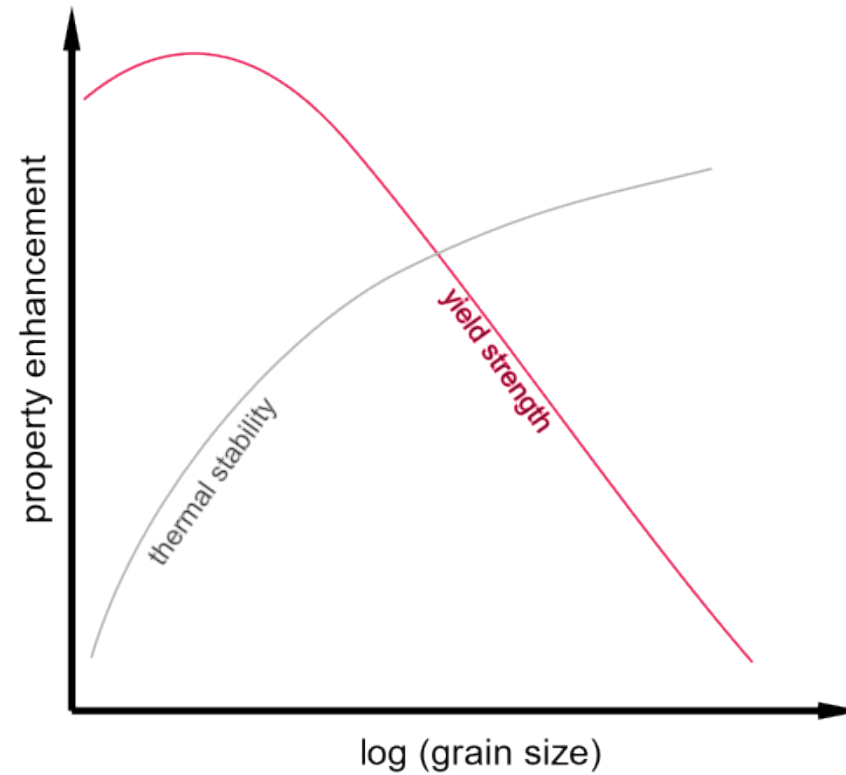


Lu, Pan, Hattar, Boyce, *MRS Bull.*, 2021

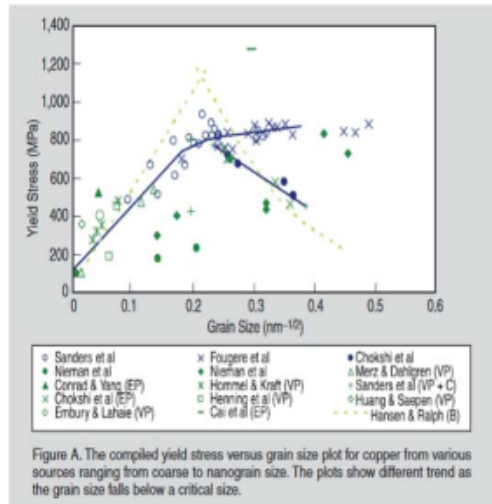
Competing Priorities



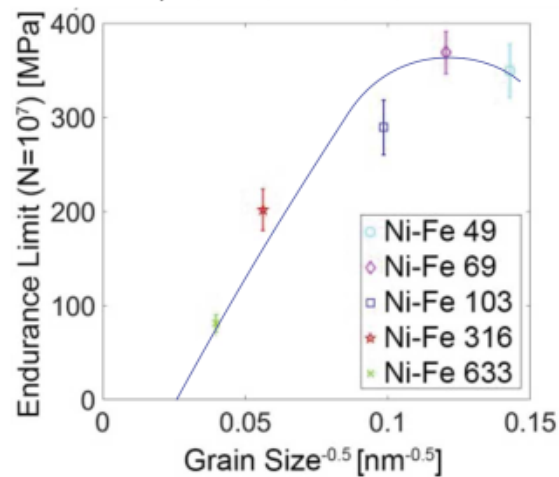
Meyers, Mishra, Benson, JOM, 2006



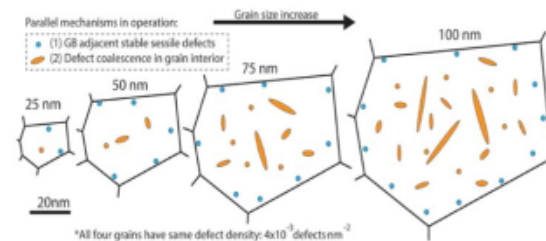
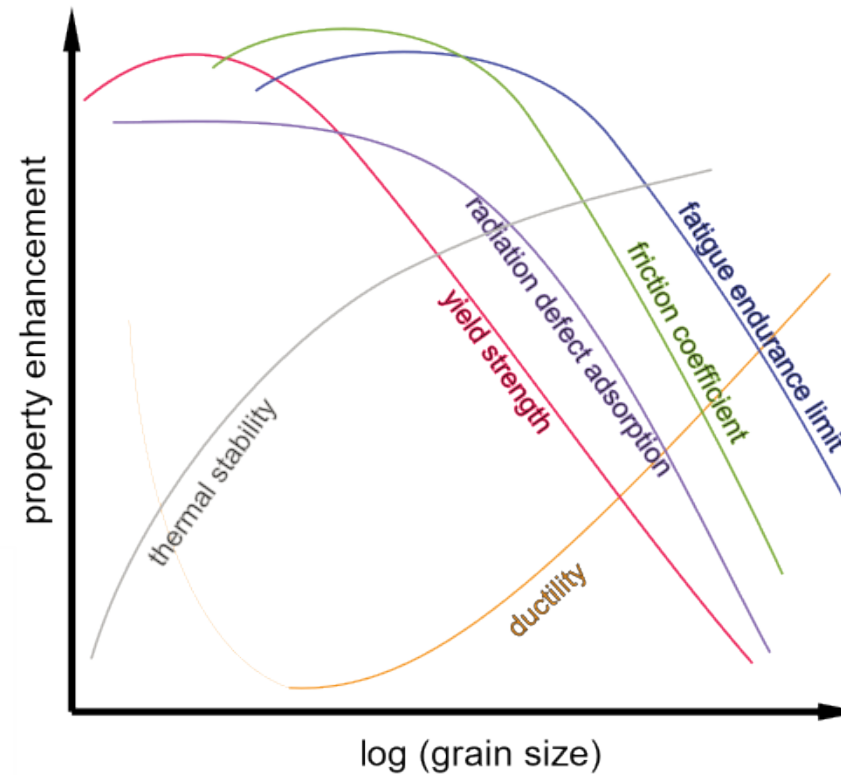
Competing Priorities



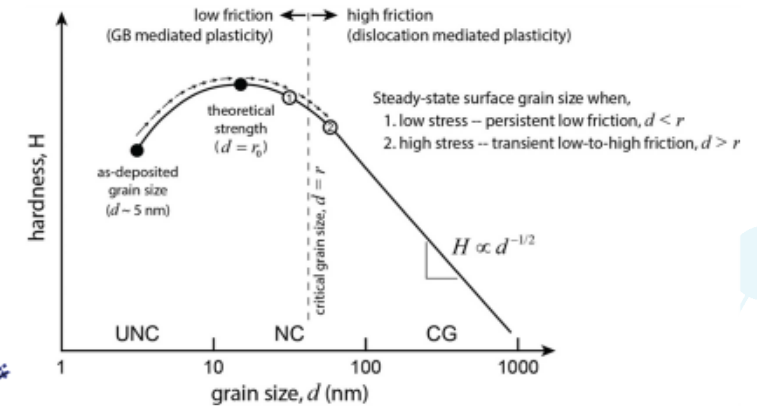
Meyers, Mishra, Benson, JOM, 2006



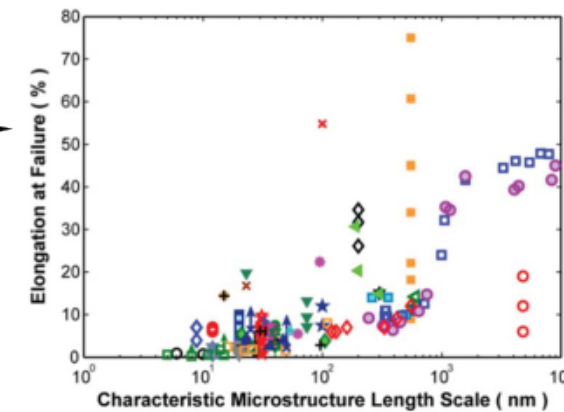
Heckman...Boyce, submitted, 2019



Barr, Li, Boyce, Hattar, Appl. Phys. Lett., 2018

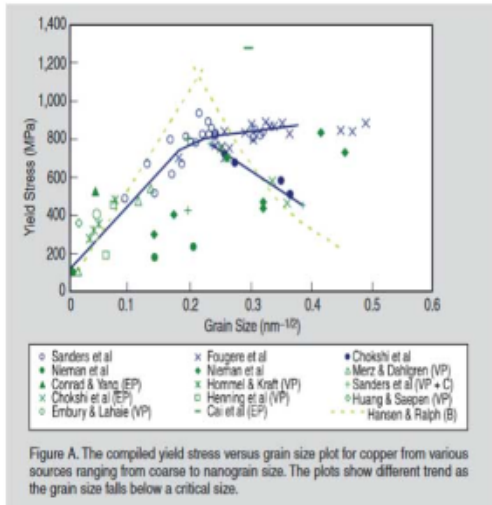


Argibay, Furnish, Clark, Boyce, Chandross, Scripta Mater, 2016

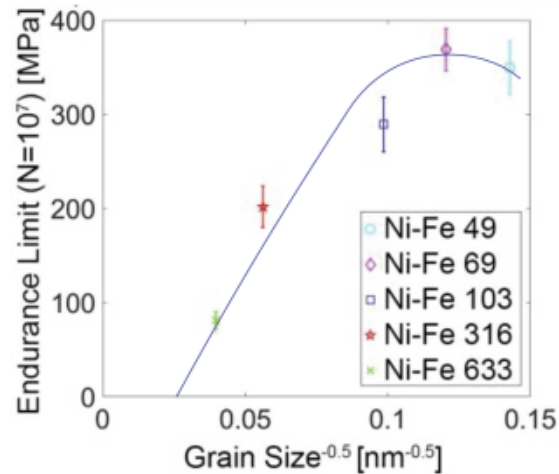


Sharon, Padilla, Boyce, J. Mater. Res., 2013

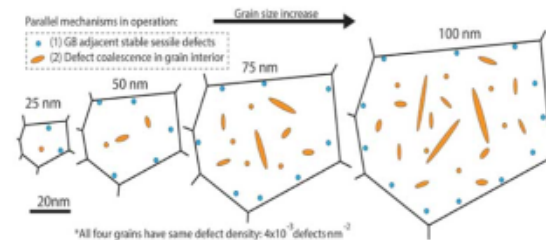
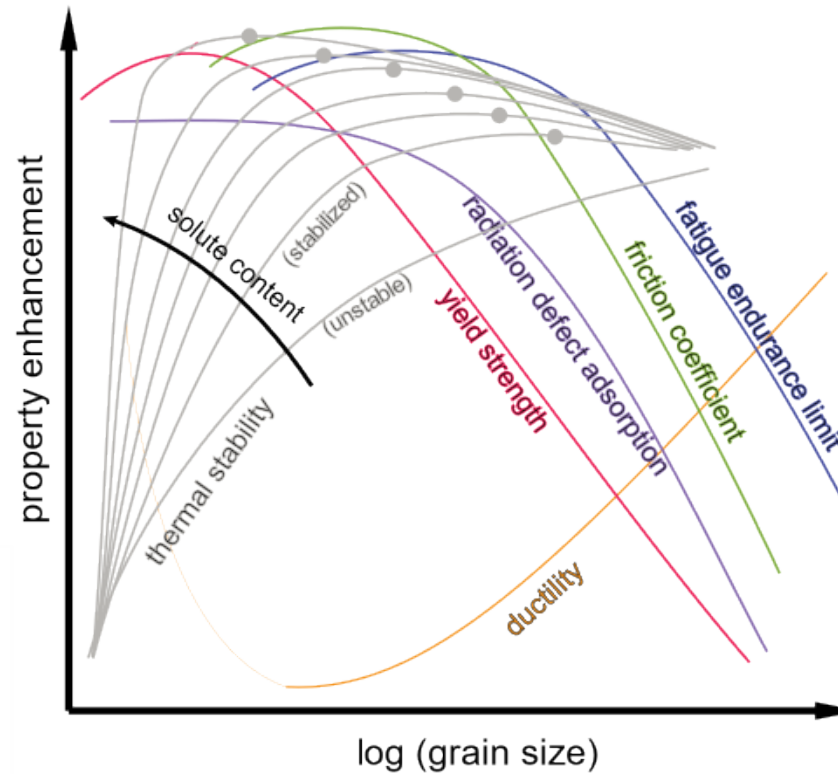
A gradient solute strategy...



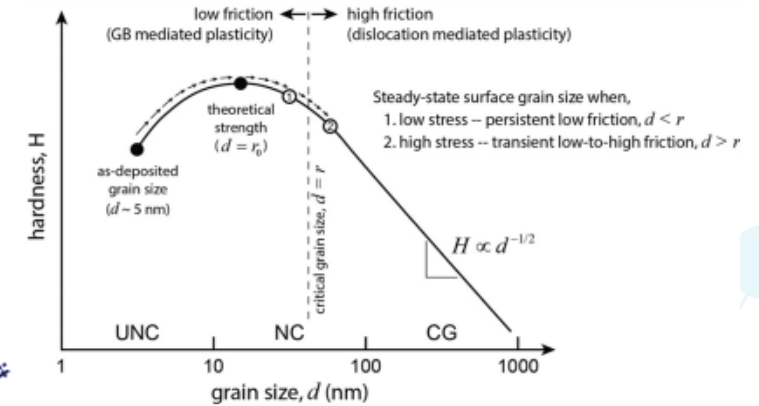
Meyers, Mishra, Benson, JOM, 2006



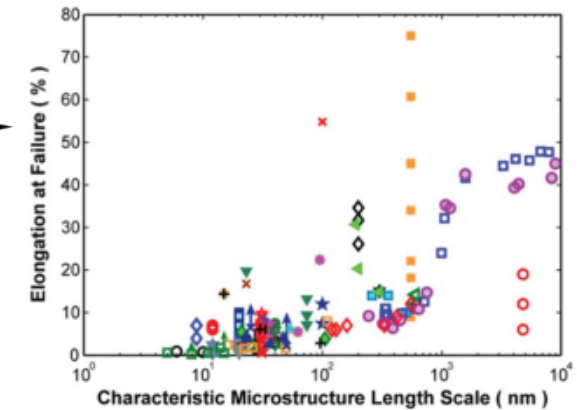
Heckman...Boyce, submitted, 2019



Barr, Li, Boyce, Hattar, Appl. Phys. Lett., 2018

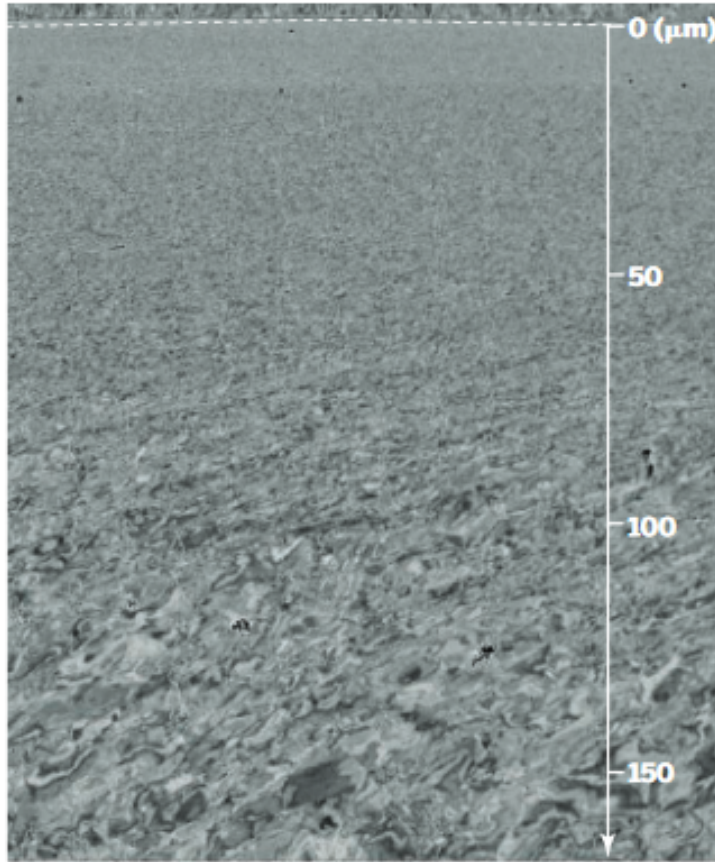


Argibay, Furnish, Clark, Boyce, Chandross, Scripta Mater, 2016

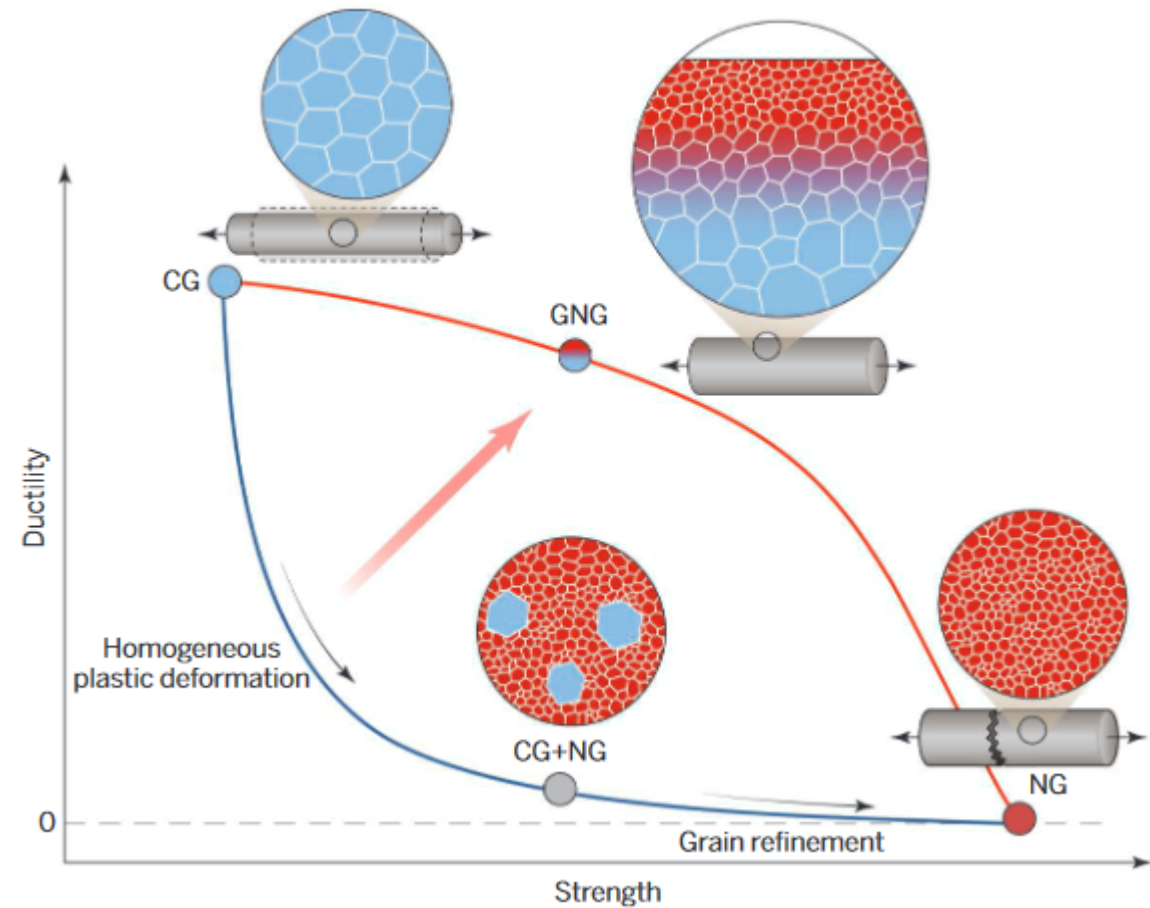


Sharon, Padilla, Boyce, J. Mater. Res., 2013

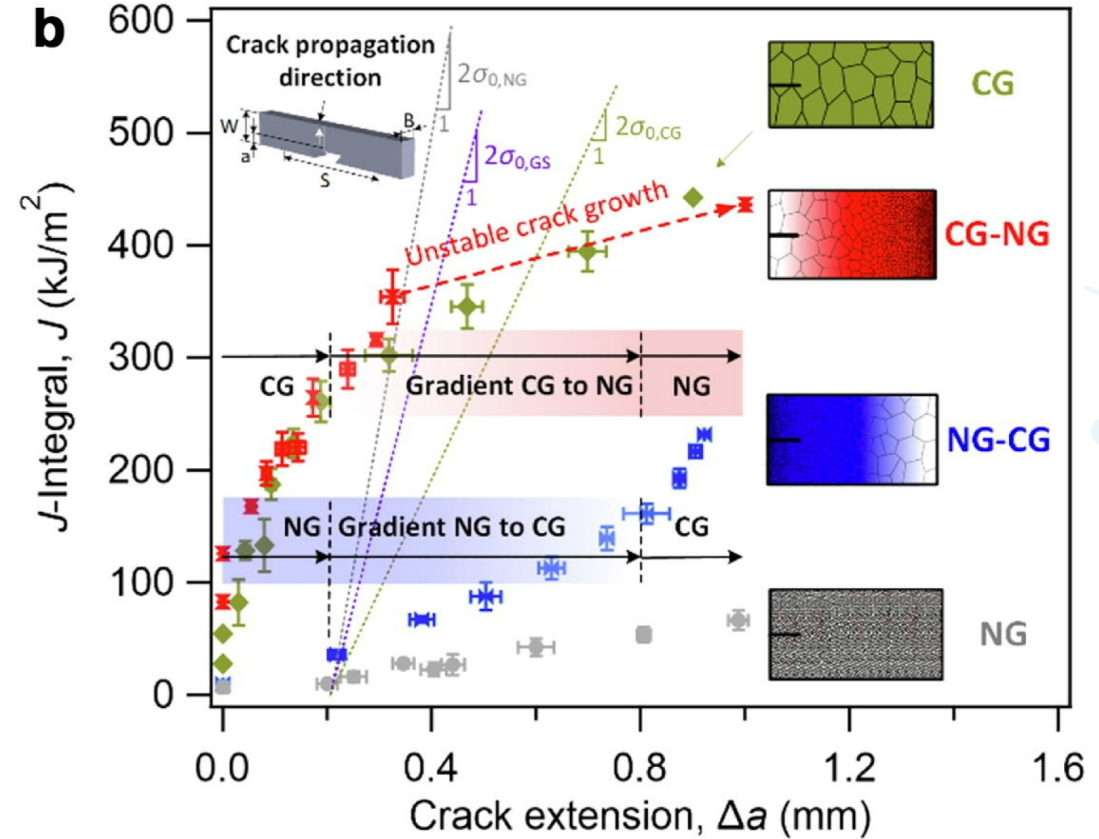
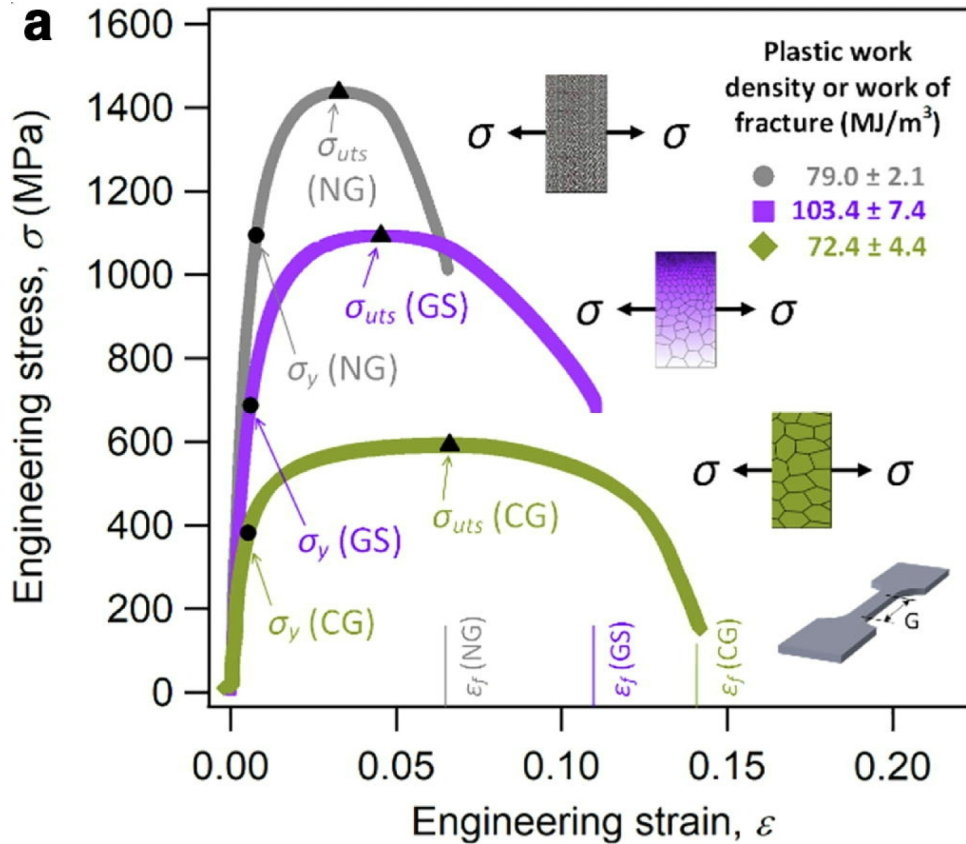
Gradients offer strength/ductility payoff



Gradient nanograined structure. After a surface mechanical grinding treatment to copper, grain sizes are about 20 nm in the topmost treated surface (outlined by dashed line) and increase gradually to the microscale with depth.

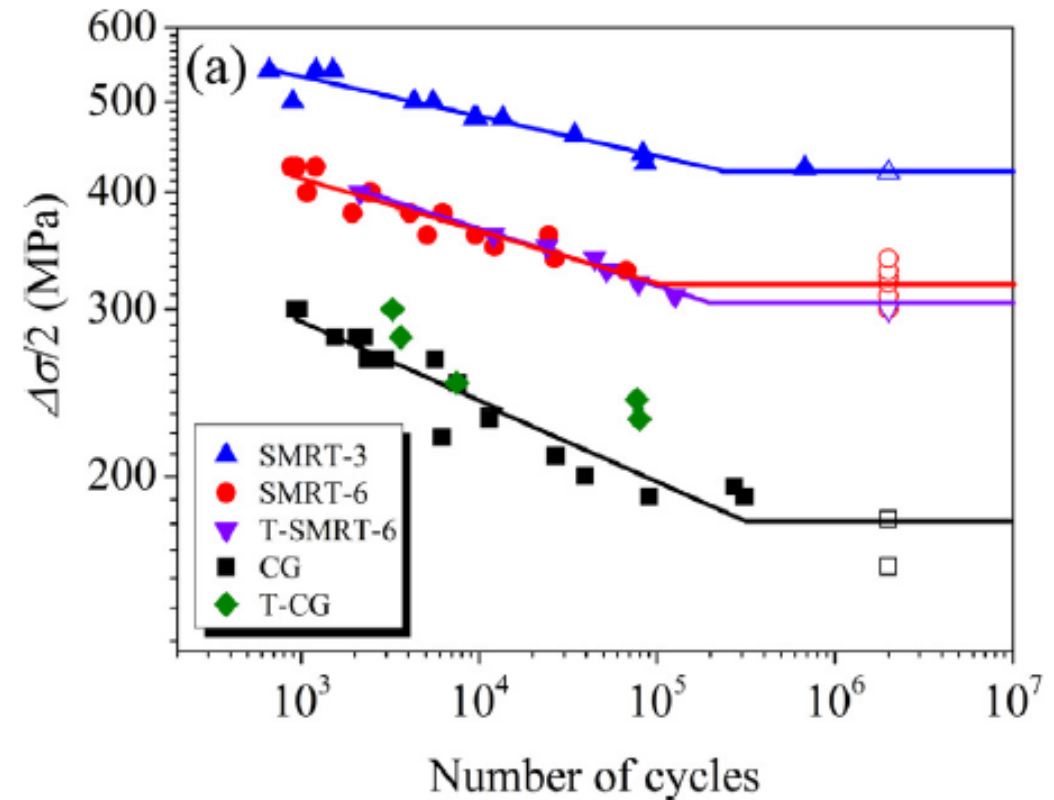
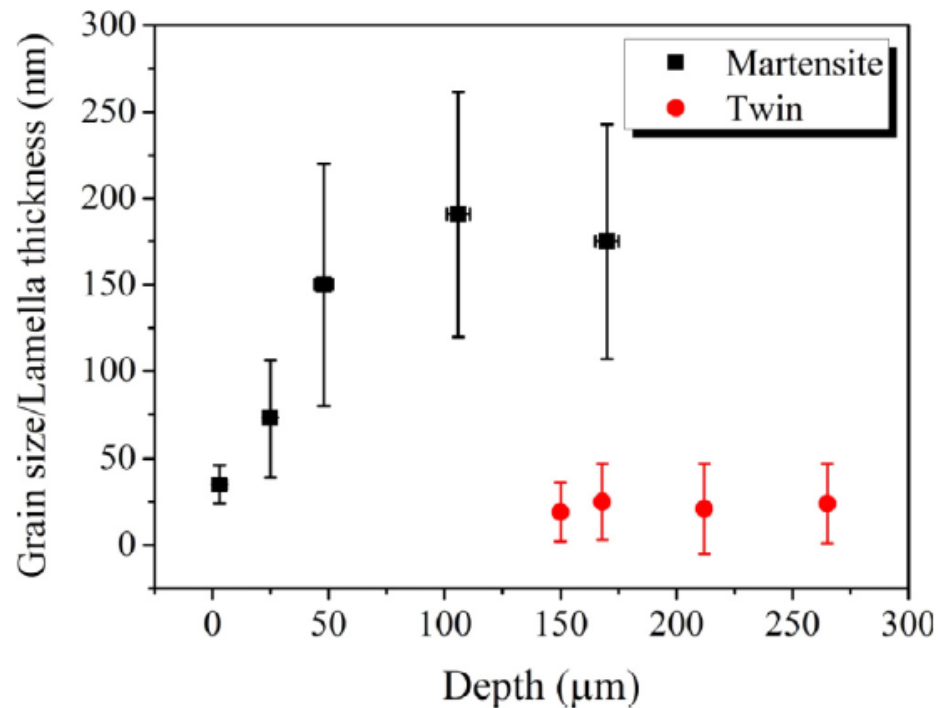
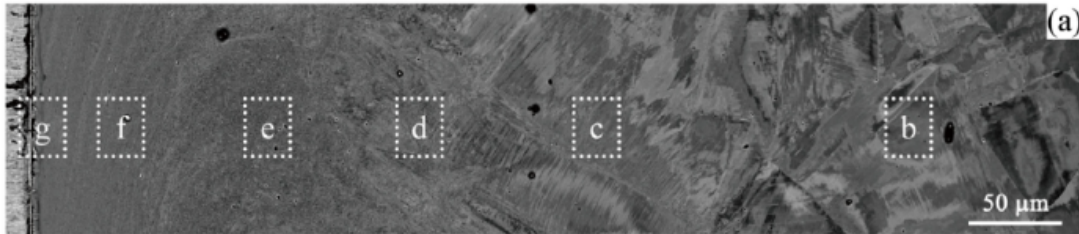


Gradients offer toughening



Gradients offer fatigue resistance

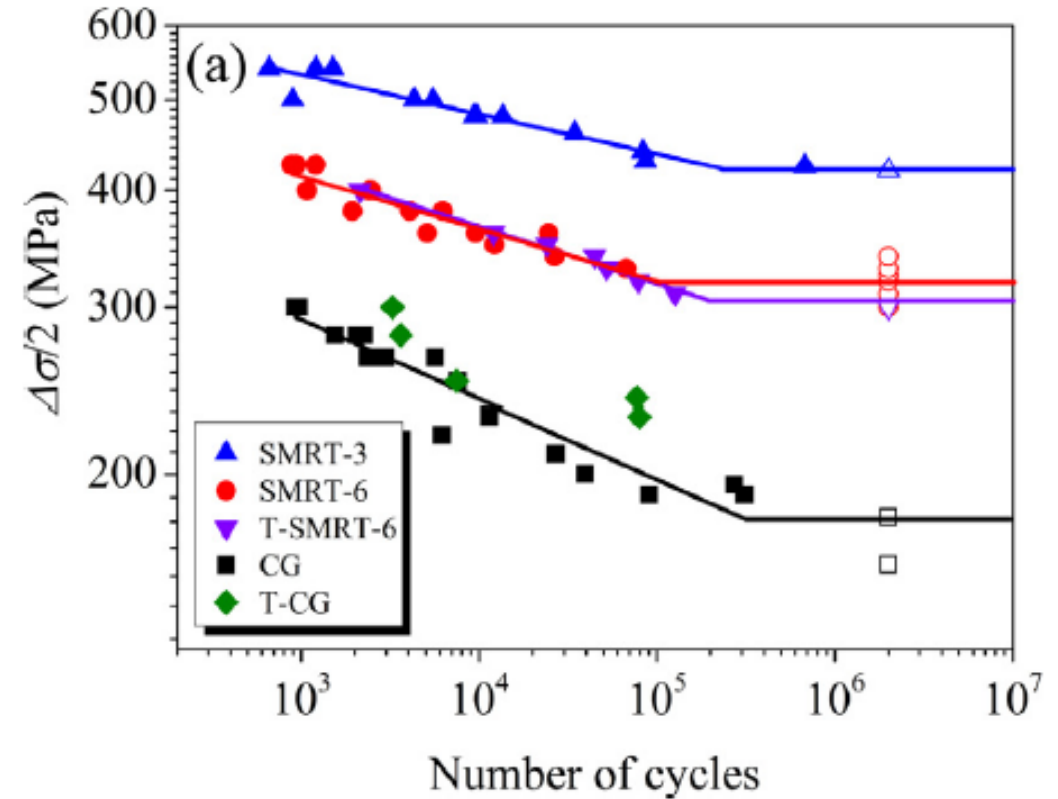
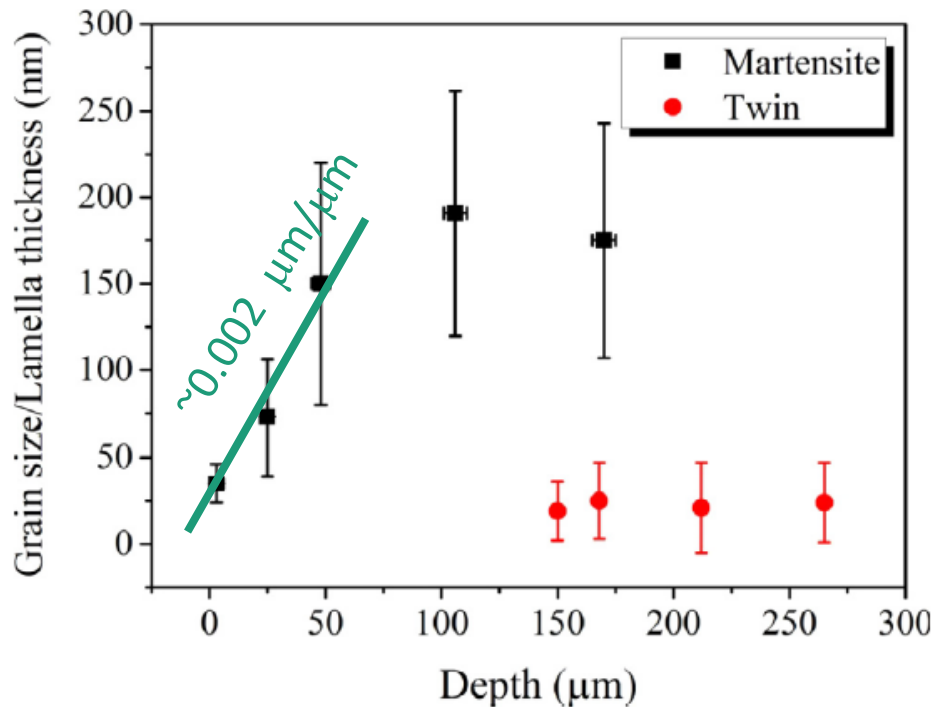
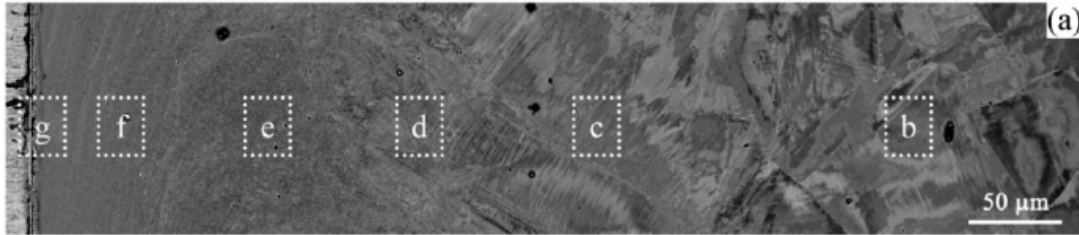
Gradient 316L by SMRT



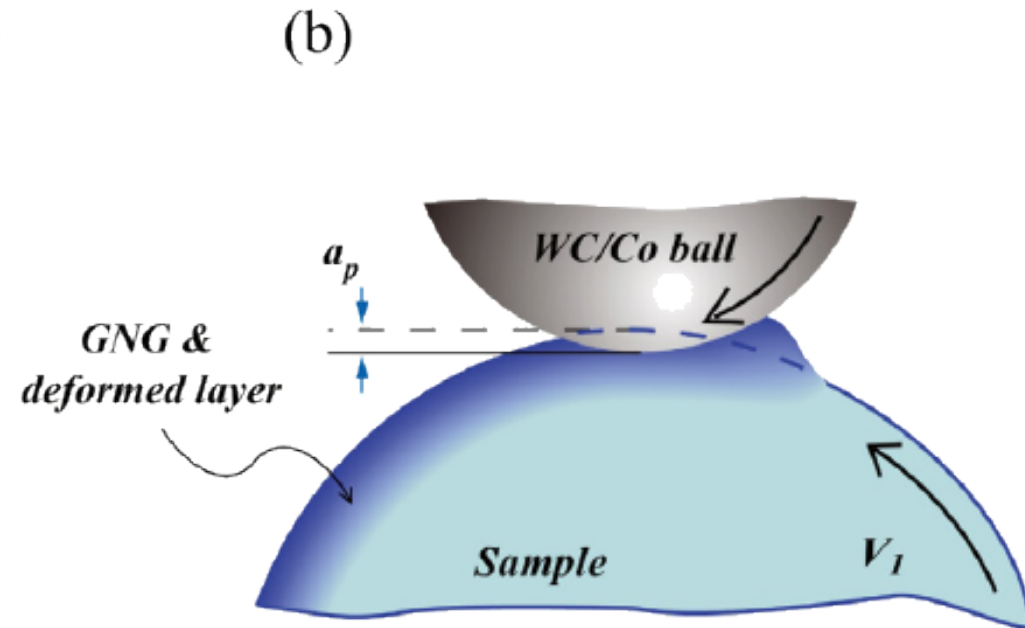
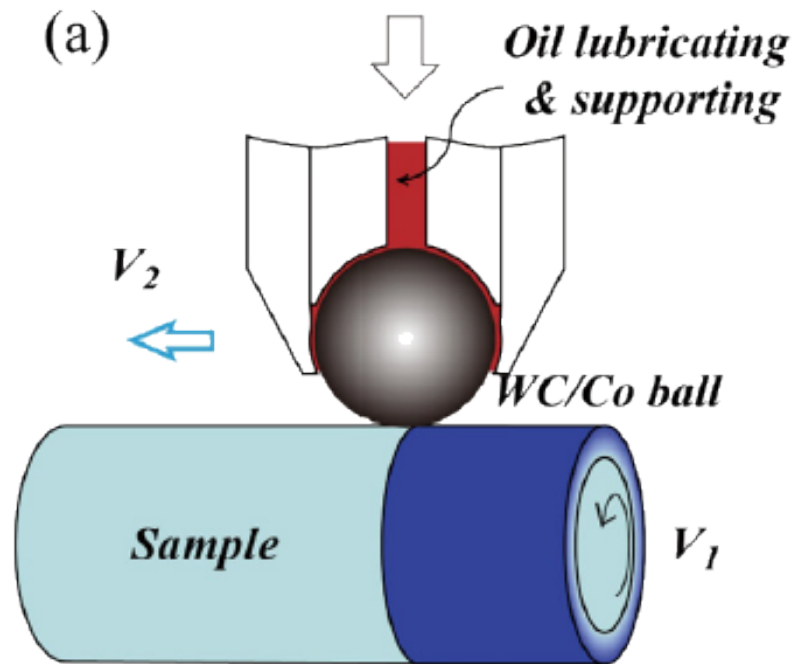
- Strain-induced martensite
- Compressive residual stresses of -1200 to -1500 MPa

Gradients offer fatigue resistance

Gradient 316L by SMRT

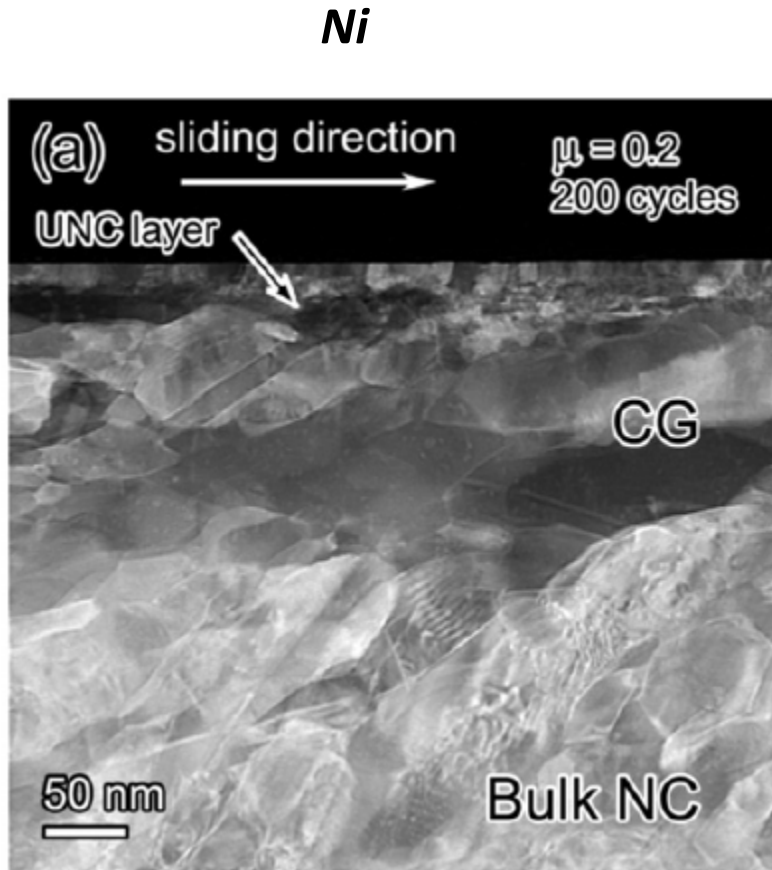


- Strain-induced martensite
- Compressive residual stresses of -1200 to -1500 MPa



Gradient refinement vs coarsening

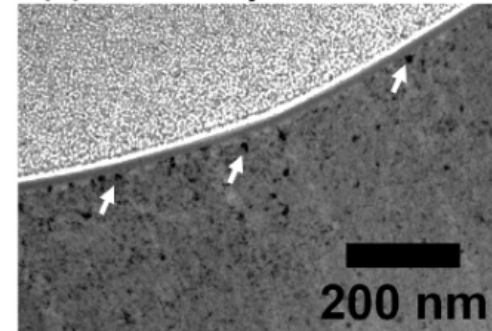
Cyclic sliding contact can surface grain refinement...



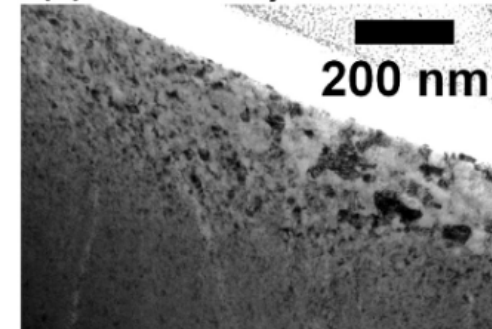
Padilla, Boyce, Battaile, Prasad,
Wear, 2013

Ni-W

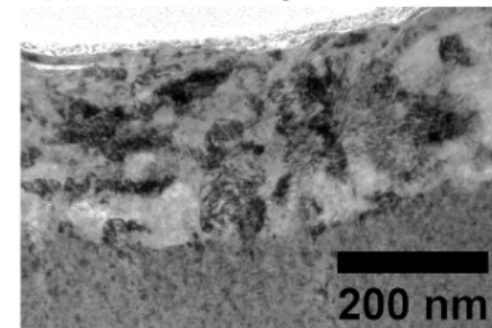
(b) 1 Cycle



(d) 30 Cycles



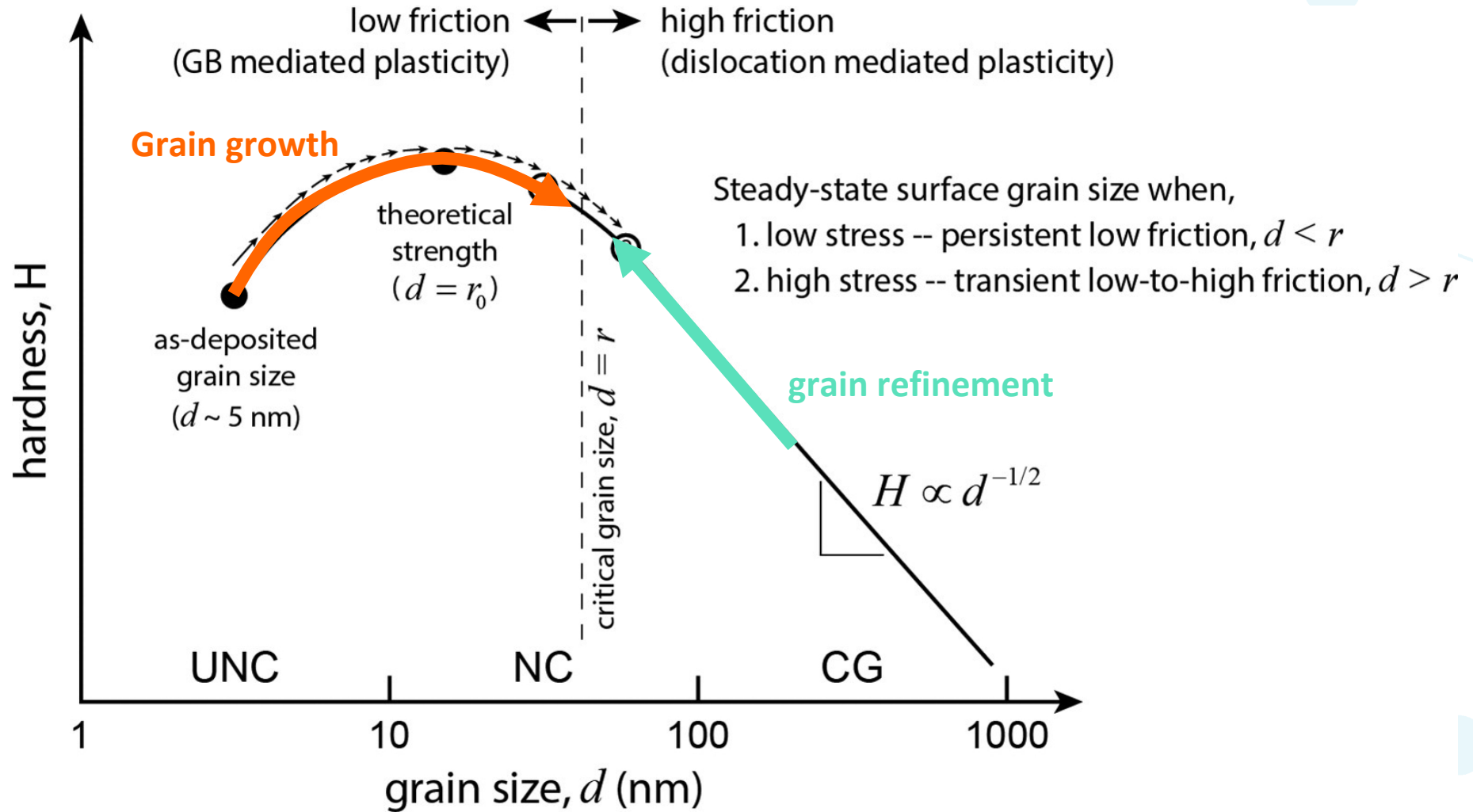
(f) 250 Cycles



...or grain coarsening

Panzarino & Rupert,
Materialia, 2018

The goldilocks zone for stability?

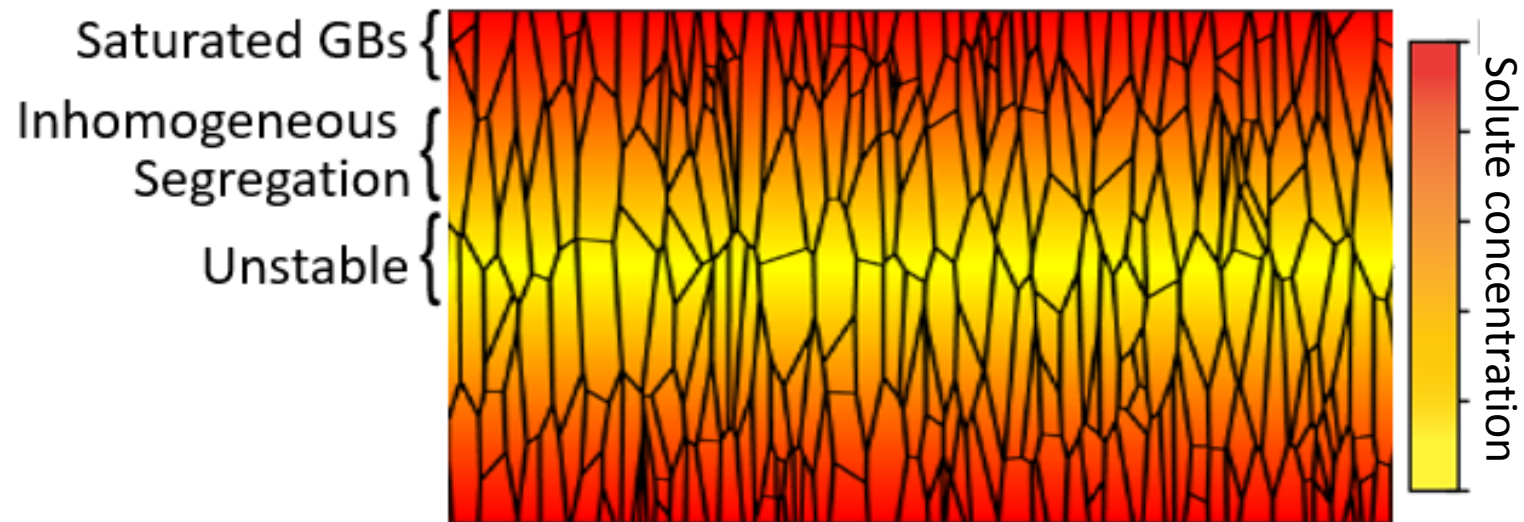


All these examples of heterostructures were achieved by gradients in “severe plastic deformation”

Can we achieve gradient nanostructures by chemical means?

- Create a structure with no/few existing dislocations & twins
- Tailor features that are not “accessible” to surface mechanical treatments
- Create microstructure that is also **stable against evolution**

Chemical gradient concept

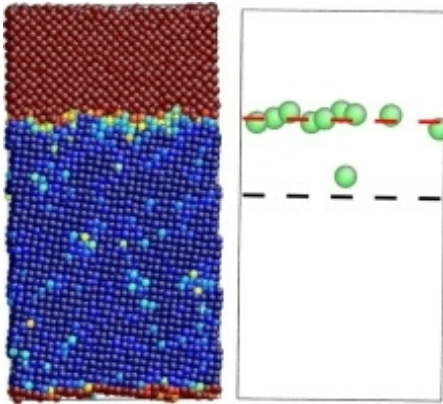


What is the role of solute in creating the microstructural gradient?

Solute effects on grain size stability

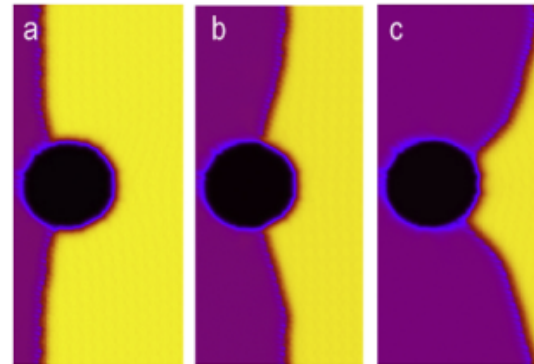
Kinetic

Solute drag



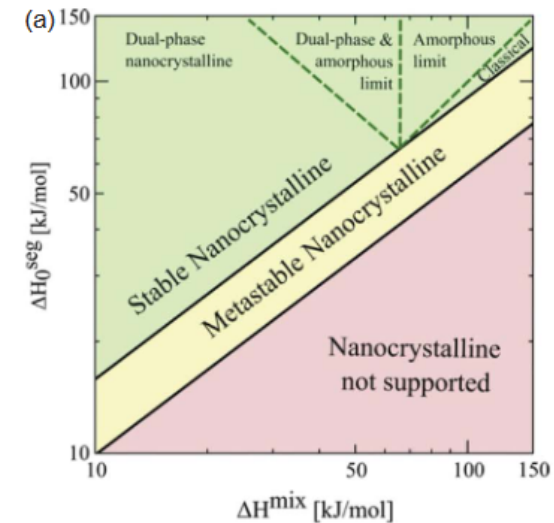
H Sun & C Deng, *Comp. Mater. Sci.*, 2014

Zener pinning



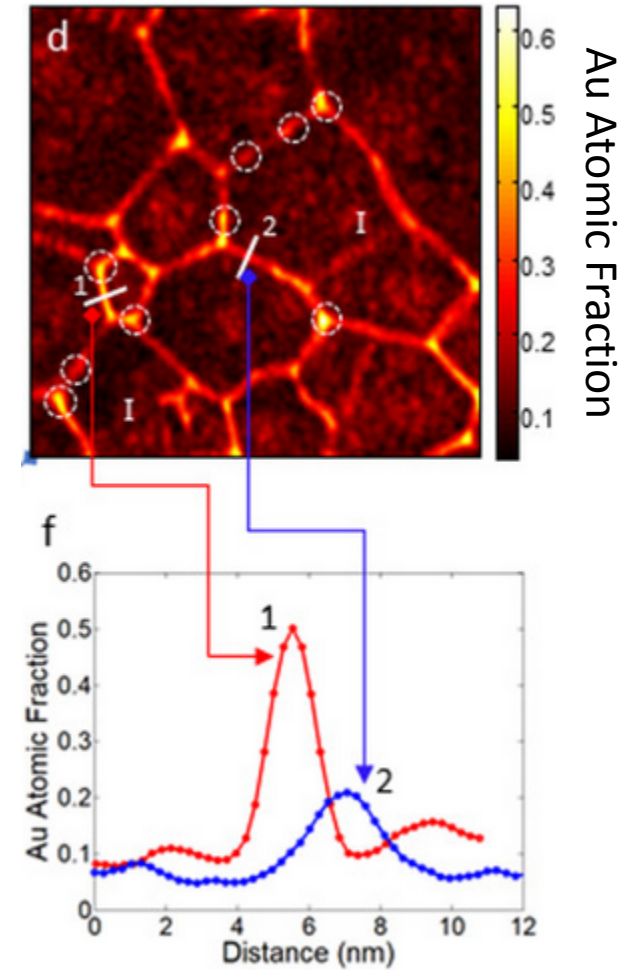
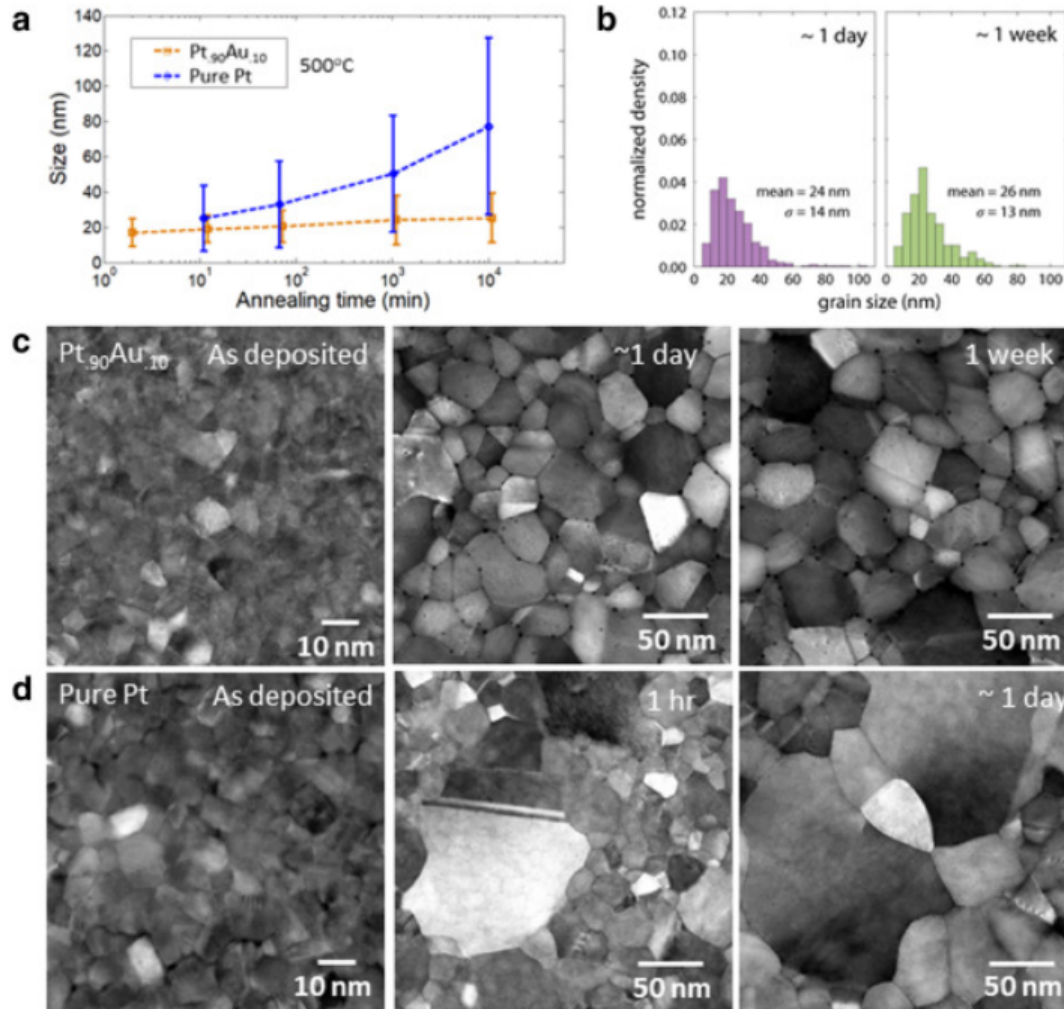
Wang, Ji, Wang, Wen, Chen, *Acta Mater*, 2017

Thermodynamic



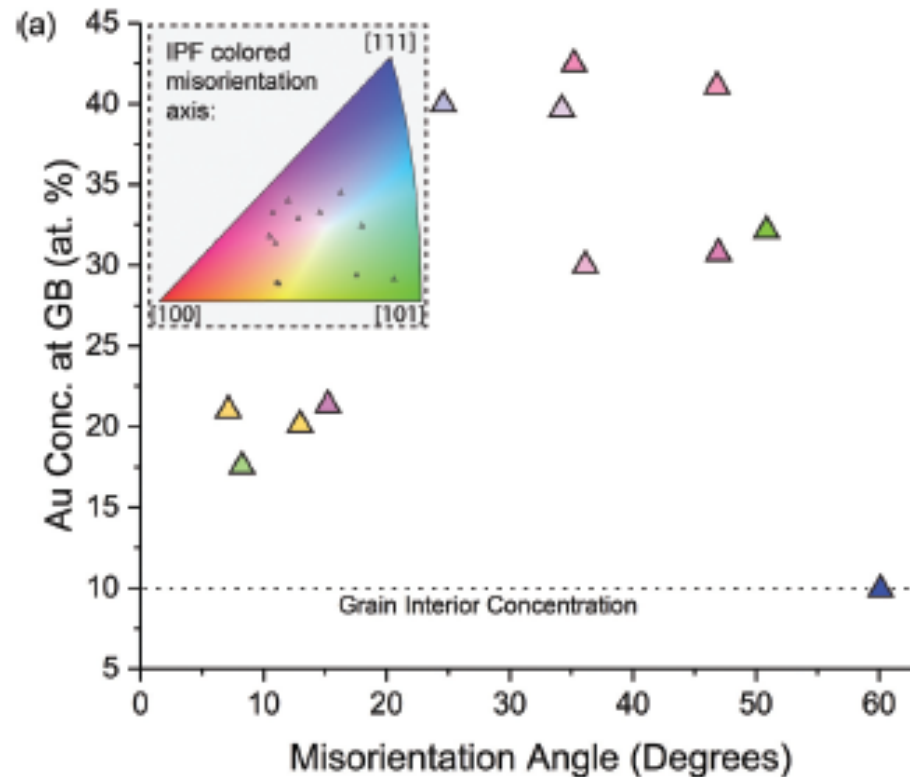
See works by Weissmuller; Schuh; Koch; Darling; others

The Pt-Au nc system



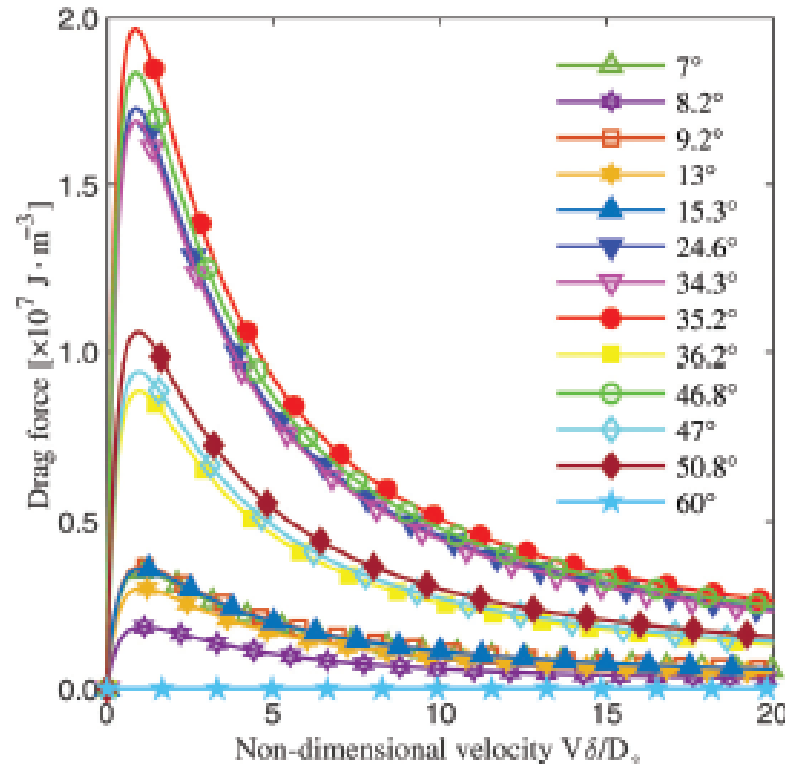
More details on Pt-Au

Au does not segregate uniformly...



For more information...

Au plays both a thermodynamic & kinetic role



Another TMS presentation

Defect and Phase Transformation Pathway Engineering for Desired Microstructures — Invited Presentations

Sponsored by: TMS Materials Processing and Manufacturing Division, TMS: Phase Transformations Committee
Program Organizers: Yufeng Zheng, University of Nevada-Reno; Rongpei Shi, Lawrence Livermore National Laboratory; Yipeng Gao, Idaho National Laboratory; Timofey Frolov, Lawrence Livermore National Laboratory; Stoichko Antonov, Max-Planck-Institut für Eisenforschung GmbH; Jessica Krogstad, University of Illinois at Urbana-Champaign; Bin Li, University of Nevada, Reno

Tuesday AM

March 16, 2021

9:50 AM Invited

Grain Boundary Segregation in Immiscible Alloys: Anisotropy and Trijunction Effects: A. Barnett¹, M. Cox¹, D. Moore¹, M. Alghalayini¹, C. Barr², K. Hattar², B. Boyce², F. Abdeljawad¹, ¹Clemson University; ²Sandia National Laboratories

GB character: C.M. Barr, et al., *Nanoscale*, 2021

Wear response: J.F. Curry, et al., *Adv. Mater.*, 2018

GB phase transformations: C.J. O'Brien et al., *J. Mater. Sci.*, 2018

Tensile behavior: N.M. Heckman et al., *Nanoscale*, 2018

Phase field model development...

Segregation-enhanced thermal stability via a phase-field model

Free energy functional

- $c(\mathbf{r}, t)$: alloy concentration
- $\Phi_i(\mathbf{r}, t)$, $\{i = 1, \dots, n_\Phi\}$: grain order parameters

$$\mathcal{F}_{tot} = \int d\mathbf{r} \left[f_{loc}(c, \vec{\phi}, T) + \underbrace{\sum_i^{n_\Phi} \frac{\epsilon_i^2}{2} |\nabla \phi_i|^2 + \frac{k^2}{2} |\nabla c|^2}_{\text{Gradient terms for GBs and phase boundaries}} \right]$$

Local energy density

Gradient terms for GBs and phase boundaries

$$f_{loc}(c, \vec{\phi}, T) = P(\vec{\phi}) f_{gb}(c, T) + [1 - P(\vec{\phi})] f_b(c, T) + W_\phi g(\vec{\phi})$$

GB energy vs. concentration

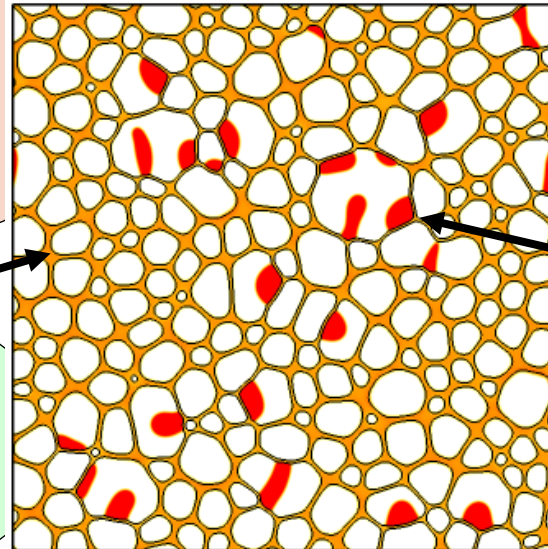
$$\Gamma = - \left(\frac{\partial \gamma_{gb}}{\partial \mu} \right)_{P, T}$$

Weissmüller, Nanostruct. Mater. (1993)

Segregation

GB anisotropy

Udler and D. Seidman, Phys. Stat. Sol. (1992)
Seki *et al.*, Acta Metall. Mater. (1991)
Hashimoto *et al.*, Acta Metall. (1984)



Solute drag

Cahn, Acta Metall. (1962)
Hillert and Sundman, Acta Metall. (1976)
Grönhagen and Ågren, Acta Mater. (2007)

Precipitation

Zener pinning

Smith, Trans. AIME **175** (1948)
Hellman and M. Hillert, Scand. J. Met. (1975)
Chen *et al.*, J. Am. Ceram. Soc. (1998)
Moelens *et al.*, Acta Mater. (2005)

Dynamics

$$\frac{\partial c}{\partial t} = \nabla \cdot \left[M_c \nabla \left(\frac{\delta \mathcal{F}_{tot}}{\delta c} \right) \right]$$

Mass conservation

Cahn-Hilliard Eq.

$$\frac{\partial \phi_i}{\partial t} = -L_i \left(\frac{\delta \mathcal{F}_{tot}}{\delta \phi_i} \right)$$

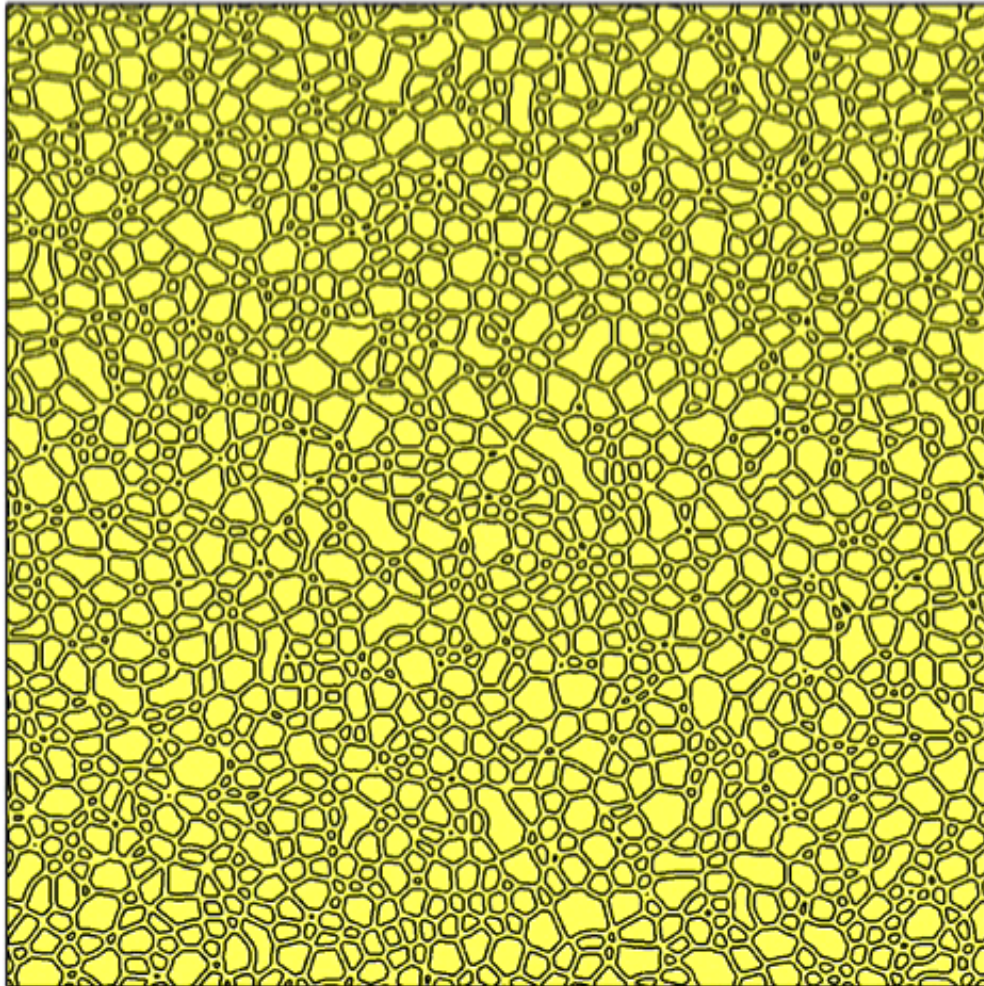
Gradient flow

Allen-Cahn Eq.

Abdeljawad and Foiles, Acta Mater, 2015

Abdeljawad, Lu, Argibay, Clark, Boyce, Foiles, Acta Mater, 2017

Segregation and stabilization



Improvements:

Anisotropic Mobility

Anisotropic Energy

Heterogeneous solute segregating behavior

Adaptive grain tracking algorithm

Grain growth with segregation

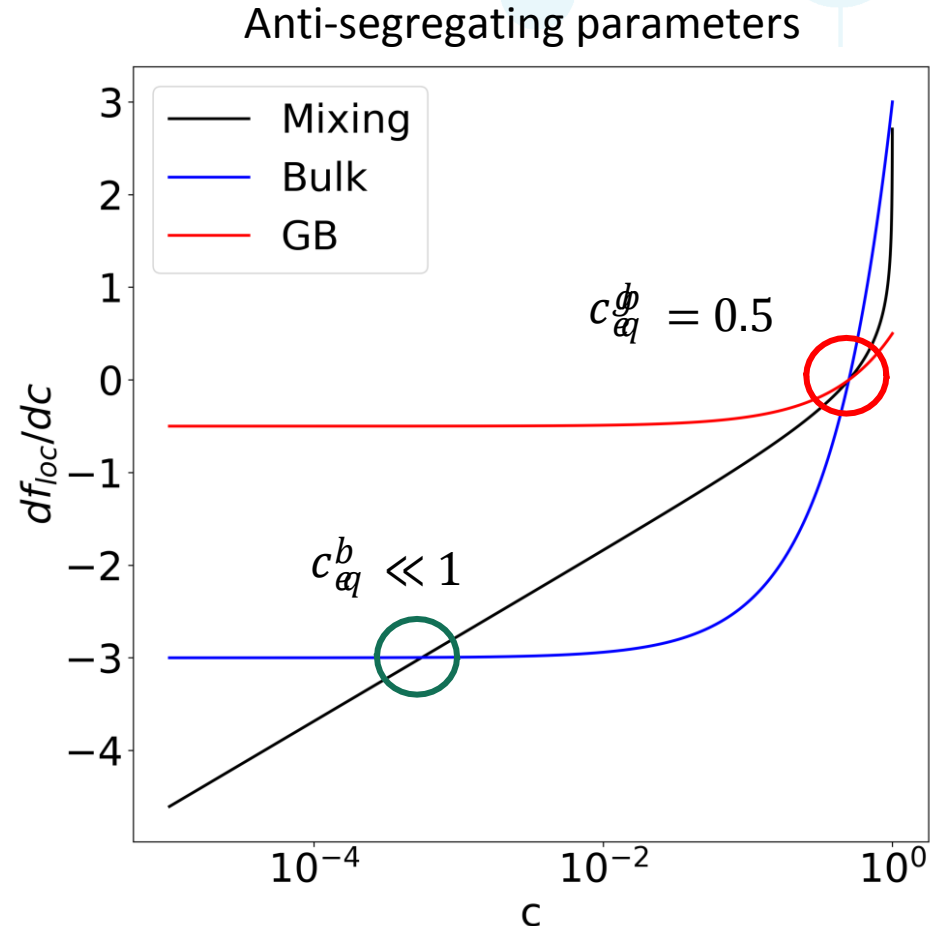
$$f_{loc}(c, T, \{\vec{\phi}\}) = \underbrace{f_b(c, T)}_{\text{bulk}} + \underbrace{[W - \xi_1 c - \xi_2 c^2]g(\vec{\phi})}_{\text{grain boundary}}$$

$$f_b = G_b^B c + (1 - c)G_b^A + \Omega_b c(1 - c) + \frac{RT}{V_m} [c \ln c + (1 - c) \ln(1 - c)]$$

$$W = W_\phi + (G_{gb}^A - G_b^A)$$

$$\xi_1 = (G_{gb}^A - G_b^A) - (G_{gb}^B - G_b^B) - (\Omega_{gb} - \Omega_b)$$

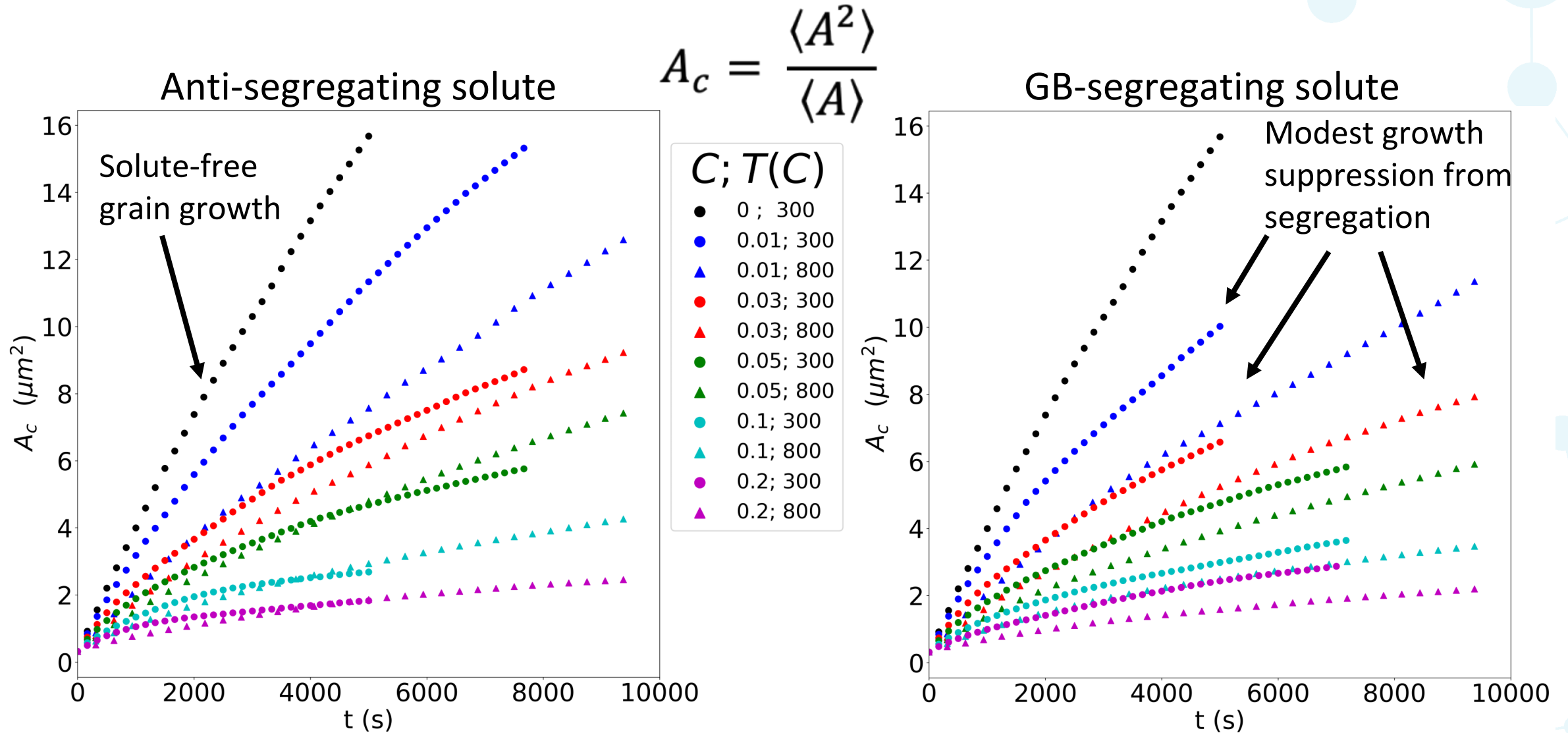
$$\xi_2 = (\Omega_{gb} - \Omega_b)$$



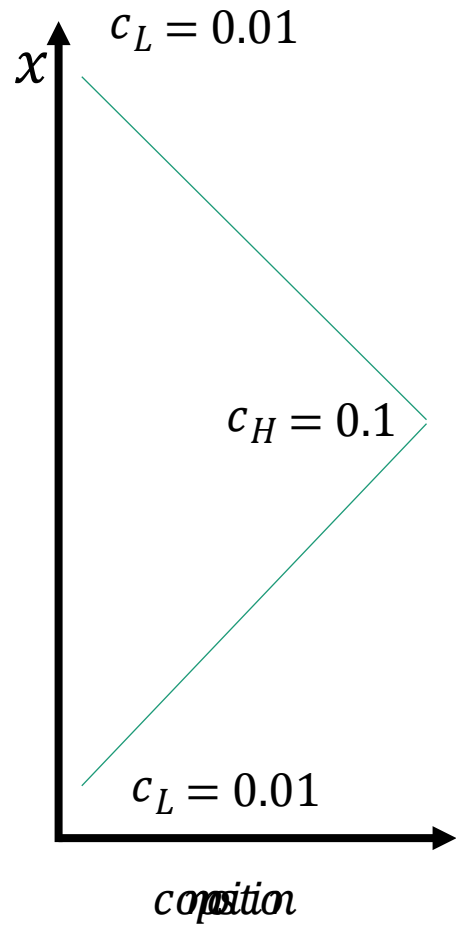
Anti-segregation: $\Omega_{gb} - \Omega_b > 0$

GB segregation: $\Omega_{gb} - \Omega_b < 0$

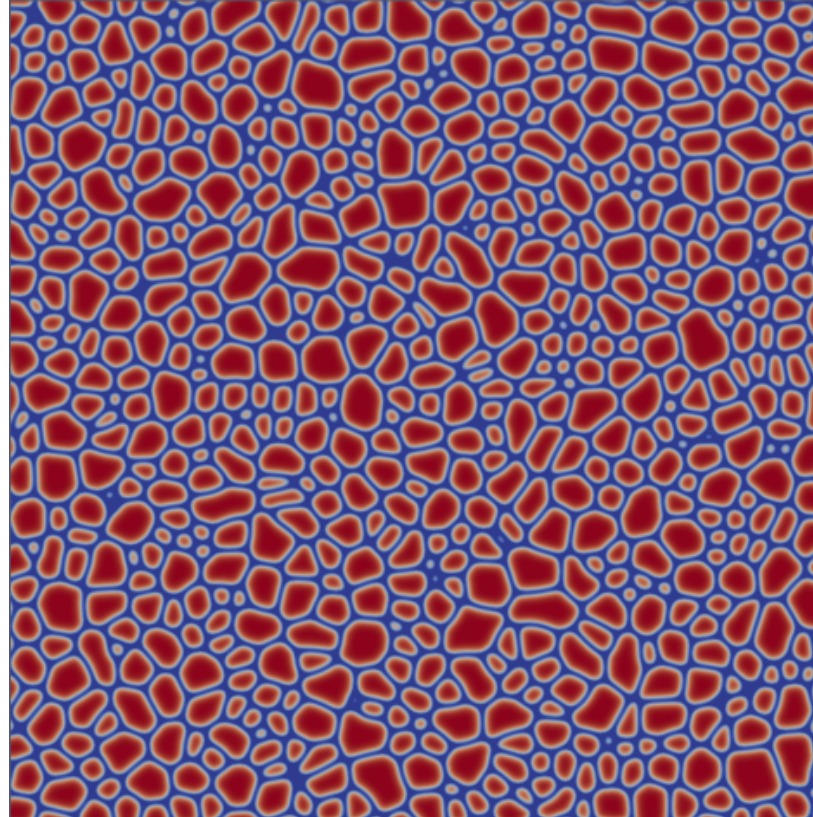
Solute impedes grain growth even without segregation



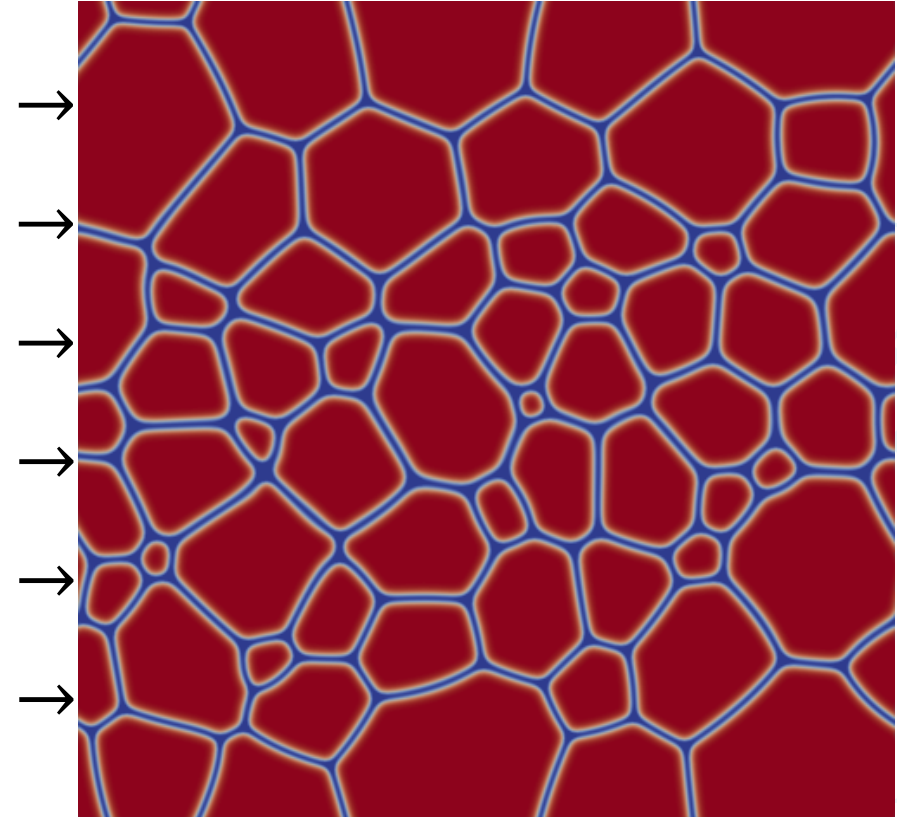
Using concentration gradient to trigger grain size gradient



Initial microstructure



After annealing



Finer Grains

Annealing experiments

800°C
Anneal
10% Au

0 min

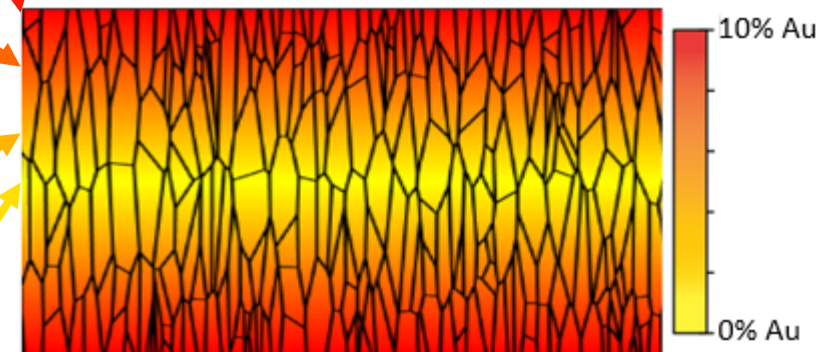
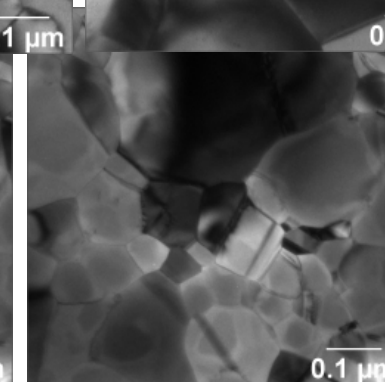
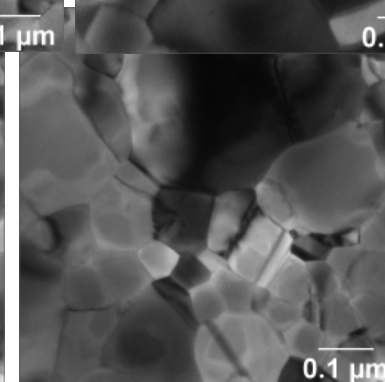
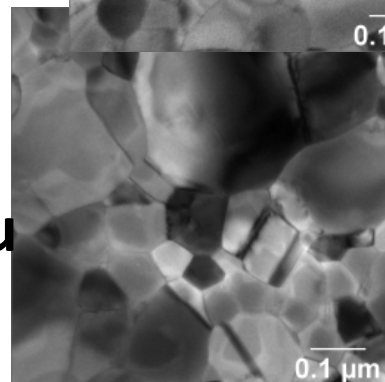
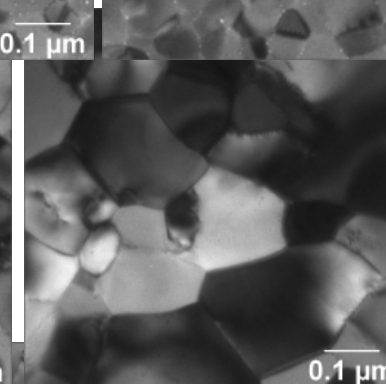
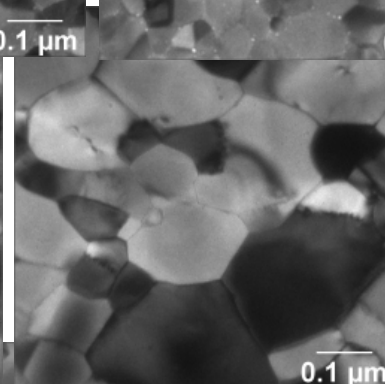
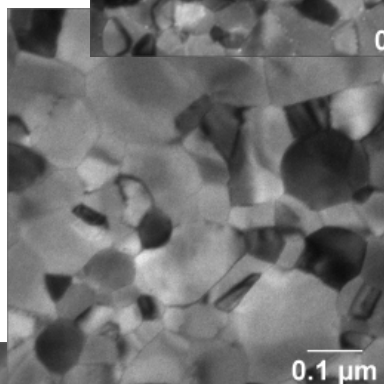
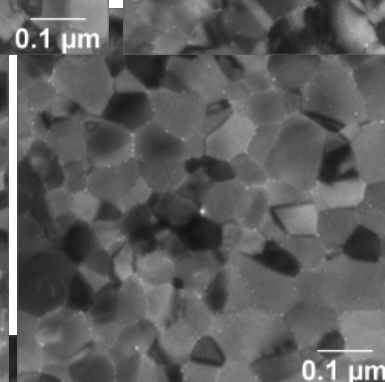
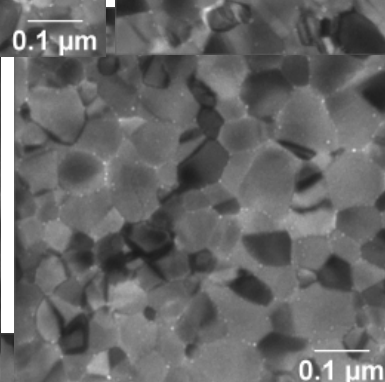
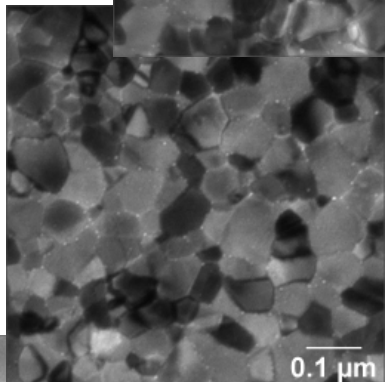
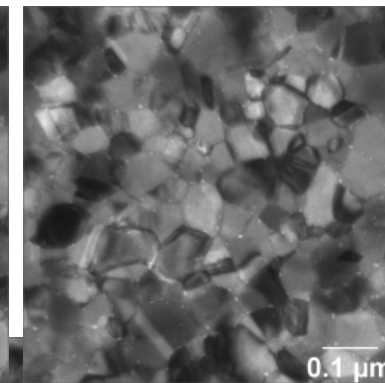
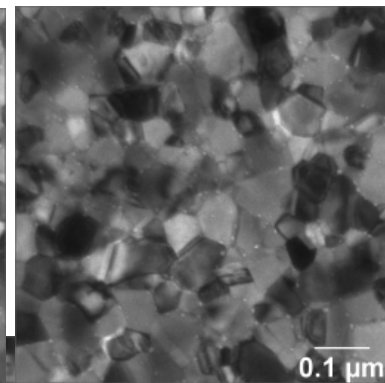
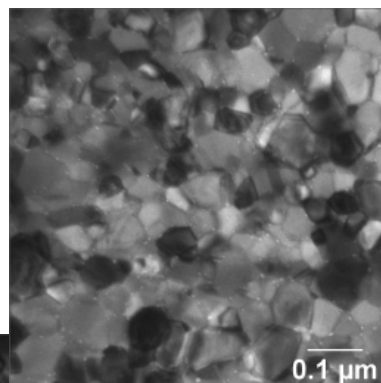
5 min

10 min

3% Au

1% Au

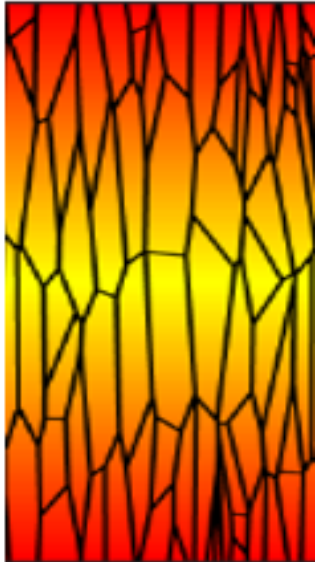
0% Au



Intern: Emily Hopkins, JHU

Step-wise compositional gradient

PVD deposition



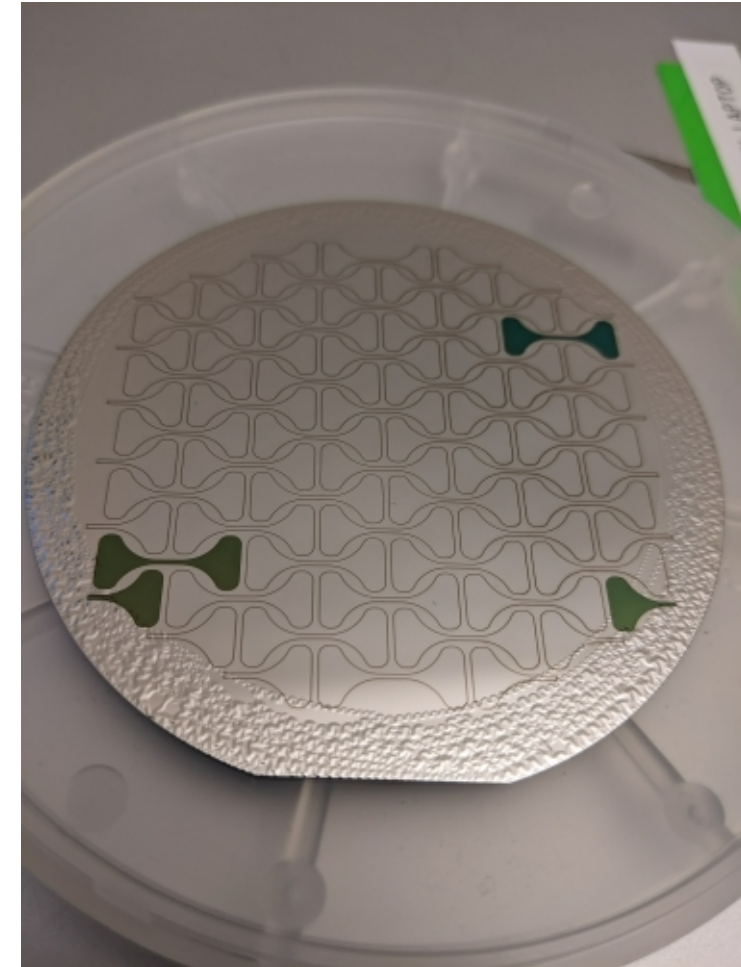
Pt-10Au	0.2 um
Pt-3Au	0.2 um
Pt-1Au	0.2 um
Pt	0.8 um
Pt-1Au	0.2 um
Pt-3Au	0.2 um
Pt-10Au	0.2 um

Across Thickness (2 um)

*only the 90/10 layers have been quantified for atomic %; Others are new targets

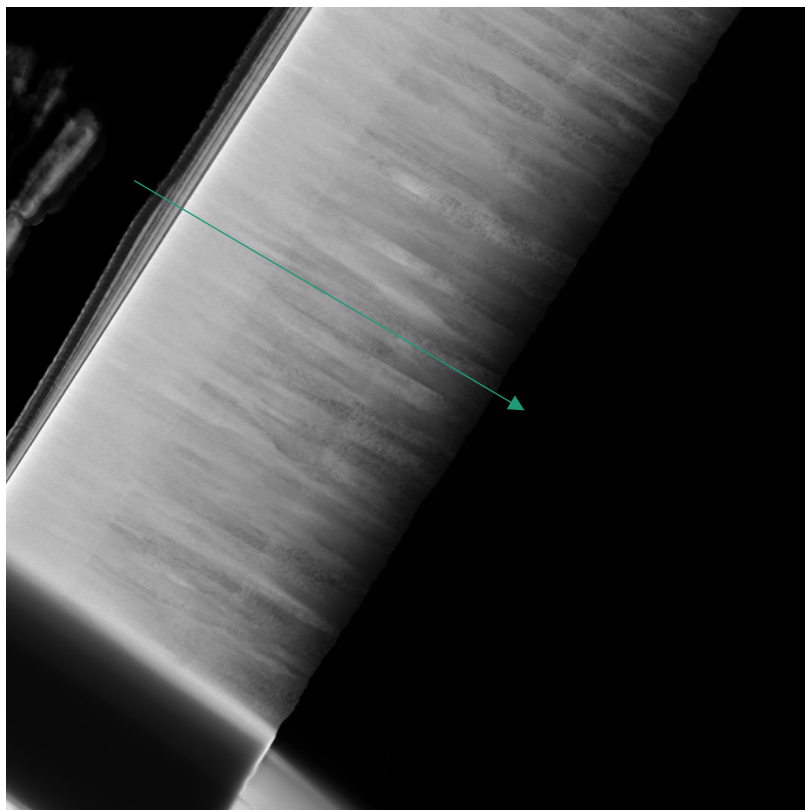
Deposited on Si/SiO wafer

Films femtolaser cut into dogbones

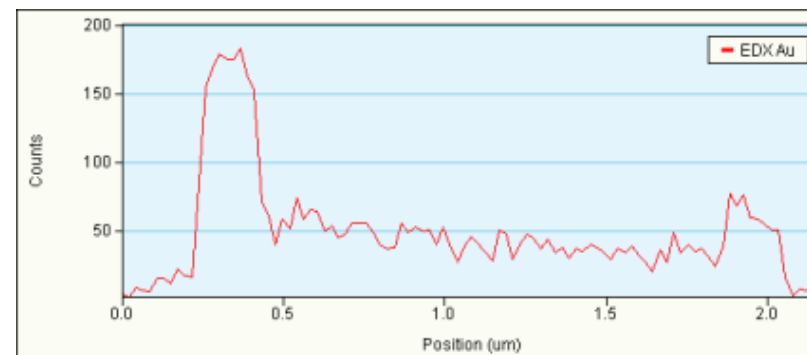


Preliminary results: EDS compositional gradients

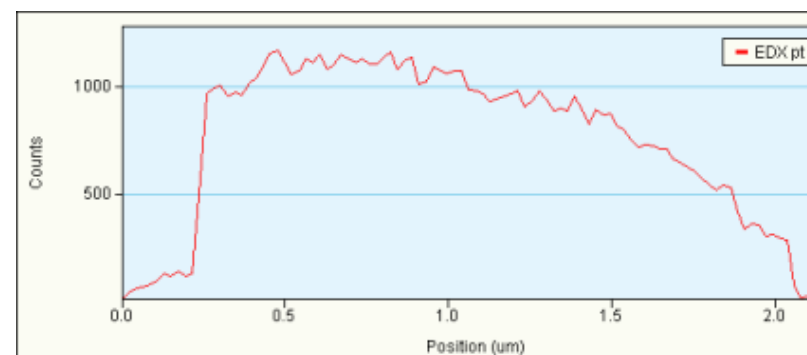
HAADF



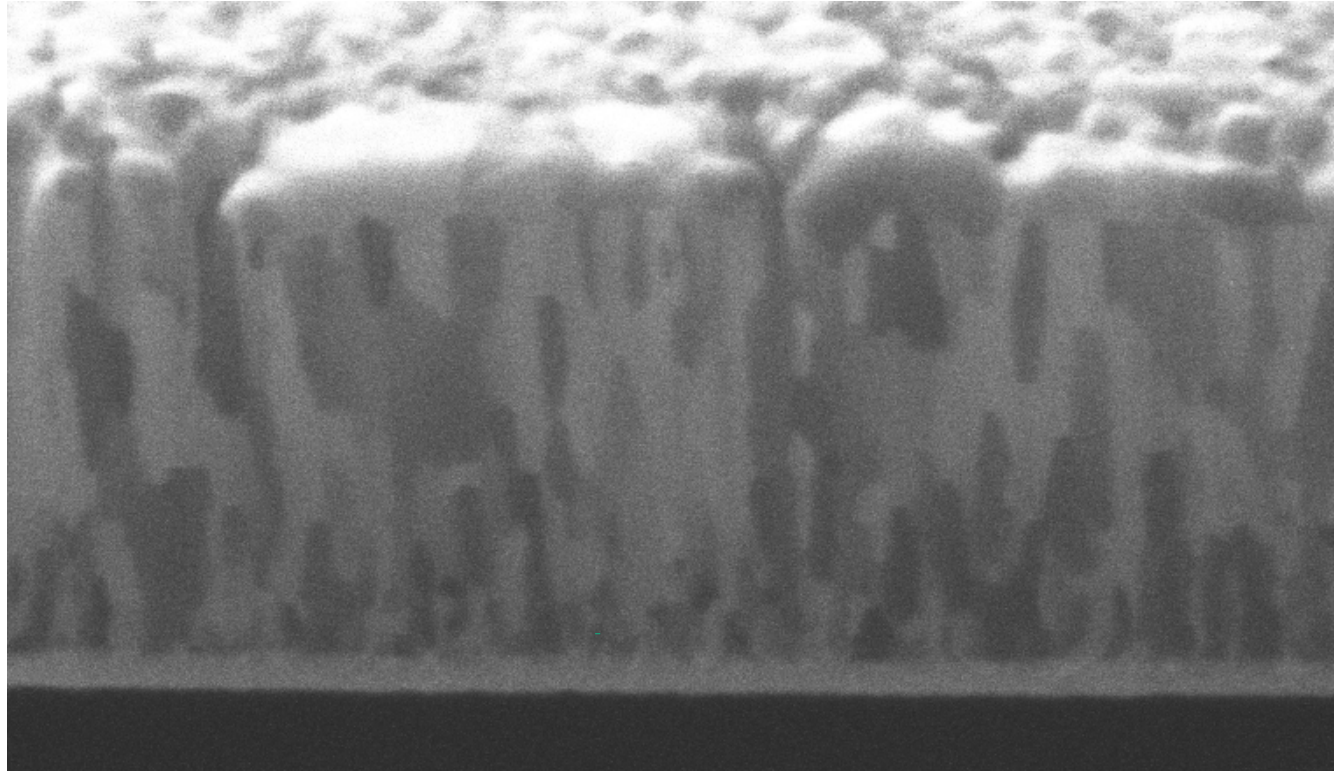
Au



Pt



Example ion channeling of gradient Pt-Au



▽ PtAu 071320, 500C, 10 min

- Most gradient nanostructures are formed by severe plastic deformation, and are expected to be thermally unstable.
- Compositional gradients can create grain size gradients during annealing
- Such chemical gradients are naturally stable, unlike SPD gradients.
- Can we achieve steeper gradients ($1 \mu\text{m}/\mu\text{m}$)?
- Can steep microstructural gradients be manipulated to control tensile, fracture, fatigue resistance, wear resistance, radiation tolerance?



BIG SCIENCE AT THE NANOSCALE

- Comprehensive nanoscience capabilities
- Free access with a successful 2-page user proposal

CINT is a user facility providing cutting-edge nanoscience and nanotechnology capabilities to the research community.

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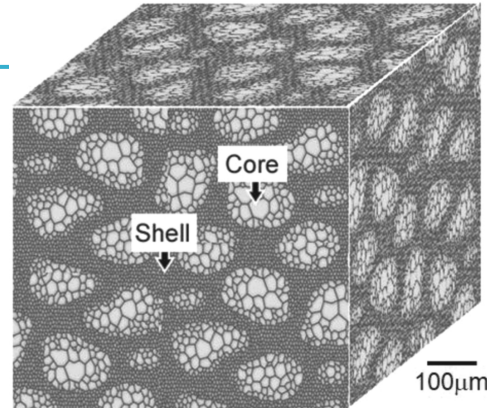
Research areas:

- Quantum Materials Systems
- Nanophotonics and Optical Nanomaterials
- ***In-Situ Characterization and Nanomechanics***
- Soft, Biological, and Composite Nanomaterials

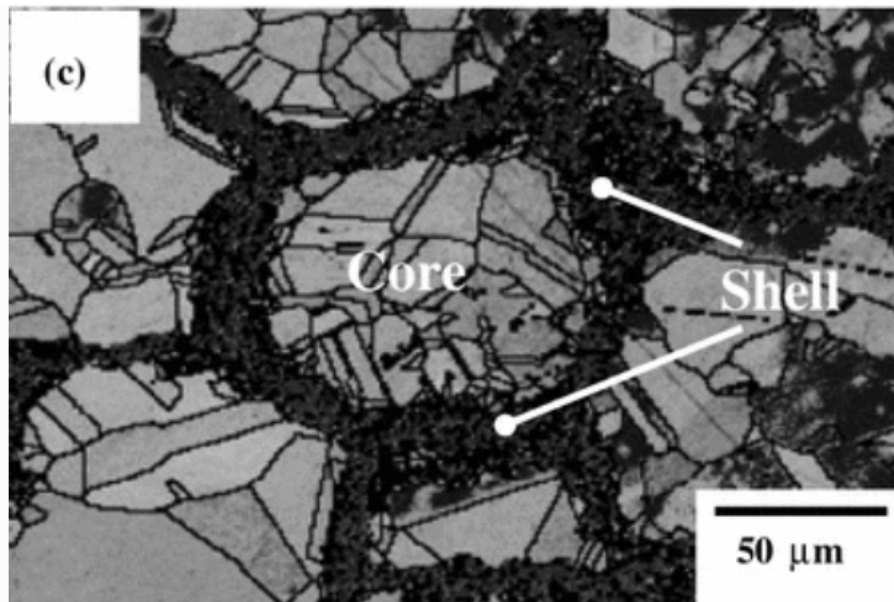
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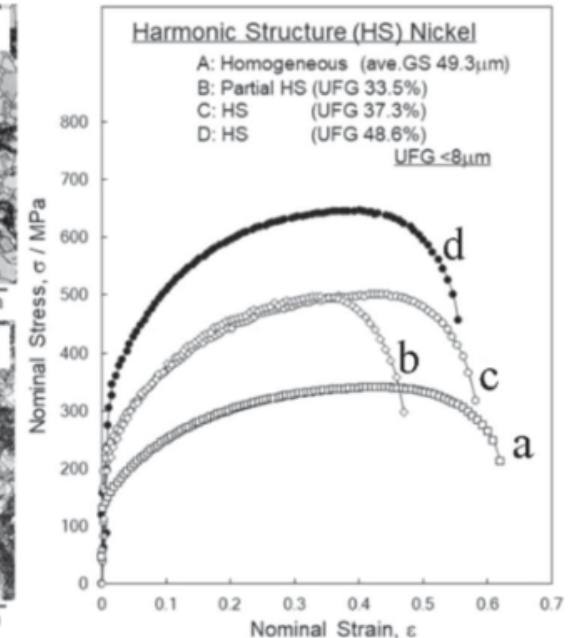
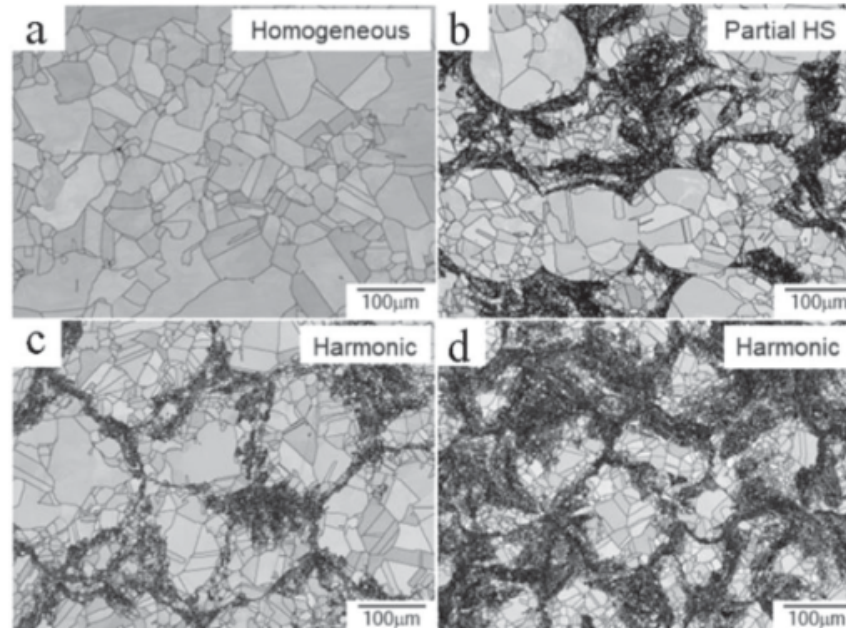
Gradients are not just from the surface



Manufactured via powder metallurgy
e.g. ball milling & sintering



Sawangrat et al, *J. Mater. Sci*, 2014



Y. Zhu et al, *Mater. Res. Lett*, 2020

Combined grain growth and segregation model: Abdeljawad and Foiles

$$\mathcal{F}_{tot} = \int dV \left[f_{loc}(c, T, \{\vec{\phi}\}) + \underbrace{\sum_i^{n_{\max}} \frac{\varepsilon^2}{2} |\nabla \phi_i|^2}_{\text{Grain boundary width}} + \frac{\kappa^2}{2} |\nabla c|^2 \right]$$

$$f_{loc}(c, T, \{\vec{\phi}\}) = \underbrace{f_b(c, T)}_{\text{Bulk concentration}} + \underbrace{[W - \xi_1 c - \xi_2 c^2]g(\vec{\phi})}_{\text{Grain dynamics}}$$

$g(\vec{\phi})$ varies smoothly between 0 (bulk) and 1 (grain boundary)

Grain growth with segregation

$$f_{loc}(c, T, \{\vec{\phi}\}) = \underbrace{f_b(c, T)}_{\text{Bulk concentration}} + \underbrace{[W - \xi_1 c - \xi_2 c^2]g(\vec{\phi})}_{\text{Grain dynamics}}$$

Bulk concentration

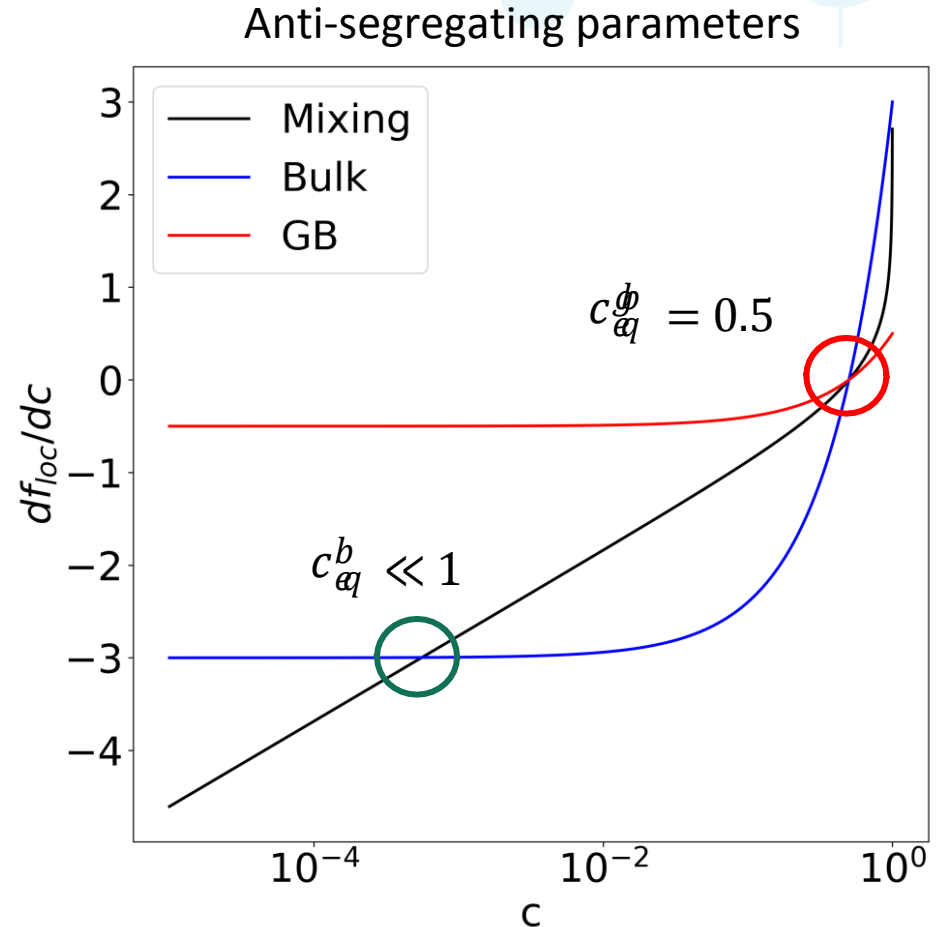
Grain dynamics

$$f_b = G_b^B c + (1 - c)G_b^A + \Omega_b c(1 - c) + \frac{RT}{V_m} [c \ln c + (1 - c) \ln(1 - c)]$$

$$W = W_\phi + (G_{gb}^A - G_b^A)$$

$$\xi_1 = (G_{gb}^A - G_b^A) - (G_{gb}^B - G_b^B) - (\Omega_{gb} - \Omega_b)$$

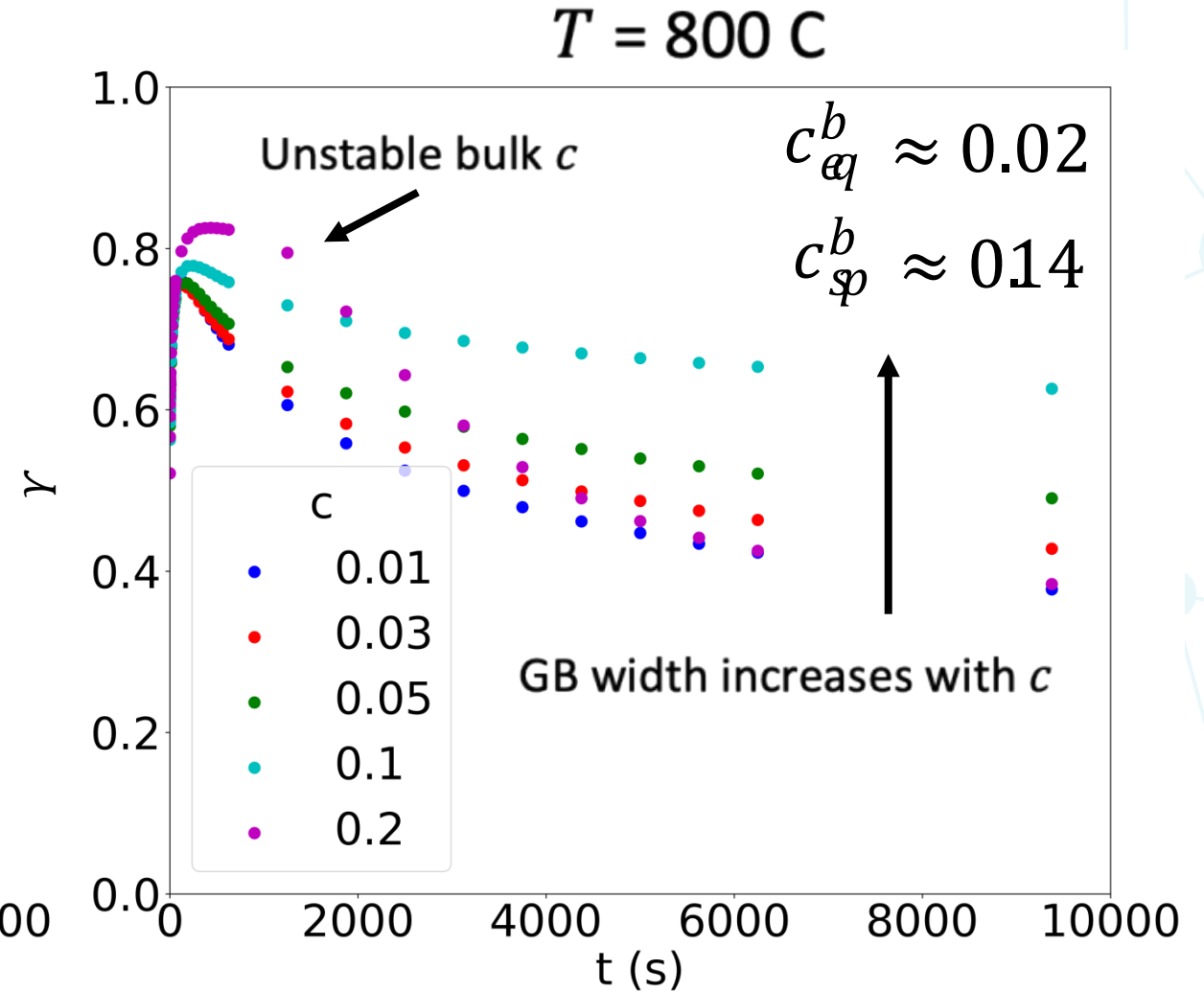
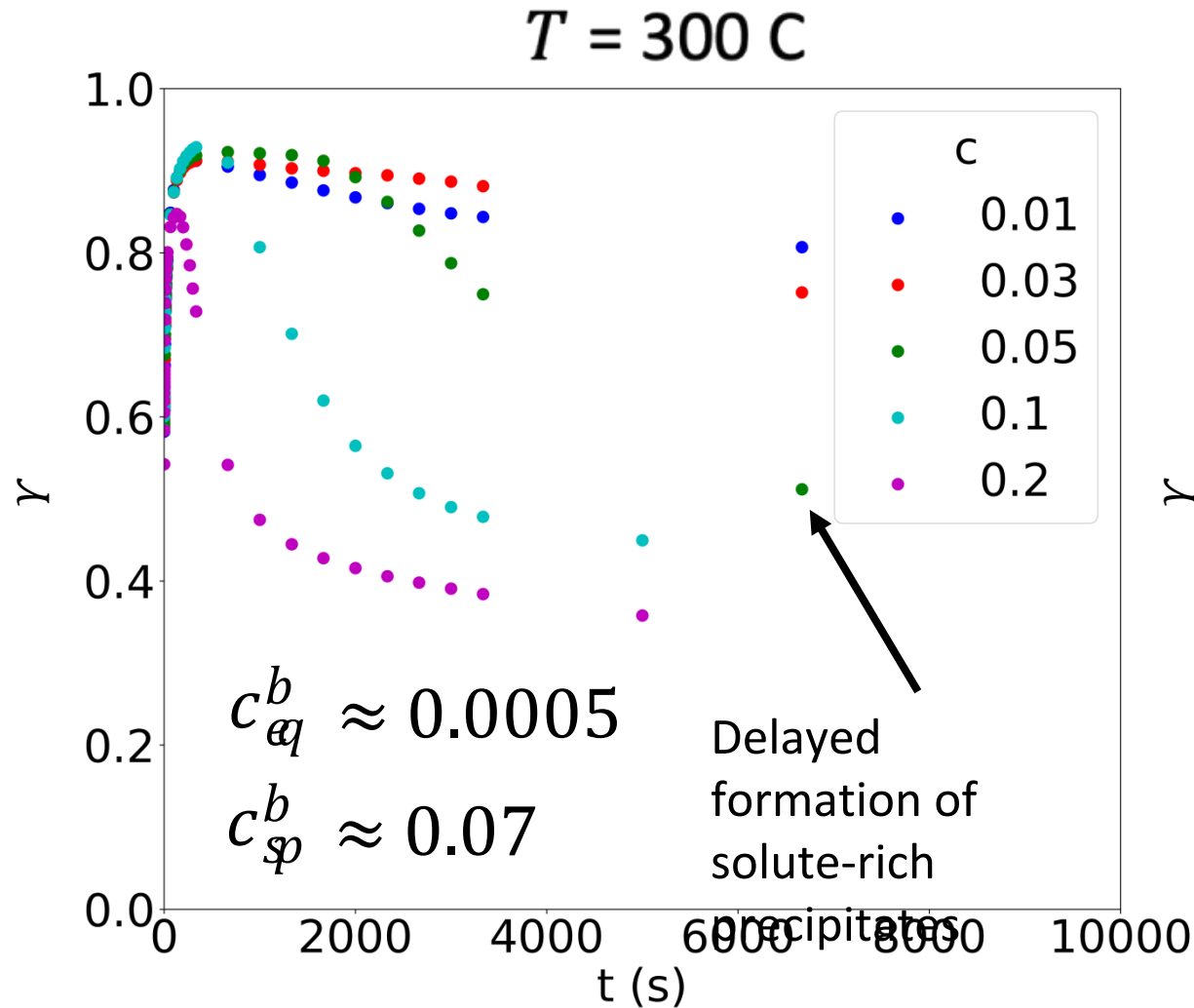
$$\xi_2 = (\Omega_{gb} - \Omega_b)$$



Anti-segregation: $\Omega_{gb} > 0$

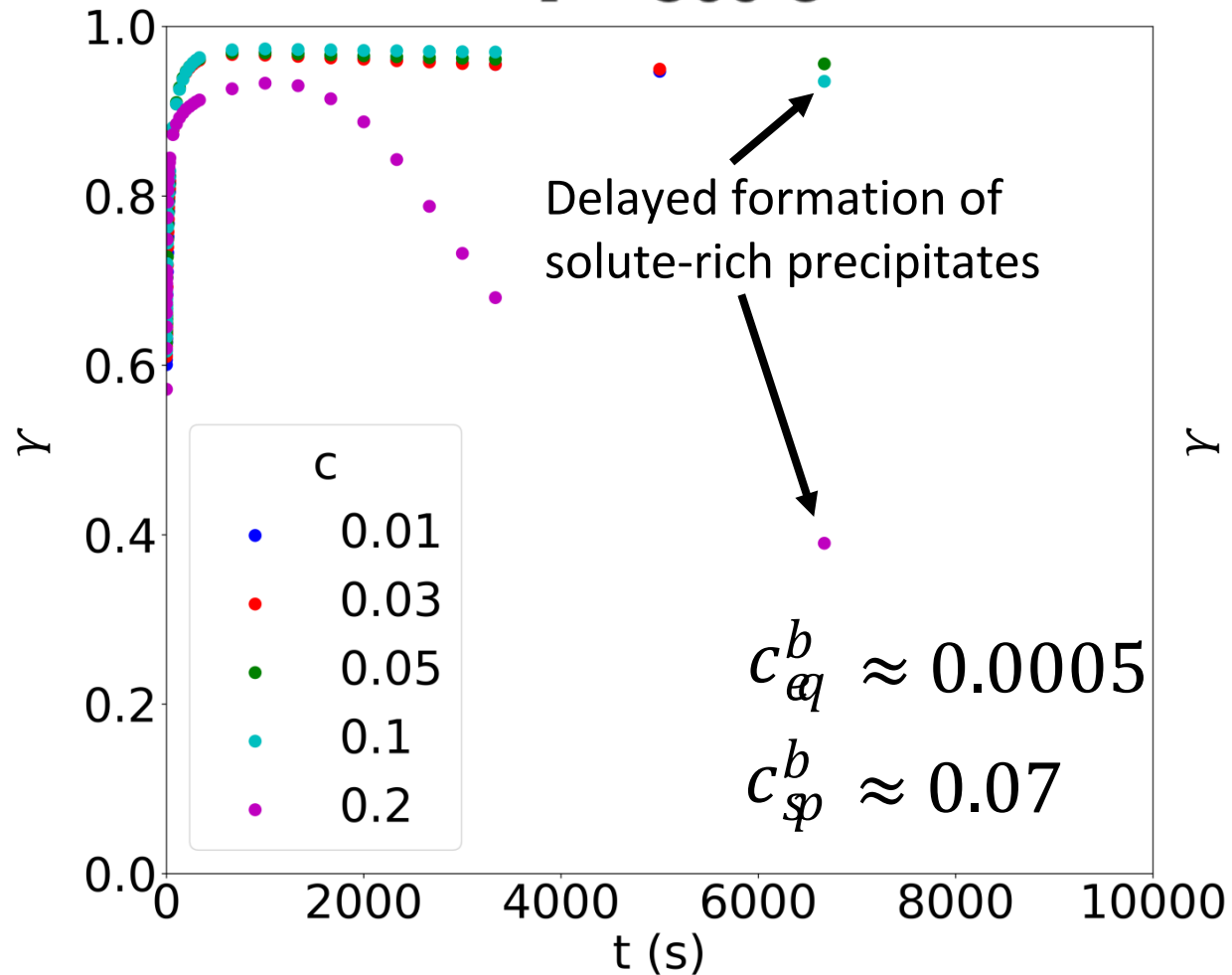
GB segregation: $\Omega_{gb} < 0$

Anti-segregating solute population

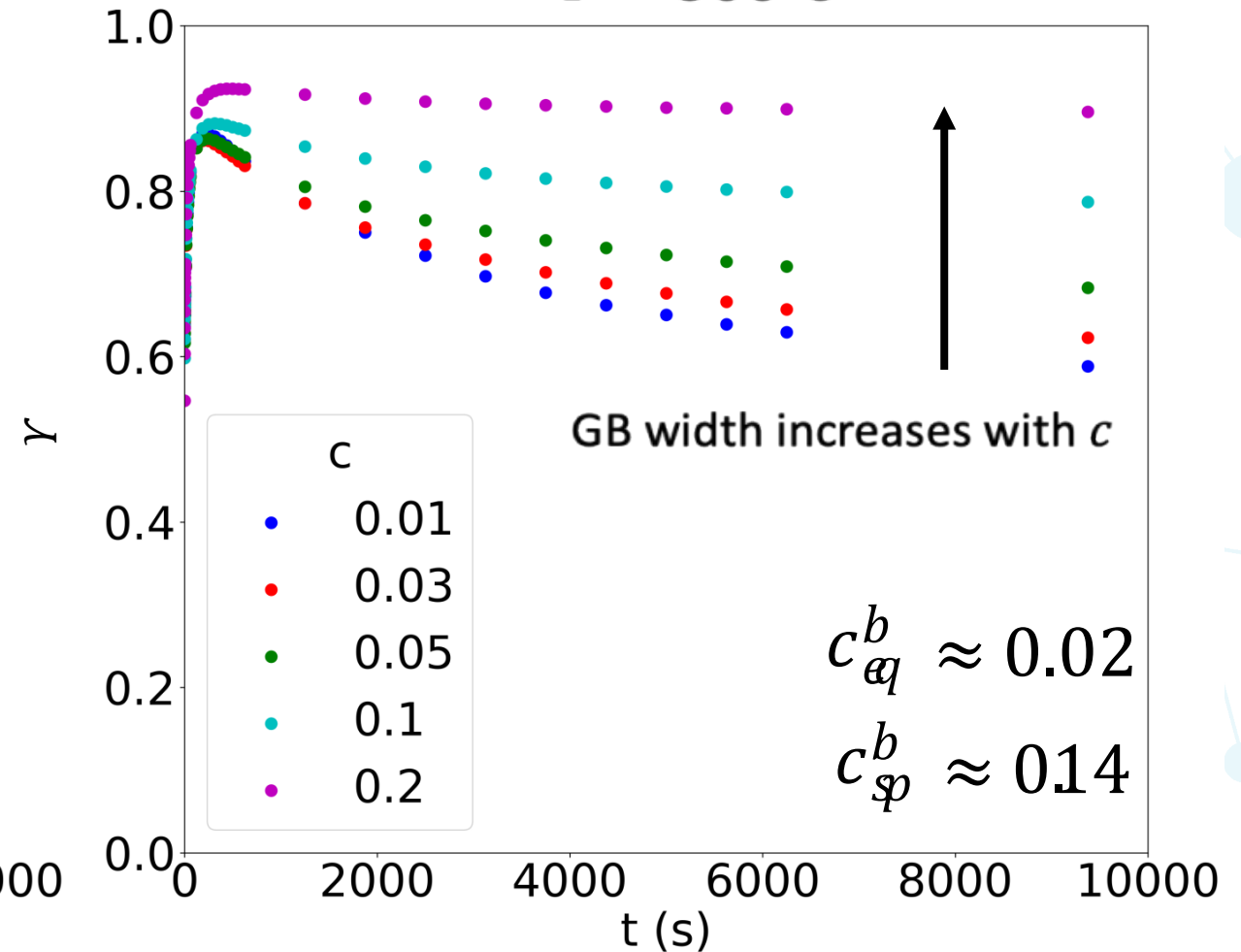


GB-segregating solute population

$T = 300\text{ C}$



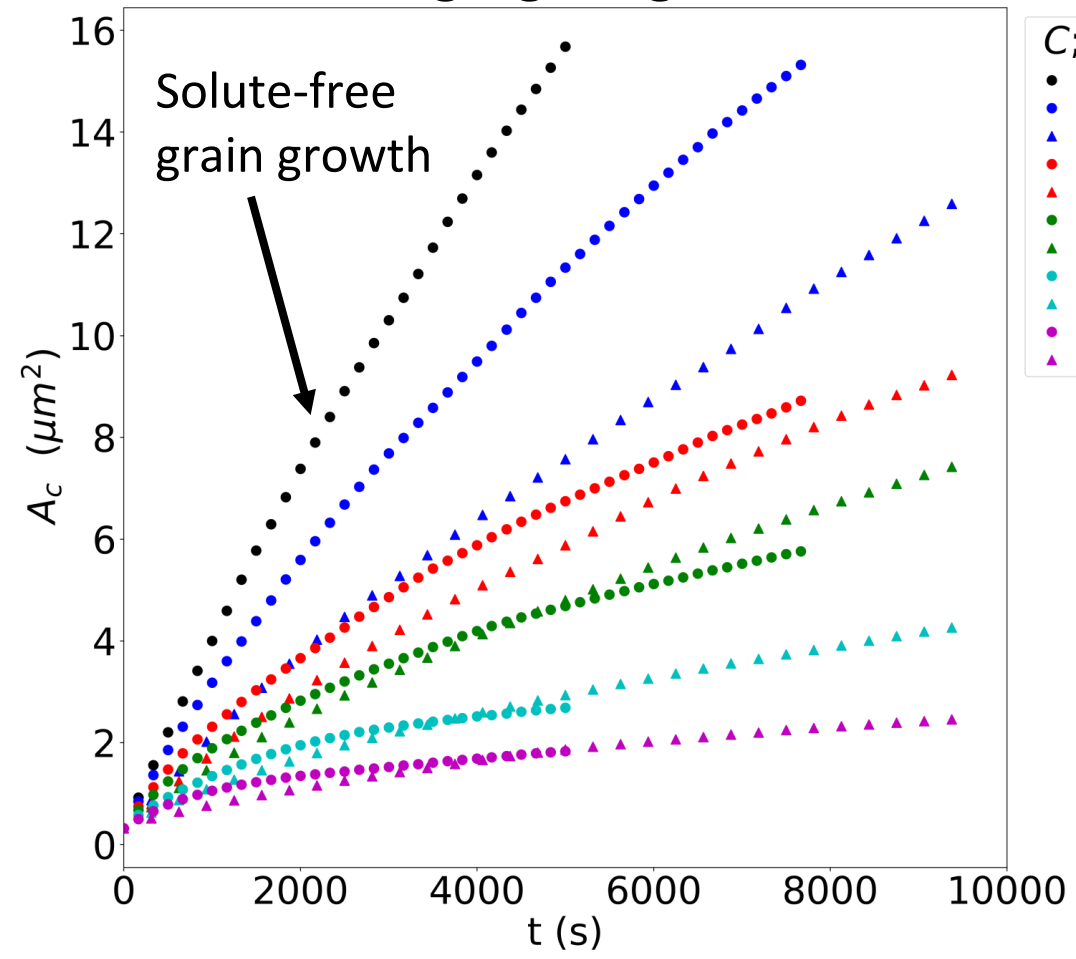
$T = 800\text{ C}$



Segregants impede grain growth

$$A_c = \frac{\langle A^2 \rangle}{\langle A \rangle}$$

Anti-segregating solute



GB-segregating solute

