



THE OHIO STATE UNIVERSITY



# Evaluating HEAC Possibility in RH-dependent Microcracking Observed in Austenitic Stainless Steels

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AMPP CORROSION 2022

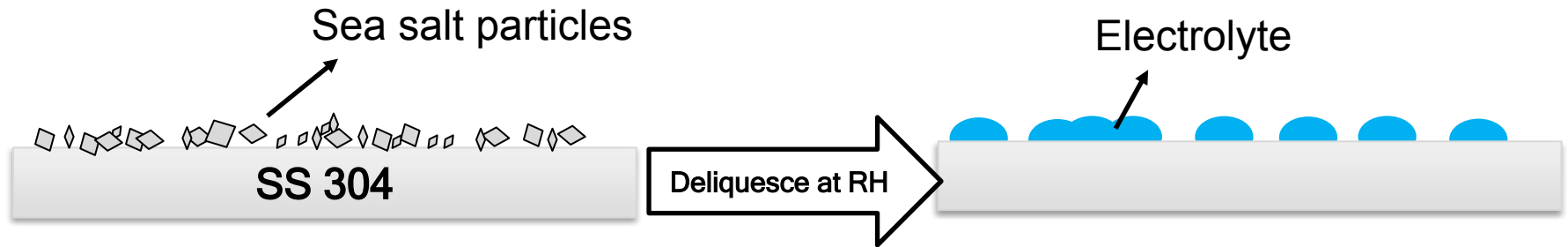
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Research in Progress - EAC

*This work is supported at the Ohio State University by Sandia National Laboratories (SNL). SNL is managed and operated by NTESS under DOE NNSA contract DE-NA0003525. Sandia National Laboratories is a multi-mission laboratory managed and operated by National Technology and Engineering Solutions of Sandia, LLC., a wholly owned subsidiary of Honeywell International, Inc., for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-NA0003525. This document*

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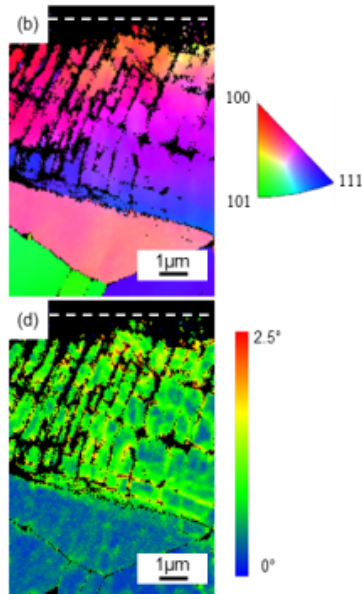
# 304 SS used for SNF storage exposed to corrosive atmospheres



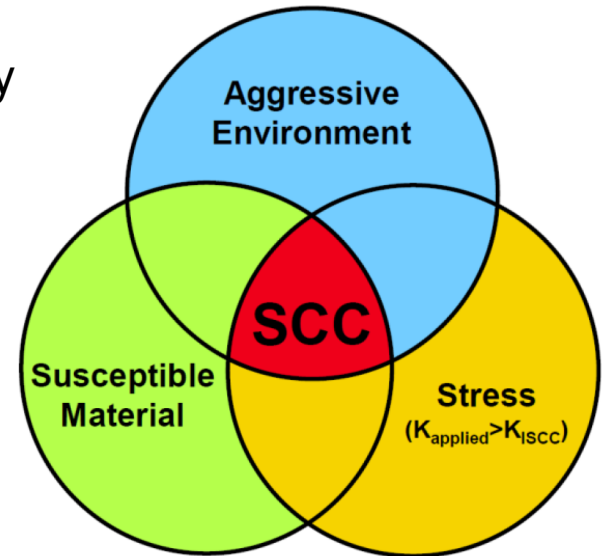
RH	$[\text{Cl}^-]$ ( $\text{mol} \cdot \text{kg}^{-1}$ )	$[\text{Na}^+]$ ( $\text{mol} \cdot \text{kg}^{-1}$ )	$[\text{Mg}^{2+}]$ ( $\text{mol} \cdot \text{kg}^{-1}$ )
40%	10.45	0.18	5.33
76%	5.65	4.85	0.54

High chloride concentration in electrolyte leads to pitting risk

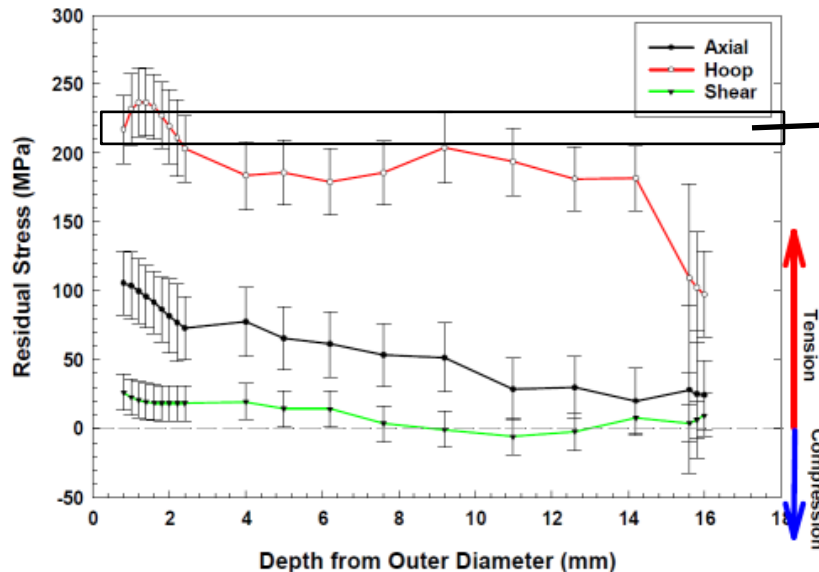
# SCC risk present when 304 SS exposed to corrosive atmospheres



Deformation from grinding may create susceptible subsurface microstructure



Weirich et al. JECS (2019).



Yield strength for annealed 304 SS

Residual stress variation in SNF canister material shows through-crack propagation likely if initiation occurs

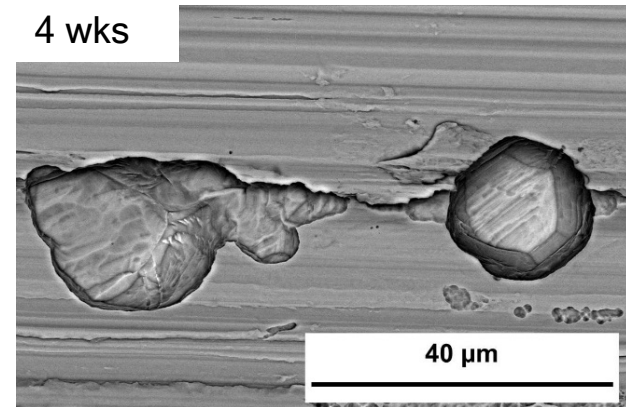
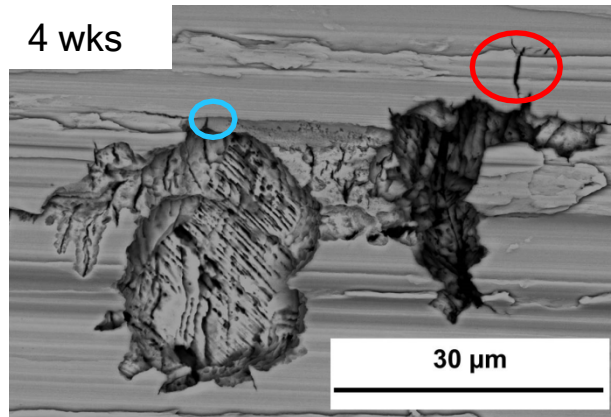
# Exposure to high and low RH leads to different pit morphology in 304 SS

40% RH

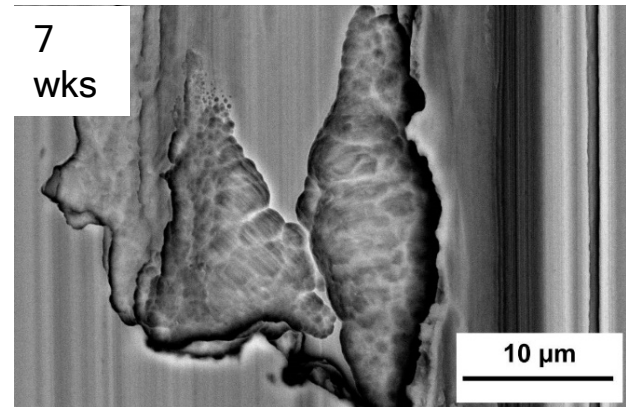
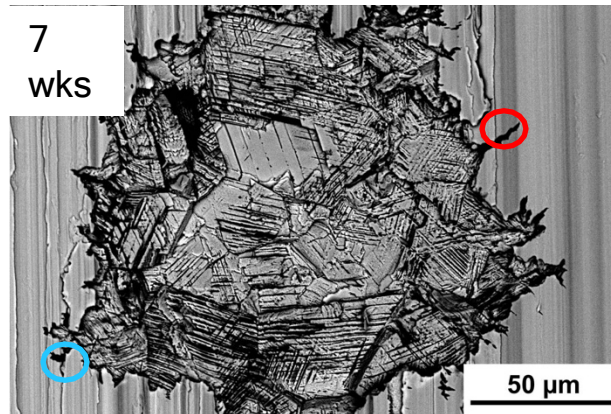
76% RH

Atmospheric exposures

35 °C



Full immersion exposures in eq. brines



cross-hatched pits,  
microcracks, fissures

Ellipsoidal, faceted pits

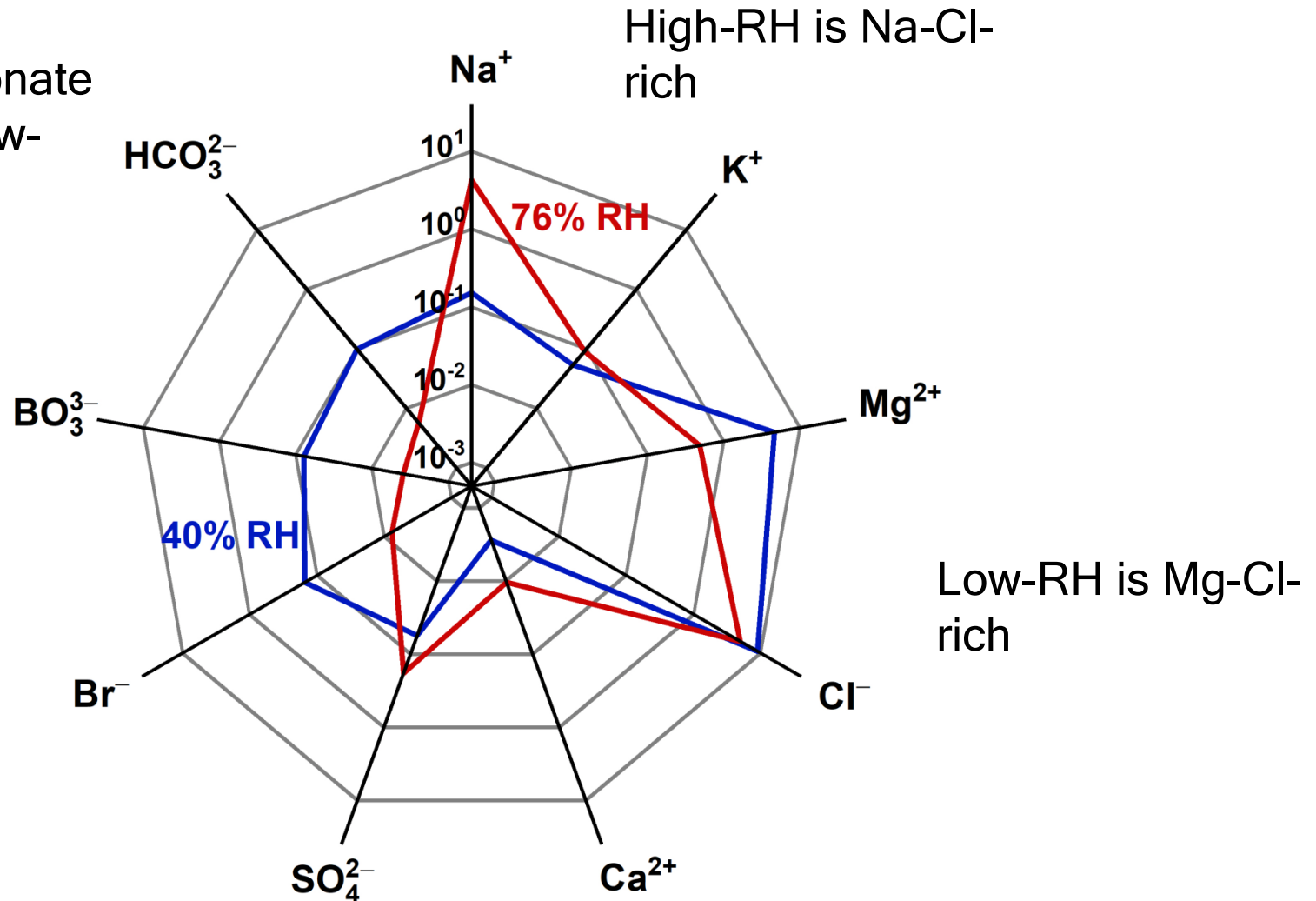
<sup>1</sup>Weirich et al., J. Electrochem. Soc. 166 (2019).

<sup>2</sup>Srinivasan et al., J. Electrochem. Soc. 168 (2021).



# Differences in electrolyte chemistry may be responsible for morphology differences

Higher carbonate species in low-RH brines

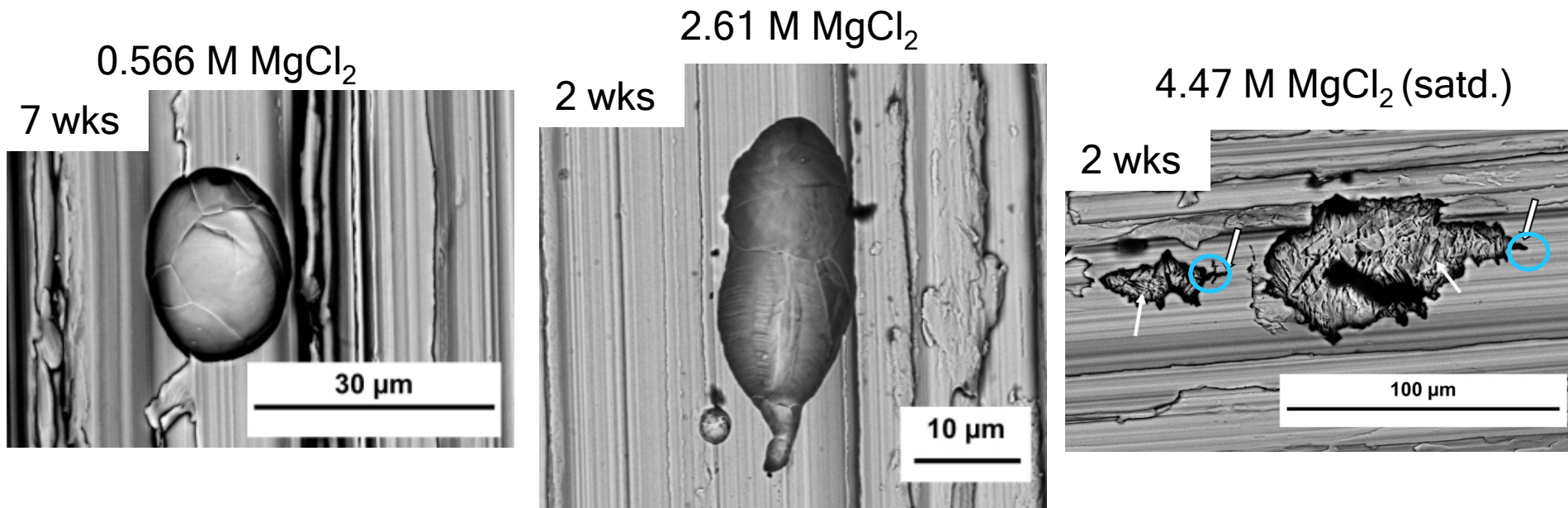


# Full immersion exposures performed at 35 °C in simulated sea salt brines

Solution	[Cl <sup>-</sup> ]/M	[HCO <sub>3</sub> <sup>-</sup> ]/M
40% RH equivalent sea salt brine	9.003	$9.79 \times 10^{-2}$
0.566 M MgCl <sub>2</sub>	1.132	$1.37 \times 10^{-5}$
2.61 M MgCl <sub>2</sub>	5.22	$1.60 \times 10^{-5}$
4.47 M MgCl <sub>2</sub>	8.94	$3.08 \times 10^{-5}$
76% RH equivalent sea salt brine	5.009	$5.73 \times 10^{-3}$

Note: These are model-calculated values of ionic concentrations. Actual measured values may be lower due to repeated filtering of precipitates prior to use in testing.

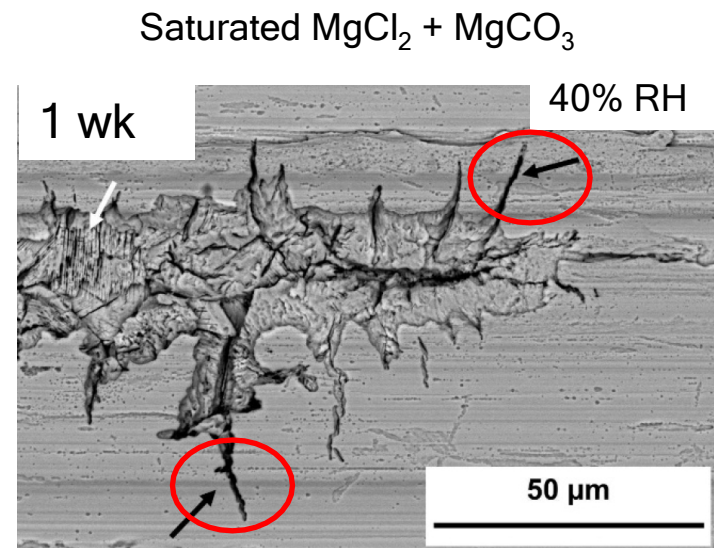
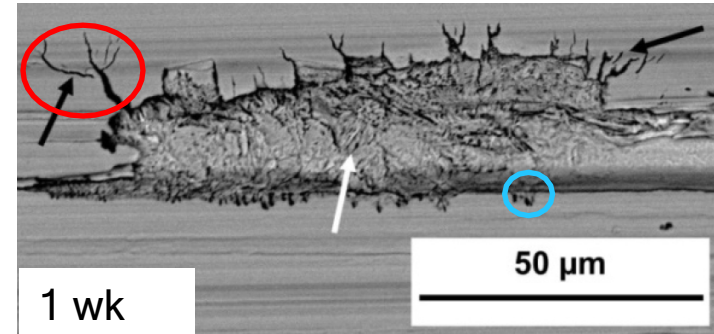
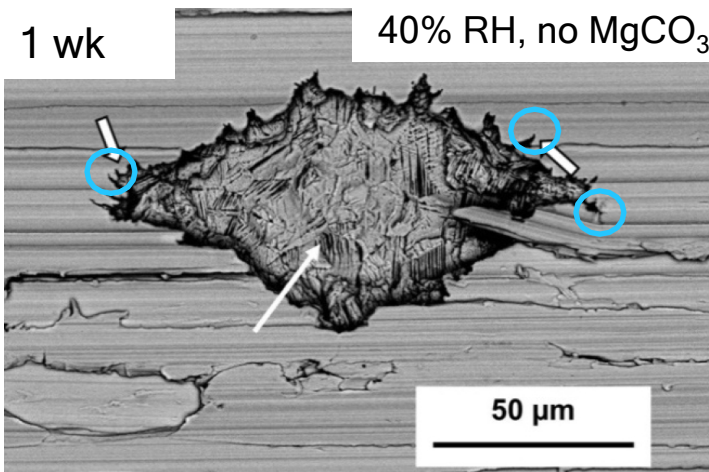
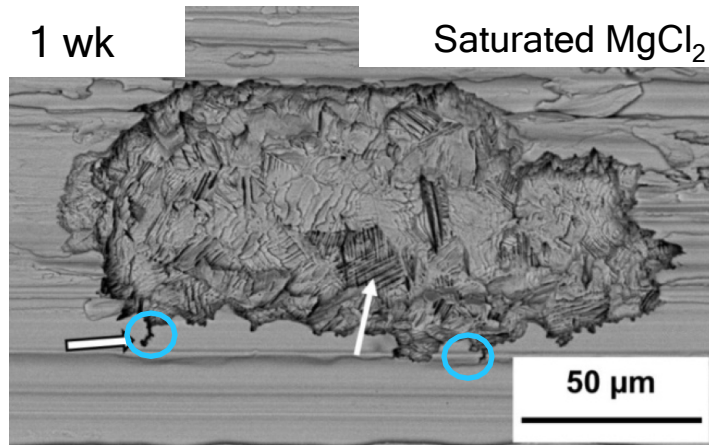
# [MgCl<sub>2</sub>] influences pit morphology



Concentrations < saturation show ellipsoidal, faceted pits

Saturated MgCl<sub>2</sub> shows cross-hatching, fissures

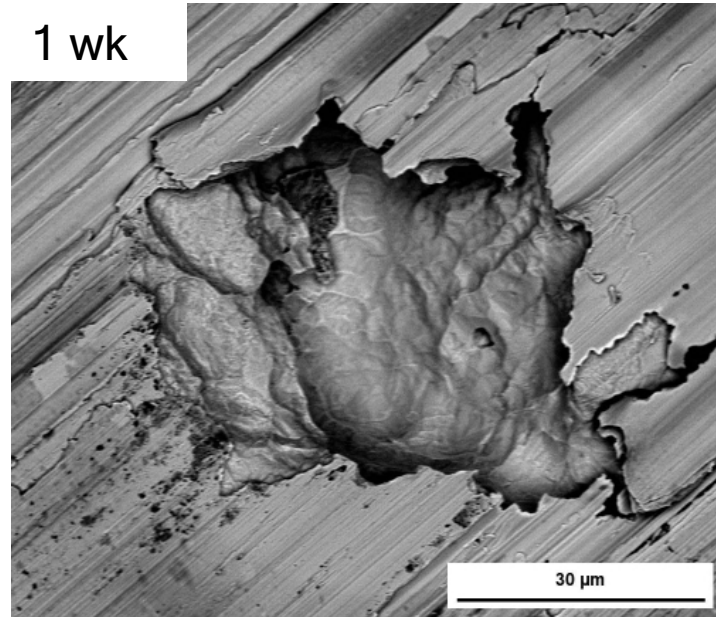
# High level of dissolved carbonates may be necessary for microcracks



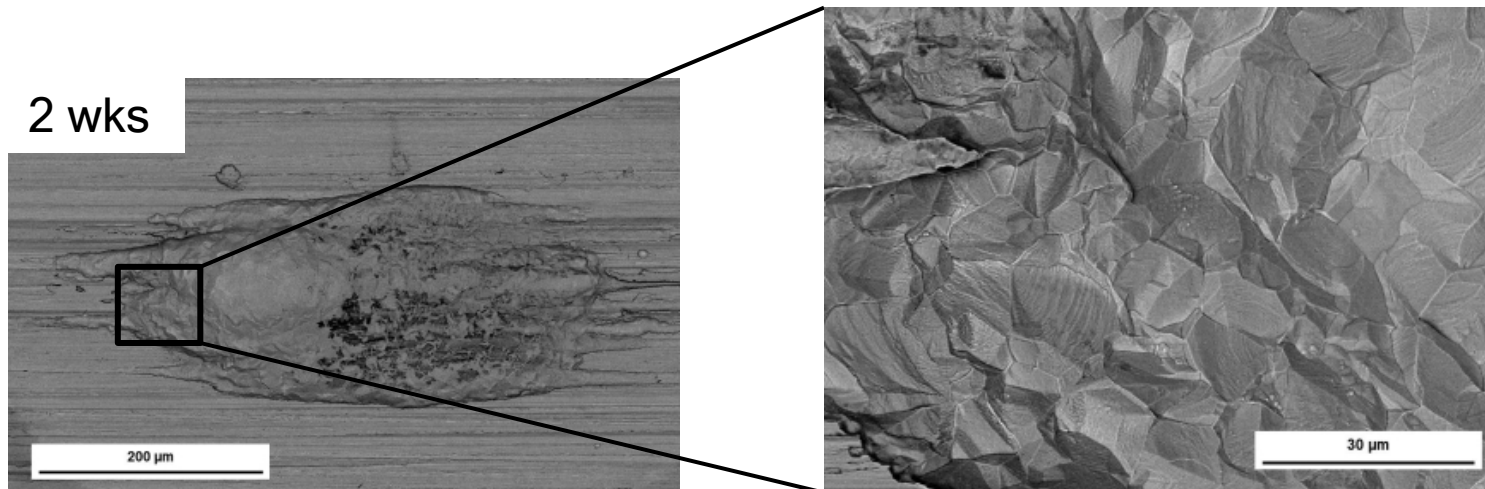
Microcracking may be linked to high levels of dissolved carbonates  
Insufficient dissolved carbonate → no prominent microcracking

Dissolved carbonate alone does not produce microcracks,  
sat.  $\text{MgCl}_2$  also necessary

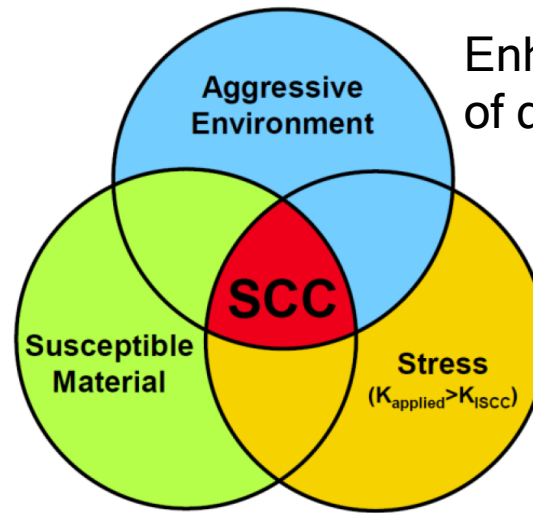
2.61 M  $\text{MgCl}_2$  +  
 $\text{MgCO}_3$



Cross-hatching  
resulting from sat.  
 $\text{MgCl}_2$  may be  
synergistic with  
microcracking



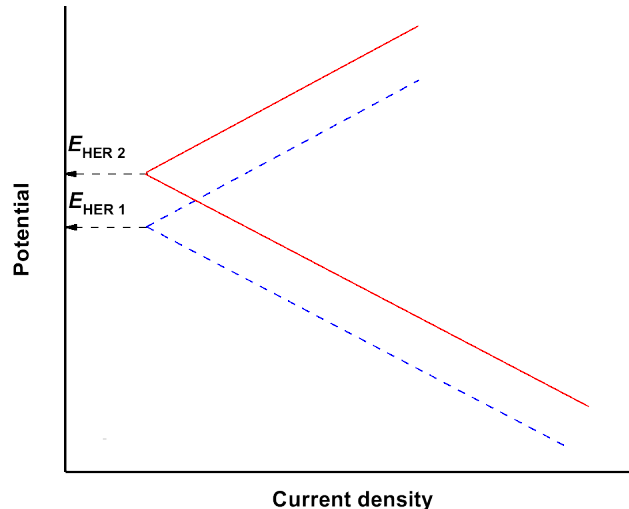
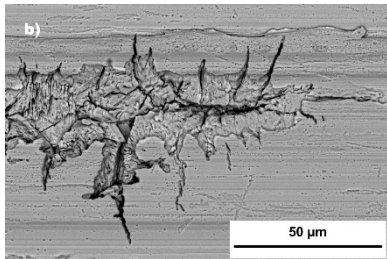
# Can micro-cracking occur via HEAC at low RH?



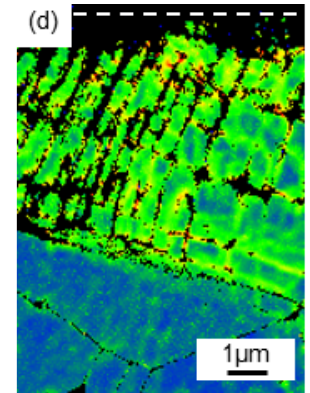
Enhanced HER due to action of dissolved carbonate

Strain-induced martensite from surface grinding

Residual stress, cross-hatching may act as stress concentrator



Accelerated HER from high carbonate level



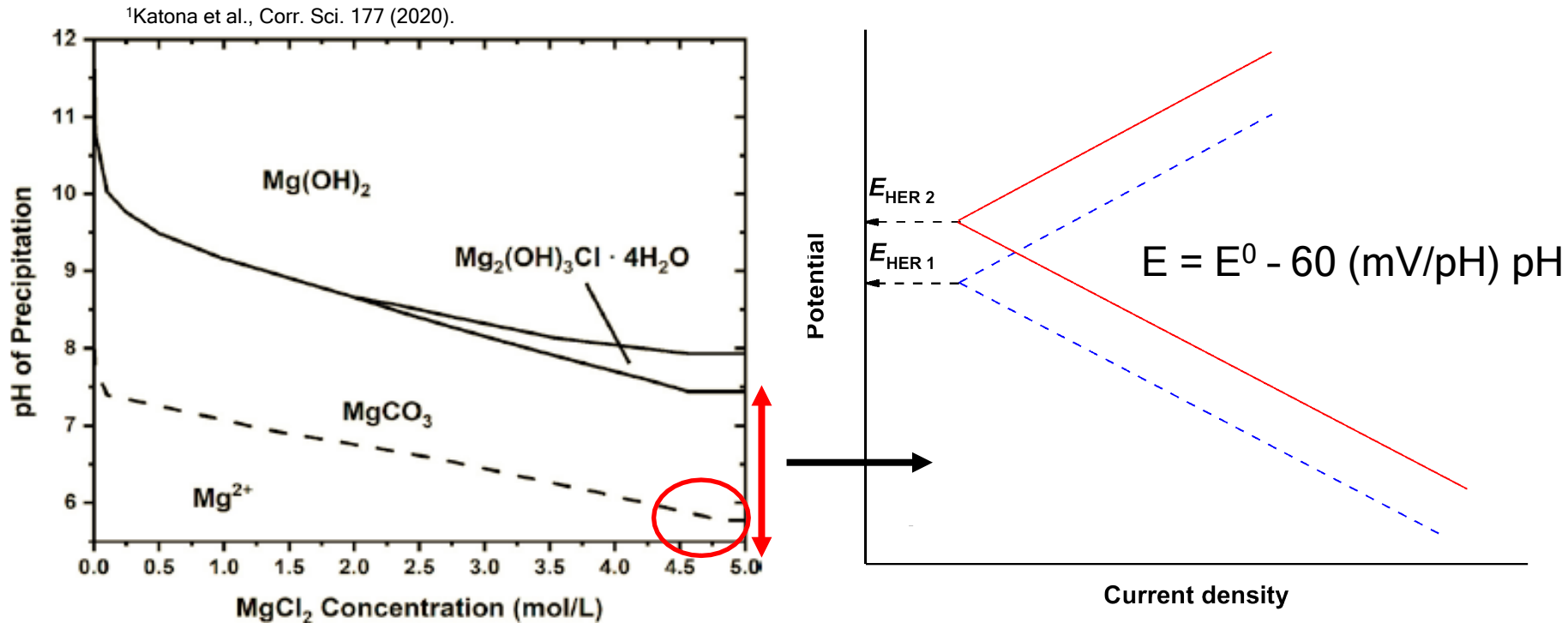
Weirich et al. JECS (2019).

Sufficient residual stress, SI martensite

Stress concentration from cross-hatching



# HER kinetics may be accelerated by precipitate buffering action of magnesium-hydroxide-carbonate phases



Dissolved carbonate species to precipitate at cathodic sites buffering to lower pH

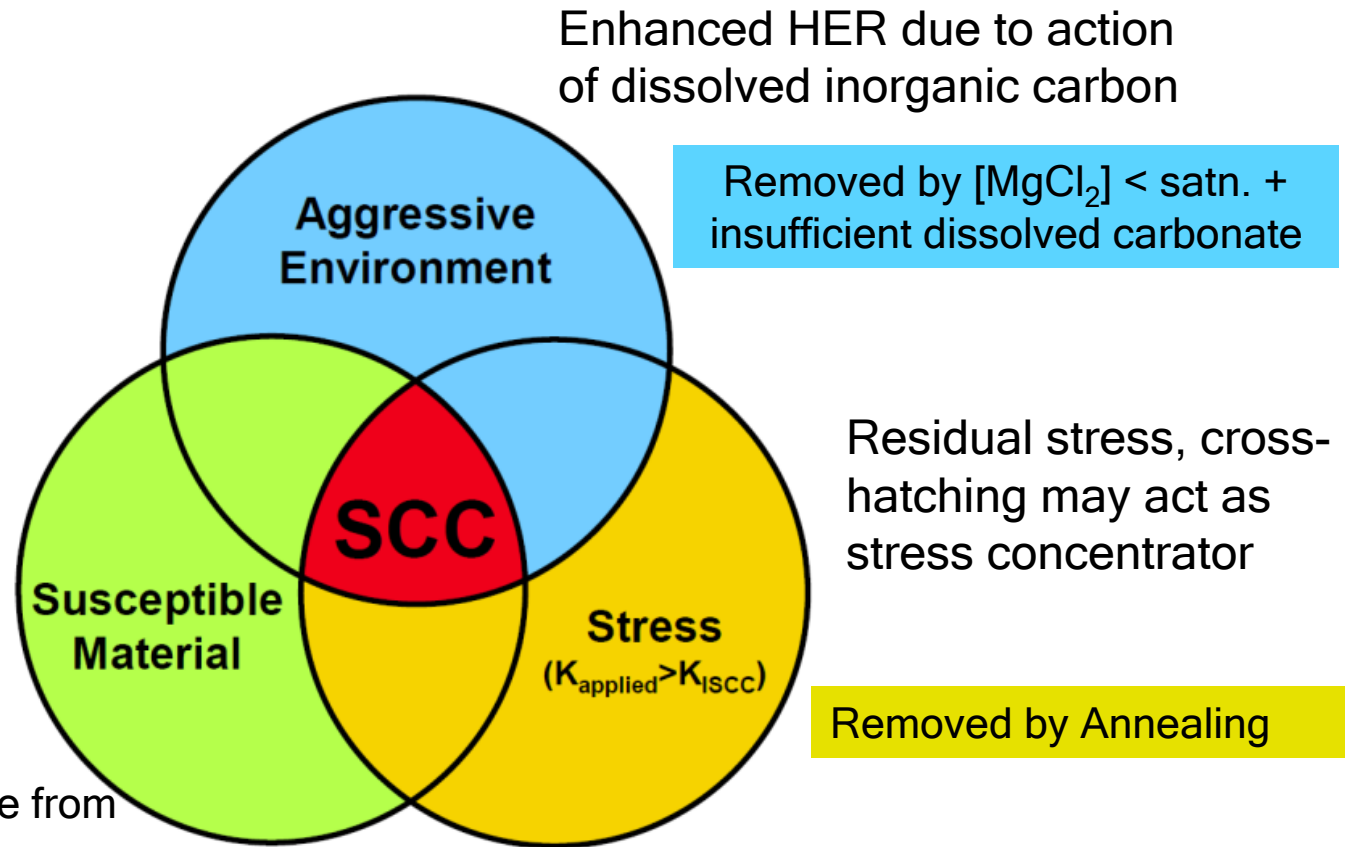
Lower pH raises HER Nernst potential, enhances kinetics

Exact species precipitating/buffering is kinetics-dependent -  $\text{MgCO}_3$  precipitation kinetically hindered<sup>2,3</sup>

<sup>2</sup>Katona et al., Echem. Comm. 118 (2020).

<sup>3</sup>Swanson et al., PCCP 16(42) (2014).

# Systematic evaluation of factors

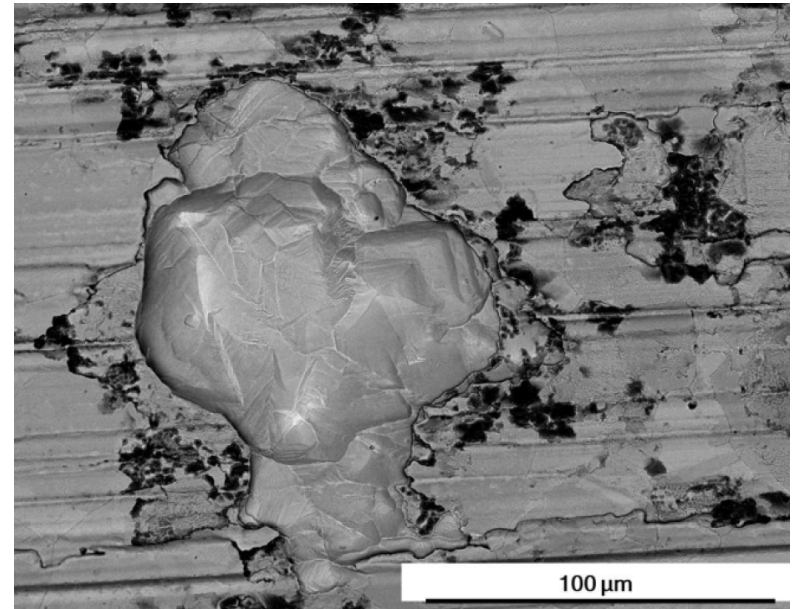
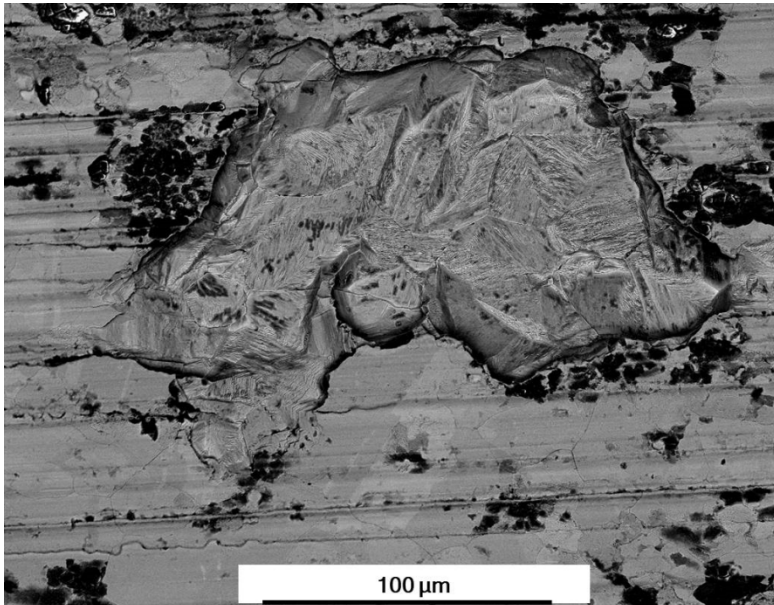


Removed by  
Annealing

Strain-induced martensite from  
surface grinding

# Microcracking not seen in annealed samples

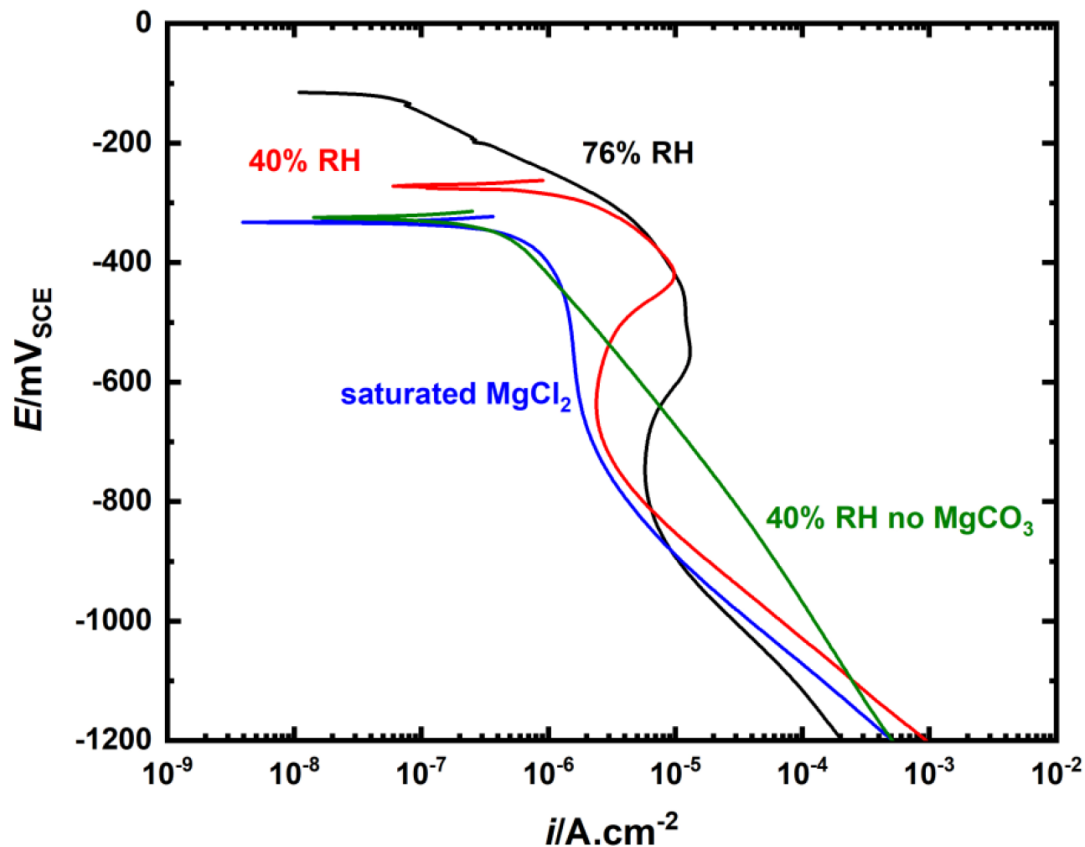
Samples solutionized at 1050 °C for 1 h and then exposed to 40% RH for 1 week at 35 °C



Few pits seen, occasionally in clusters, typically ellipsoidal and faceted

NO microcracks observed

# Cathodic kinetics may suggest precipitation in carbonate-rich brines



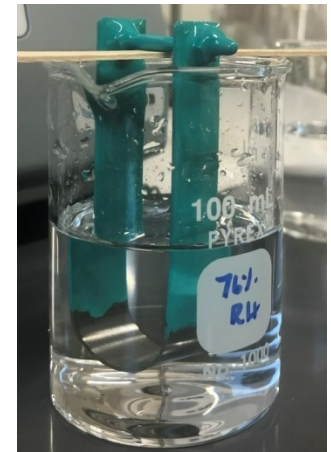
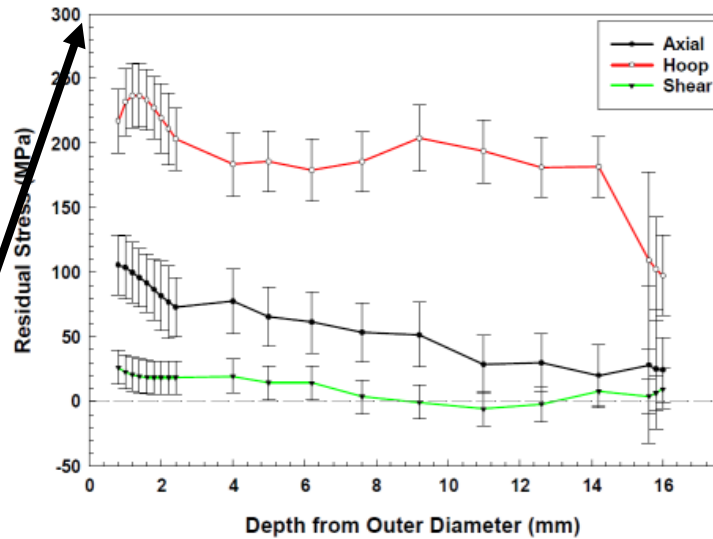
HER effects on morphology may be slow-acting, long-term - not likely captured by short scan duration

# U-bend tests ongoing - can large-scale cracking result from immersion in seawater brines?

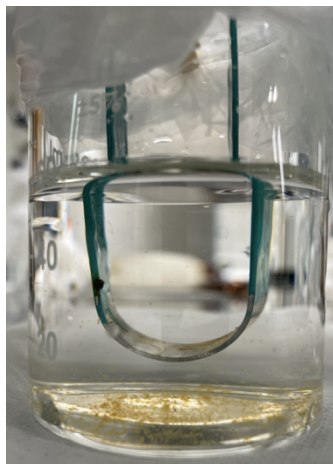
304SS at 35 °C

Strain on outer bend = 4% (ASTM G-30)

Stress on outer bend  $\approx$  300 MPa



Enos and Bryan, SNL Report, 2016.



76% RH after 5 days



40% RH after 5 days

# Key takeaway points

- Microcracking observed in low-RH brines correlates with subsurface SI martensite + residual stress + cross-hatching + dissolved carbonates
- HER may be enhanced at cathodic sites as Mg-species ppt buffer near-surface pH to lower values
  - Cathodic kinetics in carbonate-rich  $\text{MgCl}_2$  solutions suggest precipitation effects
- Annealing removes microcracking tendency
  - Removal of SI martensite, residual stress results in no microcracking



# Next steps

- Cathodic kinetics after longer-term exposure to evaluate if HER acceleration is time-dependent
- Continuing U-bend immersion tests

# Acknowledgments

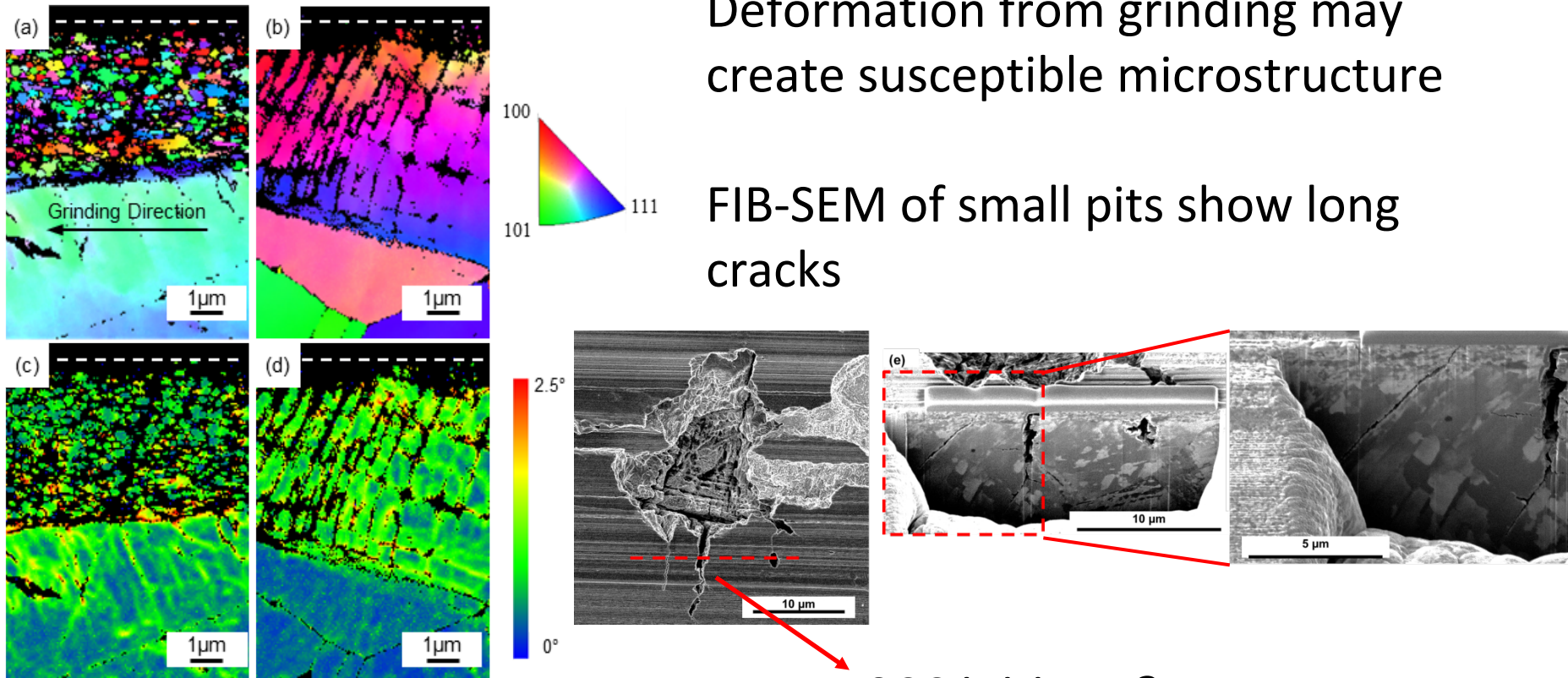
- This work is supported at the Ohio State University by Sandia National Laboratories (SNL). SNL is managed and operated by NTESS under DOE NNSA contract DE-NA0003525.
- The support of the Momental Foundation through the Mistletoe Research Fellowship 2020-2021 in purchasing equipment used in the study is acknowledged.
- Thanks to Andrew Knight, SNL, for assistance in calculation of ionic concentration using the EQ 3/6 software and the Pitzer parametrization.
- Thanks to Rashed Alazemi, graduate student, Fontana Corrosion Center, OSU for assistance with monitoring U-bend immersion experiments.

# SUPPLEMENTAL

# Deformation substructure may contribute to susceptible morphology

Deformation from grinding may create susceptible microstructure

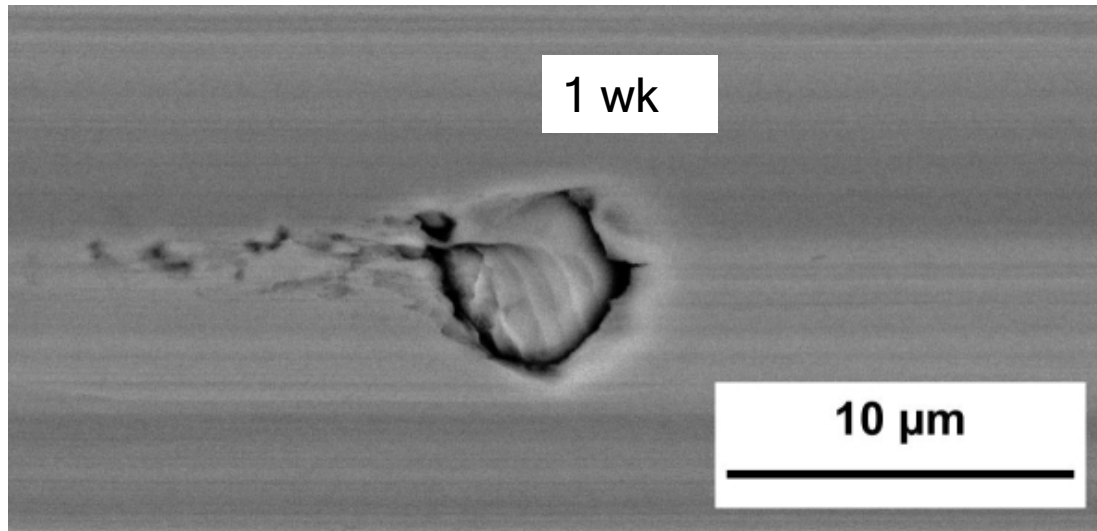
FIB-SEM of small pits show long cracks



SCC initiator?

Dissolved inorganic carbon by itself does not produce microcracks, likely synergistic with cross-hatching

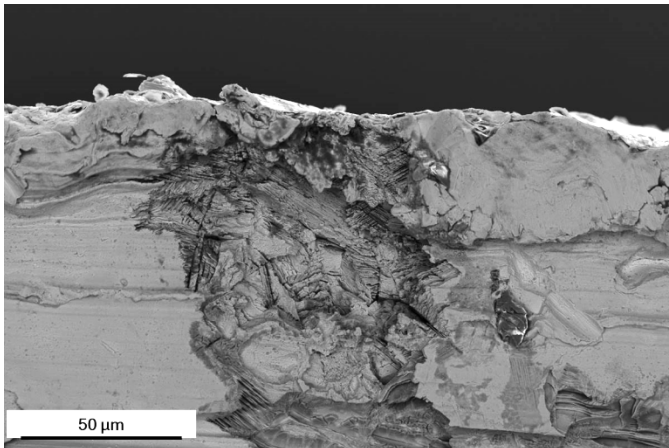
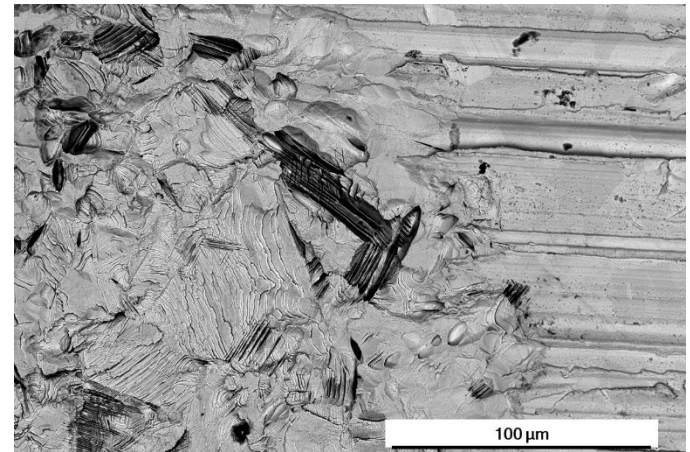
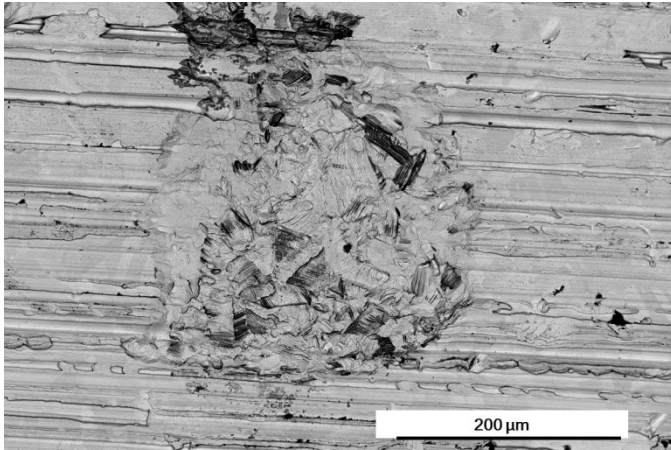
Saturated  
NaCl +  
MgCO<sub>3</sub>



40% RH sea salt brine without MgCO <sub>3</sub> addition	3.39	9.003	$2.82 \times 10^{-5}$
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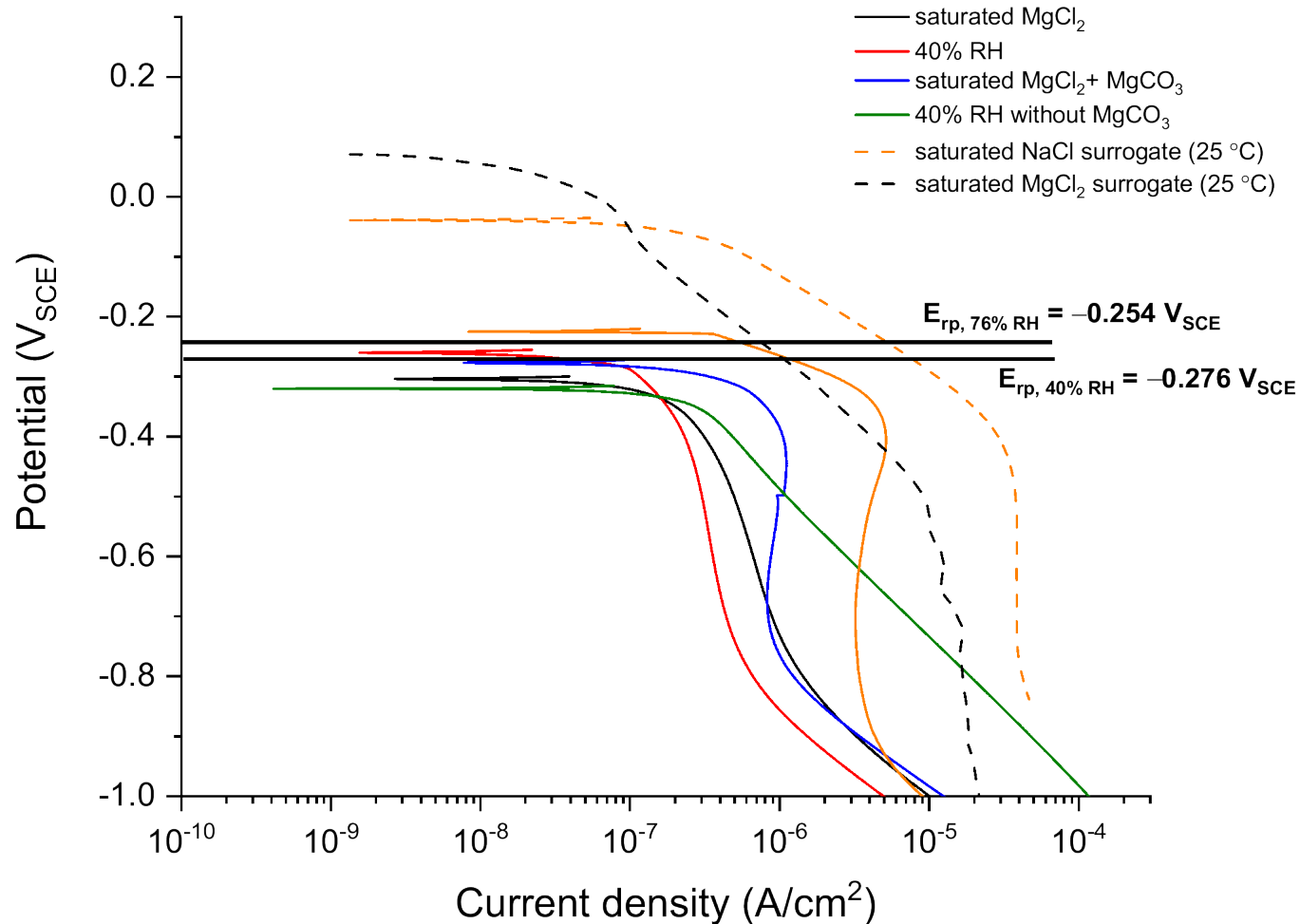
5.22 M NaCl	5.187	5.22	$5.09 \times 10^{-6}$
5.22 M NaCl + added MgCO <sub>3</sub>	8.61	5.22	$7.29 \times 10^{-3}$

4.47 M MgCl <sub>2</sub> + added MgCO <sub>3</sub>	7.07	8.94	$4.55 \times 10^{-2}$
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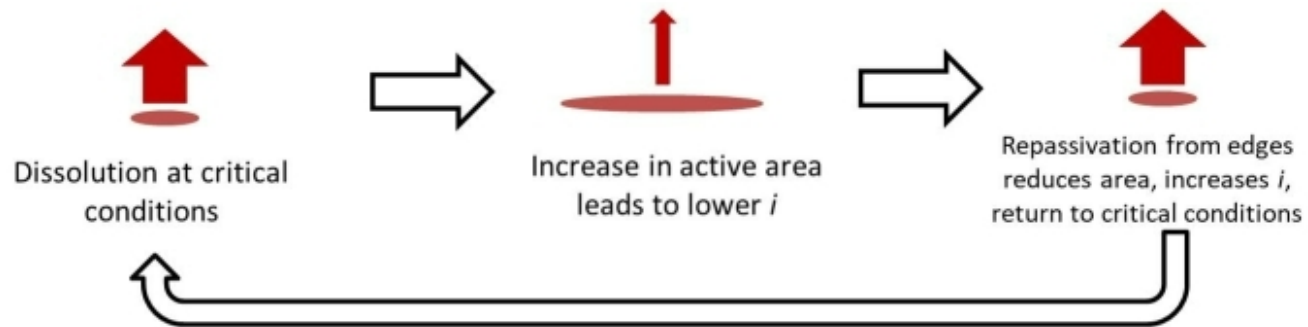


Solutions containing sat.  $\text{MgCl}_2$  have an OCP very close to  $E_{\text{rp}}$  at 40% RH, cathodic kinetics trend not conclusive of HER acceleration



# Cathodic current availability determines polarization levels, morphology

Low RH: Growth close to repassivation limits area for dissolution → fixed active area



High RH: Growth at conditions between critical stability and saturation with increasing active area

