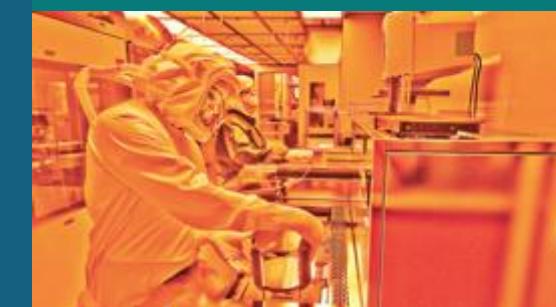




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High-Fidelity CFD Workshop 2022: Blottner Sphere and HiFire I problem overview



PRESENTED BY

Travis Fisher

2022 AIAA 1st High-Fidelity CFD Workshop

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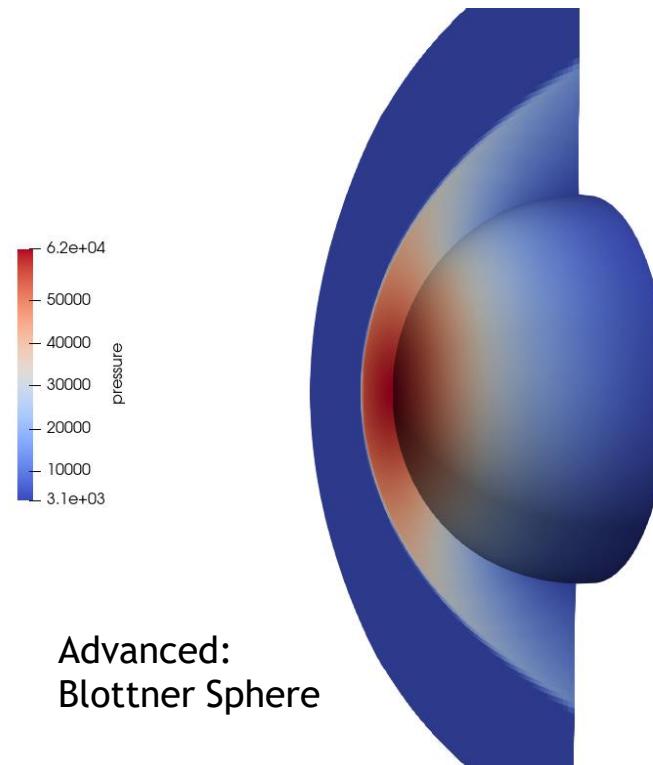
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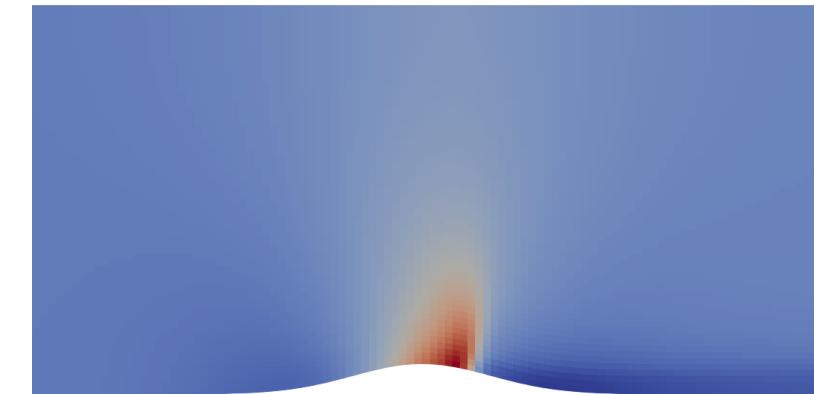
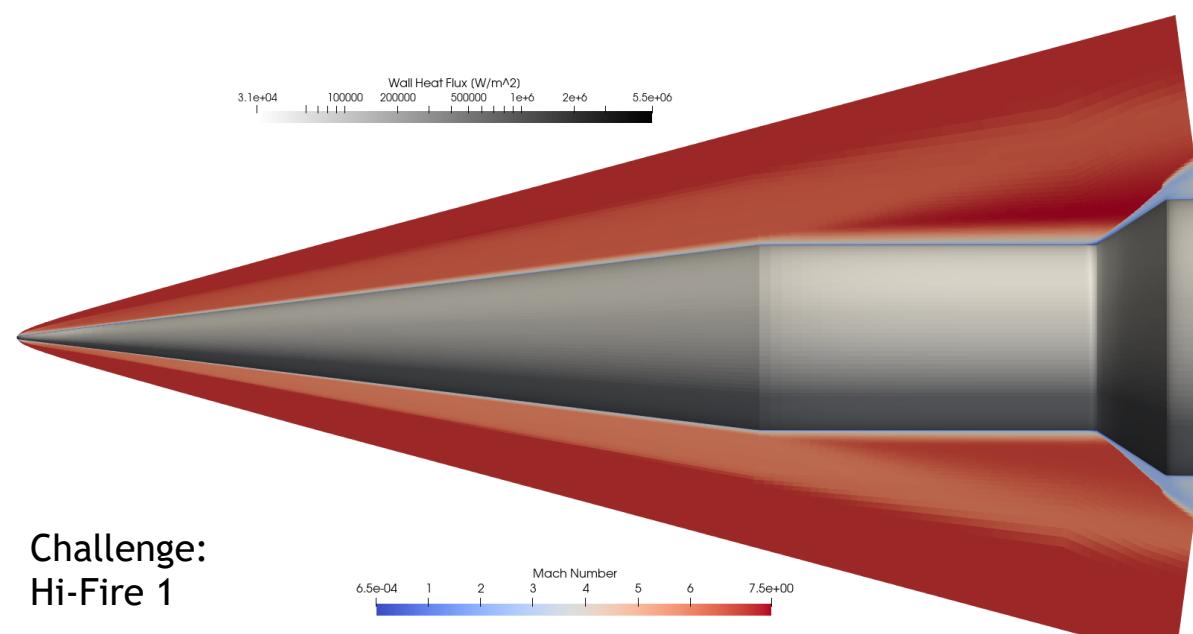
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Workshop Cases

Visit workshop website for up-to-date case descriptions and meshes: https://turbmodels.larc.nasa.gov/highfidelitycfd_workshop2022.html



Challenge:
Hi-Fire 1



Verification:
Supersonic Inviscid Bump

3 Blottner Sphere Problem Info



Viscous flow around half sphere

Sensitive to numerical methods

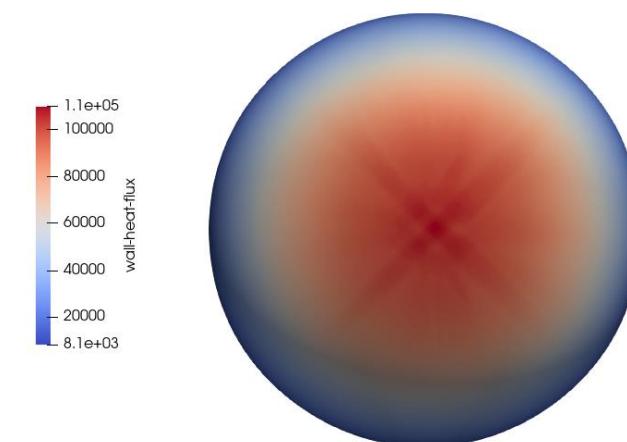
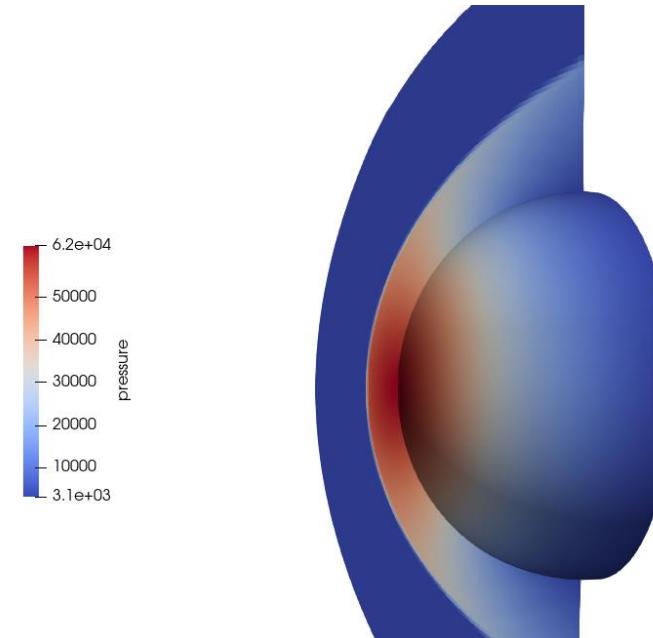
- Entropy fix
- Shock alignment
- Limiters

Run full 3D problem

Meshes provided

- Structured multi-block
- Unstructured hex, including curved high-order
- Unstructured tet, including curved high-order

Specific Heat Ratio, γ	1.4
Mach Number, Ma	5.0
Reynolds Number, Re_D	1.8875×10^6
Prandtl Number, Pr	0.72
Wall Temperature Ratio, T_w/T_∞	1.308



Blottner Sphere Required Outputs



Stagnation heat flux

Integrated wall heat flux

Wall heat flux profiles

- Intersecting x-y plane
- Intersecting 45 degrees rotation from x-y plane

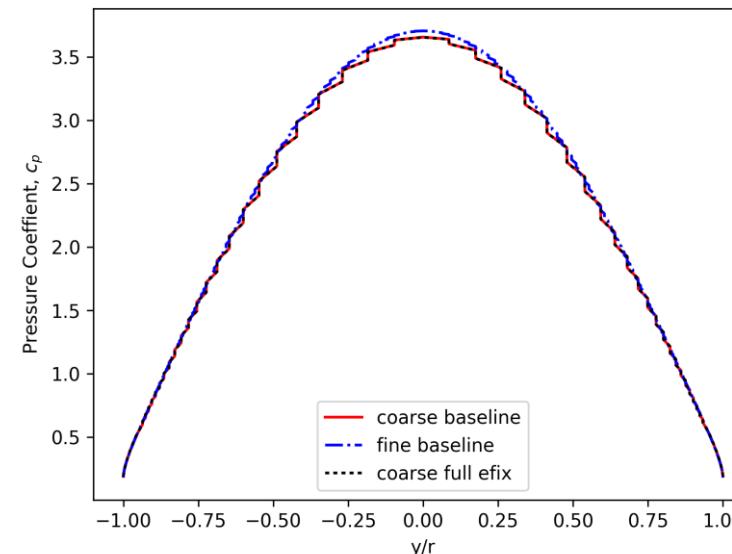
Static pressure

- Intersecting x-y plane
- Intersecting 45 degrees rotation from x-y plane

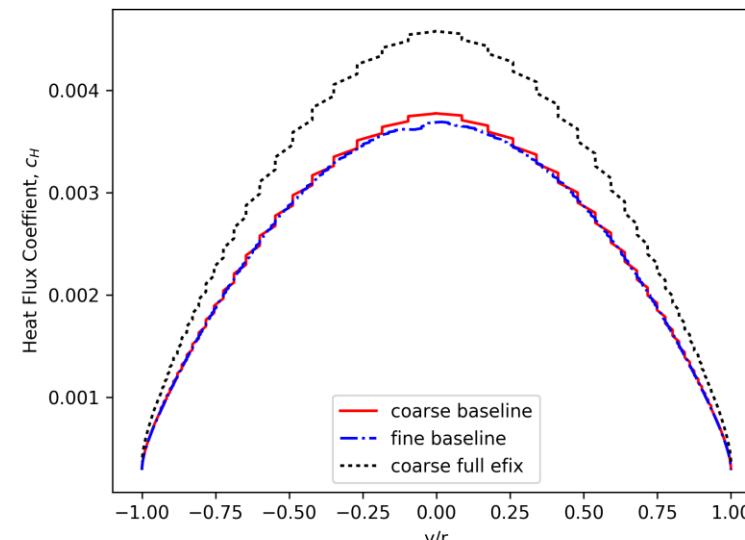
Stagnation streamline pressure

Stagnation streamline temperature

Work units for each solution



Pressure coefficient along the intersection of the surface and the x-y plane for three different simulations



Heat flux coefficient along the intersection of the surface and the x-y plane for three different simulations

5 Hi-Fire I Problem Description



Mach 7.2 flow around more complex geometry

Goal is to demonstrate convergent, cross-solver heat flux predictions of laminar and turbulent sections

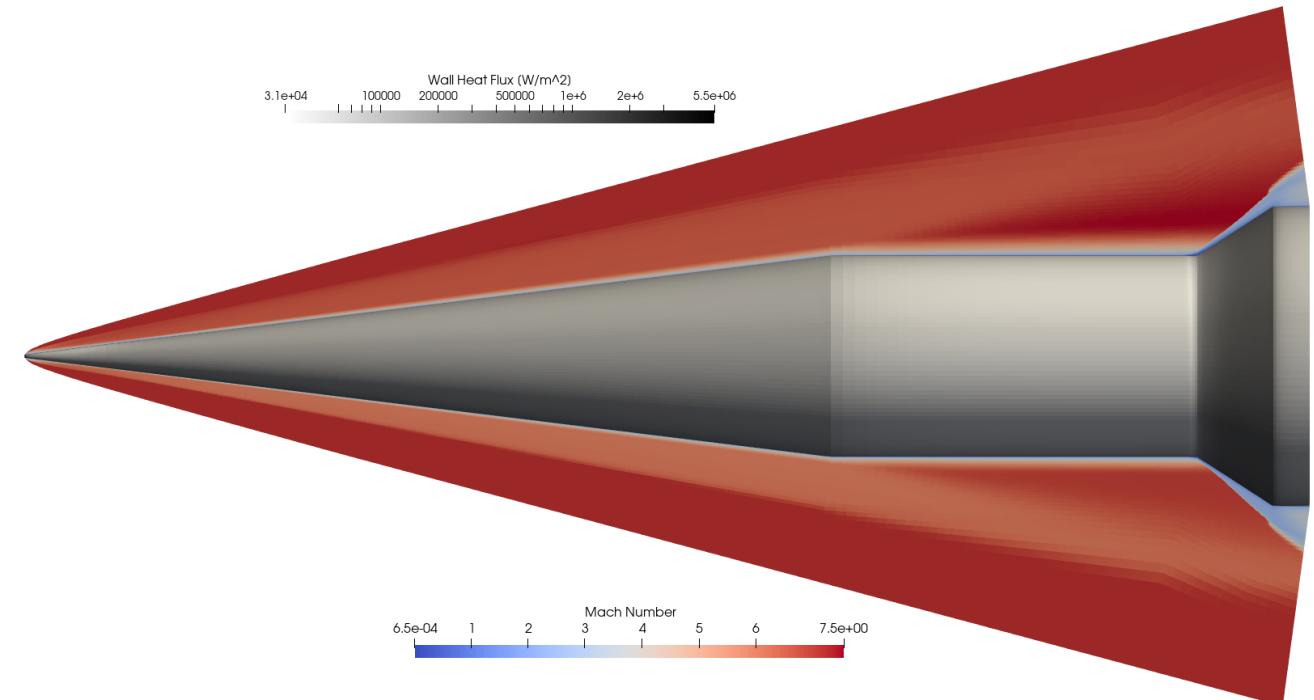
- Laminar simulation over conical forebody
- Fully turbulent simulation using SA-negative model over entire geometry

Need half geometry to predict with 2 degree AOA

Meshes provided

- Structured multi-block
- Unstructured hex, including curved high-order
- Unstructured tet, including curved high-order

Specific Heat Ratio, γ	1.4
Mach Number, Ma	7.18
Freestream Reynolds Number, Re_∞	$10.123 \times 10^6 / m$
Prandtl Number, Pr	0.72
Angle-of-Attack, α	2°
Wall Temperature Ratio, T_w / T_∞	1.279

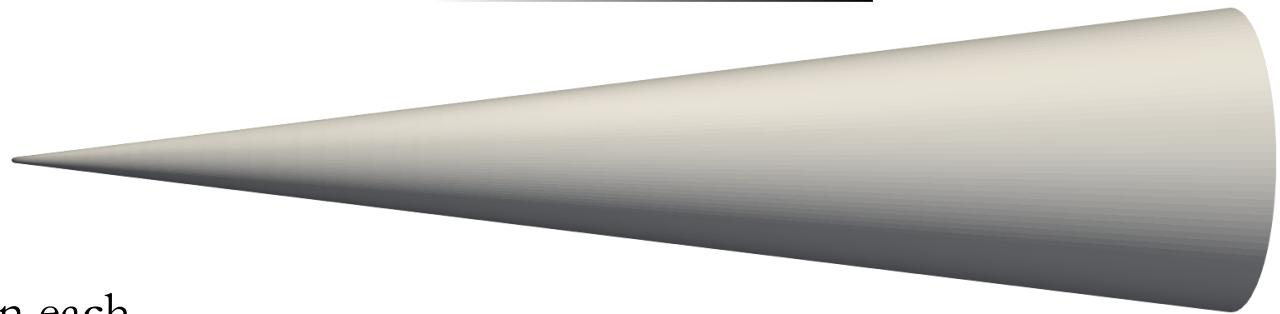
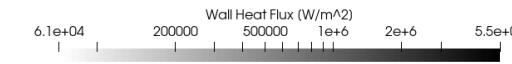


6 Hi-Fire I Required Outputs



Wall heat flux profiles for laminar and turbulent on each mesh

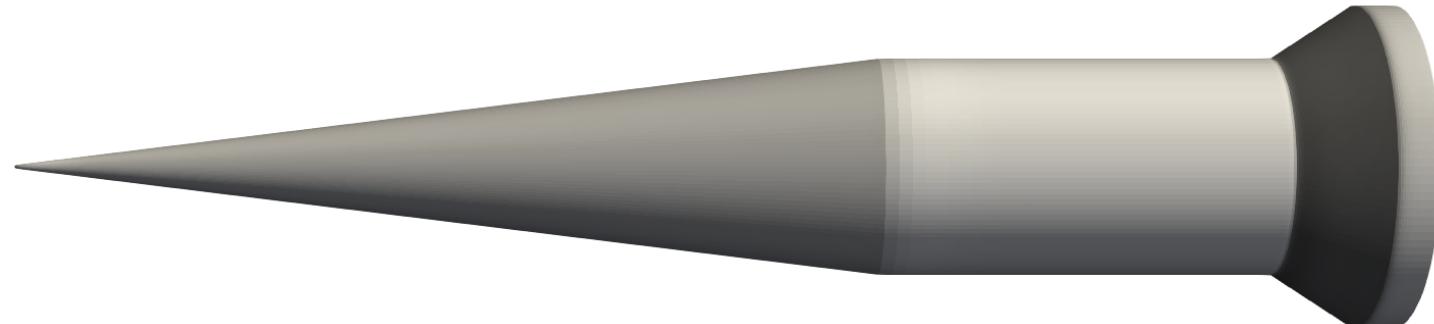
- Intersection with x-y plane on the windward side
- Intersection with x-y plane on the lee side
- Intersection of x-z plane



Wall Heat Flux Contour on laminar simulation of cone forebody

Static pressure profile for laminar and turbulent on each mesh

- Intersection with x-y plane on the windward side
- Intersection with x-y plane on the lee side
- Intersection of x-z plane



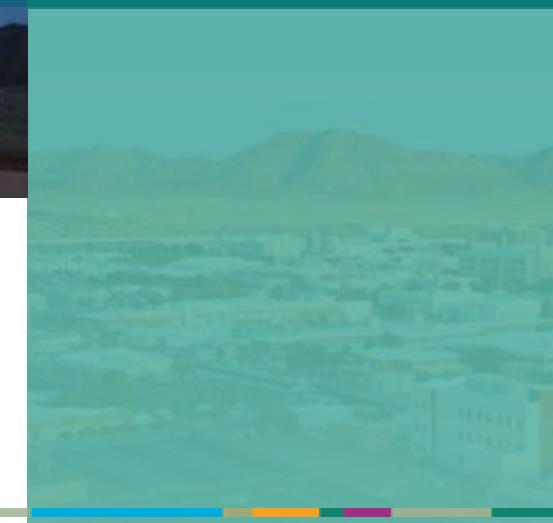
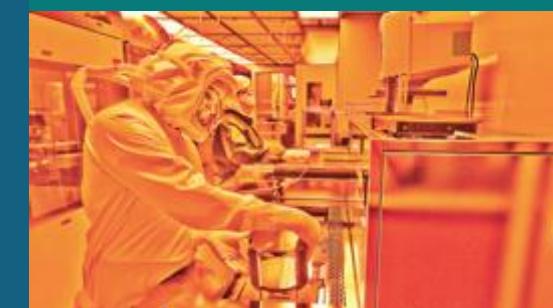
Wall Heat Flux Contour on fully turbulent simulation of entire geometry

Work units for each solution



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High-Fidelity CFD Workshop 2022: Blottner Sphere and HiFire I results



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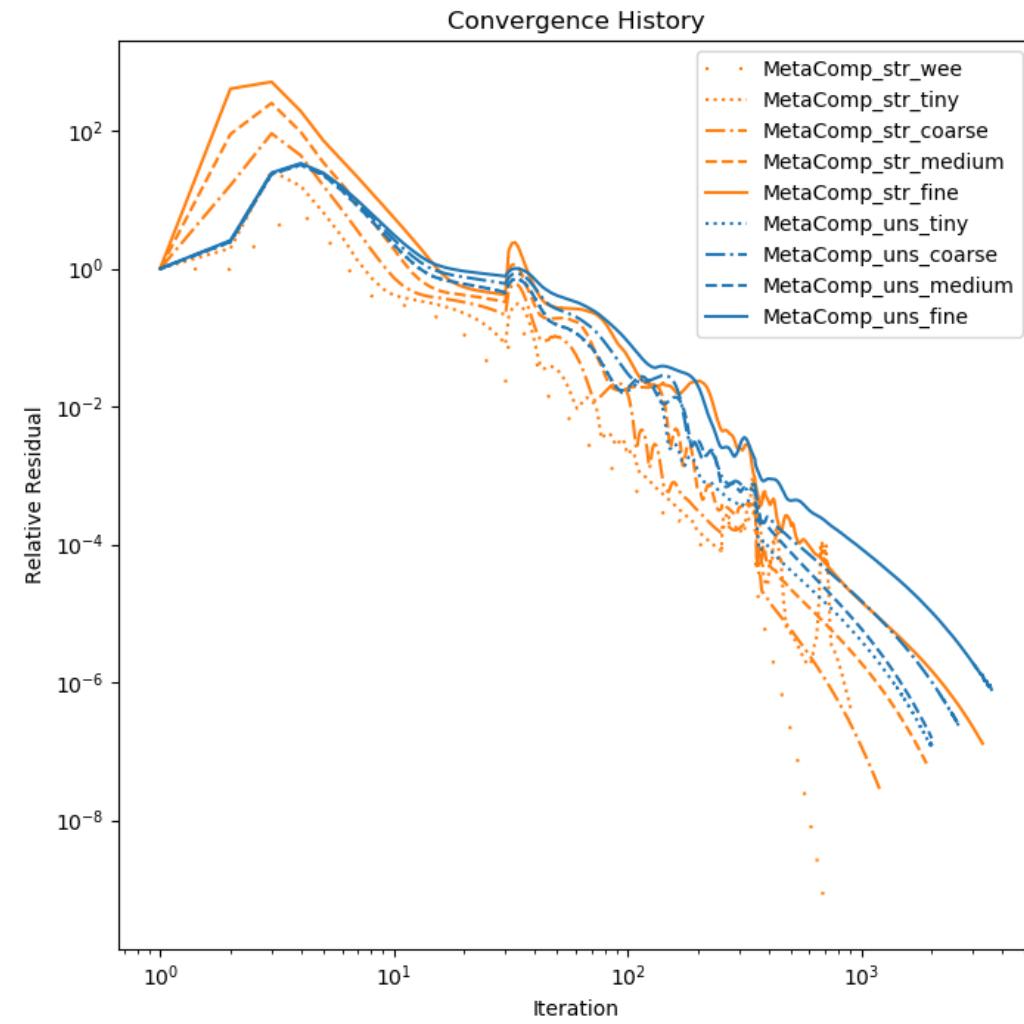
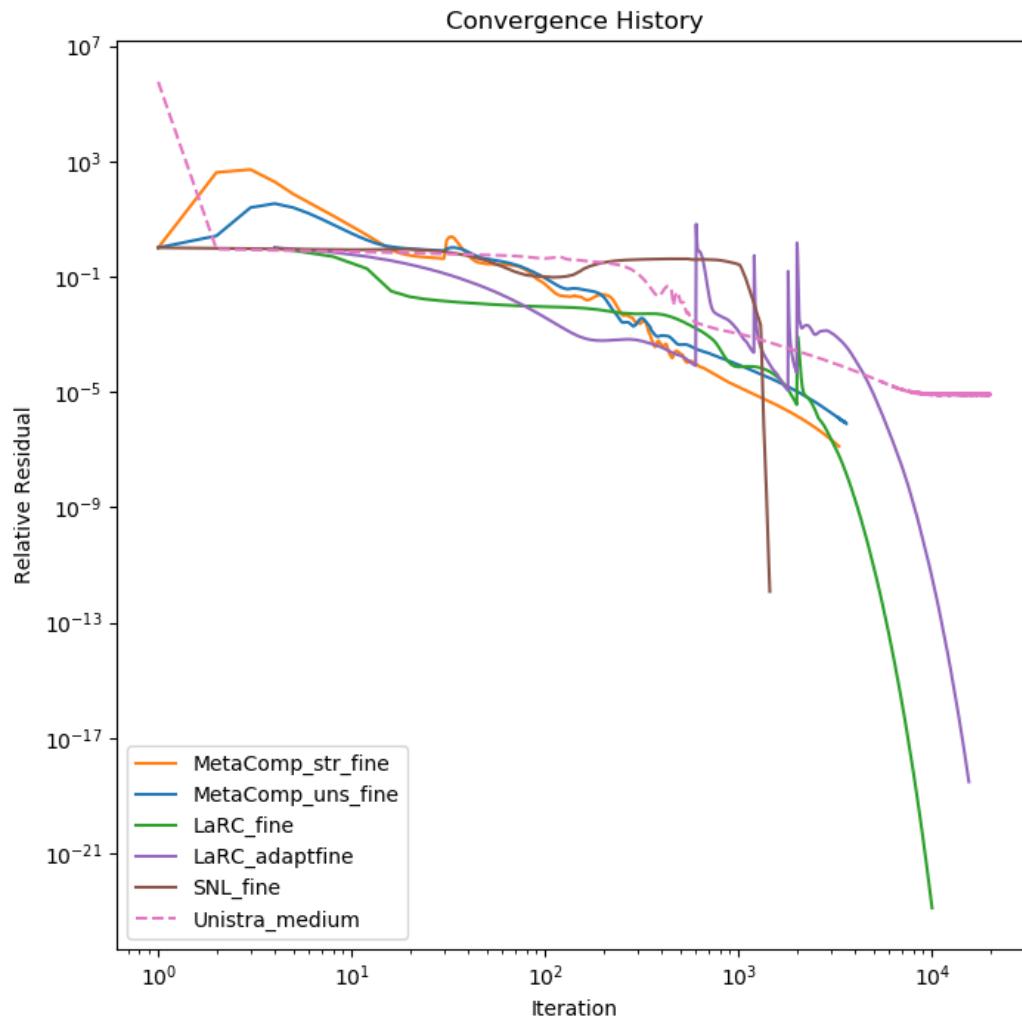
Travis Fisher

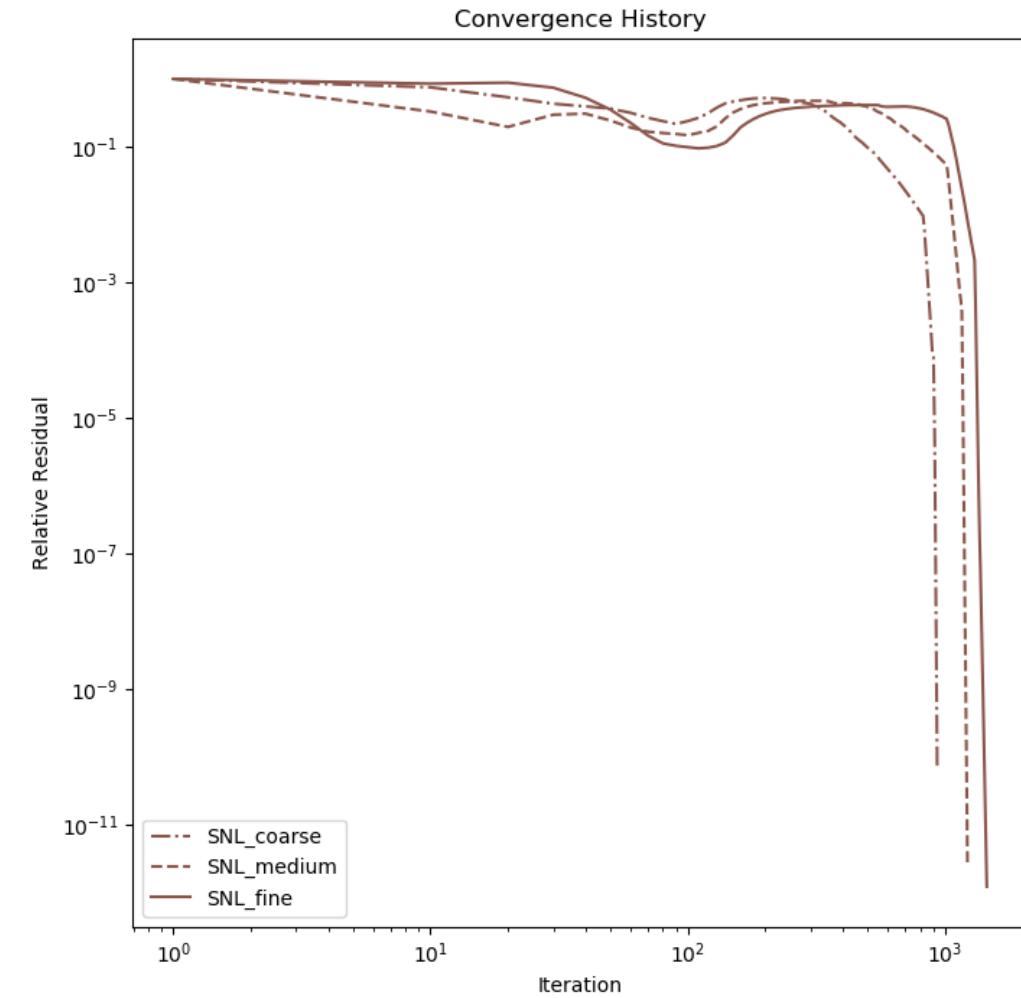
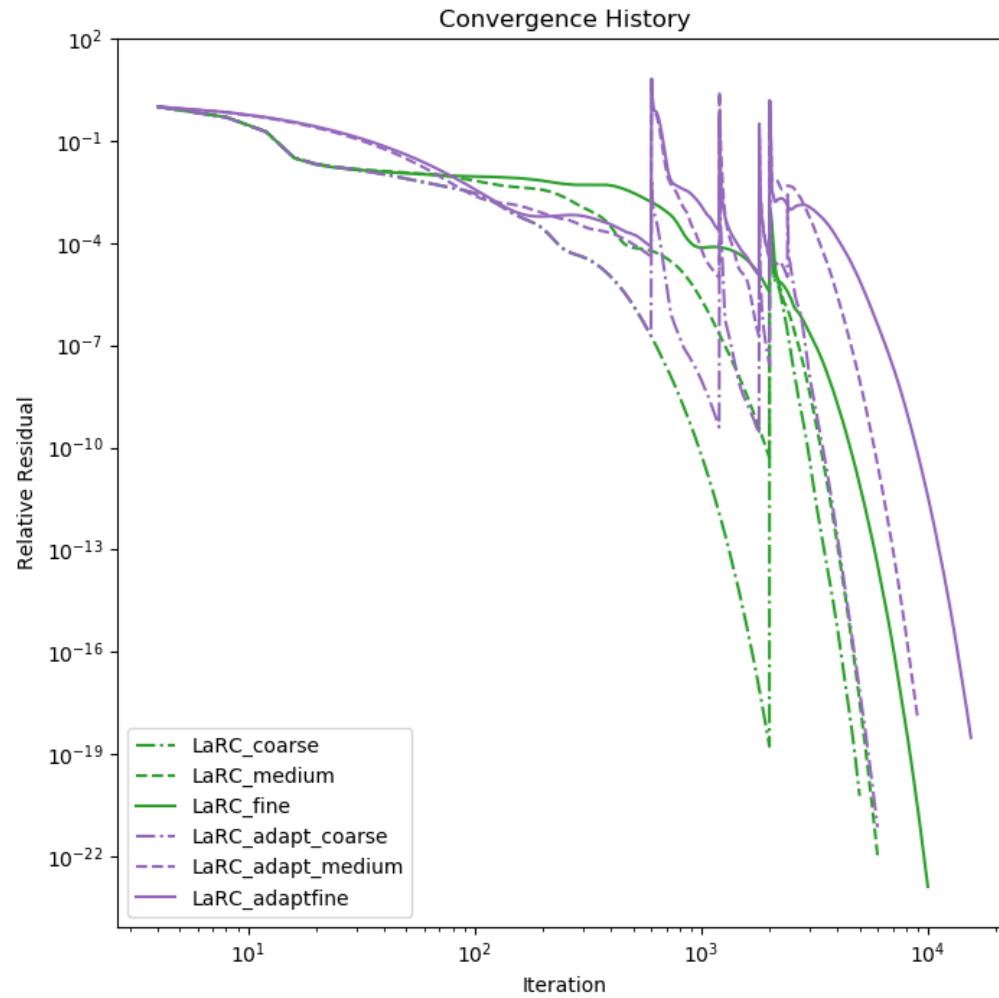
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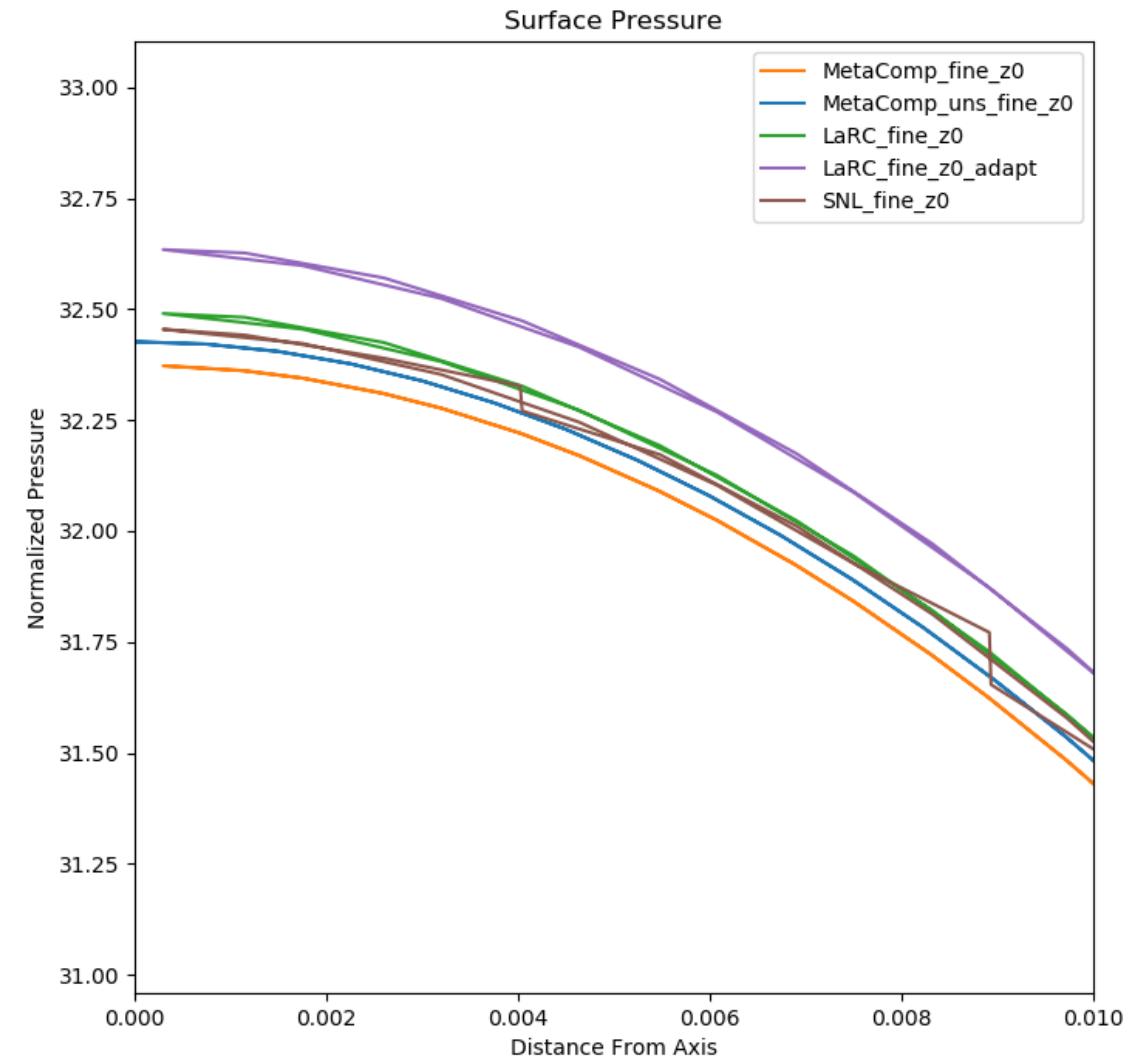
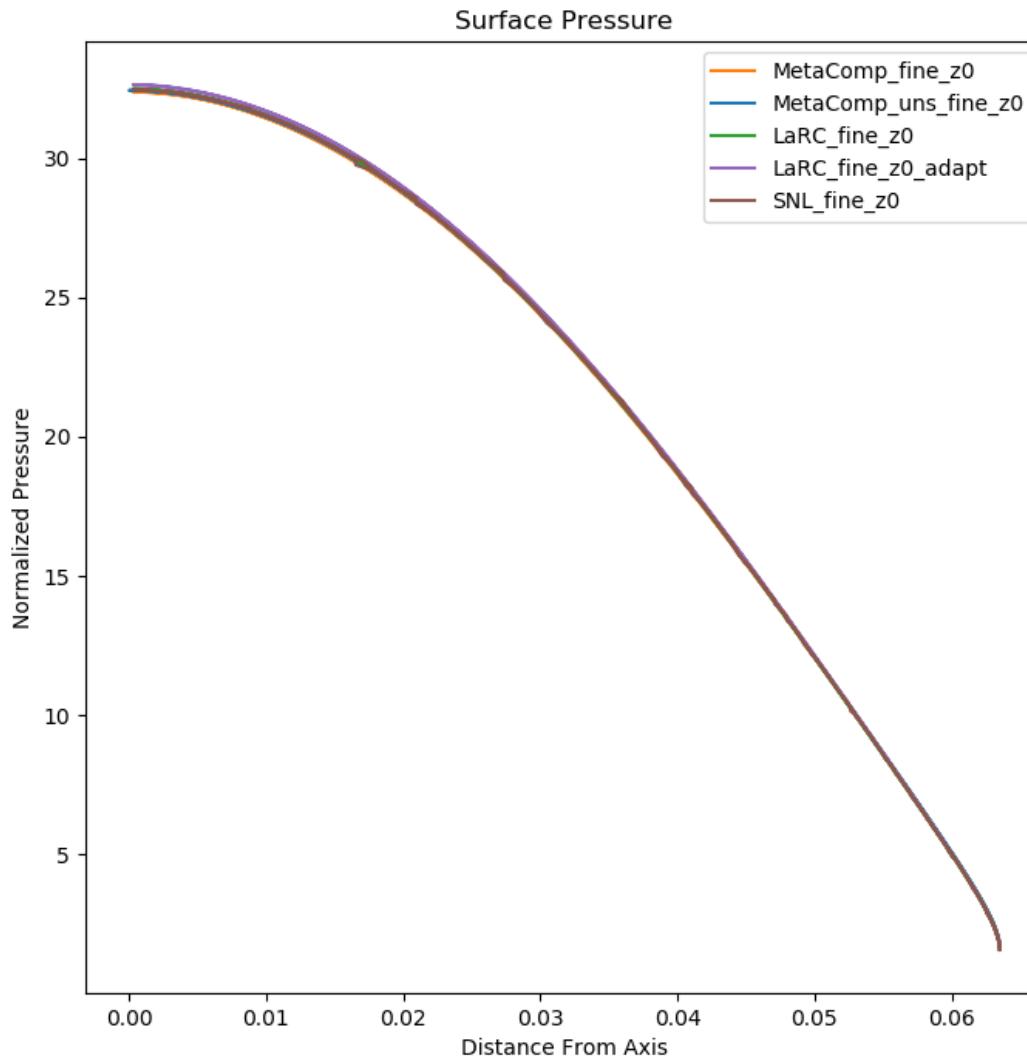
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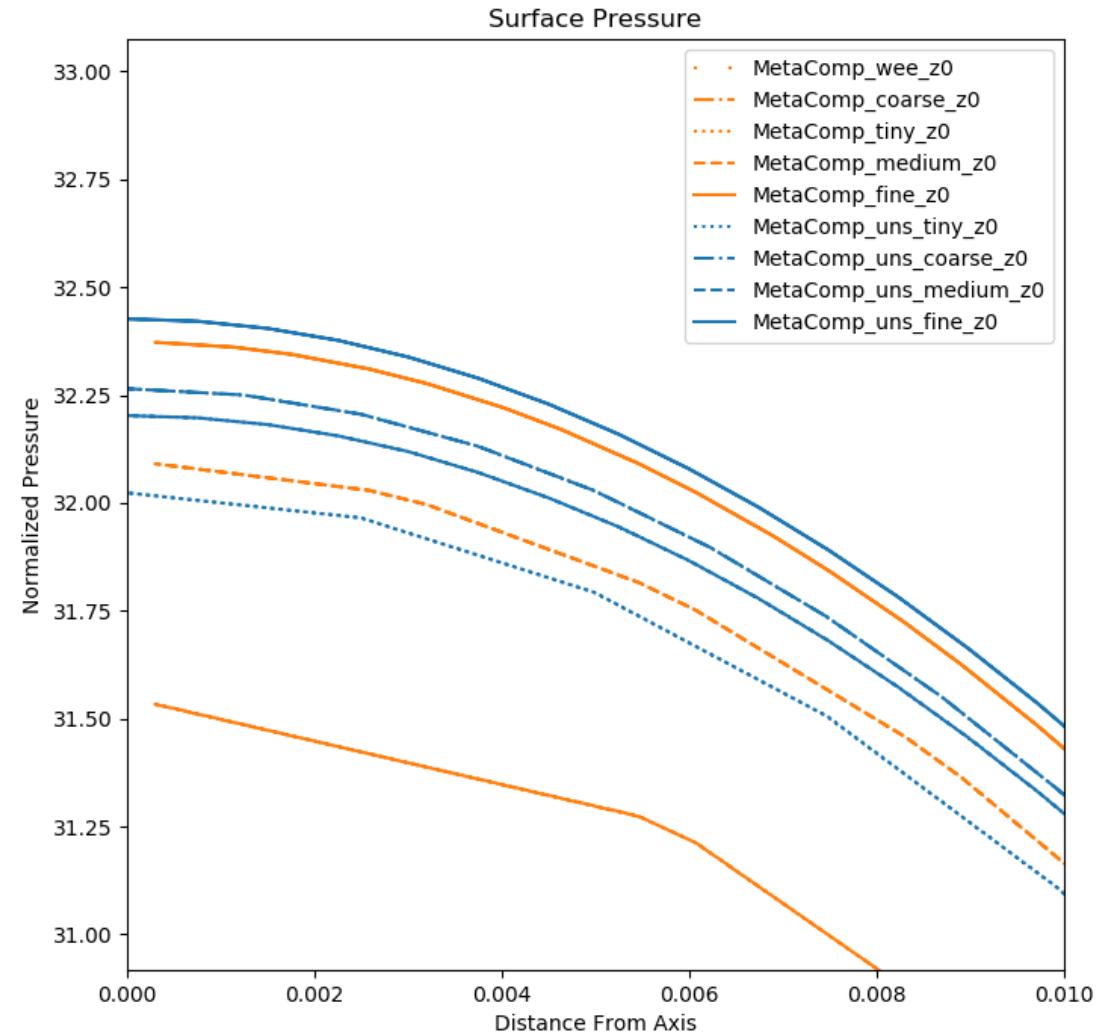
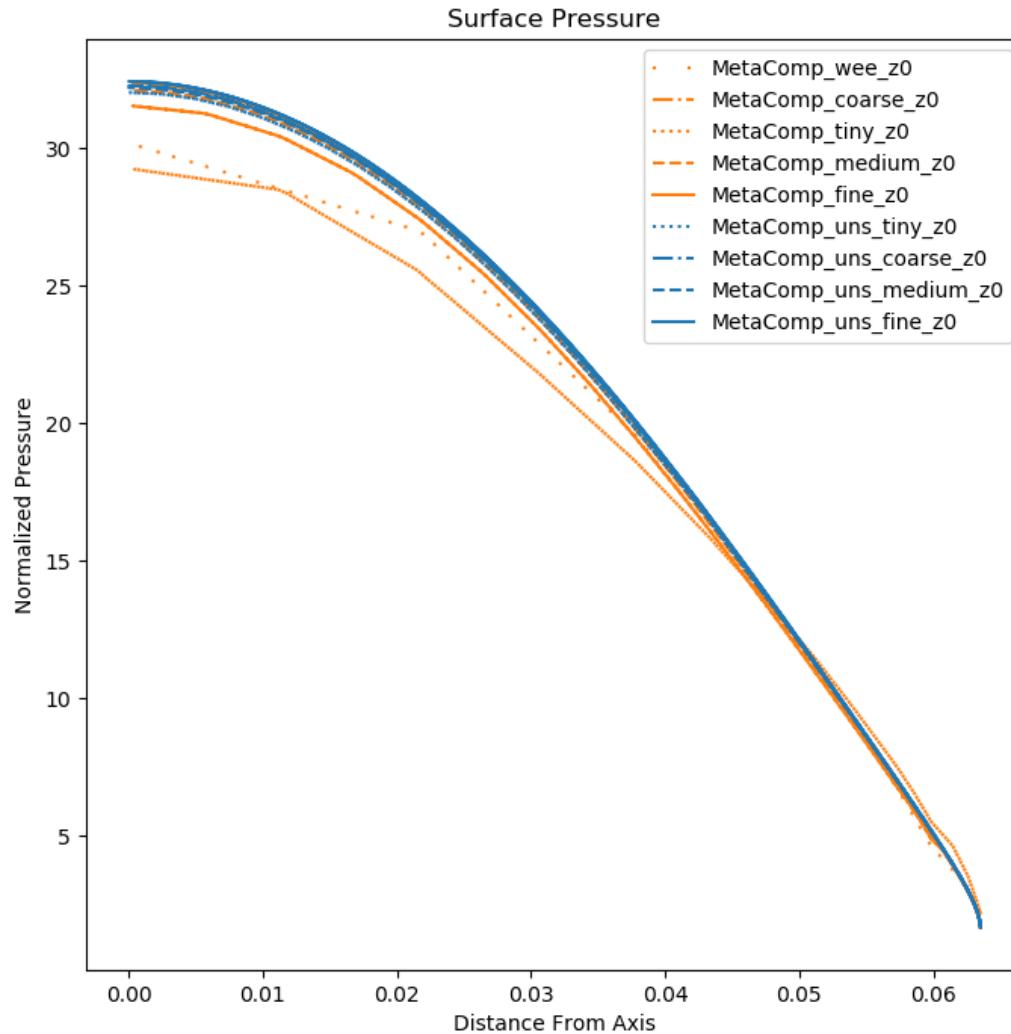
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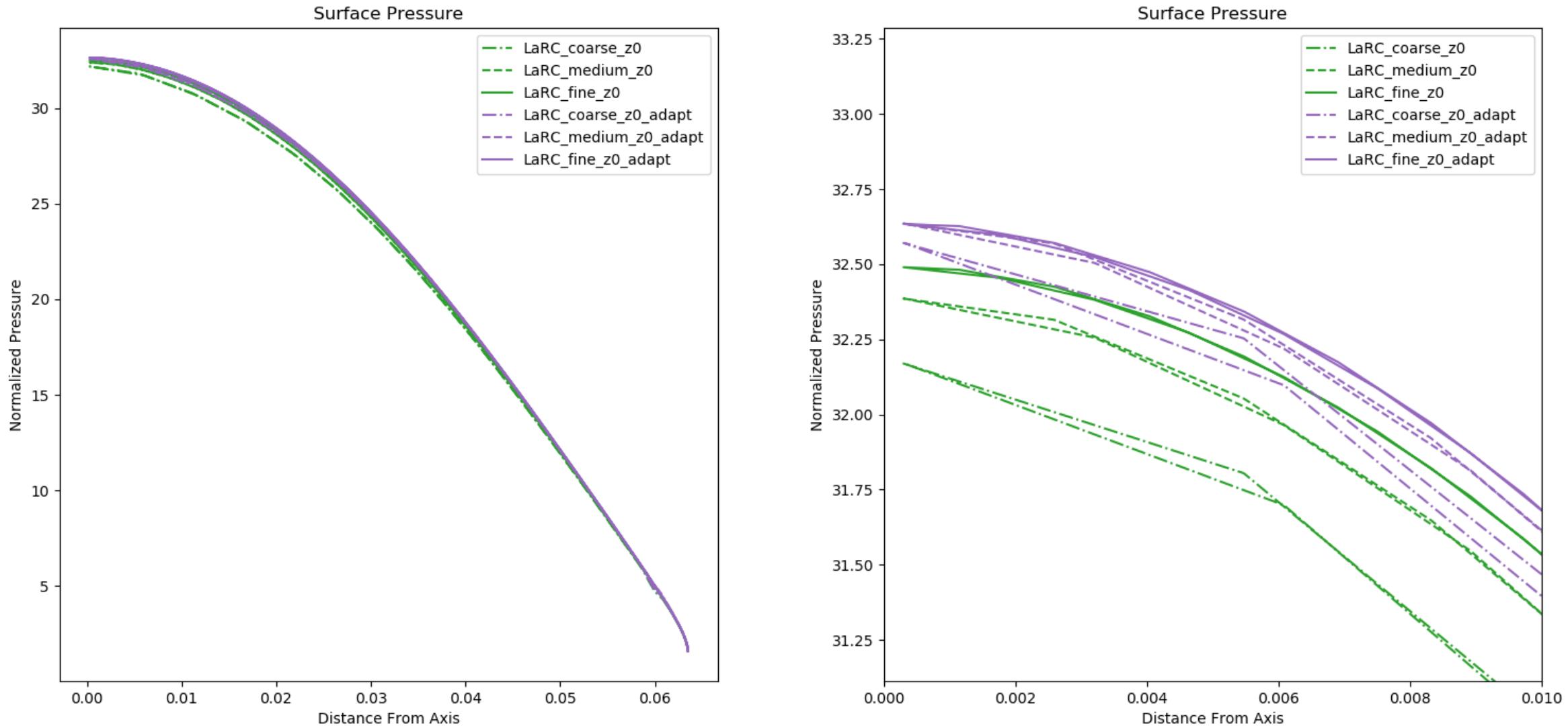


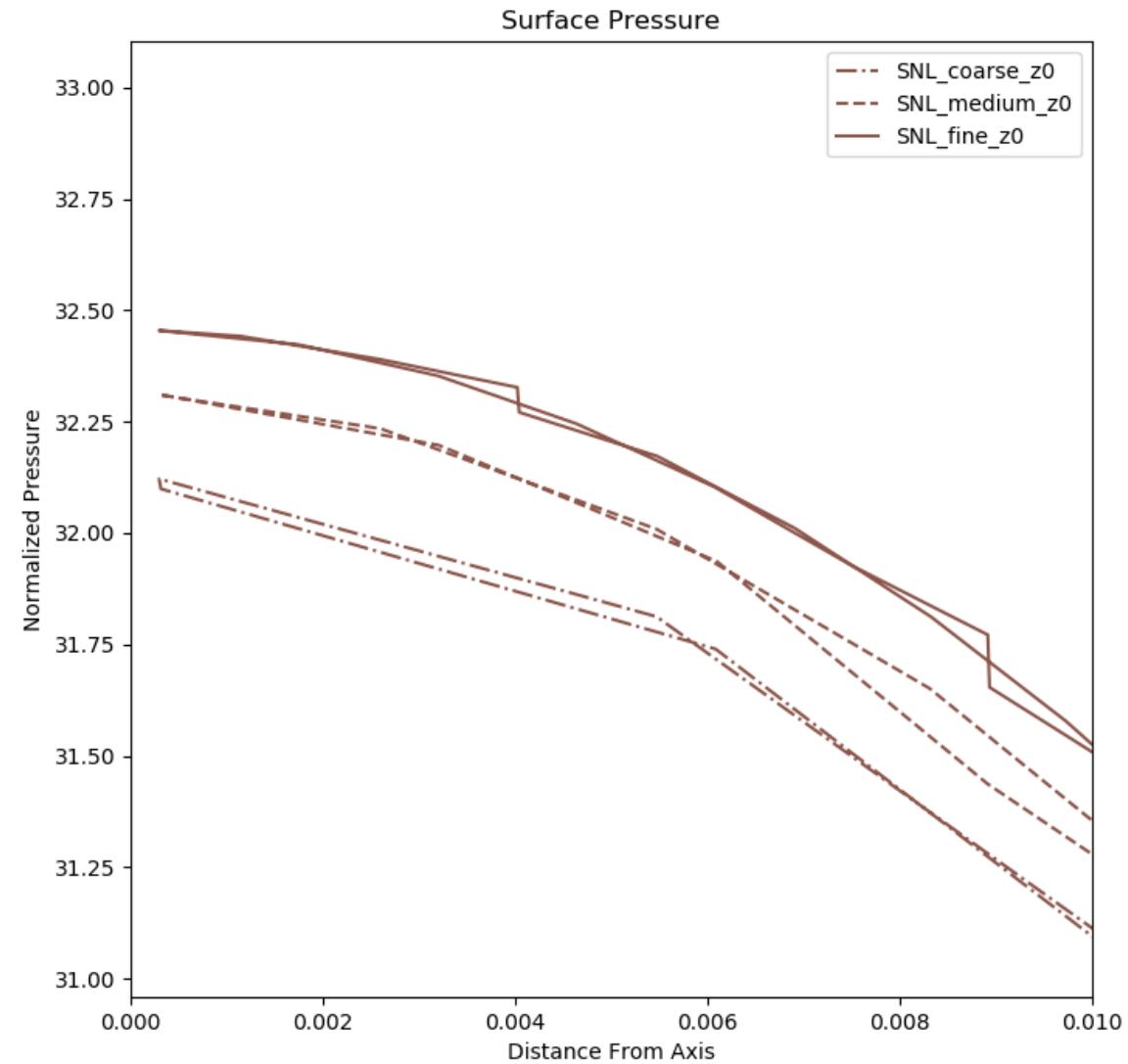
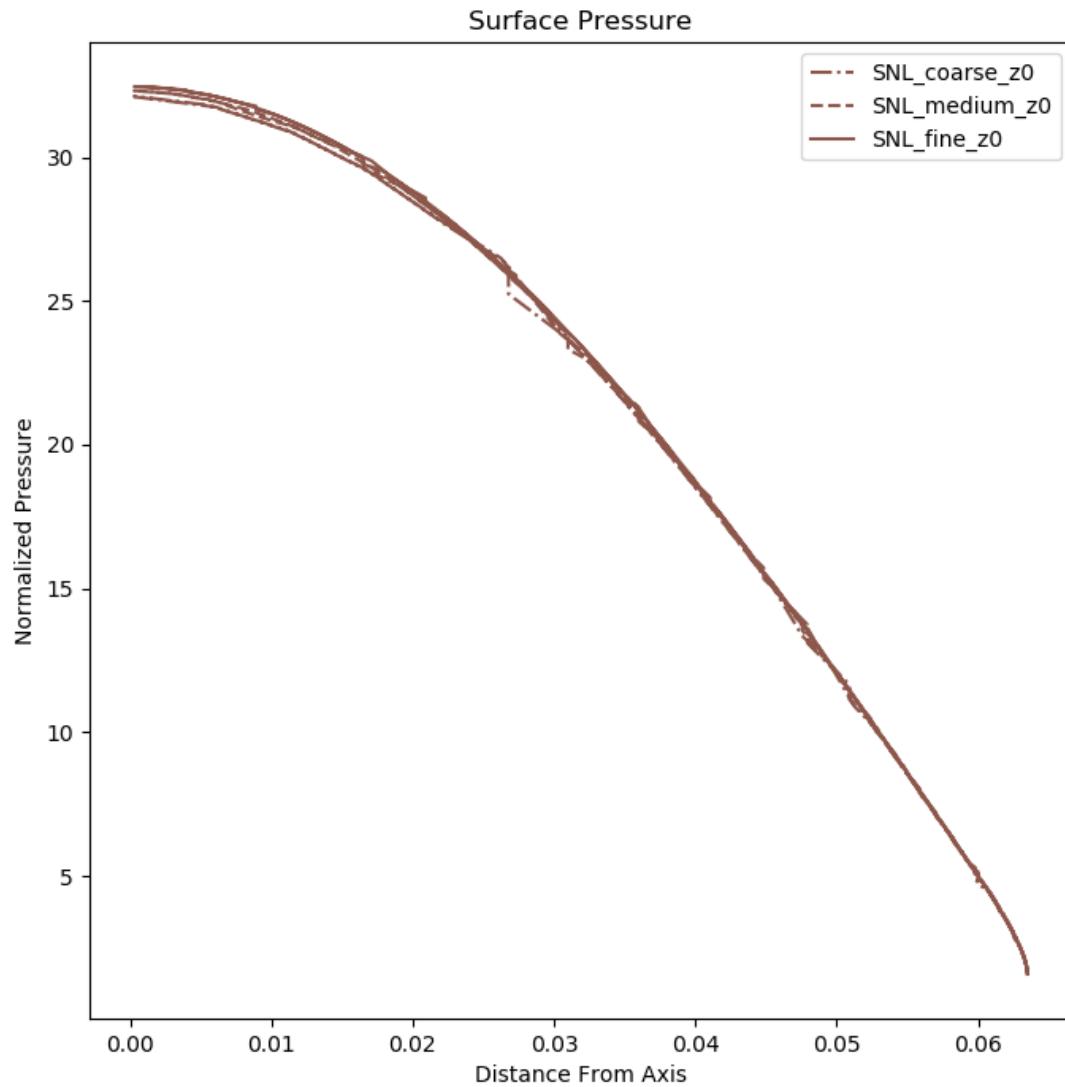


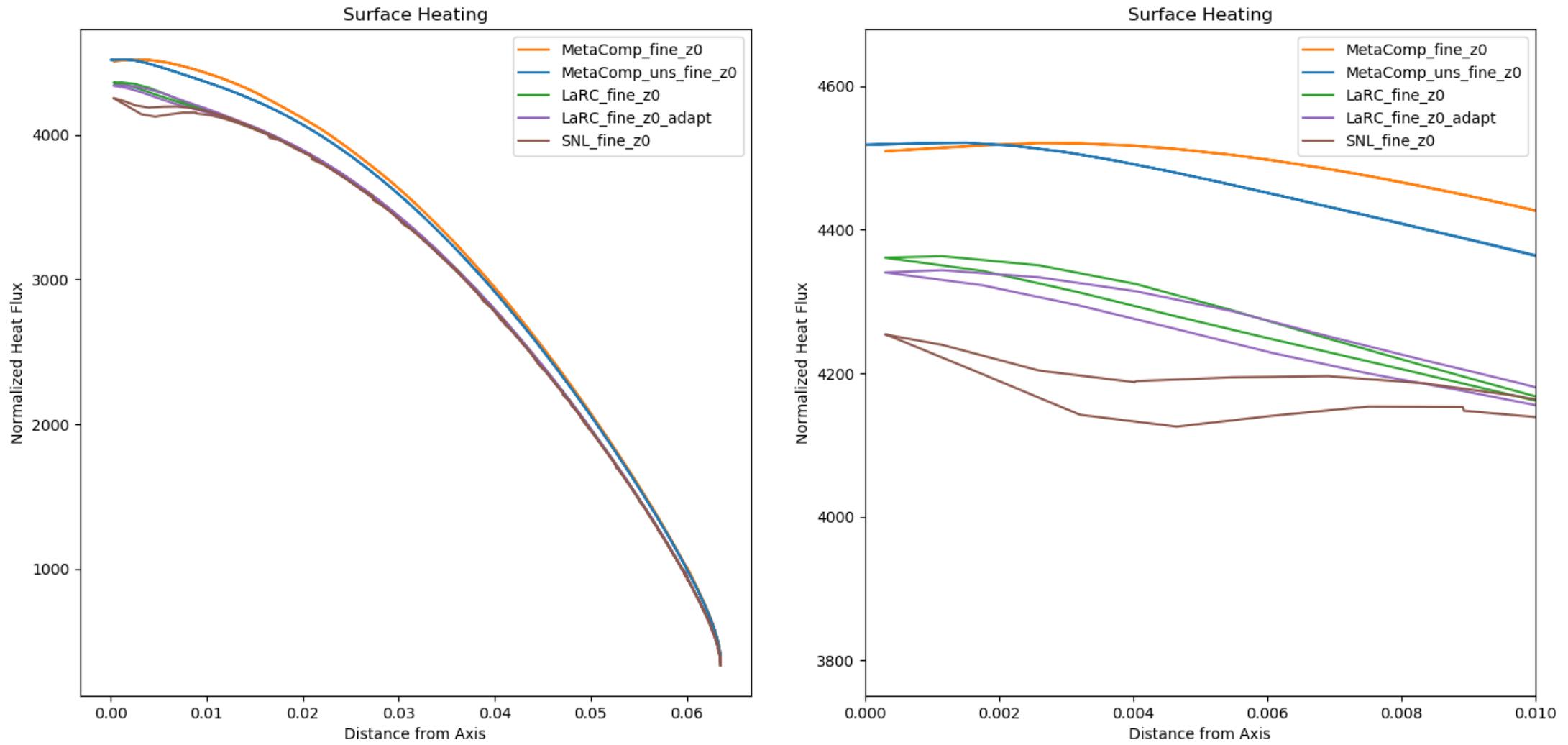


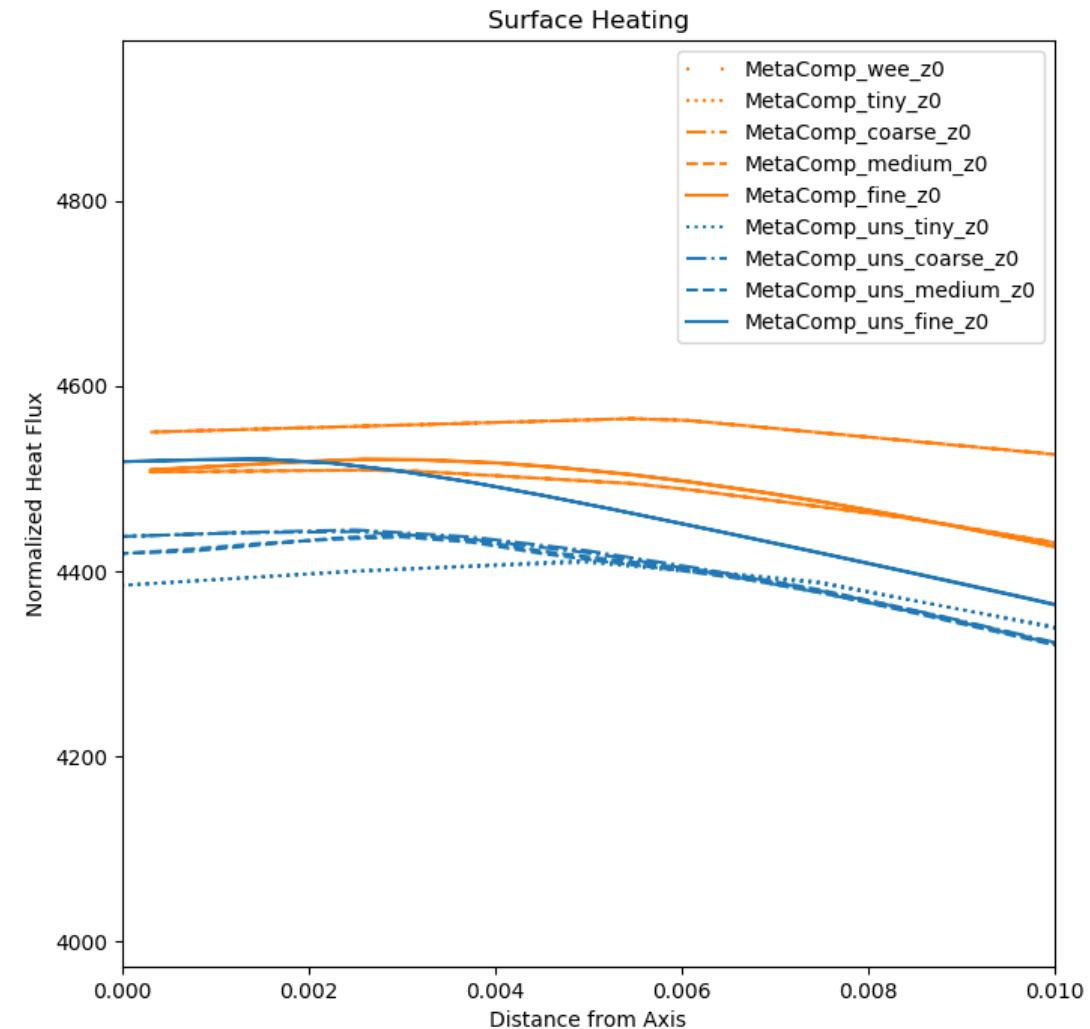
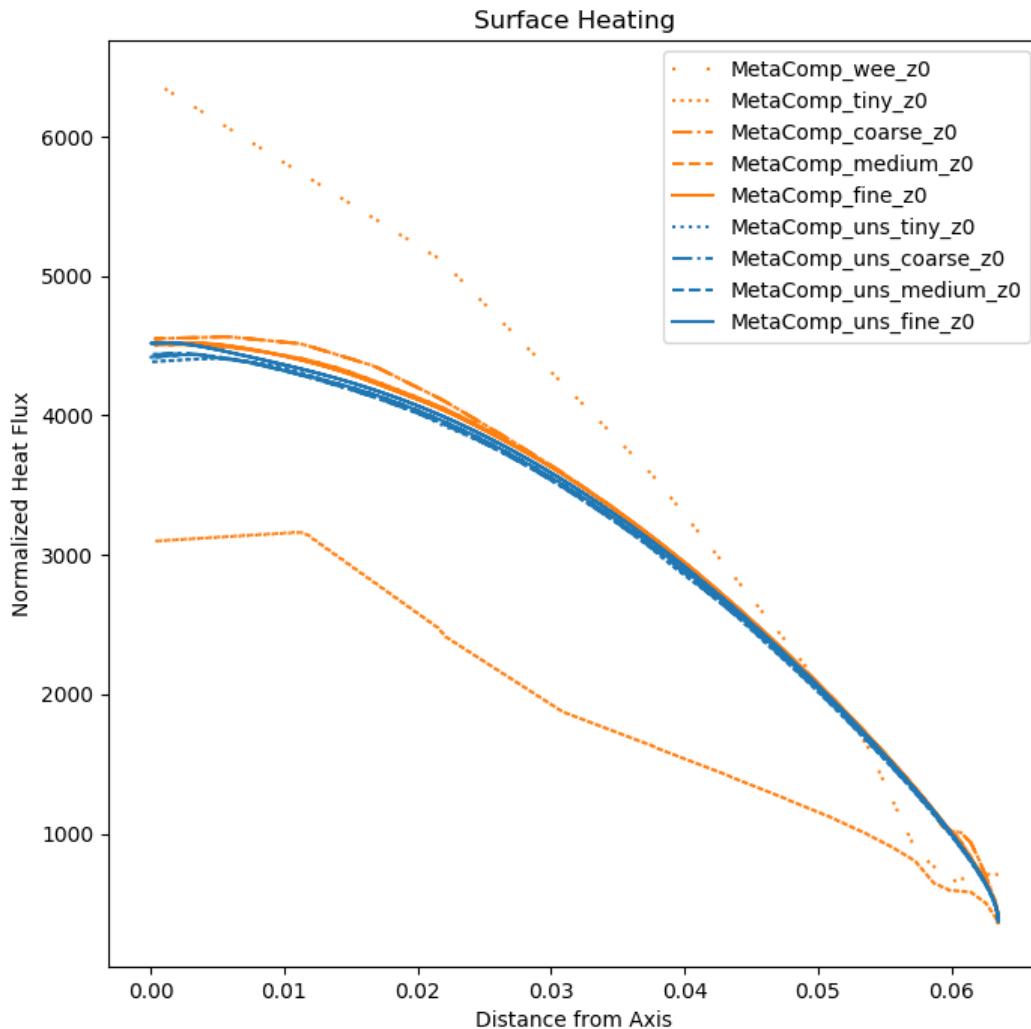
Blottner Results

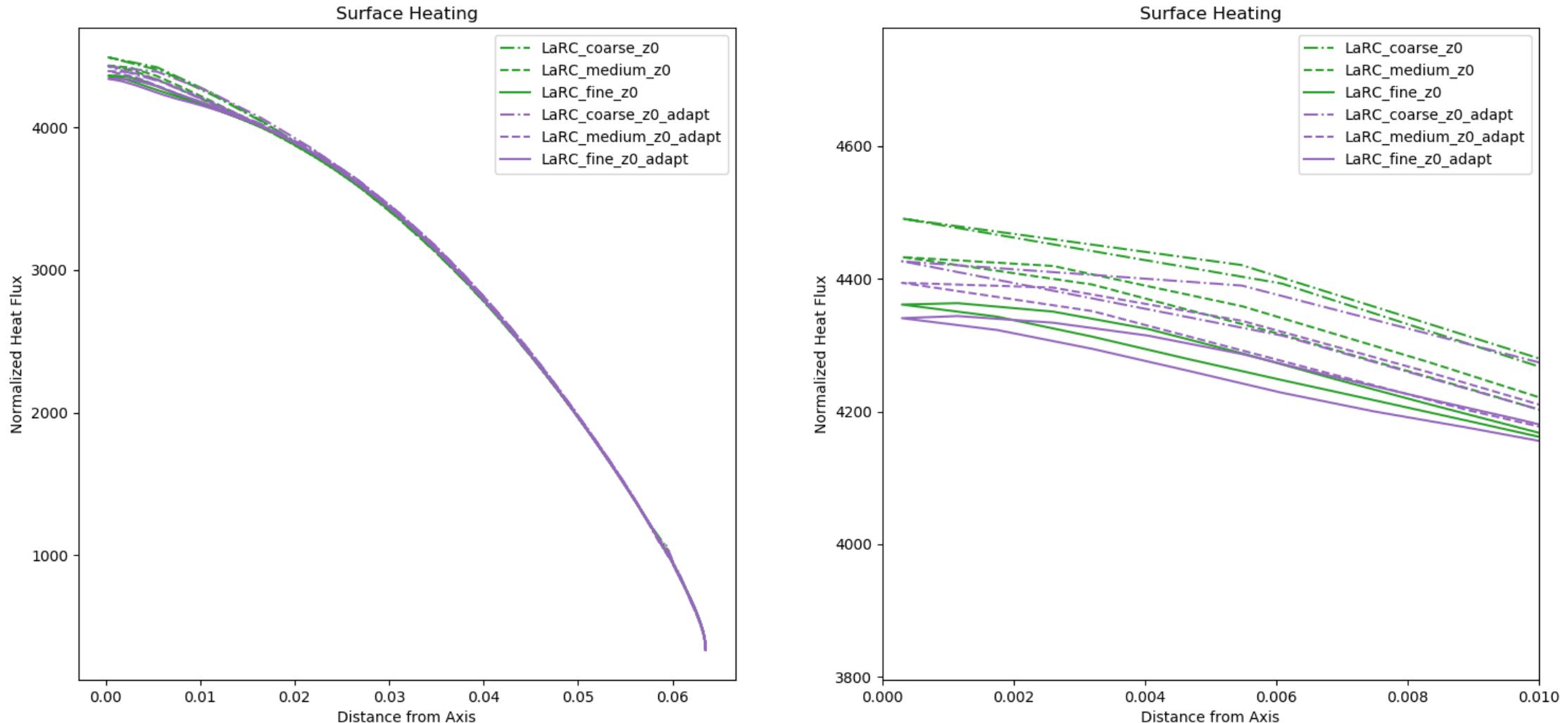


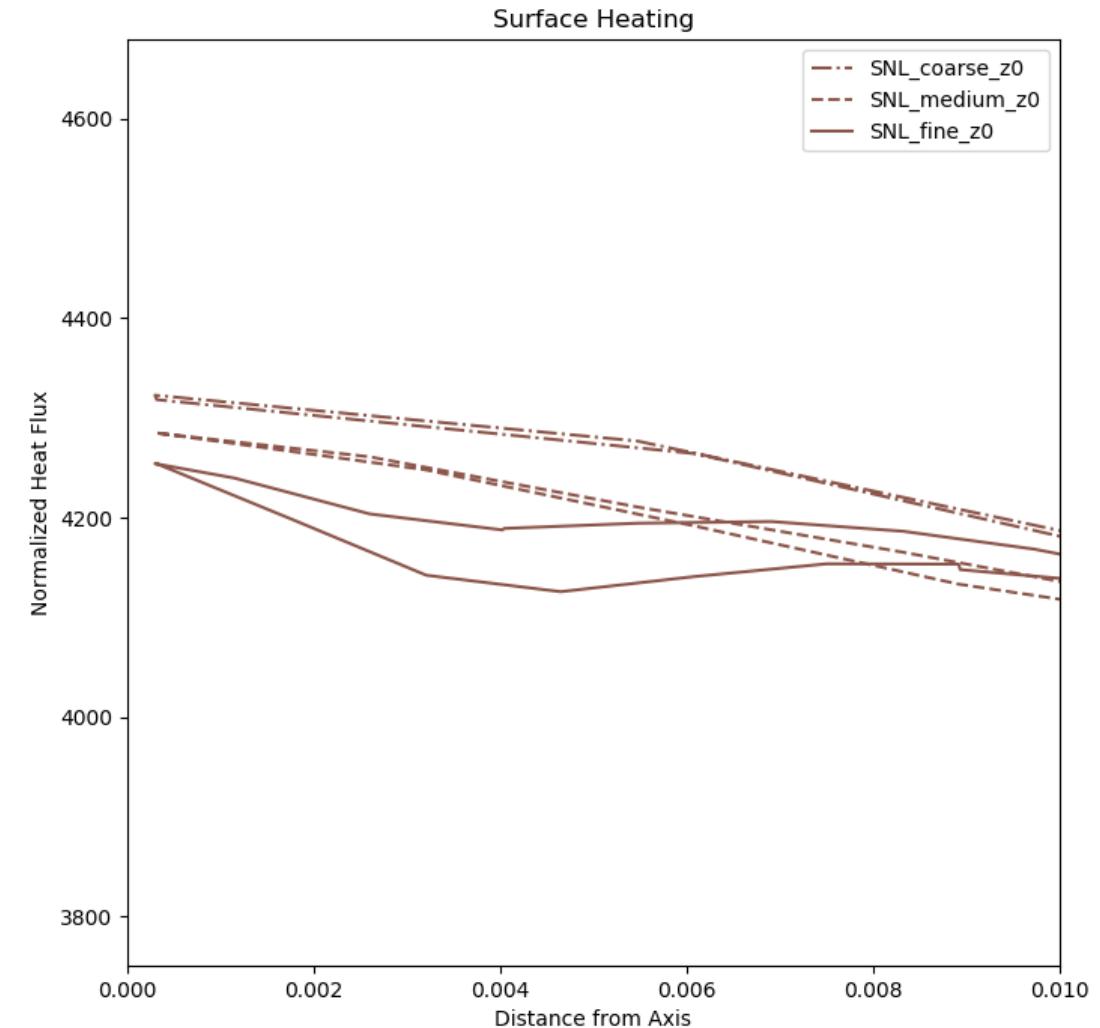
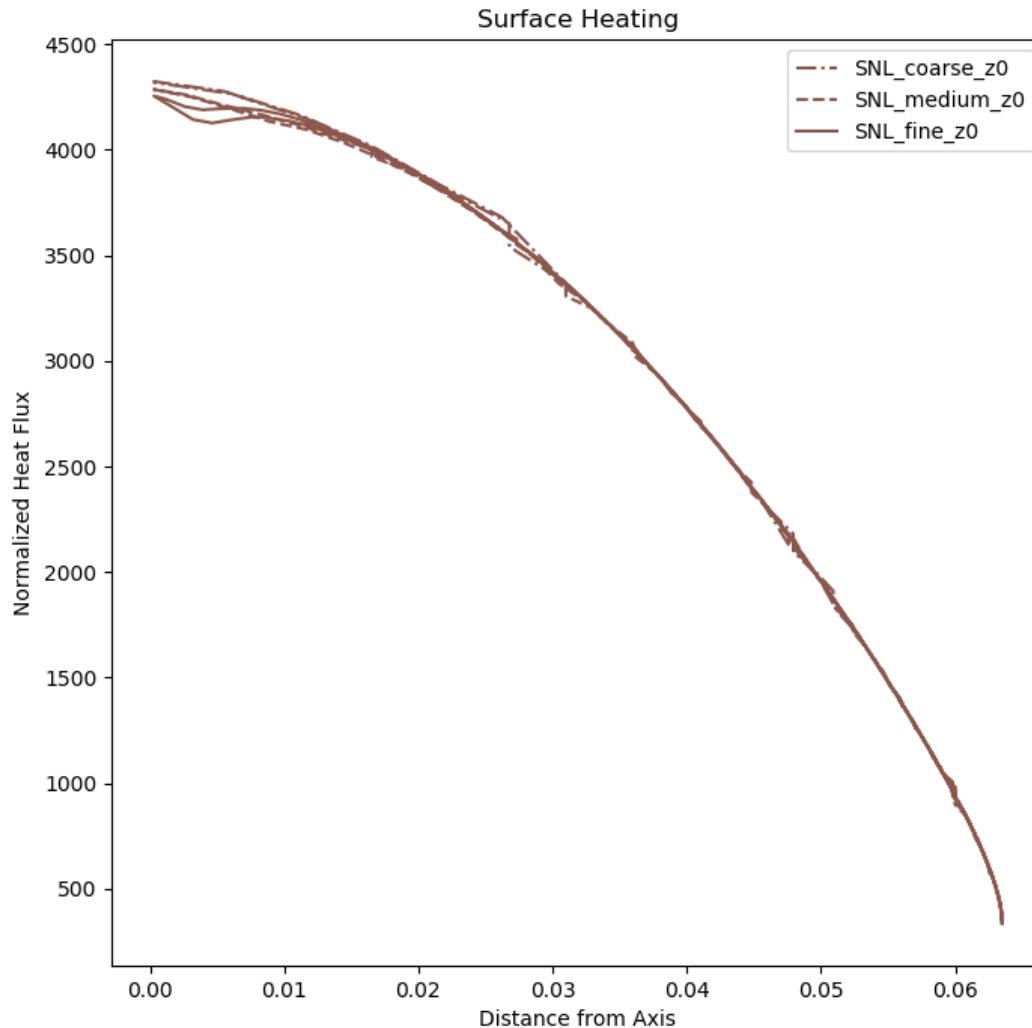












Blottner Observations



Pressure spread approx. 0.5

Heat Flux spread approx. 2000

Very different nonlinear convergence strategies

Artificial dissipation seems well controlled in most cases

Metacomp Structured	Work Units	Rel Residual
Structured Wee	21	1.00E-09
Structured Tiny	193	1.00E-06
Structured Coarse	1819	1.00E-07
Structured Medium	28042	1.00E-07
Structured Fine	299430	1.00E-06

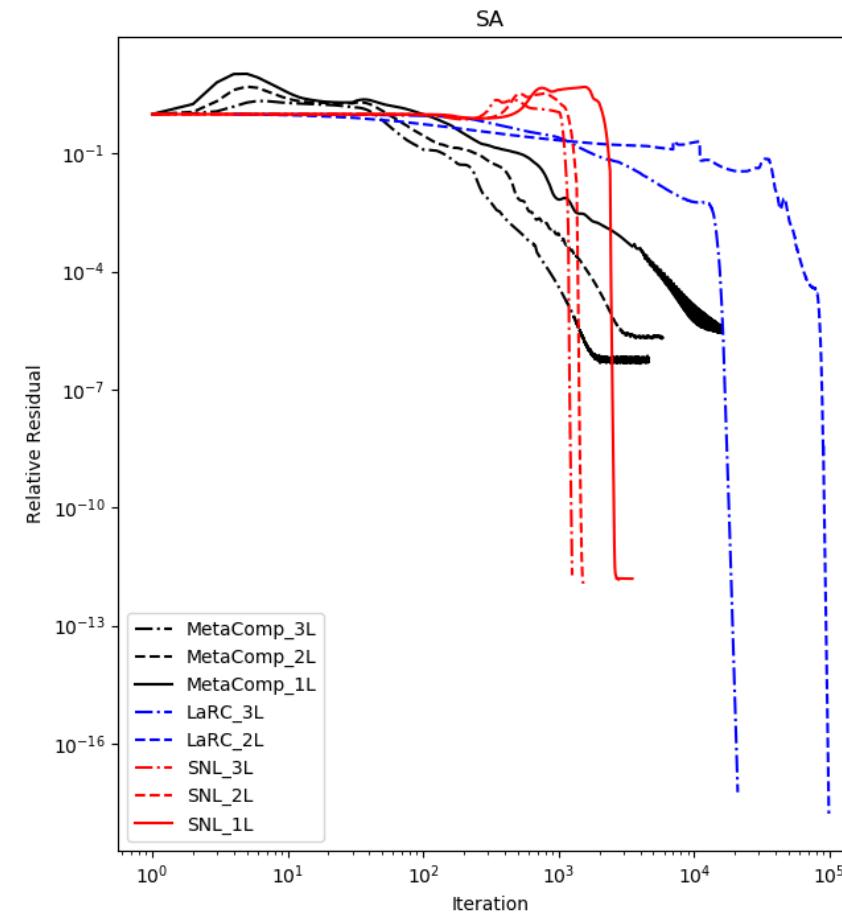
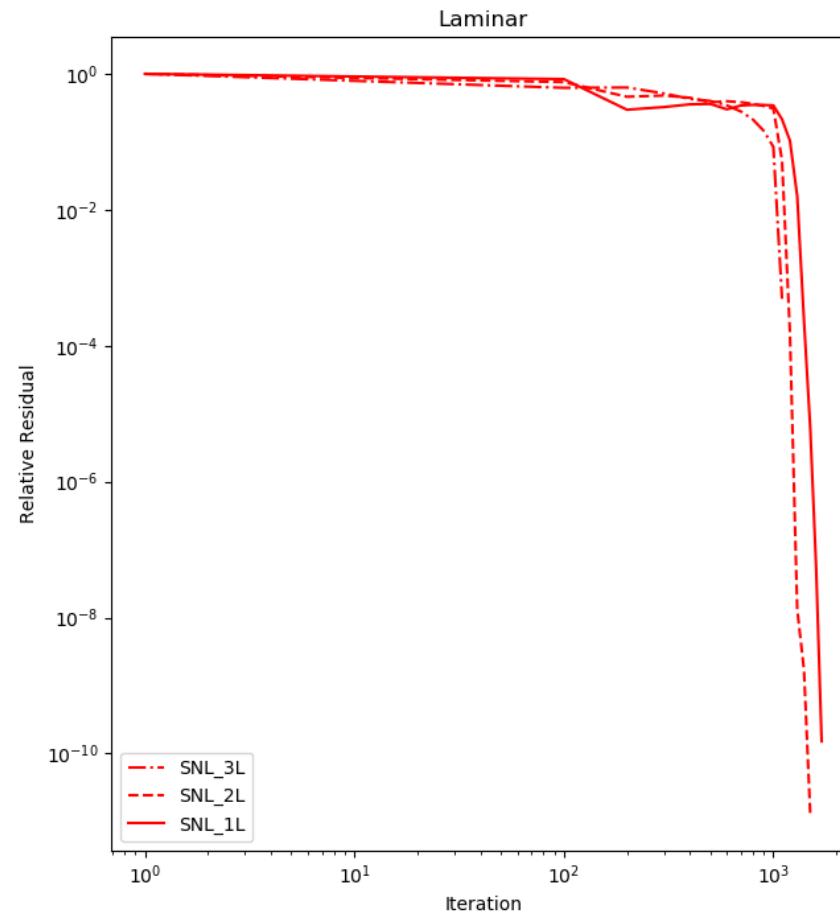
LaRC	Work Units	Rel Residual
Coarse	1855	1.00E-22
Medium	15470	1.00E-20
Fine	214036	1.00E-23

SNL	Work Units	Rel Residual
Coarse	1974	1.00E-12
Medium	23592	1.00E-12
Fine	356395	1.00E-12

Metacomp Unstructured	Work Units	Rel Residual
Unstructured Tiny	6576	1.00E-07
Unstructured Coarse	72741	1.00E-07
Unstructured Medium	225501	1.00E-06
Unstructured Fine	1503055	1.00E-06

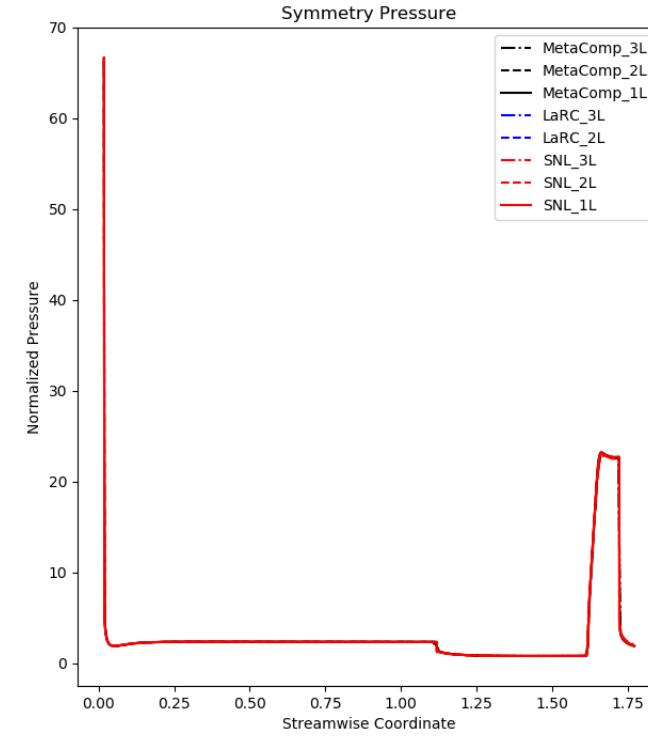
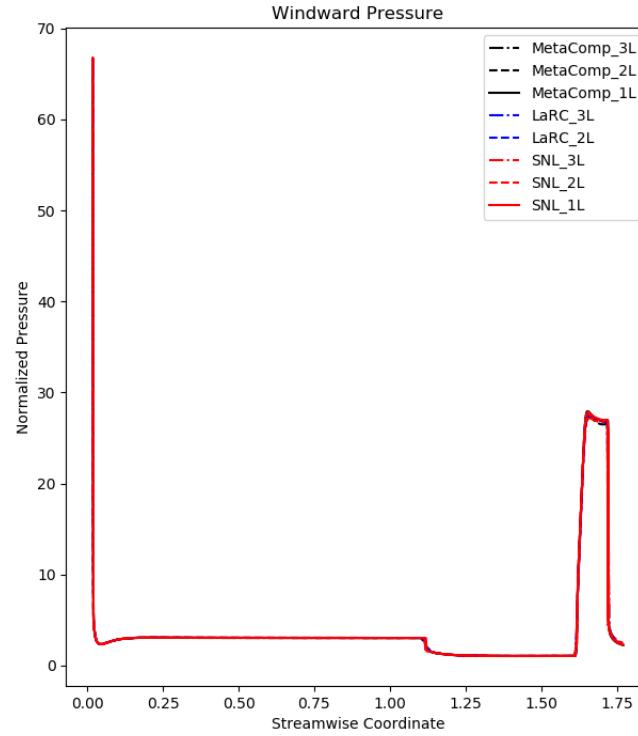
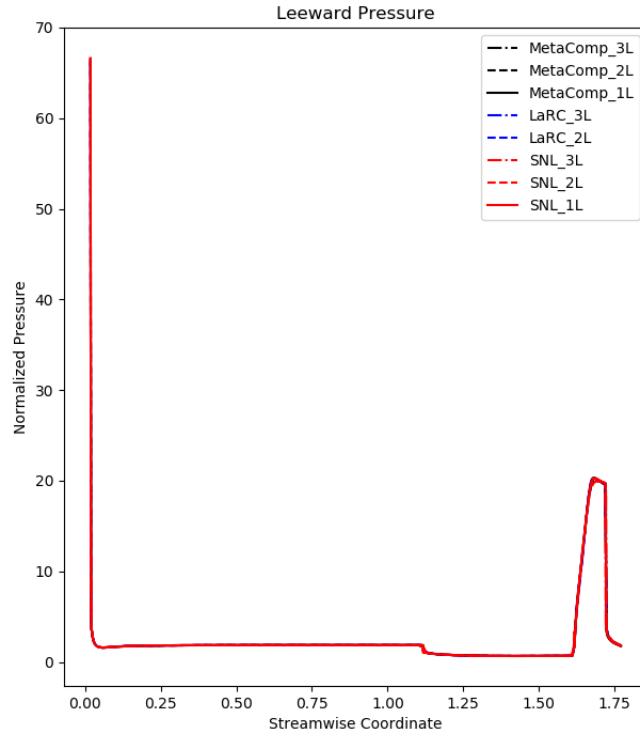
LaRC-adapt	Work Units	Rel Residual
Coarse	2201	1.00E-18
Medium	22576	1.00E-21
Fine	331508	1.00E-19

Convergence Comparison

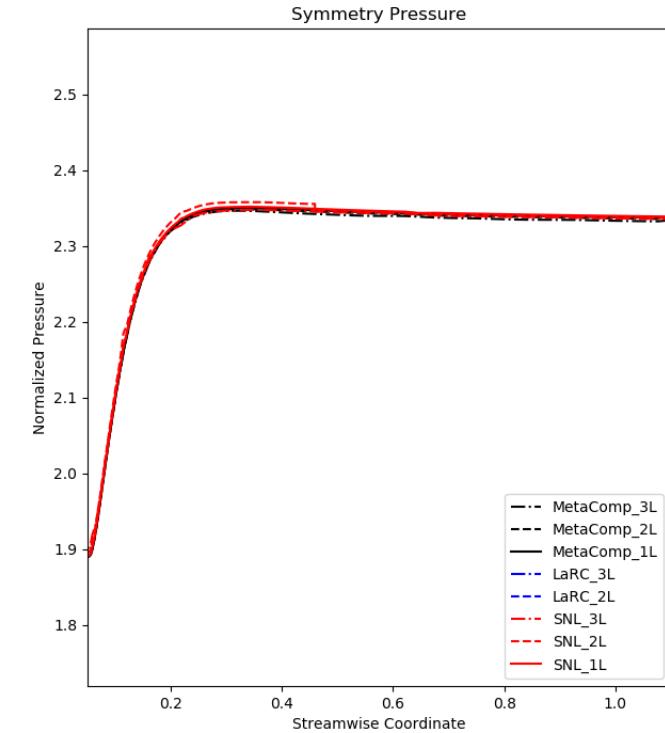
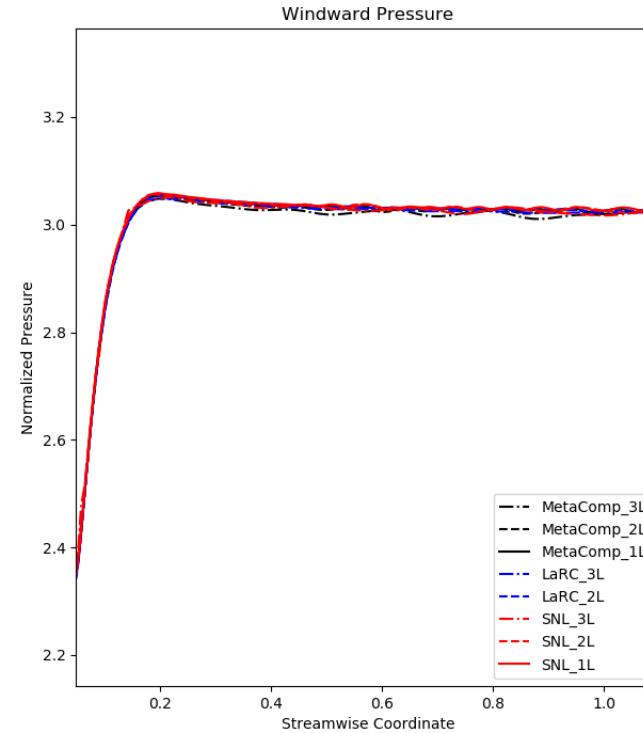
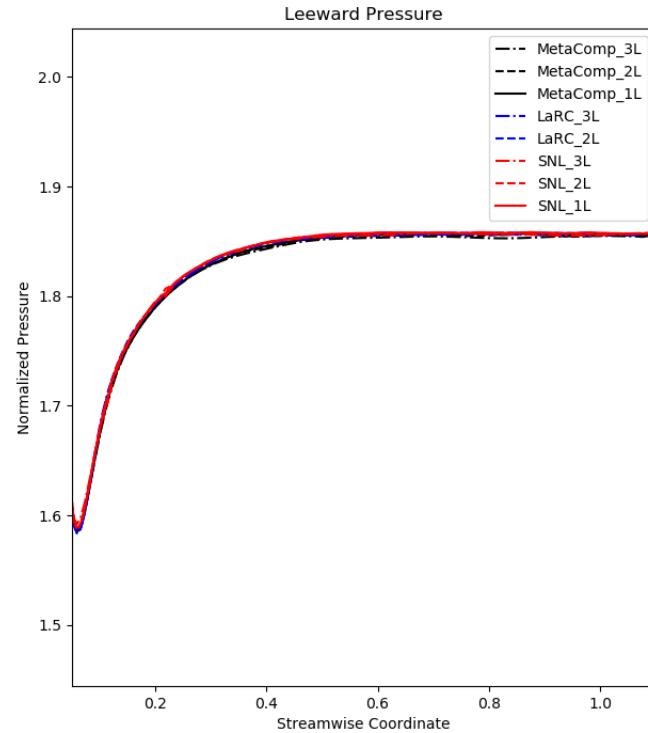




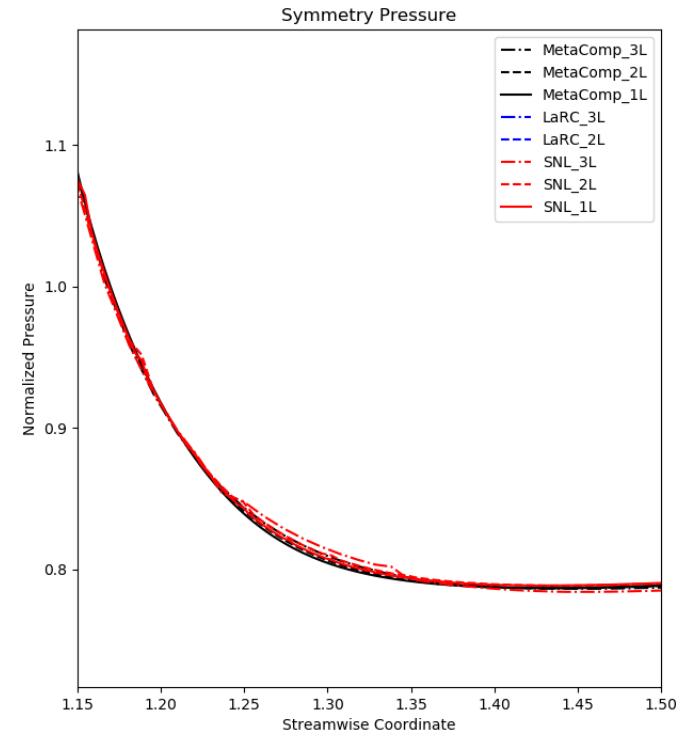
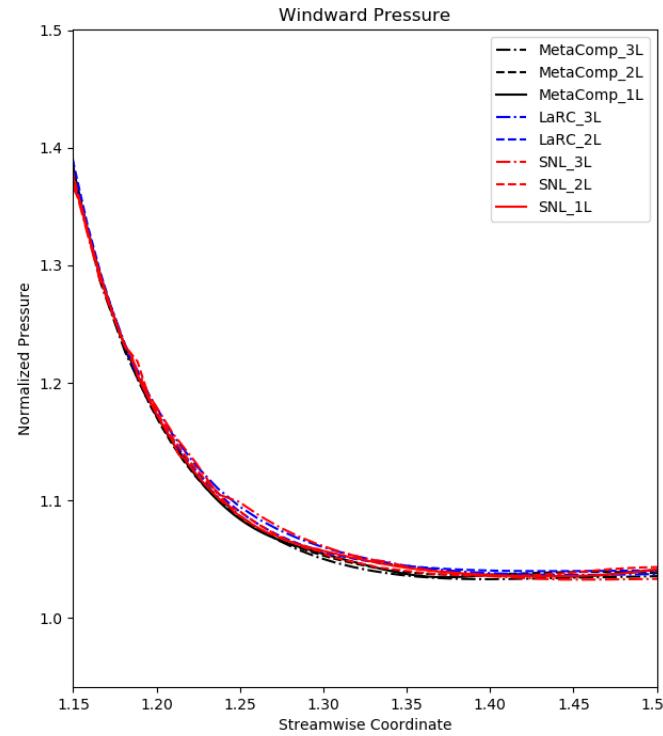
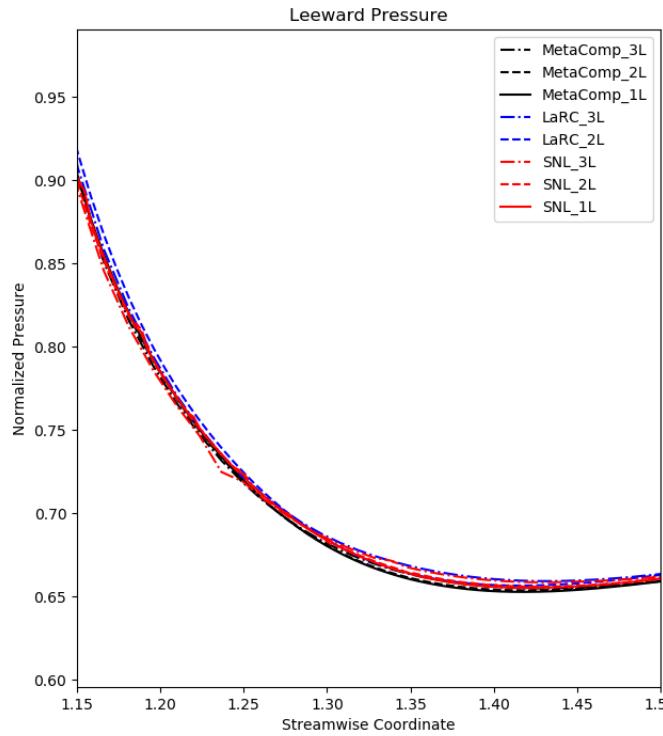
SA Normalized Pressure Comparison

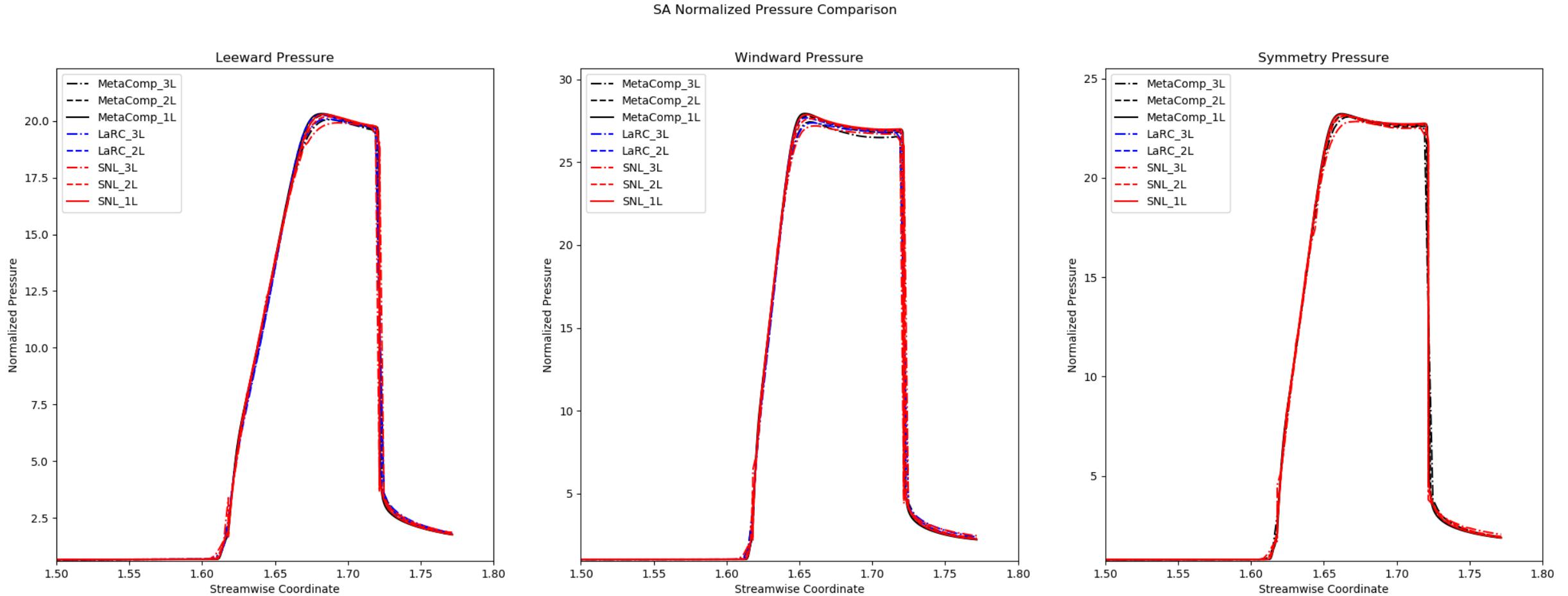


SA Normalized Pressure Comparison



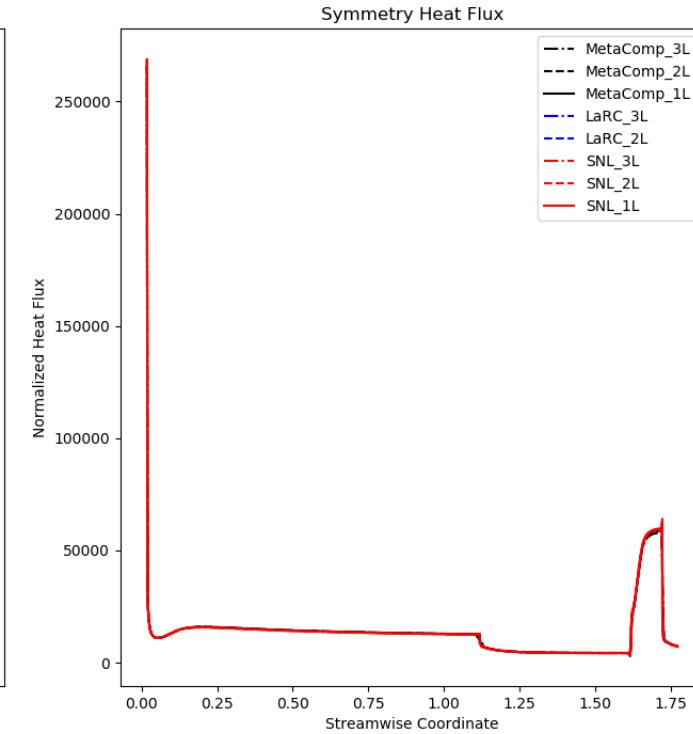
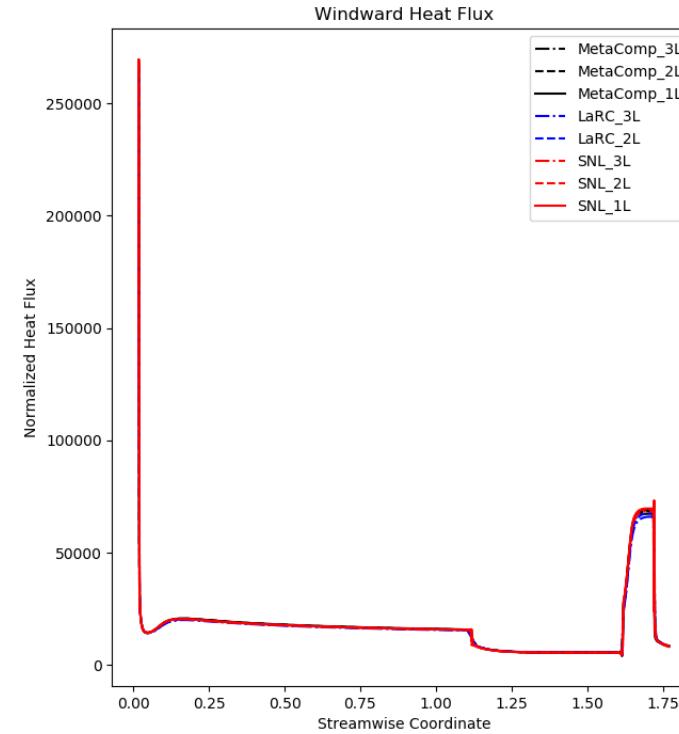
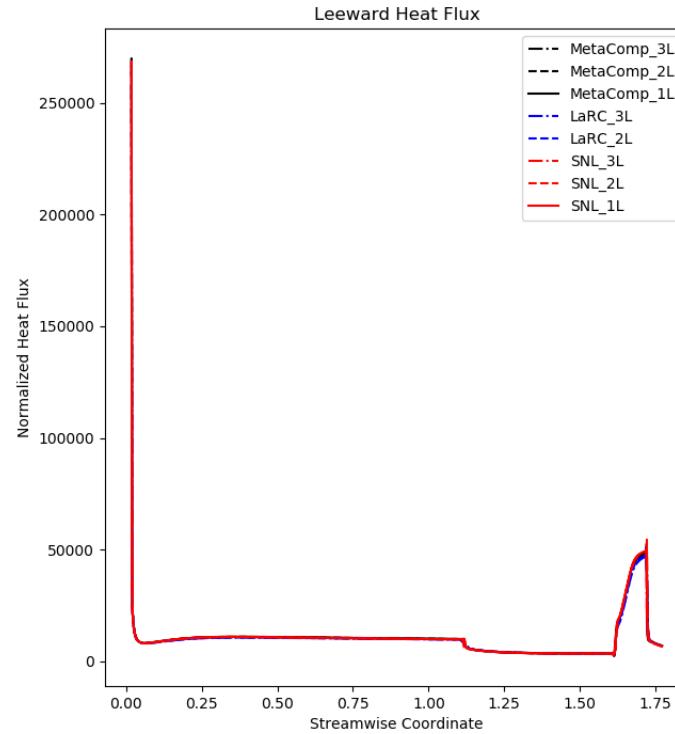
SA Normalized Pressure Comparison

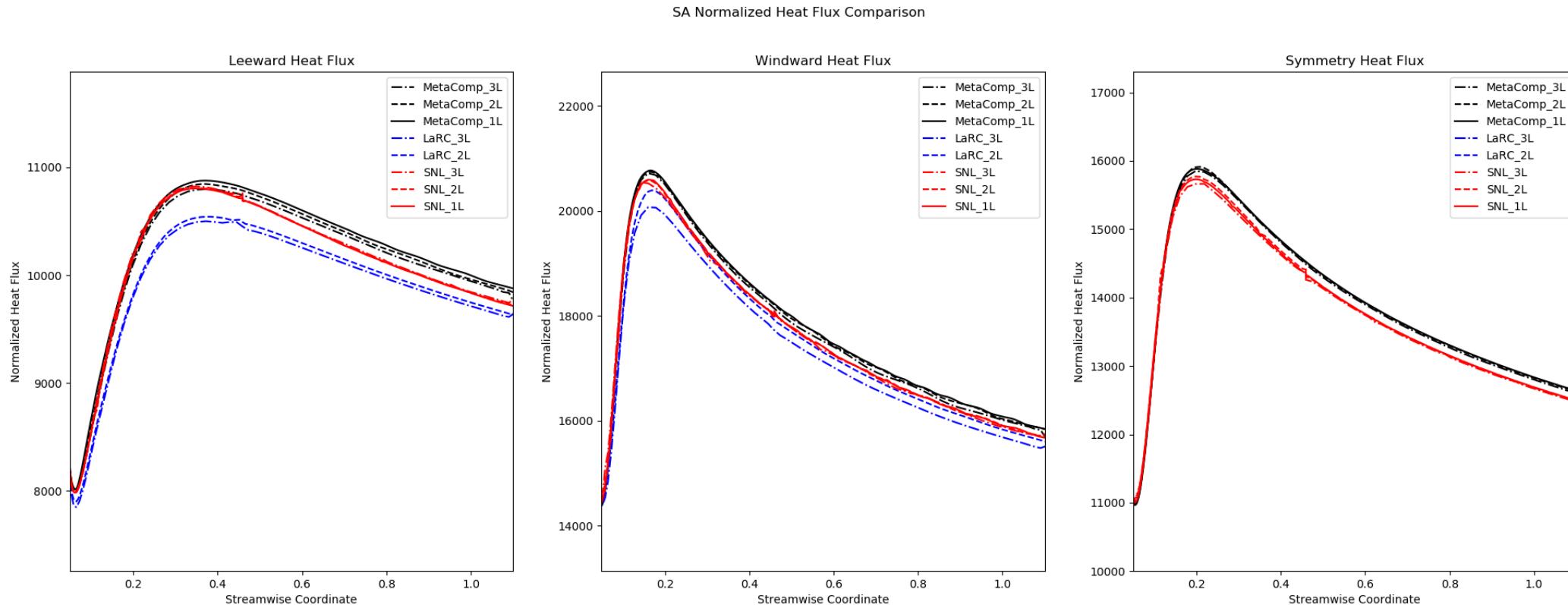


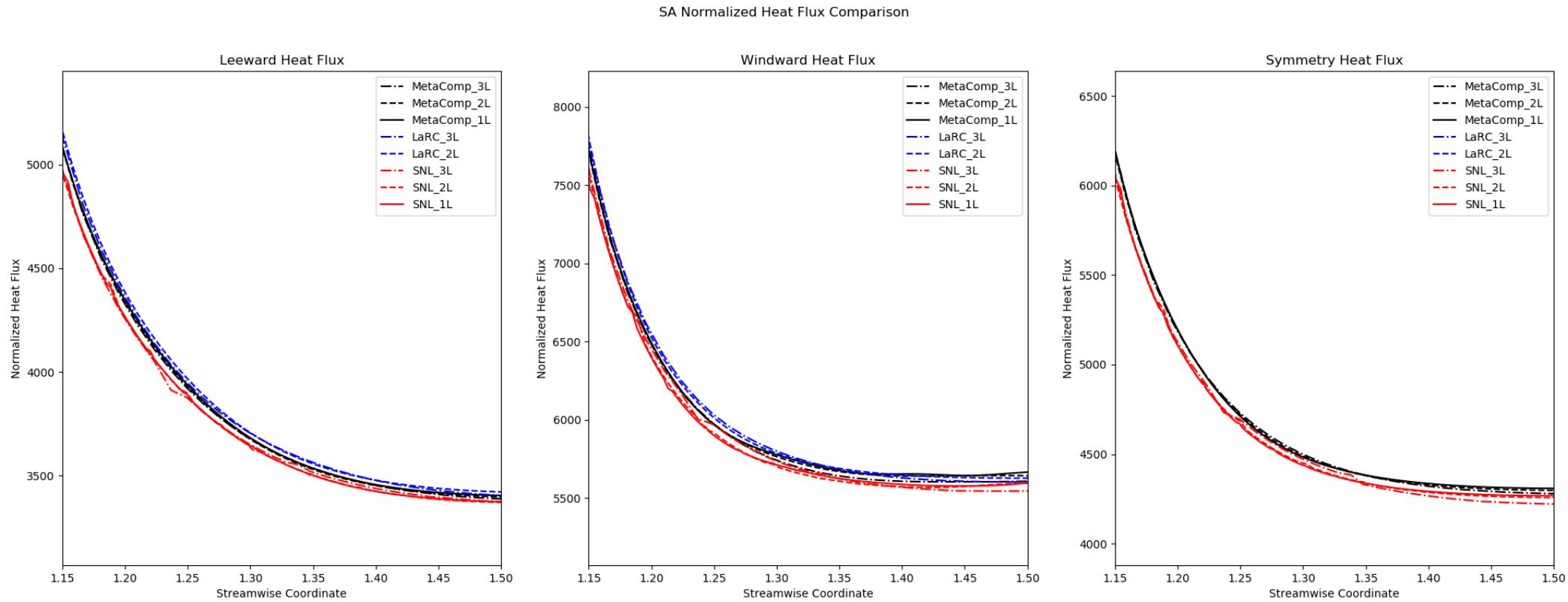




SA Normalized Heat Flux Comparison

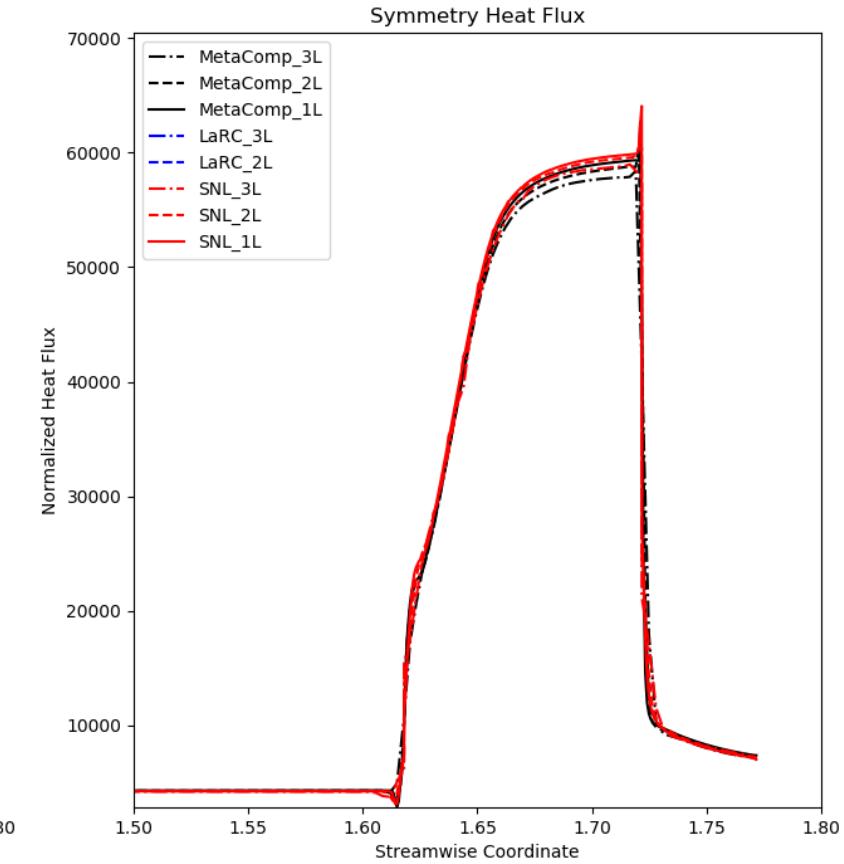
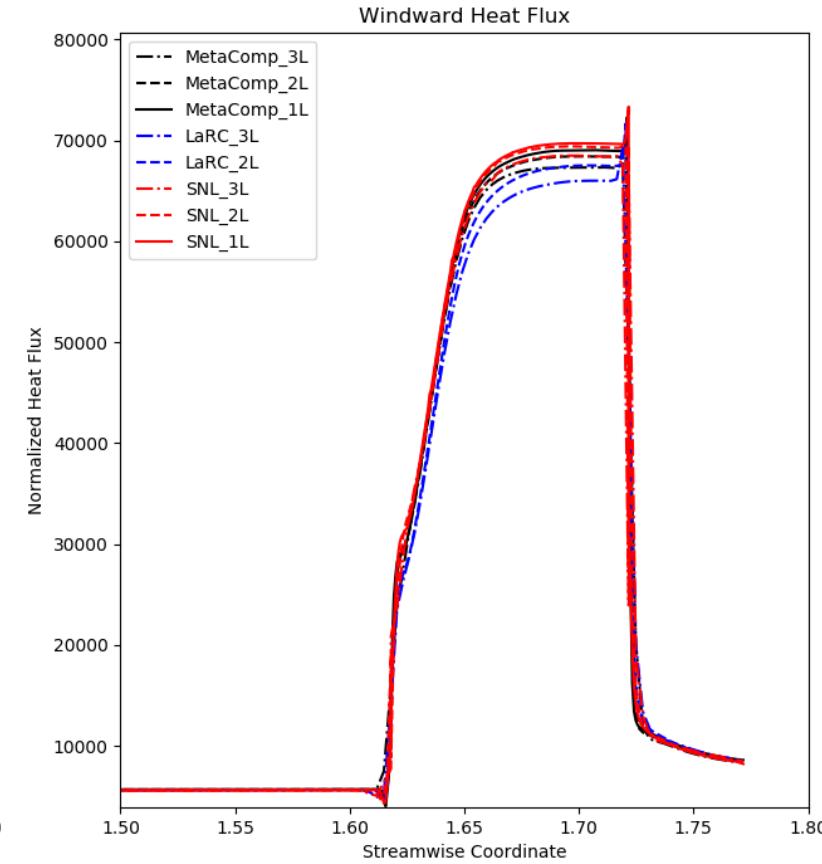
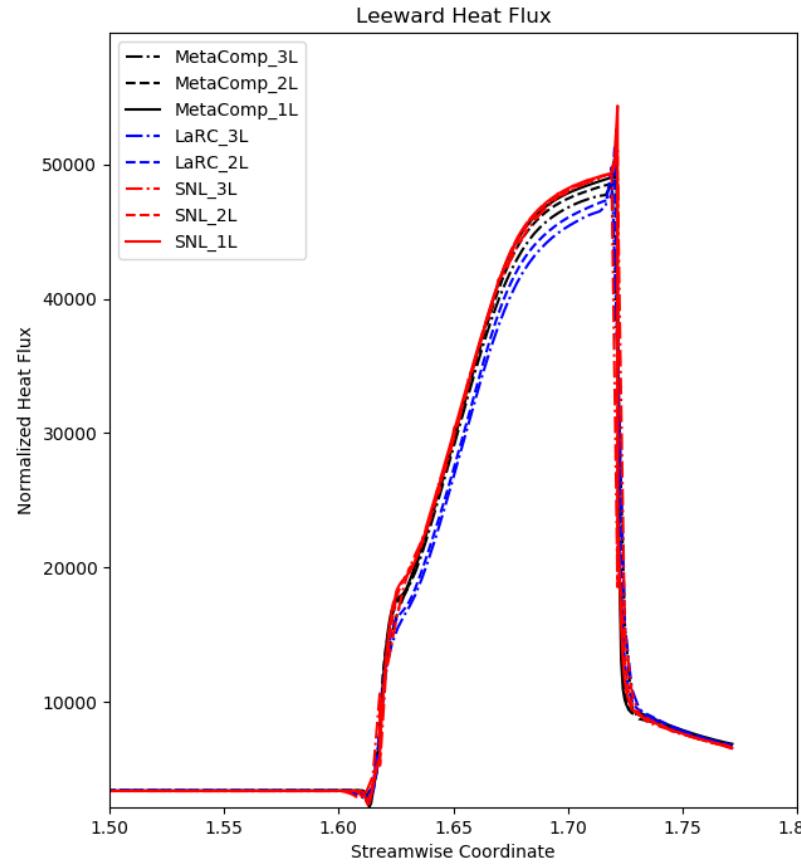








SA Normalized Heat Flux Comparison





Artificial dissipation again well-controlled

Good overall convergence on meshes

Differences are concentrated in separated region

Not enough difference to draw additional conclusions

Metacomp	Work Units	Rel Residual
3L	2.37E+04	1.00E-06
2L	4.05E+05	1.00E-05
1L	3.90E+07	1.00E-05

LaRC	Work Units	Rel Residual
3L	9.99E+04	1.00E-17
2L	3.72E+06	1.00E-18

SNL	Work Units	Rel Residual
3L	3.98E+04	1.00E-12
2L	5.30E+05	1.00E-12
1L	2.34E+07	1.00E-11

Individual Contributor Questions to Answer/Discuss



How do you control numerical dissipation?

- Especially in the boundary layer?
- Did you have to fiddle with it based on mesh resolution or problem setup?

Do you get good nonlinear convergence?

- If not, do you know what's holding your scheme up?
- Please describe your nonlinear and linear solver strategy either way.

Did you run the cases in different ways? How did the results vary?

Did you have difficulties running the cases?

- What were they?
- Did you resolve them or are they unresolved?