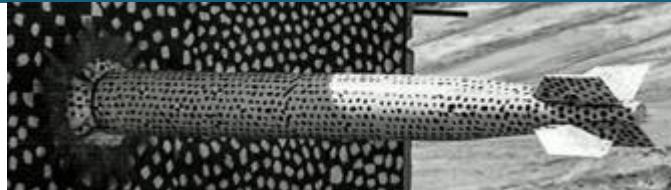
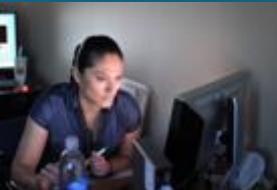




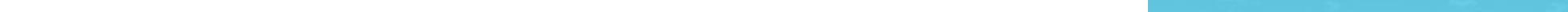
Sandia  
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# Dispersion of Stored Energy in Response to Thermal Runaway



## PRESENTED BY

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# Project Concept and Motivation



Cascading thermal runaway (TR) events present significant risk to large-scale utility battery storage installations

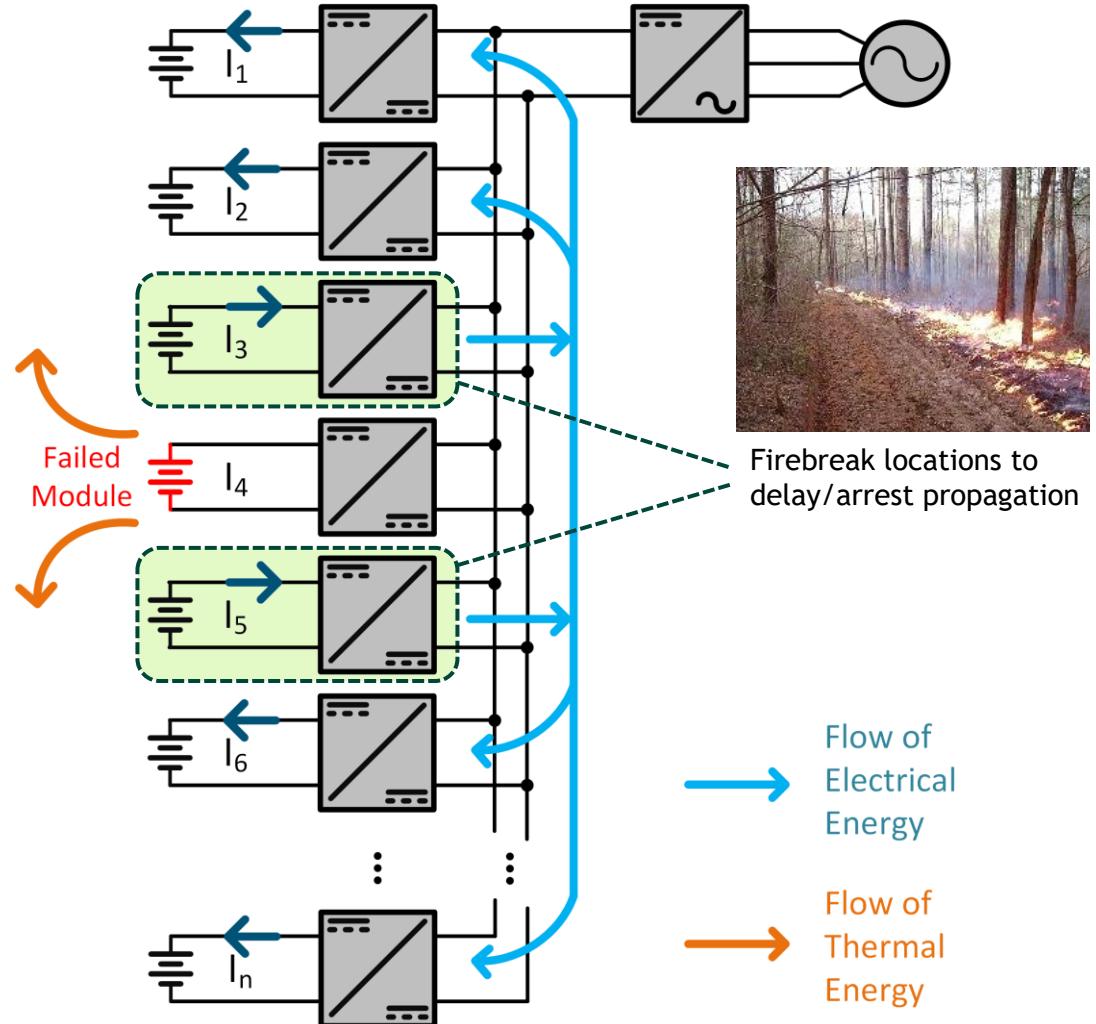
Current approaches to mitigating this risk involve electrical isolation, cooling, and fire suppression

Electrical isolation strands energy in subassemblies adjacent to the TR event, and does nothing to stop TR events once in progress

The likelihood of propagation of TR between subassemblies can be reduced through judicious dispersion of stored energy within the system, effectively placing “firebreaks” in the event’s path

The goal of this project is to develop the electrical intervention mechanisms necessary to accomplish rapid energy redistribution in response to TR events

Rate of energy transfer is critical to response efficacy; goal for electrical system is to redistribute stored energy as rapidly as possible without damaging power conversion hardware



# 3 System Under Consideration

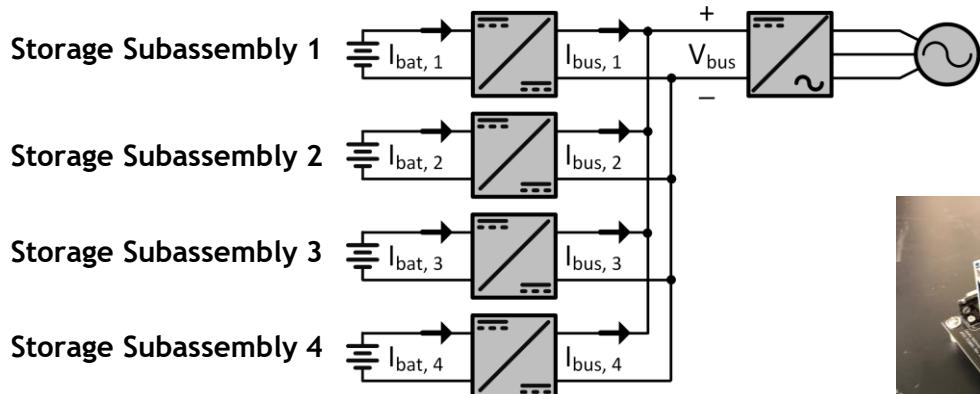


Two structural requirements for energy redistribution:

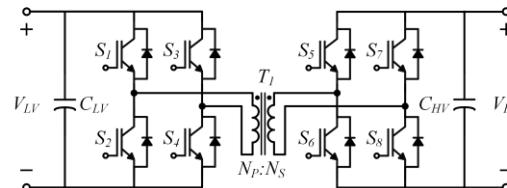
- Subassembly-level charge/discharge control
- A shared bus through which energy is exchanged

Simple example – Module-interfaced storage with parallel DC bus connection

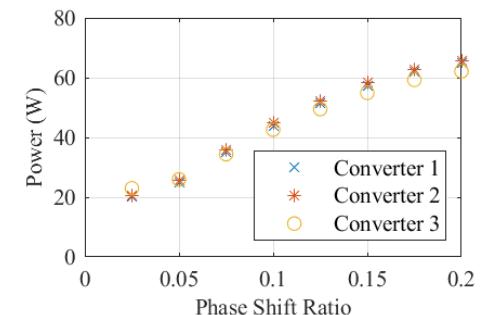
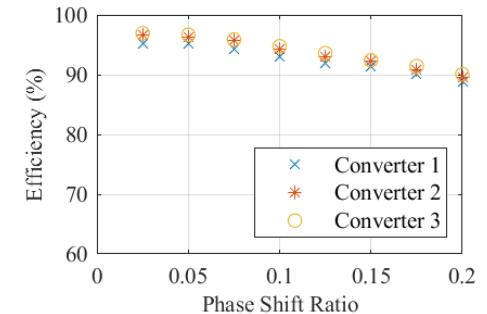
- A common system architecture for hybrid storage, “second-life” battery systems, etc.
- DC-DC converters perform charge control, DC link acts as shared bus after inverter disconnects



Low-Voltage Demonstration System



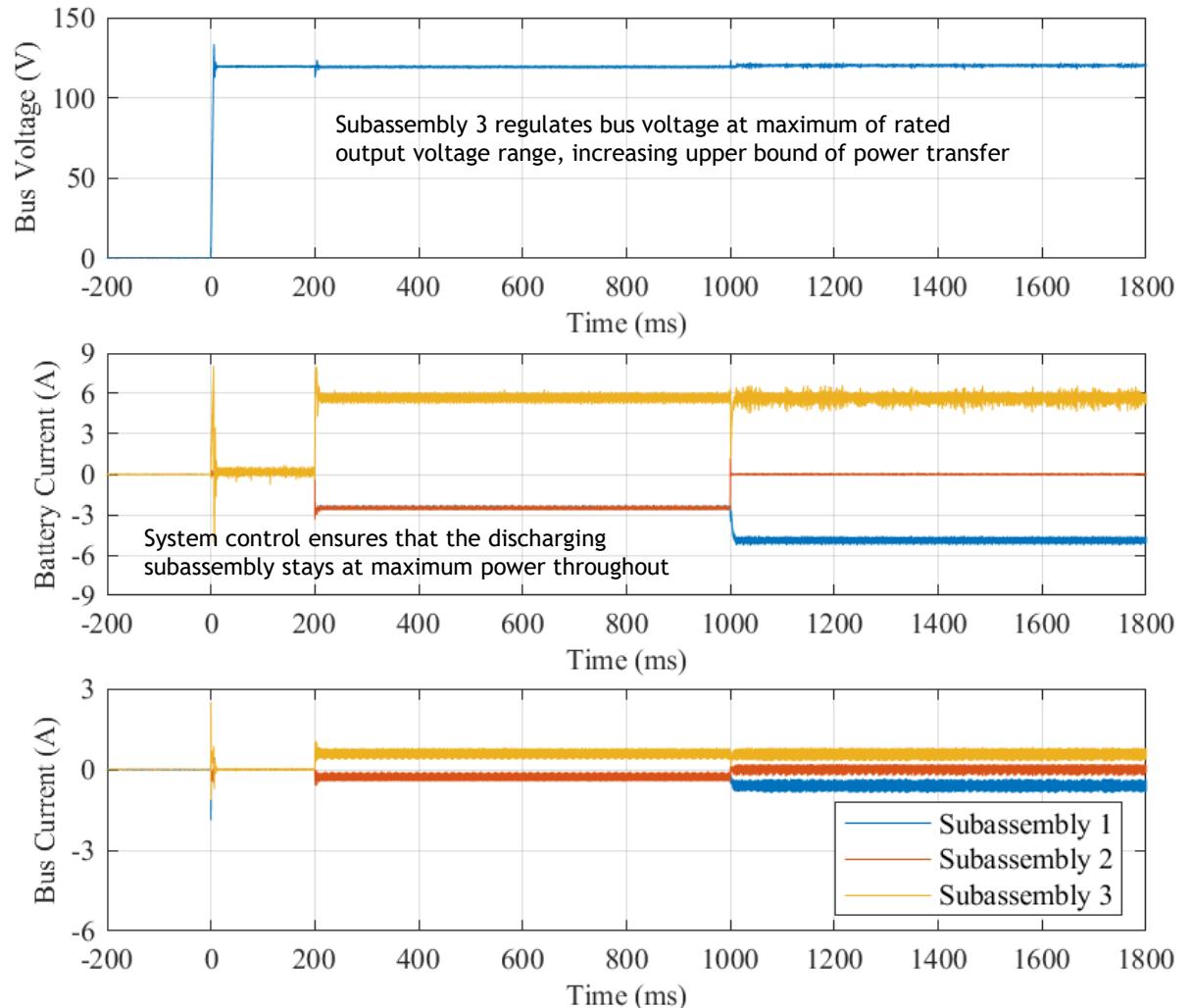
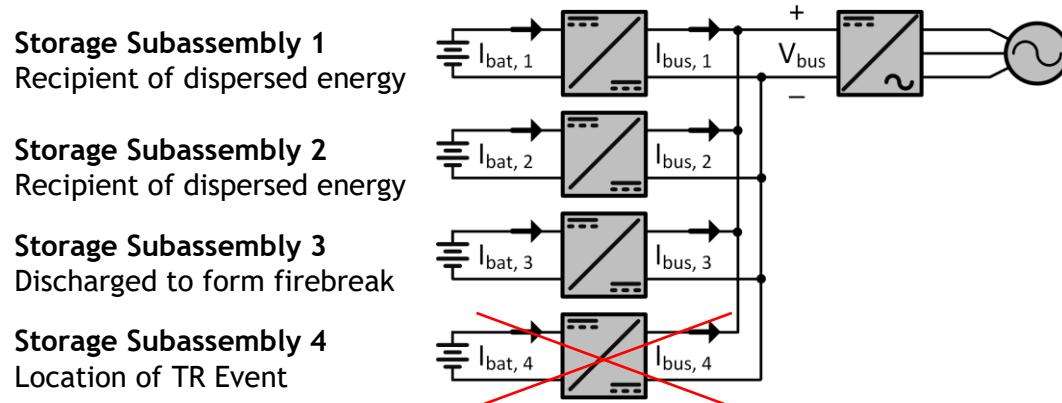
Converter Specifications	
Low-Side Voltage ( $V_{LV}$ )	11V-15V, 12V nom
High-Side Voltage ( $V_{HV}$ )	88V-120V, 96V nom
Switching Freq ( $f_{sw}$ )	100 kHz
Rated Power (P)	$\pm 60W$
Turns Ratio ( $N_p:N_s$ )	5:40



# Results From Low-Voltage Prototype System



- $t < 0\text{ms}$  TR event detected. Inverter has isolated from local grid connection and bus voltage has dropped to 0V.
- $t = 0\text{ms}$  Subassembly 3 is to be depleted. Its converter begins regulating the DC bus voltage at 120V.
- $t = 200\text{ms}$  Subassemblies 1 and 2, which are able to receive dispersed energy, begin operating in controlled current mode, charging their respective storage devices at 2.5A.
- $t = 1000\text{ms}$  Subassembly 2 reaches maximum capacity and is no longer able to receive energy; its charging current drops to 0A. Charging current for subassembly 1 increases to 5A.



# 5 Conclusions and Next Steps

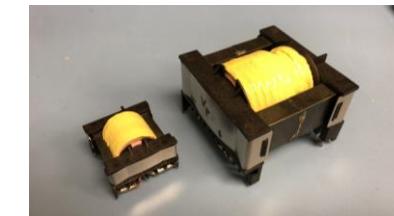


## Key Outcomes:

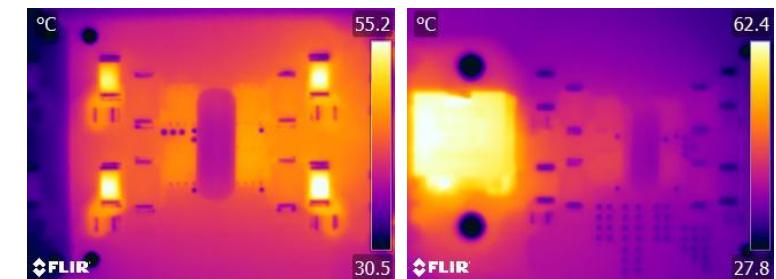
- Results from simplified low-voltage prototype system indicate feasibility of rapid charge transfer between battery subassemblies through shared bus
- Identified requirements for electrical system stability during large-signal transients resulting from energy dispersion actions (i.e. 0 to  $>100\%$  power output)
- Developed multi-converter hardware and control platform, which will be used in the coming year to further study dynamic behaviors of paralleled converters and optimize rates of response
- Filed nonprovisional patent application on energy redistribution concept

## Next Steps:

- Replicate results at practical scale
- Quantify risk acceptance problem for operating converters beyond rated limits in emergency response scenarios
  - How far do you push a converter beyond its normal limits if it could potentially prevent cascading failures and total system loss?
  - How far can normal operating limits be pushed, and for how long?
- Implement control algorithm for optimal redistribution based on system configuration, location of fault



High-frequency transformers for current prototype (60W) and forthcoming converter revision (600W)



Component temperatures in DAB converter at low side (left) and high side (right) H-bridges when operating at 50% above max rated power

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