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Fluid-shell interactions using non-intrusive coupling based on the Immersed Finite Element Method

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Fluid-structure involving thin solid



In Nature: insect flapping wings [1]



Engineering : thin-shell roof structure [2]

[1] <https://en.wikipedia.org/wiki/Dragonfly>

[2] https://en.wikipedia.org/wiki/Thin-shell_structure

Introduction

FSI simulation for thin structures

Boundary conforming mesh

❑ Arbitrary Lagrangian-Eulerian

- Sawada et al. (2007) [1]
- Expensive mesh update for large deformation

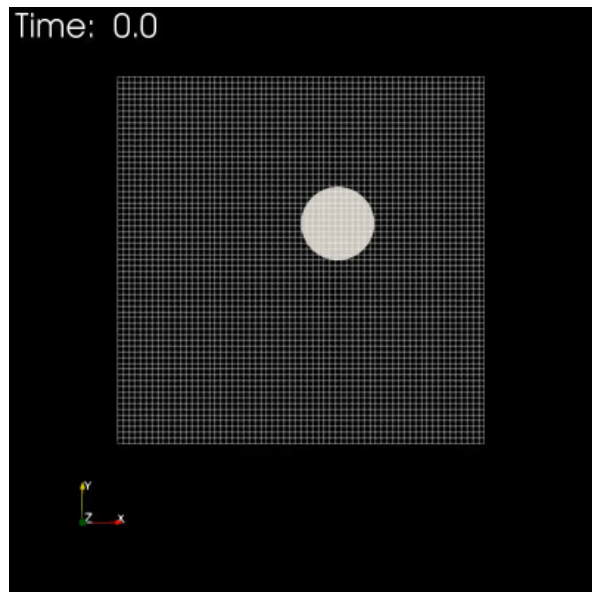
Boundary non-conforming mesh

❑ Immersed Boundary Method

- Peskin (2002) [2]
- Solid and fluid domain:
independent meshes

- Cirak et al. (2007) [3], Gilmanov et al. (2005) [4], Tian et al. [5]
- Lacks volume representation of solid
- Smeared interface
- Inaccurate solid interface loading conditions accounting for both forces and moments

Objective



- **Objective:**
 - Develop a **robust fluid-shell coupling** strategy using immersed approach.
- **Modified Immersed Finite Element Method (mIFEM) [1]:**
 - **Volume based interpolation** and **sharp interface**.
- **OpenIFEM [2], [3]:** Open source software based on mIFEM
 - Modularly couple OpenIFEM with external shell solver.

[1] Xingshi Wang and Lucy T. Zhang. Modified immersed finite element (2013)

[2] Cheng J et al.. OpenIFEM: A high performance modular open-source software fluid-structure interactions. (2019)

[3] <https://github.com/OpenIFEM>

mIFEM Fluid-Solid Coupling Formulation

virtual work done by the real fluid

virtual work done by the solid

$$\int_{\Omega^f} \delta v_i \left(\rho^f \frac{Dv_i^f}{Dt} - \sigma_{ij,j}^f - \rho^f g_i \right) d\Omega + \int_{\Omega^s} \delta v_i \left(\rho^s \frac{Dv_i^s}{Dt} - \sigma_{ij,j}^s - \rho^s g_i \right) d\Omega = 0$$

$$\int_{\bar{\Omega}} \delta v_i \left(\rho^s \frac{Dv_i^f}{Dt} - \sigma_{ij,j}^f - \rho^s g_i \right) d\Omega + \int_{\Omega^s} \delta v_i \left(\rho^s \left(\frac{Dv_i^s}{Dt} - \frac{Dv_i^f}{Dt} \right) - (\sigma_{ij,j}^s - \sigma_{ij,j}^f) \right) d\Omega$$

$$\bar{\rho} = \begin{cases} \rho^s & \text{in } \Omega^s \\ \rho^f & \text{in } \Omega^f \end{cases}$$

$$-F_i^{\text{FSI}}$$

$$\int_{\Omega} \delta v_i \left(\bar{\rho} \frac{\partial v_i^f}{\partial t} + \bar{\rho} v_j^f v_{i,j}^f - \sigma_{ij,j}^f - \bar{\rho} g_i \right) d\Omega = \int_{\Omega^s} \delta v_i F_i^{\text{FSI}} d\Omega$$

solid

$$\rho^s u_{,tt} = \sigma_{ij}^s \quad \text{in } \Omega^s$$

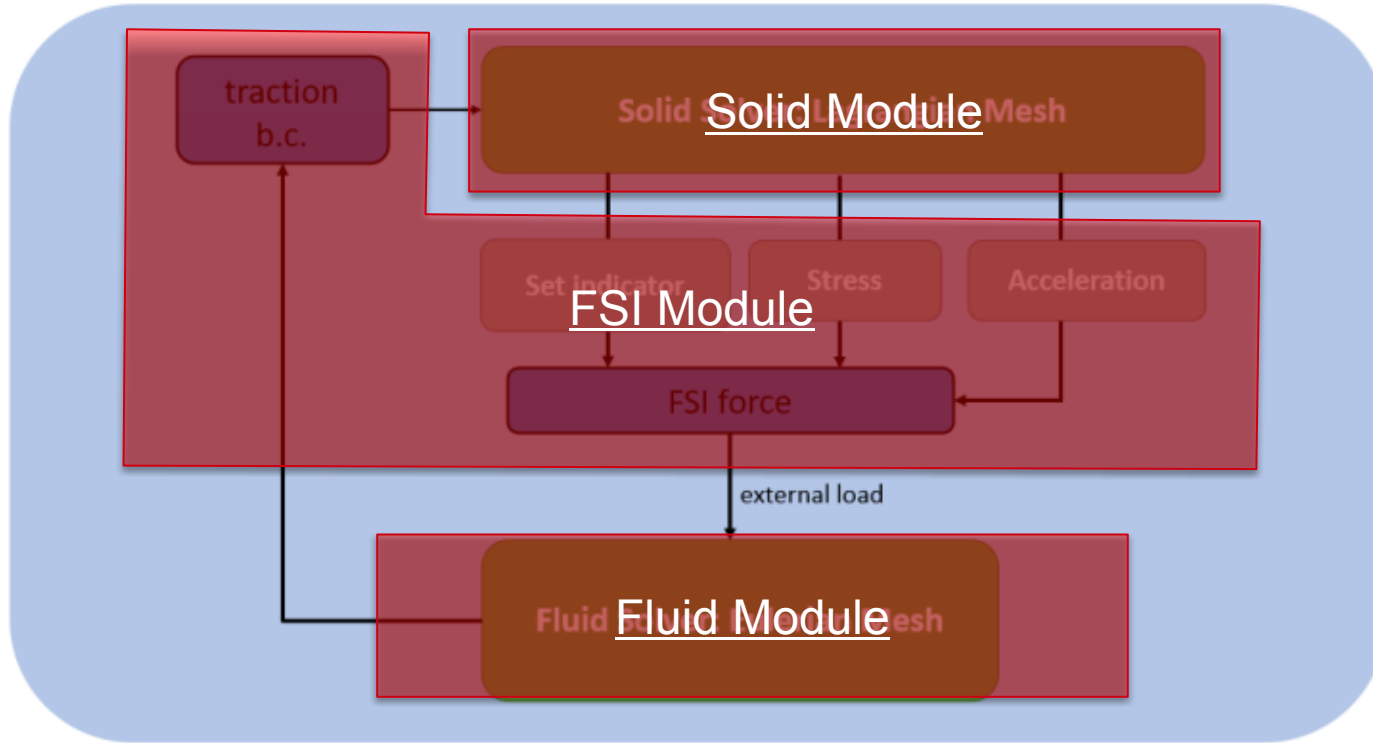
$$u_i = q_i = v_i^j L_j^s \quad \text{on } \Gamma^{sq}$$

$$\sigma_{ij}^s n_j = h_i = -\sigma_{ij}^f n_j \quad \text{on } \Gamma^{sh}$$

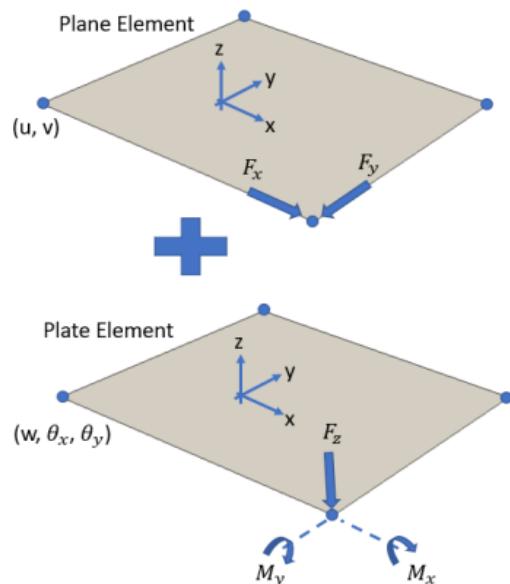
fluid

$$\bar{\rho} \left(\frac{\partial v_i^f}{\partial t} + v_j^f v_{i,j}^f \right) = \sigma_{ij,j}^f + f_i^{\text{FSI}}(\mathbf{x}, t)$$

mIFEM Workflow



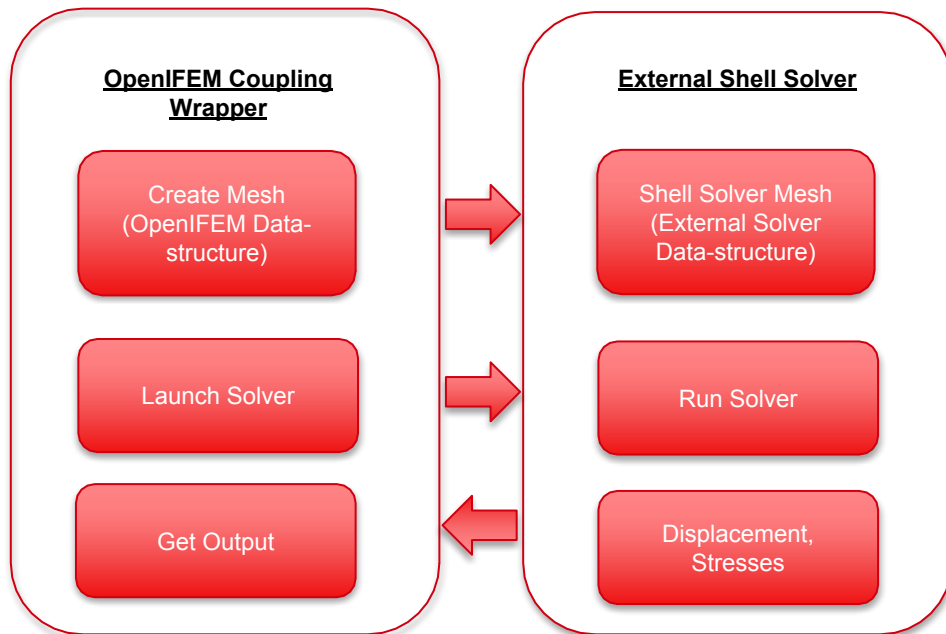
Shell Solver

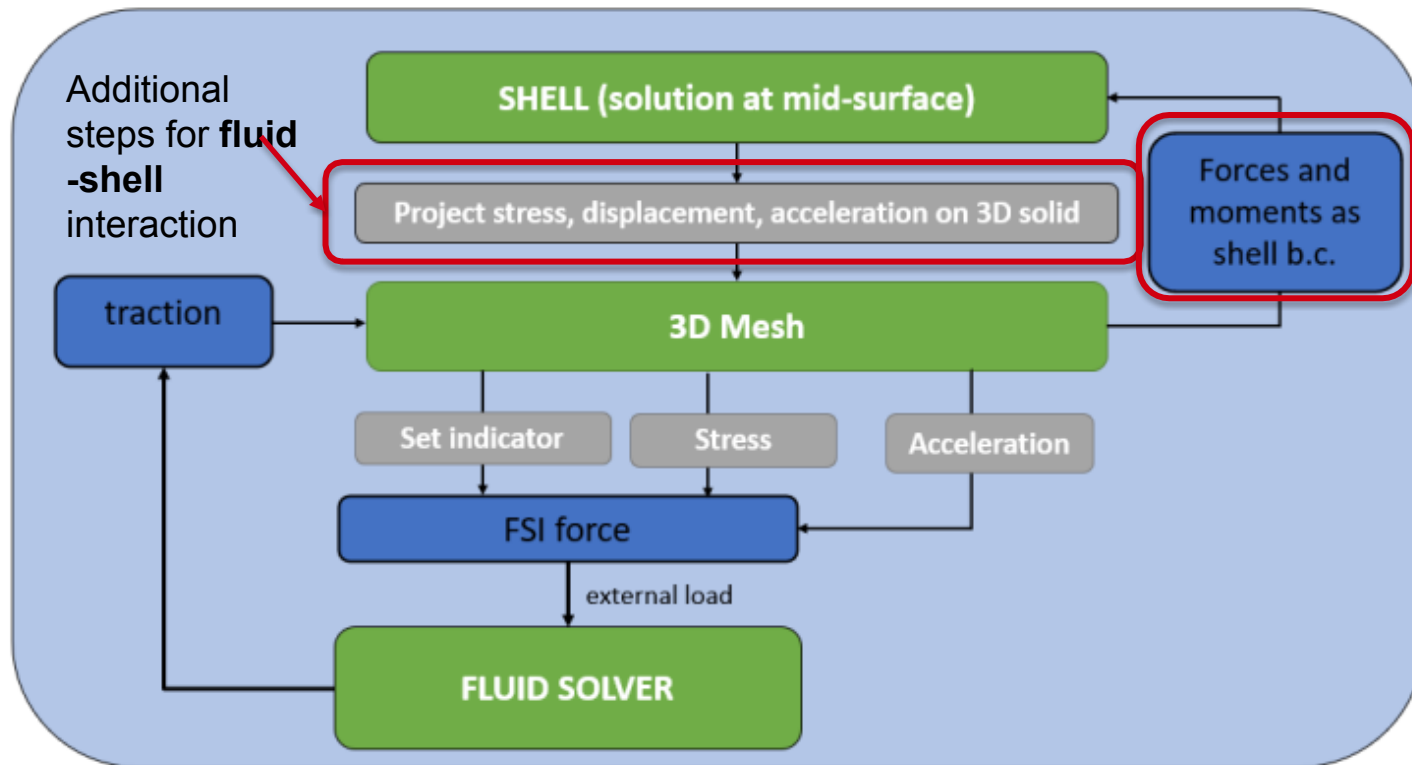


- External shell solver [4]: **flat shell theory**
- Shell Element: **6 d.o.f.** : (u, v, w, θ_x , θ_y , θ_z)

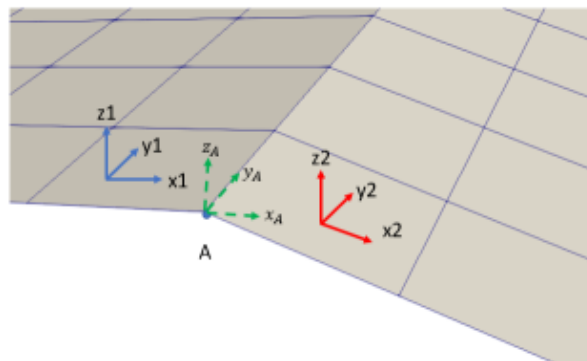
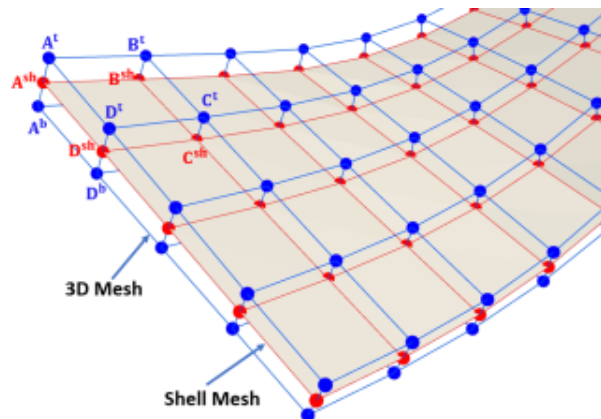
[4] <https://github.com/precice/fem-shell>

Coupling Wrapper Workflow





Project solution on 3D solid



Local coordinate system

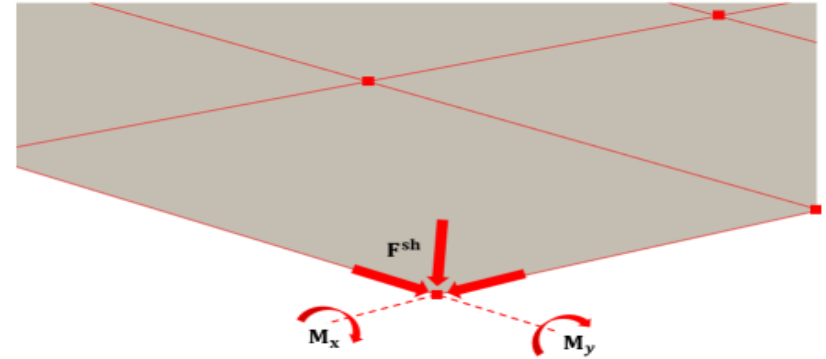
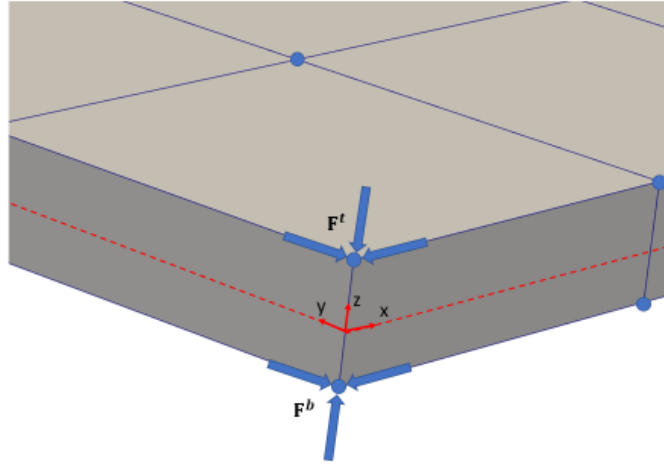
- Define Local coordinate system for each node.
- Local coordinate system at node A:

$$x_A = \frac{x1+x2}{||x1+x2||} \quad y_A = \frac{y1+y2}{||y1+y2||} \quad z_A = \frac{z1+z2}{||z1+z2||}$$
- Transformation matrix: $T_A = \begin{bmatrix} x_A \\ y_A \\ z_A \end{bmatrix}$

Project solution to 3D mesh

- Create 3D solid mesh and extrapolate solution from shell to 3D mesh to appropriate nodes:
 - $(u, v, w, \theta_x, \theta_y, \theta_z)_{global} \rightarrow (u, v, w, \theta_x, \theta_y, \theta_z)_{local}$
 - $U_{local} = u_{local} - z * (\theta_y)_{local} \quad -t/2 \leq z \leq t/2$
 - $V_{local} = v_{local} - z * (\theta_x)_{local}$
 - $W_{local} = w_{local}$
 - $(U, V, W)_{local} \rightarrow (U, V, W)_{global}$
- Similarly project velocity, acceleration and stress.

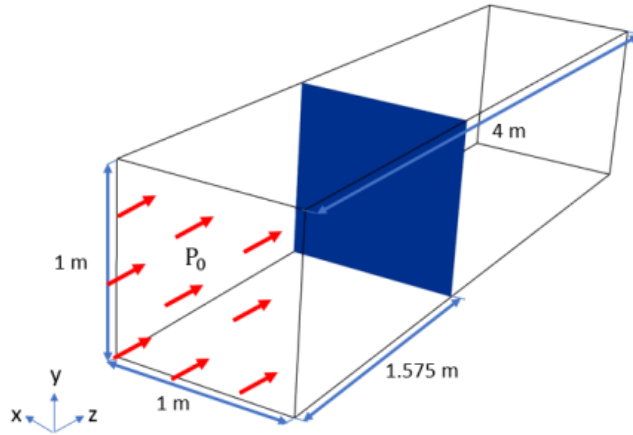
Evaluate forces and moments onto shell surface



- Evaluate solid traction from fluid stress: $\mathbf{t} = [-\mathbf{p}\mathbf{I} + \mu(\nabla\mathbf{v} + \nabla\mathbf{v}^T)].\mathbf{n}$
- Calculate nodal forces on volume (two sides)

- **Equivalent forces on shell node:** $F^{sh} = F^b + F^t$
- **Equivalent Moments on shell node:**
 - Transfer force into local coordinates
 - $M_y = F_x^t * \frac{t}{2} - F_x^b * \frac{t}{2}$
 - $M_x = -F_y^t * \frac{t}{2} + F_y^b * \frac{t}{2}$
 - Transfer moments into global coordinates

Test Cases 1: Setup



- Shell Dimensions: 1 m x 1 m
- Shell thickness: 0.05 m

- **Objective:** Verify that FSI coupling, **no numerical leaking**

Material Properties:

- Fluid Properties:
 - Viscosity : 1.8×10^{-5} Pa.s
 - Density : 1.3 kg/m^3
- Solid Properties:
 - Young's Modulus : 10^4 Pa
 - Poisson's Ration: 0.3
 - Density : 1000.0 kg/m^3

Boundary Conditions:

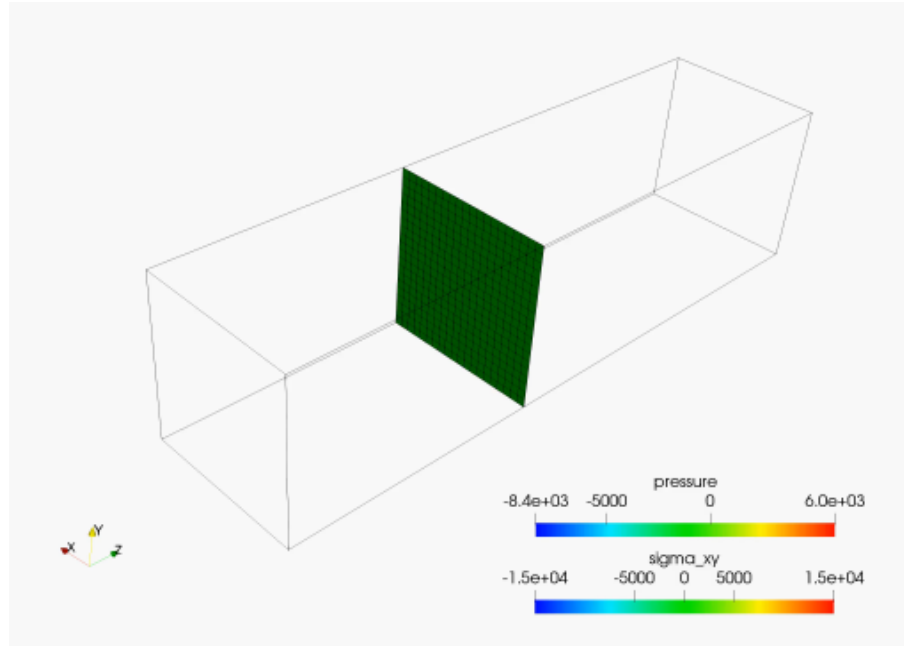
- Fluid:
 - left (inlet) : constant pressure inlet
 $P_0 = 500 \text{ Pa}$
 - right boundary : outflow
 - Other boundaries: no penetration
- Solid:
 - All sides clamped.

Time Step:

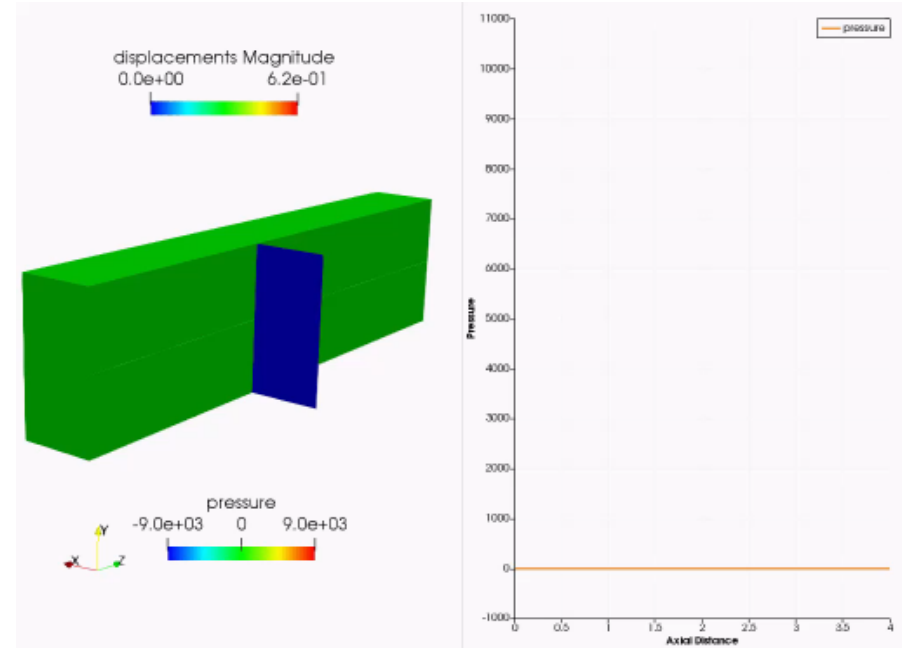
- Time Step: 10^{-6} s
- Final Time: 6×10^{-3} s

Test Case 1: Results

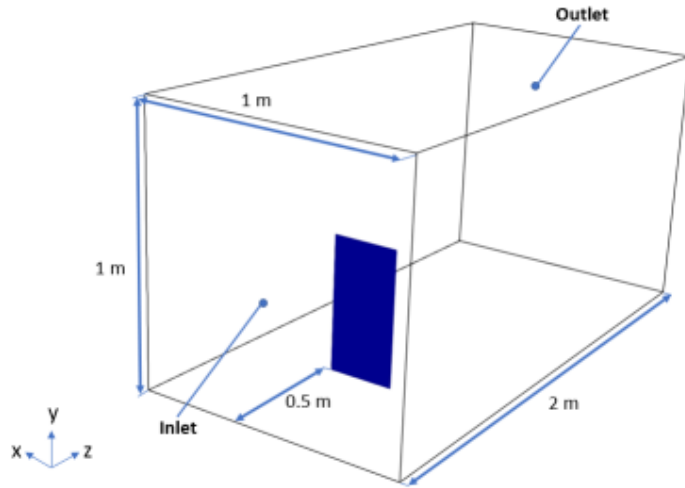
Flow streamlines coloured by pressure (Pa) and solid stress σ_{xy} on top surface (Pa)



Cross section of fluid domain and pressure (Pa) vs. time (s) along centreline



Test Cases 2: Setup



- Shell Dimensions: 0.5 m x 0.25m
- Shell thickness: 0.0125 m
- Shell thickness: 0.00625 m
- Shell thickness: 0.003125 m

- **Objective:** Demonstrate FSI coupling for problem with **large deformation**.

Material Properties:

- Fluid Properties:
 - Viscosity : 1.8×10^{-5} Pa.s
 - Density : 1.3 kg/m^3
- Solid Properties:
 - Young's Modulus : 10^3 Pa
 - Poisson's Ration: 0.4
 - Density : 5000.0 kg/m^3
- Re: 20

Boundary Conditions:

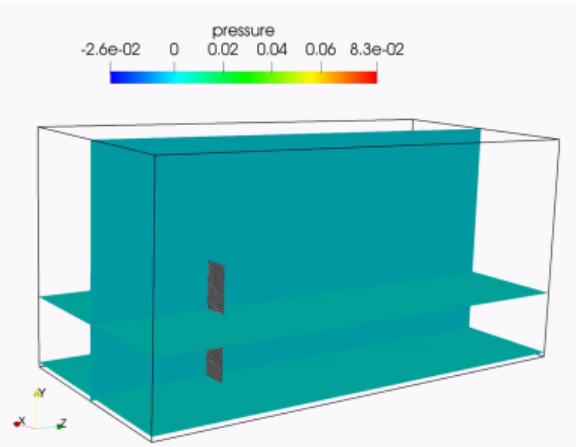
- Fluid:
 - left (inlet) : constant velocity inlet $V_0 = 0.05 \text{ m/s}$
 - right boundary : outflow
 - bottom: no slip
 - front, back, top: no penetration
- Solid:
 - Bottom side clamped.

Time Step:

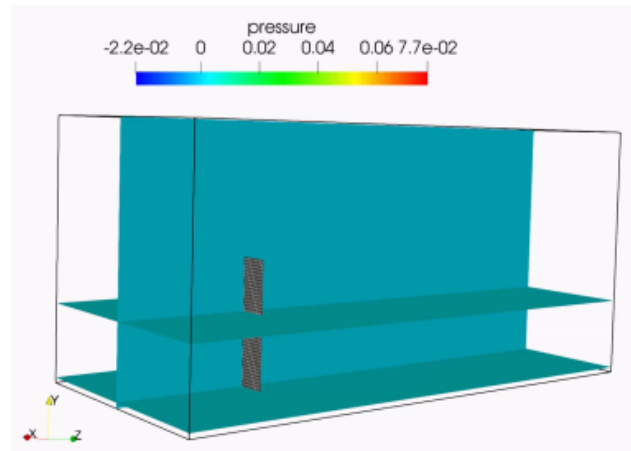
- Time Step: $2 \times 10^{-4} \text{ s}$
- Final Time: 1 s

Test Cases 2: Result

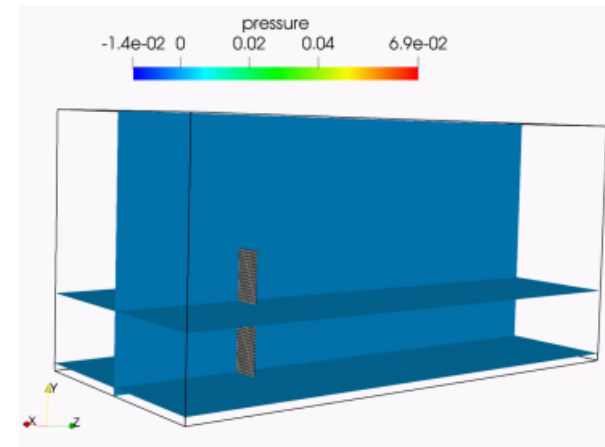
Fluid pressure contours (Pa) at various cross sections



Thickness: 0.0125 m



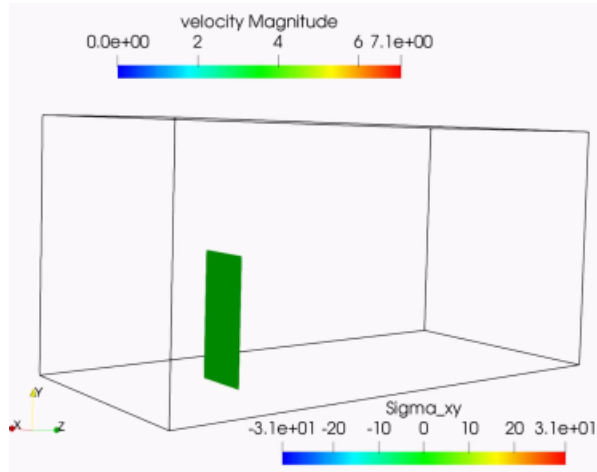
Thickness: 0.00625 m



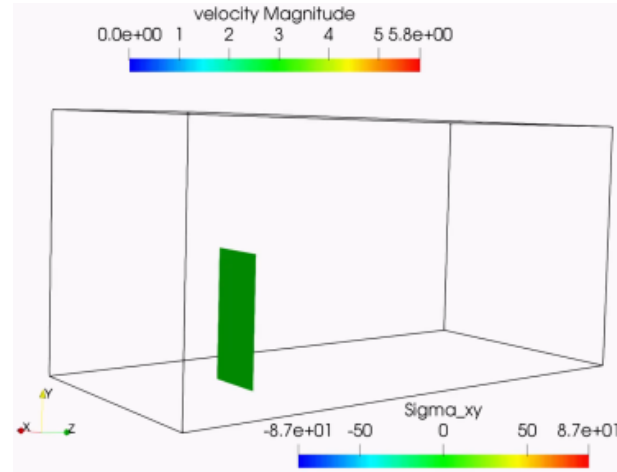
Thickness: 0.003125 m

Test Cases 2: Result

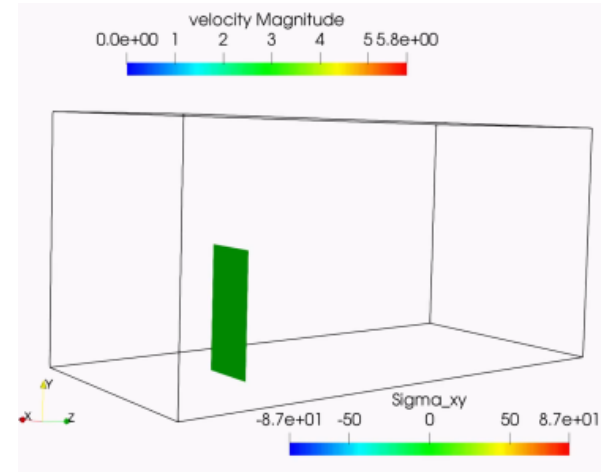
Flow streamlines coloured by velocity (m/s) and solid stress σ_{xy} on top surface (Pa)



Thickness: 0.0125 m

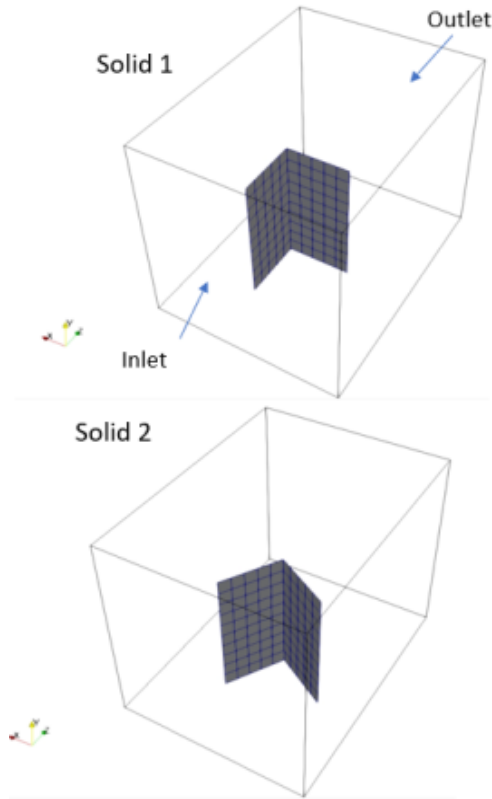


Thickness: 0.00625 m



Thickness: 0.003125 m

Test Cases 3: Setup



- **Objective:** Demonstrate that the solver can handle **shapes with bends** or shells in **different planes**. Demonstrate use of **local coordinate system**.

Material Properties:

- Fluid Properties:
 - Viscosity : 1.8×10^{-5} Pa.s
 - Density : 1.3 kg/m^3
- Solid Properties:
 - Young's Modulus : 10^3 Pa
 - Poisson's Ration: 0.4
 - Density : 5000.0 kg/m^3

Boundary Conditions:

- Fluid:
 - left (inlet) : constant velocity inlet $V_0 = 0.1 \text{ m/s}$
 - right boundary : outflow
 - bottom: no slip
 - front, back, top: no penetration
- Solid:
 - Bottom side clamped.

Time Step:

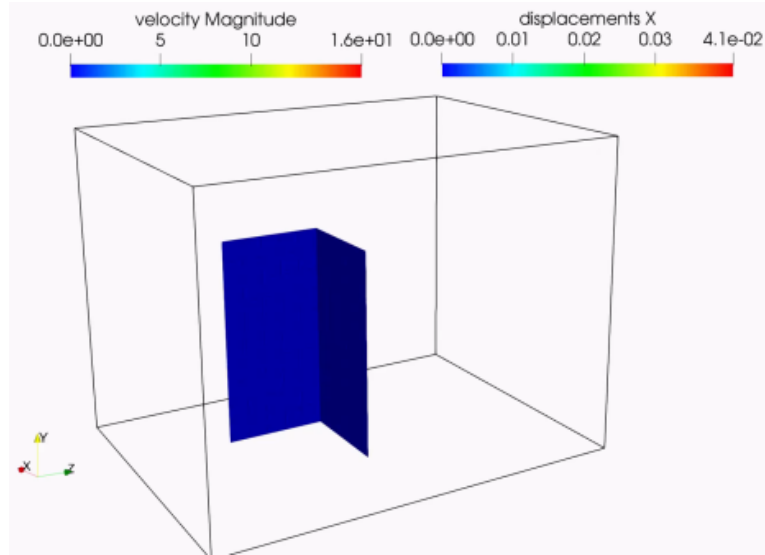
- Time Step: $2 \times 10^{-4} \text{ s}$
- Final Time: 1 s

Problem Setup:

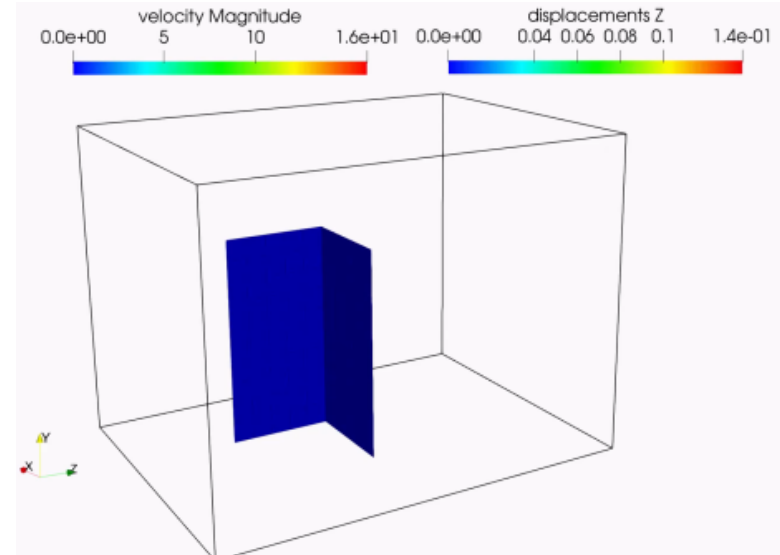
- Fluid: $1.5 \text{ m} \times 1.5 \text{ m} \times 2 \text{ m}$
- Solid:
 - $0.5 \text{ m} \times 1 \text{ m}$ rectangles intersect at right angle
 - Thickness: 0.0125 m

Test Cases 3 : Results

Solid 1 (90^0)



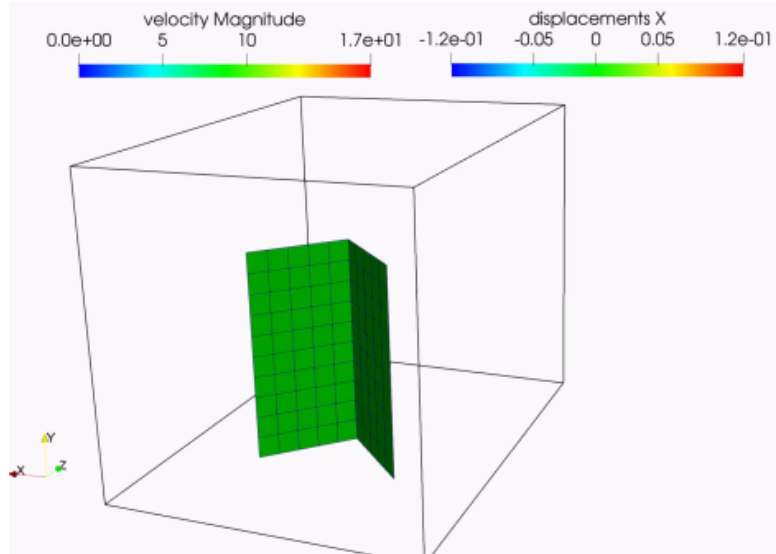
Flow streamlines coloured by velocity (m/s) and solid displacement in x direction (m)



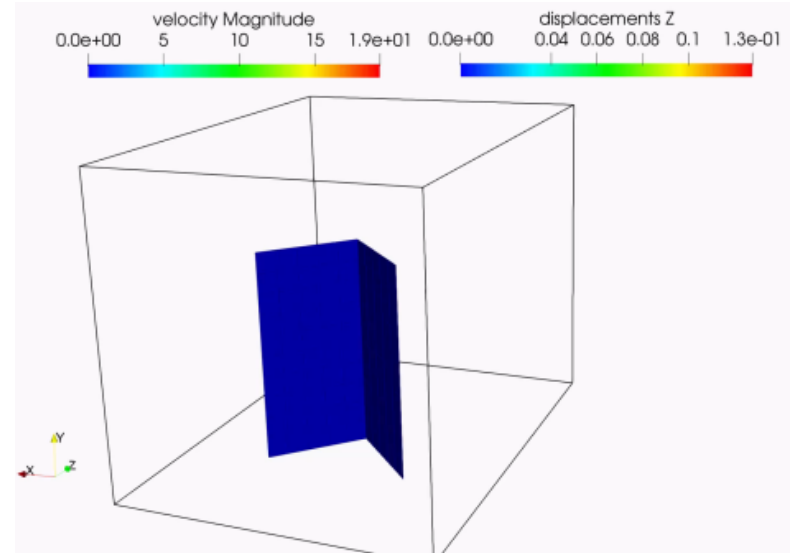
Flow streamlines coloured by velocity (m/s) and solid displacement in z direction (m)

Test Cases 3 : Results

Solid 2 (45°)



Flow streamlines coloured by velocity (m/s) and solid displacement in x direction (m)



Flow streamlines coloured by velocity (m/s) and solid displacement in z direction (m)

Summary

- **Modularly** couple an external shell solver with OpenIFEM.
- **Extend** OpenIFEM capabilities for shell structures.
 - Represent thin shell with given finite thickness
 - Realistic solid loading which accounts for both forces and moments
 - Adoptable for different shell formulations
- OpenIFEM can handle **both general 3D bodies and different types of shells**.

Acknowledgment

- Funding and Resources:
 - Sandia National Laboratories
- OpenIFEM :
 - Feimi Yu for developing coupling wrapper for shell solver.

References

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- [4] Anvar Gilmanov, Trung Bao Le, and Fotis Sotiropoulos. A numerical approach for simulating fluid structure interaction of flexible thin shells undergoing arbitrarily large deformations in complex domains. *Journal of computational physics*, 300:814–843, 2015.
- [5] Fang-Bao Tian, Hu Dai, Haoxiang Luo, James F Doyle, and Bernard Rousseau. Fluid–structure interaction involving large deformations: 3d simulations and applications to biological systems. *Journal of computational physics*, 258:451–469, 2014



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