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Fluid-shell interactions using non-intrusive coupling based on the Immersed Finite Element Method

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Motivation

Fluid-structure involving thin solid



In Nature: insect flapping wings [1]



Engineering : thin-shell roof structure [2]

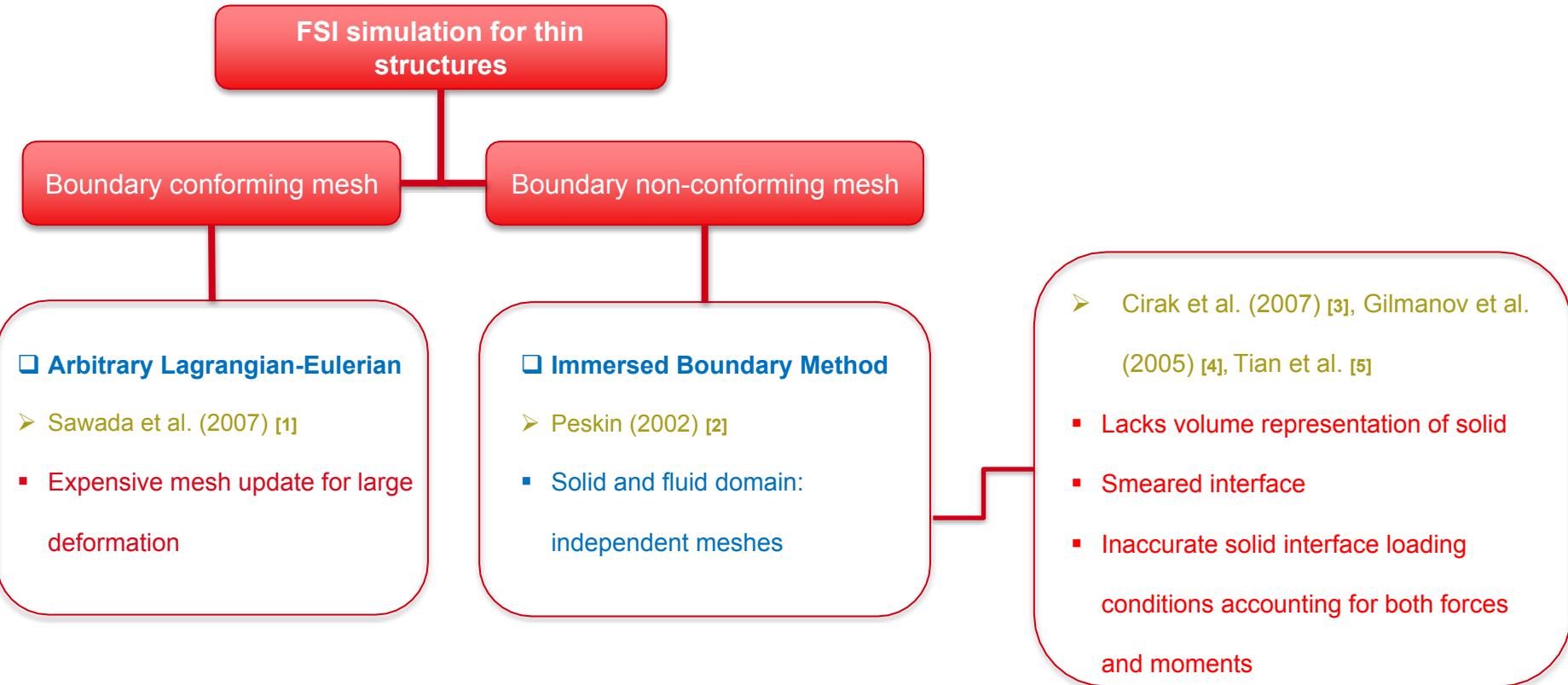
[1] <https://en.wikipedia.org/wiki/Dragonfly>

[2] https://en.wikipedia.org/wiki/Thin-shell_structure



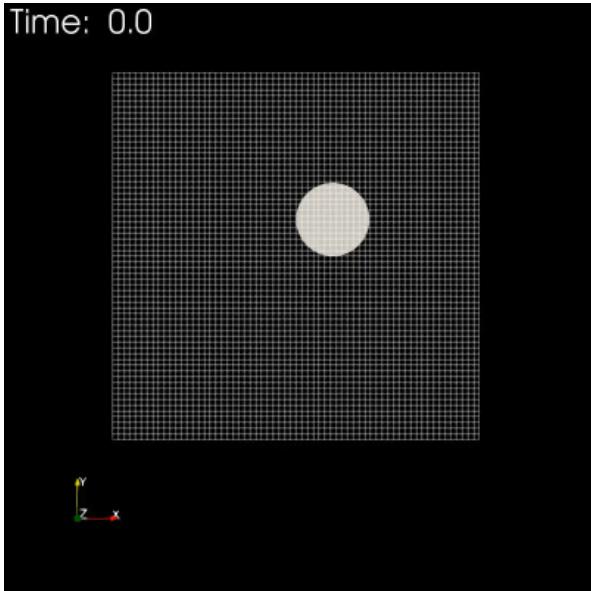
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Introduction



Objective

Time: 0.0



- **Objective:**

- Develop a **robust fluid-shell coupling** strategy using immersed approach.

- **Modified Immersed Finite Element Method (mIFEM) [1]:**

- **Volume based interpolation** and **sharp interface**.

- **OpenIFEM [2], [3]:** Open source software based on mIFEM

- Modularly couple OpenIFEM with external shell solver.

[1] Xingshi Wang and Lucy T. Zhang. Modified immersed finite element (2013)

[2] Cheng J et al., OpenIFEM: A high performance modular open-source software fluid-structure interactions. (2019)

[3] <https://github.com/OpenIFEM>



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mIFEM Fluid-Solid Coupling Formulation

virtual work done by the real fluid

$$\int_{\Omega^f} \delta v_i \left(\rho^f \frac{Dv_i^f}{Dt} - \sigma_{ij,j}^f - \rho^f g_i \right) d\Omega + \int_{\Omega^s} \delta v_i \left(\rho^s \frac{Dv_i^s}{Dt} - \sigma_{ij,j}^s - \rho^s g_i \right) d\Omega = 0$$

virtual work done by the solid

$$\int_{\Omega} \delta v_i \left(\rho^s \frac{Dv_i^f}{Dt} - \sigma_{ij,j}^f + \rho^s g_i \right) d\Omega + \int_{\Omega^s} \delta v_i \left(\rho^s \left(\frac{Dv_i^s}{Dt} - \frac{Dv_i^f}{Dt} \right) - (\sigma_{ij,j}^s - \sigma_{ij,j}^f) \right) d\Omega$$

$$\bar{\rho} = \begin{cases} \rho^s & \text{in } \Omega^s \\ \rho^f & \text{in } \Omega^f \end{cases}$$

$$-F_i^{\text{FSI}}$$

$$\int_{\Omega} \delta v_i \left(\bar{\rho} \frac{\partial v_i^f}{\partial t} + \bar{\rho} v_j^f v_{i,j}^f - \sigma_{ij,j}^f - \bar{\rho} g_i \right) d\Omega = \int_{\Omega^s} \delta v_i F_i^{\text{FSI}} d\Omega$$



mIFEM Governing Equations

solid

$$\rho^s u_{,tt} = \sigma_{ij}^s \quad \text{in } \Omega^s$$

Lagrangian on Γ^{sq}

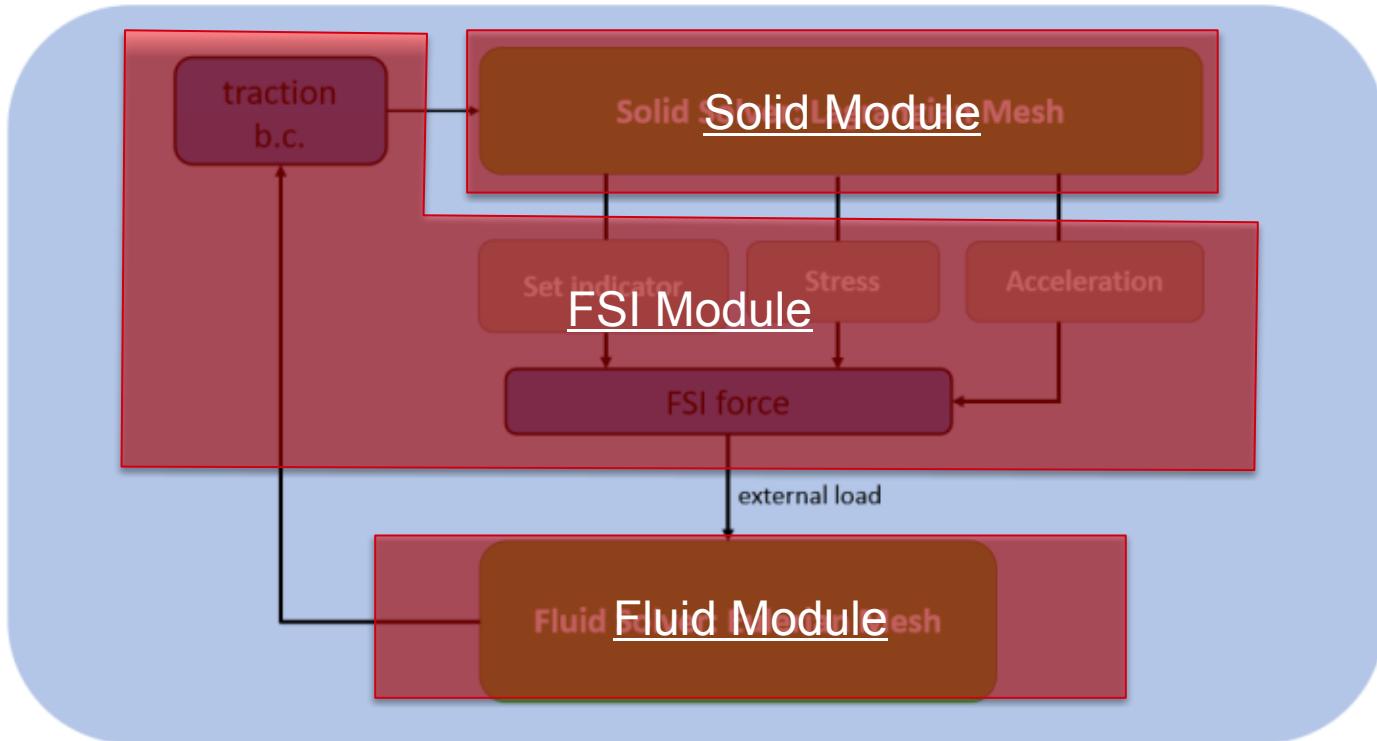
$$\sigma_{ij}^s n_j = h_i = -\sigma_{ij}^f n_j \quad \text{on } \Gamma^{\text{sh}}$$

fluid

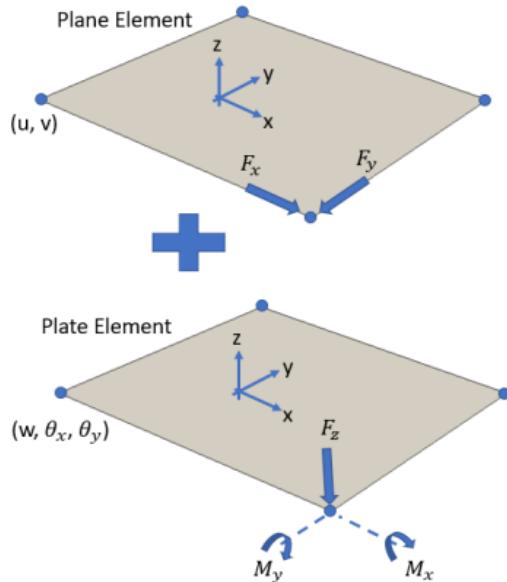
$$\bar{\rho} \left(\frac{\partial v_i^f}{\partial t} + v_j^f v_{i,j}^f \right) = \sigma_{ij,j}^f + f_i^{\text{FSI}}(\mathbf{x}, t)$$



mIFEM Workflow



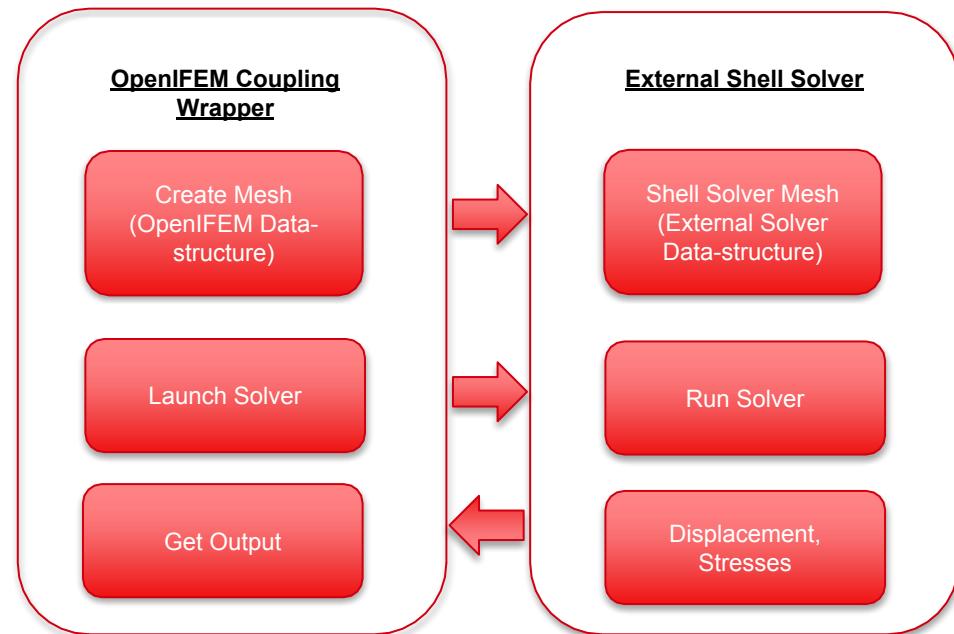
Shell Solver



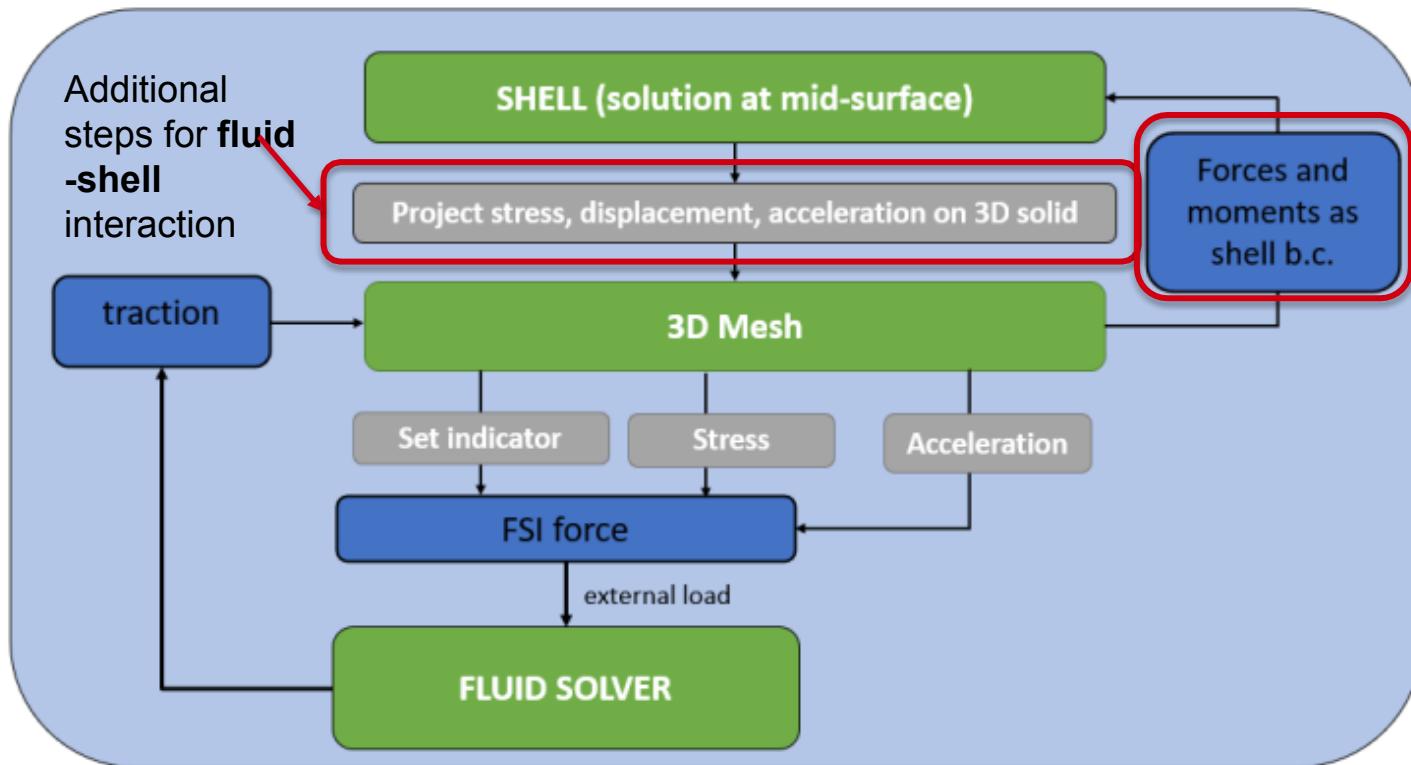
- External shell solver [4]: **flat shell theory**
- Shell Element: **6 d.o.f.** : $(u, v, w, \theta_x, \theta_y, \theta_z)$

[4] <https://github.com/precice/fem-shell>

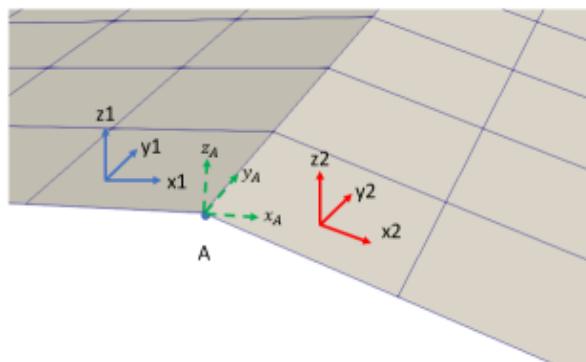
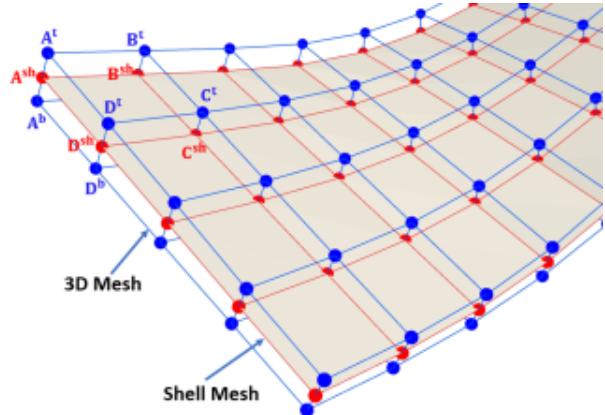
Coupling Wrapper Workflow



mIFEM for shell



Project solution on 3D solid



Local coordinate system

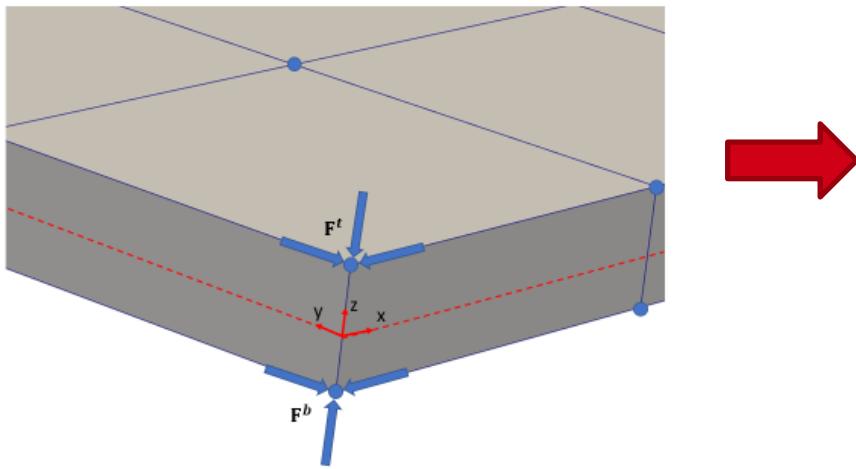
- Define Local coordinate system for each node.
- Local coordinate system at node A:
$$x_A = \frac{x_1+x_2}{\|x_1+x_2\|} \quad y_A = \frac{y_1+y_2}{\|y_1+y_2\|} \quad z_A = \frac{z_1+z_2}{\|z_1+z_2\|}$$
- Transformation matrix: $T_A = \begin{bmatrix} x_A \\ y_A \\ z_A \end{bmatrix}$

Project solution to 3D mesh

- Create 3D solid mesh and extrapolate solution from shell to 3D mesh to appropriate nodes:
 - $(u, v, w, \theta_x, \theta_y, \theta_z)_{global} \rightarrow (u, v, w, \theta_x, \theta_y, \theta_z)_{local}$
 - $U_{local} = u_{local} - z * (\theta_y)_{local}$ $-t/2 \leq z \leq t/2$
 - $V_{local} = v_{local} - z * (\theta_x)_{local}$
 - $W_{local} = w_{local}$
 - $(U, V, W)_{local} \rightarrow (U, V, W)_{global}$
- Similarly project velocity, acceleration and stress.



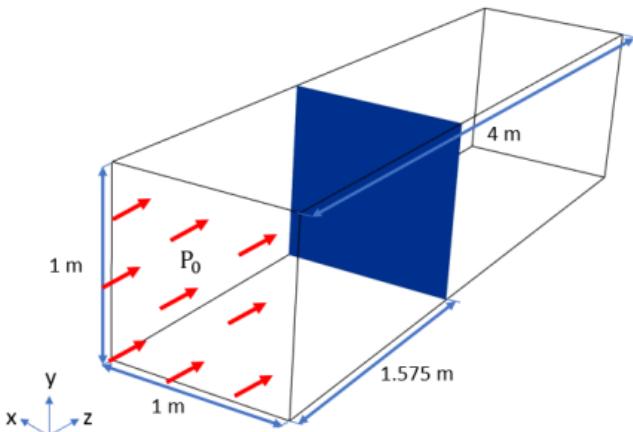
Evaluate forces and moments onto shell surface



- Evaluate solid traction from fluid stress: $t = [-p\mathbf{I} + \mu(\nabla\mathbf{v} + \nabla\mathbf{v}^T)] \cdot \mathbf{n}$
- Calculate nodal forces on volume (two sides)
- Equivalent forces on shell node: $F^{sh} = F^b + F^t$
- Equivalent Moments on shell node:
 - Transfer force into local coordinates
 - $M_y = F_x^t * \frac{t}{2} - F_x^b * \frac{t}{2}$
 - $M_x = -F_y^t * \frac{t}{2} + F_y^b * \frac{t}{2}$
 - Transfer moments into global coordinates



Test Cases 1: Setup



- Shell Dimensions: 1 m x 1m
- **Shell thickness: 0.05 m**

- **Objective:** Verify that FSI coupling, **no numerical leaking**

Material Properties:

- Fluid Properties:
 - Viscosity : $1.8 * 10^{-5}$ Pa.s
 - Density : 1.3 kg/m³
- Solid Properties:
 - Young's Modulus : 10^4 Pa
 - Poisson's Ration: 0.3
 - Density : 1000.0 kg/m³

Boundary Conditions:

- Fluid:
 - left (inlet) : constant pressure inlet $P_0 = 500$ Pa
 - right boundary : outflow
 - Other boundaries: no penetration
- Solid:
 - All sides clamped.

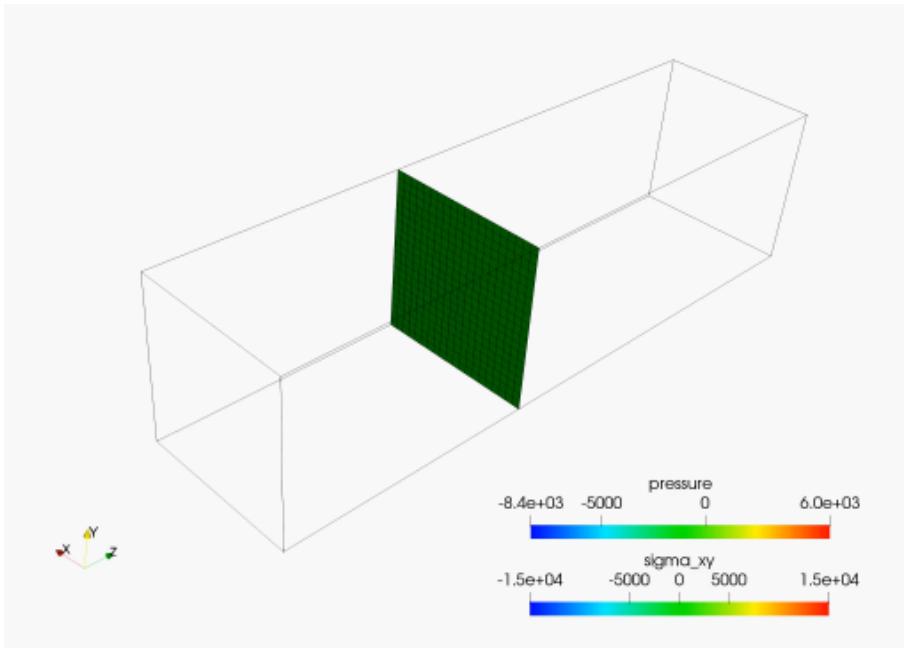
Time Step:

- Time Step: 10^{-6} s
- Final Time: $6 * 10^{-3}$ s

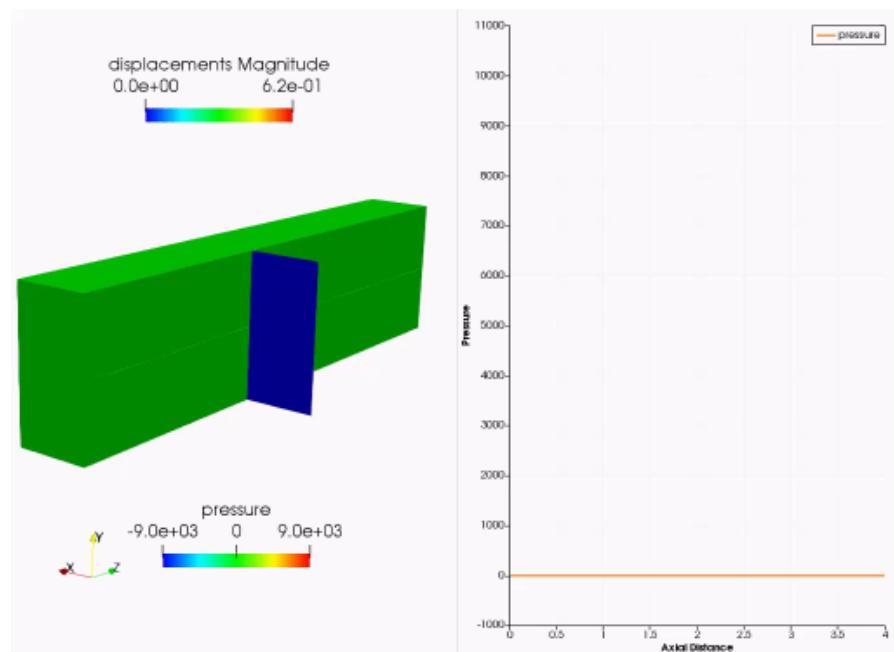


Test Case 1: Results

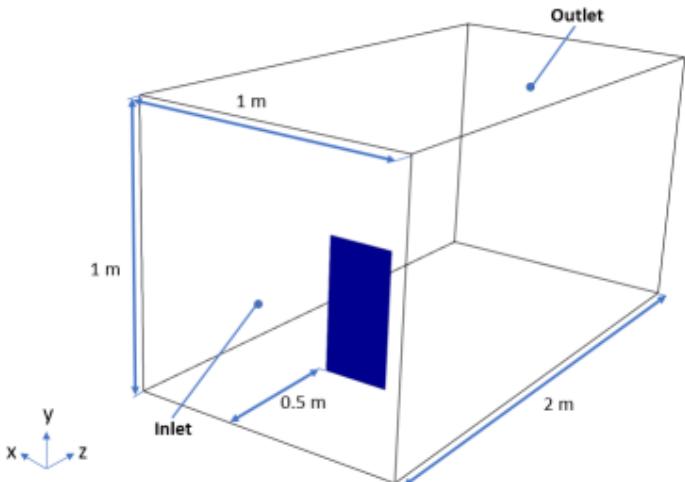
Flow streamlines coloured by pressure (Pa) and solid stress σ_{xy} on top surface (Pa)



Cross section of fluid domain and pressure (Pa) vs. time (s) along centreline



Test Cases 2: Setup



- Shell Dimensions: $0.5 \text{ m} \times 0.25\text{m}$
- **Shell thickness: 0.0125 m**
- **Shell thickness: 0.00625 m**
- **Shell thickness: 0.003125 m**

- **Objective:** Demonstrate FSI coupling for problem with **large deformation**.

Material Properties:

- Fluid Properties:
 - Viscosity: $1.8 \times 10^{-5} \text{ Pa.s}$
 - Density: 1.3 kg/m^3
- Solid Properties:
 - Young's Modulus: 10^3 Pa
 - Poisson's Ration: 0.4
 - Density: 5000.0 kg/m^3
- Re: 20

Boundary Conditions:

- Fluid:
 - left (inlet) : constant velocity inlet $V_0 = 0.05 \text{ m/s}$
 - right boundary : outflow
 - bottom: no slip
 - front, back, top: no penetration
- Solid:
 - Bottom side clamped.

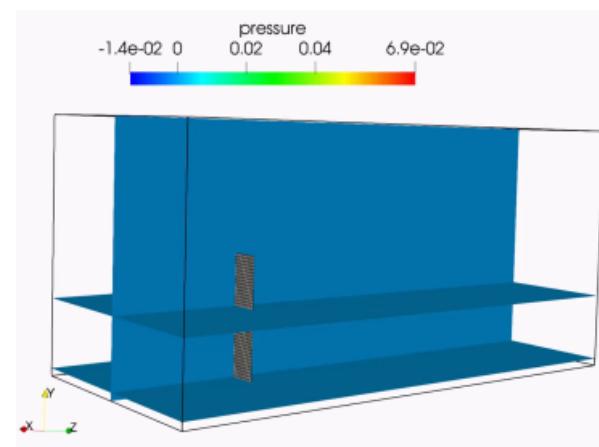
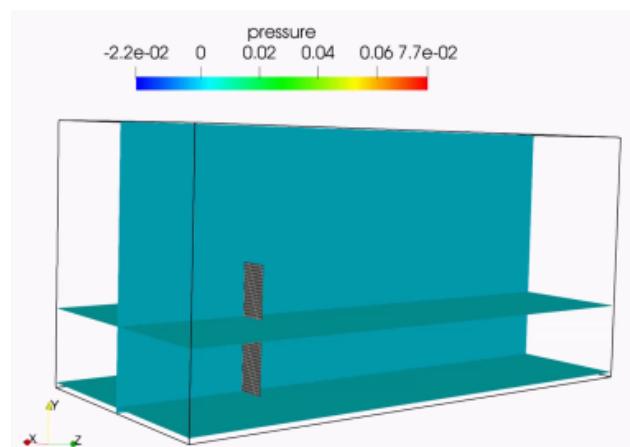
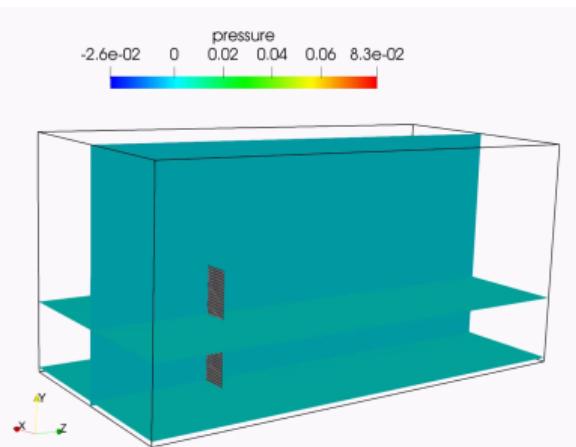
Time Step:

- Time Step: $2 \times 10^{-4} \text{ s}$
- Final Time: 1 s



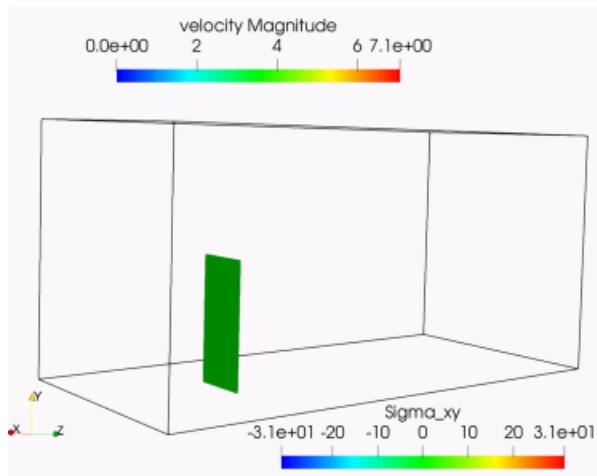
Test Cases 2: Result

Fluid pressure contours (Pa) at various cross sections

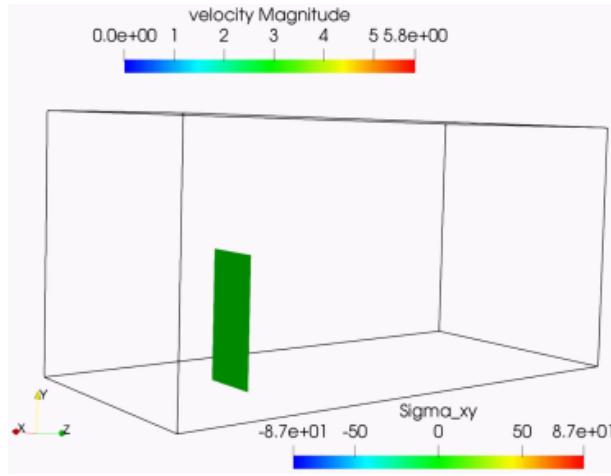


Test Cases 2: Result

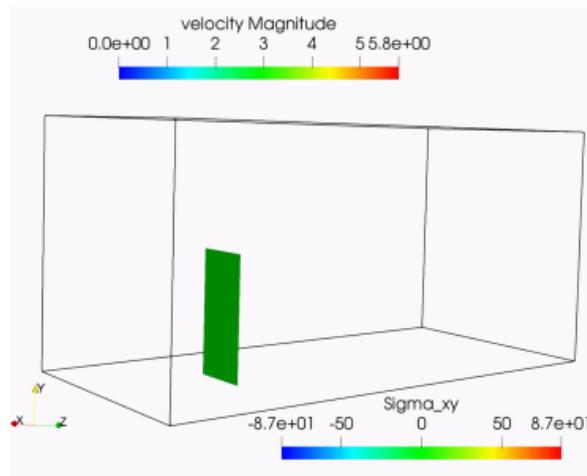
Flow streamlines coloured by velocity (m/s) and solid stress σ_{xy} on top surface (Pa)



Thickness: 0.0125 m

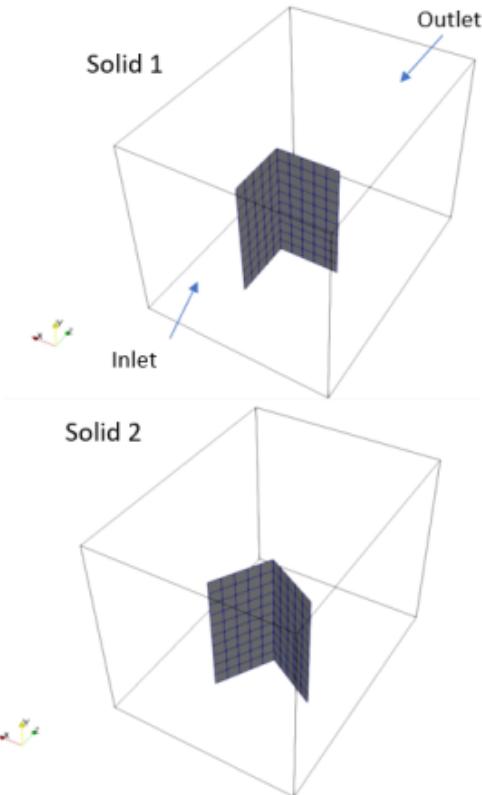


Thickness: 0.00625 m



Thickness: 0.003125 m

Test Cases 3: Setup



- **Objective:** Demonstrate that the solver can handle **shapes with bends** or shells in different planes. Demonstrate use of **local coordinate system**.

Material Properties:

- **Fluid Properties:**
 - Viscosity : 1.8×10^{-5} Pa.s
 - Density : 1.3 kg/m³
- **Solid Properties:**
 - Young's Modulus : 10³ Pa
 - Poisson's Ration: 0.4
 - Density : 5000.0 kg/m³

Boundary Conditions:

- **Fluid:**
 - left (inlet) : constant velocity inlet $V_0 = 0.1$ m/s
 - right boundary : outflow
 - bottom: no slip
 - front, back, top: no penetration
- **Solid:**
 - Bottom side clamped.

Time Step:

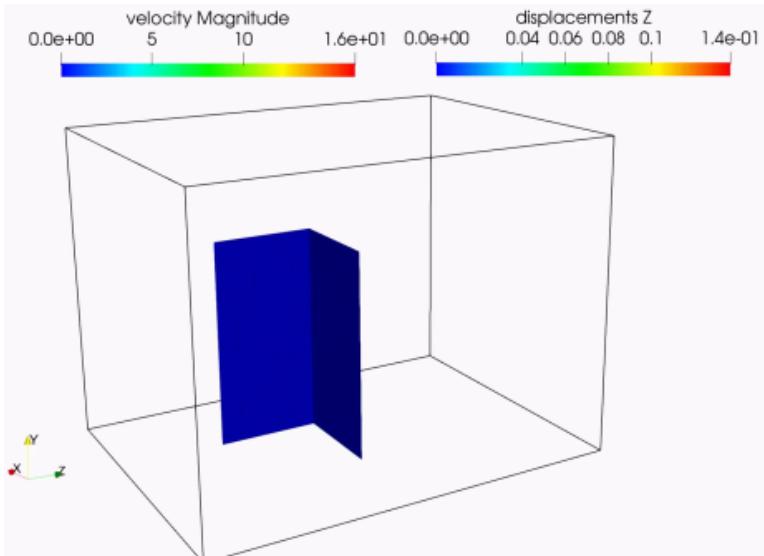
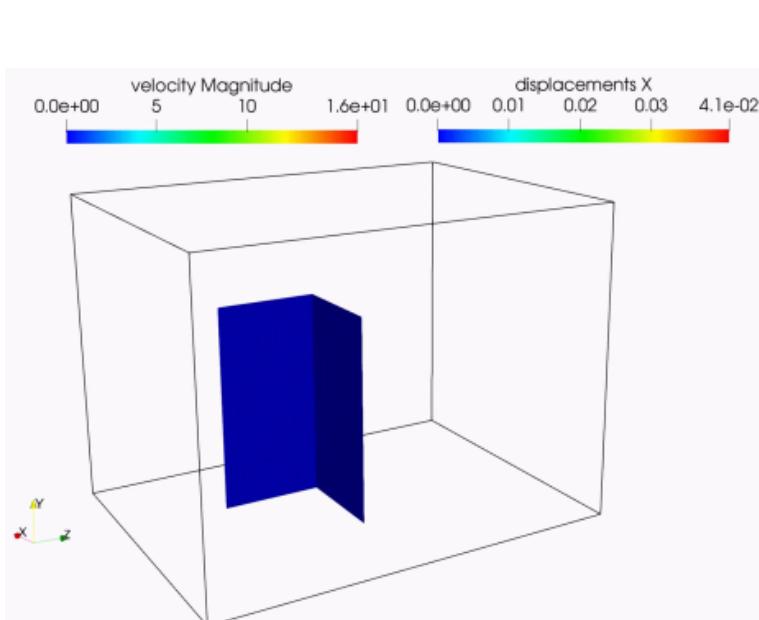
- Time Step: 2×10^{-4} s
- Final Time: 1 s

Problem Setup:

- Fluid: 1.5 m x 1.5 m x 2m
- Solid:
 - 0.5 m x 1 m rectangles intersect at right angle
 - Thickness: 0.0125 m

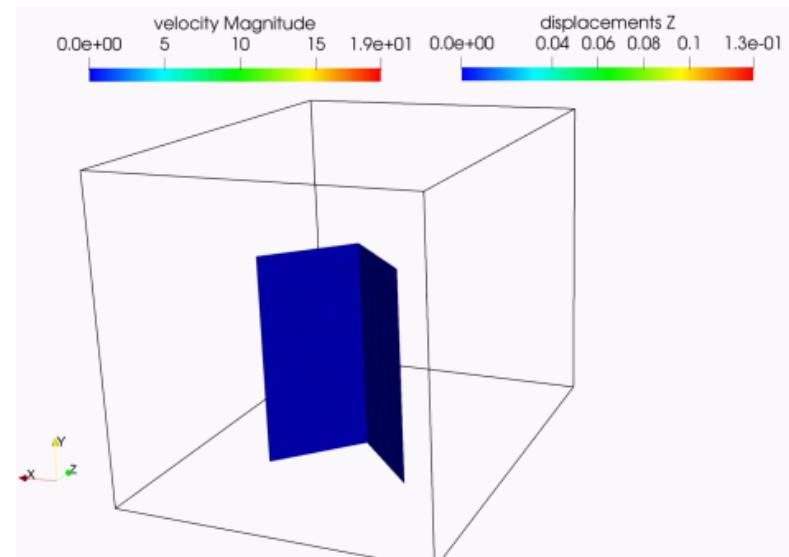
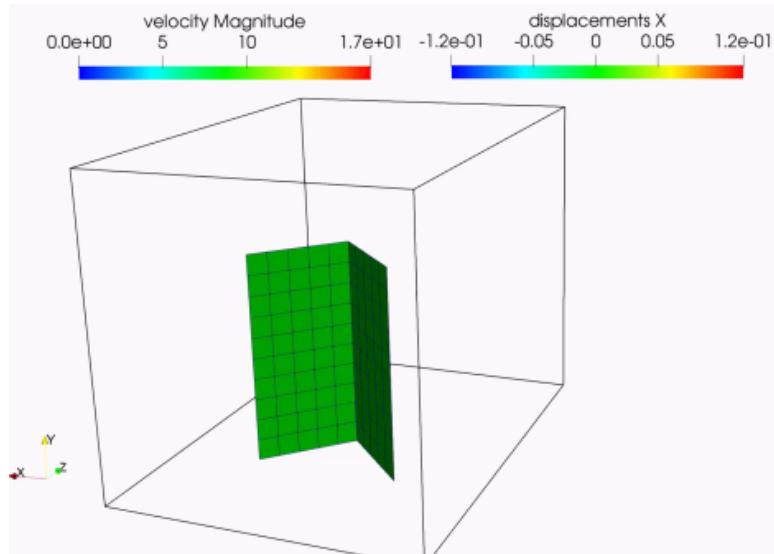


Test Cases 3 : Results



Test Cases 3 : Results

Solid 2 (45⁰)



Summary

- **Modularly** couple an external shell solver with OpenIFEM.
- **Extend** OpenIFEM capabilities for shell structures.
 - Represent thin shell with given finite thickness
 - Realistic solid loading which accounts for both forces and moments
 - Adoptable for different shell formulations
- OpenIFEM can handle **both general 3D bodies and different types of shells**.



Acknowledgment

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- OpenIFEM :
 - Feimi Yu for developing coupling wrapper for shell solver.



References

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- [4] Anvar Gilmanov, Trung Bao Le, and Fotis Sotiropoulos. A numerical approach for simulating fluid–structure interaction of flexible thin shells undergoing arbitrarily large deformations in complex domains. *Journal of computational physics*, 300:814–843, 2015.
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