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HIGH-INTENSITY DRYING PROCESS - IMPULSE DRYING

Annual Report

By
D. I. Orloff
P. M. Phelan

December 1993

Work Performed Under Contract DE-FG02-85CE40738

For
U.S. Department of Energy
Office of Industrial Technologies
Washington, D.C.

By
The Institute of Paper Science and Technology
Atlanta, GA

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TABLE OF CONTENTS

SUMMARY 1

OVERVIEW AND OBJECTIVES 2

EXPERIMENTAL PLANS AND PROCEDURES 4

RESULTS 8

CONCLUSIONS 63

RECOMMENDATIONS 64

REFERENCES 65

ACKNOWLEDGEMENTS 66

APPENDIX A 68

APPENDIX B 112

APPENDIX C 125

APPENDIX D 161

APPENDIX E 163

SUMMARY

Experiments have been conducted on a sheet-fed pilot-scale shoe press to compare impulse drying and double-felted pressing. Both an IPST ceramic coated and Beloit Type A press roll have been evaluated for linerboard sheet structures having a wide range of z-direction permeability. Both roll surfaces evaluated had thermal properties that are covered by IPST impulse drying patents.

The intent of the experiments was to find ways of correcting sheet sticking problems observed in previous pilot-scale shoe press experiments; to compare the performance of the IPST ceramic press roll surface coating to Beloit's Type A surface; to conduct the experiments over a wide range of linerboard sheet structures; and to evaluate the resulting linerboard in terms of key physical properties.

Previously observed sheet sticking problems had been partly traced to excessive press roll surface roughness. Hence, both roll surfaces used in the current experiments were diamond ground to achieve improved surface smoothness. Previous work had also raised the possibility that sheet sticking could also be contributed to by the deposit of calcium carbonate from the felt wash water to the heated press roll surface. To test this later hypothesis, the Beloit Type A press roll was evaluated using soft (deionized) and hard (calcium carbonate containing) felt wash water. It was observed that as long as the press roll surface temperature exceeded 150°C, sheets would not stick to the press roll surface. An attempt was made to evaluate the IPST ceramic coated press roll in a similar way, however roll surface failure prevented experiments from being conducted with hard felt wash water. When soft felt wash water was used, the IPST ceramic coated press roll only showed signs of sticking at press roll temperatures below 150°C. From these results, it was concluded that previously observed sheet sticking at temperatures above 150°C, were, in fact, caused by excessive press roll surface roughness.

In previous experiments, the IPST ceramic coating was applied as three separate plasma-sprayed layers. These consisted of a thin nickel-chromium bond coat, followed by a thick high porosity yttrium stabilized zirconium oxide coat and finally a thin low porosity yttrium stabilized zirconium oxide layer. In the previous experiments, inaccuracies in grinding tended to expose the porous middle layer of the ceramic coating resulting in excessive roughness. In addition, ceramic coating chipping was experienced in the previous work. Hence, it was decided to rebuild the IPST ceramic coated roll with two layers, a thin bond coat layer followed by a thick low porosity yttrium stabilized zirconium oxide layer. By doing so it was anticipated that a smoother and stronger surface would be achieved. By eliminating the high porosity middle layer, the new coating was expected to have higher density, heat capacity and thermal conductivity than the previously investigated IPST ceramic coating. As a result, slightly lower critical temperatures were anticipated. In the present experiments, the modified IPST ceramic coating performed well at temperatures above 150°C. However, when the roll surface temperature was dropped below 150°C, sheets would stick to the press roll surface. As in the previous experiments, a doctor blade was placed in contact with the press roll after the nip to prevent paper from being pulled into the clearance between the press roll and the induction coils. As in our previous experiments, when sheets stuck to the IPST ceramic surface, they experienced a shear force at the doctor blade. For the case of the present modified IPST ceramic coating, these shear forces were sometimes high enough to cause roll surface chipping. Hence, while the modified IPST ceramic surface was probably superior to the previous surface, future work will be needed to improve its mechanical properties, while, at the same time, retaining its thermal properties.

The present experiments showed that impulse drying was superior to double felted pressing in both press dryness and in important paper physical properties. The present work also confirmed laboratory-scale simulation that impulse drying critical temperature depends on; the specific

surface of the heated layer of the sheet, the thermal properties of the press roll surface and on the choice of felt. In addition, the impulse drying of recycled and two-ply liner was also demonstrated for both Southern Pine and Douglas fir containing furnishes.

OVERVIEW AND OBJECTIVES

Ongoing laboratory and pilot scale research at the Institute of Paper Science and Technology (IPST) has demonstrated that heavy weight grades of paper, such as linerboard, can be successfully impulse dried. That research has shown that deleterious sheet delamination can be avoided by a combination of processing strategies. These strategies include steps to make the pre-pressed sheets highly permeable to water flow and to reduce excessive pressure dependent heat transfer to the sheet that result in excessive internal flash evaporation at the exit of the impulse dryer.

Research at IPST suggests that high sheet Darcian permeability (low hydrodynamic specific surface) can be obtained by limiting refining to the minimum required for product aesthetics and by pre-pressing the sheet to as high a dryness as possible [1, 2]. In addition, IPST research suggest that excessive pressure dependent heat transfer can be eliminated by using press roll surfaces composed of materials having low thermal conductivity, low heat capacity, and low density [3-12].

Much of the previous IPST research was conducted with single-ply linerboard sheets composed of virgin southern pine that was minimally refined to eliminate shives. In contrast, commercial linerboard is usually two or three ply and composed of blends of virgin Kraft and recycled fiber. While current recycle content varies from mill to mill, there is increasing environmental pressure to increase recycle content. Mills in the U.S. typically use recycled fiber from old corrugated containers which are collected at warehouses and other high volume locations. In current practice, the amount of recycled fiber, included in linerboard, is limited by the fact that sheet strength properties decrease when recycle content is increased without further refining. Recycled fiber has the additional disadvantage in that it has a poor physical appearance. To improve the appearance of liner made with recycle fiber, U.S. manufacturers typically form a multi-ply sheet where the recycled fiber is contained in a bottom or inner layer, and outer layers are made from virgin Kraft sufficiently refined to impart a good appearance to the product.

Laboratory-scale impulse drying simulation experiments have been conducted with virgin southern pine, virgin Douglas fir, OCC and single and double-ply sheets made from combinations of these furnishes [2]. Both virgin furnishes have been successfully impulse dried in these laboratory experiments. OCC performed best, with regard to moisture removal and strength development, when blended with a virgin Kraft at concentrations of about 50% or less by weight. The performance of double-ply sheets was found to be controlled by the furnish characteristics of the heated-ply.

In 1992, Impulse Drying trials were conducted, with single-ply low specific surface linerboard, on Beloit's pilot shoe press [11]. The results indicated that an improvement of 8 percentage points in outgoing solids was possible compared to double felted pressing under the same operating conditions. However, there were only slight strength improvements compared to double felted pressing. In addition, sheet sticking was a major issue identified during that trial. Three potential reasons for the problem were identified: improper grinding of the ceramic roll surface, calcium deposits formed on the roll surface from hard felt wash water, and a lack of a draw force to strip handsheets from the roll.

Previous laboratory and pilot scale work [11,12] has demonstrated that pressure profile, felt design, and press load have an influence on impulse drying efficiency. The present experiments were, in part, designed to confirm these effects over a wide range of linerboard furnishes on the Beloit pilot shoe-press.

Laboratory-scale experiments had identified a methodology for structuring sheets so that they could be successfully impulse dried. The present experiments were also designed to confirm the scale-up of that methodology to conditions more representative of commercial conditions. Single and double-ply sheet structures were chosen that made use of southern pine, Douglas fir and OCC pulps. Those structures were also chosen to span a wide range of hydrodynamic specific surface.

Additional objectives of the present experiments were to compare impulse drying to double-felted and single-felted hot pressing and to unpressed controls, to compare and contrast the performance of the IPST modified ceramic and Beloit "A" press roll surfaces, and to confirm the influence of surface finish and water chemistry on sheet sticking.

EXPERIMENTAL PLANS AND PROCEDURES

Experimental Plans:

The pilot experiments were conducted in March of 1993 at Beloit Corporation's Rockton, Illinois research laboratory. The X2 pilot shoe press on machine number 3, as shown in Figure 1, was used.

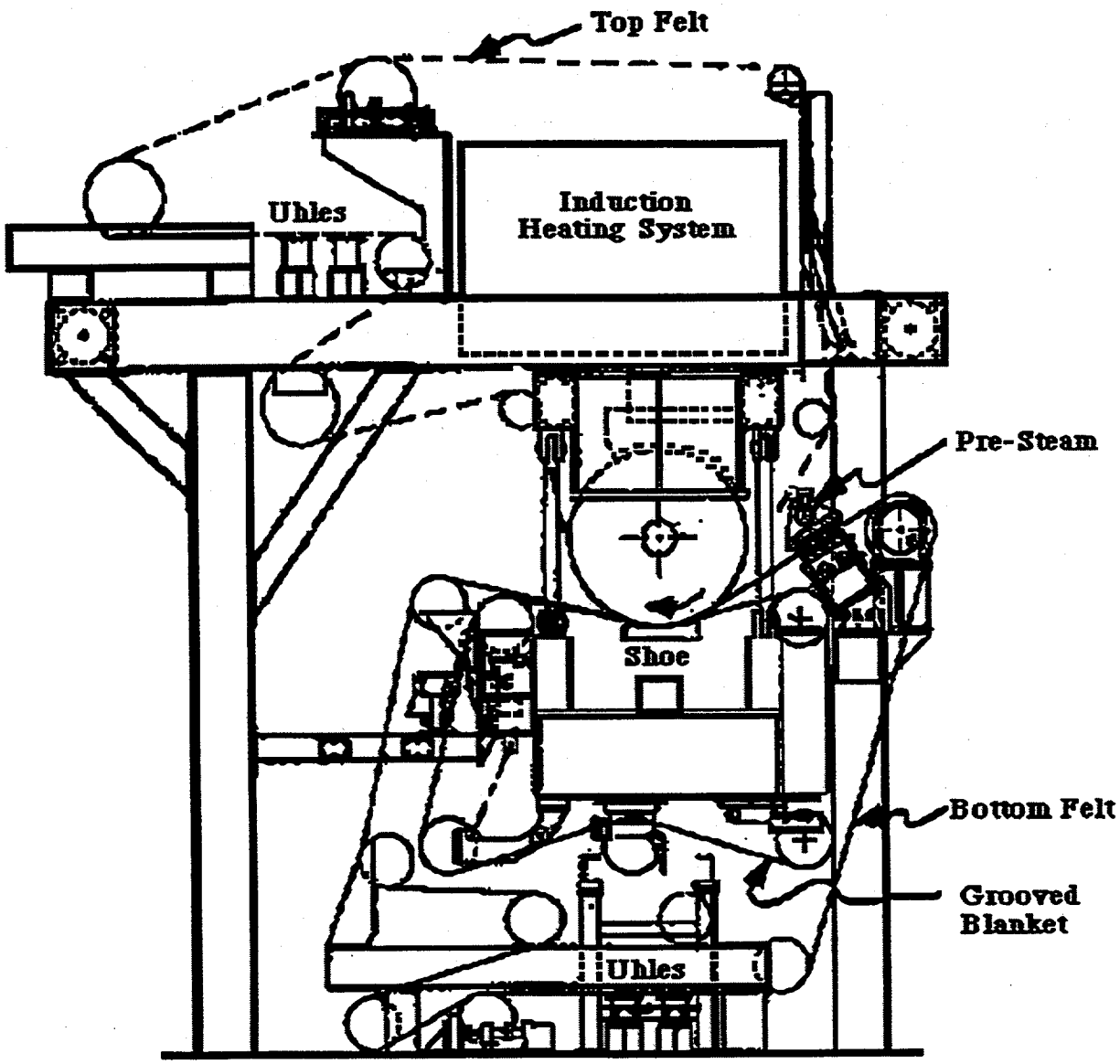

Figure 1. Pilot shoe press configured for impulse drying, double-felted or single-felted pressing

In order to meet the stated objectives the experimental conditions as shown in Table 2 were established. These conditions represent the minimum set of cases that were to be run for each of six furnishes spanning a wide range of hydrodynamic specific surface.

Table 1. Planned Experimental Conditions

Machine Configuration	X2 Shoe Press																							
Felt Type	Double Felted								Impulse Drying															
Pivot Position	B				S				B								S							
Roll Cover	0		+2		0		+2		0				+2				0				+2			
Load	Not Applicable								A		C		A		C		A		C		A		C	
	H	L	H	L	H	L	H	L	H	L	H	L	H	L	H	L	H	L	H	L	H	L	H	L
No. Of Temps.	Not Applicable								6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6
No. Of Repeats	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4

Notes:
Speed: 1200 fpm
Load: L = 6000 pli, H = 8500 pli.
Roll surface temperatures typically : 100°C, 150°C, 200°C, 250°C, 300°C, 350°C.
All sheets to have ingoing solids of 52%.
Deionized water to be used for the felt wash system.
All sheets to be steamed prior to impulse drying or double felted pressing using the same apparatus on the press.

The pulp used in these experiments was taken from the same batch used in conducting the laboratory-scale experiments (2). That earlier work demonstrated that the hydrodynamic specific surface of the heated layer of the sheet controls the maximum temperature of impulse drying. For this reason, sheets having a wide range of hydrodynamic specific surface were produced for the pilot-scale work. Table 2 shows the composition of the seven furnishes that were to be investigated. Cases with the prefix WF were produced on the Institute's low speed web former while furnish cases having a FD prefix were produced on the Institute's Formette Dynamique at conditions similar to those used in the earlier work (2).

Table 2. Planned Furnish Compositions

	Composition Of Top Ply			Composition Of Bottom Ply		
Furnish Case	Pulp Type	Freeness ml	Weight %	Pulp Type	Freeness ml	Weight %
WF1	HKSP	740	100			0
WF2	HKSP	600	100			0
WF3	HKDF	720	100			0
WF4	OCC	600	100			0
WF5	OCC	450	100			0
FD6	HKSP	740	20	HKSP OCC	740 600	40 40
FD7	HKDF	720	20	HKDF OCC	720 600	40 40

Experimental Procedures :

Each furnish was refined to the appropriate freeness level and formed into 205 g/m^2 sheets. The general procedure was to form the sheets on the IPST slow speed web former (cases: WF1,WF2, WF3, WF4, and WF5) or on the Formette Dynamique (cases: FD6 and FD7) and press the sheets on our Baldwin large platen press with blotters on both sides of the sheet. All the sheets were pressed to a target outgoing dryness of 52%. The pressing conditions used for each furnish are listed in Table 3. For example, the WF1 sheets were pressed in three batches. In the first batch the sheets had an ingoing dryness of between 32 and 37%. These sheets were placed in the Baldwin press with one blotter on top and one blotter on bottom and pressed at a pressure of 50 psi for 120 seconds. The blotters were then changed, the sheets inverted, and pressed a second time at a pressure of 50 psi for 150 seconds.

Table 3. Pressing Conditions

	Pressing Parameters						
		First Pressing			Second Pressing		
Furnish Case	Ingoing Dryness (%Solids)	Pressure (psi)	Time (seconds)	Number Of Blotters	Pressure (psi)	Time (seconds)	Number Of Blotters
WF1	32	35	120	1T;1B	35	150	1T;1B
	32	35	95	1T;1B	35	95	1T;1B
	42	35	230	1T;1B	-	-	-
WF2	35	35	160	1T;1B	35	160	1T;1B
	35	35	360	2T;2B	-	-	-
WF3	28	35	180	2T:2B	35	180	1T:1B
	32	35	180	2T:2B	30	120	1T:1B
WF4	38	35	60	1T:1B	n/a	n/a	n/a
	40	35	120	1T:1B			
WF5							
FD5	13	50	360	2T;2B	50	600	2T;2B
FD6	13	50	360	2T;2B	50	420	2T;2B
FD7	12	50	360	2T;2B	50	450	2T;2B

The results of permeability measurements indicated that the OCC sheets, produced on the web former, did not have the specific surface that was required (see Results section). Therefore, duplicate sheets for the OCC 450 ml CSF case were made on the Formette Dynamique (Case FD5). Table 4 lists the compositions of the sheets actually used in the present experiment.

Table 4. Actual Furnish Compositions

	Composition Of Top Ply			Composition Of Bottom Ply		
Furnish Case	Pulp Type	Freeness ml	Weight %	Pulp Type	Freeness ml	Weight %
WF1	HKSP	740	100			0
WF2	HKSP	600	100			0
WF3	HKDF	720	100			0
FD5	OCC	450	100			0
FD6	HKSP	740	20	HKSP	740	40
				OCC	600	40
FD7	HKDF	720	20	HKDF	720	40
				OCC	600	40

After pressing, sheets were cut to 8.5"x11" and the solids were adjusted to 52% by air drying or water misting as necessary. The sheets were then randomized to reduce any systematic errors resulting from the preparation procedures, and doubled bagged for shipment to Beloit.

In actual practice, events during the experiments precluded some conditions while opening up opportunities to examine additional variables. Table 5 lists the experimental conditions that were actually used and coded case numbers used in the remainder of this report.

Table 5. Actual Experimental Conditions

Case	Conditions						
	Pressing Type	Roll Cover	Felt	Pivot	Speed (ft/min)	Load (pli)	Wash Water
Con	Control	n/a	n/a	n/a	n/a	n/a	n/a
D1	D.F.	n/a	B	0	1200	6000	Deionized
D2	D.F.	n/a	B	0	1200	8500	Deionized
D3	D.F.	n/a	B	+2	1200	6000	Deionized
D4	D.F.	n/a	S	0	1200	6000	Deionized
D5	D.F.	n/a	S	0	1200	8500	Deionized
D6	D.F.	n/a	S	+2	1200	6000	Deionized
C1S	S.F.	IPST-C	B	0	1200	6000	Deionized
C2S	S.F.	IPST-C	B	0	1200	8500	Deionized
C3S	S.F.	IPST-C	B	+2	1200	6000	Deionized
A1S	S.F.	Beloit-A	B	0	1200	6000	Deionized
A4S	S.F.	Beloit-A	S	0	1200	6000	Deionized
A5S	S.F.	Beloit-A	S	0	1200	8500	Deionized
C1	I.D.	IPST-C	B	0	1200	6000	Deionized
C2	I.D.	IPST-C	B	0	1200	8500	Deionized
C3	I.D.	IPST-C	B	+2	1200	6000	Deionized
A1	I.D.	Beloit-A	B	0	1200	6000	Deionized
A2	I.D.	Beloit-A	B	0	1200	8500	Deionized
A4	I.D.	Beloit-A	S	0	1200	6000	Deionized
A5	I.D.	Beloit-A	S	0	1200	8500	Deionized
A6	I.D.	Beloit-A	S	+2	1200	6000	Deionized
A4F	I.D.	Beloit-A	S	0	1500	6000	Deionized
A5F	I.D.	Beloit-A	S	0	1500	8500	Deionized
A4H	I.D.	Beloit-A	S	0	1200	6000	Normal
A5H	I.D.	Beloit-A	S	0	1200	8500	Normal

RESULTS

Fiber Identification and Length Analysis:

For each furnish, samples from the prepared sheets were sent to John D. Hankey & Associates for fiber analysis. The results of the fiber identification are in Table 6. Table 7 summarizes the average fiber dimensions.

Table 6. Fiber Identification For Various Pulp Samples

Furnish	Pulp Type	USWK %	UHWK%	Softwood Species	Hardwood Species
WF1	S.Pine High Kappa	97-98	2-3	Southern yellow pine (Hard Cook) Trace of Semibleached Kraft	Mixed, incl. Gum, Yellow Poplar, and Oak
WF2	S.Pine High Kappa	97-98	2-3	Southern yellow pine (Hard Cook) Trace of Semibleached Kraft	Mixed, incl. Gum, Yellow Poplar, and Oak
WF3	D.Fir High Kappa	100(-)	Trace	Douglas Fir, Ponderosa and/or Lodgepole pine, Balsam Fir, Hemlock, Trace of Cedar and White Pine (Hard Cook)	Alder
FD5	OCC	n/a	n/a	Mixed Unbleached Kraft, and Semibleached Kraft	Mixed Kraft, Unbleached Semichemical Kraft, NSSC Pulps, and Mechanical Pulps
FD6	HKSP & OCC	90-95	5-10 & semi-chemical	Mixed Species incl. Hard Pine (Southern Yellow Pine, Ponderosa Pine, and/or Lodgepole Pine, etc.), Douglas Fir, Balsam Fir, Hemlock	Mixed, incl. Gum, Oak, Yellow Poplar, and Maple
FD7	HKDF & OCC	90-95	5-10 & semi-chemical	Mixed Species incl. Hard Pine (Southern Yellow Pine, Ponderosa Pine, and/or Lodgepole Pine, etc.), Douglas Fir, Balsam Fir, Hemlock	Mixed, incl. Gum, Oak, Yellow Poplar, and Maple

Table 7. Fiber Dimensions

Furnish Case	Pulp Type	Kappa No.	Top Ply Freeness (ml CSF)	Length (mm)			Width (μm)	Perimeter (μm)	Cell Wall Thickness (μm)	Coarseness (mg/100 m)
				Arith	LW	WW				
WF1	S.Pine	109.2	740	2.52	3.21	3.73	36.6	87.2	3.5	36.0
WF2	S.Pine	109.2	600	1.78	2.47	3.07	34.8	83.7	3.5	34.2
WF3	D.Fir	89.6	720	1.95	2.71	3.31	33.1	74.6	2.1	24.2
WF4	OCC	114.6	600	1.42	2.19	2.98	30.7	72.6	2.8	27.2
WF5	OCC	114.6	450	1.05	1.64	2.45	28.0	67.6	2.9	28.2
FD5	OCC	114.6	450	1.00	1.44	2.07	27.9	68.3	3.1	29.2
FD6	S.Pine &OCC	n/a	740	1.80	2.68	3.43	33.7	79.8	3.1	29.4
FD7	D.Fir &OCC	n/a	720	1.66	2.52	3.20	34.5	78.6	2.4	26.8

For case FD5 the dimensions given are an arithmetic average of four batches that were tested. Also note that there are three cases for OCC. The WF4 and WF5 cases are web former cases and were not used for the pilot trial because of a low hydrodynamic-specific surface. Fiber dimension data is included here for a comparison of the different formation techniques. Figure 2 shows the difference between the two fiber length distributions.

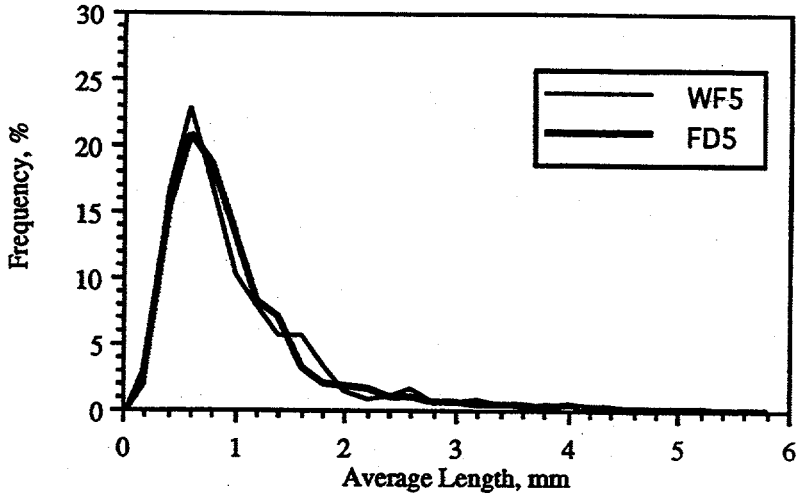

Figure 2. Comparison between fiber length distributions for webformer and formette sheets

Specific Surface:

The measured hydrodynamic specific surfaces for each furnish are in Table 8.

Table 8. Hydrodynamic Specific Surface

Furnish Case	Specific Surface (m^2/g)	Standard Deviation	Specific Volume (cm^3/g)	Standard Deviation
WF1	1.3	0.5	1.0	0.2
WF2	3.1	0.7	1.1	0.1
WF3	2.3	0.8	1.1	0.1
WF4	1.3	0.2	1.1	0.0
WF5	1.8	0.2	1.2	0.0
FD5	10.5	0.6	1.0	0.0
FD6	1.4	0.2	1.2	0.1
FD7	2.0	0.3	1.1	0.0

Plots of permeability verses porosity for each furnish are shown in Appendix DE.

Controls

Because of the limited time available on the Beloit pilot equipment, the authors wanted to perform as much preliminary work at IPST as possible.

The hydrodynamic specific surface is highly dependent on the pressing history of the sample. When the procedures for preparing the sheets for this experiment were developed, it was decided that all furnish cases should be pressed in the same manner. Formette sheets are very bulky and weak before pressing and can only be pressed on the Baldwin large platen press. Therefore, even the Webformer sheets were pressed on the Baldwin press.

Using a low pressure, long time history results in sheets with the correct solids content, but the sheet density may be lower than expected. This is most apparent in a minimally refined sheet particularly case WF1.

Sheet Sticking Issue:

There was no observed accumulation of mineral deposits on either roll with the use of deionized felt wash water. Sheet sticking to the roll was not observed for most Impulse Drying cases. For low temperature (<100°C) hot pressing cases, the sheets did stick to the rolls and had to be pulled off with the air wand. Removing stuck sheets from the ceramic roll may have provided a shear stress to the coating causing several chips to detach.

Also, for the low pressure, high speed case (A4F), the sheets stuck to the roll. To prevent damage to the roll, only one temperature was tested for that case.

Two samples of water were collected at the time of the experiment for elemental analysis. The first sample was of deionized water, while the second sample was of steam condensate taken during startup/shutdown from the presteaming system. After returning to Atlanta, it was noticed that a precipitate had settled in the steam condensate sample. Two tests were performed with this sample, one with the filtered solute. The second test was performed after redissolving the precipitate with acid. The results are summarized in Table 9.

Table 9. Elemental Water Analysis

Element	Deionized Shower Water (mg/L)	Filtered Steam Condensate (mg/L)	Redissolved Steam Condensate (mg/L)
Al	0.14	0.14	0.28
Ca	<0.01	1.09	n/a
Cr	<0.01	0.01	0.26
Cu	<0.01	0.29	1.12
Fe	<0.01	0.05	92.0
K	0.88	0.90	0.95
Mg	<0.01	1.11	1.10
Mn	<0.01	<0.01	0.60
Na	0.98	0.83	0.88
Ni	<0.01	<0.01	<0.01
S	6.74	8.25	n/a
Si	<3	<3	n/a
Sn	<0.01	<0.01	<0.01
Sr	0.001	0.004	0.002
Zn	<0.01	0.31	1.77
Zr	0.01	<0.01	<0.01

For comparison, the results from other water tests are shown in Table 10.

Table 10. Previous Water Tests

Element	IPST* Atlanta Aug, 1992 (mg/L)	Beloit Rockford May, 1991 (mg/L)	Beloit* Rockford Aug, 1992 (mg/L)	Beloit Rockford Nov, 1992 (mg/L)	Beloit Rockford Mar, 1993 (mg/L)	Beloit Rockford June, 1993 (mg/L)
Al	.04		.15	.07		
Ca	7.3	69.2	67.0	60.5		
Cr	<.01	.002	.02	<.004	.028	<.01
Cu	.02	<.005	<.01	<.004	<.02	<.01
Fe	.01	1.06	<.01	.44		
K	1.9		.75	.68		
Mg	1.2	34.0	33.0	28.3		
Mn	<.01	.35	.03	.22		
Na	3.3	3.9	3.0	2.7		
Ni		<.05		<.02		
S	2.9		8.8			
Si	3.1		6.7			
Sn	<.01		<.01			
Sr	.02		.06			
Zn	<.01	.025	<.01	.021		
Zr	.02		.01			

* From reference 11.

Critical Temperatures:

During transport and storage before the experiment moisture migrated within the sheets to some extent. Therefore, during the experiment, the sheets were selected from the bags to achieve a balanced moisture distribution. Table 11 lists the actual properties of all the sheets used during the experiments and the ranges of acceptable values for data analysis. Appendix A tabulates all of the acceptable data while the rejected data is tabulated in Appendix B.

Table 11. Ingoing Sheet Properties And Accepted Limits

	Target	Average	Std Dev	Accepted SD	Accepted Range
Basis Weight, g/m^2	205	204.53	9.81	~2 s	185-225
Ingoing Solids, %	52	51.51	2.35	~1.5 s	48-55

Critical temperatures for each impulse drying case were determined from the SEM, %CV of SEM, and the visual delamination observation data. All of this data is shown in Appendix C.

The following procedure was used to determine the critical temperatures from the data.

1) Determine the highest temperature at which the %CV of SEM does not exceed a minimum value determined for each furnish. The minimum value was determined from the control and double felted cases as shown in Table 12. Disregard high CV's at low temperatures (<100° C).

2) Determine the temperature at which the SEM values peak.

3) Determine the highest temperature at which there were no visible delaminations observed.

4) If two or more of the above determined temperatures agree, then that is the critical temperature.

5) If none of the above temperatures agree, then determine if the density and STFI data peaks at one of the possible temperatures. The critical temperature is the temperature that agrees with the majority of data.

6) If all else fails, the critical temperature is determined from the visual observations.

7) Round off the temperature to the nearest 5°C.

8) Identify any anomalies.

Table 12. Maximum Values for the Percent Coefficent of Variation of the Specific Elastic Modulus (%CV of the SEM) of the Control and Double Felted Data

Case	WF1	WF2	WF3	FD5	FD6	FD7
Con	15	10	15	10	10	10
D1	15	10	10	10	16	15
D2	15	10	16	10	25	10
D3	15	10	15	10	17	15
D4	15	10	10	10	15	10
D5	15	10	15	10	10	10
D6	16	10	10	10	15	10
Delam Value	15	10	15	10	15+	15

Previous experiments have shown that above the critical temperature, the SEM (and other strength properties) drops. Conversely, the %CV of the SEM rises just above the critical temperature. Therefore the above procedure will determine a lower limit for the critical temperature for most cases.

To determine the upper and lower uncertainties for the critical temperature, the following procedure was used.

1) The upper limit is the next higher temperature for which there is data.

2) If there is a large jump in the %CV of SEM value at the upper limit (~10 to 40+), then the lower limit is zero.

3) If the SEM data does not show a peak at the critical temperature, then the lower limit is the next lower temperature for which there is data.

4) The lower limit cannot be less than 100°C (otherwise, it would not be impulse drying).

5) Uncertainties are the difference between the critical temperatures and the limits rounded to the nearest 5°C.

Table 13 lists the determined critical temperatures and the uncertainties for each case.

Table 13. Critical Temperatures (In Degrees Celsius) for Impulse Drying on the X2 Shoe Press with Upper and Lower Uncertainties

Case	Description	WF1	WF2	WF3	FD5	FD6	FD7
C1	IPST-C/ Felt B/ 0 Pivot/ 6000 pli	245 +50 -0	195 +50 -0	195 +50 -0	155 +35 -0	240 +50 -0	240 +50 -0
C2	IPST-C/ Felt B/ 0 Pivot/ 8500 pli	245 +50 -50	245 +50 -0	195 +50 -0	150 +45 -50	245 +50 -0	150 +45 -0
C3	IPST-C/ Felt B/ +2 Pivot/ 6000 pli	150 +50 -50	150 +50 -0	150 +50 -0	145 +55 -45	245 +50 -0	245 +50 -45
A1	Beloit-A/ Felt B/ 0 Pivot/ 6000 pli	200 +55 -0	175 +25 -0	175 +25 -35	145 +55 -0	200 +55 -0	145 +55 -0
A2	Beloit-A/ Felt B/ 0 Pivot/ 8500 pli	200 +55 -0	175 +25 -0	175 +25 -35	120 +25 -0	200 +55 -0	145 +55 -0
A4	Beloit-A/ Felt S/ 0 Pivot/ 6000 pli	155 +55 -0	155 +55 -0	155 +55 -0	130 +25 -0	130 +25 -0	155 +55 -0
A5	Beloit-A/ Felt S/ 0 Pivot/ 8500 pli	155 +55 -0	155 +55 -0	155 +55 -0	100 +30 -0	155 +55 -0	130 +25 -0
A6	Beloit-A/ Felt S/ +2 Pivot/ 6000 pli	150 +25 -0	150 +25 -0	150 +25 -0	120 +30 -0	150 +25 -0	150 +25 -0
A4F	Beloit-A/ Felt S/ 0 Pivot/ 6000 pli/ 30 ms	<150	<150	<150	<150	<150	<150
A5F	Beloit-A/ Felt S/ 0 Pivot/ 8500 pli/ 30 ms	175 +25 -0	150 +25 -0	150 +25 -0	100 +50 -0	175 +25 -25	150 +25 -50
A4H	Beloit-A/ Felt S/ 0 Pivot/ 6000 pli/ hard water	175 +• -0	175 +• -0	150 +25 -0	100 +50 -0	175 +25 -0	150 +25 -0
A5H	Beloit-A/ Felt S/ 0 Pivot/ 8500 pli/ hard water	150 +25 -0	150 +25 -0	150 +25 -0	100 +50 -0	175 +25 -25	150 +25 -0

For case A4F, sheet sticking precluded testing any temperature other than 150° C. All of those sheets were delaminated and no further testing was performed.

Water Removal and Physical Properties:

For the control, single felted pressing, and double felted pressing cases, the water removal and physical property data was averaged and a 95% confidence interval was calculated using the standard equation below. The results are shown in Tables 14 through 47.

$$C.I. = \pm t_{a/2,n-1} \frac{s}{\sqrt{n}}$$

where,
confidence = (1-a)100%
n = number of data points
s = standard deviation of the data
t = student t-distribution.

Previous experiments have shown that, for impulse drying, water removal and physical property development can be approximated by a linear function of temperature below the critical temperature. To determine a value for each property at the critical temperature for the impulse dried cases, a linear regression was performed on the best data. The data was filtered to remove data that showed a drop in properties above the critical temperature. Also, any data below 100° C that shows evidence that the sheets may have stuck to the roll were eliminated. All data between 100° and the critical temperature were retained. Figure 3 shows a typical case before and after the questionable data were removed.

After removing the questionable data, a linear regression was performed and the 95% confidence limits on the true mean were calculated. The following equation was used to calculate the confidence limits on the regression mean.

$$C.L. = \pm t_{\alpha/2,n-2}\ s \sqrt{\frac{1}{n} + \frac{(x - \bar{x})^2}{S_{xx}}}$$

where,

confidence = $(1-\alpha)100\%$
n = number of data points
t = student t-distribution
s = standard distribution of data
$\bar{x}$ = temperature mean

$$S_{xx} = \sum_{i=1}^{n} x_i^{\,2} - \frac{\left(\sum_{i=1}^{n} x_i\right)^2}{n}$$

For the impulse dried cases, physical properties at the critical temperature were determined from the regression. These values are in Tables 14 through 37. The upper and lower uncertainties were determined from the region bounded by the confidence limits on the regression mean and the upper and lower limits of the critical temperature.

Figure 3 shows a typical case before the questionable data were removed and the remaining data with the regression line and calculated confidence limits. The shaded region indicates the region bound by the confidence limits for the critical temperature and the regression mean.

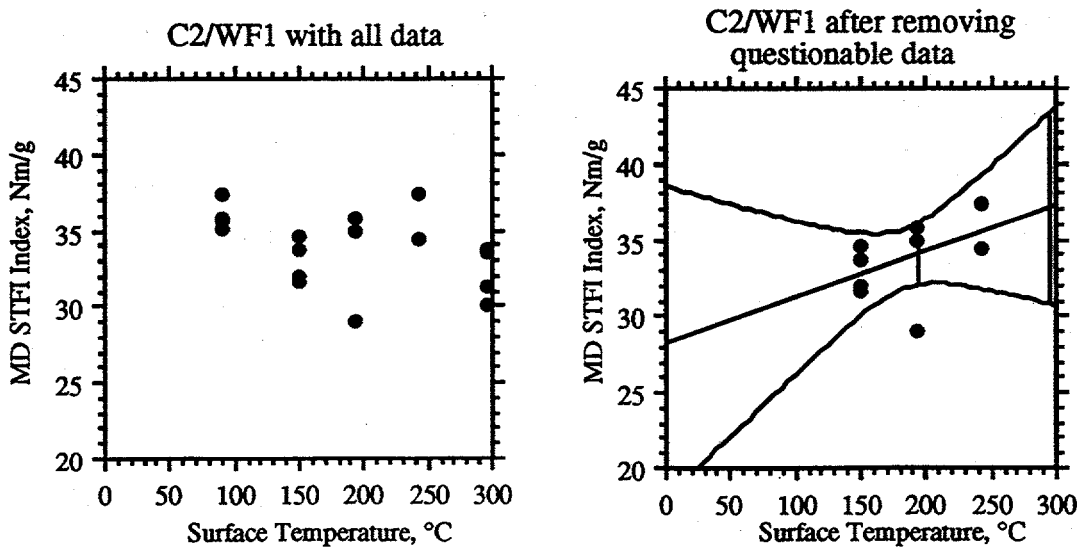

Figure 3. Case C2/WF1 MD STFI data before and after removing the questionable data and calculating the linear regression and confidence limits on the mean value. The critical temperature was 245°C ± 50°.

Table 14. Outgoing Solids for Furnish WF1 with Upper and Lower 95% Confidence Intervals*

Case	Test 0			Test 1			Test 2			Test 3		
	Sout %	C.I. +	C.I. -	Sout Mean	s	n	Sout Mean	s	n	Sout Mean	s	n
Con/WF1												
D1/WF1	60.1	1.2	1.2	60.1	0.727	4	60.1	0.727	4	60.1	0.727	4
D2/WF1	62.2	2.3	2.3	62.2	0.181	2	62.2	0.181	2	62.2	0.181	2
D3/WF1	59.5	0.9	0.9	59.5	0.358	3	59.5	0.358	3	59.5	0.358	3
D4/WF1	59.6	3.3	3.3	59.6	2.091	4	59.6	2.091	4	59.6	2.091	4
D5/WF1	61.7	1.4	1.4	61.7	0.878	4	61.7	0.878	4	61.7	0.878	4
D6/WF1	57.9	3.2	3.2	57.9	2.008	4	57.9	2.008	4	57.9	2.008	4
C1S/WF1	59.6	9.0	9.0	59.6	3.615	3	59.6	3.615	3	59.6	3.615	3
C2S/WF1	63.8	1.0	1.0	63.8	0.616	4	63.8	0.616	4	63.8	0.616	4
C3S/WF1	61.3	45.8	45.8	61.3	3.602	2	61.3	3.602	2	61.3	3.602	2
A1S/WF1	61.1	1.3	1.3	61.1	0.102	2	61.1	0.102	2	61.1	0.102	2
A4S/WF1	59.5	2.9	2.9	59.5	1.818	4	59.5	1.818	4	59.5	1.818	4
A5S/WF1												
C1/WF1	63.8	4.0	1.6	63.8	4.780	8	65.0	3.355	8	63.8	1.014	4
C2/WF1	64.6	5.5	4.3	64.6	7.115	9	65.2	6.371	9	64.6	0.253	2
C3/WF1	62.4	3.5	5.1	62.4	6.104	8	61.6	5.135	8	62.4	1.434	4
A1/WF1	67.9	5.5	2.0	67.9	6.556	8	69.7	4.444	8	67.9	1.226	4
A2/WF1	68.0	3.7	1.1	68.0	4.417	8	69.2	2.886	8	68.0	0.712	4
A4/WF1	64.9	5.1	1.6	64.9	7.150	10	66.7	4.719	10	64.9	1.029	4
A5/WF1	66.4	3.7	1.1	66.4	5.484	11	67.7	3.539	11	66.4	0.674	4
A6/WF1	66.9	5.4	1.7	66.9	3.414	4	68.7	2.249	4	66.9	1.085	4
A4F/WF1												
A5F/WF1	64.9	3.1	1.0	64.9	3.680	8	65.9	2.427	8	64.9	0.618	4
A4H/WF1	67.4	∞	∞	67.4	40.26	3	67.4	40.26	3	67.4	1.471	3
A5H/WF1	67.1	3.0	1.5	67.1	2.824	6	67.8	2.112	6	67.1	0.924	4

*Data for the impulse drying cases are at the critical temperatures while all other data are the mean values. Data used for hypothesis testing are also shown.

Table 15. Outgoing Solids for Furnish WF2 with Upper and Lower 95% Confidence Intervals*

Case	Test 0			Test 1			Test 2			Test 3		
	Sout %	C.I. +	C.I. -	Sout Mean	s	n	Sout Mean	s	n	Sout Mean	s	n
Con/WF2												
D1/WF2	58.7	1.5	1.5	58.7	0.621	3	58.7	0.621	3	58.7	0.621	3
D2/WF2	59.0	3.9	3.9	59.0	1.579	3	59.0	1.579	3	59.0	1.579	3
D3/WF2	57.9	3.7	3.7	57.9	2.291	4	57.9	2.291	4	57.9	2.291	4
D4/WF2	57.1	2.5	2.5	57.1	1.551	4	57.1	1.551	4	57.1	1.551	4
D5/WF2	58.5	1.7	1.7	58.5	1.088	4	58.5	1.088	4	58.5	1.088	4
D6/WF2	57.0	2.2	2.2	57.0	1.370	4	57.0	1.370	4	57.0	1.370	4
C1S/WF2	56.8	4.7	4.7	56.8	2.981	4	56.8	2.981	4	56.8	2.981	4
C2S/WF2	60.6	1.9	1.9	60.6	1.205	4	60.6	1.205	4	60.6	1.205	4
C3S/WF2	58.9	2.2	2.2	58.9	1.353	4	58.9	1.353	4	58.9	1.353	4
A1S/WF2												
A4S/WF2	55.4	1.3	1.3	55.4	0.832	4	55.4	0.832	4	55.4	0.832	4
A5S/WF2	56.7	2.0	2.0	56.7	1.262	4	56.7	1.262	4	56.7	1.262	4
C1/WF2	59.6	5.0	1.7	59.6	5.990	8	61.2	4.012	8	59.6	1.069	4
C2/WF2	61.4	2.0	1.1	61.4	2.207	7	61.9	1.706	7	61.4	0.449	3
C3/WF2	60.2	2.0	1.0	60.2	2.359	8	60.7	1.751	8	60.2	0.601	4
A1/WF2	61.8	2.5	2.1	61.8	3.024	8	62.0	2.797	8	61.8	1.350	4
A2/WF2	62.8	1.9	1.2	62.8	2.291	8	63.1	1.857	8	62.8	0.748	4
A4/WF2	60.3	5.2	1.8	60.3	6.166	8	62.0	4.173	8	60.3	1.146	4
A5/WF2	61.2	4.7	1.6	61.2	5.116	7	62.8	3.409	7	61.2	0.989	4
A6/WF2	61.7	2.0	1.4	61.7	2.353	8	61.9	2.017	8	61.7	0.883	4
A4F/WF2												
A5F/WF2	60.7	1.9	1.3	60.7	2.297	8	61.1	1.925	8	60.7	0.816	4
A4H/WF2	63.5	∞	∞	63.5	62.8	4	63.5	62.8	4	63.5	1.598	4
A5H/WF2	63.8	8.8	8.8							63.8	0.696	2

*Data for the impulse drying cases are at the critical temperatures while all other data are the mean values. The data used for hypothesis testing are also shown.

Table 16. Outgoing Solids for Furnish WF3 with Upper and Lower 95% Confidence Intervals*

Case	Test 0			Test 1			Test 2			Test 3		
	Sout %	C.I. +	C.I. -	Sout Mean	s	n	Sout Mean	s	n	Sout Mean	s	n
Con/WF3												
D1/WF3	59.9	0.8	0.8	59.9	0.317	3	59.9	0.317	3	59.9	0.317	3
D2/WF3	61.7	0.8	0.8	61.7	0.320	3	61.7	0.320	3	61.7	0.320	3
D3/WF3	60.4	9.0	9.0	60.4	0.708	2	60.4	0.708	2	60.4	0.708	2
D4/WF3	59.8	2.8	2.8	59.8	1.125	3	59.8	1.125	3	59.8	1.125	3
D5/WF3	61.3	1.6	1.6	61.3	0.658	3	61.3	0.658	3	61.3	0.658	3
D6/WF3	57.4	2.1	2.1	57.4	0.841	3	57.4	0.841	3	57.4	0.841	3
C1S/WF3	60.6	3.7	3.7	60.6	2.930	2	60.6	2.930	2	60.6	2.930	2
C2S/WF3	62.4	1.9	1.9	62.4	0.761	3	62.4	0.761	3	62.4	0.761	3
C3S/WF3	61.9	0.3	0.3	61.9	0.024	2	61.9	0.024	2	61.9	0.024	2
A1S/WF3												
A4S/WF3	58.2	0.8	0.8	58.2	0.515	4	58.2	0.515	4	58.2	0.515	4
A5S/WF3	59.5	∞	∞									
C1/WF3	62.4	2.1	1.0	62.4	2.045	6	63.0	1.503	6	62.4	0.406	3
C2/WF3	63.3	2.9	0.9	63.3	3.496	8	64.3	2.301	8	63.3	0.581	4
C3/WF3	62.9	4.1	2.0	62.9	4.427	7	63.9	3.272	7	62.9	0.788	3
A1/WF3	64.7	1.5	1.9	64.7	2.498	9	64.5	2.193	9	64.7	0.537	4
A2/WF3	65.4	2.5	3.5	65.4	4.215	8	64.9	3.584	8	65.4	0.188	2
A4/WF3	63.5	6.5	2.3	63.5	5.229	5	65.6	3.556	5	63.5	0.941	3
A5/WF3	64.5	4.7	1.5	64.5	4.495	6	66.1	2.983	6	64.5	0.622	3
A6/WF3	63.9	4.3	2.0	63.9	1.745	3	65.0	1.276	3	63.9	0.633	3
A4F/WF3												
A5F/WF3	63.6	0.0	0.0							63.6	0.000	2
A4H/WF3	63.1	3.0	1.5	63.1	3.606	8	63.9	2.682	8	63.1	0.925	4
A5H/WF3	65.1	1.0	0.5	65.1	1.183	8	65.3	0.907	8	65.1	0.332	4

*Data for the impulse drying cases are at the critical temperatures while all other data are the mean values. The data used for hypothesis testing are also shown.

Table 17. Outgoing Solids for Furnish FD5 with Upper and Lower 95% Confidence Intervals*

Case	Test 0			Test 1			Test 2			Test 3		
	Sout %	C.I. +	C.I. -	Sout Mean	s	n	Sout Mean	s	n	Sout Mean	s	n
Con/FD5												
D1/FD5	57.6	2.0	2.0	57.6	1.247	4	57.6	1.247	4	57.6	1.247	4
D2/FD5	57.9	2.6	2.6	57.9	1.646	4	57.9	1.646	4	57.9	1.646	4
D3/FD5	57.5	1.7	1.7	57.5	1.037	4	57.5	1.037	4	57.5	1.037	4
D4/FD5	59.4	0.4	0.4	59.4	0.028	2	59.4	0.028	2	59.4	0.028	2
D5/FD5	59.0	1.8	1.8	59.0	1.153	4	59.0	1.153	4	59.0	1.153	4
D6/FD5	59.0	1.6	1.6	59.0	1.029	4	59.0	1.029	4	59.0	1.029	4
C1S/FD5	58.4	1.4	1.4	58.4	0.901	4	58.4	0.901	4	58.4	0.901	4
C2S/FD5	58.4	2.0	2.0	58.4	1.237	4	58.4	1.237	4	58.4	1.237	4
C3S/FD5	56.8	2.9	2.9	56.8	1.821	4	56.8	1.821	4	56.8	1.821	4
A1S/FD5												
A4S/FD5	59.1	3.9	3.9	59.1	0.310	2	59.1	0.310	2	59.1	0.310	2
A5S/FD5	58.5	1.4	1.4	58.5	0.855	4	58.5	0.855	4	58.5	0.855	4
C1/FD5	59.8	2.6	1.4	59.8	2.124	5	60.5	1.619	5			
C2/FD5	60.7	6.0	3.7	60.7	2.397	3	61.9	1.934	3	60.7	0.902	3
C3/FD5	59.2	5.1	4.6	59.2	4.068	5	59.4	3.895	5	59.2	1.314	4
A1/FD5	60.2	12.0	6.0	60.2	4.823	3	63.2	3.626	3	60.2	0.554	2
A2/FD5	60.8	4.8	2.3	60.8	4.573	6	62.1	3.381	6	60.8	1.444	4
A4/FD5	60.6	1.6	0.9	60.6	1.971	8	61.0	1.531	8	60.6	0.573	4
A5/FD5	59.6	1.6	0.9	59.6	1.026	4	59.9	0.803	4			
A6/FD5	61.1	3.6	3.1	61.1	2.258	4	61.4	2.095	4	61.1	0.342	2
A4F/FD5												
A5F/FD5	60.2	4.2	4.2	60.2	2.666	4	60.2	2.666	4			
A4H/FD5												
A5H/FD5												

*Data for the impulse drying cases are at the critical temperatures while all other data are the mean values. The data used for hypothesis testing are also shown.

Table 18. Outgoing Solids for Furnish FD6 with Upper and Lower 95% Confidence Intervals*

Case	Test 0			Test 1			Test 2			Test 3		
	Sout %	C.I. +	C.I. -	Sout Mean	s	n	Sout Mean	s	n	Sout Mean	s	n
Con/FD6												
D1/FD6	60.6	1.4	1.4	60.6	0.552	3	60.6	0.552	3	60.6	0.552	3
D2/FD6	62.3	0.9	0.9	62.3	0.550	4	62.3	0.550	4	62.3	0.550	4
D3/FD6	60.4	0.8	0.8	60.4	0.510	4	60.4	0.510	4	60.4	0.510	4
D4/FD6	61.2	2.2	2.2	61.2	1.359	4	61.2	1.359	4	61.2	1.359	4
D5/FD6	61.5	0.9	0.9	61.5	0.569	4	61.5	0.569	4	61.5	0.569	4
D6/FD6	58.4	4.5	4.5	58.4	2.819	4	58.4	2.819	4	58.4	2.819	4
C1S/FD6	60.6	5.6	5.6	60.6	2.261	3	60.6	2.261	3	60.6	2.261	3
C2S/FD6	63.7	2.4	2.4	63.7	1.850	2	63.7	1.850	2	63.7	1.850	2
C3S/FD6	61.8	1.4	1.4	61.8	0.882	4	61.8	0.882	4	61.8	0.882	4
A1S/FD6												
A4S/FD6	59.0	0.6	0.6	59.0	0.391	4	59.0	0.391	4	59.0	0.391	4
A5S/FD6	59.6	1.5	1.5	59.6	0.908	4	59.6	0.908	4	59.6	0.908	4
C1/FD6	65.1	3.7	1.5	65.1	4.409	8	66.2	3.075	8	65.1	0.915	4
C2/FD6	66.1	4.6	1.7	66.1	2.892	4	67.5	1.992	4	66.1	1.092	4
C3/FD6	66.4	2.8	1.1	66.4	3.306	8	67.2	2.303	8	66.4	0.684	4
A1/FD6	67.5	2.9	1.2	67.5	3.516	8	68.4	2.457	8	67.5	0.734	4
A2/FD6	68.3	3.1	1.2	68.3	3.699	8	69.2	2.560	8	68.3	0.747	4
A4/FD6	62.9	2.8	1.6	62.9	3.395	8	63.5	2.637	8	62.9	0.988	4
A5/FD6	66.5	8.3	2.8	66.5	5.227	4	69.2	3.489	4	66.5	1.751	4
A6/FD6	65.8	2.7	1.2	65.8	2.533	6	66.5	1.839	6	65.8	0.755	4
A4F/FD6												
A5F/FD6	66.3	1.5	1.4	66.3	2.160	11	66.3	2.151	11	66.3	0.328	3
A4H/FD6	66.3	3.9	1.2	66.3	4.200	7	67.6	2.758	7	66.3	0.765	4
A5H/FD6	67.9	1.9	2.0	67.9	3.036	11	67.8	2.912	11	67.9	0.616	4

*Data for the impulse drying cases are at the critical temperatures while all other data are the mean values. The data used for hypothesis testing are also shown.

Table 19. Outgoing Solids for Furnish FD7 with Upper and Lower 95% Confidence Intervals*

Case	Test 0			Test 1			Test 2			Test 3		
	Sout %	C.I. +	C.I. -	Sout Mean	s	n	Sout Mean	s	n	Sout Mean	s	n
Con/FD7												
D1/FD7	58.8	∞	∞									
D2/FD7	60.2	0.5	0.5	60.2	0.326	4	60.2	0.326	4	60.2	0.326	4
D3/FD7	60.0	1.9	1.9	60.0	1.173	4	60.0	1.173	4	60.0	1.173	4
D4/FD7	58.1	0.7	0.7	58.1	0.442	4	58.1	0.442	4	58.1	0.442	4
D5/FD7	59.6	0.3	0.3	59.6	0.172	4	59.6	0.172	4	59.6	0.172	4
D6/FD7	58.0	∞	∞									
C1S/FD7	60.5	1.4	1.4	60.5	0.903	4	60.5	0.903	4	60.5	0.903	4
C2S/FD7	62.6	0.8	0.8	62.6	0.309	3	62.6	0.309	3	62.6	0.309	3
C3S/FD7	59.1	1.6	1.6	59.1	0.641	3	59.1	0.641	3	59.1	0.641	3
A1S/FD7												
A4S/FD7	58.2	3.5	3.5	58.2	1.393	3	58.2	1.393	3	58.2	1.393	3
A5S/FD7	58.0	0.4	0.4	58.0	0.310	5	58.0	0.310	5	58.0	0.310	5
C1/FD7	62.8	2.4	1.0	62.8	2.847	8	63.5	2.000	8	62.8	0.606	4
C2/FD7	61.0	2.2	1.5	61.0	2.356	7	61.3	1.990	7	61.0	0.604	3
C3/FD7	64.1	2.9	2.4	64.1	4.556	12	64.4	4.140	12	64.1	0.716	4
A1/FD7	63.7	2.7	2.2	63.7	2.213	5	64.0	1.998	5	63.7	0.247	2
A2/FD7	65.9	1.9	1.3	65.9	2.230	8	66.2	1.910	8	65.9	0.836	4
A4/FD7	62.2	4.9	1.7	62.2	5.317	7	63.8	3.562	7	62.2	1.050	4
A5/FD7	62.7	3.8	2.2	62.7	3.062	5	63.5	2.419	5	62.7	1.385	4
A6/FD7	63.4	3.2	1.2	63.4	3.448	7	64.4	2.360	7	63.4	0.740	4
A4F/FD7												
A5F/FD7	62.6	2.9	7.7	62.6	9.154	8	60.2	6.308	8	62.6	0.810	4
A4H/FD7	62.6	3.3	1.8	62.6	3.984	8	63.3	3.062	8	62.6	1.124	4
A5H/FD7	65.1	2.4	2.4						4	65.1	1.535	4

*Data for the impulse drying cases are at the critical temperatures while all other data are the mean values. The data used for hypothesis testing are also shown.

Table 20. CD STFI Index for Furnish WF1 with Upper and Lower 95% Confidence Intervals*

Case	Test 0			Test 1			Test 2			Test 3		
	CD STFI	C.I. +	C.I. -	CD STFI Mean	s	n	CD STFI Mean	s	n	CD STFI Mean	s	n
Con/WF1	11.5	1.1	1.1	11.5	0.086	2	11.5	0.086	2	11.5	0.086	2
D1/WF1	19.3	2.3	2.3	19.3	1.436	4	19.3	1.436	4	19.3	1.436	4
D2/WF1	21.4	27.6	27.6	21.4	2.167	2	21.4	2.167	2	21.4	2.167	2
D3/WF1	20.3	2.8	2.8	20.3	1.121	3	20.3	1.121	3	20.3	1.121	3
D4/WF1	22.6	2.2	2.2	22.6	1.366	4	22.6	1.366	4	22.6	1.366	4
D5/WF1	24.9	1.0	1.0	24.9	0.647	4	24.9	0.647	4	24.9	0.647	4
D6/WF1	23.5	1.6	1.6	23.5	0.985	4	23.5	0.985	4	23.5	0.985	4
C1S/WF1	21.3	9.5	9.5	21.3	3.818	3	21.3	3.818	3	21.3	3.818	3
C2S/WF1	24.4	1.0	1.0	24.4	0.647	4	24.4	0.647	4	24.4	0.647	4
C3S/WF1	22.2	8.7	8.7	22.2	0.685	2	22.2	0.685	2	22.2	0.685	2
A1S/WF1	19.5	27.5	27.5	19.5	2.167	2	19.5	2.167	2	19.5	2.167	2
A4S/WF1	19.8	3.0	3.0	19.8	1.897	4	19.8	1.897	4	19.8	1.897	4
A5S/WF1												
C1/WF1	20.5	2.7	3.1	20.5	1.96	4	20.3	1.82	4	20.5	1.21	4
C2/WF1	23.4	7.4	6.2	23.4	5.93	5	24.0	5.46	5	23.4	0.45	2
C3/WF1	21.3	3.9	5.3	21.3	3.33	4	20.6	2.87	4	21.3	1.32	4
A1/WF1	24.7	5.8	2.3	24.7	3.64	4	26.4	2.55	4	24.7	1.45	4
A2/WF1	23.4	2.4	2.6	23.4	1.61	4	23.3	1.56	4	23.4	0.71	4
A4/WF1	23.3	4.9	1.8	23.3	3.05	4	24.9	2.08	4	23.3	1.11	4
A5/WF1	25.7	7.3	2.0	25.7	4.57	4	28.3	2.92	4	25.7	0.79	4
A6/WF1	24.0	2.6	2.5	24.0	1.67	4	24.1	1.61	4	24.0	0.78	4
A4F/WF1												
A5F/WF1	23.0	2.8	1.4	23.0	1.76	4	23.7	1.32	4	23.0	0.61	4
A4H/WF1	23.0	∞	∞	23.0	40.26	3	23.0	40.26	3	23.0	0.98	3
A5H/WF1	24.6	3.3	1.7	24.6	3.12	6	25.4	2.38	6	24.6	1.09	4

*Data for the impulse drying cases are at the critical temperatures while all other data are the mean values. The data used for hypothesis testing are also shown.

Table 21. CD STFI Index for Furnish WF2 with Upper and Lower 95% Confidence Intervals*

Case	Test 0			Test 1			Test 2			Test 3		
	CD STFI	C.I. +	C.I. -	CD STFI Mean	s	n	CD STFI Mean	s	n	CD STFI Mean	s	n
Con/WF2	17.9	1.0	1.0	17.9	0.649	4	17.9	0.649	4	17.9	0.649	4
D1/WF2	23.8	5.1	5.1	23.8	2.068	3	23.8	2.068	3	23.8	2.068	3
D2/WF2	25.6	1.2	1.2	25.6	0.486	3	25.6	0.486	3	25.6	0.486	3
D3/WF2	24.7	1.5	1.5	24.7	0.952	4	24.7	0.952	4	24.7	0.952	4
D4/WF2	24.0	1.8	1.8	24.0	1.157	4	24.0	1.157	4	24.0	1.157	4
D5/WF2	25.6	1.7	1.7	25.6	1.036	4	25.6	1.036	4	25.6	1.036	4
D6/WF2	25.6	1.2	1.2	25.6	0.764	4	25.6	0.764	4	25.6	0.764	4
C1S/WF2	25.3	1.8	1.8	25.3	1.153	4	25.3	1.153	4	25.3	1.153	4
C2S/WF2	26.6	1.2	1.2	26.6	0.756	4	26.6	0.756	4	26.6	0.756	4
C3S/WF2	25.3	2.8	2.8	25.3	1.732	4	25.3	1.732	4	25.3	1.732	4
A1S/WF2												
A4S/WF2	21.6	1.1	1.1	21.6	0.699	4	21.6	0.699	4	21.6	0.699	4
A5S/WF2	22.7	2.0	2.0	22.7	1.260	4	22.7	1.260	4	22.7	1.260	4
C1/WF2	25.5	7.0	2.7	25.5	6.70	6	27.7	4.62	6	25.5	1.12	4
C2/WF2	26.6	1.2	1.1	26.6	0.48	3	26.6	0.47	3	26.6	0.32	3
C3/WF2	24.6	3.0	4.0	24.6	2.52	4	24.1	2.20	4	24.6	1.08	4
A1/WF2	24.6	2.9	4.3	24.6	2.71	4	23.9	2.25	4	24.6	0.97	4
A2/WF2	26.4	0.8	1.8	26.4	2.17	8	25.9	1.57	8	26.4	0.51	4
A4/WF2	24.4	3.8	1.4	24.4	2.40	4	25.6	1.64	4	24.4	0.89	4
A5/WF2	25.4	4.0	1.6	25.4	2.50	4	26.5	1.76	4	25.4	1.01	4
A6/WF2	25.3	8.2	3.8	25.3	5.13	4	27.5	3.78	4	25.3	1.46	4
A4F/WF2												
A5F/WF2	23.8	1.9	1.9							23.8	1.20	4
A4H/WF2	24.4	∞	∞	24.4	62.9	4	24.4	62.9	4	24.4	0.94	4
A5H/WF2	25.4	10.5	10.5							25.4	0.83	2

*Data for the impulse drying cases are at the critical temperatures while all other data are the mean values. The data used for hypothesis testing are also shown.

Table 22. CD STFI Index for Furnish WF3 with Upper and Lower 95% Confidence Intervals*

Case	Test 0			Test 1			Test 2			Test 3		
	CD STFI	C.I. +	C.I. -	CD STFI Mean	s	n	CD STFI Mean	s	n	CD STFI Mean	s	n
Con/WF3	13.1	1.0	1.0	13.1	0.408	3	13.1	0.408	3	13.1	0.408	3
D1/WF3	22.9	1.1	1.1	22.9	0.450	3	22.9	0.450	3	22.9	0.450	3
D2/WF3	21.9	2.8	2.8	21.9	1.141	3	21.9	1.141	3	21.9	1.141	3
D3/WF3	22.0	6.7	6.7	22.0	0.530	2	22.0	0.530	2	22.0	0.530	2
D4/WF3	19.8	2.8	2.8	19.8	1.113	3	19.8	1.113	3	19.8	1.113	3
D5/WF3	23.5	2.8	2.8	23.5	1.108	3	23.5	1.108	3	23.5	1.108	3
D6/WF3	23.8	2.2	2.2	23.8	0.877	3	23.8	0.877	3	23.8	0.877	3
C1S/WF3	23.0	23.3	23.3	23.0	1.836	2	23.0	1.836	2	23.0	1.836	2
C2S/WF3	24.4	2.4	2.4	24.4	0.958	3	24.4	0.958	3	24.4	0.958	3
C3S/WF3	21.9	1.2	1.2	21.9	0.466	3	21.9	0.466	3	21.9	0.466	3
A1S/WF3												
A4S/WF3	19.1	2.2	2.2	19.1	1.383	4	19.1	1.383	4	19.1	1.383	4
A5S/WF3	20.3	∞	∞									
C1/WF3	22.3	3.2	4.2	22.3	1.68	3	21.8	1.48	3	22.3	0.87	3
C2/WF3	23.1	1.6	0.7	23.1	1.96	8	23.5	1.43	8	23.1	0.47	4
C3/WF3	23.1	4.2	2.1	23.1	1.69	3	24.2	1.27	3	23.1	0.62	3
A1/WF3	22.9	1.0	1.0	22.9	1.32	9	22.9	1.31	9	22.9	0.35	4
A2/WF3	22.9	1.7	1.6	22.9	2.02	8	23.0	1.94	8	22.9	0.10	2
A4/WF3	23.3	6.1	2.4	23.3	2.47	3	25.1	1.71	3	23.3	0.95	3
A5/WF3	23.2	4.2	1.4	23.2	1.71	3	24.7	1.13	3	23.2	0.55	3
A6/WF3	23.2	1.4	1.3	23.2	0.58	3	23.2	0.55	3	23.2	0.27	3
A4F/WF3												
A5F/WF3	22.0	7.4	7.4							22.0	0.58	2
A4H/WF3	21.6	2.3	2.3							21.6	1.42	4
A5H/WF3	23.7	0.8	0.8							23.7	0.49	4

*Data for the impulse drying cases are at the critical temperatures while all other data are the mean values. The data used for hypothesis testing are also shown.

Table 23. CD STFI Index for Furnish FD5 with Upper and Lower 95% Confidence Intervals*

Case	Test 0			Test 1			Test 2			Test 3		
	CD STFI	C.I. +	C.I. -	CD STFI Mean	s	n	CD STFI Mean	s	n	CD STFI Mean	s	n
Con/FD5	15.3	3.6	3.6	15.3	2.259	4	15.3	2.259	4	15.3	2.259	4
D1/FD5	18.5	5.4	5.4	18.5	3.382	4	18.5	3.382	4	18.5	3.382	4
D2/FD5	17.3	0.5	0.5	17.3	0.300	4	17.3	0.300	4	17.3	0.300	4
D3/FD5	18.6	2.7	2.7	18.6	1.705	4	18.6	1.705	4	18.6	1.705	4
D4/FD5	15.8	0.5	0.5	15.8	0.039	2	15.8	0.039	2	15.8	0.039	2
D5/FD5	15.5	1.1	1.1	15.5	0.719	4	15.5	0.719	4	15.5	0.719	4
D6/FD5	19.2	4.3	4.3	19.2	2.672	4	19.2	2.672	4	19.2	2.672	4
C1S/FD5	18.2	3.7	3.7	18.2	2.301	4	18.2	2.301	4	18.2	2.301	4
C2S/FD5	20.1	3.5	3.5	20.1	2.201	4	20.1	2.201	4	20.1	2.201	4
C3S/FD5	17.0	1.2	1.2	17.0	0.739	4	17.0	0.739	4	17.0	0.739	4
A1S/FD5												
A4S/FD5	16.6	48.4	48.4	16.6	3.810	2	16.6	3.810	2	16.6	3.810	2
A5S/FD5	14.5	2.6	2.6	14.5	1.641	4	14.5	1.641	4	14.5	1.641	4
C1/FD5	17.6	3.1	3.7	17.6	3.01	5	17.3	2.77	5			
C2/FD5	18.1	4.6	4.9	18.1	4.70	6	17.9	4.54	6	18.1	0.88	3
C3/FD5	17.3	2.3	1.7	17.3	1.44	4	17.6	1.24	4	17.3	0.55	4
A1/FD5	17.3	57.6	51.7	17.3	6.41	2	20.3	6.09	2	17.3	1.31	2
A2/FD5	17.7	4.0	4.0							17.7	2.52	4
A4/FD5	16.3	1.6	1.6	16.3	1.89	8	16.3	1.89	8	16.3	0.79	4
A5/FD5	14.1	1.6	2.1	14.1	1.29	4	13.9	1.14	4			
A6/FD5	18.3	34.1	34.1							18.3	2.68	2
A4F/FD5												
A5F/FD5												
A4H/FD5												
A5H/FD5												

*Data for the impulse drying cases are at the critical temperatures while all other data are the mean values. The data used for hypothesis testing are also shown.

Table 24. CD STFI Index for Furnish FD6 with Upper and Lower 95% Confidence Intervals*

Case	Test 0			Test 1			Test 2			Test 3		
	CD STFI	C.I. +	C.I. -	CD STFI Mean	s	n	CD STFI Mean	s	n	CD STFI Mean	s	n
Con/FD6	12.8	1.2	1.2	12.8	0.769	4	12.8	0.769	4	12.8	0.769	4
D1/FD6	19.0	0.4	0.4	19.0	0.144	3	19.0	0.144	3	19.0	0.144	3
D2/FD6	17.6	3.2	3.2	17.6	2.024	4	17.6	2.024	4	17.6	2.024	4
D3/FD6	18.1	2.7	2.7	18.1	1.699	4	18.1	1.699	4	18.1	1.699	4
D4/FD6	18.2	4.0	4.0	18.2	2.541	4	18.2	2.541	4	18.2	2.541	4
D5/FD6	18.5	0.7	0.7	18.5	0.429	4	18.5	0.429	4	18.5	0.429	4
D6/FD6	19.1	1.7	1.7	19.1	1.047	4	19.1	1.047	4	19.1	1.047	4
C1S/FD6	17.2	5.0	5.0	17.2	1.997	3	17.2	1.997	3	17.2	1.997	3
C2S/FD6	21.7	0.4	0.4	21.7	0.028	2	21.7	0.028	2	21.7	0.028	2
C3S/FD6	18.2	1.4	1.4	18.2	0.868	4	18.2	0.868	4	18.2	0.868	4
A1S/FD6												
A4S/FD6	15.4	2.1	2.1	15.4	1.337	4	15.4	1.337	4	15.4	1.337	4
A5S/FD6	14.5	3.6	3.6	14.5	2.254	4	14.5	2.254	4	14.5	2.254	4
C1/FD6	20.3	3.4	1.6	20.3	2.14	4	21.2	1.58	4	20.3	1.02	4
C2/FD6	19.8	1.6	3.4	19.8	2.14	4	18.9	1.58	4	19.8	0.92	4
C3/FD6	21.4	2.9	1.4	21.4	1.79	4	22.1	1.33	4	21.4	0.87	4
A1/FD6	21.6	10.5	4.3	21.6	6.62	4	24.7	4.67	4	21.6	1.71	4
A2/FD6	21.7	6.1	9.9	21.7	6.23	4	19.7	5.03	4	21.7	2.11	4
A4/FD6	21.1	7.1	3.9	21.1	4.45	4	22.7	3.46	4	21.1	2.48	4
A5/FD6	21.6	9.0	3.2	21.6	5.65	4	24.5	3.82	4	21.6	1.99	4
A6/FD6	19.7	5.1	6.2	19.7	3.89	4	19.1	3.53	4	19.7	1.71	4
A4F/FD6												
A5F/FD6	20.1	1.5	2.5	20.1	2.97	8	19.6	2.37	8	20.1	0.56	4
A4H/FD6	21.0	8.4	3.6	21.0	5.27	4	23.4	3.77	4	21.0	1.76	4
A5H/FD6	21.8	5.7	5.7	21.8	6.83	8	21.9	6.79	8	21.8	1.66	4

*Data for the impulse drying cases are at the critical temperatures while all other data are the mean values. The data used for hypothesis testing are also shown.

Table 25. CD STFI Index for Furnish FD7 with Upper and Lower 95% Confidence Intervals*

Case	Test 0			Test 1			Test 2			Test 3		
	CD STFI	C.I. +	C.I. -	CD STFI Mean	s	n	CD STFI Mean	s	n	CD STFI Mean	s	n
Con/FD7	13.6	1.0	1.0	13.6	0.654	4	13.6	0.654	4	13.6	0.654	4
D1/FD7	17.7	∞	∞									
D2/FD7	20.5	1.6	1.6	20.5	0.974	4	20.5	0.974	4	20.5	0.974	4
D3/FD7	20.0	2.3	2.3	20.0	1.449	4	20.0	1.449	4	20.0	1.449	4
D4/FD7	19.4	2.1	2.1	19.4	1.338	4	19.4	1.338	4	19.4	1.338	4
D5/FD7	19.5	1.0	1.0	19.5	0.616	4	19.5	0.616	4	19.5	0.616	4
D6/FD7	20.4	∞	∞									
C1S/FD7	20.2	1.8	1.8	20.2	1.150	4	20.2	1.150	4	20.2	1.150	4
C2S/FD7	18.8	4.3	4.3	18.8	1.709	3	18.8	1.709	3	18.8	1.709	3
C3S/FD7	20.3	1.4	1.4	20.3	0.543	3	20.3	0.543	3	20.3	0.543	3
A1S/FD7												
A4S/FD7	17.0	0.7	0.7	17.0	0.264	3	17.0	0.264	3	17.0	0.264	3
A5S/FD7	17.0	0.8	0.8	17.0	0.676	5	17.0	0.676	5	17.0	0.676	5
C1/FD7	19.2	1.0	1.6	19.2	0.98	4	18.9	0.81	4	19.2	0.55	4
C2/FD7	20.5	1.7	1.7	20.5	1.81	7	20.5	1.81	7	20.5	0.67	3
C3/FD7	20.3	1.4	1.7	20.3	2.05	8	20.2	1.84	8	20.3	0.66	4
A1/FD7	21.3	13.9	13.9							21.3	1.10	2
A2/FD7	22.0	2.5	2.5							22.0	1.56	4
A4/FD7	21.1	5.4	1.9	21.1	3.40	4	22.9	2.29	4	21.1	1.19	4
A5/FD7	22.2	6.1	3.4	22.2	3.83	4	23.6	2.97	4	22.2	2.11	4
A6/FD7	20.9	7.4	4.1	20.9	4.62	4	22.5	3.61	4	20.9	1.61	4
A4F/FD7												
A5F/FD7	18.9	1.5	1.5							18.9	0.95	4
A4H/FD7	19.1	1.8	1.8							19.1	1.14	4
A5H/FD7	20.7	3.1	3.1							20.7	1.98	4

*Data for the impulse drying cases are at the critical temperatures while all other data are the mean values. The data used for hypothesis testing are also shown.

Table 26. MD STFI Index for Furnish WF1 with Upper and Lower 95% Confidence Limits*

Case	Test 0			Test 1			Test 2			Test 3		
	MD STFI	C.I. +	C.I. -	Mean	s	n	Mean	s	n	Mean	s	n
Con/WF1	20.6	1.2	1.2	20.6	0.10	2	20.6	0.10	2	20.6	0.10	2
D1/WF1	31.5	3.6	3.6	31.5	2.24	4	31.5	2.24	4	31.5	2.24	4
D2/WF1	33.6	60.2	60.2	33.6	4.74	2	33.6	4.74	2	33.6	4.74	2
D3/WF1	33.5	2.8	2.8	33.5	1.12	3	33.5	1.12	3	33.5	1.12	3
D4/WF1	33.2	7.1	7.1	33.2	4.44	4	33.2	4.44	4	33.2	4.44	4
D5/WF1	36.1	3.4	3.4	36.1	2.15	4	36.1	2.15	4	36.1	2.15	4
D6/WF1	32.7	3.4	3.4	32.7	2.13	4	32.7	2.13	4	32.7	2.13	4
C1S/WF1	32.9	15.0	15.0	32.9	6.04	3	32.9	6.04	3	32.9	6.04	3
C2S/WF1	35.9	1.5	1.5	35.9	0.96	4	35.9	0.96	4	35.9	0.96	4
C3S/WF1	32.7	63.3	63.3	32.7	4.98	2	32.7	4.98	2	32.7	4.98	2
A1S/WF1	27.0	47.3	47.3	27.0	3.72	2	27.0	3.72	2	27.0	3.72	2
A4S/WF1	28.3	3.3	3.3	28.3	2.09	4	28.3	2.09	4	28.3	2.09	4
A5S/WF1												
C1/WF1	34.3	5.8	2.8	34.3	3.67	4	35.8	2.71	4	34.3	1.63	4
C2/WF1	35.5	7.8	4.8	35.5	6.27	5	37.0	5.06	5	35.5	0.42	2
C3/WF1	30.2	11.5	15.7	30.2	9.86	4	28.1	8.54	4	30.2	3.93	4
A1/WF1	36.0	9.4	4.0	36.0	5.89	4	38.7	4.19	4	36.0	2.48	4
A2/WF1	34.1	3.5	7.8	34.1	4.89	4	32.0	3.54	4	34.1	1.61	4
A4/WF1	34.8	8.9	3.2	34.8	5.61	4	37.7	3.82	4	34.8	2.03	4
A5/WF1	38.3	14.1	2.1	38.3	8.89	4	44.3	5.11	4	38.3	1.33	4
A6/WF1	34.7	5.8	4.5	34.7	3.63	4	35.4	3.22	4	34.7	1.56	4
A4F/WF1												
A5F/WF1	34.8	10.7	3.7	34.8	6.72	4	38.3	4.54	4	34.8	2.11	4
A4H/WF1	35.2	∞	∞	35.2	40.26	3	35.2	40.26	3	35.2	1.18	3
A5H/WF1	37.1	3.0	1.7	37.1	2.83	6	37.7	2.23	6	37.1	1.07	4

*Data for the impulse drying cases are at the critical temperatures while all other data are the mean values. The data used for hypothesis testing are also shown.

Table 27. MD STFI Index for Furnish WF2 with Upper and Lower 95% Confidence Limits*

Case	Test 0			Test 1			Test 2			Test 3		
	MD STFI	C.I. +	C.I. -	Mean	s	n	Mean	s	n	Mean	s	n
Con/WF2	27.5	2.3	2.3	27.5	1.42	4	27.5	1.42	4	27.5	1.42	4
D1/WF2	37.0	4.4	4.4	37.0	1.78	3	37.0	1.78	3	37.0	1.78	3
D2/WF2	37.3	1.3	1.3	37.3	0.53	3	37.3	0.53	3	37.3	0.53	3
D3/WF2	37.1	1.2	1.2	37.1	0.75	4	37.1	0.75	4	37.1	0.75	4
D4/WF2	36.1	1.9	1.9	36.1	1.21	4	36.1	1.21	4	36.1	1.21	4
D5/WF2	38.6	1.4	1.4	38.6	0.89	4	38.6	0.89	4	38.6	0.89	4
D6/WF2	37.4	1.7	1.7	37.4	1.05	4	37.4	1.05	4	37.4	1.05	4
C1S/WF2	36.8	2.7	2.7	36.8	1.71	4	36.8	1.71	4	36.8	1.71	4
C2S/WF2	37.7	1.2	1.2	37.7	0.77	4	37.7	0.77	4	37.7	0.77	4
C3S/WF2	37.6	2.3	2.3	37.6	1.47	4	37.6	1.47	4	37.6	1.47	4
A1S/WF2												
A4S/WF2	32.9	1.1	1.1	32.9	0.66	4	32.9	0.66	4	32.9	0.66	4
A5S/WF2	33.0	3.2	3.2	33.0	2.03	4	33.0	2.03	4	33.0	2.03	4
C1/WF2	36.6	10.1	4.1	36.6	9.65	6	39.7	6.76	6	36.6	1.64	4
C2/WF2	38.0	1.8	1.6	38.0	0.72	3	38.1	0.67	3	38.0	0.46	3
C3/WF2	35.1	1.7	3.4	35.1	4.03	8	34.3	3.06	8	35.1	1.10	4
A1/WF2	36.3	3.1	3.5	36.3	2.17	4	36.1	2.05	4	36.3	0.89	4
A2/WF2	37.3	0.9	1.3	37.3	1.51	8	37.1	1.27	8	37.3	0.45	4
A4/WF2	35.9	4.3	1.6	35.9	2.67	4	37.2	1.85	4	35.9	1.02	4
A5/WF2	37.2	5.8	2.2	37.2	3.62	4	38.9	2.51	4	37.2	1.39	4
A6/WF2	34.6	6.2	7.0	34.6	4.37	4	34.2	4.12	4	34.6	1.60	4
A4F/WF2												
A5F/WF2	34.9	2.1	2.1							34.9	1.35	4
A4H/WF2	35.9	∞	∞	35.9	62.85	4	35.9	62.85	4	35.9	1.17	4
A5H/WF2	37.8	29.5	29.5							37.8	2.32	2

*Data for the impulse drying cases are at the critical temperatures while all other data are the mean values. The data used for hypothesis testing are also shown.

Table 28. MD STFI Index for Furnish WF3 with Upper and Lower 95% Confidence Limits*

Case	Test 0			Test 1			Test 2			Test 3		
	MD STFI	CI. +	CI. -	Mean	s	n	Mean	s	n	Mean	s	n
Con/WF3	18.5	3.2	3.2	18.5	1.27	3	18.5	1.27	3	18.5	1.27	3
D1/WF3	29.3	8.4	8.4	29.3	3.37	3	29.3	3.37	3	29.3	3.37	3
D2/WF3	30.9	2.0	2.0	30.9	0.80	3	30.9	0.80	3	30.9	0.80	3
D3/WF3	29.5	24.5	24.5	29.5	1.93	2	29.5	1.93	2	29.5	1.93	2
D4/WF3	28.0	4.4	4.4	28.0	1.76	3	28.0	1.76	3	28.0	1.76	3
D5/WF3	31.9	1.5	1.5	31.9	0.60	3	31.9	0.60	3	31.9	0.60	3
D6/WF3	30.5	4.4	4.4	30.5	1.78	3	30.5	1.78	3	30.5	1.78	3
C1S/WF3	30.3	31.2	31.2	30.3	2.46	2	30.3	2.46	2	30.3	2.46	2
C2S/WF3	32.6	3.5	3.5	32.6	1.39	3	32.6	1.39	3	32.6	1.39	3
C3S/WF3	29.0	1.9	1.9	29.0	0.75	3	29.0	0.75	3	29.0	0.75	3
A1S/WF3												
A4S/WF3	26.4	0.8	0.8	26.4	0.48	4	26.4	0.48	4	26.4	0.48	4
A5S/WF3	22.6	∞	∞									
C1/WF3	30.3	3.4	3.8	30.3	1.52	3	30.1	1.45	3	30.3	0.85	3
C2/WF3	31.6	1.1	2.5	31.6	3.00	8	30.9	2.19	8	31.6	0.72	4
C3/WF3	31.4	7.5	3.5	31.4	3.01	3	33.4	2.20	3	31.4	1.08	3
A1/WF3	30.5	2.5	2.5	30.5	3.21	9	30.5	3.20	9	30.5	0.78	4
A2/WF3	30.2	3.9	3.5	30.2	4.64	8	30.4	4.41	8	30.2	0.18	2
A4/WF3	31.7	7.3	2.7	31.7	2.93	3	34.0	2.01	3	31.7	1.09	3
A5/WF3	33.7	15.2	4.8	33.7	6.12	3	38.9	4.02	3	33.7	1.93	3
A6/WF3	31.6	3.0	4.8	31.6	1.93	3	30.8	1.57	3	31.6	0.78	3
A4F/WF3												
A5F/WF3	31.2	19.1	19.1							31.2	1.51	2
A4H/WF3	30.3	3.9	3.9							30.3	2.45	4
A5H/WF3	32.4	0.9	0.9							32.4	0.54	4

*Data for the impulse drying cases are at the critical temperatures while all other data are the mean values. The data used for hypothesis testing are also shown.

Table 29. MD STFI Index for Furnish FD5 with Upper and Lower 95% Confidence Limits*

Case	Test 0			Test 1			Test 2			Test 3		
	MD STFI	C.I. +	C.I. -	Mean	s	n	Mean	s	n	Mean	s	n
Con/FD5	23.7	5.0	5.0	23.7	3.14	4	23.7	3.14	4	23.7	3.14	4
D1/FD5	27.0	5.3	5.3	27.0	3.33	4	27.0	3.33	4	27.0	3.33	4
D2/FD5	32.1	1.7	1.7	32.1	1.07	4	32.1	1.07	4	32.1	1.07	4
D3/FD5	31.3	3.3	3.3	31.3	2.09	4	31.3	2.09	4	31.3	2.09	4
D4/FD5	27.5	19.7	19.7	27.5	1.55	2	27.5	1.55	2	27.5	1.55	2
D5/FD5	30.2	2.7	2.7	30.2	1.69	4	30.2	1.69	4	30.2	1.69	4
D6/FD5	29.6	6.4	6.4	29.6	4.04	4	29.6	4.04	4	29.6	4.04	4
C1S/FD5	29.4	4.7	4.7	29.4	2.93	4	29.4	2.93	4	29.4	2.93	4
C2S/FD5	30.2	4.1	4.1	30.2	2.59	4	30.2	2.59	4	30.2	2.59	4
C3S/FD5	30.5	3.1	3.1	30.5	1.96	4	30.5	1.96	4	30.5	1.96	4
A1S/FD5												
A4S/FD5	21.7	93.2	93.2	21.7	7.34	2	21.7	7.34	2	21.7	7.34	2
A5S/FD5	20.8	5.9	5.9	20.8	3.69	4	20.8	3.69	4	20.8	3.69	4
C1/FD5	30.2	12.9	12.0									
C2/FD5	28.9	5.5	7.5	28.9	3.02	3	27.9	2.62	3	28.9	1.11	3
C3/FD5	29.8	3.7	5.0	29.8	3.14	4	29.2	2.74	4	29.8	1.22	4
A1/FD5	28.5	125.8	134.1	28.5	14.93	2	24.4	14.47	2	28.5	3.11	2
A2/FD5	30.0	4.5	4.5							30.0	2.80	4
A4/FD5	28.6	12.3	8.0	28.6	7.74	4	30.8	6.40	4	28.6	4.62	4
A5/FD5	24.5	7.0	3.6	24.5	4.43	4	26.2	3.33	4			
A6/FD5	29.1	41.4	41.4							29.1	3.26	2
A4F/FD5												
A5F/FD5												
A4H/FD5												
A5H/FD5												

*Data for the impulse drying cases are at the critical temperatures while all other data are the mean values. The data used for hypothesis testing are also shown.

Table 30. MD STFI Index for Furnish FD6 with Upper and Lower 95% Confidence Limits*

Case	Test 0			Test 1			Test 2			Test 3		
	MD STFI	C.I. +	C.I. -	Mean	s	n	Mean	s	n	Mean	s	n
Con/FD6	19.3	2.5	2.5	19.3	1.59	4	19.3	1.59	4	19.3	1.59	4
D1/FD6	24.7	1.6	1.6	24.7	0.66	3	24.7	0.66	3	24.7	0.66	3
D2/FD6	25.3	4.0	4.0	25.3	2.53	4	25.3	2.53	4	25.3	2.53	4
D3/FD6	26.8	5.1	5.1	26.8	3.17	4	26.8	3.17	4	26.8	3.17	4
D4/FD6	24.9	3.7	3.7	24.9	2.34	4	24.9	2.34	4	24.9	2.34	4
D5/FD6	24.8	2.5	2.5	24.8	1.58	4	24.8	1.58	4	24.8	1.58	4
D6/FD6	25.4	4.2	4.2	25.4	2.61	4	25.4	2.61	4	25.4	2.61	4
C1S/FD6	25.0	3.9	3.9	25.0	1.56	3	25.0	1.56	3	25.0	1.56	3
C2S/FD6	28.0	8.3	8.3	28.0	0.65	2	28.0	0.65	2	28.0	0.65	2
C3S/FD6	26.9	0.9	0.9	26.9	0.59	4	26.9	0.59	4	26.9	0.59	4
A1S/FD6												
A4S/FD6	22.1	1.9	1.9	22.1	1.18	4	22.1	1.18	4	22.1	1.18	4
A5S/FD6	20.9	4.4	4.4	20.9	2.76	4	20.9	2.76	4	20.9	2.76	4
C1/FD6	26.4	2.8	1.7	26.4	1.77	4	27.0	1.41	4	26.4	0.93	4
C2/FD6	28.7	4.4	1.7	28.7	2.73	4	30.0	1.91	4	28.7	1.08	4
C3/FD6	26.0	0.5	1.0	26.0	0.65	4	25.8	0.49	4	26.0	0.34	4
A1/FD6	28.2	6.5	10.0	28.2	6.27	4	26.4	5.17	4	28.2	1.89	4
A2/FD6	28.8	5.2	3.7	28.8	3.26	4	29.5	2.80	4	28.8	1.17	4
A4/FD6	27.1	6.3	3.5	27.1	3.94	4	28.4	3.08	4	27.1	2.21	4
A5/FD6	28.8	9.9	3.5	28.8	6.24	4	31.9	4.23	4	28.8	2.23	4
A6/FD6	28.5	2.0	1.6	28.5	1.88	6	28.7	1.69	6	28.5	0.65	4
A4F/FD6												
A5F/FD6	26.6	3.8	2.4	26.6	4.58	8	27.3	3.70	8	26.6	0.83	4
A4H/FD6	28.8	10.9	3.5	28.8	6.84	4	32.5	4.51	4	28.8	2.10	4
A5H/FD6	29.5	4.5	4.9	29.5	5.84	8	29.3	5.58	8	29.5	1.37	4

*Data for the impulse drying cases are at the critical temperatures while all other data are the mean values. The data used for hypothesis testing are also shown.

Table 31. MD STFI Index for Furnish FD7 with Upper and Lower 95% Confidence Limits*

Case	Test 0			Test 1			Test 2			Test 3		
	MD STFI	C.I. +	C.I. -	Mean	s	n	Mean	s	n	Mean	s	n
Con/FD7	21.3	1.4	1.4	21.3	0.90	4	21.3	0.90	4	21.3	0.90	4
D1/FD7	28.1	∞	∞									
D2/FD7	27.8	3.0	3.0	27.8	1.91	4	27.8	1.91	4	27.8	1.91	4
D3/FD7	28.7	2.1	2.1	28.7	1.33	4	28.7	1.33	4	28.7	1.33	4
D4/FD7	29.2	3.4	3.4	29.2	2.14	4	29.2	2.14	4	29.2	2.14	4
D5/FD7	27.5	1.4	1.4	27.5	0.90	4	27.5	0.90	4	27.5	0.90	4
D6/FD7	29.2	∞	∞									
C1S/FD7	29.2	2.3	2.3	29.2	1.44	4	29.2	1.44	4	29.2	1.44	4
C2S/FD7	28.9	3.1	3.1	28.9	1.24	3	28.9	1.24	3	28.9	1.24	3
C3S/FD7	29.2	1.7	1.7	29.2	0.70	3	29.2	0.70	3	29.2	0.70	3
A1S/FD7												
A4S/FD7	22.3	5.3	5.3	22.3	2.12	3	22.3	2.12	3	22.3	2.12	3
A5S/FD7	21.9	1.2	1.2	21.9	0.96	5	21.9	0.96	5	21.9	0.96	5
C1/FD7	27.1	1.5	2.6	27.1	1.65	4	26.6	1.30	4	27.1	0.87	4
C2/FD7	27.4	1.6	1.6	27.4	1.70	7	27.4	1.70	7	27.4	0.63	3
C3/FD7	27.4	1.8	2.9	27.4	3.50	8	26.9	2.80	8	27.4	0.88	4
A1/FD7	29.0	3.0	3.0	29.0	2.41	5	29.0	2.41	5	29.0	0.33	2
A2/FD7	32.0	1.5	1.5							32.0	0.96	4
A4/FD7	28.8	8.7	3.1	28.8	5.46	4	31.6	3.70	4	28.8	1.94	4
A5/FD7	31.0	10.6	5.8	31.0	6.67	4	33.4	5.17	4	31.0	3.67	4
A6/FD7	29.3	3.6	4.6	29.3	2.91	4	28.8	2.60	4	29.3	1.16	4
A4F/FD7												
A5F/FD7	27.4	3.2	3.2							27.4	2.01	4
A4H/FD7	27.1	2.0	1.3	27.1	2.43	8	27.4	1.99	8	27.1	0.81	4
A5H/FD7	29.7	1.2	1.2							29.7	0.77	4

*Data for the impulse drying cases are at the critical temperatures while all other data are the mean values. The data used for hypothesis testing are also shown.

Table 32. Density for Furnish WF1 with Upper and Lower 95% Confidence Limits*

Case	Test 0			Test 1			Test 2			Test 3		
	Den	C.I. +	C.I. -	Mean	s	n	Mean	s	n	Mean	s	n
Con/WF1	0.430	0.007	0.007	0.430	0.0044	4	0.430	0.0044	4	0.430	0.0044	4
D1/WF1	0.743	0.029	0.029	0.743	0.0348	8	0.743	0.0348	8	0.743	0.0348	8
D2/WF1	0.830	0.036	0.036	0.830	0.0226	4	0.830	0.0226	4	0.830	0.0226	4
D3/WF1	0.819	0.013	0.013	0.819	0.0129	6	0.819	0.0129	6	0.819	0.0129	6
D4/WF1	0.743	0.038	0.038	0.743	0.0454	8	0.743	0.0454	8	0.743	0.0454	8
D5/WF1	0.870	0.012	0.012	0.870	0.0148	8	0.870	0.0148	8	0.870	0.0148	8
D6/WF1	0.920	0.042	0.042	0.920	0.0499	8	0.920	0.0499	8	0.920	0.0499	8
C1S/WF1	0.806	0.070	0.070	0.806	0.0663	6	0.806	0.0663	6	0.806	0.0663	6
C2S/WF1	0.917	0.018	0.018	0.917	0.0213	8	0.917	0.0213	8	0.917	0.0213	8
C3S/WF1	0.900	0.080	0.080	0.900	0.0506	4	0.900	0.0506	4	0.900	0.0506	4
A1S/WF1	0.764	0.077	0.077	0.764	0.0481	4	0.764	0.0481	4	0.764	0.0481	4
A4S/WF1	0.753	0.014	0.014	0.753	0.0172	8	0.753	0.0172	8	0.753	0.0172	8
A5S/WF1												
C1/WF1	0.885	0.076	0.027	0.885	0.1424	16	0.909	0.0965	16	0.885	0.0322	8
C2/WF1	0.992	0.249	0.153	0.992	0.3474	10	1.040	0.2809	10	0.992	0.0532	4
C3/WF1	0.865	0.062	0.083	0.865	0.1563	16	0.854	0.1363	16	0.865	0.0512	8
A1/WF1	0.941	0.137	0.047	0.941	0.1641	8	0.986	0.1099	8	0.941	0.0556	8
A2/WF1	0.917	0.042	0.029	0.917	0.0500	8	0.923	0.0421	8	0.917	0.0192	8
A4/WF1	0.865	0.111	0.031	0.865	0.1327	8	0.905	0.0849	8	0.865	0.0372	8
A5/WF1	0.926	0.179	0.022	0.926	0.2139	8	1.004	0.1202	8	0.926	0.0264	8
A6/WF1	0.838	0.075	0.021	0.838	0.0902	8	0.865	0.0575	8	0.838	0.0247	8
A4F/WF1												
A5F/WF1	0.830	0.073	0.040	0.830	0.0872	8	0.846	0.0676	8	0.830	0.0315	8
A4H/WF1	0.773	∞	∞	0.773	105	6	0.773	105	6	0.773	0.0185	6
A5H/WF1	0.854	0.003	0.003							0.854	0.0041	8

*Data for the impulse drying cases are at the critical temperatures while all other data are the mean values. The data used for hypothesis testing are also shown.

Table 33. Density for Furnish WF2 with Upper and Lower 95% Confidence Limits*

Case	Test 0			Test 1			Test 2			Test 3		
	Den	C.I. +	C.I. -	Mean	s	n	Mean	s	n	Mean	s	n
Con/WF2	0.549	0.007	0.007	0.549	0.0084	8	0.549	0.0084	8	0.549	0.0084	8
D1/WF2	0.803	0.034	0.034	0.803	0.0325	6	0.803	0.0325	6	0.803	0.0325	6
D2/WF2	0.905	0.024	0.024	0.905	0.0230	6	0.905	0.0230	6	0.905	0.0230	6
D3/WF2	0.850	0.020	0.020	0.850	0.0242	8	0.850	0.0242	8	0.850	0.0242	8
D4/WF2	0.759	0.009	0.009	0.759	0.0111	8	0.759	0.0111	8	0.759	0.0111	8
D5/WF2	0.863	0.008	0.008	0.863	0.0098	8	0.863	0.0098	8	0.863	0.0098	8
D6/WF2	0.805	0.018	0.018	0.805	0.0212	8	0.805	0.0212	8	0.805	0.0212	8
C1S/WF2	0.850	0.048	0.048	0.850	0.0569	8	0.850	0.0569	8	0.850	0.0569	8
C2S/WF2	0.981	0.017	0.017	0.981	0.0207	8	0.981	0.0207	8	0.981	0.0207	8
C3S/WF2	0.900	0.017	0.017	0.900	0.0202	8	0.900	0.0202	8	0.900	0.0202	8
A1S/WF2												
A4S/WF2	0.723	0.008	0.008	0.723	0.0097	8	0.723	0.0097	8	0.723	0.0097	8
A5S/WF2	0.757	0.015	0.015	0.757	0.0173	8	0.757	0.0173	8	0.757	0.0173	8
C1/WF2	0.881	0.118	0.024	0.881	0.1850	12	0.927	0.1118	12	0.881	0.0293	8
C2/WF2	0.928	0.020	0.047	0.928	0.0446	6	0.914	0.0318	6	0.928	0.0191	6
C3/WF2	0.851	0.021	0.043	0.851	0.0810	16	0.840	0.0601	16	0.851	0.0250	8
A1/WF2	0.908	0.039	0.027	0.908	0.0465	8	0.914	0.0394	8	0.908	0.0170	8
A2/WF2	0.896	0.010	0.035	0.896	0.0662	16	0.883	0.0426	16	0.896	0.0121	8
A4/WF2	0.913	0.188	0.054	0.913	0.2249	8	0.980	0.1447	8	0.913	0.0645	8
A5/WF2	0.893	0.130	0.038	0.893	0.1559	8	0.939	0.1005	8	0.893	0.0451	8
A6/WF2	0.925	0.069	0.035	0.925	0.0826	8	0.943	0.0621	8	0.925	0.0241	8
A4F/WF2												
A5F/WF2	0.810	0.017	0.017							0.810	0.0200	8
A4H/WF2	0.771	∞	∞	0.771	119	8	0.771	119	8	0.771	0.0117	8
A5H/WF2	0.857	0.092	0.092							0.857	0.0579	4

*Data for the impulse drying cases are at the critical temperatures while all other data are the mean values. The data used for hypothesis testing are also shown.

Table 34. Density for Furnish WF3 with Upper and Lower 95% Confidence Limits*

Case	Test 0			Test 1			Test 2			Test 3		
	Den	C.I. +	C.I. -	Mean	s	n	Mean	s	n	Mean	s	n
Con/WF3	0.496	0.013	0.013	0.496	0.0127	6	0.496	0.0127	6	0.496	0.0127	6
D1/WF3	0.793	0.032	0.032	0.793	0.0300	6	0.793	0.0300	6	0.793	0.0300	6
D2/WF3	0.858	0.028	0.028	0.858	0.0269	6	0.858	0.0269	6	0.858	0.0269	6
D3/WF3	0.861	0.026	0.026	0.861	0.0162	4	0.861	0.0162	4	0.861	0.0162	4
D4/WF3	0.769	0.019	0.019	0.769	0.0182	6	0.769	0.0182	6	0.769	0.0182	6
D5/WF3	0.894	0.022	0.022	0.894	0.0209	6	0.894	0.0209	6	0.894	0.0209	6
D6/WF3	0.799	0.031	0.031	0.799	0.0297	6	0.799	0.0297	6	0.799	0.0297	6
C1S/WF3	0.876	0.038	0.038	0.876	0.0237	4	0.876	0.0237	4	0.876	0.0237	4
C2S/WF3	0.959	0.023	0.023	0.959	0.0223	6	0.959	0.0223	6	0.959	0.0223	6
C3S/WF3	0.810	0.030	0.030	0.810	0.0284	6	0.810	0.0284	6	0.810	0.0284	6
A1S/WF3												
A4S/WF3	0.735	0.016	0.016	0.735	0.0191	8	0.735	0.0191	8	0.735	0.0191	8
A5S/WF3	0.709	0.341	0.341	0.709	0.0269	2	0.709	0.0269	2	0.709	0.0269	2
C1/WF3	0.880	0.032	0.026	0.880	0.0303	6	0.883	0.0278	6	0.880	0.0163	6
C2/WF3	0.931	0.014	0.022	0.931	0.0420	16	0.927	0.0340	16	0.931	0.0139	8
C3/WF3	0.909	0.196	0.055	0.909	0.1865	6	0.979	0.1193	6	0.909	0.0521	6
A1/WF3	0.851	0.036	0.036	0.851	0.0728	18	0.851	0.0722	18	0.851	0.0201	8
A2/WF3	0.819	0.034	0.031	0.819	0.0647	16	0.821	0.0613	16	0.819	0.0080	4
A4/WF3	0.932	0.203	0.062	0.932	0.1936	6	1.003	0.1261	6	0.932	0.0586	6
A5/WF3	0.903	0.189	0.047	0.903	0.1800	6	0.974	0.1124	6	0.903	0.0448	6
A6/WF3	0.925	0.106	0.035	0.925	0.1013	6	0.960	0.0672	6	0.925	0.0331	6
A4F/WF3												
A5F/WF3	0.837	0.019	0.019							0.837	0.0119	4
A4H/WF3	0.780	0.093	0.052	0.780	0.1752	16	0.801	0.1361	16	0.780	0.0618	8
A5H/WF3	0.807	0.009	0.009							0.807	0.0111	8

*Data for the impulse drying cases are at the critical temperatures while all other data are the mean values. The data used for hypothesis testing are also shown.

Table 35. Density for Furnish FD5 with Upper and Lower 95% Confidence Limits*

Case	Test 0			Test 1			Test 2			Test 3		
	Den	C.I. +	C.I. -	Mean	s	n	Mean	s	n	Mean	s	n
Con/FD5	0.617	0.016	0.016	0.617	0.0196	8	0.617	0.0196	8	0.617	0.0196	8
D1/FD5	0.773	0.031	0.031	0.773	0.0370	8	0.773	0.0370	8	0.773	0.0370	8
D2/FD5	0.794	0.013	0.013	0.794	0.0147	8	0.794	0.0147	8	0.794	0.0147	8
D3/FD5	0.820	0.013	0.013	0.820	0.0159	8	0.820	0.0159	8	0.820	0.0159	8
D4/FD5	0.703	0.026	0.026	0.703	0.0162	4	0.703	0.0162	4	0.703	0.0162	4
D5/FD5	0.783	0.014	0.014	0.783	0.0168	8	0.783	0.0168	8	0.783	0.0168	8
D6/FD5	0.754	0.010	0.010	0.754	0.0125	8	0.754	0.0125	8	0.754	0.0125	8
C1S/FD5	0.826	0.013	0.013	0.826	0.0155	8	0.826	0.0155	8	0.826	0.0155	8
C2S/FD5	0.832	0.016	0.016	0.832	0.0192	8	0.832	0.0192	8	0.832	0.0192	8
C3S/FD5	0.798	0.010	0.010	0.798	0.0115	8	0.798	0.0115	8	0.798	0.0115	8
A1S/FD5												
A4S/FD5	0.675	0.036	0.036	0.675	0.0227	4	0.675	0.0227	4	0.675	0.0227	4
A5S/FD5	0.741	0.016	0.016	0.741	0.0191	8	0.741	0.0191	8	0.741	0.0191	8
C1/FD5	0.847	0.053	0.030	0.847	0.0059	2	0.859	0.0046	2	0.847	0.0029	2
C2/FD5	0.838	0.032	0.023	0.838	0.0302	6	0.842	0.0260	6	0.838	0.0138	6
C3/FD5	0.812	0.043	0.023	0.812	0.0509	8	0.822	0.0389	8	0.812	0.0155	8
A1/FD5	0.782	0.040	0.100	0.782	0.0630	4	0.752	0.0441	4	0.782	0.0095	4
A2/FD5	0.763	0.121	0.038	0.763	0.1906	12	0.804	0.1256	12	0.763	0.0460	8
A4/FD5	0.723	0.046	0.022	0.723	0.0550	8	0.734	0.0409	8	0.723	0.0268	8
A5/FD5	0.784	0.057	0.023	0.784	0.0679	8	0.801	0.0475	8			
A6/FD5	0.758	0.097	0.039	0.758	0.1157	8	0.787	0.0813	8	0.758	0.0246	4
A4F/FD5												
A5F/FD5												
A4H/FD5												
A5H/FD5												

*Data for the impulse drying cases are at the critical temperatures while all other data are the mean values. The data used for hypothesis testing are also shown.

Table 36. Density for Furnish FD6 with Upper and Lower 95% Confidence Limits*

Case	Test 0			Test 1			Test 2			Test 3		
	Den	C.I. +	C.I. -	Mean	s	n	Mean	s	n	Mean	s	n
Con/FD6	0.498	0.010	0.010	0.498	0.0119	8	0.498	0.0119	8	0.498	0.0119	8
D1/FD6	0.769	0.010	0.010	0.769	0.0097	6	0.769	0.0097	6	0.769	0.0097	6
D2/FD6	0.805	0.020	0.020	0.805	0.0235	8	0.805	0.0235	8	0.805	0.0235	8
D3/FD6	0.792	0.010	0.010	0.792	0.0115	8	0.792	0.0115	8	0.792	0.0115	8
D4/FD6	0.693	0.010	0.010	0.693	0.0118	8	0.693	0.0118	8	0.693	0.0118	8
D5/FD6	0.803	0.024	0.024	0.803	0.0287	8	0.803	0.0287	8	0.803	0.0287	8
D6/FD6	0.728	0.023	0.023	0.728	0.0273	8	0.728	0.0273	8	0.728	0.0273	8
C1S/FD6	0.807	0.035	0.035	0.807	0.0329	6	0.807	0.0329	6	0.807	0.0329	6
C2S/FD6	0.931	0.039	0.039	0.931	0.0246	4	0.931	0.0246	4	0.931	0.0246	4
C3S/FD6	0.829	0.014	0.014	0.829	0.0162	8	0.829	0.0162	8	0.829	0.0162	8
A1S/FD6												
A4S/FD6	0.685	0.013	0.013	0.685	0.0150	8	0.685	0.0150	8	0.685	0.0150	8
A5S/FD6	0.706	0.028	0.028	0.706	0.0338	8	0.706	0.0338	8	0.706	0.0338	8
C1/FD6	0.841	0.022	0.011	0.841	0.0418	16	0.846	0.0314	16	0.841	0.0134	8
C2/FD6	0.836	0.025	0.041	0.836	0.0494	8	0.828	0.0398	8	0.836	0.0231	8
C3/FD6	0.880	0.042	0.028	0.880	0.0508	8	0.887	0.0420	8	0.880	0.0289	8
A1/FD6	0.860	0.067	0.014	0.860	0.0807	8	0.886	0.0490	8	0.860	0.0173	8
A2/FD6	0.839	0.033	0.141	0.839	0.1685	8	0.785	0.1038	8	0.839	0.0391	8
A4/FD6	0.806	0.111	0.055	0.806	0.1329	8	0.834	0.0992	8	0.806	0.0654	8
A5/FD6	0.832	0.137	0.047	0.832	0.1635	8	0.877	0.1098	8	0.832	0.0560	8
A6/FD6	0.911	0.010	0.023	0.911	0.0369	12	0.904	0.0266	12	0.911	0.0117	8
A4F/FD6												
A5F/FD6	0.853	0.111	0.069	0.853	0.2074	16	0.874	0.1688	16	0.853	0.0443	8
A4H/FD6	0.797	0.061	0.014	0.797	0.0729	8	0.820	0.0449	8	0.797	0.0170	8
A5H/FD6	0.874	0.136	0.095	0.874	0.2554	16	0.894	0.2168	16	0.874	0.0443	8

*Data for the impulse drying cases are at the critical temperatures while all other data are the mean values. The data used for hypothesis testing are also shown.

Table 37. Density for Furnish FD7 with Upper and Lower 95% Confidence Limits*

Case	Test 0			Test 1			Test 2			Test 3		
	Den	C.I. +	C.I. -	Mean	s	n	Mean	s	n	Mean	s	n
Con/FD7	0.552	0.008	0.008	0.552	0.0092	8	0.552	0.0092	8	0.552	0.0092	8
D1/FD7	0.777	0.081	0.081	0.777	0.0064	2	0.777	0.0064	2	0.777	0.0064	2
D2/FD7	0.820	0.012	0.012	0.820	0.0152	8	0.820	0.0152	8	0.820	0.0152	8
D3/FD7	0.833	0.012	0.012	0.833	0.0142	8	0.833	0.0142	8	0.833	0.0142	8
D4/FD7	0.717	0.011	0.011	0.717	0.0135	8	0.717	0.0135	8	0.717	0.0135	8
D5/FD7	0.792	0.009	0.009	0.792	0.0106	8	0.792	0.0106	8	0.792	0.0106	8
D6/FD7	0.830	0.036	0.036	0.830	0.0028	2	0.830	0.0028	2	0.830	0.0028	2
C1S/FD7	0.868	0.012	0.012	0.868	0.0148	8	0.868	0.0148	8	0.868	0.0148	8
C2S/FD7	0.931	0.023	0.023	0.931	0.0218	6	0.931	0.0218	6	0.931	0.0218	6
C3S/FD7	0.848	0.012	0.012	0.848	0.0112	6	0.848	0.0112	6	0.848	0.0112	6
A1S/FD7												
A4S/FD7	0.687	0.021	0.021	0.687	0.0199	6	0.687	0.0199	6	0.687	0.0199	6
A5S/FD7	0.695	0.020	0.020	0.695	0.0273	10	0.695	0.0273	10	0.695	0.0273	10
C1/FD7	0.866	0.017	0.013	0.866	0.0200	8	0.867	0.0180	8	0.866	0.0121	8
C2/FD7	0.800	0.115	0.057	0.800	0.1988	14	0.829	0.1492	14	0.800	0.0547	6
C3/FD7	0.802	0.054	0.087	0.802	0.1625	16	0.786	0.1321	16	0.802	0.0452	8
A1/FD7	0.860	0.034	0.018	0.860	0.0476	10	0.868	0.0363	10	0.860	0.0113	4
A2/FD7	0.789	0.007	0.007							0.789	0.0083	8
A4/FD7	0.836	0.147	0.041	0.836	0.1753	8	0.889	0.1123	8	0.836	0.0493	8
A5/FD7	0.736	0.042	0.022	0.736	0.0504	8	0.746	0.0383	8	0.736	0.0263	8
A6/FD7	0.927	0.064	0.023	0.927	0.0766	8	0.947	0.0523	8	0.927	0.0232	8
A4F/FD7												
A5F/FD7	0.848	0.013	0.013							0.848	0.0158	8
A4H/FD7	0.804	0.005	0.005							0.804	0.0055	8
A5H/FD7	0.904	0.015	0.015							0.904	0.0176	8

*Data for the impulse drying cases are at the critical temperatures while all other data are the mean values. The data used for hypothesis testing are also shown.

Hypothesis Testing:

For any one-variable, process condition change, the difference in physical property means were statistically evaluated using hypothesis testing. The following hypothesis was used for the test.

Null Hypothesis H_0: $P_1 - P_2 = 0$
Alternate Hypothesis H_1: $P_1 - P_2 \neq 0$

Assuming that the population standard deviations are unknown and unequal ($\sigma_1 \neq \sigma_2$), the following t-statistic is appropriate.

$$t' = \frac{(P_1 - P_2)}{\sqrt{\frac{(s_1)^2}{n_1} + \frac{(s_2)^2}{n_2}}}$$

$$\nu = \frac{\left(\frac{(s_1)^2}{n_1} + \frac{(s_2)^2}{n_2}\right)^2}{\frac{\left(\frac{(s_1)^2}{n_1}\right)^2}{n_1 - 1} + \frac{\left(\frac{(s_2)^2}{n_2}\right)^2}{n_2 - 1}}$$

where,
ν = degrees of freedom
P = physical property mean
s = data standard deviation
n = number of data points.

A 90% confidence level was chosen, therefore, $\alpha = 0.10$. The Alternate Hypothesis implies that a two-tailed test should be used and the calculated statistic is compared to $t_{\alpha/2,\nu}$. If $t' > t$ or $t' < -t$, then the Null Hypothesis is rejected and the Alternate Hypothesis is accepted. Otherwise, the hypothesis test is inconclusive.

A preliminary test (Test 0) was performed by looking for overlap between the confidence intervals. Because the confidence limits for the impulse dried cases are not symmetrical, an "effective" standard deviation had to be determined. The authors used the standard equation for calculating the confidence interval to backout an effective standard deviation for a given number of data points and confidence limit.

Three possible sets of values can be used to calculate the effective standard deviation for hypothesis testing. For the first set, the highest confidence limit was used along with the number of data points within the range of possible critical temperatures. For example, with the case used in Figure 3, there were 5 data points and the higher confidence limit was 7.8. This resulted in an effective standard deviation of 6.27.

The second set of values was calculated by adjusting the mean to be in the middle of the confidence range and using the average of the confidence limits. For the third set, only the number of data points at the critical temperature were used with the confidence limits at the critical temperature.

Tables 14 through 37 contain the mean values, confidence limits, standard deviations, and number of data points used for each hypothesis test. If there is not enough data to calculate a

points the hypothesis test could not be performed, therefore, that data was not used and is not shown in the chart. A few cases had a confidence interval that was infinite. For those cases, a confidence interval of 100 was used for the calculations.

Because of the low number of data points, many of the hypothesis tests were inconclusive. For these cases, the confidence level if the Null Hypothesis was rejected was calculated by integrating the t-distribution between the limits of $\pm t'$.

The results of the hypothesis tests are in Appendix E. The authors decided that Test 2 was not appropriate because changing the mean values would adversely effect any test on the means. Results of Tests 0, 1, and 3 for some important cases are summarized in Tables 38 to 77.

Table 38. Roll Surface Comparisons of Case A1 to Case C1

	TEST 0						TEST 1						TEST 3					
Property	WF 1	WF2	WF3	FD5	FD6	FD7	WF1	WF2	WF3	FD5	FD6	FD7	WF 1	WF2	WF3	FD5	FD6	FD7
% Sout	?	?	?	?	?	?	?(>)	?(>)	>	?(>)	?(>)	?(>)	>	>	>	id	>	>
%Confidence							82.0	63.2	92.4	8.8	74.9	47.1	99.8	95.9	99.9	id	99.3	94.2
CD STFI Index	?	?	?	?	?	?	>	?(<)	?(>)	?(<)	?(>)	id	>	?(<)	?(>)	id	?(>)	?(>)
%Confidence							90.1	21.4	35.4	3.2	27.7	id	99.6	71.0	58.4	id	76.0	76.1
MD STFI Index	?	?	?	?	?	?	?(>)	?(<)	?(>)	id	?(>)	?(>)	?(>)	?(<)	?(>)	id	?(>)	>
%Confidence							36.4	5.8	12.2	id	37.5	78.1	70.8	24.6	25.5	id	83.1	97.9
Density	?	?	?	?	?	?	?(>)	?(>)	?(<)	?(<)	?(>)	?(<)	>	>	<	<	>	?(<)
%Confidence							57.4	36.9	82.3	86.7	44.6	27.0	96.9	95.8	99.0	100.0	96.9	56.5

Table 39. Roll Surface Comparisons of Case A2 to Case C2

	TEST 0						TEST 1						TEST 3					
Property	WF 1	WF2	WF3	FD5	FD6	FD7	WF1	WF2	WF3	FD5	FD6	FD7	WF 1	WF2	WF3	FD5	FD6	FD7
% Sout	?	?	?	?	?	>	?(>)	?(>)	?(>)	?(>)	?(>)	>	>	>	>	?(>)	>	>
%Confidence							73.9	72.4	69.8	3.9	70.4	99.9	99.9	96.7	99.7	10.1	97.9	100.0
CD STFI Index	?	?	?	?	?	?	?(>)	?(<)	?(<)	id	?(>)	id	?(>)	?(<)	?(<)	?(<)	?(>)	?(>)
%Confidence							0.8	16.1	14.5	id	40.4	id	4.5	38.8	49.7	21.1	82.6	84.3
MD STFI Index	?	?	?	?	?	>	?(<)	?(<)	?(<)	id	?(>)	id	?(<)	?(<)	<	?(>)	?(>)	>
%Confidence							28.1	67.0	51.2	id	3.6	id	82.0	88.5	97.8	47.3	9.6	99.9
Density	?	?	<	?	?	?	?(<)	?(<)	<	?(<)	?(>)	id	<	<	<	<	?(>)	?(<)
%Confidence							48.5	78.8	100.0	79.2	3.3	id	92.9	99.3	100.0	99.8	13.0	35.4

Table 40. Pressure Comparisons of Case C2 to Case C1

	TEST 0						TEST 1						TEST 3					
Property	WF 1	WF2	WF3	FD5	FD6	FD7	WF1	WF2	WF3	FD5	FD6	FD7	WF 1	WF2	WF3	FD5	FD6	FD7
% Sout	?	?	?	?	?	?	?(>)	?(>)	?(>)	?(>)	?(>)	?(<)	?(>)	>	>	id	?(>)	<
%Confidence							21.0	56.0	44.8	36.2	35.6	80.3	78.5	96.4	94.2	id	79.6	98.3
CD STFI Index	?	?	?	?	?	?	?(>)	?(>)	?(>)	?(>)	?(<)	?(>)	>	?(>)	?(>)	id	?(<)	>
%Confidence							64.3	29.4	43.7	17.9	24.9	83.2	98.6	86.3	73.2	id	50.9	94.3
MD STFI Index	?	?	?	?	?	?	?(>)	?(>)	?(>)	id	?(>)	?(>)	?(>)	?(>)	>	id	>	?(>)
%Confidence							27.7	25.8	63.1	id	78.3	20.0	77.3	81.6	90.2	id	98.2	35.1
Density	?	?	?	?	?	?	?(>)	?(>)	>	?(<)	?(<)	?(<)	>	>	>	?(<)	?(<)	<
%Confidence							62.7	57.8	99.2	50.8	17.5	75.8	97.9	99.6	100.0	83.6	36.5	96.6

Table 41. Pressure Comparisons of Case A2 to Case A1

	TEST 0						TEST 1						TEST 3					
Property	WF 1	WF2	WF3	FD5	FD6	FD7	WF1	WF2	WF3	FD5	FD6	FD7	WF 1	WF2	WF3	FD5	FD6	FD7
% Sout	?	?	?	?	?	?	?(>)	?(>)	?(>)	?(>)	?(>)	?(>)	?(>)	?(>)	>	?(>)	?(>)	>
%Confidence							1.7	49.7	31.0	13.4	33.7	88.4	6.6	71.5	92.0	49.8	82.5	99.2
CD STFI Index	?	?	?	?	?	?	?(<)	?(>)	?(>)	id	?(>)	id	?(<)	>	?(>)	?(>)	?(>)	?(>)
%Confidence							44.5	69.6	2.3	id	1.2	id	81.2	97.7	9.8	18.8	3.9	42.7
MD STFI Index	?	?	?	?	?	?	?(<)	?(>)	?(<)	id	?(>)	id	?(<)	?(>)	?(<)	?(>)	?(>)	>
%Confidence							36.4	54.8	12.1	id	13.5	id	74.6	88.2	49.9	36.6	40.5	99.5
Density	?	?	?	?	?	<	?(<)	?(<)	?(<)	?(<)	?(<)	id	?(<)	?(<)	<	?(<)	?(<)	<
%Confidence							30.0	41.2	80.6	23.7	23.8	id	72.5	89.5	99.7	71.7	79.6	100.0

Table 42. Pressure Comparisons of Case A5 to Case A4

	TEST 0						TEST 1						TEST 3					
Property	WF 1	WF2	WF3	FD5	FD6	FD7	WF1	WF2	WF3	FD5	FD6	FD7	WF 1	WF2	WF3	FD5	FD6	FD7
% Sout	?	?	?	?	?	?	?(>)	?(>)	?(>)	?(<)	?(>)	?(>)	>	?(>)	?(>)	id	>	?(>)
%Confidence							39.5	22.6	25.0	75.3	71.5	14.7	93.8	69.8	77.1	id	98.3	38.6
CD STFI Index	?	?	?	?	?	?	?(>)	?(>)	?(<)	<	?(>)	?(>)	>	?(>)	?(<)	id	?(>)	?(>)
%Confidence							57.3	38.7	2.1	95.8	10.4	31.2	98.3	78.2	5.6	id	23.1	58.8
MD STFI Index	?	?	?	?	?	?	?(>)	?(>)	?(>)	?(<)	?(>)	?(>)	>	?(>)	?(>)	id	?(>)	?(>)
%Confidence							46.5	39.8	34.8	60.7	33.3	36.7	96.6	79.0	77.7	id	67.7	65.5
Density	?	?	?	?	?	<	?(>)	?(<)	?(<)	>	?(>)	?(<)	>	?(<)	?(<)	id	?(>)	<
%Confidence							49.2	15.8	20.4	93.2	26.8	84.0	99.8	50.7	63.3	id	59.4	100.0

Table 43. Pivot Position Comparisons of Case C3 to Case C1

	TEST 0						TEST 1						TEST 3					
Property	WF 1	WF2	WF3	FD5	FD6	FD7	WF1	WF2	WF3	FD5	FD6	FD7	WF 1	WF2	WF3	FD5	FD6	FD7
% Sout	?	?	?	?	?	?	?(<)	?(>)	?(>)	?(<)	?(>)	?(>)	?(<)	?(>)	?(>)	id	>	>
%Confidence							39.2	19.0	17.8	24.3	48.9	57.6	83.8	60.1	54.0	id	93.9	97.2
CD STFI Index	?	?	?	?	?	?	?(>)	?(<)	?(>)	?(<)	?(>)	?(>)	?(>)	?(<)	?(>)	id	?(>)	>
%Confidence							30.7	21.7	40.9	13.6	56.1	78.0	59.9	68.9	73.6	id	86.5	96.4
MD STFI Index	?	?	?	?	?	?	?(<)	?(<)	?(>)	id	?(<)	?(>)	?(<)	?(<)	?(>)	id	?(<)	?(>)
%Confidence							51.2	26.4	39.8	id	29.6	16.0	86.8	80.7	77.4	id	51.8	36.3
Density	?	?	?	?	?	?	?(<)	?(<)	?(>)	<	>	?(<)	?(<)	<	?(>)	<	>	<
%Confidence							29.1	38.7	27.2	90.9	91.6	85.8	62.9	95.2	75.1	100.0	99.4	99.5

Table 44. Pivot Position Comparisons of Case A6 to Case A4

	TEST 0						TEST 1						TEST 3					
Property	WF 1	WF2	WF3	FD5	FD6	FD7	WF1	WF2	WF3	FD5	FD6	FD7	WF 1	WF2	WF3	FD5	FD6	FD7
% Sout	?	?	?	?	?	?	?(>)	?(>)	?(>)	?(>)	>	?(>)	>	?(>)	?(>)	?(>)	>	?(>)
%Confidence							49.2	41.7	10.9	27.7	90.3	36.3	95.9	88.4	39.5	72.4	99.6	87.1
CD STFI Index	?	?	?	?	?	?	?(>)	?(>)	?(<)	id	?(<)	?(<)	?(>)	?(>)	?(<)	?(>)	?(<)	?(<)
%Confidence							28.6	22.8	4.8	id	34.6	5.7	63.5	64.8	12.2	50.5	60.2	16.3
MD STFI Index	?	?	?	?	?	?	?(<)	?(<)	?(<)	id	?(>)	?(>)	?(<)	?(<)	?(<)	?(>)	?(>)	?(>)
%Confidence							1.6	36.6	2.6	id	46.3	12.9	4.3	77.1	7.1	11.0	71.7	34.1
Density	?	?	?	?	?	?	?(<)	?(>)	?(<)	?(>)	>	?(>)	?(<)	?(>)	?(<)	>	>	>
%Confidence							36.3	11.5	6.2	55.2	93.9	79.2	89.3	38.4	20.0	94.5	99.7	99.9

Table 45. Felt Comparisons of Case A4 to Case A1

	TEST 0						TEST 1						TEST 3					
Property	WF 1	WF2	WF3	FD5	FD6	FD7	WF1	WF2	WF3	FD5	FD6	FD7	WF 1	WF2	WF3	FD5	FD6	FD7
% Sout	?	?	?	?	<	?	?(<)	?(<)	?(<)	?(>)	<	?(<)	<	?(<)	?(<)	?(>)	<	<
%Confidence							62.7	44.9	35.3	10.2	98.1	48.5	99.0	85.8	86.0	51.7	100.0	94.8
CD STFI Index	?	?	?	?	?	?	?(<)	?(<)	?(>)	?(<)	?(<)	id	?(<)	?(<)	?(>)	?(<)	?(<)	?(<)
%Confidence							40.9	8.6	17.3	13.4	9.4	id	81.0	23.3	41.4	49.1	24.5	9.6
MD STFI Index	?	?	?	?	?	?	?(<)	?(<)	?(>)	?(>)	?(<)	?(<)	?(<)	?(<)	?(>)	?(>)	?(<)	?(<)
%Confidence							22.0	17.9	43.0	0.5	22.1	4.1	51.4	43.2	80.7	2.0	51.9	11.8
Density	?	?	?	?	?	?	?(<)	?(>)	?(>)	?(<)	?(<)	?(<)	<	?(>)	>	<	<	?(<)
%Confidence							67.3	4.2	63.7	83.1	65.1	28.4	99.3	14.2	98.2	100.0	94.5	77.6

Table 46. Felt Comparisons of Case A5 to Case A2

	TEST 0						TEST 1						TEST 3					
Property	WF 1	WF2	WF3	FD5	FD6	FD7	WF1	WF2	WF3	FD5	FD6	FD7	WF 1	WF2	WF3	FD5	FD6	FD7
% Sout	?	?	?	?	?	?	?(<)	?(<)	?(<)	?(<)	?(<)	<	<	<	?(<)	id	?(<)	<
%Confidence							49.7	52.3	29.8	45.8	43.8	92.2	98.1	95.5	86.4	id	87.1	99.0
CD STFI Index	?	?	?	?	?	?	?(>)	?(<)	?(>)	id	?(<)	id	>	?(<)	?(>)	id	?(<)	?(>)
%Confidence							60.5	49.9	18.1	id	1.4	id	99.5	86.7	54.6	id	4.0	14.6
MD STFI Index	?	?	?	?	?	?	?(>)	?(<)	?(>)	id	?(<)	id	>	?(<)	>	id	?(<)	?(<)
%Confidence							55.6	6.1	56.5	id	0.8	id	99.3	15.6	91.1	id	2.2	35.7
Density	?	?	>	?	?	<	?(>)	?(<)	?(>)	?(>)	?(<)	id	?(>)	?(<)	>	id	?(<)	<
%Confidence							8.9	3.2	68.3	27.3	6.5	id	55.0	11.2	99.3	id	22.0	99.9

Table 47. Speed (NRT) Comparisons of Case A5F to Case A5

	TEST 0						TEST 1						TEST 3					
Property	WF 1	WF2	WF3	FD5	FD6	FD7	WF1	WF2	WF3	FD5	FD6	FD7	WF 1	WF2	WF3	FD5	FD6	FD7
% Sout	?	?	?	?	?	?	?(<)	?(<)	id	?(>)	?(<)	?(<)	<	?(<)	?(<)	id	?(<)	?(<)
%Confidence							52.2	16.4	id	33.7	4.4	2.1	98.4	49.0	87.4	id	13.0	9.2
CD STFI Index	?	?	?	id	?	?	?(<)	id	id	id	?(<)	id	<	<	?(<)	id	?(<)	<
%Confidence							66.4	id	id	id	34.3	id	99.8	91.3	85.3	id	74.3	95.3
MD STFI Index	?	?	?	id	?	?	?(<)	id	id	id	?(<)	id	<	<	?(<)	id	?(<)	?(<)
%Confidence							44.6	id	id	id	43.8	id	96.2	94.1	79.0	id	86.0	84.9
Density	<	<	<	id	?	>	?(<)	id	id	id	?(>)	id	<	<	<	id	?(>)	>
%Confidence							73.0	id	id	id	21.3	id	100.0	99.9	98.6	id	58.5	100.0

Table 48. Felt Wash Water Chemistry Comparisons of Case A4H to Case A4

	TEST 0						TEST 1						TEST 3					
Property	WF 1	WF2	WF3	FD5	FD6	FD7	WF1	WF2	WF3	FD5	FD6	FD7	WF 1	WF2	WF3	FD5	FD6	FD7
% Sout	?	?	?	id	?	?	?(>)	?(>)	?(<)	id	?(>)	?(>)	>	>	?(<)	id	>	?(>)
%Confidence							7.5	7.3	12.2	id	88.4	11.7	91.3	97.5	41.7	id	99.8	35.2
CD STFI Index	?	?	?	id	?	?	?(<)	?(<)	id	id	?(<)	id	?(<)	?(<)	?(<)	id	?(<)	<
%Confidence							0.9	0.0	id	id	1.9	id	28.6	0.4	87.3	id	4.2	95.1
MD STFI Index	?	?	?	id	?	?	?(>)	?(>)	id	id	?(>)	?(<)	?(>)	?(>)	?(<)	id	?(>)	?(<)
%Confidence							1.2	0.0	id	id	32.5	42.6	25.0	0.8	62.7	id	70.7	82.9
Density	?	?	?	id	?	?	?(<)	?(<)	?(<)	id	?(<)	id	<	<	<	id	?(<)	?(<)
%Confidence							0.2	0.3	86.8	id	13.7	id	100.0	100.0	99.9	id	29.9	88.7

Table 49. Felt Wash Water Chemistry Comparisons of Case A5H to Case A5

	TEST 0						TEST 1						TEST 3					
Property	WF 1	WF2	WF3	FD5	FD6	FD7	WF1	WF2	WF3	FD5	FD6	FD7	WF 1	WF2	WF3	FD5	FD6	FD7
% Sout	?	?	?	id	?	?	?(>)	id	?(>)	id	?(>)	id	?(>)	>	?(>)	id	?(>)	>
%Confidence							26.0	id	25.1	id	36.3	id	71.4	96.7	79.1	id	79.7	94.4
CD STFI Index	?	?	?	id	?	?	?(<)	id	id	id	?(>)	id	?(<)	?(>)	?(>)	id	?(>)	?(<)
%Confidence							30.7	id	id	id	5.5	id	83.7	6.0	71.0	id	15.4	65.7
MD STFI Index	?	?	?	id	?	?	?(<)	id	id	id	?(>)	id	?(<)	?(>)	?(<)	id	?(>)	?(<)
%Confidence							19.4	id	id	id	16.0	id	80.1	22.2	63.2	id	42.6	45.3
Density	<	?	<	id	?	>	id	id	id	id	?(>)	id	<	?(<)	<	id	?(>)	>
%Confidence							id	id	id	id	36.4	id	100.0	68.2	99.6	id	87.4	100.0

Table 50. Double Felted Pressing Comparisons of Case C1 to Case D1

	TEST 0						TEST 1						TEST 3					
Property	WF 1	WF2	WF3	FD5	FD6	FD7	WF1	WF2	WF3	FD5	FD6	FD7	WF 1	WF2	WF3	FD5	FD6	FD7
% Sout	>	?	>	?	>	?	>	?(>)	>	>	>	id	>	?(>)	>	id	>	id
%Confidence							93.7	32.7	97.0	91.4	97.7	id	99.8	79.8	99.9	id	100.0	id
CD STFI Index	?	?	?	?	?	?	?(>)	?(>)	?(<)	?(<)	?(>)	id	?(>)	?(>)	?(<)	id	>	id
%Confidence							64.2	41.7	34.8	31.3	67.9	id	75.5	71.9	57.9	id	91.0	id
MD STFI Index	?	?	?	?	?	?	?(>)	?(<)	?(>)	id	?(>)	id	?(>)	?(<)	?(>)	id	>	id
%Confidence							74.1	6.8	30.4	id	85.2	id	89.5	20.4	30.8	id	96.5	id
Density	>	>	>	>	>	?	>	?(>)	>	>	>	>	>	>	>	>	>	>
%Confidence							99.9	81.7	99.9	99.9	100.0	100.0	100.0	99.9	100.0	99.9	100.0	99.9

Table 51. Double Felted Pressing Comparisons of Case A1 to Case D1

	TEST 0						TEST 1						TEST 3					
Property	WF 1	WF2	WF3	FD5	FD6	FD7	WF1	WF2	WF3	FD5	FD6	FD7	WF 1	WF2	WF3	FD5	FD6	FD7
% Sout	>	?	>	?	>	?	>	>	>	?(>)	>	id	>	>	>	>	>	id
%Confidence							98.7	97.8	100.0	54.7	99.9	id	100.0	98.6	100.0	97.7	100.0	id
CD STFI Index	>	?	?	?	?	?	>	?(>)	?(>)	?(<)	?(>)	id	>	?(>)	?(>)	?(<)	>	id
%Confidence							94.9	35.0	2.2	14.9	51.1	id	99.8	45.2	3.5	41.8	94.4	id
MD STFI Index	?	?	?	?	?	?	?(>)	?(<)	?(>)	?(>)	?(>)	id	>	?(<)	?(>)	?(>)	>	id
%Confidence							77.2	32.8	35.6	9.2	65.1	id	96.4	40.9	37.6	37.2	97.3	id
Density	>	>	?	?	>	?	>	>	>	?(>)	>	>	>	>	>	?(>)	>	>
%Confidence							99.0	100.0	98.8	19.7	98.4	100.0	100.0	100.0	99.6	47.1	100.0	100.0

Table 52. Double Felted Pressing Comparisons of Case C2 to Case D2

	TEST 0						TEST 1						TEST 3					
Property	WF 1	WF2	WF3	FD5	FD6	FD7	WF1	WF2	WF3	FD5	FD6	FD7	WF 1	WF2	WF3	FD5	FD6	FD7
% Sout	?	?	?	?	>	?	?(>)	?(>)	?(>)	?(>)	>	?(>)	>	?(>)	>	>	>	?(>)
%Confidence							66.4	89.7	77.4	82.3	91.7	54.2	99.2	87.9	99.5	96.7	99.7	84.1
CD STFI Index	?	?	?	?	?	?	?(>)	>	?(>)	?(>)	?(>)	?(<)	?(>)	>	?(>)	?(>)	?(>)	?(<)
%Confidence							44.5	93.0	73.3	32.0	81.5	6.3	56.7	93.6	80.3	74.7	88.1	8.3
MD STFI Index	?	?	?	?	?	?	?(>)	?(>)	?(>)	?(<)	?(>)	?(<)	?(>)	?(>)	?(>)	<	>	?(<)
%Confidence							31.3	75.9	42.6	77.5	87.9	27.0	33.4	84.5	68.6	98.1	92.9	29.6
Density	?	?	>	>	?	?	?(>)	?(>)	>	>	?(>)	?(<)	>	>	>	>	>	?(<)
%Confidence							82.4	69.7	100.0	98.6	86.3	28.6	99.5	90.8	100.0	100.0	98.2	58.2

Table 53. Double Felted Pressing Comparisons of Case A2 to Case D2

	TEST 0						TEST 1						TEST 3					
Property	WF 1	WF2	WF3	FD5	FD6	FD7	WF1	WF2	WF3	FD5	FD6	FD7	WF 1	WF2	WF3	FD5	FD6	FD7
% Sout	>	?	?	?	>	>	>	>	>	?(>)	>	>	>	>	>	>	>	>
%Confidence							99.2	97.3	95.8	80.9	99.8	100.0	100.0	96.9	100.0	96.4	100.0	100.0
CD STFI Index	?	?	?	?	?	?	?(>)	?(>)	?(>)	id	?(>)	id	?(>)	>	?(>)	?(>)	>	?(>)
%Confidence							62.6	64.1	64.8	id	72.1	id	57.0	91.0	71.9	25.6	96.9	82.4
MD STFI Index	?	?	?	?	?	?	?(>)	?(>)	?(<)	id	?(>)	id	?(>)	?(>)	?(<)	?(<)	>	>
%Confidence							9.3	0.5	31.8	id	85.6	id	10.1	0.8	73.0	76.7	93.2	98.2
Density	>	?	?	?	?	<	>	?(<)	<	?(<)	?(>)	id	>	?(<)	<	?(<)	>	<
%Confidence							99.8	37.5	93.7	41.8	41.0	id	99.9	60.9	98.4	89.7	94.1	100.0

Table 54. Double Felted Pressing Comparisons of Case C3 to Case D3

	TEST 0						TEST 1						TEST 3					
Property	WF 1	WF2	WF3	FD5	FD6	FD7	WF1	WF2	WF3	FD5	FD6	FD7	WF 1	WF2	WF3	FD5	FD6	FD7
% Sout	?	?	?	?	>	?	?(>)	?(>)	?(>)	?(>)	>	>	>	?(>)	>	>	>	>
%Confidence							77.9	83.5	79.5	57.7	99.9	98.9	97.0	84.5	93.1	90.4	100.0	99.8
CD STFI Index	?	?	?	?	?	?	?(>)	?(<)	?(>)	?(<)	>	?(>)	?(>)	?(<)	?(>)	?(<)	>	?(>)
%Confidence							39.0	1.7	65.7	70.7	96.3	27.0	66.5	3.3	89.2	77.5	97.4	33.1
MD STFI Index	?	?	?	?	?	?	?(<)	?(<)	?(>)	?(<)	?(<)	?(<)	?(<)	<	?(>)	?(<)	?(<)	?(<)
%Confidence							43.8	77.2	54.8	51.0	35.9	59.2	80.7	96.6	57.5	70.2	36.4	81.2
Density	?	?	?	?	>	?	?(>)	?(>)	?(>)	?(<)	>	?(<)	>	?(>)	>	?(<)	>	?(<)
%Confidence							73.8	4.8	44.0	32.9	99.9	53.8	95.9	8.6	92.0	69.3	100.0	89.7

Table 55. Double Felted Pressing Comparisons of Case A4 to Case D4

	TEST 0						TEST 1						TEST 3					
Property	WF 1	WF2	WF3	FD5	FD6	FD7	WF1	WF2	WF3	FD5	FD6	FD7	WF 1	WF2	WF3	FD5	FD6	FD7
% Sout	>	?	?	>	?	>	>	?(>)	?(>)	?(>)	?(>)	>	>	>	>	>	>	>
%Confidence							94.5	79.9	81.6	89.1	75.9	91.2	99.0	98.4	98.9	97.9	90.4	99.8
CD STFI Index	?	?	?	?	?	?	?(>)	?(>)	?(>)	?(>)	?(>)	?(>)	?(>)	?(>)	>	?(>)	?(>)	>
%Confidence							33.8	23.0	88.5	56.5	68.6	61.5	59.6	41.2	98.5	74.3	84.2	90.7
MD STFI Index	?	?	?	?	?	?	?(>)	?(<)	?(>)	?(>)	?(>)	?(<)	?(>)	?(<)	>	?(>)	?(>)	?(<)
%Confidence							33.1	11.2	84.0	20.0	60.3	9.9	45.3	21.0	94.6	31.4	76.4	20.4
Density	>	>	>	?	>	>	>	>	>	?(>)	>	>	>	>	>	?(>)	>	>
%Confidence							96.4	90.5	90.4	62.3	95.2	90.2	100.0	100.0	99.9	84.9	99.8	100.0

Table 56. Double Felted Pressing Comparisons of Case A5 to Case D5

	TEST 0						TEST 1						TEST 3					
Property	WF 1	WF2	WF3	FD5	FD6	FD7	WF1	WF2	WF3	FD5	FD6	FD7	WF 1	WF2	WF3	FD5	FD6	FD7
% Sout	>	?	>	?	>	>	>	?(>)	?(>)	?(>)	?(>)	>	>	>	>	id	>	>
%Confidence							98.0	78.5	85.2	53.3	84.4	91.3	100.0	99.0	99.6	id	99.4	97.9
CD STFI Index	?	?	?	?	?	?	?(>)	?(<)	?(<)	?(<)	?(>)	?(>)	?(>)	?(<)	?(<)	id	>	>
%Confidence							25.6	14.8	20.5	87.2	64.7	75.0	84.5	27.6	32.7	id	94.5	93.4
MD STFI Index	?	?	?	?	?	?	?(>)	?(<)	?(>)	<	?(>)	?(>)	?(>)	?(<)	?(>)	id	>	?(>)
%Confidence							34.1	50.6	33.5	92.6	69.5	62.3	86.2	86.0	73.5	id	96.7	83.8
Density	>	?	?	?	?	<	?(>)	?(>)	?(>)	?(>)	?(>)	<	>	?(>)	?(>)	id	?(>)	<
%Confidence							51.4	39.7	9.2	3.1	36.5	98.5	100.0	89.8	33.2	id	77.9	100.0

Table 57. Double Felted Pressing Comparisons of Case A6 to Case D6

	TEST 0						TEST 1						TEST 3					
Property	WF 1	WF2	WF3	FD5	FD6	FD7	WF1	WF2	WF3	FD5	FD6	FD7	WF 1	WF2	WF3	FD5	FD6	FD7
% Sout	>	>	>	?	>	?	>	>	>	?(>)	>	id	>	>	>	>	>	id
%Confidence							99.4	99.9	99.0	83.9	99.4	id	99.9	99.8	100.0	98.0	98.5	id
CD STFI Index	?	?	?	?	?	?	?(>)	?(<)	?(<)	id	?(>)	id	?(>)	?(<)	?(<)	?(<)	?(>)	id
%Confidence							36.8	6.6	64.6	id	22.6	id	53.8	21.2	66.3	25.2	44.4	id
MD STFI Index	?	?	?	?	?	?	?(>)	?(<)	?(>)	id	>	id	?(>)	<	?(>)	?(<)	?(>)	id
%Confidence							63.3	70.3	50.0	id	90.0	id	83.5	96.9	61.C	11.8	89.2	id
Density	?	>	>	?	>	>	<	>	>	?(>)	>	>	<	>	>	?(>)	>	>
%Confidence							95.5	99.6	97.3	8.2	100.0	99.1	99.8	100.0	100.0	24.6	100.0	100.0

Table 58. Single Felted Pressing Comparisons of Case C1 to Case C1S

	TEST 0						TEST 1						TEST 3					
Property	WF 1	WF2	WF3	FD5	FD6	FD7	WF1	WF2	WF3	FD5	FD6	FD7	WF 1	WF2	WF3	FD5	FD6	FD7
% Sout	?	?	?	?	?	?	?(>)	?(>)	?(>)	?(>)	>	>	?(>)	?(>)	?(>)	id	>	>
%Confidence							82.3	69.2	43.6	79.1	93.7	93.0	81.2	84.6	45.7	id	91.7	99.1
CD STFI Index	?	?	?	?	?	?	?(<)	?(>)	?(<)	?(<)	?(>)	?(<)	?(<)	?(>)	?(<)	id	>	?(<)
%Confidence							24.4	6.5	28.3	28.5	89.2	78.1	24.6	22.6	28.8	id	90.7	82.1
MD STFI Index	?	?	?	?	?	?	?(>)	?(<)	?(<)	id	?(>)	?(<)	?(>)	?(<)	?(<)	id	?(>)	<
%Confidence							25.0	3.8	2.5	id	69.3	88.6	26.2	13.1	2.4	id	74.8	93.9
Density	?	?	?	?	?	?	>	?(>)	?(>)	>	>	?(<)	>	?(>)	?(>)	>	>	?(<)
%Confidence							90.6	40.3	19.5	97.2	92.8	19.6	96.9	79.8	23.9	99.3	94.5	25.2

Table 59. Single Felted Pressing Comparisons of Case C2 to Case C2S

	TEST 0						TEST 1						TEST 3					
Property	WF 1	WF2	WF3	FD5	FD6	FD7	WF1	WF2	WF3	FD5	FD6	FD7	WF 1	WF2	WF3	FD5	FD6	FD7
% Sout	?	?	?	?	?	?	?(>)	?(>)	?(>)	?(>)	?(>)	?(<)	>	?(>)	?(>)	>	?(>)	<
%Confidence							27.3	58.8	50.6	77.2	68.7	88.1	92.8	75.2	85.1	96.4	65.5	97.6
CD STFI Index	?	?	?	?	<	?	?(<)	?(<)	?(<)	?(<)	?(<)	?(>)	?(<)	?(<)	?(<)	?(<)	<	?(>)
%Confidence							28.1	1.9	80.8	59.2	84.0	75.7	89.1	2.1	87.4	81.6	97.7	78.0
MD STFI Index	?	?	?	?	?	?	?(<)	?(>)	?(<)	?(<)	?(>)	?(<)	?(<)	?(>)	?(<)	?(<)	?(>)	?(<)
%Confidence							11.7	37.8	55.0	41.7	35.1	81.7	52.6	44.6	68.4	58.0	60.9	83.8
Density	?	<	?	?	<	?	?(>)	<	<	?(>)	<	<	>	<	<	?(>)	<	<
%Confidence							48.8	97.0	93.8	30.3	99.9	97.1	92.7	100.0	97.2	46.8	99.9	99.9

Table 60. Single Felted Pressing Comparisons of Case C3 to Case C3S

	TEST 0						TEST 1						TEST 3					
Property	WF 1	WF2	WF3	FD5	FD6	FD7	WF1	WF2	WF3	FD5	FD6	FD7	WF 1	WF2	WF3	FD5	FD6	FD7
% Sout	?	?	?	?	>	>	?(>)	?(>)	?(>)	?(>)	>	>	?(>)	?(>)	?(>)	>	>	>
%Confidence							22.7	73.9	41.2	71.2	99.5	99.7	24.1	84.1	83.0	91.2	100.0	100.0
CD STFI Index	?	?	?	?	>	?	?(<)	?(<)	?(>)	?(>)	>	?(>)	?(<)	?(<)	>	?(>)	>	?(>)
%Confidence							34.0	29.4	65.1	28.1	96.8	4.6	63.7	42.4	94.8	47.7	99.8	7.9
MD STFI Index	?	?	?	?	?	?	?(<)	?(<)	?(>)	?(<)	<	?(<)	?(<)	<	>	?(<)	<	<
%Confidence							29.6	84.7	68.4	25.2	90.2	79.2	39.8	96.5	96.5	39.0	94.7	96.9
Density	?	<	>	?	>	?	?(<)	<	?(>)	?(>)	>	?(<)	?(<)	<	>	>	>	<
%Confidence							53.7	96.4	74.4	51.9	97.3	72.1	69.7	99.9	99.6	93.4	99.9	97.5

Table 61. Single Felted Pressing Comparisons of Case A1 to Case A1S

	TEST 0						TEST 1						TEST 3					
Property	WF 1	WF2	WF3	FD5	FD6	FD7	WF1	WF2	WF3	FD5	FD6	FD7	WF 1	WF2	WF3	FD5	FD6	FD7
% Sout	>	id	id	id	id	id	>	id	id	id	id	id	>	id	id	id	id	id
%Confidence							97.8	id	id	id	id	id	99.8	id	id	id	id	id
CD STFI Index	?	id	id	id	id	id	?(>)	id	id	id	id	id	?(>)	id	id	id	id	id
%Confidence							88.3	id	id	id	id	id	80.0	id	id	id	id	id
MD STFI Index	?	id	id	id	id	id	?(>)	id	id	id	id	id	?(>)	id	id	id	id	id
%Confidence							89.4	id	id	id	id	id	80.2	id	id	id	id	id
Density	>	id	id	id	id	id	>	id	id	id	id	id	>	id	id	id	id	id
%Confidence							98.0	id	id	id	id	id	99.9	id	id	id	id	id

Table 62. Single Felted Pressing Comparisons of Case A4 to Case A4S

	TEST 0						TEST 1						TEST 3					
Property	WF 1	WF2	WF3	FD5	FD6	FD7	WF1	WF2	WF3	FD5	FD6	FD7	WF 1	WF2	WF3	FD5	FD6	FD7
% Sout	>	>	>	?	>	?	>	>	>	>	>	?(>)	>	>	>	>	>	>
%Confidence							95.4	93.8	91.3	93.5	98.5	89.3	99.7	99.9	99.7	98.8	99.8	98.6
CD STFI Index	?	>	?	?	?	>	?(>)	>	>	?(<)	>	>	>	>	>	?(<)	>	>
%Confidence							89.7	91.2	92.1	6.3	93.0	90.6	97.8	99.7	99.5	6.4	99.0	99.3
MD STFI Index	?	>	>	?	?	?	>	?(>)	>	?(>)	>	>	>	>	>	?(>)	>	>
%Confidence							90.5	88.2	91.1	60.4	92.7	90.4	99.6	99.6	99.6	56.3	98.9	98.6
Density	>	>	>	?	>	>	>	>	>	>	>	>	>	>	>	>	>	>
%Confidence							95.0	95.1	94.4	93.9	96.2	95.1	100.0	100.0	100.0	98.5	99.9	100.0

Table 63. Single Felted Pressing Comparisons of Case A5 to Case A5S

	TEST 0						TEST 1						TEST 3					
Property	WF 1	WF2	WF3	FD5	FD6	FD7	WF1	WF2	WF3	FD5	FD6	FD7	WF 1	WF2	WF3	FD5	FD6	FD7
% Sout	id	>	?	?	>	>	id	>	id	?(>)	>	>	id	>	id	id	>	>
%Confidence							id	93.9	id	83.6	91.8	97.3	id	99.9	id	id	99.9	99.3
CD STFI Index	id	?	?	?	>	>	id	?(>)	id	?(<)	>	>	id	>	id	id	>	>
%Confidence							id	86.8	id	28.2	92.0	92.5	id	98.3	id	id	99.7	98.2
MD STFI Index	id	?	?	?	?	>	id	?(>)	id	?(>)	>	>	id	>	id	id	>	>
%Confidence							id	89.9	id	74.5	91.7	92.6	id	98.0	id	id	99.6	98.3
Density	id	>	?	>	>	?	id	>	>	?(>)	>	>	id	>	>	id	>	>
%Confidence							id	95.6	95.7	87.7	93.5	93.3	id	100.0	99.5	id	100.0	99.4

Table 64. Control Comparisons of Case C1 to Case Con

	TEST 0						TEST 1						TEST 3					
Property	WF 1	WF2	WF3	FD5	FD6	FD7	WF1	WF2	WF3	FD5	FD6	FD7	WF 1	WF2	WF3	FD5	FD6	FD7
% Sout	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id
%Confidence							id	id	id	id	id	id	id	id	id	id	id	id
CD STFI Index	>	>	>	?	>	>	>	>	>	?(>)	>	>	>	>	>	id	>	>
%Confidence							99.7	96.1	98.9	76.6	99.7	100.0	99.9	100.0	100.0	id	100.0	100.0
MD STFI Index	>	>	>	?	>	>	>	>	>	id	>	>	>	>	>	id	>	>
%Confidence							99.5	92.8	100.0	id	99.9	99.8	100.0	100.0	99.9	id	99.9	100.0
Density	>	>	>	>	>	>	>	>	>	>	>	>	>	>	>	>	>	>
%Confidence							100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0

Table 65. Control Comparisons of Case C2 to Case Con

	TEST 0						TEST 1						TEST 3					
Property	WF 1	WF2	WF3	FD5	FD6	FD7	WF1	WF2	WF3	FD5	FD6	FD7	WF 1	WF2	WF3	FD5	FD6	FD7
% Sout	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id
%Confidence							id	id	id	id	id	id	id	id	id	id	id	id
CD STFI Index	>	>	>	?	>	>	>	>	>	?(>)	>	>	>	>	>	>	>	>
%Confidence							98.9	100.0	100.0	76.1	99.6	100.0	98.3	100.0	100.0	91.6	100.0	100.0
MD STFI Index	>	>	>	?	>	>	>	>	>	>	>	>	>	>	>	>	>	>
%Confidence							99.4	100.0	100.0	92.4	99.8	100.0	98.7	100.0	100.0	96.3	100.0	100.0
Density	>	>	>	>	>	>	>	>	>	>	>	>	>	>	>	>	>	>
%Confidence							99.9	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0

Table 66. Control Comparisons of Case C3 to Case Con

	TEST 0						TEST 1						TEST 3					
Property	WF 1	WF2	WF3	FD5	FD6	FD7	WF1	WF2	WF3	FD5	FD6	FD7	WF 1	WF2	WF3	FD5	FD6	FD7
% Sout	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id
%Confidence							id	id	id	id	id	id	id	id	id	id	id	id
CD STFI Index	>	>	>	?	>	>	>	>	>	?(>)	>	>	>	>	>	?(>)	>	>
%Confidence							99.0	98.6	99.0	80.7	99.9	100.0	99.9	100.0	100.0	81.8	100.0	100.0
MD STFI Index	?	>	>	?	>	>	?(>)	>	>	>	>	>	>	>	>	>	>	>
%Confidence							85.5	99.9	99.4	96.7	99.9	99.9	98.4	100.0	100.0	97.8	99.6	100.0
Density	>	>	>	>	>	>	>	>	>	>	>	>	>	>	>	>	>	>
%Confidence							100.0	100.0	99.7	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0

Table 67. Control Comparisons of Case A1 to Case Con

	TEST 0						TEST 1						TEST 3					
Property	WF 1	WF2	WF3	FD5	FD6	FD7	WF1	WF2	WF3	FD5	FD6	FD7	WF 1	WF2	WF3	FD5	FD6	FD7
% Sout	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id
%Confidence							id	id	id	id	id	id	id	id	id	id	id	id
CD STFI Index	>	>	>	?	>	?	>	>	>	?(>)	>	id	>	>	>	?(>)	>	>
%Confidence							99.5	98.3	100.0	26.2	92.2	id	100.0	100.0	100.0	76.6	99.9	93.1
MD STFI Index	>	>	>	?	?	>	>	>	>	?(>)	>	>	>	>	>	?(>)	>	>
%Confidence							98.6	99.9	100.0	27.1	92.8	99.9	99.9	100.0	99.9	78.5	100.0	100.0
Density	>	>	>	>	>	>	>	>	>	>	>	>	>	>	>	>	>	>
%Confidence							100.0	100.0	100.0	98.6	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0

Table 68. Control Comparisons of Case A2 to Case Con

	TEST 0						TEST 1						TEST 3					
Property	WF 1	WF2	WF3	FD5	FD6	FD7	WF1	WF2	WF3	FD5	FD6	FD7	WF 1	WF2	WF3	FD5	FD6	FD7
% Sout	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id
%Confidence							id	id	id	id	id	id	id	id	id	id	id	id
CD STFI Index	>	>	>	?	?	>	>	>	>	id	>	id	>	>	>	?(>)	>	>
%Confidence							99.9	100.0	100.0	id	93.3	id	100.0	100.0	99.9	80.1	99.9	99.9
MD STFI Index	>	>	>	?	>	>	>	>	>	id	>	id	>	>	>	>	>	>
%Confidence							98.8	100.0	100.0	id	99.4	id	100.0	100.0	99.6	97.6	100.0	100.0
Density	>	>	>	>	>	>	>	>	>	>	>	id	>	>	>	>	>	>
%Confidence							100.0	100.0	100.0	97.6	99.9	id	100.0	100.0	100.0	100.0	100.0	100.0

Table 69. Control Comparisons of Case A4 to Case Con

	TEST 0						TEST 1						TEST 3					
Property	WF 1	WF2	WF3	FD5	FD6	FD7	WF1	WF2	WF3	FD5	FD6	FD7	WF 1	WF2	WF3	FD5	FD6	FD7
% Sout	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id
%Confidence							id	id	id	id	id	id	id	id	id	id	id	id
CD STFI Index	>	>	>	?	>	>	>	>	>	?(>)	>	>	>	>	>	?(>)	>	>
%Confidence							99.6	98.7	98.0	54.6	96.5	97.8	100.0	100.0	100.0	57.6	99.7	100.0
MD STFI Index	>	>	>	?	>	>	>	>	>	?(>)	>	>	>	>	>	?(>)	>	>
%Confidence							98.5	99.7	99.4	69.7	97.8	92.8	99.9	100.0	100.0	86.2	99.8	99.8
Density	>	>	>	>	>	>	>	>	>	>	>	>	>	>	>	>	>	>
%Confidence							100.0	99.7	99.7	99.9	100.0	99.7	100.0	100.0	100.0	100.0	100.0	100.0

Table 70. Control Comparisons of Case A5 to Case Con

	TEST 0						TEST 1						TEST 3					
Property	WF 1	WF2	WF3	FD5	FD6	FD7	WF1	WF2	WF3	FD5	FD6	FD7	WF 1	WF2	WF3	FD5	FD6	FD7
% Sout	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id
%Confidence							id	id	id	id	id	id	id	id	id	id	id	id
CD STFI Index	>	>	>	?	>	>	>	>	>	?(<)	>	>	>	>	>	id	>	>
%Confidence							99.2	99.0	99.0	57.7	94.5	97.9	100.0	100.0	100.0	id	99.9	99.9
MD STFI Index	>	>	>	?	>	>	>	>	>	?(>)	>	>	>	>	>	id	>	>
%Confidence							97.2	99.2	94.8	21.1	93.9	93.7	100.0	100.0	99.9	id	99.9	98.6
Density	>	>	>	>	>	>	>	>	>	>	>	>	>	>	>	id	>	>
%Confidence							100.0	100.0	99.7	100.0	99.9	100.0	100.0	100.0	100.0	id	100.0	100.0

Table 71. Control Comparisons of Case A6 to Case Con

	TEST 0						TEST 1						TEST 3					
Property	WF 1	WF2	WF3	FD5	FD6	FD7	WF1	WF2	WF3	FD5	FD6	FD7	WF 1	WF2	WF3	FD5	FD6	FD7
% Sout	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id
%Confidence							id	id	id	id	id	id	id	id	id	id	id	id
CD STFI Index	>	>	>	?	?	>	>	>	>	id	>	>	>	>	>	?(>)	>	>
%Confidence							99.9	93.7	100.0	id	95.9	94.8	100.0	99.9	100.0	69.7	99.8	99.9
MD STFI Index	>	?	>	?	>	>	>	>	>	id	>	>	>	>	>	?(>)	>	>
%Confidence							99.6	96.4	99.8	id	100.0	99.4	100.0	99.9	99.9	80.9	100.0	100.0
Density	>	>	>	>	>	>	>	>	>	>	>	>	>	>	>	>	>	>
%Confidence							100.0	100.0	100.0	98.9	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0

Table 72. Comparisons of Furnish WF2 to Furnish WF1

	TEST 0						TEST 1						TEST 3					
Property	D1	D2	D3	D4	D5	D6	D1	D2	D3	D4	D5	D6	D1	D2	D3	D4	D5	D6
% Sout	?	?	?	?	<	?	<	<	?(<)	?(<)	<	?(<)	<	<	?(<)	?(<)	<	?(<)
%Confidence							96.4	92.7	72.7	89.6	99.7	50.3	96.4	92.7	72.7	89.6	99.7	50.3
CD STFI Index	?	?	>	?	?	?	>	?(>)	>	?(>)	?(>)	>	>	?(>)	>	?(>)	?(>)	>
%Confidence							95.1	77.3	99.4	84.8	72.0	98.3	95.1	77.3	99.4	84.8	72.0	98.3
MD STFI Index	?	?	?	?	?	?	>	?(>)	>	?(>)	>	>	>	?(>)	>	?(>)	>	>
%Confidence							98.4	53.4	98.3	70.5	90.2	98.4	98.4	53.4	98.3	70.5	90.2	98.4
Density	?	>	?	?	?	<	>	>	>	?(>)	?(<)	<	>	>	>	?(>)	?(<)	<
%Confidence							99.3	99.9	99.0	63.8	71.4	100.0	99.3	99.9	99.0	63.8	71.4	100.0

	TEST 0						TEST 1						TEST 3					
Property	Con	C1	C2	C3	A1	A2	Con	C1	C2	C3	A1	A2	Con	C1	C2	C3	A1	A2
% Sout	id	?	?	?	<	<	id	?(<)	?(<)	?(<)	<	<	id	<	<	<	<	<
%Confidence							id	85.8	76.6	64.0	96.1	98.7	id	99.9	99.8	95.5	99.9	100.0
CD STFI Index	>	?	?	?	?	?	>	?(>)	?(>)	?(>)	?(<)	>	>	>	>	>	?(<)	>
%Confidence							100.0	86.3	70.6	83.7	1.6	97.3	100.0	99.9	98.7	99.2	4.2	99.9
MD STFI Index	>	?	?	?	?	?	>	?(>)	?(>)	?(>)	?(>)	?(>)	>	>	>	>	?(>)	>
%Confidence							99.8	39.7	57.4	60.6	7.4	70.9	99.8	91.3	97.6	90.4	17.4	96.9
Density	>	?	?	?	?	?	>	?(<)	?(<)	?(<)	?(<)	?(<)	>	?(<)	<	?(<)	?(<)	<
%Confidence							100.0	4.8	42.3	24.0	39.6	60.8	100.0	19.9	91.9	48.5	84.8	97.9

	TEST 0						TEST 1						TEST 3					
Property	A4	A5	A6	A5F	A4H	A5H	A4	A5	A6	A5F	A4H	A5H	A4	A5	A6	A5F	A4H	A5H
% Sout	?	?	<	<	?	?	?(<)	<	<	<	?(<)	id	<	<	<	<	<	<
%Confidence							83.6	94.0	94.8	98.0	7.7	id	99.9	98.9	100.0	100.0	98.1	98.3
CD STFI Index	?	?	?	?	?	?	?(>)	?(<)	?(>)	id	?(>)	id	?(>)	?(<)	?(>)	?(>)	?(>)	?(>)
%Confidence							40.7	10.4	34.5	id	2.7	id	82.7	66.0	82.3	65.0	87.1	61.1
MD STFI Index	?	?	?	?	?	?	?(>)	?(<)	?(<)	id	?(>)	id	?(>)	?(<)	?(<)	?(>)	?(>)	?(>)
%Confidence							25.7	18.1	3.6	id	1.3	id	60.9	87.0	9.2	4.2	51.4	24.8
Density	?	?	?	?	?	?	?(>)	?(<)	>	id	?(<)	id	>	?(<)	>	?(<)	?(<)	?(>)
%Confidence							38.5	26.7	93.8	id	0.0	id	90.3	73.7	100.0	85.0	18.4	6.3

Table 73. Comparisons of Furnish FD5 to Furnish WF1

	TEST 0						TEST 1						TEST 3					
Property	D1	D2	D3	D4	D5	D6	D1	D2	D3	D4	D5	D6	D1	D2	D3	D4	D5	D6
% Sout	?	?	?	?	?	?	<	<	<	?(<)	<	?(>)	<	<	<	?(<)	<	?(>)
%Confidence							98.3	98.6	97.5	19.4	99.1	63.0	98.3	98.6	97.5	19.4	99.1	63.0
CD STFI Index	?	?	?	<	<	?	?(<)	?(<)	?(<)	<	<	<	?(<)	?(<)	?(<)	<	<	<
%Confidence							32.5	77.5	83.9	99.8	100.0	96.2	32.5	77.5	83.9	99.8	100.0	96.2
MD STFI Index	?	?	?	?	?	?	<	?(<)	?(<)	<	<	?(<)	<	?(<)	?(<)	<	<	?(<)
%Confidence							92.7	25.7	87.0	91.7	99.5	76.0	92.7	25.7	87.0	91.7	99.5	76.0
Density	?	?	?	?	<	<	?(>)	<	?(>)	<	<	<	?(>)	<	?(>)	<	<	<
%Confidence							88.3	95.6	10.1	95.0	100.0	100.0	88.3	95.6	10.1	95.0	100.0	100.0

	TEST 0						TEST 1						TEST 3					
Property	Con	C1	C2	C3	A1	A2	Con	C1	C2	C3	A1	A2	Con	C1	C2	C3	A1	A2
% Sout	id	?	?	?	?	<	id	<	?(<)	?(<)	<	<	id	id	<	<	<	<
%Confidence							id	93.3	81.6	72.0	91.2	98.6	id	id	98.1	98.4	100.0	99.9
CD STFI Index	?	?	?	?	?	?	>	?(<)	?(<)	<	?(<)	id	>	id	<	<	<	<
%Confidence							95.4	88.1	85.4	91.0	62.7	id	95.4	id	99.7	99.5	97.5	97.7
MD STFI Index	?	?	?	?	?	?	?(>)	id	<	?(<)	?(<)	id	?(>)	id	<	?(<)	<	<
%Confidence							86.0	id	90.6	5.8	38.0	id	86.0	id	99.7	14.5	90.2	94.8
Density	>	?	?	?	<	<	>	?(<)	?(<)	?(<)	<	<	>	<	<	<	<	<
%Confidence							100.0	68.9	80.4	77.0	96.3	98.1	100.0	98.6	98.9	97.7	100.0	100.0

	TEST 0						TEST 1						TEST 3					
Property	A4	A5	A6	A5F	A4H	A5H	A4	A5	A6	A5F	A4H	A5H	A4	A5	A6	A5F	A4H	A5H
% Sout	<	<	<	?	id	id	<	<	<	<	id	id	<	<	<	id	id	id
%Confidence							90.3	99.8	96.2	96.2	id	id	99.9	100.0	99.9	id	id	id
CD STFI Index	<	<	?	id	id	id	<	<	id	id	id	id	<	<	?(<)	id	id	id
%Confidence							98.6	98.3	id	id	id	id	100.0	99.9	79.2	id	id	id
MD STFI Index	?	<	?	id	id	id	?(<)	<	id	id	id	id	<	<	?(<)	id	id	id
%Confidence							74.8	95.1	id	id	id	id	93.0	99.8	74.0	id	id	id
Density	<	<	?	id	id	id	<	?(<)	?(<)	id	id	id	<	<	<	id	id	id
%Confidence							97.9	88.8	84.8	id	id	id	100.0	99.8	99.8	id	id	id

Table 74. Comparisons of Furnish FD6 to Furnish WF1

	TEST 0						TEST 1						TEST 3					
Property	D1	D2	D3	D4	D5	D6	D1	D2	D3	D4	D5	D6	D1	D2	D3	D4	D5	D6
% Sout	?	?	?	?	?	?	?(>)	?(>)	>	?(>)	?(<)	?(>)	?(>)	?(>)	>	?(>)	?(<)	?(>)
%Confidence							65.1	30.9	95.8	73.3	30.8	23.6	65.1	30.9	95.8	73.3	30.8	23.6
CD STFI Index	?	?	?	?	<	<	?(<)	?(<)	<	<	<	<	?(<)	?(<)	<	<	<	<
%Confidence							31.2	83.2	90.8	97.0	100.0	99.9	31.2	83.2	90.8	97.0	100.0	99.9
MD STFI Index	<	?	?	?	<	?	<	?(<)	<	<	<	<	<	?(<)	<	<	<	<
%Confidence							99.6	73.9	98.2	97.8	100.0	99.5	99.6	73.9	98.2	97.8	100.0	99.5
Density	?	?	<	<	<	<	>	?(<)	<	<	<	<	>	?(<)	<	<	<	<
%Confidence							92.1	87.5	99.8	98.3	100.0	100.0	92.1	87.5	99.8	98.3	100.0	100.0

	TEST 0						TEST 1						TEST 3					
Property	Con	C1	C2	C3	A1	A2	Con	C1	C2	C3	A1	A2	Con	C1	C2	C3	A1	A2
% Sout	id	?	?	?	?	?	id	?(>)	?(>)	?(>)	?(<)	?(>)	id	?(>)	>	>	?(<)	?(>)
%Confidence							id	40.4	39.3	86.9	12.4	12.3	id	88.2	93.7	99.3	41.9	44.3
CD STFI Index	?	?	?	?	?	?	>	?(<)	?(<)	?(>)	?(<)	?(<)	>	?(<)	<	?(>)	<	?(<)
%Confidence							95.5	13.2	73.9	3.9	55.1	37.6	95.5	24.0	99.7	9.3	96.8	81.0
MD STFI Index	?	<	?	?	?	?	?(<)	<	<	?(<)	?(<)	?(<)	?(<)	<	<	?(<)	<	<
%Confidence							77.8	98.2	92.8	54.6	88.2	86.9	77.8	100.0	100.0	87.9	99.8	99.7
Density	>	?	?	?	?	<	>	?(<)	?(<)	?(>)	?(<)	?(<)	>	<	<	?(>)	<	<
%Confidence							100.0	74.8	80.5	27.0	76.3	75.4	100.0	99.4	99.5	51.6	99.6	99.9

	TEST 0						TEST 1						TEST 3					
Property	A4	A5	A6	A5F	A4H	A5H	A4	A5	A6	A5F	A4H	A5H	A4	A5	A6	A5F	A4H	A5H
% Sout	?	?	?	?	?	?	?(<)	?(>)	?(<)	?(>)	?(<)	?(>)	<	?(>)	?(<)	>	?(<)	?(>)
%Confidence							55.4	1.5	39.6	65.0	3.4	39.7	97.0	50.9	84.4	98.9	68.6	78.5
CD STFI Index	?	?	?	<	?	?	?(<)	?(<)	?(<)	<	?(<)	?(<)	?(<)	?(<)	<	<	?(<)	<
%Confidence							55.8	70.2	88.9	93.7	6.1	66.8	82.7	84.1	99.0	100.0	89.0	96.2
MD STFI Index	?	?	?	<	?	<	<	?(<)	<	<	?(<)	<	<	<	<	<	<	<
%Confidence							92.7	86.1	96.6	90.9	18.9	99.1	99.8	99.0	99.8	99.8	99.6	100.0
Density	?	?	?	?	?	?	?(<)	?(<)	>	?(>)	?(>)	id	<	<	>	?(>)	>	?(>)
%Confidence							61.0	65.7	94.3	30.1	0.0	id	95.1	95.6	100.0	75.8	96.5	74.4

Table 75. Comparisons of Furnish WF3 to Furnish WF1

	TEST 0						TEST 1						TEST 3					
Property	D1	D2	D3	D4	D5	D6	D1	D2	D3	D4	D5	D6	D1	D2	D3	D4	D5	D6
% Sout	?	?	?	?	?	?	?(<)	?(<)	?(>)	?(>)	?(<)	?(<)	?(<)	?(<)	?(>)	?(>)	?(<)	?(<)
%Confidence							42.8	89.2	66.7	8.0	52.6	28.0	42.8	89.2	66.7	8.0	52.6	28.0
CD STFI Index	>	?	?	?	?	?	>	?(>)	?(>)	<	?(<)	?(>)	>	?(>)	?(>)	<	?(<)	?(>)
%Confidence							99.0	18.5	88.4	96.7	84.4	31.1	99.0	18.5	88.4	96.7	84.4	31.1
MD STFI Index	?	?	?	?	?	?	?(<)	?(<)	?(<)	?(<)	<	?(<)	?(<)	?(<)	?(<)	?(<)	<	?(<)
%Confidence							59.6	42.3	77.0	89.8	97.9	79.2	59.6	42.3	77.0	89.8	97.9	79.2
Density	?	?	>	?	?	<	>	?(>)	>	?(>)	>	<	>	?(>)	>	?(>)	>	<
%Confidence							98.6	88.1	99.3	82.7	96.0	100.0	98.6	88.1	99.3	82.7	96.0	100.0

	TEST 0						TEST 1						TEST 3					
Property	Con	C1	C2	C3	A1	A2	Con	C1	C2	C3	A1	A2	Con	C1	C2	C3	A1	A2
% Sout	id	?	?	?	?	?	id	?(<)	?(<)	?(>)	?(<)	?(<)	id	<	<	?(>)	<	<
%Confidence							id	52.8	36.0	13.2	77.1	74.1	id	93.5	98.0	39.2	99.1	99.7
CD STFI Index	?	?	?	?	?	?	>	?(>)	?(<)	?(>)	?(<)	?(<)	>	>	?(<)	>	<	?(<)
%Confidence							97.6	75.9	7.8	61.3	59.3	34.4	97.6	93.3	45.1	92.8	90.5	73.8
MD STFI Index	?	?	?	?	?	?	?(<)	?(<)	?(<)	?(>)	?(<)	?(<)	?(<)	<	<	?(>)	<	<
%Confidence							89.7	87.9	75.2	16.3	84.7	76.9	89.7	99.2	99.9	39.3	98.7	98.3
Density	>	?	?	?	<	<	>	?(<)	?(<)	?(>)	?(<)	<	>	?(<)	?(<)	?(>)	<	<
%Confidence							100.0	9.3	40.5	37.8	82.6	99.9	100.0	25.9	89.0	85.5	99.8	100.0

	TEST 0						TEST 1						TEST 3					
Property	A4	A5	A6	A5F	A4H	A5H	A4	A5	A6	A5F	A4H	A5H	A4	A5	A6	A5F	A4H	A5H
% Sout	?	?	?	<	?	?	?(<)	?(<)	?(<)	id	?(<)	?(<)	?(<)	?(<)	<	<	<	<
%Confidence							32.9	54.6	80.8	id	13.0	84.0	88.4	66.7	99.4	97.5	97.9	98.4
CD STFI Index	?	?	?	?	?	?	?(<)	?(<)	?(<)	id	id	id	?(<)	<	?(<)	?(<)	?(<)	?(<)
%Confidence							3.0	63.0	60.6	id	id	id	8.2	91.8	88.9	81.8	82.2	80.4
MD STFI Index	?	?	?	?	?	<	?(<)	?(<)	?(<)	id	id	id	<	?(<)	<	<	<	<
%Confidence							61.2	54.9	79.4	id	id	id	95.1	82.4	98.2	90.4	97.5	99.9
Density	?	?	?	?	?	<	?(>)	?(<)	?(>)	id	?(>)	id	>	?(<)	>	?(>)	?(>)	<
%Confidence							51.1	16.7	87.3	id	0.0	id	96.0	36.1	100.0	40.5	23.1	100.0

Table 76. Comparisons of Furnish FD5 to Furnish WF3

	TEST 0						TEST 1						TEST 3					
Property	D1	D2	D3	D4	D5	D6	D1	D2	D3	D4	D5	D6	D1	D2	D3	D4	D5	D6
% Sout	?	<	?	?	?	?	<	<	<	?(<)	<	>	<	<	<	?(<)	<	>
%Confidence							97.5	98.0	97.2	40.7	98.0	92.3	97.5	98.0	97.2	40.7	98.0	92.3
CD STFI Index	?	<	?	<	<	?	<	<	<	<	<	<	<	<	<	<	<	<
%Confidence							91.8	98.0	97.8	97.5	99.8	96.9	91.8	98.0	97.8	97.5	99.8	96.9
MD STFI Index	?	?	?	?	?	?	?(<)	?(>)	?(>)	?(<)	?(<)	?(<)	?(<)	?(>)	?(>)	?(<)	?(<)	?(<)
%Confidence							59.1	85.0	58.6	24.8	86.8	28.8	59.1	85.0	58.6	24.8	86.8	28.8
Density	?	<	<	<	<	<	?(<)	<	<	<	<	<	?(<)	<	<	<	<	<
%Confidence							71.3	99.9	99.4	99.9	100.0	98.7	71.3	99.9	99.4	99.9	100.0	98.7

	TEST 0						TEST 1						TEST 3					
Property	Con	C1	C2	C3	A1	A2	Con	C1	C2	C3	A1	A2	Con	C1	C2	C3	A1	A2
% Sout	id	?	?	?	?	?	id	<	?(<)	?(<)	?(<)	<	id	id	<	<	<	<
%Confidence							id	92.8	78.5	82.9	73.8	91.6	id	id	97.9	99.4	98.9	99.2
CD STFI Index	?	?	?	<	?	?	?(>)	<	<	<	?(<)	id	?(>)	id	<	<	?(<)	<
%Confidence							84.6	97.2	95.0	99.2	56.3	id	84.6	id	99.7	100.0	89.3	97.4
MD STFI Index	?	?	?	?	?	?	>	id	?(<)	?(<)	?(<)	id	>	id	<	?(<)	?(<)	?(<)
%Confidence							96.1	id	73.4	46.3	11.5	id	96.1	id	96.3	86.5	45.4	9.2
Density	>	?	<	?	?	?	>	<	<	?(<)	?(<)	?(<)	>	<	<	<	<	<
%Confidence							100.0	95.5	100.0	73.9	88.6	66.0	100.0	99.7	100.0	99.6	100.0	99.1

	TEST 0						TEST 1						TEST 3					
Property	A4	A5	A6	A5F	A4H	A5H	A4	A5	A6	A5F	A4H	A5H	A4	A5	A6	A5F	A4H	A5H
% Sout	?	<	?	?	id	id	?(<)	<	?(<)	id	id	id	<	<	<	id	id	id
%Confidence							70.8	95.8	87.0	id	id	id	98.2	99.7	99.2	id	id	id
CD STFI Index	<	<	?	id	id	id	<	<	id	id	id	id	<	<	?(<)	id	id	id
%Confidence							97.8	99.8	id	id	id	id	100.0	100.0	76.2	id	id	id
MD STFI Index	?	?	?	id	id	id	?(<)	<	id	id	id	id	?(<)	<	?(<)	id	id	id
%Confidence							49.4	90.8	id	id	id	id	71.2	98.9	52.2	id	id	id
Density	<	<	<	id	id	id	<	?(<)	<	id	id	id	<	<	<	id	id	id
%Confidence							95.8	82.5	98.5	id	id	id	100.0	98.8	100.0	id	id	id

Table 77. Comparisons of Furnish FD7 to Furnish WF3

	TEST 0						TEST 1						TEST 3					
Property	D1	D2	D3	D4	D5	D6	D1	D2	D3	D4	D5	D6	D1	D2	D3	D4	D5	D6
% Sout	?	<	?	?	?	?	id	<	?(<)	?(<)	<	id	id	<	?(<)	?(<)	<	id
%Confidence							id	99.8	41.5	86.7	95.3	id	id	99.8	41.5	86.7	95.3	id
CD STFI Index	?	?	?	?	<	?	id	?(<)	<	?(<)	<	id	id	?(<)	<	?(<)	<	id
%Confidence							id	84.2	93.0	35.2	99.0	id	id	84.2	93.0	35.2	99.0	id
MD STFI Index	?	?	?	?	<	?	id	<	?(<)	?(>)	<	id	id	<	?(<)	?(>)	<	id
%Confidence							id	95.6	36.1	53.2	99.9	id	id	95.6	36.1	53.2	99.9	id
Density	?	?	?	<	<	?	?(<)	<	<	<	<	>	?(<)	<	<	<	<	>
%Confidence							73.4	98.3	96.8	100.0	100.0	94.7	73.4	98.3	96.8	100.0	100.0	94.7

	TEST 0						TEST 1						TEST 3					
Property	Con	C1	C2	C3	A1	A2	Con	C1	C2	C3	A1	A2	Con	C1	C2	C3	A1	A2
% Sout	id	?	?	?	?	?	id	?(>)	?(<)	?(>)	?(<)	?(>)	id	?(>)	<	>	<	?(>)
%Confidence							id	21.4	85.6	44.4	54.4	22.5	id	61.3	99.4	91.0	96.5	67.7
CD STFI Index	?	?	<	?	?	?	?(>)	<	<	<	id	id	?(>)	<	<	<	?(<)	?(<)
%Confidence							73.8	93.7	98.2	91.8	id	id	73.8	98.8	99.0	99.8	70.8	68.4
MD STFI Index	?	?	<	?	?	?	>	<	<	?(<)	?(<)	id	>	<	<	<	<	>
%Confidence							95.2	95.1	99.4	86.2	65.9	id	95.2	99.5	100.0	99.3	97.0	96.2
Density	>	?	?	?	?	?	>	?(<)	<	?(<)	?(>)	id	>	<	<	<	?(>)	<
%Confidence							100.0	66.4	97.0	74.8	30.9	id	100.0	90.1	99.8	99.8	66.5	99.9

	TEST 0						TEST 1						TEST 3					
Property	A4	A5	A6	A5F	A4H	A5H	A4	A5	A6	A5F	A4H	A5H	A4	A5	A6	A5F	A4H	A5H
% Sout	?	?	?	?	?	?	?(<)	?(<)	?(<)	id	?(<)	id	?(<)	?(<)	?(<)	<	?(<)	?(<)
%Confidence							32.0	55.7	23.8	id	21.2	id	85.8	85.8	63.5	91.4	49.9	2.5
CD STFI Index	?	?	?	?	?	?	?(<)	?(<)	?(<)	id	id	id	<	?(<)	<	<	<	<
%Confidence							61.5	32.8	58.9	id	id	id	95.3	45.0	92.8	98.4	96.6	93.8
MD STFI Index	?	?	?	?	?	<	?(<)	?(<)	?(<)	id	id	id	<	?(<)	<	<	<	<
%Confidence							59.3	39.7	73.6	id	id	id	94.7	82.7	97.5	91.9	93.6	99.8
Density	?	<	?	?	?	>	?(<)	<	?(>)	id	id	id	<	<	?(>)	?(>)	?(>)	>
%Confidence							63.7	93.1	3.8	id	id	id	99.1	99.7	12.0	77.9	69.0	100.0

The following figures show the same data for outgoing solids and STFI index presented in the previous tables. Figures 4 through 10 show outgoing solids, comparing double felted pressing (D_) and impulse drying with the IPST-C (C_) and Beloit-A (A_) press rolls.

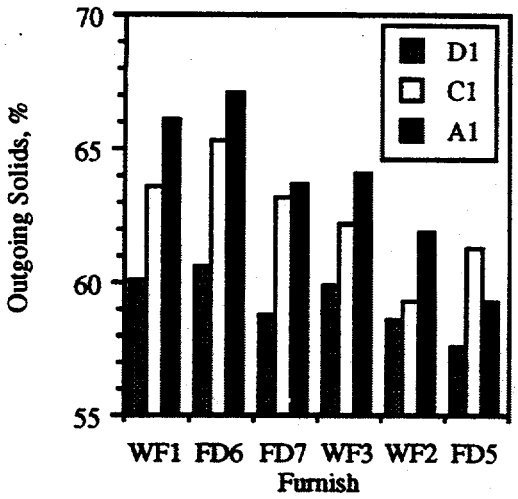

Figure 4. Outgoing Soliods For Case 1.

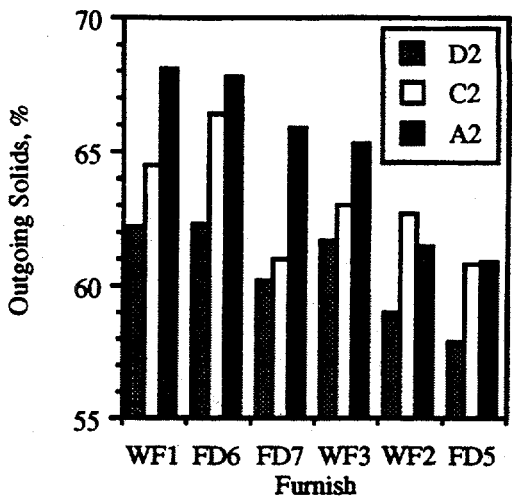

Figure 5. Outgoing Soliods For Case 2.

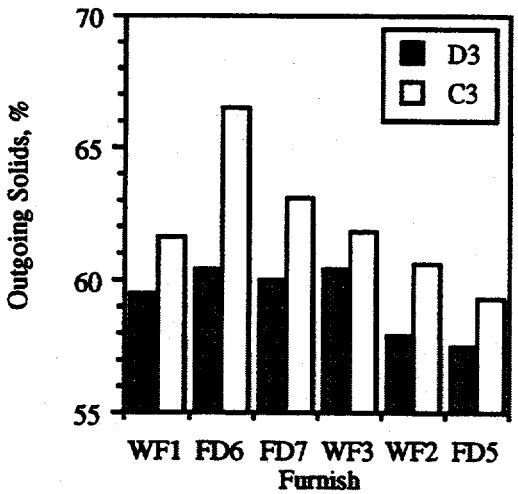

Figure 6. Outgoing Soliods For Case 3.

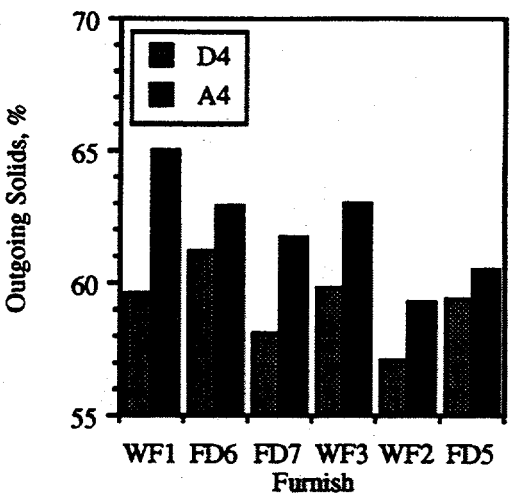

Figure 7. Outgoing Soliods For Case 4.

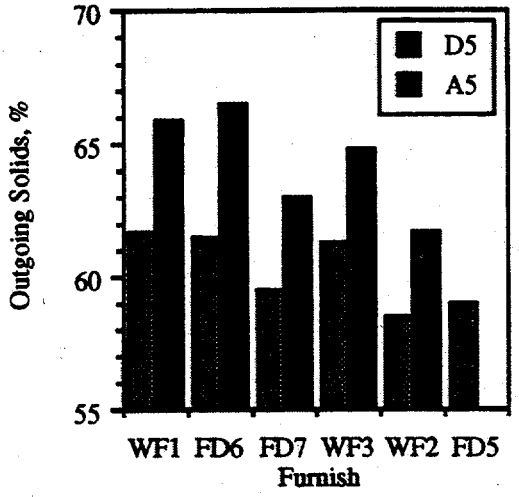

Figure 8. Outgoing Soliods For Case 5.

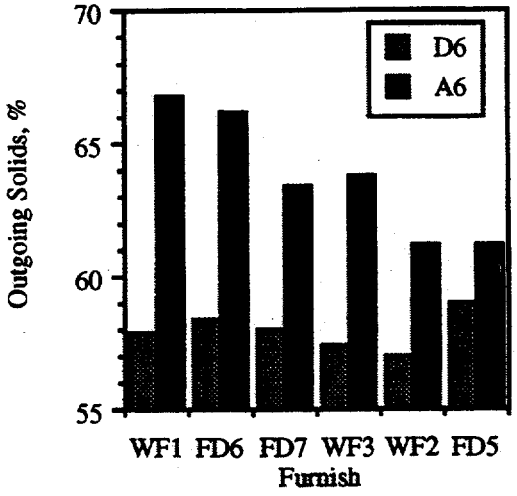

Figure 9. Outgoing Soliods For Case 6.

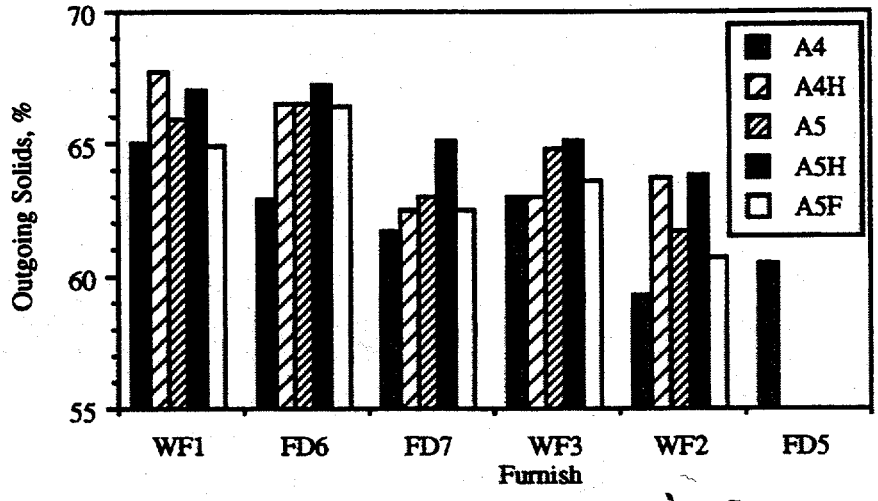

Figure 10. Outgoing Soliods For Remaining Cases.

Figures 11 through 16 show the geometric mean STFI indexes for cases 1 to 6, comparing double felted pressing (D_) and impulse drying with the IPST-C (C_) and Beloit-A (A_) press rolls.

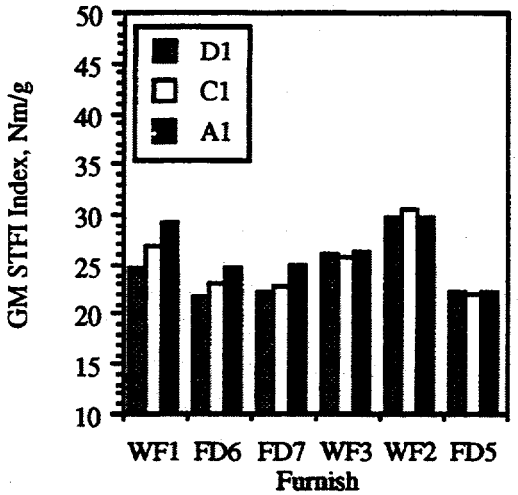

Figure 11. GM STFI Index For Case 1.

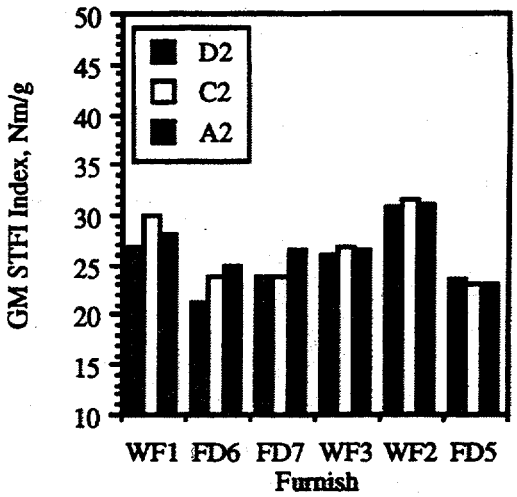

Figure 12. GM STFI Index For Case 2.

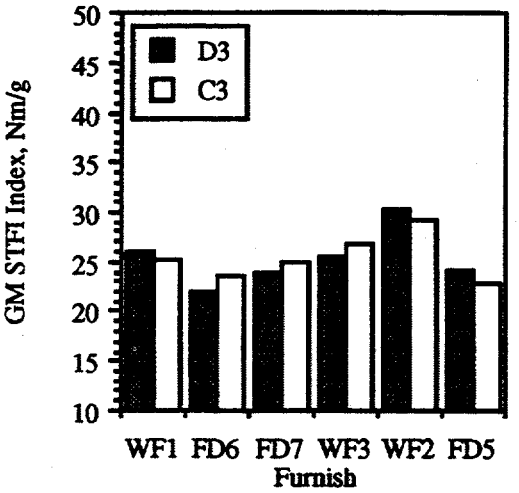

Figure 13. GM STFI Index For Case 3.

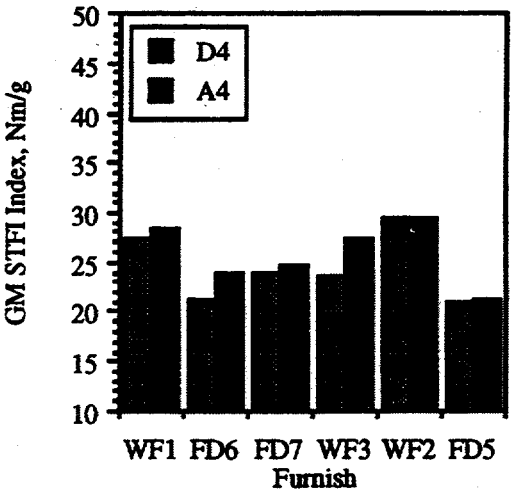

Figure 14. GM STFI Index For Case 4.

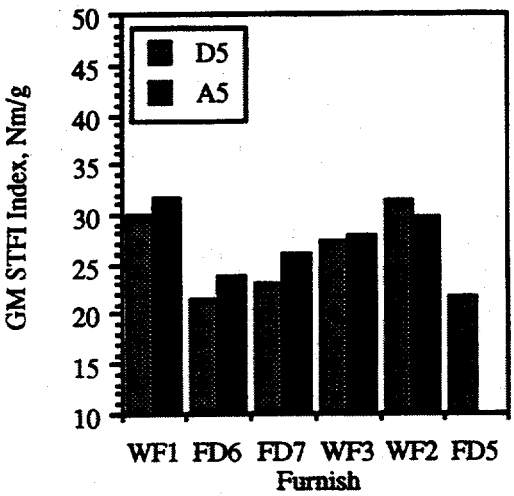

Figure 15. GM STFI Index For Case 5.

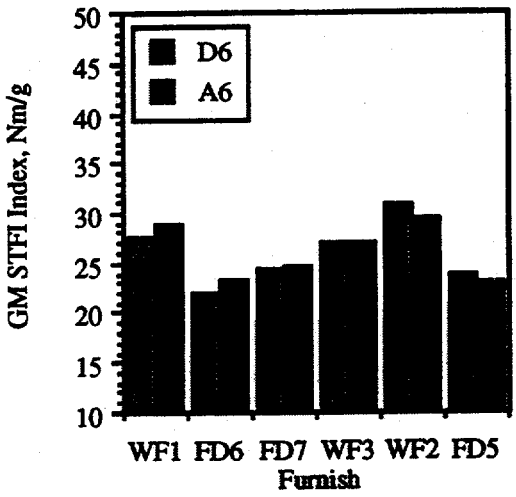

Figure 16. GM STFI Index For Case 6.

CONCLUSIONS

Experiments have been completed on the Beloit sheet-fed pilot impulse drying shoe press. The major conclusions to be drawn from these experiments may be summarized as;

Sheet Sticking: The Beloit "A" and IPST modified ceramic rolls were operated without sheet sticking at temperatures above 150°C with de ionized felt wash water. The Beloit A roll also did not stick when normal "hard" felt water was used. Hence, it is concluded, that previously observed high temperature sheet sticking was due to excessive press roll surface roughness.

Press Roll Surface Strength: The IPST modified ceramic roll coating was susceptible to chipping under shear, while the Beloit A roll did not chip.

Critical Impulse Drying Temperature : As in previous laboratory-scale experiments (2), critical impulse drying temperature was found to depend on the hydrodynamic specific surface of the heated layer of the sheet. As expected, critical impulse drying temperature was higher for the "low thermal mass" IPST modified ceramic press roll than for the "higher thermal mass" Beloit "A" press roll. Interestingly, it may also be concluded that the choice of felt can influence the critical temperature.

Press Dryness : It may be concluded that, for a given set of pressing conditions, press dryness tends to decrease when the hydrodynamic specific surface of the sheet is increased. In addition, it may be concluded that press dryness resulting from impulse drying was generally higher than that achieved by double-felted pressing. Differences in dryness ranged from 8 percentage points for sheets having low heated ply hydrodynamic specific surface to 3 percentage points for less permeable sheets . The Beloit "A" roll yielded higher press dryness than the IPST modified ceramic roll even though it was generally operated at lower temperature. While increasing the press load from 6000 pli to 8500 pli increased press dryness, the improvement was observed to be relatively small.

STFI Compression Strength: The Geometric mean STFI compression strength of impulse dried sheets were consistently higher than that obtained by double-felted pressing. The difference in strength tended to be more significant for the more permeable sheet structures. For two-ply sheets, the STFI compression strength resulting from impulse drying was as much as 17 percent higher than that produced by double-felted pressing. No substantial strength difference was observed comparing sheets impulse dried with the Beloit "A" roll to those dried using the IPST modified ceramic coated press roll.

Felt Water Chemistry For an unexplained reason, using hard felt wash water tended to increased outgoing solids by up to about 3 percentage points. STFI Index, however was not effected by water chemistry.

Speed Effects: Increasing machine speed results in decreasing the nip residence time from about 42 ms to about 32 ms. Decreasing residence time had the expected result of decreasing water removal and STFI compression strength for all furnishes.

Gurly Porosity : For all furnishes, the impulse dried sheets were less porous than double-felted pressed sheets, which in turn were less porous than the control sheets that were pressed to 52% solids .

Ink Penetration Test : The rate of change of the contact angle for black flexographic ink drops on the felt side of the samples were measured. Impulse dried and double-felted samples were generally independent of furnish and similar to commercial samples.

Sheet Surface Roughness: The roughness of the wire side of sheets was measured by Sheffield and Bendson roughness tests. It was concluded that while the method of pressing and the extent of refining control surface smoothness, the method of pressing is the dominant variable. In general, impulse dried samples were smoother than single-felted pressed samples, which were smother than double-felted pressed samples.

ZD Tensile: The zd tensile strength is a measure of ply-bond strength. Through these measurements it was concluded that impulse drying can be used to increase ply-bond strength.

Burst Index : Impulse drying tended to increase burst strength as compared to double-felted pressing.

Cracking Angle: Cracking angle was found to be dependent on the level of refining of the fibers on the wire side of the sheet and the method of pressing. Refining was found to be the dominant effect, in that excessive refining leads to a low cracking angle. Impulse dried samples tended to have slightly lower cracking angles than double or single-felted pressed sheets. As impulse drying performs best when the heated ply (wire side) is not heavily refined, there should no problem in achieving acceptable cracking angle results in commercial practice.

RECOMMENDATIONS

Based on the research results to date, IPST is forming a joint venture with Union Camp Corporation and Beloit Corporation for the purpose of commercializing impulse drying technology. Four initiatives are planned:

1.) Optimization of roll coatings for performance and durability.

2.) Development of mechanical equipment culminating in continuous, high speed, pilot paper machine experiments.

3.) Development, construction, and demonstration on a wide-width, commercial paper machine producing linerboard.

4.) Extending the use of impulse drying to a wide range of paper grades.

The first initiative will be conducted at IPST in FY'94, and is being funded by a continuation of Contract No. FG02-85CE40738. The initiative consists of a number of interrelated tasks. These included; experiments to optimize the thermal and mechanical strength properties of the heated press roll surface, construction and use of a high speed test stand to monitor stresses and long term durability of optimized roll surface coatings, and theoretical work to predict stress and temperature within the prototype press rolls.

The second initiative will be jointly conducted by Beloit, Union Camp and IPST in FY'94 and FY'95. That initiative will consist of the engineering design, construction and experimentation associated with the evaluation of a continuous commercial speed impulse dryer. The dryer will be installed on Beloits' new #4 pilot paper machine. The focus of early experimentation will on verifying the mechanical and runnability aspects of the impulse dryer. Experiments to define the furnish variables specific to the eventual Union Camp commercial application will also be undertaken. In addition, paper produced on the pilot paper machine will be converted to corrugated board to allow final use testing and evaluation.

The third initiative will be conducted if the second initiative is successful. The work will be jointly conducted by Union Camp, Beloit and IPST in FY'96 through FY'99. In this initiative, a commercial width impulse dryer will be designed, constructed, and installed on a Union Camp commercial paper machine. Experiments will then be conducted to evaluate impulse drying technology. Once operational, the performance of the impulse dryer will be monitored over a period of two years.

The fourth initiative will be coordinated by the Beloit, Union Camp, IPST joint venture, while various aspects of the work may be sub-contracted to Beloit, IPST or such organizations as the Herty Foundation. This initiative can begin once the mechanical equipment has been perfected (FY'97 at the earliest). The purpose of the initiate will be to expand the application of impulse drying technology to a wide range of grades and furnishes.

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APPENDIX A

The following tables contain data that were used for physical testing and analysis.

Table A1. Control Samples that were Finish Dried without Pressing

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF1	59162.3		191.2	54.8				0.060	0.060	10.0	6.7	0.434	0.433	20.50	11.47
WF1	59162.4		204.1	53.9				0.061	0.057	9.8	8.8	0.425	0.427	20.64	11.60
WF2	59163.1		199.0	51.5				0.111	0.098	3.6	7.1	0.541	0.539	25.98	16.98
WF2	59163.2		210.1	51.9				0.119	0.123	7.6	6.5	0.561	0.561	29.19	17.84
WF2	59163.3		208.1	48.8				0.129	0.123	7.8	6.5	0.544	0.546	28.09	18.52
WF2	59163.4		209.9	51.1				0.128	0.127	6.3	8.7	0.548	0.550	26.73	18.10
WF3	59164.2		200.5	49.2				0.070	0.063	8.6	11.1	0.497	0.503	18.92	13.10
WF3	59164.3		213.3	50.2				0.055	0.059	10.9	13.6	0.472	0.497	17.02	12.66
WF3	59164.4		201.5	50.2				0.066	0.069	6.1	5.8	0.499	0.509	19.43	13.48
FD5	59165.1		193.3	49.8				0.122	0.115	4.1	3.5	0.626	0.620	26.44	13.90
FD5	59165.2		201.8	50.2				0.120	0.108	5.8	6.5	0.649	0.621	23.24	17.21
FD5	59165.3		189.2	49.5				0.107	0.098	2.8	4.1	0.592	0.587	19.46	17.17
FD5	59165.4		204.1	49.6				0.118	0.111	6.8	9.0	0.620	0.622	25.65	12.81
FD6	59166.1		206.5	53.0				0.069	0.061	4.3	8.2	0.503	0.495	17.97	13.72
FD6	59166.2		206.1	51.3				0.065	0.056	9.2	5.4	0.497	0.490	20.40	12.19
FD6	59166.3		199.2	51.8				0.069	0.065	7.2	4.6	0.517	0.510	21.00	12.17
FD6	59166.4		205.1	51.2				0.059	0.050	8.5	8.0	0.485	0.483	17.98	13.19
FD7	59167.1		196.3	50.5				0.073	0.067	2.7	6.0	0.565	0.555	20.86	12.88
FD7	59167.2		193.5	50.5				0.080	0.076	6.3	7.9	0.557	0.551	20.67	13.45
FD7	59167.3		197.0	51.4				0.076	0.072	6.6	6.9	0.550	0.534	20.87	13.58
FD7	59167.4		201.8	52.0				0.091	0.084	7.7	16.7	0.557	0.546	22.58	14.46

Table A2. Double Felted Pressing for Case D1 on the X2 Shoe Press
(Felt B, 0" pivot, and 6000 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m^2	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm^3		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF1	59104.1	49	201.0	52.0	59.1			0.147	0.142	12.9	6.3	0.771	0.753	32.01	19.14
WF1	59104.2	49	207.3	54.8	60.2			0.176	0.172	6.3	15.7	0.787	0.767	34.00	21.16
WF1	59104.3	49	214.9	53.5	60.3			0.119	0.125	21.0	26.4	0.741	0.733	31.49	19.24
WF1	59104.4	49	194.7	53.1	60.8			0.108	0.129	18.5	28.7	0.683	0.706	28.59	17.66
WF2	59105.2	49	206.8	52.9	59.3			0.262	0.257	5.0	7.8	0.836	0.840	38.57	25.90
WF2	59105.3	49	214.9	52.6	58.7			0.215	0.195	7.4	13.3	0.817	0.785	37.36	23.65
WF2	59105.4	49	203.8	52.5	58.0			0.209	0.191	18.7	8.4	0.780	0.761	35.06	21.77
WF3	59106.2	49	217.6	51.5	60.1			0.202	0.200	8.4	5.5	0.817	0.825	33.00	23.34
WF3	59106.3	49	216.6	51.5	59.9			0.158	0.175	13.9	11.4	0.755	0.790	28.67	22.44
WF3	59106.4	49	220.7	51.7	59.5			0.150	0.219	38.0	4.6	0.760	0.812	26.35	22.83
FD5	59107.1	49	196.3	49.6	57.7			0.129	0.129	6.2	9.3	0.746	0.776	23.51	20.52
FD5	59107.2	49	199.2	49.8	57.9			0.112	0.110	4.5	14.5	0.719	0.731	29.69	15.32
FD5	59107.3	49	204.5	48.2	55.9			0.141	0.123	2.8	10.6	0.797	0.791	29.95	15.89
FD5	59107.4	49	187.9	53.1	58.9			0.134	0.132	6.7	9.8	0.815	0.812	24.76	22.15
FD6	59108.1	49	213.4	51.4	61.1			0.133	0.126	9.0	15.1	0.775	0.775	24.31	18.96
FD6	59108.3	49	201.6	52.2	60.8			0.126	0.122	9.5	18.9	0.759	0.780	25.42	18.85
FD6	59108.4	49	204.3	54.1	60.0			0.147	0.117	12.9	23.9	0.771	0.756	24.24	19.14
FD7	59109.1	49	200.2	48.0	58.8			0.149	0.146	10.1	9.6	0.772	0.781	28.08	17.71

Table A3. Double Felted Pressing for Case D2 on the X2 Shoe Press
(Felt B, 0" pivot, and 8500 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF1	59110.1	66	218.2	52.9	62.1			0.236	0.229	6.8	12.2	0.852	0.847	36.90	22.97
WF1	59110.2	66	208.3	52.5	62.3			0.165	0.156	20.6	16.7	0.811	0.810	30.20	19.90
WF2	59111.1	66	204.0	53.6	60.3			0.270	0.253	7.0	9.1	0.900	0.900	36.77	25.11
WF2	59111.2	66	208.0	50.2	57.2			0.277	0.260	5.8	8.8	0.874	0.891	37.82	26.06
WF2	59111.4	66	209.9	51.7	59.4			0.302	0.288	10.6	5.6	0.928	0.935	37.31	25.73
WF3	59112.1	66	222.7	52.9	62.0			0.218	0.231	15.1	2.2	0.876	0.899	31.79	23.16
WF3	59112.2	66	206.0	52.2	61.4			0.194	0.206	6.2	14.1	0.827	0.858	30.69	21.76
WF3	59112.4	66	213.8	51.7	61.6			0.207	0.167	14.0	18.6	0.852	0.833	30.23	20.90
FD5	59113.1	66	214.9	48.5	55.5			0.137	0.130	3.6	4.6	0.793	0.789	31.93	17.53
FD5	59113.2	66	201.0	49.5	58.4			0.129	0.135	6.2	8.1	0.779	0.799	30.91	17.51
FD5	59113.3	66	204.3	49.5	59.2			0.153	0.152	6.5	11.8	0.790	0.773	33.51	16.99
FD5	59113.4	66	222.9	51.6	58.4			0.135	0.133	6.7	5.3	0.815	0.815	32.08	17.02
FD6	59114.1	66	210.1	53.4	62.8			0.127	0.113	13.4	23.9	0.812	0.799	24.65	16.62
FD6	59114.2	66	216.3	52.0	62.8			0.144	0.150	17.4	11.3	0.807	0.835	28.33	16.27
FD6	59114.3	66	188.0	50.9	61.8			0.120	0.137	12.5	6.6	0.796	0.823	26.02	16.74
FD6	59114.4	66	194.3	52.2	61.9			0.126	0.145	16.7	12.4	0.756	0.813	22.28	20.57
FD7	59115.1	66	198.5	49.3	60.2			0.156	0.176	9.6	4.0	0.814	0.847	28.58	19.95
FD7	59115.2	66	204.8	49.5	60.2			0.175	0.167	4.6	7.8	0.827	0.835	29.63	20.60
FD7	59115.3	66	191.2	48.5	59.9			0.140	0.145	10.0	7.6	0.806	0.814	25.16	21.86
FD7	59115.4	66	198.7	49.4	60.7			0.149	0.160	11.4	9.4	0.809	0.809	27.94	19.67

Table A4. Double Felted Pressing for Case D3 on the X2 Shoe Press
(Felt B, 2" pivot, and 6000 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF1	59116.1	66	201.8	52.4	59.7			0.155	0.122	12.9	12.3	0.815	0.797	34.38	19.04
WF1	59116.2	66	202.0	52.4	59.7			0.152	0.157	20.4	20.4	0.828	0.834	32.23	20.98
WF1	59116.3	66	207.0	52.7	59.1			0.167	0.150	11.4	36.7	0.823	0.817	33.82	20.97
WF2	59117.1	66	212.8	53.1	57.5			0.242	0.247	8.7	7.3	0.847	0.850	38.09	25.40
WF2	59117.2	66	205.3	54.5	60.6			0.243	0.215	7.0	10.7	0.848	0.851	36.86	23.29
WF2	59117.3	66	210.8	49.8	55.1			0.218	0.190	9.2	9.5	0.822	0.815	37.03	24.86
WF2	59117.4	66	199.2	51.2	58.5			0.242	0.243	5.0	7.8	0.879	0.885	36.30	25.15
WF3	59118.2	66	206.0	51.0	59.9			0.164	0.184	6.7	13.0	0.837	0.872	28.12	21.60
WF3	59118.4	66	201.3	51.7	60.9			0.197	0.188	5.6	17.6	0.866	0.869	30.85	22.35
FD5	59119.1	66	213.4	50.6	57.5			0.180	0.166	10.0	8.4	0.815	0.807	29.80	19.65
FD5	59119.2	66	195.2	50.7	58.2			0.196	0.182	3.1	3.8	0.827	0.823	33.58	17.25
FD5	59119.3	66	214.9	50.4	56.1			0.208	0.160	4.3	15.0	0.824	0.791	32.43	16.99
FD5	59119.4	66	209.8	52.4	58.3			0.193	0.199	5.7	9.0	0.836	0.840	29.20	20.39
FD6	59120.1	66	201.8	51.0	59.9			0.170	0.135	8.2	16.3	0.803	0.781	26.09	19.49
FD6	59120.2	66	208.5	51.6	60.3			0.133	0.126	21.8	6.3	0.777	0.786	25.87	16.36
FD6	59120.3	66	200.0	51.7	61.1			0.175	0.159	5.7	5.7	0.802	0.797	31.39	16.95
FD6	59120.4	66	210.4	51.8	60.2			0.134	0.135	23.1	11.9	0.782	0.806	24.01	19.64
FD7	59121.1	66	206.5	51.2	58.8			0.196	0.173	6.6	11.6	0.854	0.844	30.47	20.09
FD7	59121.2	66	208.8	50.7	59.8			0.160	0.162	8.8	15.4	0.810	0.833	27.54	21.93
FD7	59121.3	66	205.8	50.3	61.6			0.183	0.164	5.5	11.0	0.841	0.832	28.85	18.56
FD7	59121.4	66	193.2	49.4	59.5			0.155	0.165	7.7	7.3	0.818	0.828	27.80	19.31

Table A5. Double Felted Pressing for Case D4 on the X2 Shoe Press
(Felt S, 0" pivot, and 6000 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF1	59274.1	49	193.3	50.8	61.2			0.259	0.216	9.7	12.5	0.764	0.746	36.00	21.62
WF1	59274.2	49	189.9	50.6	59.3			0.239	0.268	6.3	6.0	0.746	0.773	36.40	23.23
WF1	59274.3	49	193.0	52.4	56.8			0.097	0.169	17.5	27.8	0.645	0.715	26.80	21.22
WF1	59274.4	49	212.3	52.7	61.3			0.266	0.289	4.1	4.2	0.763	0.791	33.62	24.13
WF2	59275.1	49	204.1	50.2	55.5			0.245	0.251	6.1	4.0	0.745	0.767	35.69	25.15
WF2	59275.2	49	206.8	51.8	59.2			0.266	0.251	4.1	8.4	0.756	0.751	35.38	23.12
WF2	59275.3	49	201.0	49.3	56.7			0.274	0.283	2.9	3.9	0.752	0.781	37.93	24.87
WF2	59275.4	49	203.0	50.3	57.1			0.286	0.281	3.5	5.3	0.758	0.760	35.51	22.92
WF3	59276.1	49	221.4	52.0	58.7			0.202	0.229	6.4	6.6	0.746	0.794	28.86	21.06
WF3	59276.2	49	199.3	50.3	60.9			0.193	0.181	13.0	15.5	0.765	0.754	26.02	18.92
WF3	59276.3	49	210.4	50.0	59.7			0.199	0.201	7.5	6.5	0.770	0.785	29.25	19.46
FD5	59277.1	49	214.1	52.5	59.4			0.121	0.118	3.3	5.1	0.717	0.716	28.61	15.75
FD5	59277.3	49	219.1	53.0	59.3			0.108	0.107	5.6	4.7	0.685	0.693	26.42	15.80
FD6	59278.1	49	200.3	54.5	62.7			0.148	0.150	10.1	8.7	0.692	0.695	23.75	19.96
FD6	59278.2	49	204.8	51.8	62.0			0.124	0.137	16.9	10.9	0.669	0.689	24.33	16.55
FD6	59278.3	49	213.4	48.6	60.2			0.159	0.140	3.8	12.1	0.707	0.692	28.40	15.59
FD6	59278.4	49	200.5	52.5	59.9			0.162	0.173	9.3	5.2	0.696	0.706	23.30	20.79
FD7	59279.1	49	200.7	50.6	58.7			0.169	0.162	4.7	7.4	0.730	0.727	30.80	19.72
FD7	59279.2	49	185.9	49.6	58.1			0.158	0.167	5.7	9.6	0.697	0.717	27.94	19.52
FD7	59279.3	49	198.8	49.8	57.9			0.184	0.184	3.3	4.3	0.726	0.731	31.22	20.70
FD7	59279.4	49	197.5	48.9	57.6			0.141	0.142	6.4	6.3	0.700	0.710	26.85	17.51

Table A6. Double Felted Pressing for Case D5 on the X2 Shoe Press
(Felt S, 0" pivot, and 8500 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF1	59280.1	49	204.3	51.9	62.9			0.236	0.258	11.9	5.4	0.864	0.892	34.97	25.40
WF1	59280.2	49	201.6	50.1	61.7			0.238	0.240	6.7	7.1	0.878	0.881	36.99	23.98
WF1	59280.3	49	212.4	50.7	61.5			0.270	0.276	4.1	8.3	0.868	0.874	38.63	25.30
WF1	59280.4	49	205.3	53.1	60.8			0.244	0.263	9.8	5.3	0.847	0.853	33.77	24.89
WF2	59281.1	49	203.6	52.2	58.4			0.266	0.257	5.6	3.9	0.847	0.871	37.59	25.19
WF2	59281.2	49	195.8	50.3	58.6			0.274	0.262	2.9	3.4	0.855	0.866	39.51	26.14
WF2	59281.3	49	207.0	49.0	57.1			0.269	0.267	2.2	6.0	0.867	0.870	39.16	26.77
WF2	59281.4	49	204.3	52.1	59.7			0.261	0.242	3.1	4.1	0.855	0.875	38.12	24.43
WF3	59282.1	49	221.6	50.5	60.7			0.227	0.251	10.1	3.6	0.919	0.920	32.52	24.76
WF3	59282.2	49	196.3	50.3	62.0			0.203	0.205	2.0	6.3	0.878	0.896	31.34	22.58
WF3	59282.4	49	199.5	50.4	61.1			0.225	0.208	5.8	4.3	0.879	0.874	31.82	23.29
FD5	59283.1	49	207.0	51.2	59.1			0.134	0.132	5.2	4.5	0.758	0.763	30.58	16.43
FD5	59283.2	49	207.6	51.6	60.2			0.143	0.142	2.8	4.2	0.776	0.779	31.50	15.63
FD5	59283.3	49	206.6	50.0	57.4			0.121	0.114	5.8	10.5	0.807	0.797	30.88	15.07
FD5	59283.4	49	200.0	53.2	59.2			0.111	0.108	10.8	6.5	0.793	0.788	27.71	14.80
FD6	59284.1	49	206.0	52.5	61.9			0.188	0.158	4.3	9.5	0.853	0.826	26.62	18.87
FD6	59284.2	49	201.1	51.3	62.1			0.166	0.173	12.7	11.0	0.803	0.820	25.06	18.66
FD6	59284.3	49	210.8	52.0	61.0			0.142	0.124	9.2	15.3	0.789	0.779	22.79	18.48
FD6	59284.4	49	202.1	51.8	61.0			0.149	0.121	7.4	11.6	0.783	0.767	24.66	17.87
FD7	59285.1	49	187.5	48.2	59.7			0.186	0.184	3.8	6.0	0.803	0.809	28.62	20.14
FD7	59285.2	49	194.7	48.0	59.7			0.151	0.149	4.6	8.1	0.780	0.794	26.57	18.65
FD7	59285.3	49	197.0	48.7	59.4			0.166	0.154	8.4	8.4	0.788	0.780	27.02	19.59
FD7	59285.4	49	195.7	49.1	59.4			0.174	0.184	8.0	8.2	0.785	0.797	27.74	19.47

Table A7. Double Felted Pressing for Case D6 on the X2 Shoe Press
(Felt S, 2" pivot, and 6000 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m^2	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm^3		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF1	59286.1	49	210.8	52.5	60.7			0.188	0.183	9.0	15.8	0.943	0.957	35.56	22.28
WF1	59286.2	49	214.8	51.7	57.5			0.121	0.182	19.0	15.9	0.861	0.948	31.08	24.55
WF1	59286.3	49	187.0	51.0	55.9			0.114	0.180	14.0	17.8	0.828	0.936	31.05	23.23
WF1	59286.4	49	224.2	49.9	57.3			0.156	0.209	19.2	7.7	0.913	0.970	32.94	24.01
WF2	59287.1	49	208.8	52.7	58.6			0.264	0.251	4.5	6.0	0.781	0.794	37.43	24.75
WF2	59287.2	49	198.0	51.5	57.5			0.297	0.283	4.4	4.6	0.821	0.832	37.40	25.51
WF2	59287.3	49	208.8	50.8	56.3			0.287	0.274	3.8	5.5	0.825	0.819	38.75	26.58
WF2	59287.4	49	205.6	51.3	55.5			0.258	0.256	4.3	4.3	0.781	0.788	36.19	25.34
WF3	59288.1	49	224.9	51.9	58.3			0.224	0.254	8.5	4.7	0.812	0.846	32.55	23.97
WF3	59288.2	49	216.6	51.0	56.7			0.185	0.255	12.4	3.9	0.775	0.801	29.82	24.61
WF3	59288.3	49	204.8	50.4	57.3			0.182	0.216	11.5	6.5	0.761	0.799	29.19	22.88
FD5	59289.1	49	206.0	53.3	60.5			0.184	0.185	6.0	6.5	0.748	0.754	25.02	23.08
FD5	59289.2	49	205.8	51.7	58.2			0.189	0.187	8.5	2.1	0.741	0.742	31.69	18.13
FD5	59289.3	49	215.9	51.8	58.5			0.185	0.181	5.9	8.8	0.746	0.758	27.71	18.33
FD5	59289.4	49	191.2	54.0	58.9			0.204	0.198	2.0	3.5	0.769	0.775	34.07	17.09
FD6	59290.1	49	205.5	54.4	61.7			0.178	0.178	8.4	12.9	0.755	0.767	28.42	19.78
FD6	59290.2	49	193.2	51.1	56.2			0.096	0.140	8.3	29.3	0.695	0.739	22.21	19.68
FD6	59290.3	49	195.5	52.3	59.9			0.114	0.101	6.1	12.9	0.710	0.714	26.32	17.53
FD6	59290.4	49	196.5	50.9	55.9			0.097	0.144	8.2	19.4	0.699	0.748	24.83	19.23
FD7	59291.4	49	204.5	48.5	58.0			0.172	0.177	7.6	7.9	0.828	0.832	29.21	20.41

Table A8. Impulse Drying for Case C1 on the X2 Shoe Press using the IPST-C roll
(Felt B, 0" pivot, and 6000 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF1	59064.2	91	196.5	51.6	62.2		0	0.190	0.175	4.2	4.6	0.839	0.852	34.27	23.33
WF1	59064.3	91	203.0	50.6	61.2		0	0.205	0.199	6.8	6.5	0.846	0.858	38.11	23.73
WF1	59064.4	91	200.2	50.8	55.5		0	0.056	0.054	17.9	9.3	0.721	0.721	26.27	16.93
WF1	59018.1	147	198.5	51.7	61.7		0	0.125	0.152	19.2	8.6	0.832	0.870	34.56	23.82
WF1	59018.2	147	206.1	51.8	58.7		0	0.105	0.127	29.5	26.0	0.803	0.852	30.63	20.87
WF1	59018.3	147	207.5	53.1	58.9		0	0.086	0.126	30.2	30.2	0.784	0.830	31.41	20.75
WF1	59018.4	147	207.3	52.3	61.4		0	0.149	0.167	10.1	8.4	0.854	0.857	34.76	22.49
WF1	59024.1	161	204.5	51.6	60.5		0	0.093	0.076	14.0	10.5	0.764	0.760	28.68	19.18
WF1	59024.2	161	203.6	50.4	60.7		0	0.129	0.160	19.4	11.3	0.784	0.805	31.73	22.03
WF1	59024.3	161	203.5	50.6	60.9		0	0.085	0.099	22.4	26.3	0.716	0.736	29.71	19.45
WF1	59024.4	161	200.8	51.6	61.6		0	0.096	0.111	35.4	37.8	0.710	0.749	29.00	17.99
WF1	59031.1	202	199.2	51.9	63.0		0	0.126	0.105	18.3	16.2	0.880	0.873	32.41	19.88
WF1	59031.2	202	195.0	51.4	62.5		0	0.148	0.152	15.5	12.5	0.896	0.893	34.86	22.06
WF1	59031.3	202	207.8	51.7	58.9		0	0.088	0.054	28.4	11.1	0.815	0.762	31.04	17.02
WF1	59031.4	202	201.5	52.6	63.9		0	0.155	0.147	19.4	17.7	0.862	0.888	31.67	22.29
WF1	59043.1	243	195.2	54.3	66.0		0	0.158	0.154	13.9	13.6	0.917	0.936	33.74	21.29
WF1	59043.2	243	200.2	51.8	65.5		0	0.196	0.211	13.8	7.1	0.944	0.949	39.29	23.07
WF1	59043.3	243	216.4	51.3	62.0		0	0.146	0.103	20.5	15.5	0.860	0.856	33.35	21.81
WF1	59043.4	243	207.1	51.0	60.8		0	0.092	0.069	15.2	10.1	0.858	0.833	31.62	17.74
WF1	59054.1	293	204.0	52.6	63.2		2	0.129	0.107	21.7	47.7	0.915	0.929	30.81	20.16
WF1	59054.2	293	201.0	51.3	66.1		2	0.112	0.077	23.2	57.1	0.895	0.882	29.39	19.35
WF1	59054.3	293	194.0	50.2	67.5		0	0.169	0.167	11.8	13.8	0.956	0.984	35.08	22.75
WF1	59054.4	293	195.5	51.6	66.8		2	0.128	0.086	25.0	43.0	0.935	0.923	31.62	20.69
WF2	59065.1	91	196.8	53.4	60.1		0	0.238	0.238	6.7	4.2	0.909	0.911	38.15	25.65
WF2	59065.2	91	201.3	50.2	55.8		0	0.245	0.242	5.7	5.8	0.865	0.867	37.55	25.71
WF2	59065.3	91	207.3	49.2	58.1		0	0.281	0.272	3.9	4.4	0.855	0.864	37.31	26.12
WF2	59065.4	91	200.3	49.4	53.2		0	0.161	0.170	4.3	10.0	0.756	0.773	34.32	23.56
WF2	59019.1	151	207.5	49.2	55.7		0	0.181	0.190	7.7	7.4	0.807	0.836	34.55	24.16
WF2	59019.2	151	203.5	51.5	59.4		0	0.217	0.232	13.4	9.9	0.846	0.855	33.37	22.99

Table A8 Continued. Impulse Drying for Case C1 on the X2 Shoe Press using the IPST-C roll (Felt B, 0" pivot, and 6000 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF2	59032.1	192	197.8	51.8	60.6		0	0.202	0.234	18.3	6.8	0.871	0.918	36.16	24.65
WF2	59032.2	192	204.8	48.4	57.9		0	0.231	0.233	7.4	5.2	0.879	0.880	38.17	26.31
WF2	59032.3	192	192.2	50.4	60.5		0	0.198	0.205	19.2	8.3	0.878	0.891	34.70	24.68
WF2	59032.4	192	200.3	49.6	58.2		0	0.200	0.187	4.0	9.1	0.849	0.856	36.77	25.84
WF2	59044.1	243	205.0	52.8	62.8		3	0.201	0.219	26.4	7.3	0.873	0.891	33.29	24.29
WF2	59044.2	243	203.6	49.8	60.9		3	0.137	0.198	34.3	24.7	0.814	0.870	28.99	22.58
WF2	59044.3	243	198.3	50.4	62.2		0	0.226	0.225	7.1	7.6	0.928	0.929	36.09	24.26
WF2	59044.4	243	212.8	52.5	62.2		3	0.123	0.121	53.7	62.8	0.823	0.823	30.46	19.59
WF2	59055.1	293	200.3	51.9	62.7		0	0.200	0.186	10.0	7.0	0.848	0.844	34.77	24.39
WF2	59055.2	293	199.7	50.4	60.4		2	0.093	0.132	22.6	18.9	0.755	0.779	30.50	21.88
WF2	59055.3	293	199.5	51.8	62.6		0	0.202	0.187	6.4	4.8	0.813	0.820	34.50	23.93
WF2	59055.4	293	210.9	53.7	63.0		0	0.147	0.181	12.2	7.2	0.754	0.793	32.55	21.98
WF3	59066.1	91	213.6	51.0	60.4		0	0.213	0.218	6.6	5.0	0.890	0.901	32.07	24.32
WF3	59066.2	91	192.4	50.3	60.8		0	0.154	0.141	11.0	8.5	0.859	0.852	28.59	21.72
WF3	59020.1	154	215.6	50.5	61.1		0	0.214	0.216	3.3	4.6	0.875	0.892	32.42	24.26
WF3	59020.4	154	217.7	50.7	61.4		0	0.199	0.192	8.0	7.3	0.866	0.872	30.07	23.11
WF3	59033.2	192	202.3	50.2	62.7		0	0.189	0.167	15.3	10.8	0.876	0.909	29.03	21.65
WF3	59033.3	192	204.6	49.9	61.9		0	0.162	0.199	15.4	9.0	0.836	0.875	29.44	20.32
WF3	59033.4	192	223.2	50.5	61.9		0	0.220	0.221	5.5	4.5	0.887	0.903	31.31	23.98
WF3	59045.1	242	214.9	50.3	63.7		3	0.116	0.082	53.4	74.4	0.826	0.810	27.68	18.54
WF3	59045.2	242	199.8	49.7	64.0		3	0.190	0.162	8.4	23.5	0.896	0.883	31.81	22.20
WF3	59045.4	242	199.5	50.5	65.4		3	0.045	0.034	22.2	20.6	0.799	0.742	25.42	16.65
WF3	59056.3	293	223.1	49.7	62.2		1	0.183	0.196	10.4	5.1	0.761	0.780	30.84	22.60
WF3	59056.4	293	199.3	50.4	64.5		0	0.159	0.173	20.1	12.1	0.760	0.796	28.99	21.56
FD5	59067.1	91	221.9	55.5	59.2		0	0.142	0.136	4.2	3.7	0.843	0.843	31.50	16.43
FD5	59067.2	91	216.4	52.3	57.2		0	0.130	0.139	5.4	3.6	0.812	0.830	25.06	21.58
FD5	59067.3	91	206.5	51.2	58.2		0	0.113	0.115	4.4	5.2	0.798	0.820	30.39	17.11
FD5	59067.4	91	207.6	54.1	59.0		0	0.129	0.120	5.4	6.7	0.834	0.826	30.64	17.82
FD5	59021.1	157	185.0	53.7	61.3		0	0.115	0.125	4.3	5.6	0.844	0.852	30.23	16.02

Table A8 Continued. Impulse Drying for Case C1 on the X2 Shoe Press using the IPST-C roll (Felt B, 0" pivot, and 6000 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
FD5	59034.1	191	208.9	52.6	59.9		2	0.066	0.072	25.8	30.6	0.757	0.791	18.92	19.49
FD5	59034.2	191	200.7	52.8	62.6		0	0.131	0.136	3.8	2.9	0.885	0.898	25.65	22.58
FD5	59034.3	191	207.6	51.3	58.4		2	0.082	0.060	22.0	10.0	0.785	0.765	28.17	13.13
FD5	59034.4	191	191.0	52.5	60.6		2	0.101	0.055	21.8	10.9	0.830	0.771	29.19	14.79
FD6	59068.1	91	204.6	53.0	62.2		0	0.111	0.113	20.7	10.6	0.814	0.830	25.98	15.32
FD6	59068.2	91	189.5	50.9	58.0		0	0.076	0.068	5.3	7.4	0.764	0.768	23.16	16.93
FD6	59068.4	91	197.7	50.8	61.6		0	0.152	0.145	4.6	6.2	0.839	0.828	25.73	19.29
FD6	59023.3	164	199.5	53.4	62.5		0	0.110	0.117	10.9	13.7	0.879	0.896	23.10	19.59
FD6	59023.4	164	194.8	52.3	62.3		0	0.131	0.128	6.9	5.5	0.896	0.884	25.85	19.96
FD6	59035.1	192	198.3	53.0	64.0		0	0.106	0.113	25.5	27.4	0.829	0.844	25.68	17.66
FD6	59035.2	192	208.1	50.1	61.6		0	0.143	0.129	11.9	10.9	0.824	0.818	27.54	17.39
FD6	59035.3	192	207.5	49.8	62.6		0	0.143	0.141	11.2	12.8	0.816	0.812	24.49	20.67
FD6	59035.4	192	204.1	51.0	64.1		0	0.156	0.147	7.7	6.8	0.820	0.825	26.02	20.36
FD6	59047.1	241	198.2	52.2	65.4		0	0.180	0.165	4.4	19.4	0.832	0.828	28.03	19.35
FD6	59047.2	241	207.8	50.1	65.1		0	0.175	0.165	8.0	10.3	0.823	0.822	23.85	21.98
FD6	59047.3	241	194.3	50.8	64.8		0	0.156	0.144	3.8	8.3	0.825	0.833	26.52	19.68
FD6	59047.4	241	204.5	50.4	65.8		0	0.193	0.204	5.7	3.4	0.849	0.862	27.85	19.98
FD6	59057.1	293	201.5	51.5	66.0		2	0.135	0.112	8.9	32.1	0.850	0.836	24.39	18.89
FD6	59057.2	293	204.8	51.9	67.0		1	0.112	0.099	23.2	14.1	0.839	0.839	25.57	16.45
FD6	59057.3	293	203.0	51.3	66.6		0	0.127	0.129	22.0	12.4	0.836	0.861	24.44	19.77
FD6	59057.4	293	196.2	51.7	68.1		0	0.136	0.125	15.4	13.6	0.857	0.865	25.46	18.42
FD7	59069.1	91	201.0	52.4	60.1		0	0.166	0.162	2.4	6.8	0.860	0.863	29.25	19.94
FD7	59069.2	91	195.8	51.9	61.4		0	0.160	0.165	4.4	8.5	0.871	0.894	27.15	21.88
FD7	59069.3	91	197.0	51.6	61.2		0	0.161	0.158	4.3	4.4	0.875	0.879	29.72	19.20
FD7	59069.4	91	200.0	52.5	59.5		0	0.158	0.153	5.1	2.6	0.852	0.850	30.50	19.91
FD7	59022.1	161	198.2	54.4	61.9		0	0.125	0.114	8.8	20.2	0.859	0.872	25.30	19.12
FD7	59022.2	161	195.0	51.0	59.8		0	0.137	0.130	10.9	13.1	0.874	0.859	28.68	19.47
FD7	59022.3	161	198.3	49.5	59.4		0	0.122	0.136	10.7	6.6	0.825	0.847	25.54	19.39
FD7	59022.4	161	201.3	49.5	59.5		0	0.144	0.137	4.2	5.8	0.825	0.820	28.50	18.09

Table A8 Continued. Impulse Drying for Case C1 on the X2 Shoe Press using the IPST-C roll
(Felt B, 0" pivot, and 6000 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m^2	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm^3		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
FD7	59036.1	192	196.5	48.9	61.2		0	0.146	0.117	9.6	23.9	0.855	0.884	27.23	19.12
FD7	59036.2	192	191.2	48.8	60.8		0	0.141	0.151	7.8	5.3	0.869	0.890	28.47	20.70
FD7	59036.3	192	192.4	49.7	62.9		0	0.131	0.145	12.2	11.7	0.865	0.870	28.51	19.61
FD7	59036.4	192	199.5	49.9	61.2		0	0.148	0.150	10.1	7.3	0.853	0.858	29.09	19.05
FD7	59048.1	241	195.7	50.4	62.9		0	0.136	0.151	11.0	11.3	0.858	0.873	25.86	20.55
FD7	59048.2	241	193.7	49.2	63.3		0	0.145	0.145	9.0	7.6	0.862	0.874	27.53	18.03
FD7	59048.3	241	192.4	49.7	63.7		0	0.150	0.144	4.0	4.9	0.861	0.875	25.94	20.37
FD7	59048.4	241	189.5	50.6	62.8		0	0.156	0.143	5.8	13.3	0.879	0.882	29.35	18.43
FD7	59058.1	293	191.0	50.3	63.9		1	0.090	0.102	14.4	14.7	0.821	0.848	23.53	17.11
FD7	59058.2	293	195.8	50.4	63.6		1	0.099	0.100	21.2	13.0	0.830	0.833	22.95	17.09
FD7	59058.3	293	192.8	48.4	63.9		2	0.109	0.091	8.3	18.7	0.833	0.822	26.69	18.01
FD7	59058.4	293	194.7	50.9	64.9		1	0.099	0.115	16.2	9.6	0.845	0.861	22.16	19.94

Table A9. Impulse Drying for Case C2 on the X2 Shoe Press using the IPST-C roll
(Felt B, 0" pivot, and 8500 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF1	59070.1	91	199.0	51.7	64.5		0	0.237	0.226	5.5	3.1	0.898	0.907	37.31	25.21
WF1	59070.2	91	188.4	51.1	63.8		0	0.221	0.215	2.7	3.3	0.886	0.903	35.09	23.81
WF1	59070.3	91	205.6	51.1	63.0		0	0.224	0.209	3.6	16.3	0.931	0.930	35.56	23.96
WF1	59070.4	91	188.5	51.2	63.8		0	0.217	0.201	4.1	4.0	0.942	0.941	35.80	24.65
WF1	59030.1	151	199.3	51.3	59.9		0	0.158	0.180	27.8	37.2	0.756	0.781	31.93	21.82
WF1	59030.2	151	209.9	52.7	63.9		0	0.217	0.241	11.1	4.6	0.806	0.818	33.64	23.05
WF1	59030.3	151	203.1	51.4	56.8		0	0.211	0.236	19.9	9.3	0.789	0.816	34.53	25.27
WF1	59030.4	151	206.3	51.4	62.2		0	0.184	0.183	23.9	30.6	0.763	0.769	31.68	22.79
WF1	59037.1	194	200.3	51.6	60.2		0	0.109	0.071	27.5	14.1	0.846	0.802	29.06	16.49
WF1	59037.3	194	201.6	51.4	63.3		0	0.184	0.154	10.9	29.2	0.890	0.917	34.88	22.73
WF1	59037.4	194	193.8	51.0	64.2		0	0.215	0.190	7.0	6.3	0.943	0.926	35.85	21.88
WF1	59049.2	243	206.0	54.6	67.5		0	0.259	0.250	4.2	6.0	0.979	0.992	37.38	25.04
WF1	59049.3	243	202.1	53.1	61.5		0	0.159	0.233	18.2	7.7	0.941	1.027	34.44	25.02
WF1	59059.1	295	206.0	52.1	66.3		0	0.162	0.198	6.2	10.6	0.945	0.986	33.56	23.42
WF1	59059.2	295	211.3	51.1	64.6		2	0.106	0.095	17.0	20.0	0.853	0.864	31.21	19.38
WF1	59059.3	295	207.8	51.3	67.3		0	0.148	0.177	30.4	10.7	0.873	0.927	30.00	22.90
WF1	59059.4	295	195.7	52.9	68.5		0	0.176	0.175	11.9	10.9	0.938	0.921	33.79	23.57
WF2	59071.1	91	196.5	51.4	60.9		0	0.235	0.233	6.8	3.4	0.964	0.997	36.88	26.73
WF2	59071.2	91	200.5	48.8	58.8		0	0.241	0.226	4.1	3.5	0.977	1.015	38.05	27.59
WF2	59071.3	91	209.1	52.3	61.7		0	0.244	0.251	4.1	3.6	0.985	0.994	37.30	25.80
WF2	59071.4	91	200.0	50.6	60.8		0	0.263	0.245	4.2	4.1	0.951	0.967	38.61	26.31
WF2	59025.2	158	203.0	52.5	59.4		0	0.231	0.236	5.2	2.5	1.003	0.999	36.15	27.07
WF2	59025.3	158	207.5	53.3	62.2		0	0.243	0.247	5.8	10.5	0.958	0.958	37.69	25.61
WF2	59025.4	158	208.3	51.6	59.0		0	0.201	0.196	8.0	13.8	0.921	0.936	37.32	24.76
WF2	59038.1	194	208.3	49.3	59.5		0	0.255	0.273	7.8	4.8	0.950	0.973	37.60	27.52
WF2	59038.2	194	202.0	48.9	59.0		0	0.246	0.236	5.3	10.2	0.935	0.918	38.15	27.08
WF2	59038.3	194	197.7	50.0	61.6		0	0.255	0.268	6.7	5.6	0.963	0.975	39.65	27.31
WF2	59038.4	194	203.6	48.7	58.6		0	0.245	0.227	6.5	8.8	0.908	0.925	39.51	26.76

Table A9 Continued. Impulse Drying for Case C2 on the X2 Shoe Press using the IPST-C roll
(Felt B, 0" pivot, and 8500 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF2	59050.1	243	206.0	53.1	62.0		0	0.214	0.239	6.5	7.1	0.920	0.918	38.33	26.61
WF2	59050.2	243	207.3	52.0	63.6		0	0.243	0.250	4.9	6.8	0.924	0.943	38.78	25.97
WF2	59050.4	243	195.0	48.1	62.5		0	0.246	0.246	5.3	6.9	0.935	0.935	35.64	26.54
WF2	59060.1	295	207.8	53.1	65.0		0	0.189	0.208	5.8	5.8	0.948	0.947	34.98	24.48
WF2	59060.2	295	205.6	48.9	59.6		0	0.099	0.095	34.3	25.3	0.858	0.850	32.17	21.57
WF2	59060.3	295	204.3	50.2	63.0		0	0.177	0.188	7.9	10.6	0.935	0.959	35.66	25.60
WF2	59060.4	295	207.8	49.2	60.2		1	0.110	0.104	42.7	44.2	0.854	0.859	32.63	22.87
WF3	59072.1	91	214.4	50.5	62.7		0	0.235	0.239	4.7	2.9	0.946	0.997	32.92	24.02
WF3	59072.2	91	200.7	49.4	63.0		0	0.212	0.210	5.7	3.8	0.941	0.974	31.13	23.63
WF3	59072.3	91	222.1	48.3	61.5		0	0.237	0.231	3.4	3.9	0.943	0.951	33.86	25.45
WF3	59026.2	153	199.3	53.3	63.0		0	0.190	0.216	4.2	3.7	0.962	0.957	30.69	23.71
WF3	59026.3	153	208.1	51.2	61.7		0	0.191	0.175	12.0	12.0	0.900	0.933	33.06	20.75
WF3	59026.4	153	216.3	51.9	62.4		0	0.214	0.184	5.1	6.0	0.927	0.926	33.30	23.56
WF3	59039.1	195	214.9	51.9	62.2		0	0.202	0.198	7.4	4.5	0.930	0.937	31.96	23.52
WF3	59039.2	195	199.0	49.5	64.3		0	0.187	0.224	8.0	3.1	0.938	0.943	30.28	23.93
WF3	59039.3	195	209.8	48.4	62.2		0	0.205	0.174	5.4	22.4	0.904	0.905	30.78	21.57
WF3	59039.4	195	205.5	50.2	63.2		0	0.226	0.228	4.4	2.6	0.945	0.960	32.23	23.45
WF3	59051.1	243	210.8	51.7	65.3		0	0.222	0.201	6.3	5.5	0.926	0.958	33.04	23.62
WF3	59051.2	243	220.9	48.9	64.2		3	0.194	0.115	12.4	55.7	0.922	0.926	30.62	22.62
WF3	59051.3	243	205.3	49.6	65.1		3	0.122	0.199	51.6	25.6	0.847	0.937	27.74	23.79
WF3	59051.4	243	210.4	51.1	65.1		0	0.209	0.221	9.6	5.9	0.951	0.947	32.59	24.16
WF3	59061.1	295	212.1	51.1	64.2		2	0.198	0.180	4.0	8.9	0.812	0.798	29.35	20.02
WF3	59061.2	295	197.8	49.7	65.3		2	0.182	0.174	18.7	12.1	0.793	0.794	28.61	21.85
WF3	59061.3	295	220.9	49.5	64.0		2	0.208	0.213	2.9	6.6	0.802	0.816	30.00	22.44
WF3	59061.4	295	220.7	50.6	64.5		1	0.209	0.191	5.3	5.2	0.817	0.812	30.20	22.05
FD5	59073.1	91	202.5	51.2	59.8		0	0.169	0.169	5.3	7.7	0.856	0.849	26.92	22.90
FD5	59073.2	91	215.3	50.5	57.6		0	0.149	0.146	4.7	10.3	0.819	0.820	31.30	18.56
FD5	59073.3	91	219.2	50.1	57.2		0	0.152	0.137	5.3	3.6	0.824	0.800	29.70	20.64
FD5	59073.4	91	198.5	50.3	59.1		0	0.145	0.148	3.4	4.1	0.839	0.848	33.00	18.09

Table A9 Continued. Impulse Drying for Case C2 on the X2 Shoe Press using the IPST-C roll (Felt B, 0" pivot, and 8500 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
FD5	59027.2	151	200.5	54.8	60.4		0	0.112	0.110	13.4	7.3	0.827	0.829	30.37	17.11
FD5	59027.3	151	189.7	53.4	60.8		0	0.103	0.122	10.7	7.4	0.822	0.848	29.75	16.55
FD5	59027.4	151	209.1	54.5	61.0		0	0.121	0.130	7.4	6.2	0.846	0.855	26.76	21.07
FD5	59040.1	196	206.5	52.0	61.5		3	0.118	0.125	5.1	5.6	0.850	0.864	28.30	20.79
FD5	59040.3	196	191.4	53.4	61.4		3	0.123	0.080	19.5	31.3	0.840	0.780	31.59	14.14
FD5	59040.4	196	209.6	52.4	59.4		3	0.095	0.076	30.5	39.5	0.789	0.753	29.68	14.40
FD6	59074.1	91	201.6	50.8	63.6		0	0.180	0.181	3.3	3.9	0.950	0.946	28.45	21.72
FD6	59074.2	91	202.5	49.4	63.9		0	0.175	0.177	2.9	3.4	0.933	0.896	27.52	21.76
FD6	59029.1	151	199.3	52.2	64.2		0	0.166	0.165	6.0	6.1	0.872	0.871	25.89	22.61
FD6	59029.2	151	200.2	51.2	63.1		0	0.152	0.153	7.2	12.4	0.841	0.848	25.60	20.47
FD6	59029.3	151	204.0	51.9	63.4		0	0.148	0.141	5.4	5.0	0.825	0.819	26.86	20.27
FD6	59029.4	151	209.4	50.5	63.1		0	0.170	0.170	5.9	5.9	0.840	0.837	26.39	22.07
FD6	59041.1	197	201.5	50.9	65.0		0	0.161	0.165	7.5	5.5	0.901	0.901	26.53	22.83
FD6	59041.2	197	205.1	50.7	64.4		0	0.141	0.167	12.8	6.0	0.869	0.884	28.83	19.07
FD6	59041.3	197	197.8	50.2	61.8		0	0.107	0.099	10.3	14.1	0.824	0.810	24.50	21.16
FD6	59041.4	197	198.7	50.6	64.2		0	0.147	0.184	7.5	6.0	0.827	0.859	28.54	19.86
FD6	59052.1	243	202.1	51.6	66.5		0	0.205	0.172	7.3	10.5	0.866	0.841	27.64	20.13
FD6	59052.2	243	207.8	50.2	65.0		0	0.188	0.187	10.6	11.2	0.830	0.836	28.77	19.98
FD6	59052.3	243	201.3	51.4	67.4		0	0.206	0.193	5.8	13.0	0.835	0.819	28.60	20.74
FD6	59052.4	243	204.8	51.8	66.7		0	0.196	0.170	15.8	17.6	0.808	0.799	30.04	18.06
FD6	59062.1	295	194.0	52.0	67.8		0	0.178	0.187	7.9	6.4	0.809	0.814	28.87	18.66
FD6	59062.2	295	195.8	50.8	67.2		0	0.188	0.153	5.9	18.3	0.802	0.779	27.34	18.48
FD6	59062.4	295	199.7	51.2	67.1		0	0.153	0.167	5.9	7.8	0.809	0.830	24.55	22.19
FD7	59075.2	91	191.5	49.8	62.8		0	0.169	0.164	13.6	16.5	0.910	0.906	29.09	20.60
FD7	59075.3	91	204.1	51.4	62.8		0	0.183	0.176	3.3	5.7	0.919	0.957	30.04	18.61
FD7	59075.4	91	194.3	52.6	62.3		0	0.165	0.151	3.6	6.6	0.947	0.946	27.58	17.20
FD7	59028.1	151	197.0	48.1	60.3		0	0.192	0.199	7.8	6.0	0.795	0.815	30.33	20.72
FD7	59028.2	151	198.5	49.5	62.1		0	0.161	0.182	9.9	9.9	0.779	0.794	25.78	19.37
FD7	59028.4	151	201.6	49.2	60.8		0	0.151	0.153	4.6	11.8	0.765	0.780	26.47	21.47

Table A9 Continued. Impulse Drying for Case C2 on the X2 Shoe Press using the IPST-C roll
(Felt B, 0" pivot, and 8500 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
FD7	59042.1	197	185.7	49.8	63.0		0	0.173	0.165	6.9	5.5	0.958	0.949	28.43	22.24
FD7	59042.2	197	197.7	49.3	62.1		0	0.148	0.122	9.5	15.6	0.922	0.888	26.80	19.29
FD7	59042.3	197	194.2	48.6	62.1		0	0.148	0.157	4.1	10.8	0.906	0.900	27.29	21.34
FD7	59042.4	197	188.9	48.7	61.7		0	0.124	0.138	13.7	13.0	0.867	0.867	26.96	19.73
FD7	59053.1	243	201.3	50.9	63.2		0	0.115	0.133	17.4	9.0	0.894	0.937	27.34	18.91
FD7	59053.2	243	198.2	49.6	63.2		0	0.152	0.129	7.9	6.2	0.959	0.942	27.10	19.92
FD7	59053.3	243	197.3	50.9	63.6		0	0.166	0.159	5.4	5.0	0.977	0.985	29.46	22.71
FD7	59053.4	243	197.7	51.1	64.7		0	0.158	0.152	8.2	9.2	0.977	0.988	27.07	22.77
FD7	59063.1	295	191.9	51.3	64.5		1	0.112	0.117	6.3	3.4	0.934	0.946	27.39	22.62
FD7	59063.2	295	198.7	51.0	64.6		1	0.134	0.131	5.2	2.3	0.964	0.956	28.26	21.89
FD7	59063.3	295	190.2	50.5	63.6		0	0.108	0.117	6.5	3.4	0.927	0.974	27.79	20.69
FD7	59063.4	295	198.7	51.4	64.1		0	0.122	0.132	7.4	9.8	0.940	0.947	29.13	20.27

Table A10. Impulse Drying for Case C3 on the X2 Shoe Press using the IPST-C roll
(Felt B, 2" pivot, and 6000 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF1	59098.1	91	201.5	50.9	58.8		0	0.134	0.205	44.0	5.9	0.825	0.932	29.20	22.65
WF1	59098.3	91	203.1	51.0	63.9		0	0.210	0.191	4.8	4.2	0.930	0.911	36.24	21.68
WF1	59076.1	152	211.9	51.9	53.6		0	0.058	0.074	25.9	8.1	0.729	0.821	22.77	18.48
WF1	59076.2	152	195.7	51.5	64.0		0	0.165	0.165	9.1	10.3	0.883	0.902	33.53	22.62
WF1	59076.3	152	208.0	51.1	64.1		0	0.157	0.145	15.9	5.5	0.910	0.890	32.69	21.95
WF1	59076.4	152	204.3	52.4	64.9		0	0.148	0.151	13.5	13.2	0.909	0.913	31.64	22.09
WF1	59082.1	200	212.1	51.5	64.5		0	0.112	0.129	22.3	24.0	0.887	0.919	28.30	19.02
WF1	59082.2	200	193.3	51.8	63.5		0	0.064	0.107	40.6	25.2	0.792	0.873	25.30	18.56
WF1	59082.3	200	205.5	50.7	64.3		0	0.084	0.116	23.8	13.8	0.861	0.921	28.39	20.58
WF1	59082.4	200	204.5	52.1	65.0		0	0.063	0.141	23.8	15.6	0.757	0.918	27.70	21.24
WF1	59088.1	247	204.8	52.1	64.7		0	0.118	0.116	16.1	12.9	0.927	0.954	29.27	20.12
WF1	59088.2	247	193.3	53.1	66.2		0	0.092	0.114	26.1	23.7	0.878	0.951	26.32	21.49
WF1	59088.3	247	207.6	51.9	65.2		0	0.134	0.186	13.4	10.8	0.896	0.931	27.14	21.53
WF1	59088.4	247	199.7	51.9	64.9		0	0.077	0.095	24.7	11.6	0.774	0.809	26.06	19.28
WF2	59099.1	91	212.9	53.6	58.1		0	0.223	0.210	4.9	3.3	0.886	0.913	36.43	24.14
WF2	59099.2	91	211.3	52.4	60.9		0	0.234	0.252	4.7	5.2	0.898	0.911	38.77	26.45
WF2	59099.3	91	202.1	51.0	58.5		0	0.214	0.188	7.5	10.6	0.882	0.869	36.29	23.42
WF2	59099.4	91	209.4	49.5	58.0		0	0.228	0.243	3.9	3.3	0.913	0.930	39.01	26.98
WF2	59077.1	150	199.7	50.5	60.7		0	0.148	0.186	41.9	22.6	0.815	0.833	32.01	22.91
WF2	59077.2	150	210.1	51.1	60.4		0	0.222	0.258	6.8	7.4	0.832	0.863	34.22	25.44
WF2	59077.3	150	210.6	52.2	61.6		0	0.261	0.273	7.3	2.9	0.847	0.861	35.43	24.95
WF2	59077.4	150	210.9	51.1	59.7		0	0.283	0.301	7.1	4.3	0.836	0.845	38.04	25.26
WF2	59083.1	200	204.3	48.1	59.1		0	0.086	0.103	30.2	37.9	0.680	0.737	26.86	20.59
WF2	59083.2	200	202.1	50.0	61.1		0	0.127	0.231	27.6	13.0	0.743	0.819	33.22	23.15
WF2	59083.3	200	206.6	48.9	59.7		0	0.145	0.179	18.6	22.3	0.768	0.791	32.65	23.10
WF2	59083.4	200	203.3	52.0	62.5		0	0.206	0.243	24.8	5.8	0.802	0.834	35.04	24.02
WF2	59089.1	247	211.3	53.6	64.0		0	0.193	0.162	7.3	9.9	0.855	0.862	31.83	21.93
WF2	59089.2	247	202.5	49.5	60.9		0	0.172	0.188	12.2	3.2	0.842	0.857	33.01	23.61
WF2	59089.3	247	209.4	51.8	62.2		0	0.225	0.222	7.1	4.1	0.844	0.868	34.93	23.97
WF2	59089.4	247	204.5	50.8	61.9		0	0.169	0.160	10.1	9.4	0.851	0.853	33.69	22.61

Table A10 Continued. Impulse Drying for Case C3 on the X2 Shoe Press using the IPST-C roll
(Felt B, 2" pivot, and 6000 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF3	59100.1	91	204.8	51.5	61.9		0	0.206	0.179	8.3	22.9	0.829	0.811	29.73	21.41
WF3	59100.2	91	214.9	50.5			0	0.156	0.241	25.0	5.4	0.758	0.839	28.24	22.32
WF3	59100.3	91	194.8	50.8	61.9		0	0.195	0.213	10.8	7.0	0.802	0.818	29.10	22.01
WF3	59078.2	148	213.3	52.0	63.1		0	0.228	0.225	11.0	7.1	0.927	0.937	32.73	23.75
WF3	59078.3	148	208.1	52.4	64.8		0	0.205	0.214	8.8	5.6	0.913	0.924	29.90	23.52
WF3	59078.4	148	201.0	51.6	57.6		0	0.179	0.201	6.1	13.4	0.851	0.879	31.29	22.02
WF3	59084.1	200	217.1	53.2	65.4		3	0.103	0.094	39.8	30.9	0.790	0.823	22.66	19.56
WF3	59084.2	200	223.7	52.7	64.5		3	0.126	0.131	30.2	29.0	0.827	0.840	30.05	21.41
WF3	59084.3	200	195.3	50.9	64.9		3	0.138	0.154	21.7	22.7	0.814	0.835	28.28	22.43
WF3	59084.4	200	199.3	50.9	63.9		3	0.132	0.159	17.4	17.0	0.813	0.829	32.32	20.82
WF3	59090.1	247	219.9	51.8	64.3		0	0.176	0.191	14.2	11.5	0.912	0.914	31.83	23.15
WF3	59090.2	247	216.6	51.7	65.0		0	0.147	0.168	12.9	11.9	0.896	0.893	29.14	21.13
WF3	59090.3	247	209.1	49.9	65.4		0	0.141	0.162	10.6	10.5	0.892	0.905	28.29	21.75
WF3	59090.4	247	210.4	49.5	63.8		0	0.129	0.135	10.9	12.6	0.957	0.991	30.02	21.71
FD5	59101.1	91	185.0	51.7	58.8		0	0.179	0.159	4.5	22.6	0.815	0.803	30.02	16.60
FD5	59101.2	91	218.7	50.8	55.9		0	0.179	0.147	6.1	16.3	0.793	0.781	28.12	18.06
FD5	59101.3	91	191.9	51.2	57.8		0	0.178	0.176	6.2	5.1	0.801	0.809	32.83	16.79
FD5	59101.4	91	216.7	50.6	54.7		0	0.184	0.173	2.2	6.4	0.799	0.785	30.91	16.44
FD5	59079.1	147	190.2	51.9	59.5		0	0.173	0.156	6.4	7.1	0.846	0.834	30.66	17.06
FD5	59079.2	147	209.4	50.0	57.2		0	0.168	0.151	6.5	9.3	0.799	0.793	27.71	17.85
FD5	59079.3	147	204.0	50.2	58.7		0	0.142	0.138	11.3	8.0	0.789	0.799	29.87	16.23
FD5	59079.4	147	190.4	51.6	61.8		0	0.150	0.159	8.0	4.4	0.811	0.825	31.01	18.04
FD5	59085.2	200	187.4	54.8	63.2		3	0.124	0.112	8.1	21.4	0.800	0.799	27.01	17.00
FD5	59091.2	247	201.3	53.4	64.8		2	0.139	0.118	3.6	12.7	0.943	0.923	24.94	22.92
FD5	59091.3	247	213.9	52.1	60.7		2	0.127	0.128	4.7	9.4	0.875	0.876	29.10	16.75
FD6	59102.1	91	201.6	53.4	63.0		0	0.129	0.120	5.4	11.7	0.845	0.843	27.11	17.68
FD6	59102.2	91	219.1	51.8	61.2		0	0.129	0.101	7.0	17.8	0.824	0.807	26.38	18.46
FD6	59102.3	91	205.3	51.8	61.0		0	0.159	0.152	5.0	11.8	0.842	0.843	27.58	19.27
FD6	59102.4	91	198.8	52.2	61.8		0	0.135	0.114	10.4	21.1	0.815	0.811	26.38	17.32

Table A10 Continued. Impulse Drying for Case C3 on the X2 Shoe Press using the IPST-C roll (Felt B, 2" pivot, and 6000 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
FD6	59080.2	146	211.6	53.7	64.5		0	0.149	0.152	8.1	6.6	0.904	0.959	26.38	20.67
FD6	59080.3	146	192.5	52.9	65.2		0	0.131	0.149	3.1	5.4	0.946	0.957	26.13	20.86
FD6	59080.4	146	197.7	51.4	64.0		0	0.138	0.128	5.8	12.5	0.923	0.923	26.71	21.83
FD6	59086.1	200	207.5	51.7	65.2		0	0.154	0.151	5.8	6.6	0.854	0.847	26.02	20.32
FD6	59086.2	200	198.2	52.8	66.0		0	0.164	0.159	3.0	4.4	0.854	0.848	27.33	20.02
FD6	59086.3	200	207.0	50.6	64.7		0	0.168	0.175	6.0	3.4	0.856	0.853	25.99	21.12
FD6	59086.4	200	203.0	51.6	65.3		0	0.166	0.162	4.2	11.1	0.856	0.858	25.45	20.77
FD6	59092.1	247	200.5	51.1	65.0		0	0.148	0.166	17.6	7.8	0.843	0.859	25.94	18.91
FD6	59092.2	247	207.6	50.7	66.3		0	0.170	0.176	4.7	11.9	0.867	0.860	25.65	22.94
FD6	59092.3	247	197.8	50.9	67.2		0	0.145	0.160	6.9	3.8	0.906	0.901	25.91	21.31
FD6	59092.4	247	201.0	51.7	67.6		0	0.164	0.164	4.9	5.5	0.887	0.878	26.68	21.52
FD6	59094.1	297	203.6	51.7	68.7		0	0.164	0.150	11.0	8.7	0.864	0.843	28.89	17.64
FD6	59094.2	297	207.1	50.2	67.6		0	0.088	0.094	27.3	28.7	0.778	0.781	22.18	18.26
FD6	59094.3	297	203.0	51.0	65.6		0	0.155	0.145	11.6	11.0	0.811	0.804	27.62	18.78
FD6	59094.4	297	199.2	51.4	67.2		0	0.179	0.176	14.0	8.5	0.817	0.810	24.68	21.58
FD6	59096.1	316	207.0	50.4	67.4		0	0.129	0.131	13.2	12.2	0.953	0.955	25.49	20.07
FD6	59096.2	316	210.4	52.9	68.1		0	0.108	0.117	14.8	13.7	0.907	0.905	28.18	16.48
FD6	59096.3	316	205.0	50.9	69.2		0	0.134	0.148	9.7	7.4	0.930	0.921	25.83	22.39
FD6	59096.4	316	199.0	51.2	69.2		0	0.147	0.140	6.8	10.0	0.907	0.901	25.89	22.93
FD7	59103.1	91	201.0	49.2	59.2		0	0.145	0.126	9.7	7.9	0.862	0.855	28.60	20.19
FD7	59103.3	91	197.0	48.2	58.4		0	0.145	0.145	6.2	7.6	0.835	0.834	29.10	20.88
FD7	59103.4	91	194.3	50.1	59.7		0	0.155	0.147	9.0	11.6	0.852	0.849	29.98	19.80
FD7	59081.1	145	199.8	51.3	60.7		0	0.160	0.127	5.0	7.9	0.962	0.948	30.61	21.01
FD7	59081.3	145	195.7	53.8	63.3		0	0.162	0.161	3.7	3.7	0.964	0.962	29.81	22.17
FD7	59081.4	145	197.0	53.7	63.2		0	0.170	0.165	4.1	9.1	0.956	0.935	29.26	20.46
FD7	59087.1	200	192.7	51.2	64.2		0	0.187	0.187	3.7	4.8	0.805	0.806	29.44	19.47
FD7	59087.2	200	204.3	50.8	63.3		0	0.209	0.204	5.3	3.4	0.805	0.805	29.78	20.40
FD7	59087.3	200	199.0	49.6	62.7		0	0.196	0.210	5.6	2.9	0.801	0.801	28.98	22.69
FD7	59087.4	200	193.2	49.8	62.1		0	0.192	0.195	5.7	4.1	0.796	0.804	28.31	21.94

Table A10 Continued. Impulse Drying for Case C3 on the X2 Shoe Press using the IPST-C roll
(Felt B, 2" pivot, and 6000 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m^2	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm^3		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
FD7	59093.1	247	194.5	50.7	64.3		0	0.178	0.168	8.4	8.3	0.815	0.803	27.66	18.41
FD7	59093.2	247	195.7	49.5	64.5		0	0.172	0.175	5.2	5.7	0.807	0.803	26.33	21.07
FD7	59093.3	247	196.7	48.9	64.2		0	0.175	0.190	6.3	4.2	0.815	0.794	27.58	19.26
FD7	59093.4	247	202.8	48.8	62.9		0	0.181	0.192	9.4	4.7	0.761	0.766	24.74	20.28
FD7	59095.1	297	187.5	49.2	64.3		2	0.119	0.131	31.1	6.1	0.741	0.799	24.84	21.08
FD7	59095.2	297	198.3	49.4	65.3		1	0.138	0.142	11.6	9.9	0.804	0.803	27.49	20.58
FD7	59095.3	297	193.3	48.5	65.7		1	0.121	0.132	17.4	6.1	0.784	0.778	28.41	19.23
FD7	59095.4	297	187.0	50.4	67.2		1	0.115	0.108	20.0	20.4	0.784	0.766	27.93	16.98
FD7	59097.1	316	194.3	49.0	66.4		1	0.088	0.109	27.3	11.9	0.867	0.878	26.43	20.24
FD7	59097.2	316	191.5	48.7	65.5		1	0.098	0.079	12.2	29.1	0.878	0.913	26.97	20.76
FD7	59097.4	316	195.5	48.9	65.7		0	0.110	0.111	7.3	10.8	0.924	0.932	27.49	19.43

Table A11. Impulse Drying for Case A1 on the X2 Shoe Press using the Beloit-A roll
(Felt B, 0" pivot, and 6000 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF1	59161.1	71	197.5	53.1	61.2		0	0.132	0.156	33.3	10.3	0.768	0.826	29.60	21.02
WF1	59161.4	71	211.1	52.0	61.0		0	0.074	0.115	44.6	33.0	0.710	0.751	24.34	17.95
WF1	59122.1	144	203.1	51.4	65.7		0	0.188	0.195	3.2	7.2	0.930	0.982	35.69	22.60
WF1	59122.2	144	217.1	54.2	67.0		0	0.195	0.202	4.1	7.4	0.903	0.911	35.21	24.92
WF1	59122.3	144	213.6	54.2	67.2		0	0.189	0.194	9.5	3.1	0.902	0.929	36.09	23.13
WF1	59122.4	144	207.5	51.9	64.6		0	0.218	0.218	5.0	4.1	0.911	0.927	37.25	23.53
WF1	59134.1	202	216.6	54.2	67.3		0	0.206	0.220	4.4	7.7	0.936	0.958	34.78	25.63
WF1	59134.2	202	210.6	53.9	69.1		0	0.200	0.191	8.0	11.5	0.928	0.917	34.85	22.46
WF1	59134.3	202	210.1	52.9	66.9		0	0.194	0.185	4.6	20.5	0.899	0.897	35.39	24.42
WF1	59134.4	202	209.6	52.1	67.1		0	0.194	0.216	15.5	6.9	0.903	0.918	33.06	24.85
WF1	59145.1	254	202.1	52.7	70.4		0	0.161	0.161	14.9	8.7	0.900	0.919	34.80	22.05
WF1	59145.2	254	204.1	51.8	68.3		0	0.179	0.184	14.5	10.9	0.901	0.899	34.15	23.80
WF1	59145.3	254	201.5	52.6	71.0		0	0.167	0.159	12.6	13.8	0.898	0.902	34.99	21.99
WF1	59145.4	254	206.6	53.0	71.7		3	0.080	0.102	53.8	56.9	0.834	0.827	31.08	19.39
WF2	59123.1	144	208.9	53.8	63.8		0	0.238	0.238	9.2	5.9	0.901	0.901	36.55	25.54
WF2	59155.1	177	204.3	51.2	61.9		0	0.217	0.218	8.8	12.4	0.921	0.939	36.49	24.39
WF2	59155.2	177	207.6	50.5	61.3		0	0.197	0.210	7.6	4.8	0.889	0.894	36.58	24.96
WF2	59155.3	177	200.3	52.6	63.7		0	0.191	0.193	11.5	17.1	0.885	0.909	34.80	23.20
WF2	59155.4	177	208.9	51.5	60.6		0	0.215	0.224	9.8	6.3	0.900	0.934	37.34	25.75
WF2	59135.1	202	216.1	51.2	63.2		0	0.240	0.250	8.3	7.2	0.940	0.938	37.65	26.28
WF2	59135.2	202	210.9	49.4	60.2		0	0.198	0.214	10.6	6.1	0.910	0.926	36.42	26.30
WF2	59135.3	202	198.8	52.0	64.3		0	0.222	0.223	10.4	8.5	0.919	0.971	36.81	25.06
WF2	59135.4	202	202.6	53.0	57.3		1	0.075	0.052	37.3	21.2	0.778	0.781	28.86	18.07
WF2	59146.1	254	209.6	54.6	67.8		0	0.172	0.174	9.9	7.5	0.895	0.931	33.88	23.81
WF2	59146.2	254	210.9	52.5	64.4		0	0.144	0.129	6.9	10.1	0.874	0.886	34.69	22.12
WF2	59146.3	254	202.6	51.4	65.1		0	0.177	0.207	9.6	8.7	0.905	0.907	34.89	24.36
WF2	59146.4	254	211.8	52.7	64.5		0	0.166	0.165	8.4	9.1	0.858	0.857	35.04	22.67
WF3	59124.1	144	201.6	51.1	65.1		0	0.211	0.197	3.3	4.6	0.871	0.884	28.53	22.29
WF3	59124.2	144	216.7	51.3	64.1		0	0.239	0.233	4.6	3.0	0.869	0.868	32.36	23.81
WF3	59124.3	144	221.7	54.2	64.5		0	0.232	0.246	3.9	3.3	0.876	0.868	32.46	23.48

Table A11 Continued. Impulse Drying for Case A1 on the X2 Shoe Press using the Beloit-A roll (Felt B, 0" pivot, and 6000 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF3	59157.1	177	212.6	50.8	63.4		0	0.190	0.207	13.2	6.8	0.819	0.814	31.03	22.82
WF3	59157.2	177	205.6	51.2	65.2		0	0.204	0.214	6.9	3.3	0.812	0.832	29.25	22.29
WF3	59157.3	177	211.3	50.8	63.8		0	0.199	0.212	6.0	10.8	0.827	0.857	30.70	22.53
WF3	59157.4	177	204.0	51.3	64.1		0	0.174	0.198	18.4	9.1	0.815	0.862	30.18	22.66
WF3	59136.1	202	212.1	48.5	65.6		0	0.193	0.213	7.3	7.5	0.878	0.905	31.95	24.02
WF3	59136.3	202	219.4	52.7	65.4		2	0.130	0.211	59.2	6.2	0.786	0.890	28.45	22.19
WF3	59147.1	254	213.3	52.2	67.4		0	0.176	0.168	6.8	7.1	0.835	0.802	29.86	20.87
WF3	59147.2	254	218.2	51.2	66.3		3	0.119	0.148	33.6	39.9	0.767	0.760	29.10	20.60
FD5	59159.4	121	207.6	52.5	60.2		0	0.117	0.118	6.8	7.6	0.789	0.801	30.35	16.03
FD5	59125.3	144	213.9	50.9	58.5		0	0.139	0.129	8.6	10.9	0.790	0.784	31.42	16.23
FD5	59125.4	144	208.3	49.5	60.0		3	0.122	0.115	4.1	8.7	0.787	0.769	25.82	18.29
FD5	59137.2	202	200.0	54.3			3	0.048	0.066	14.6	15.2	0.706	0.758	21.60	14.89
FD5	59137.4	202	191.4		63.8		3	0.068	0.072	7.4	6.9	0.726	0.749	27.48	14.80
FD6	59126.4	144	191.9	55.0	66.8		0	0.179	0.186	5.6	7.0	0.826	0.836	29.93	18.42
FD6	59138.1	202	203.8	52.7	68.1		0	0.193	0.187	7.8	9.1	0.862	0.871	26.41	21.64
FD6	59138.2	202	202.1	51.1	66.9		0	0.183	0.187	4.4	5.9	0.848	0.858	29.65	20.12
FD6	59138.3	202	202.3	50.7	66.1		0	0.181	0.159	5.5	19.5	0.842	0.845	26.24	22.39
FD6	59138.4	202	191.0	51.0	67.3		0	0.190	0.189	4.2	5.3	0.876	0.882	30.06	22.64
FD6	59148.1	254	201.8	52.1	69.8		3	0.106	0.081	37.7	33.3	0.845	0.812	24.84	17.19
FD6	59148.2	254	208.5	50.6	69.5		3	0.130	0.121	13.8	30.6	0.856	0.861	24.79	20.80
FD6	59148.3	254	214.4	51.8	68.0		0	0.128	0.144	7.0	5.6	0.845	0.872	28.21	17.30
FD6	59148.4	254	206.1	51.1	69.4		0	0.143	0.161	11.2	10.6	0.866	0.886	27.18	20.33

Table A11 Continued. Impulse Drying for Case A1 on the X2 Shoe Press using the Beloit-A roll (Felt B, 0" pivot, and 6000 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
FD7	59127.3	144	203.8	53.5	63.5		0	0.165	0.174	3.0	6.9	0.850	0.868	28.69	20.50
FD7	59127.4	144	194.8	52.2	63.9		0	0.180	0.184	3.9	6.0	0.856	0.863	29.23	22.05
FD7	59139.1	202	201.8	52.5	65.2		2	0.143	0.117	9.8	23.9	0.883	0.859	27.89	17.88
FD7	59139.2	202	205.1	52.9	63.9		1	0.154	0.150	4.5	8.7	0.872	0.878	31.52	19.53
FD7	59139.3	202	198.7	53.5	66.5		2	0.155	0.163	21.3	5.5	0.886	0.902	29.18	19.06
FD7	59149.1	254	197.5	51.1	66.0		1	0.105	0.115	16.2	13.0	0.853	0.861	26.28	20.44
FD7	59149.2	254	205.1	49.9	66.2		2	0.089	0.108	20.2	14.8	0.823	0.825	24.87	20.49
FD7	59149.3	254	198.5	50.7	66.8		1	0.080	0.092	11.3	13.0	0.819	0.828	26.92	18.36
FD7	59149.4	254	213.3	53.3	68.0		2	0.102	0.081	20.6	13.6	0.826	0.822	28.56	17.73

Table A12. Impulse Drying for Case A2 on the X2 Shoe Press using the Beloit-A roll (Felt B, 0" pivot, and 8500 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF1	59128.1	144	196.5	52.8	65.3		0	0.210	0.204	9.0	9.8	0.918	0.915	37.04	23.13
WF1	59128.2	144	205.3	51.5	65.7		0	0.226	0.234	9.7	2.6	0.911	0.922	36.09	24.28
WF1	59128.3	144	200.3	52.1	65.8		0	0.233	0.232	10.3	7.3	0.914	0.886	37.65	24.47
WF1	59128.4	144	197.7	53.4	67.1		0	0.218	0.222	10.1	7.2	0.893	0.922	34.35	22.09
WF1	59140.1	202	208.0	53.1	67.6		0	0.216	0.228	9.3	9.2	0.923	0.931	35.37	23.29
WF1	59140.2	202	211.3	52.2	68.5		0	0.217	0.254	16.6	8.3	0.909	0.938	34.06	24.74
WF1	59140.3	202	210.8	53.0	68.3		0	0.144	0.205	20.8	17.6	0.849	0.927	30.70	23.07
WF1	59140.4	202	212.1	52.7	67.9		0	0.231	0.228	6.5	15.4	0.929	0.930	35.95	22.52
WF1	59150.1	254	213.9	52.9	68.8		0	0.198	0.216	16.7	9.7	0.912	0.924	33.38	23.85
WF1	59150.2	254	190.9	52.0	71.1		1	0.112	0.155	55.4	41.9	0.846	0.918	30.48	20.97
WF1	59150.3	254	216.4	52.4	69.6		3	0.063	0.077	12.7	36.4	0.770	0.814	26.12	18.52
WF1	59150.4	254	187.5	52.8	69.6		2	0.096	0.120	39.6	29.2	0.846	0.896	30.29	19.94
WF2	59129.1	144	209.8	50.9	62.0		0	0.221	0.224	4.1	5.8	0.919	0.925	37.72	27.56
WF2	59129.2	144	204.0	51.6	62.7		0	0.233	0.242	3.4	5.0	0.917	0.947	36.42	27.47
WF2	59129.3	144	205.8	50.7	61.9		0	0.227	0.216	6.2	4.2	0.915	0.917	38.09	26.04
WF2	59129.4	144	212.1	50.9	63.0		0	0.241	0.242	3.3	3.7	0.917	0.943	38.31	28.09
WF2	59156.1	177	208.5	52.2	59.6		0	0.193	0.211	10.4	9.5	0.883	0.894	36.77	26.16
WF2	59156.2	177	210.4	52.1	61.6		0	0.207	0.211	10.1	15.2	0.866	0.902	37.98	25.49
WF2	59156.3	177	209.4	53.0	64.6		0	0.217	0.233	12.0	5.2	0.890	0.888	35.33	25.23
WF2	59156.4	177	210.6	49.8	60.4		0	0.226	0.243	10.2	7.4	0.868	0.885	38.41	27.62
WF2	59141.1	202	215.6	53.6	65.9		0	0.213	0.223	13.6	9.0	0.883	0.900	37.84	27.08
WF2	59141.2	202	207.6	51.4	63.1		0	0.192	0.203	13.5	7.4	0.867	0.872	35.78	25.19
WF2	59141.3	202	213.9	52.9	64.3		0	0.242	0.217	5.8	7.8	0.883	0.869	36.41	24.01
WF2	59141.4	202	205.1	50.8	63.1		0	0.229	0.214	5.7	11.2	0.873	0.886	38.67	27.30

Table A12 Continued. Impulse Drying for Case A2 on the X2 Shoe Press using the Beloit-A roll (Felt B, 0" pivot, and 8500 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF2	59151.1	254	200.8	50.9	65.2		0	0.202	0.175	3.5	4.6	0.883	0.883	35.04	23.96
WF2	59151.2	254	209.6	51.2	65.4		0	0.158	0.166	5.1	7.8	0.847	0.851	36.30	24.05
WF2	59151.3	254	209.9	53.3	66.6		0	0.194	0.220	7.2	7.3	0.844	0.883	36.02	25.91
WF2	59151.4	254	209.1	52.9	64.9		1	0.091	0.089	34.1	18.0	0.767	0.777	28.66	21.17
WF3	59130.2	144	205.1	49.9	65.1		0	0.247	0.251	3.2	3.2	0.832	0.844	31.20	23.14
WF3	59130.3	144	220.6	50.0	63.9		0	0.235	0.244	6.0	3.7	0.826	0.842	30.83	22.50
WF3	59130.4	144	216.1	51.2	64.7		0	0.238	0.242	6.3	4.5	0.822	0.846	32.86	23.65
WF3	59158.2	177	204.1	50.9	65.6		0	0.202	0.204	7.4	6.9	0.804	0.821	29.79	23.64
WF3	59158.4	177	211.8	50.4	65.1		0	0.220	0.197	4.5	6.1	0.822	0.819	30.49	23.16
WF3	59142.1	202	207.1	52.6	68.6		0	0.230	0.227	3.5	4.4	0.832	0.833	30.78	24.20
WF3	59142.2	202	217.9	52.1	66.3		3	0.113	0.215	67.3	11.6	0.753	0.829	26.35	22.18
WF3	59142.4	202	209.1	54.5	62.7		0	0.174	0.153	4.6	10.5	0.790	0.800	29.54	20.91
WF3	59152.2	254	201.1	51.0	69.8		3	0.143	0.147	32.2	25.9	0.821	0.818	26.39	20.59
WF3	59152.3	254	218.1	50.6	68.0		0	0.209	0.219	4.3	6.4	0.857	0.857	31.02	22.93
WF3	59152.4	254	215.6	51.6	68.4		3	0.146	0.129	36.3	36.4	0.808	0.810	28.30	21.05
FD5	59160.1	121	208.3	52.6	59.8		0	0.162	0.158	6.8	7.0	0.739	0.746	32.11	17.20
FD5	59160.2	121	210.1	52.6	61.0		0	0.144	0.147	9.0	8.2	0.737	0.738	31.13	17.15
FD5	59160.3	121	187.7	52.8	62.9		0	0.150	0.110	10.0	18.2	0.724	0.814	30.88	15.26
FD5	59160.4	121	213.1	51.3	59.9		0	0.144	0.137	9.0	7.3	0.813	0.817	25.88	21.25
FD5	59131.2	144	210.6	49.8	61.0		2	0.152	0.141	5.9	10.6	0.848	0.845	30.89	18.50
FD5	59131.3	144	197.5	50.3	63.6		3	0.082	0.109	39.0	41.3	0.790	0.828	27.73	15.83

Table A12 Continued. Impulse Drying for Case A2 on the X2 Shoe Press using the Beloit-A roll (Felt B, 0" pivot, and 8500 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
FD6	59132.1	144	204.8	53.8	68.6		0	0.209	0.216	2.4	3.7	0.939	0.957	28.32	24.82
FD6	59132.4	144	210.3	52.6	66.1		0	0.205	0.196	5.9	5.6	0.867	0.850	27.76	22.37
FD6	59143.1	202	202.5	51.9	67.1		0	0.170	0.199	8.2	8.0	0.827	0.833	26.67	23.67
FD6	59143.2	202	209.6	52.1	68.2		0	0.203	0.208	4.9	3.8	0.842	0.845	30.82	19.02
FD6	59143.3	202	208.3	50.6	66.8		0	0.233	0.224	4.3	7.6	0.841	0.846	28.76	24.25
FD6	59143.4	202	208.5	52.2	69.0		0	0.206	0.200	10.7	23.5	0.834	0.829	29.02	19.39
FD6	59153.1	254	210.9	51.6	69.3		1	0.155	0.159	14.8	18.2	0.791	0.788	28.55	17.41
FD6	59153.2	254	204.8	51.7	71.3		1	0.157	0.192	12.1	8.9	0.788	0.801	24.87	21.65
FD6	59153.3	254	198.0	50.3	70.1		1	0.200	0.201	8.0	12.4	0.802	0.792	28.85	23.60
FD6	59153.4	254	205.0	50.3	69.0		2	0.131	0.146	32.1	32.9	0.759	0.755	26.86	21.93
FD7	59133.1	144	198.8	53.2	65.1		0	0.198	0.217	8.1	5.1	0.788	0.795	30.93	20.50
FD7	59133.2	144	206.1	52.0	66.4		0	0.225	0.239	4.9	3.3	0.787	0.800	31.33	24.15
FD7	59133.3	144	209.6	52.3	68.1		0	0.234	0.232	3.4	7.8	0.793	0.792	32.65	21.36
FD7	59133.4	144	203.8	49.4	64.1		0	0.227	0.225	5.7	9.8	0.776	0.778	32.88	21.85
FD7	59144.1	202	197.8	51.4	67.2		0	0.204	0.196	5.4	5.1	0.777	0.772	28.60	23.12
FD7	59144.2	202	191.2	52.5	67.6		3	0.090	0.160	51.1	20.6	0.689	0.776	26.24	18.31
FD7	59144.3	202	199.5	52.4	66.4		0	0.177	0.161	6.2	4.3	0.794	0.786	29.38	19.41
FD7	59144.4	202	204.8	52.5	66.6		3	0.178	0.169	9.0	17.2	0.800	0.804	28.02	19.30
FD7	59154.1	254	200.2	49.9	67.8		3	0.135	0.129	8.9	13.2	0.789	0.790	28.33	20.47
FD7	59154.2	254	197.7	50.9	68.4		1	0.136	0.139	11.0	15.1	0.794	0.795	28.84	19.79
FD7	59154.3	254	196.0	50.1	67.7		1	0.098	0.106	17.3	14.2	0.906	0.895	28.09	20.61
FD7	59154.4	254	195.7	50.9	68.0		1	0.098	0.113	28.6	10.6	0.899	0.898	28.16	20.33

Table A13. Impulse Drying for Case A4 on the X2 Shoe Press using the Beloit-A roll (Felt S, 0" pivot, and 6000 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF1	59292.1	49	207.3	52.2	60.6		0	0.119	0.139	15.1	17.3	0.773	0.775	26.57	19.41
WF1	59292.3	49	203.6	50.2	59.2		0	0.115	0.123	38.3	26.0	0.769	0.739	26.41	17.22
WF1	59292.4	49	196.7	52.0	61.0		0	0.174	0.175	9.2	5.1	0.746	0.748	30.42	21.07
WF1	59292.5	49	189.7	50.8	57.0		0	0.170	0.190	16.5	7.9	0.732	0.738	29.73	21.35
WF1	59168.1	129	187.2	54.0	65.5		0	0.176	0.236	10.8	7.6	0.827	0.853	30.91	23.07
WF1	59168.2	129	209.4	51.7	63.5		0	0.198	0.234	16.7	9.8	0.821	0.855	31.54	23.90
WF1	59168.3	129	218.6	51.4	63.2		0	0.212	0.212	15.1	17.9	0.828	0.841	34.39	22.23
WF1	59168.4	129	197.2	51.7	64.3		0	0.258	0.240	4.7	6.3	0.863	0.866	37.02	21.78
WF1	59180.1	157	215.3	53.2	64.5		0	0.224	0.263	7.6	4.6	0.843	0.877	32.37	22.68
WF1	59180.2	157	202.1	50.9	65.2	Yes	0	0.223	0.225	9.9	6.7	0.816	0.844	34.81	22.44
WF1	59180.3	157	201.0	51.7	66.4		0	0.267	0.271	7.5	3.3	0.855	0.882	34.12	24.29
WF1	59180.4	157	210.9	51.0	63.9	Yes	0	0.268	0.265	4.1	3.4	0.873	0.908	37.79	23.43
WF1	59192.3	210	201.0	50.8	67.2		2	0.229	0.163	10.9	52.8	0.936	0.905	33.43	22.08
WF1	59192.4	210	202.1	50.6	67.0		2	0.067	0.079	26.9	62.0	0.778	0.810	28.78	20.31
WF1	59204.1	210	188.9	51.9	69.2		0	0.265	0.243	6.0	13.6	0.805	0.786	34.05	21.87
WF1	59204.2	210	208.3	51.2	67.4		0	0.247	0.251	5.7	5.6	0.806	0.811	33.23	21.12
WF1	59204.3	210	199.5	50.0	67.4		0	0.306	0.293	4.2	4.1	0.812	0.808	37.15	23.53
WF1	59204.4	210	200.5	50.6	66.7		2	0.280	0.264	3.9	3.8	0.793	0.792	33.42	23.01
WF1	59205.1	232	195.2	51.9	69.2		1	0.164	0.179	37.2	33.0	0.742	0.736	30.71	19.12
WF1	59205.2	232	206.3	51.0	68.1		3	0.078	0.105	10.3	40.0	0.647	0.728	25.06	19.59
WF1	59205.3	232	199.7	51.4	68.2		3	0.075	0.150	6.7	50.0	0.681	0.757	27.10	20.32
WF1	59205.4	232	212.4	50.9	67.1		0	0.304	0.280	3.6	4.3	0.858	0.856	36.07	22.81

Table A13 Continued. Impulse Drying for Case A4 on the X2 Shoe Press using the Beloit-A roll (Felt S, 0" pivot, and 6000 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF2	59293.1	49	216.4	51.3	55.5		0	0.182	0.187	6.0	10.7	0.721	0.736	32.60	21.34
WF2	59293.2	49	207.1	49.3	55.0		0	0.164	0.171	15.9	15.8	0.718	0.713	32.21	20.94
WF2	59293.3	49	209.6	51.6	56.5		0	0.221	0.223	3.6	8.5	0.719	0.717	33.74	21.65
WF2	59293.4	49	198.8	49.2	54.6		0	0.211	0.222	6.6	4.1	0.718	0.740	33.08	22.58
WF2	59169.1	129	202.8	51.4	59.3		0	0.214	0.221	3.7	6.3	0.872	0.885	36.49	25.04
WF2	59169.2	129	208.5	54.1	61.7		0	0.237	0.229	11.0	6.6	0.872	0.889	34.37	23.38
WF2	59169.3	129	200.0	54.1	61.8		0	0.247	0.250	7.3	8.8	0.893	0.905	36.26	23.67
WF2	59181.1	157	196.5	48.8	58.0		0	0.221	0.224	4.1	2.7	0.877	0.895	35.98	25.18
WF2	59181.2	157	199.8	50.4	59.5		0	0.234	0.242	3.8	3.7	0.921	0.928	37.29	23.72
WF2	59181.3	157	208.6	49.4	57.8	Yes	0	0.220	0.225	14.1	5.3	0.871	0.893	33.84	25.04
WF2	59181.4	157	199.7	53.2	61.8		0	0.268	0.240	4.1	4.2	0.908	0.953	35.63	23.40
WF2	59193.1	210	210.1	50.6	63.3		1	0.240	0.225	5.4	8.0	0.946	0.956	34.77	23.81
WF2	59193.2	210	204.0	51.2	63.7		1	0.209	0.204	7.7	7.4	0.921	0.988	35.47	23.97
WF2	59193.3	210	202.0	50.0	61.6		1	0.073	0.085	49.3	35.3	0.824	0.835	26.64	17.15
WF2	59193.4	210	197.2	51.7	62.8		1	0.196	0.189	7.1	9.0	0.940	0.189	33.80	24.32
WF3	59294.1	49	188.0	48.4	58.0		0	0.155	0.151	6.5	11.3	0.717	0.739	26.83	18.99
WF3	59294.2	49	196.7	50.8	58.7		2	0.152	0.132	11.8	25.0	0.733	0.732	26.11	19.25
WF3	59294.3	49	213.4	49.1	57.6		0	0.128	0.114	13.3	12.3	0.730	0.720	25.80	17.38
WF3	59294.4	49	210.3	50.3	58.5		2	0.148	0.182	14.9	3.8	0.732	0.779	26.67	20.76
WF3	59170.1	129	213.3	53.0	62.4	Yes	0	0.194	0.173	10.3	16.2	0.905	0.911	31.40	20.55
WF3	59170.2	129	207.8	49.9	62.7		0	0.179	0.197	5.0	4.6	0.899	0.908	30.39	22.57
WF3	59170.4	129	197.5	49.6	61.9	Yes	0	0.180	0.181	11.1	7.2	0.884	0.900	30.13	22.49
WF3	59182.1	157	221.4	49.6	62.6		0	0.226	0.217	3.1	5.1	0.920	0.949	32.06	23.67
WF3	59182.2	157	204.0	49.3	63.4		0	0.179	0.186	6.7	10.8	0.889	0.926	30.93	23.19
WF3	59182.4	157	202.3	49.3	63.1	Yes	0	0.202	0.193	6.9	6.2	0.921	0.927	31.95	23.93
WF3	59194.1	210	200.8	53.8	67.9		1	0.179	0.174	5.6	11.5	0.951	0.941	31.12	21.35
WF3	59194.2	210	201.8	52.9	65.7		2	0.075	0.066	56.0	59.1	0.792	0.808	27.35	17.81

Table A13 Continued. Impulse Drying for Case A4 on the X2 Shoe Press using the Beloit-A roll (Felt S, 0" pivot, and 6000 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
FD5	59295.1	49	197.0	54.6	58.8		0	0.080	0.089	3.1	5.1	0.688	0.696	26.89	13.91
FD5	59295.4	49	185.4	54.0	59.3		3	0.065	0.093	6.7	10.8	0.645	0.669	16.51	19.30
FD5	59171.1	129	198.2	50.2	60.8		0	0.125	0.125	6.9	6.2	0.730	0.727	29.19	15.89
FD5	59171.2	129	197.7	50.1	60.3		0	0.131	0.139	5.6	11.5	0.727	0.732	30.60	14.92
FD5	59171.3	129	206.6	50.5	59.3		0	0.128	0.121	56.0	59.1	0.719	0.721	29.63	15.14
FD5	59171.4	129	193.5	53.2	61.6		3	0.087	0.122	3.1	5.1	0.694	0.728	24.76	17.37
FD5	59183.1	157	190.7	50.9	62.3		1	0.107	0.118	6.7	10.8	0.720	0.726	27.41	15.99
FD5	59183.2	157	200.2	50.1	60.2		1	0.077	0.090	6.9	6.2	0.684	0.696	23.31	15.92
FD5	59183.3	157	191.5	49.6	62.4	Yes	1	0.125	0.112	5.6	11.5	0.726	0.718	22.33	18.91
FD5	59183.4	157	205.0	51.4	60.2		1	0.094	0.104	56.0	59.1	0.705	0.711	25.44	16.01
FD6	59296.1	49	206.1	52.1	59.6	Yes	0	0.089	0.095	24.7	15.8	0.694	0.710	20.88	16.66
FD6	59296.2	49	200.8	50.8	59.0		0	0.080	0.092	21.3	25.0	0.663	0.687	22.07	14.99
FD6	59296.3	49	204.1	50.8	58.7		0	0.091	0.094	26.4	22.3	0.668	0.691	23.69	13.67
FD6	59296.4	49	205.3	50.2	58.7		0	0.090	0.082	20.0	25.6	0.678	0.685	21.72	16.18
FD6	59172.1	129	200.5	53.3	63.4		0	0.181	0.191	8.8	9.9	0.743	0.756	26.10	21.18
FD6	59172.2	129	205.5	51.0	62.6		0	0.210	0.230	8.1	6.1	0.761	0.785	26.67	21.38
FD6	59172.3	129	195.0	51.8	63.5		0	0.157	0.172	4.5	4.1	0.834	0.860	26.54	21.67
FD6	59172.4	129	210.8	50.5	62.0		0	0.176	0.184	5.0	5.4	0.846	0.854	28.70	19.82
FD6	59184.1	157	199.5	52.4	64.4		0	0.176	0.171	8.5	5.8	0.857	0.869	27.79	20.72
FD6	59184.2	157	206.6	51.0	64.7		0	0.153	0.162	22.9	5.6	0.849	0.868	28.56	18.20
FD6	59184.3	157	199.7	50.6	64.2		0	0.189	0.166	4.2	8.4	0.867	0.857	26.53	22.45
FD6	59184.4	157	201.1	50.7	63.8		0	0.175	0.168	12.6	10.1	0.850	0.863	29.14	18.87
FD6	59196.1	210	203.5	51.6	66.3		0	0.187	0.184	4.8	7.6	0.863	0.879	27.64	22.43
FD6	59196.2	210	206.0	50.9	66.7		0	0.173	0.172	6.9	12.2	0.862	0.872	28.12	22.22
FD6	59196.3	210	209.8	52.0	67.4		2	0.149	0.164	18.8	7.9	0.841	0.855	29.06	18.47
FD6	59196.4	210	211.6	50.8	66.4		0	0.150	0.154	12.0	6.5	0.845	0.858	25.37	20.58

Table A13 Continued. Impulse Drying for Case A4 on the X2 Shoe Press using the Beloit-A roll
(Felt S, 0" pivot, and 6000 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
FD7	59297.1	49	197.5	48.0	56.6		0	0.063	0.108	38.1	7.4	0.649	0.690	21.25	16.91
FD7	59297.2	49	193.7	53.1	59.2		0	0.086	0.111	32.6	16.2	0.683	0.700	20.93	17.32
FD7	59297.3	49	193.0	54.2	58.8		0	0.126	0.116	5.6	11.2	0.698	0.702	24.76	16.82
FD7	59173.1	129	204.8	50.0	60.7		0	0.158	0.144	8.2	9.7	0.810	0.824	28.25	19.65
FD7	59173.2	129	195.3	49.1	60.6		0	0.153	0.163	6.5	2.5	0.815	0.827	26.34	21.63
FD7	59173.3	129	196.7	51.2	60.8		0	0.152	0.155	5.3	3.9	0.816	0.829	28.32	19.56
FD7	59185.1	157	192.0	49.1	62.3		0	0.182	0.155	6.0	9.0	0.845	0.828	28.66	21.88
FD7	59185.2	157	193.3	48.9	61.3	Yes	0	0.163	0.176	3.7	4.5	0.824	0.846	30.10	20.53
FD7	59185.3	157	199.3	49.1	62.0		0	0.176	0.172	5.1	8.1	0.835	0.839	29.19	21.30
FD7	59185.4	157	200.2	50.3	61.2		0	0.151	0.157	15.2	7.6	0.798	0.815	26.87	20.89
FD7	59197.1	210	196.5	50.6	64.7		0	0.148	0.126	8.8	17.5	0.819	0.795	27.01	17.85
FD7	59197.2	210	203.0	51.9	65.1		1	0.139	0.125	12.2	35.2	0.792	0.777	26.67	18.06
FD7	59197.3	210	192.0	53.4	65.9		2	0.134	0.131	40.3	28.2	0.759	0.759	26.83	18.11

Table A14. Impulse Drying for Case A5 on the X2 Shoe Press using the Beloit-A roll (Felt S, 0" pivot, and 8500 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF1	59174.1	129	195.3	52.8	66.6		0	0.254	0.259	6.3	4.2	0.857	0.868	34.39	23.77
WF1	59174.2	129	218.2	52.0	65.5		0	0.275	0.271	4.4	4.8	0.887	0.905	34.95	24.24
WF1	59174.3	129	195.8	50.8	65.3		0	0.269	0.268	3.7	3.7	0.874	0.879	36.76	24.05
WF1	59174.4	129	203.0	51.4	65.4		0	0.259	0.267	4.6	5.6	0.881	0.889	35.29	25.83
WF1	59186.1	157	187.7	51.3	66.8		0	0.242	0.243	5.4	6.2	0.886	0.912	38.15	24.60
WF1	59186.2	157	198.5	49.8	66.0		0	0.226	0.245	6.6	3.3	0.938	0.954	38.80	25.97
WF1	59186.3	157	215.8	49.2	65.3		0	0.256	0.269	4.7	3.0	0.949	0.935	38.87	25.98
WF1	59186.4	157	206.5	48.6	65.4	Yes	0	0.255	0.260	4.7	9.6	0.920	0.940	38.41	26.69
WF1	59198.1	210	202.1	51.8	69.0		1	0.224	0.197	13.8	19.8	0.928	0.921	37.45	20.93
WF1	59198.2	210	206.0	51.3	68.9		1	0.194	0.168	16.5	22.6	0.919	0.912	33.57	21.88
WF1	59198.3	210	192.5	50.6	69.1		1	0.153	0.164	23.5	10.4	0.890	0.912	30.57	21.06
WF1	59198.4	210	202.3	51.1	68.9		1	0.226	0.252	11.5	6.3	0.914	0.937	36.06	23.97
WF1	59203.1	210	189.2	51.7	69.4		2	0.116	0.141	60.3	50.4	0.749	0.770	25.87	19.01
WF1	59203.3	210	224.7	50.9	67.8		1	0.196	0.219	23.5	10.0	0.809	0.831	35.87	22.24
WF1	59203.4	210	196.5	50.3	68.9		3	0.088	0.104	50.0	61.5	0.709	0.727	28.63	17.35
WF1	59206.1	232	202.3	53.5	71.8		1	0.166	0.183	10.2	13.7	0.792	0.791	31.61	21.15
WF1	59206.2	232	197.8	50.8	69.6		1	0.139	0.142	29.5	19.0	0.784	0.791	33.41	22.58
WF1	59206.3	232	223.2	50.0	68.0		3	0.086	0.085	27.9	48.2	0.707	0.790	28.99	18.79
WF1	59206.4	232	208.9	51.8	68.8		3	0.069	0.077	10.1	42.9	0.727	0.781	26.39	19.54

Table A14 Continued. Impulse Drying for Case A5 on the X2 Shoe Press using the Beloit-A roll (Felt S, 0" pivot, and 8500 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF2	59299.1	49	193.8	51.0	57.5		0	0.215	0.238	16.7	10.5	0.757	0.775	33.29	23.76
WF2	59299.2	49	199.0	49.7	54.9		0	0.213	0.201	6.1	7.5	0.728	0.745	35.37	23.09
WF2	59299.3	49	204.1	49.3	56.7		0	0.231	0.220	3.5	8.2	0.747	0.774	32.85	23.17
WF2	59299.5	49	194.7	50.1	57.6		0	0.182	0.195	20.9	5.6	0.754	0.777	30.42	20.89
WF2	59175.1	129	200.7	50.4	59.1		0	0.230	0.221	2.6	4.1	0.915	0.916	37.02	25.07
WF2	59175.2	129	206.0	50.3	61.3		0	0.266	0.274	5.3	6.2	0.924	0.921	38.09	27.39
WF2	59175.3	129	202.0	50.2	59.3		0	0.269	0.250	2.6	2.8	0.886	0.875	37.82	25.07
WF2	59175.4	129	201.3	52.3	61.2		1	0.271	0.268	5.2	2.6	0.882	0.883	38.35	26.09
WF2	59187.1	157	205.8	50.0	61.4		0	0.232	0.200	6.9	5.5	0.870	0.847	34.24	22.92
WF2	59187.2	157	212.9	51.0	61.5		0	0.300	0.292	2.3	4.1	0.879	0.886	37.52	26.06
WF2	59187.3	157	192.0	50.3	61.3		0	0.255	0.246	3.9	4.9	0.849	0.869	35.16	25.77
WF2	59187.4	157	211.6	52.6	62.7		0	0.278	0.264	2.9	4.2	0.874	0.864	37.21	23.54
WF2	59199.1	210	207.0	48.8	64.2		2	0.072	0.074	45.8	41.9	0.696	0.721	22.69	15.02
WF2	59199.3	210	204.1	48.3	62.6		1	0.206	0.184	8.7	12.0	0.837	0.837	34.81	22.73
WF2	59199.4	210	206.8	49.6	62.1		2	0.063	0.053	12.7	11.3	0.710	0.696	28.31	15.17
WF3	59300.4	49	208.8	50.4	59.5		1	0.112	0.141	28.6	10.6	0.690	0.728	22.57	20.25
WF3	59176.2	129	202.6	49.5	63.5		0	0.221	0.234	5.4	3.4	0.881	0.886	31.74	22.49
WF3	59176.3	129	218.9	50.2	63.4		0	0.245	0.239	2.0	5.0	0.879	0.889	33.09	23.28
WF3	59176.4	129	209.6	49.6	63.8	Yes	0	0.231	0.219	6.5	18.3	0.864	0.850	29.87	21.94
WF3	59188.2	157	217.7	51.6	64.8		0	0.261	0.235	3.4	6.4	0.893	0.881	33.39	22.94
WF3	59188.3	157	219.6	50.1	64.9		0	0.256	0.259	3.5	3.5	0.896	0.900	33.73	23.53
WF3	59188.4	157	207.6	49.2	64.7		0	0.246	0.224	6.1	5.8	0.898	0.897	33.37	23.18
WF3	59200.1	210	203.5	50.5	66.5		2	0.094	0.086	61.7	46.5	0.789	0.790	26.45	18.44
WF3	59200.2	210	212.1	51.0	66.4		3	0.093	0.082	46.2	39.0	0.787	0.789	28.40	19.32
WF3	59200.3	210	209.9	51.6	66.8		2	0.072	0.096	18.1	54.2	0.756	0.785	24.34	19.03

Table A14 Continued. Impulse Drying for Case A5 on the X2 Shoe Press using the Beloit-A roll (Felt S, 0" pivot, and 8500 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
FD5	59301.1	49	200.7	50.1	58.0		3	0.057	0.059	12.3	18.6	0.709	0.724	18.20	12.86
FD5	59301.2	49	191.9	51.2	59.8		0	0.069	0.080	18.8	20.0	0.752	0.757	17.34	16.77
FD5	59301.3	49	203.6	50.9	58.0	Yes	0	0.078	0.077	15.4	11.7	0.731	0.749	22.78	14.01
FD5	59301.5	49	210.6	52.9	58.3		3	0.070	0.087	7.1	16.1	0.737	0.767	25.05	14.48
FD5	59177.1	129	194.3	49.8	61.0		1	0.073	0.088	13.7	19.3	0.820	0.843	26.59	13.54
FD5	59177.2	129	209.9	49.7	58.4		1	0.072	0.065	13.9	26.2	0.785	0.803	28.08	13.47
FD5	59177.3	129	215.6	49.6	60.0		2	0.098	0.088	8.2	20.5	0.816	0.829	25.08	15.99
FD5	59177.4	129	201.6	51.6	60.3		1	0.064	0.047	12.5	14.9	0.803	0.771	26.38	12.64
FD5	59189.1	157	213.3	50.6	61.4		3	0.042	0.041	9.5	7.3	0.751	0.756	23.80	14.12
FD5	59189.2	157	212.3	50.2	62.1		3	0.115	0.120	30.4	10.0	0.844	0.844	24.73	19.93
FD5	59189.3	157	202.6	49.6	60.7		3	0.043	0.042	11.6	7.1	0.706	0.708	21.44	12.67
FD5	59189.4	157	215.1	50.5	60.1		3	0.044	0.050	13.6	20.0	0.729	0.760	22.00	15.72
FD6	59302.1	49	200.2	51.5	61.0		0	0.059	0.097	15.3	9.3	0.692	0.739	19.12	16.99
FD6	59302.3	49	207.8	49.7	59.2		1	0.098	0.110	22.4	17.3	0.704	0.726	24.84	13.65
FD6	59302.4	49	198.8	50.2	59.2		3	0.073	0.108	19.2	14.8	0.669	0.762	20.77	15.51
FD6	59302.5	49	212.6	50.1	59.2		0	0.064	0.052	23.4	30.8	0.679	0.673	18.89	11.80
FD6	59178.1	129	201.0	53.1	66.1		1	0.156	0.169	15.4	7.1	0.870	0.907	27.65	19.15
FD6	59178.2	129	205.3	50.4	64.3		0	0.200	0.160	5.0	19.4	0.917	0.914	30.94	19.67
FD6	59178.3	129	208.1	49.9	64.6		0	0.208	0.190	4.8	4.2	0.915	0.915	28.63	23.35
FD6	59178.4	129	196.3	50.1	64.9		0	0.245	0.246	5.3	4.9	0.777	0.787	28.13	21.71
FD6	59190.1	157	198.2	52.3	67.1		0	0.233	0.225	6.9	8.4	0.777	0.780	28.24	20.68
FD6	59190.2	157	210.8	49.7	65.5		0	0.211	0.211	8.5	7.6	0.781	0.782	26.07	20.06
FD6	59190.3	157	207.8	51.1	66.7		0	0.241	0.238	6.6	10.5	0.781	0.787	28.28	20.58
FD6	59190.4	157	205.1	50.6	66.7		0	0.258	0.252	1.9	6.7	0.785	0.785	27.36	22.38
FD6	59201.1	210	206.5	51.6	66.6		1	0.126	0.091	33.3	53.8	0.739	0.711	27.94	15.26
FD6	59201.2	210	206.3	49.7	68.5		2	0.133	0.142	42.9	57.7	0.738	0.725	25.63	19.00
FD6	59201.3	210	202.0	51.0	69.3		3	0.071	0.073	21.1	38.4	0.665	0.659	23.43	16.29
FD6	59201.4	210	206.5	49.7	67.7		1	0.199	0.193	7.5	16.1	0.770	0.760	27.40	21.49

Table A14 Continued. Impulse Drying for Case A5 on the X2 Shoe Press using the Beloit-A roll
(Felt S, 0" pivot, and 8500 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m^2	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm^3		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
FD7	59303.1	49	197.5	49.2	58.2		0	0.105	0.114	22.9	8.8	0.719	0.736	23.56	16.95
FD7	59303.2	49	195.8	48.2	57.6	Yes	0	0.079	0.115	19.0	20.9	0.673	0.714	21.48	16.94
FD7	59303.3	49	193.8	48.6	58.0		3	0.081	0.110	17.3	16.4	0.662	0.701	21.60	17.18
FD7	59303.4	49	195.3	48.9	58.3	Yes	0	0.111	0.123	12.6	7.3	0.707	0.711	21.69	18.00
FD7	59303.5	49	193.3	49.2	57.7	Yes	0	0.080	0.084	37.5	19.0	0.659	0.667	21.10	16.11
FD7	59179.1	129	195.0	49.2	62.9		0	0.214	0.197	3.7	6.6	0.744	0.734	29.75	22.42
FD7	59179.2	129	189.7	48.7	62.6	Yes	0	0.241	0.231	5.0	3.5	0.744	0.732	33.31	22.95
FD7	59179.3	129	193.3	49.7	63.1		0	0.226	0.205	3.5	1.5	0.739	0.733	30.78	20.76
FD7	59179.4	129	192.8	52.0	63.3		0	0.235	0.231	1.7	5.2	0.726	0.731	29.43	22.48
FD7	59191.1	157	199.2	51.8	64.8		0	0.162	0.105	24.1	47.6	0.698	0.672	24.48	15.34
FD7	59202.1	210	188.7	49.9	67.2		2	0.094	0.079	39.4	41.8	0.672	0.662	24.65	14.01
FD7	59202.2	210	201.5	49.8	65.9		2	0.048	0.076	31.3	39.5	0.773	0.797	23.51	14.44
FD7	59202.3	210	192.7	50.0	67.7		2	0.051	0.041	27.5	56.1	0.762	0.699	20.93	12.12
FD7	59202.4	210	193.7	50.3	66.4		1	0.099	0.101	28.3	29.7	0.788	0.795	23.48	17.60

Table A15. Impulse Drying for Case A6 on the X2 Shoe Press using the Beloit-A roll
(Felt S, 2" pivot, and 6000 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF1	59207.1	121	196.5	54.9	65.2		0	0.244	0.284	12.3	2.8	0.815	0.827	34.89	24.65
WF1	59207.2	121	191.2	50.9	63.8		0	0.251	0.253	7.2	7.1	0.802	0.799	34.26	23.16
WF1	59207.3	121	200.5	51.4	64.6		0	0.296	0.300	4.7	4.3	0.755	0.793	36.60	25.18
WF1	59207.4	121	209.1	52.5	65.3		0	0.191	0.247	30.4	11.3	0.784	0.822	30.21	22.63
WF1	59213.1	149	214.1	51.5	65.6		0	0.298	0.291	3.4	4.8	0.842	0.838	35.04	23.10
WF1	59213.2	149	215.9	51.9	66.5		0	0.308	0.309	3.2	5.2	0.836	0.847	36.03	24.88
WF1	59213.3	149	203.8	53.5	67.9		0	0.246	0.285	9.3	4.2	0.810	0.825	33.34	24.62
WF1	59213.4	149	205.3	52.1	67.1		0	0.290	0.278	3.8	3.6	0.841	0.852	34.46	23.44
WF1	59219.1	177	202.6	48.7	66.5		1	0.272	0.245	4.0	8.2	0.835	0.840	34.76	24.53
WF1	59219.2	177	191.0	52.4	67.5		0	0.288	0.266	4.5	3.8	0.865	0.877	36.24	22.87
WF1	59219.3	177	213.3	51.9	65.7	Yes	0	0.258	0.246	5.4	6.5	0.931	0.910	35.02	25.13
WF1	59219.4	177	205.1	52.2	67.3	Yes	0	0.225	0.222	19.1	14.9	0.915	0.921	33.93	24.01
WF1	59225.1	199	206.0	53.0	66.7	Yes	1	0.213	0.188	8.5	26.6	0.879	0.889	34.65	23.60
WF1	59225.2	199	206.1	54.6	70.6		1	0.141	0.193	39.7	11.9	0.876	0.891	32.68	23.15
WF1	59225.4	199	209.1	53.2	67.2		1	0.194	0.187	16.0	5.3	0.912	0.933	33.89	23.57
WF2	59208.1	121	205.1	53.4	62.5		0	0.235	0.198	7.7	19.7	0.926	0.885	35.07	22.81
WF2	59214.1	149	206.3	49.9	60.4		0	0.201	0.211	8.5	7.6	0.899	0.907	33.95	25.97
WF2	59214.2	149	203.8	51.0	60.9		0	0.236	0.241	5.1	4.6	0.927	0.935	36.54	25.84
WF2	59214.3	149	210.8	50.8	60.4		0	0.180	0.196	13.3	10.7	0.907	0.909	32.52	23.71
WF2	59214.4	149	199.0	53.0	62.9		0	0.221	0.236	6.8	5.5	0.956	0.957	35.50	25.41
WF2	59220.1	177	206.6	48.1	59.5		1	0.177	0.192	9.6	11.5	0.877	0.915	32.44	24.94
WF2	59220.2	177	198.5	51.3	63.2		1	0.205	0.217	6.3	6.0	0.899	0.912	35.85	24.45
WF2	59220.3	177	207.3	50.6	62.2		1	0.089	0.118	32.6	31.4	0.832	0.875	29.13	22.01
WF2	59220.4	177	202.5	50.2	63.1		1	0.166	0.188	22.3	8.5	0.920	0.924	32.23	24.45
WF2	59226.1	199	213.6	52.2	64.2		1	0.114	0.125	12.3	15.2	0.820	0.809	33.24	21.48
WF2	59226.2	199	210.8	52.5	65.0		1	0.138	0.162	9.4	14.2	0.837	0.829	33.50	22.19
WF2	59226.3	199	206.0	48.9	61.9		1	0.119	0.123	13.4	10.6	0.784	0.791	32.63	20.14
WF2	59226.4	199	203.3	51.9	64.8		1	0.125	0.153	14.4	14.4	0.801	0.811	32.91	23.59

Table A15 Continued. Impulse Drying for Case A6 on the X2 Shoe Press using the Beloit-A roll
(Felt S, 2" pivot, and 6000 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF3	59209.1	121	218.9	51.5	63.1		0	0.255	0.248	2.4	3.2	0.899	0.889	31.31	23.48
WF3	59209.2	121	214.8	51.6	62.6		0	0.263	0.258	3.8	6.2	0.872	0.882	34.01	22.27
WF3	59209.3	121	202.1	51.4	63.4		0	0.255	0.256	2.7	3.5	0.879	0.884	32.18	23.30
WF3	59209.4	121	210.3	51.8	61.1		0	0.261	0.265	3.1	3.0	0.872	0.883	33.22	23.25
WF3	59215.1	149	213.1	50.8	64.1		0	0.253	0.240	4.3	6.3	0.861	0.859	31.29	23.36
WF3	59215.3	149	203.0	50.3	63.6		0	0.196	0.197	4.1	2.5	0.965	0.964	30.57	23.36
WF3	59215.4	149	203.3	51.0	63.8		0	0.220	0.218	4.5	5.0	0.945	0.944	33.17	22.74
WF3	59221.1	177	196.0	49.8	65.5		1	0.200	0.194	4.0	1.5	0.902	0.881	30.22	23.81
WF3	59221.2	177	217.7	48.4	63.0		1	0.197	0.199	5.6	4.5	0.867	0.870	30.89	23.57
WF3	59221.3	177	202.5	49.5	64.8		1	0.205	0.211	5.9	2.4	0.858	0.859	30.09	22.34
WF3	59221.4	177	201.5	49.5	63.6	Yes	1	0.148	0.187	14.9	21.9	0.789	0.823	26.39	20.66
FD5	59210.2	121	200.3	53.8	62.1		0	0.170	0.158	5.3	3.8	0.776	0.764	26.82	20.20
FD5	59210.3	121	189.4	52.2	60.2		0	0.178	0.167	6.7	6.6	0.757	0.745	31.43	16.41
FD5	59216.3	149	189.9	50.8	64.2		1	0.107	0.105	26.2	11.4	0.812	0.826	21.24	18.30
FD5	59216.4	149	212.9	53.7	61.7		1	0.084	0.104	9.5	21.2	0.799	0.820	27.39	15.35
FD5	59222.1	177	195.2	52.2	64.9		1	0.055	0.062	14.5	12.9	0.773	0.782	25.29	14.09
FD5	59222.2	177	186.0	53.0	65.2		1	0.060	0.063	21.7	20.6	0.768	0.809	24.42	14.25
FD5	59222.3	177	207.1	53.2	63.5		1	0.054	0.066	7.4	21.2	0.772	0.778	26.43	13.71
FD6	59211.1	121	205.3	54.1	64.5		0	0.196	0.188	4.1	4.8	0.954	0.939	28.34	21.72
FD6	59211.2	121	196.5	52.7	64.7		0	0.178	0.167	5.6	3.6	0.906	0.927	30.01	18.48
FD6	59211.3	121	199.5	51.2	63.7		0	0.194	0.197	3.6	3.6	0.925	0.916	29.24	19.82
FD6	59211.4	121	204.5	50.1	63.1		0	0.199	0.183	5.5	5.5	0.904	0.904	26.80	21.43
FD6	59217.1	149	193.7	51.6	67.5	Yes	0	0.200	0.201	5.0	4.5	0.913	0.920	26.40	22.73
FD6	59217.2	149	212.4	50.6	64.7		0	0.174	0.177	6.3	9.0	0.871	0.890	29.62	16.71
FD6	59217.3	149	187.9	50.3	66.3		0	0.169	0.184	13.6	9.2	0.885	0.905	28.62	17.92
FD6	59217.4	149	191.4	50.0	66.1	Yes	0	0.201	0.180	2.5	17.8	0.930	0.931	26.65	21.53
FD6	59223.3	177	205.6	53.1	66.0		0	0.184	0.180	6.0	5.0	0.912	0.930	29.27	17.92
FD6	59223.4	177	198.0	53.7	67.2	Yes	1	0.157	0.166	9.6	7.8	0.891	0.908	29.46	17.22

Table A15 Continued. Impulse Drying for Case A6 on the X2 Shoe Press using the Beloit-A roll (Felt S, 2" pivot, and 6000 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
FD6	59227.1	199	209.9	53.3	68.6		1	0.175	0.187	9.7	10.2	0.803	0.805	25.55	21.81
FD6	59227.2	199	209.6	53.5	69.7		1	0.178	0.180	18.0	22.8	0.821	0.825	26.01	21.52
FD6	59227.3	199	212.8	52.4	67.3		1	0.165	0.147	6.7	16.3	0.826	0.827	28.26	16.36
FD6	59227.4	199	199.7	51.7	68.4		1	0.197	0.188	3.6	4.3	0.820	0.820	28.70	20.60
FD7	59212.2	121	204.3	49.5	60.9		0	0.186	0.173	5.4	6.4	0.892	0.882	30.16	19.33
FD7	59212.3	121	200.0	52.1	62.3		0	0.176	0.172	7.4	2.9	0.914	0.925	29.65	18.80
FD7	59218.1	149	197.7	51.1	63.4		0	0.168	0.156	11.3	9.6	0.936	0.934	28.70	18.20
FD7	59218.2	149	194.3	51.6	64.6		0	0.177	0.173	4.0	5.2	0.958	0.956	29.91	20.63
FD7	59218.3	149	206.1	48.3	62.8		0	0.175	0.172	2.9	6.4	0.903	0.907	27.54	22.24
FD7	59218.4	149	194.0	48.3	62.7		0	0.182	0.182	3.3	3.3	0.906	0.908	31.26	22.38
FD7	59224.1	177	202.8	54.2	65.3		1	0.076	0.100	31.6	48.0	0.812	0.820	25.26	16.57
FD7	59224.2	177	195.2	54.8	65.4		1	0.126	0.137	24.6	10.2	0.828	0.824	27.20	19.91
FD7	59224.4	177	205.6	54.5	63.9		1	0.132	0.127	9.1	28.3	0.821	0.813	27.82	17.27

Table A16. Impulse Drying for Case A4F on the X2 Shoe Press using the Beloit-A roll (Felt S, 0" pivot, and 6000 pli at 30 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF1	59228.1	149	219.9	50.8	60.6	Yes	2	0.071	0.056	54.9	12.5	0.677	0.663	24.84	18.20
WF2	59229.1	149	202.5	50.5	57.1		0	0.124	0.144	12.1	17.4	0.778	0.805	31.53	22.33
WF2	59229.2	149	198.0	51.0	59.1		1	0.147	0.168	23.8	18.5	0.762	0.787	34.54	22.81
WF2	59229.3	149	203.1	50.7	56.7		0	0.164	0.164	11.0	16.5	0.764	0.773	33.75	22.87
WF2	59229.4	149	208.1	53.8	60.7		1	0.181	0.209	8.3	8.1	0.779	0.815	34.07	22.91
WF3	59230.1	149	198.5		61.8		1	0.091	0.140	34.1	13.6	0.675	0.741	23.27	18.94
WF3	59230.2	149	224.2	49.8	58.8		1	0.069	0.109	26.1	17.4	0.647	0.700	21.93	17.97
FD5	59231.1	149	196.0	53.2	62.6		1	0.116	0.115	3.4	6.1	0.700	0.694	27.93	13.42
FD5	59231.2	149	208.9	53.9	63.6		1	0.111	0.103	4.5	9.7	0.697	0.693	23.16	17.13
FD5	59231.3	149	205.6	50.9	57.9		1	0.105	0.093	6.7	14.0	0.683	0.680	27.16	13.61
FD5	59231.4	149	211.3	54.3	61.0		1	0.109	0.106	4.6	5.7	0.692	0.693	25.28	16.64
FD6	59232.1	149	197.5	52.6	62.1		1	0.098	0.105	19.4	21.9	0.660	0.674	20.85	18.20
FD6	59232.2	149	213.4	50.2	59.8		1	0.082	0.087	14.6	14.9	0.646	0.772	22.35	15.55
FD7	59233.1	149	192.4	48.6	57.6		1	0.062	0.064	16.1	9.4	0.746	0.763	23.59	15.53

Table A17. Impulse Drying for Case A5F on the X2 Shoe Press using the Beloit-A roll
(Felt S, 0" pivot, and 8500 pli at 30 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF1	59234.1	149	211.8	54.7	63.7	Yes	1	0.126	0.194	23.8	7.7	0.769	0.820	27.13	20.88
WF1	59234.2	149	204.6	51.7	62.7		0	0.144	0.203	20.1	6.4	0.761	0.798	30.93	23.16
WF1	59234.3	149	199.7	51.1	62.9	Yes	1	0.209	0.229	7.7	9.2	0.801	0.841	33.18	22.71
WF1	59234.4	149	211.9	52.4	64.0	Yes	1	0.229	0.239	12.7	6.7	0.836	0.873	33.35	22.51
WF1	59240.1	177	210.1	52.6	65.3		1	0.201	0.219	12.4	15.1	0.780	0.811	33.38	23.38
WF1	59240.2	177	204.1	51.6	65.4		1	0.225	0.228	7.1	3.1	0.857	0.870	34.41	23.72
WF1	59240.3	177	201.5	51.2	65.7	Yes	1	0.215	0.233	11.2	5.6	0.865	0.865	35.97	22.44
WF1	59240.4	177	210.4	53.3	63.1		1	0.213	0.227	8.0	5.3	0.796	0.802	36.35	22.87
WF1	59246.1	199	215.1	51.7	66.7		2	0.070	0.211	35.7	18.0	0.709	0.818	26.86	21.40
WF1	59246.2	199	197.3	51.6	67.0		1	0.147	0.130	33.3	42.3	0.774	0.771	27.83	21.27
WF1	59246.3	199	207.5	52.1	66.6		0	0.232	0.229	5.6	8.3	0.774	0.793	36.56	24.53
WF1	59246.4	199	201.0	52.8	65.4		0	0.219	0.234	5.9	12.0	0.763	0.775	36.92	22.97
WF2	59235.1	149	206.1	51.0	60.5		1	0.218	0.225	6.4	6.2	0.786	0.793	33.41	22.78
WF2	59235.2	149	207.6	53.9	61.3		0	0.306	0.302	4.2	2.3	0.829	0.830	36.56	25.35
WF2	59235.3	149	203.3	49.3	59.2		1	0.259	0.243	3.9	6.6	0.796	0.801	35.27	24.01
WF2	59235.4	149	210.4	52.8	61.9		1	0.264	0.271	6.8	4.8	0.802	0.839	34.34	22.88
WF2	59241.1	177	195.8	51.3	61.8		1	0.251	0.241	7.2	5.8	0.833	0.851	34.17	23.92
WF2	59241.2	177	211.6	52.6	62.5		1	0.258	0.261	3.5	4.6	0.817	0.825	35.39	23.93
WF2	59241.3	177	204.6	49.9	60.1		1	0.105	0.108	23.8	30.6	0.750	0.781	28.18	19.18
WF2	59241.4	177	197.8	51.3	61.4		1	0.271	0.235	4.4	11.5	0.846	0.816	37.48	23.56
WF2	59247.1	199	203.3	51.7	62.0		1	0.223	0.214	8.1	5.1	0.811	0.797	35.64	23.13
WF2	59247.2	199	211.4	50.9	60.9		1	0.084	0.072	40.5	30.6	0.701	0.699	27.59	16.91
WF2	59247.3	199	205.5	52.6	64.2		1	0.201	0.200	16.4	14.0	0.797	0.784	32.95	22.02
WF2	59247.4	199	209.8	49.8	60.0		1	0.147	0.106	14.3	33.0	0.755	0.714	30.98	18.08
WF3	59236.3	149	204.8	49.9	63.6		0	0.225	0.213	1.8	8.5	0.828	0.847	30.16	22.42
WF3	59236.4	149	207.1	50.7	63.6		0	0.231	0.231	3.9	6.1	0.825	0.847	32.29	21.60
WF3	59242.1	177	198.0	50.0	64.0		1	0.168	0.217	41.7	6.5	0.776	0.801	27.68	22.37
WF3	59242.2	177	203.0	49.3	61.2		1	0.233	0.225	3.4	4.9	0.807	0.807	31.83	22.75
WF3	59242.3	177	199.0	50.7	64.4		1	0.225	0.206	3.6	10.2	0.788	0.785	31.11	22.69
WF3	59242.4	177	210.6	50.7	62.3		1	0.217	0.215	4.6	5.6	0.769	0.776	32.85	22.08

Table A17 Continued. Impulse Drying for Case A5F on the X2 Shoe Press using the Beloit-A roll (Felt S, 0" pivot, and 8500 pli at 30 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
FD5	59237.1	149	204.8	51.8	62.4		3	0.053	0.052	13.2	23.1	0.647	0.645	22.91	12.02
FD5	59237.2	149	226.4	51.3	60.9		3	0.057	0.053	7.0	11.3	0.610	0.599	22.31	11.81
FD5	59237.3	149	202.8	51.1	63.2		3	0.064	0.094	18.8	22.3	0.683	0.707	19.43	16.42
FD5	59237.4	149	208.5	52.6	62.4		3	0.047	0.050	4.3	14.0	0.643	0.660	21.70	12.21
FD5	59243.1	177	209.1	50.8	64.6		3	0.063	0.066	12.7	21.2	0.668	0.673	19.81	16.95
FD5	59243.2	177	202.6	50.8	63.3		3	0.055	0.058	9.1	13.8	0.648	0.664	17.86	16.34
FD5	59243.3	177	204.3	51.8	62.8		3	0.054	0.053	9.3	9.4	0.629	0.653	24.09	12.40
FD5	59243.4	177	213.9	52.0	62.5		3	0.045	0.044	6.7	13.6	0.622	0.625	20.19	13.42
FD6	59238.1	149	198.8	56.5	66.8		1	0.179	0.144	16.2	20.1	0.745	0.729	24.40	20.69
FD6	59238.2	149	210.4	54.8	65.9		0	0.194	0.181	8.8	6.1	0.772	0.783	27.28	21.25
FD6	59238.3	149	220.6	54.2	65.3		0	0.148	0.149	6.1	8.1	0.885	0.902	25.88	19.79
FD6	59238.4	149	197.0	53.8	66.3		1	0.163	0.157	5.5	8.3	0.883	0.866	24.60	21.08
FD6	59244.1	177	208.6	55.0	67.5		1	0.175	0.144	5.1	11.8	0.866	0.871	25.73	20.97
FD6	59244.2	177	226.4	55.3			1	0.155	0.151	10.3	7.3	0.840	0.858	26.70	20.14
FD6	59244.3	177	201.3	54.6	68.1		1	0.170	0.166	10.0	6.6	0.864	0.873	27.54	20.33
FD6	59244.4	177	211.4	51.6	63.6		1	0.144	0.134	12.5	13.4	0.829	0.841	26.64	18.88
FD6	59248.1	199	205.8	52.7	65.7		0	0.158	0.156	4.4	5.1	0.868	0.866	27.98	19.39
FD6	59248.2	199	209.9	51.9	66.8		2	0.156	0.133	7.1	21.1	0.867	0.859	28.76	17.89
FD6	59248.3	199	206.5	51.5	66.2		2	0.162	0.127	3.1	22.0	0.865	0.853	26.28	20.33
FD6	59248.4	199	204.1	52.3	67.1		1	0.131	0.153	25.2	11.8	0.835	0.872	23.94	20.37

Table A17 Continued. Impulse Drying for Case A5F on the X2 Shoe Press using the Beloit-A roll
(Felt S, 0" pivot, and 8500 pli at 30 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m^2	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm^3		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
FD7	59239.1	149	198.3	50.3	62.7		0	0.157	0.139	3.8	5.8	0.862	0.866	28.09	20.03
FD7	59239.2	149	194.5	49.7	62.3		0	0.154	0.120	5.8	27.5	0.853	0.820	29.45	17.86
FD7	59239.3	149	197.3	51.5	63.3		0	0.139	0.128	11.5	17.2	0.843	0.830	24.67	18.51
FD7	59239.4	149	203.0	50.3	61.7		0	0.152	0.141	5.3	4.3	0.856	0.851	27.50	19.34
FD7	59245.1	177	202.8	52.1	64.0		2	0.102	0.079	23.5	34.2	0.810	0.799	25.41	17.02
FD7	59245.2	177	200.5	51.2	64.4		1	0.111	0.112	11.7	15.2	0.827	0.838	26.72	17.60
FD7	59245.3	177	201.6	51.5	64.3		1	0.108	0.103	20.4	20.4	0.816	0.802	22.97	15.87
FD7	59245.4	177	199.5	52.3	64.6		2	0.102	0.102	16.7	30.4	0.813	0.823	24.40	16.85
FD7	59249.1	199	203.5	53.8	65.4		3	0.058	0.034	22.4	29.4	0.689	0.622	21.22	11.69
FD7	59249.3	199	198.8	55.8	67.4		3	0.047	0.036	10.6	27.8	0.661	0.622	19.94	10.38
FD7	59249.4	199	199.5	56.8	66.9		3	0.055	0.065	20.0	35.4	0.696	0.699	22.57	15.36

Table A18. Impulse Drying for Case A4H on the X2 Shoe Press using the Beloit-A roll
(Felt S, 0" pivot, and 6000 pli at 40 ms using hard felt wash water)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF1	59250.1	149	210.1	51.1	62.7		0	0.148	0.178	15.5	19.7	0.717	0.728	32.65	22.24
WF1	59250.2	149	197.2	51.6	64.9		0	0.214	0.202	6.1	8.4	0.739	0.741	36.24	21.59
WF1	59250.3	149	200.7	51.2	64.2		0	0.221	0.254	6.8	7.5	0.753	0.770	35.21	24.33
WF1	59250.4	149	202.0	52.1	65.1		0	0.169	0.194	25.4	17.0	0.731	0.756	30.69	19.88
WF1	59262.2	177	200.2	52.7	68.4		0	0.256	0.204	5.5	17.2	0.782	0.757	34.11	21.09
WF1	59262.3	177	198.5	51.8	68.0		0	0.262	0.279	4.6	6.1	0.762	0.767	35.24	23.95
WF1	59262.4	177	199.2	51.3	66.6		0	0.276	0.283	6.2	2.1	0.794	0.791	36.70	24.32
WF2	59251.1	149	209.6	51.7	61.9		0	0.285	0.281	2.8	2.8	0.775	0.779	34.94	24.26
WF2	59251.2	149	197.2	50.0	60.3		0	0.289	0.288	1.7	3.5	0.777	0.785	36.58	24.77
WF2	59251.3	149	205.0	48.9	58.7		0	0.264	0.250	2.7	5.2	0.770	0.773	35.30	24.45
WF2	59251.4	149	207.5	53.3	62.5		0	0.249	0.251	3.2	3.6	0.762	0.763	31.96	22.29
WF2	59263.1	177	205.8	53.2	64.0		0	0.298	0.296	3.0	3.7	0.794	0.788	37.34	25.52
WF2	59263.2	177	206.5	51.6	62.3		1	0.206	0.203	11.7	10.3	0.742	0.746	34.61	22.61
WF2	59263.3	177	214.1	54.2	66.2		0	0.273	0.274	4.8	2.6	0.769	0.783	35.79	23.71
WF2	59263.4	177	218.9	51.3	62.2		0	0.285	0.293	3.9	3.4	0.768	0.776	36.29	26.06
WF3	59252.1	149	200.0	51.5	64.1		0	0.208	0.201	5.8	7.0	0.748	0.750	27.13	20.28
WF3	59252.2	149	199.3	48.8	61.6		0	0.161	0.181	9.3	8.3	0.713	0.740	30.73	20.54
WF3	59252.3	149	215.3	50.4	62.9		0	0.210	0.212	7.1	6.1	0.751	0.759	30.42	22.43
WF3	59252.4	149	210.8	52.5	63.5		0	0.209	0.211	4.8	6.6	0.889	0.878	33.08	23.19
WF3	59264.1	177	223.7	51.2	64.3		0	0.210	0.218	5.7	5.0	0.874	0.863	30.46	22.96
WF3	59264.2	177	224.2	51.7	65.5		1	0.211	0.215	6.2	5.1	0.863	0.869	30.62	22.73
WF3	59264.3	177	197.2	50.1	65.2		1	0.203	0.195	4.4	11.3	0.856	0.865	27.23	21.71
WF3	59264.4	177	210.6	50.4	64.3		2	0.067	0.080	47.8	76.3	0.705	0.723	23.38	15.97
FD5	59253.1	149	208.9	50.9	60.1		2	0.077	0.063	10.4	23.8	0.718	0.700	25.81	11.88
FD5	59253.2	149	195.8	50.7	63.2		2	0.085	0.064	17.6	15.6	0.731	0.699	19.39	15.90
FD5	59253.3	149	189.2	50.9	62.6		1	0.105	0.080	8.6	15.0	0.736	0.721	26.43	12.96
FD5	59253.4	149	208.8	51.8	61.5		1	0.084	0.071	9.5	9.9	0.713	0.701	22.94	15.54

Table A18 Continued. Impulse Drying for Case A4H on the X2 Shoe Press using the Beloit-A roll
(Felt S, 0" pivot, and 6000 pli at 40 ms using hard felt wash water)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
FD6	59254.1	149	199.8	51.2	64.8		0	0.153	0.152	16.3	11.8	0.766	0.779	23.52	18.88
FD6	59254.2	149	204.6	51.5	64.4		0	0.156	0.159	14.1	13.2	0.771	0.775	27.63	16.01
FD6	59254.3	149	203.5	49.8	63.1		0	0.167	0.165	3.6	9.7	0.764	0.759	25.71	19.95
FD6	59254.4	149	207.3	51.7	65.2		0	0.136	0.143	19.9	13.3	0.749	0.762	23.00	19.24
FD6	59265.1	177	209.6	51.3	65.8		0	0.203	0.200	3.0	5.5	0.786	0.800	30.70	19.32
FD6	59265.2	177	205.3	51.7	67.4		0	0.205	0.204	2.9	3.4	0.792	0.795	27.02	23.36
FD6	59265.3	177	208.8	51.9	66.8		0	0.206	0.204	3.4	2.9	0.812	0.817	30.97	18.72
FD6	59265.4	177	205.6	51.0	65.8		0	0.203	0.204	2.0	5.9	0.794	0.803	27.79	23.35
FD6	59272.1	199	197.3	51.2	67.5		2	0.072	0.093	45.8	60.2	0.714	0.725	23.39	18.34
FD6	59272.2	199	200.8	51.2	67.0		2	0.060	0.059	10.0	15.3	0.687	0.712	25.90	15.06
FD6	59272.3	199	201.1	51.8	69.6		2	0.154	0.158	11.7	13.9	0.792	0.779	26.79	19.20
FD7	59255.1	149	197.2	51.7	63.0		0	0.154	0.155	3.2	4.5	0.803	0.809	27.89	19.47
FD7	59255.2	149	192.0	51.8	61.9		0	0.147	0.159	5.4	5.0	0.792	0.805	28.22	19.20
FD7	59255.3	149	195.5	51.5	62.1		0	0.165	0.166	3.6	3.6	0.801	0.808	26.70	20.25
FD7	59255.4	149	199.3	52.6	63.0		0	0.151	0.144	14.6	10.4	0.806	0.807	25.31	17.54
FD7	59266.1	177	202.5	51.5	65.5		2		0.113	#DIV	49.6		0.766	27.77	20.04
FD7	59266.2	177	212.3	51.7	64.4		0	0.149	0.114	6.7	21.9	0.800	0.782	28.53	16.56
FD7	59266.3	177	208.3	52.1	65.4		1	0.111	0.108	24.3	22.2	0.753	0.742	26.93	15.59
FD7	59266.4	177	191.5	49.5	61.9		1	0.142	0.157	21.1	7.0	0.776	0.785	28.41	19.82

Table A19. Impulse Drying for Case A5H on the X2 Shoe Press using the Beloit-A roll
(Felt S, 0" pivot, and 8500 pli at 40 ms using hard felt wash water)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF1	59256.1	149	191.5	52.5	67.9		0	0.269	0.260	3.7	4.6	0.852	0.858	37.36	24.60
WF1	59256.2	149	216.3	50.6	65.7		0	0.280	0.291	5.7	2.1	0.856	0.849	37.36	26.54
WF1	59256.3	149	219.7	51.5	66.7		0	0.274	0.260	4.0	9.2	0.854	0.851	38.45	24.32
WF1	59256.4	149	200.5	52.2	67.9		0	0.267	0.262	3.0	1.9	0.851	0.861	35.08	22.90
WF1	59267.2	177	204.5	51.7	68.8		0	0.274	0.251	6.2	25.5	0.842	0.838	36.97	25.96
WF1	59267.3	177	208.5	51.3	67.4		0	0.276	0.282	4.3	6.0	0.843	0.828	38.61	25.26
WF2	59257.3	149	211.9	53.6	63.3		0	0.231	0.216	6.9	10.6	0.802	0.812	36.16	24.84
WF2	59257.4	149	210.1	54.0	64.3		0	0.278	0.271	3.6	6.6	0.916	0.896	39.44	26.01
WF2	59268.1	177	209.6	51.4	62.2		1	0.188	0.174	6.9	13.8	0.854	0.818	34.90	22.46
WF2	59268.2	177	199.3	51.6	64.0		0	0.267	0.261	2.6	3.8	0.871	0.856	36.60	24.84
WF2	59268.3	177	202.5	48.0	60.0		0	0.195	0.183	7.7	21.3	0.818	0.811	34.47	23.80
WF2	59268.4	177	197.2	51.1	63.5		0	0.289	0.276	4.8	4.0	0.836	0.843	39.01	26.27
WF3	59258.1	149	208.5	50.9	65.3		0	0.252	0.247	5.2	6.1	0.817	0.816	31.65	23.50
WF3	59258.2	149	212.4	50.9	64.5		0	0.260	0.258	3.8	2.7	0.818	0.814	32.24	23.54
WF3	59258.3	149	202.8	51.3	65.6		0	0.260	0.259	1.5	3.5	0.806	0.795	32.62	24.42
WF3	59258.4	149	223.4	52.4	65.0		0	0.265	0.266	2.6	4.1	0.804	0.788	32.91	23.32
WF3	59269.1	177	213.3	51.2	65.4		2	0.201	0.180	23.4	43.3	0.766	0.764	29.44	21.34
WF3	59269.2	177	217.4	51.5	65.6		2	0.062	0.149	22.6	53.0	0.667	0.765	25.40	20.43
WF3	59269.3	177	206.3	50.5	65.8		1	0.243	0.252	4.9	3.2	0.796	0.803	30.73	23.37
WF3	59269.4	177	200.0	51.2	65.7		1	0.152	0.182	27.6	22.5	0.746	0.757	30.29	20.05
FD5	59259.1	149	199.5	50.5	60.8		3	0.066	0.098	18.2	30.6	0.653	0.684	24.87	13.70
FD5	59259.3	149	217.7	50.3	61.7		3	0.071	0.079	8.5	12.7	0.672	0.689	23.71	15.80
FD5	59259.4	149	204.1	51.9	63.6		2	0.066	0.067	22.7	35.8	0.676	0.677	25.18	11.91
FD6	59260.1	149	210.1	54.4	70.9		0	0.220	0.211	4.1	9.0	0.787	0.788	29.70	21.98
FD6	59260.2	149	218.2	52.5	68.9		0	0.231	0.232	5.2	2.2	0.791	0.795	27.80	23.78
FD6	59260.3	149	218.7	53.0	68.6		0	0.200	0.197	4.5	5.1	0.840	0.842	32.91	18.48
FD6	59260.4	149	200.7	50.6	65.9		0	0.212	0.215	3.8	3.7	0.833	0.844	28.65	23.00

Table A19 Continued. Impulse Drying for Case A5H on the X2 Shoe Press using the Beloit-A roll
(Felt S, 0" pivot, and 8500 pli at 40 ms using hard felt wash water)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m^2	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm^3		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
FD6	59270.1	177	198.2	51.7	66.7		0	0.208	0.197	6.7	4.6	0.837	0.831	30.74	19.36
FD6	59270.2	177	205.5	50.9	67.1		0	0.213	0.217	1.9	4.1	0.822	0.823	28.37	24.06
FD6	59270.3	177	204.3	50.6	66.3		0	0.178	0.175	4.5	5.7	0.927	0.925	31.44	19.71
FD6	59270.4	177	195.8	51.3	68.6		0	0.182	0.178	8.2	4.5	0.930	0.932	27.54	24.24
FD6	59273.1	199	198.3	50.8	67.7		2	0.081	0.096	53.1	40.6	0.815	0.834	22.53	17.95
FD6	59273.2	199	207.3	51.4	68.6		2	0.084	0.123	53.6	27.6	0.817	0.863	26.59	17.02
FD6	59273.3	199	197.0	50.9	67.8		2	0.087	0.063	39.1	50.8	0.784	0.805	26.87	16.54
FD7	59261.1	149	206.8	52.4	66.0		0	0.161	0.160	5.6	6.9	0.888	0.889	29.28	20.98
FD7	59261.2	149	202.6	52.4	66.2		0	0.151	0.112	7.3	18.8	0.888	0.886	29.05	18.55
FD7	59261.3	149	197.0	51.4	65.3		0	0.171	0.161	2.9	5.6	0.925	0.916	29.70	23.29
FD7	59261.4	149	192.2	50.5	62.9		0	0.162	0.161	5.6	5.0	0.918	0.922	30.79	20.11
FD7	59271.1	177	198.8	50.9	65.3		2	0.096	0.121	49.0	41.3	0.854	0.876	25.92	20.97
FD7	59271.2	177	200.7	50.4	65.0		2	0.092	0.124	45.7	20.2	0.836	0.893	28.20	19.73
FD7	59271.3	177	191.9	49.1	62.9		2	0.125	0.132	34.4	18.2	0.870	0.878	28.05	19.67
FD7	59271.4	177	200.0	50.6	66.2		2	0.110	0.085	38.2	44.7	0.853	0.829	26.18	17.91

APPENDIX B

The following tables contain data that was rejected from analysis because either the basis weight or ingoing solids were outside of acceptable limits.

Table B1. Rejected Control Samples that were Finish Dried without Pressing

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF1	59162.1	70	195.7	56.5				0.059	0.051	8.5	9.8	0.439	0.439	20.01	11.12
WF1	59162.2	70	228.7	55.1				0.060	0.056	6.7	7.1	0.445	0.441	22.24	12.05
WF3	59164.1	70	232.2	48.7				0.064	0.058	6.3	6.9	0.480	0.476	18.02	12.65

Table B2. Rejected Data for Double Felted Pressing for Case D1 on the X2 Shoe Press
(Felt B and the 0" pivot, and 6000 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF2	59105.1	49	218.4	55.2	59.0			0.215	0.212	12.1	10.4	0.793	0.778	34.93	22.57
WF3	59106.1	49	209.3	57.1	63.0			0.193	0.172	16.1	11.6	0.839	0.808	30.30	21.07
FD6	59108.2	49	179.7	50.6	60.3			0.139	0.135	5.8	3.7	0.803	0.798	25.29	19.28
FD7	59109.2	49	191.2	45.9	58.4			0.135	0.146	5.9	9.6	0.752	0.778	29.47	19.08
FD7	59109.3	49	200.2	46.8	57.0			0.136	0.125	6.6	14.4	0.786	0.791	28.09	18.97
FD7	59109.4	49	198.2	46.8	58.6			0.122	0.123	9.8	13.0	0.767	0.787	24.31	19.74

Table B3. Rejected Data for Double Felted Pressing for Case D2 on the X2 Shoe Press
(Felt B and the 0" pivot, and 8500 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF1	59110.3	66	225.5	51.9	61.4			0.218	0.197	14.2	14.7	0.854	0.848	34.61	21.67
WF1	59110.4	66	219.2	55.6	64.2			0.245	0.233	7.3	6.0	0.857	0.829	37.27	23.93
WF2	59111.3	66	220.1	55.9	63.1			0.228	0.203	3.5	6.9	0.833	0.848	33.26	20.04
WF3	59112.3	66	250.4	51.2	61.1			0.240	0.230	12.1	14.3	0.887	0.894	32.31	23.24

Table B4. Rejected Data for Double Felted Pressing for Case D3 on the X2 Shoe Press
(Felt B and the 2" pivot, and 6000 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF1	59116.4	66	210.0	55.2	58.8			0.127	0.101	23.6	24.8	0.772	0.765	29.32	17.30
WF3	59118.1	66	231.5	52.0	61.2			0.167	0.232	31.7	4.3	0.817	0.886	28.18	23.30
WF3	59118.3	66	229.5	48.2	59.3			0.234	0.224	10.3	12.9	0.898	0.884	31.11	22.56

Table B5. Rejected Data for Double Felted Pressing for Case D4 on the X2 Shoe Press
(Felt S and the 0" pivot, and 6000 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF3	59276.4	49	246.8	50.9	59.6			0.231	0.226	3.5	2.2	0.805	0.806	29.49	22.10
FD5	59277.2	49	181.2	52.8	58.3			0.118	0.117	9.3	5.1	0.695	0.695	29.09	14.99
FD5	59277.4	49	214.1	56.0	59.9			0.124	0.118	5.6	3.4	0.705	0.701	28.95	14.35

Table B6. Rejected Data for Double Felted Pressing for Case D5 on the X2 Shoe Press
(Felt S and the 0" pivot, and 8500 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF3	59282.3	49	229.7	47.0	58.8			0.223	0.206	4.5	4.9	0.869	0.861	32.92	22.70

Table B7. Rejected Data for Double Felted Pressing for Case D6 on the X2 Shoe Press
(Felt S and the 2" pivot, and 6000 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF3	59288.4	49	227.5	51.6	59.3			0.242	0.255	5.8	4.3	0.816	0.820	33.21	24.29
FD7	59291.1	49	202.6	45.5	57.2			0.188	0.179	6.9	11.2	0.780	0.784	29.69	20.65
FD7	59291.2	49	193.5	46.1	56.2			0.150	0.135	6.7	10.4	0.848	0.836	28.52	19.89
FD7	59291.3	49	183.6	46.9	57.6			0.171	0.174	4.7	6.3	0.855	0.853	29.32	21.46

Table B8. Rejected Data for Impulse Drying for Case C1 on the X2 Shoe Press using the IPST-C Ceramic Roll (Felt B, 0" pivot, and 6000 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF1	59064.1	91	229.0	52.0	62.1		0	0.216	0.231	4.2	4.8	0.868	0.895	35.26	23.61
WF2	59019.3	151	203.3	58.1	61.1		0	0.265	0.265	6.4	3.4	0.905	0.899	36.03	26.25
WF2	59019.4	151	203.5	43.1	52.3		0	0.169	0.200	17.2	14.0	0.790	0.801	32.41	23.72
WF3	59066.3	91	226.5	46.6	58.8		0	0.169	0.156	4.1	7.1	0.844	0.850	31.35	21.92
WF3	59066.4	91	226.2	48.7	60.5		0	0.215	0.218	2.3	3.7	0.893	0.917	32.08	23.06
WF3	59020.2	154	206.5	61.7	65.5		0	0.205	0.202	5.9	6.9	0.895	0.895	29.15	22.46
WF3	59020.3	154	218.1	45.3	59.9		0	0.194	0.166	10.3	12.7	0.848	0.829	30.72	21.60
WF3	59033.1	192	226.2	53.3	63.0		0	0.189	0.204	11.6	8.8	0.880	0.901	30.78	22.37
WF3	59045.3	242	230.2	50.9	64.3		3	0.046	0.069	28.3	10.1	0.739	0.798	24.02	19.62
WF3	59056.1	293	230.4	50.8	63.7		2	0.173	0.174	9.2	12.1	0.754	0.761	28.19	20.90
WF3	59056.2	293	227.9	46.5	61.9		0	0.173	0.181	11.6	8.8	0.741	0.759	27.45	21.13
FD5	59021.2	157	208.0	64.6	66.1		0	0.131	0.115	9.9	6.1	0.895	0.881	28.46	17.31
FD5	59021.3	157	199.0	41.8	57.2		0	0.106	0.111	9.4	8.1	0.823	0.836	23.11	19.16
FD5	59021.4	157	203.5	69.1	69.7		0	0.111	0.117	6.3	9.4	0.907	0.928	26.86	14.80
FD5	59046.1	242	208.0	52.5	60.7		3			#DIV	#DIV/			#DIV/	#DIV
FD5	59046.2	242	206.8	50.7	59.9		3			#DIV	#DIV/			#DIV/	#DIV
FD6	59068.3	91	181.9	50.9	60.6		0	0.110	0.094	21.8	26.6	0.816	0.798	23.16	19.38
FD6	59023.1	164	199.8	60.0	64.1		0	0.138	0.135	5.1	5.9	0.862	0.867	25.11	19.65
FD6	59023.2	164	205.1	55.7	63.9		0	0.131	0.117	9.9	6.8	0.853	0.848	24.83	18.11

Table B9. Rejected Data for Impulse Drying for Case C2 on the X2 Shoe Press using the IPST-C Ceramic Roll (Felt B, 0" pivot, and 8500 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF1	59037.2	194	228.2	51.2	63.5		0	0.248	0.255	6.9	5.1	0.930	0.965	34.28	23.05
WF1	59049.1	243	196.8	47.1	66.2		0	0.198	0.222	28.3	6.3	0.925	0.949	34.96	21.72
WF1	59049.4	243	225.2	51.5	57.8		0	0.075	0.076	9.3	11.8	0.819	0.837	29.32	18.37
WF2	59025.1	158	197.8	55.5	62.8		0	0.229	0.226	6.1	8.8	0.969	0.993	37.81	25.50
WF2	59050.3	243	209.1	48.0	60.1		0	0.216	0.228	6.9	7.5	0.923	0.939	35.68	25.41
WF3	59072.4	91	218.7	46.8	62.3		0	0.228	0.228	4.4	5.3	0.945	0.977	34.53	24.65
WF3	59026.1	153	220.9	56.5	63.0		0	0.241	0.215	3.3	5.1	0.947	0.946	33.19	24.29
FD5	59027.1	151	201.0	58.5	62.8		0	0.099	0.097	7.1	10.3	0.860	0.856	30.04	17.38
FD5	59040.2	196	183.7	51.5	61.4		3	0.083	0.096	47.0	40.6	0.762	0.804	29.42	14.39
FD6	59074.3	91	193.8	44.5	62.1		0	0.174	0.181	5.7	3.3	0.880	0.887	27.96	21.57
FD6	59074.4	91	197.5	56.9	65.2		0	0.189	0.173	6.3	2.9	0.901	0.877	26.81	21.19
FD6	59062.3	295	176.9	49.7	67.6		2	0.105	0.085	30.5	35.3	0.757	0.750	23.28	16.92
FD7	59075.1	91	196.5	56.5	63.6		0	0.159	0.156	4.4	5.8	0.921	0.932	29.55	18.59
FD7	59028.3	151	205.3	48.0	60.1		0	0.181	0.169	8.3	7.7	0.789	0.786	27.20	21.45

Table B10. Rejected Data for Impulse Drying for Case C3 on the X2 Shoe Press using the IPST-C Ceramic Roll (Felt B, 2" pivot, and 6000 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF3	59100.4	91	228.4	52.2	61.4		0	0.223	0.213	5.8	10.8	0.834	0.841	31.98	22.84
WF3	59078.1	148	203.1	55.9	65.4		0	0.230	0.234	3.9	3.8	0.950	0.959	33.13	23.71
FD5	59085.1	200	213.3	56.4	62.2		3	0.169	0.154	5.3	5.8	0.842	0.822	27.52	18.68
FD5	59085.3	200	200.7	58.9	64.8		3	0.157	0.158	8.3	2.5	0.830	0.834	30.06	16.74
FD5	59085.4	200	207.8	56.3	61.9		3	0.139	0.130	5.8	6.2	0.804	0.792	28.70	16.13
FD5	59091.1	247	200.2	56.8	65.4		1	0.139	0.131	5.8	4.6	0.926	0.916	24.91	23.39
FD5	59091.4	247	184.4	53.5	64.3		2	0.104	0.085	8.7	15.3	0.899	0.896	28.96	15.06
FD6	59080.1	146	209.9	55.5	64.1		0	0.150	0.160	8.7	6.9	0.892	0.896	28.64	18.82
FD7	59103.2	91	182.9	49.4	58.7		0	0.150	0.153	6.7	4.6	0.839	0.851	28.65	21.84
FD7	59081.2	145	199.2	55.5	63.8		0	0.152	0.147	4.6	4.8	0.957	0.944	28.70	20.69
FD7	59097.3	316	187.0	47.9	64.8		0	0.097	0.090	14.4	13.3	0.924	0.906	27.06	20.25

Table B11. Rejected Data for Impulse Drying for Case A1 on the X2 Shoe Press using the Beloit-A Roll (Felt B, 0" pivot, and 6000 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF2	59123.2	144	214.3	57.5	63.4		0	0.193	0.223	5.7	6.3	0.838	0.881	34.83	22.68
WF2	59123.3	144	198.7	58.1	64.8		0	0.244	0.207	9.4	10.1	0.886	0.946	33.67	22.85
WF2	59123.4	144	208.1	61.5	65.2		0	0.233	0.226	5.6	5.8	0.937	0.938	37.10	23.90
WF3	59124.4	144	193.7	59.2	65.7		0	0.221	0.224	5.4	5.8	0.833	0.857	31.75	22.38
WF3	59136.2	202	247.3	49.4	64.0		2	0.125	0.178	48.8	32.0	0.839	0.885	27.87	21.41
WF3	59136.4	202	223.9	55.0	66.0		2	0.223	0.148	15.2	54.1	0.933	0.880	31.47	22.07
WF3	59147.3	254	245.6	50.8	65.9		3	0.138	0.096	36.2	35.4	0.770	0.847	26.70	19.00[a]
WF3	59147.4	254	228.4	48.9	65.0		0	0.167	0.169	13.2	10.7	0.880	0.881	28.47	21.05
FD5	59159.1	121	208.5	55.3	60.6		0	0.108	0.103	7.4	6.8	0.799	0.801	29.01	15.70
FD5	59159.2	121	194.0	55.2	62.7		0	0.125	0.131	4.8	4.6	0.814	0.816	31.35	16.50
FD5	59159.3	121	205.5	55.5	62.7		0	0.110	0.112	5.5	8.0	0.793	0.807	23.57	21.07
FD5	59125.1	144	223.4	59.6	64.7		3	0.079	0.064	19.0	17.2	0.766	0.760	24.33	15.47
FD5	59125.2	144	211.8	57.4	69.1		0	0.183	0.167	4.4	7.8	0.861	0.852	27.37	21.17
FD5	59137.1	202	213.8	57.6	64.3		3	0.059	0.061	6.8	8.2	0.745	0.743	27.06	14.16
FD6	59126.1	144	198.2	67.5	59.1		0	0.068	0.075	5.9	8.0	0.751	0.788	18.81	16.27
FD6	59126.2	144	213.1	59.2	66.5		0	0.173	0.160	4.0	7.5	0.830	0.825	29.28	17.88
FD6	59126.3	144	213.3	55.7	65.0		0	0.165	0.173	6.7	10.4	0.824	0.830	26.08	19.29
FD7	59127.1	144	200.3	60.9	67.0		0	0.173	0.173	2.9	4.6	0.897	0.901	28.38	20.49
FD7	59127.2	144	194.5	56.1	65.0		0	0.160	0.155	4.4	5.8	0.870	0.880	28.51	17.93
FD7	59139.4	202	193.5	55.1	66.6		2	0.137	0.133	25.5	24.8	0.861	0.860	27.94	19.25

Table B12. Rejected Data for Impulse Drying for Case A2 on the X2 Shoe Press using the Beloit-A Roll (Felt B, 0" pivot, and 8500 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF3	59130.1	144	227.2	47.0	63.5		0	0.253	0.255	6.7	3.9	0.847	0.837	32.77	24.21
WF3	59158.1	177	240.0	52.2	65.0		0	0.254	0.260	3.5	5.4	0.849	0.856	33.49	23.04
WF3	59158.3	177	232.2	51.3	64.8		0	0.218	0.244	6.4	7.4	0.816	0.837	32.43	22.92
WF3	59142.3	202	225.7	53.5	68.2		0	0.240	0.240	7.5	6.7	0.836	0.833	31.48	22.40
WF3	59152.1	254	235.5	52.4	68.3		0	0.223	0.220	4.5	5.9	0.868	0.881	32.16	22.83
FD5	59131.1	144	215.8	56.5	64.7		3	0.104	0.092	36.5	22.8	0.835	0.826	23.44	19.69
FD5	59131.4	144	235.2	50.3	60.2		3	0.076	0.085	13.2	21.2	0.776	0.805	26.83	15.27
FD6	59132.2	144	226.5	53.9	65.9		0	0.173	0.200	8.7	5.0	0.890	0.893	28.85	22.19
FD6	59132.3	144	207.6	55.4	70.1		0	0.197	0.209	6.1	4.3	0.872	0.880	29.11	22.32

Table B13. Rejected Data for Impulse Drying for Case A4 on the X2 Shoe Press using the Beloit-A Roll (Felt S, 0" pivot, and 6000 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF1	59292.2	49	209.6	57.3	61.8		0	0.073	0.107	20.5	11.2	0.666	0.696		17.55
WF1	59192.1	210	192.7	56.1	68.4		0	0.219	0.138	12.8	52.2	0.897	0.852		19.42
WF1	59192.2	210	228.7	51.2	66.4		3	0.076	0.069	34.2	26.1	0.792	0.815		18.90
WF3	59170.3	129	240.1	50.1	61.8		0	0.176	0.196	4.0	6.1	0.884	0.917		23.41
WF3	59182.3	157	242.0	49.7	62.3		0	0.210	0.214	3.3	4.2	0.925	0.932		23.56
WF3	59194.3	210	225.0	54.5	65.2		2	0.212	0.203	3.3	10.3	0.938	0.901		24.00
WF3	59194.4	210	215.9	56.7	66.6		1	0.205	0.188	7.3	9.6	0.940	0.916	32.58	22.39
FD5	59295.2	49	197.3	55.8	60.0		0	0.096	0.104	10.4	2.9	0.705	0.702		18.91
FD5	59295.3	49	199.0	55.6	59.6		0	0.096	0.083	6.3	13.3	0.696	0.683		12.64
FD5	59195.1	210	216.7	49.7	60.2		3								
FD7	59297.4	49	193.3	55.1	59.3		0	0.088	0.104	12.5	9.6	0.667	0.693	#DIV/	16.94
FD7	59173.4	129	188.0	56.1	62.9		0	0.167	0.160	7.8	7.5	0.839	0.840	#DIV/	20.29
FD7	59197.4	210	196.0	56.8	67.2		2	0.091	0.120	46.2	38.3	0.762	0.786	#DIV/	17.94

Table B14. Rejected Data for Impulse Drying for Case A5 on the X2 Shoe Press using the Beloit-A Roll (Felt S, 0" pivot, and 8500 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF2	59299.4	49	208.8	47.0	56.3		0	0.173	0.168	6.9	8.9	0.691	0.787	31.00	20.99
WF2	59199.2	210	207.8	47.3	61.2		1	0.139	0.144	17.3	11.8	0.784	0.779	32.35	21.79
WF3	59300.1	49	193.8	47.4	55.0		1	0.127	0.146	15.0	16.4	0.733	0.751	26.04	19.80
WF3	59300.2	49	199.0	46.0	53.4		0	0.176	0.186	6.3	6.5	0.773	0.778	30.92	21.92
WF3	59300.3	49	204.1	46.3	54.2		0	0.170	0.170	11.2	6.5	0.754	0.749	29.71	20.77
WF3	59300.5	49	194.7	41.5	47.6		0	0.175	0.159	8.0	10.1	0.734	0.729	27.23	20.02
WF3	59176.1	129	233.7	47.6	61.8		0	0.249	0.254	2.8	3.5	0.861	0.886	32.56	24.47
WF3	59188.1	157	202.1	44.3	64.9		1	0.248	0.233	5.2	5.2	0.902	0.883	33.00	23.53
WF3	59200.4	210	229.4	52.8	66.5		2	0.081	0.131	38.3	52.7	0.786	0.801	27.79	18.47

Table B15. Rejected Data for Impulse Drying for Case A6 on the X2 Shoe Press using the Beloit-A Roll (Felt S, 2" pivot, and 6000 pli at 40 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF1	59225.3	199	229.0	53.2	67.5	Yes	1	0.179	0.142	19.0	38.7	0.840	0.812	30.78	19.66
WF2	59208.2	121	218.7	57.0	63.5		0	0.256	0.249	5.1	2.8	0.949	0.955	38.61	24.49
WF2	59208.3	121	202.6	56.2	62.8		0	0.248	0.244	2.4	2.9	0.981	0.973	37.99	24.14
WF2	59208.4	121	206.6	58.0	62.1		0	0.256	0.259	5.9	5.0	0.974	0.989	36.42	25.57
WF3	59215.2	149	248.3	51.0	62.5		0	0.233	0.250	4.3	3.2	0.850	0.870	29.56	23.23
FD5	59210.1	121	210.1	56.0	60.5		0	0.168	0.172	7.1	8.7	0.785	0.777	30.67	17.03
FD5	59216.1	149	192.2	56.1	64.3		1	0.043	0.047	32.6	29.8	0.752	0.765	19.51	11.40
FD5	59216.2	149	189.2	57.9	66.6		1	0.059	0.094	32.2	33.0	0.778	0.835	17.80	19.29
FD5	59222.4	177	195.5	56.7	61.1		1	0.057	0.066	29.8	74.2	0.780	0.757	19.93	15.29
FD6	59223.1	177	194.2	56.6	66.9	Yes	1	0.155	0.149	11.6	10.1	0.886	0.897	24.16	18.89
FD6	59223.2	177	203.1	55.0	67.4		0	0.184	0.181	9.2	7.2	0.904	0.904	26.85	21.49
FD7	59212.1	121	194.3	45.0	61.6		0	0.179	0.145	6.7	20.0	0.902	0.883	26.65	18.59
FD7	59212.4	121	200.7	61.3	66.3		0	0.196	0.192	8.2	4.7	0.964	0.965	27.75	21.24
FD7	59224.3	177	191.9	55.8	66.7		1	0.105	0.105	35.2	36.2	0.802	0.796	27.30	16.70

Table B16. Rejected Data for Impulse Drying for Case A4F on the X2 Shoe Press using the Beloit-A Roll (Felt S, 0" pivot, and 6000 pli at 30 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF1	59228.3	149	207.8	56.0	62.8	P	2	0.086	0.109	30.2	37.6	0.710	0.767	28.42	18.27
FD6	59232.3	149	182.6	49.0	61.6		1	0.091	0.095	13.2	18.9	0.775	0.787	22.44	17.87
FD6	59232.4	149	203.3	47.8	59.7		1	0.055	0.085	20.0	20.0	0.681	0.773	20.24	16.91
FD7	59233.2	149	202.5	44.5	57.9		1	0.086	0.090	14.0	12.2	0.763	0.781	25.73	16.39
FD7	59233.3	149	201.3	47.0	58.9		1	0.100	0.101	7.0	10.9	0.786	0.782	28.17	17.40
FD7	59233.4	149	192.5	46.9	58.1		1	0.092	0.105	8.7	14.3	0.774	0.796	25.41	19.01

Table B17. Rejected Data for Impulse Drying for Case A5F on the X2 Shoe Press using the Beloit-A Roll (Felt S, 0" pivot, and 8500 pli at 30 ms)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF3	59236.1	149	243.0	50.2	61.5		0	0.200	0.199	5.0	8.0	0.856	0.866	28.99	21.11
WF3	59236.2	149	228.9	47.1	60.4		0	0.203	0.190	4.4	12.1	0.807	0.830	30.86	21.58
FD7	59249.2	199	182.6	55.0	67.4		3	0.053	0.052	5.7	21.2	0.671	0.695	23.08	15.44

Table B18. Rejected Data for Impulse Drying for Case A4H on the X2 Shoe Press using the Beloit-A Roll (Felt S, 0" pivot, and 6000 pli at 40 ms and using normal hard felt wash water)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF1	59262.1	177	235.2	58.4	77.0		0	0.301	0.282	4.0	5.7	0.823	0.836	39.91	25.61
FD6	59272.4	199	183.7	50.8	68.7		2	0.134	0.056	50.0	12.5	0.741	0.670	24.32	16.84

Table B19. Rejected Data for Impulse Drying for Case A5H on the X2 Shoe Press using the Beloit-A Roll (Felt S, 0" pivot, and 8500 pli at 40 ms and using normal hard felt wash water)

Furnish	Sample ID	Roll Temp °C	Basis Weight g/m²	Solids In %	Solids Out %	Surf. Pick	Delam. Code	SEM MN·m/kg		CV SEM %		Density g/cm³		STFI Index N·m/g	
								MD	CD	MD	CD	MD	CD	MD	CD
WF1	59267.1	177	208.8	44.9	60.5		0	0.273	0.277	3.3	4.0	0.851	0.827	36.85	23.58
WF1	59267.4	177	194.2	59.0	70.1		0	0.280	0.268	2.9	4.5	0.844	0.849	39.09	24.59
WF2	59257.1	149	203.8	58.9	65.6		0	0.240	0.242	11.7	5.0	0.832	0.856	34.84	24.65
WF2	59257.2	149	201.8	55.7	65.6		0	0.272	0.220	9.9	22.3	0.837	0.812	36.28	23.42
FD5	59259.2	149	184.7	50.8	64.0		3	0.074	0.087	20.3	25.3	0.667	0.672	25.69	13.51
FD6	59273.4	199	181.7	50.9	69.5		2	0.033	0.042	42.4	26.2	0.625	0.716	16.61	12.78

APPENDIX C

Case C1- SEM and %CV of SEM for Impulse Drying with the IPST-C Ceramic Roll (Felt B, 0 pivot, and 6000 pli)

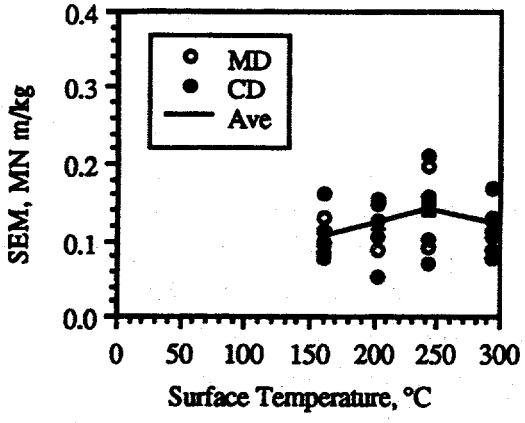

Figure C1. SEM for Furnish WF1.

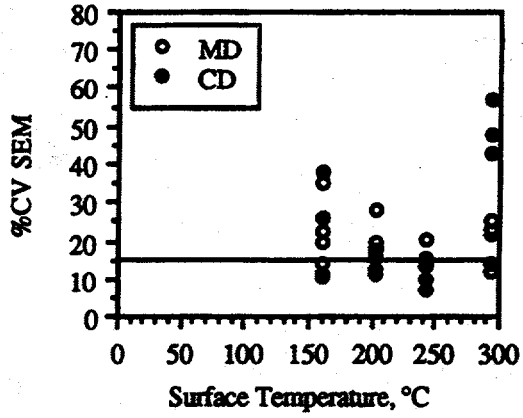

Figure C2. %CV of SEM for Furnish WF1.

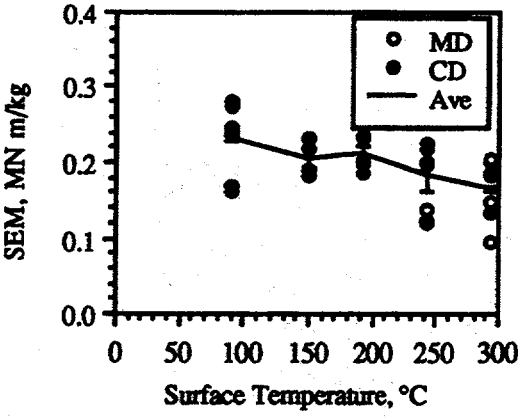

Figure C3. SEM for Furnish WF2.

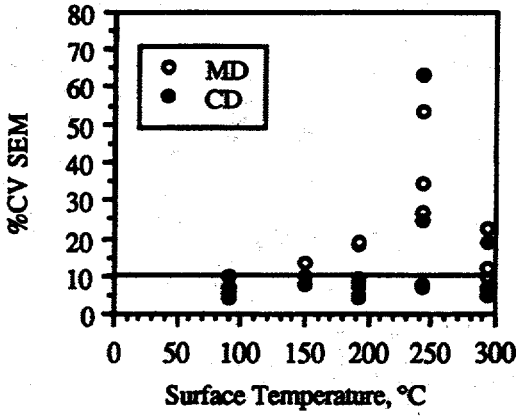

Figure C4. %CV of SEM for Furnish WF2.

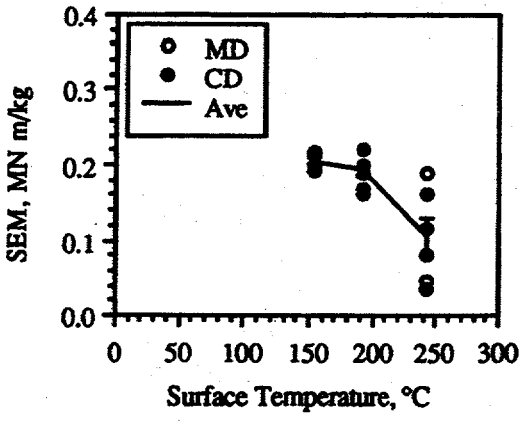

Figure C5. SEM for Furnish WF3.

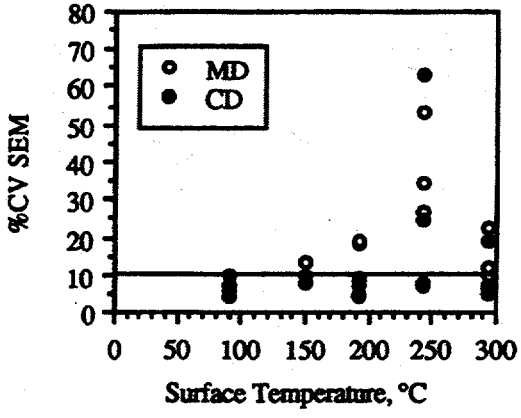

Figure C6. %CV of SEM for Furnish WF3.

Case C1- SEM and %CV of SEM for Impulse Drying with the IPST-C Ceramic Roll
(Felt B, 0 pivot, and 6000 pli)

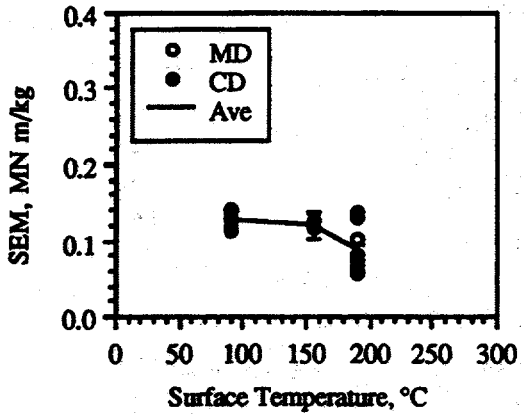

Figure C7. SEM for Furnish FD5.

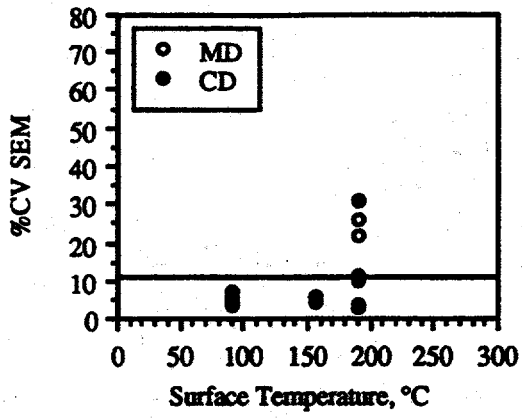

Figure C8. %CV of SEM for Furnish FD5.

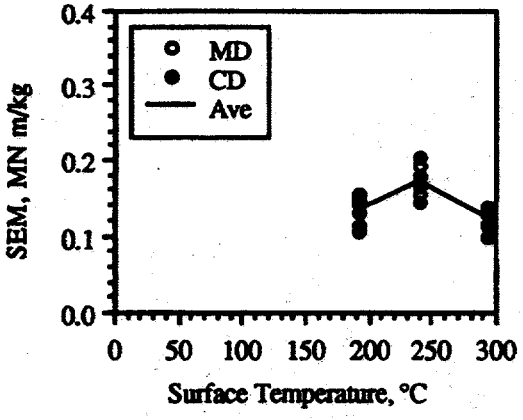

Figure C9. SEM for Furnish FD6.

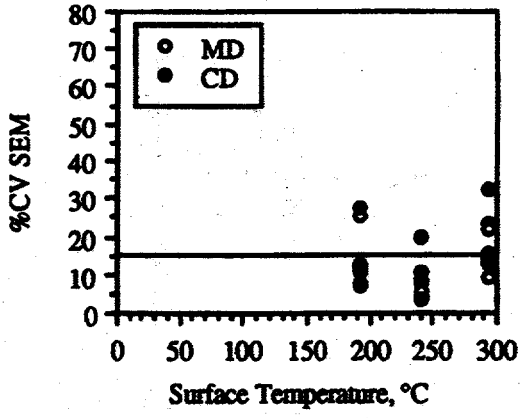

Figure C10. %CV of SEM for Furnish FD6.

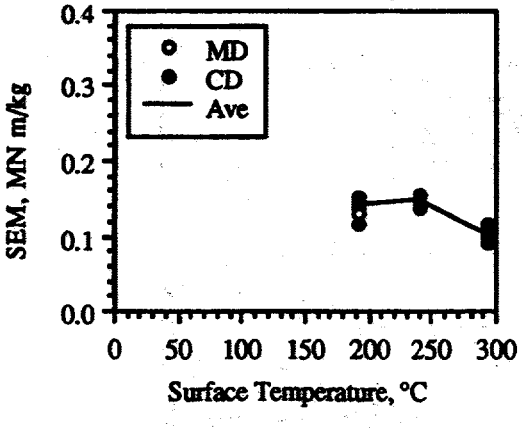

Figure C11. SEM for Furnish FD7.

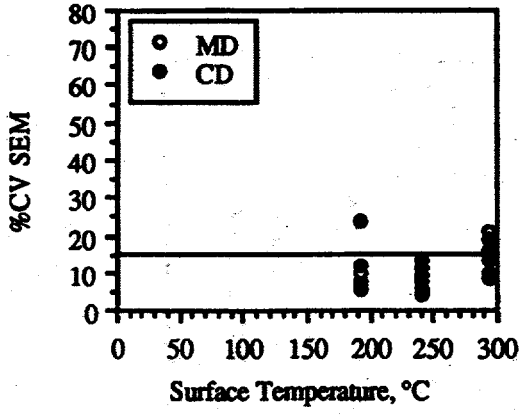

Figure C12. %CV of SEM for Furnish FD7.

Case C1- Visual Delamination Code for Impulse Drying with the IPST-C Ceramic Roll
(Felt B, 0 pivot, and 6000 pli)

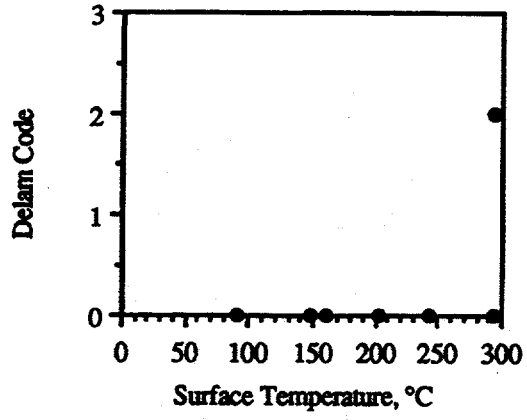

Figure C13. Furnish WF1.

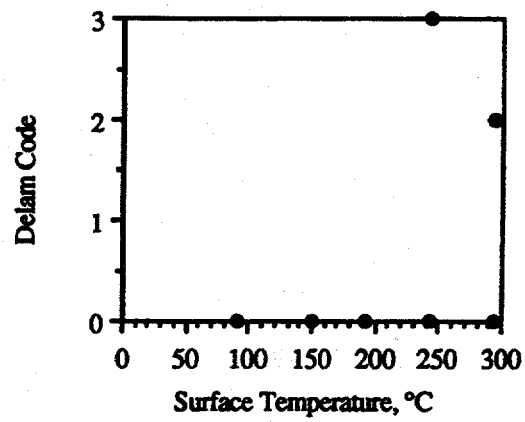

Figure C14. Furnish WF2.

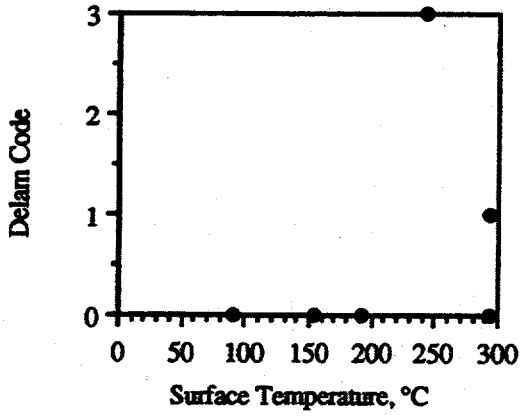

Figure C15. Furnish WF3.

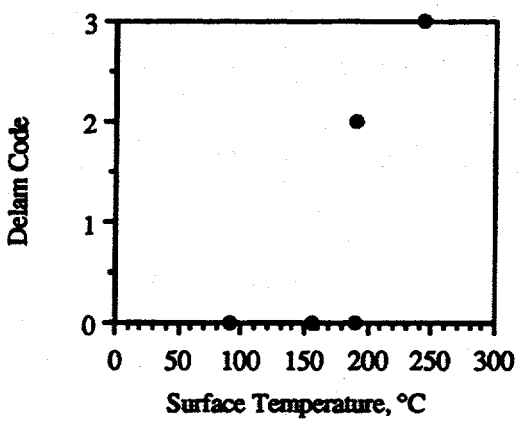

Figure C16. Furnish FD5.

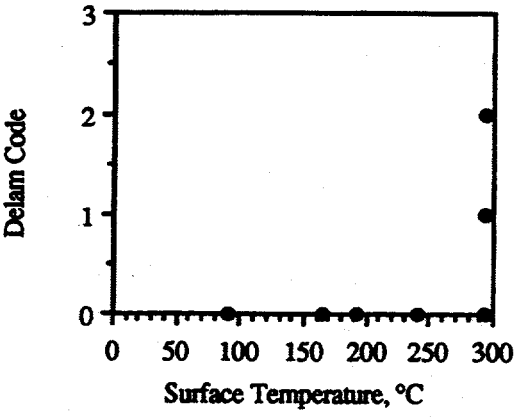

Figure C17. Furnish FD6.

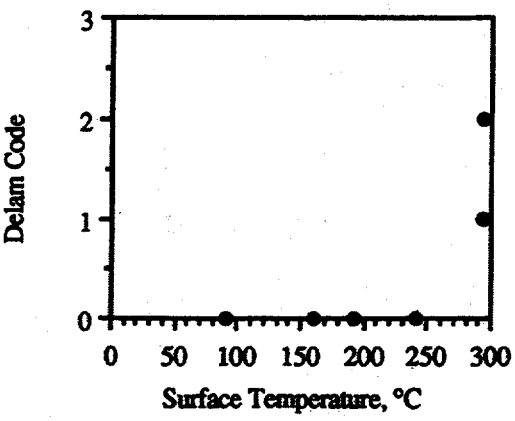

Figure C18. Furnish FD7.

Case C2- SEM and %CV of SEM for Impulse Drying with the IPST-C Ceramic Roll
(Felt B, 0 pivot, and 8500 pli)

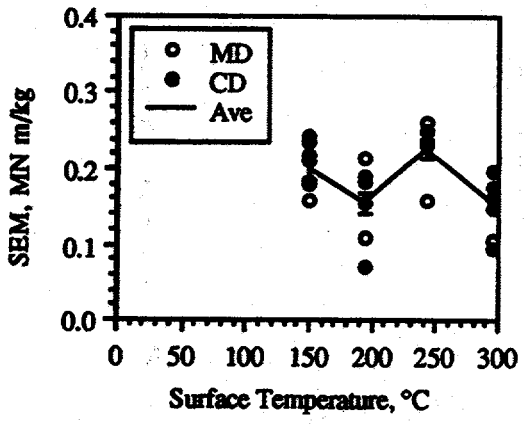

Figure C19. SEM for Furnish WF1.

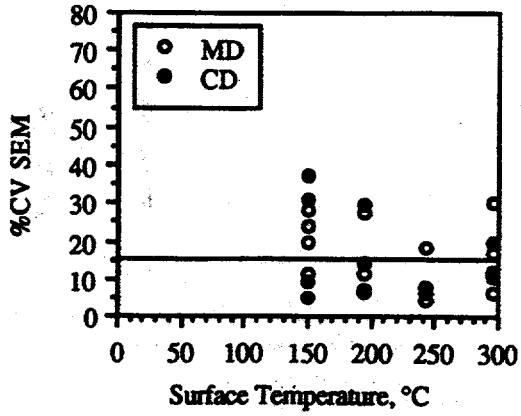

Figure C20. %CV of SEM for Furnish WF1.

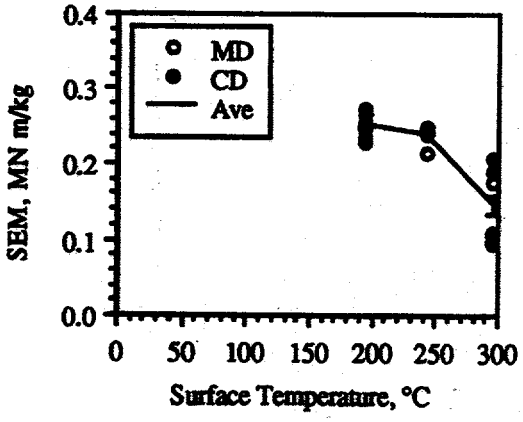

Figure C21. SEM for Furnish WF2.

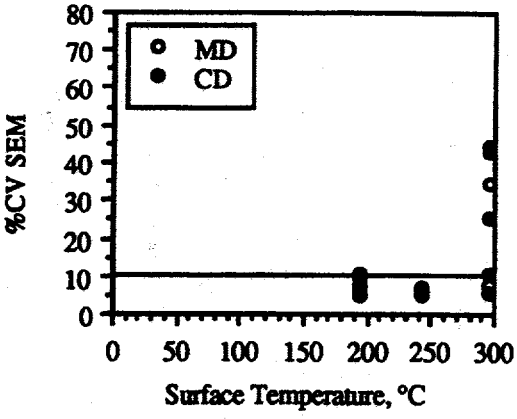

Figure C22. %CV of SEM for Furnish WF2.

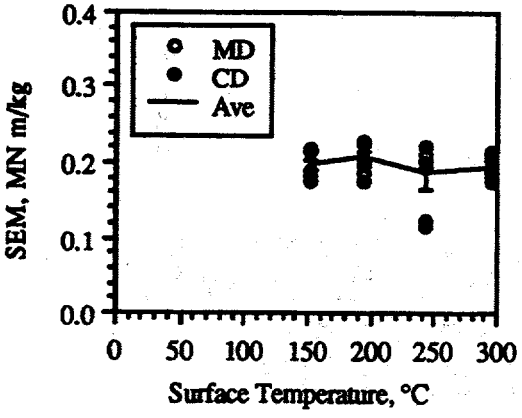

Figure C23. SEM for Furnish WF3.

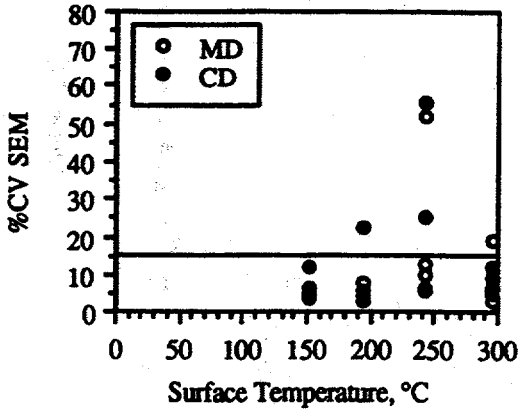

Figure C24. %CV of SEM for Furnish WF3.

Case C2- SEM and %CV of SEM for Impulse Drying with the IPST-C Ceramic Roll
(Felt B, 0 pivot, and 8500 pli)

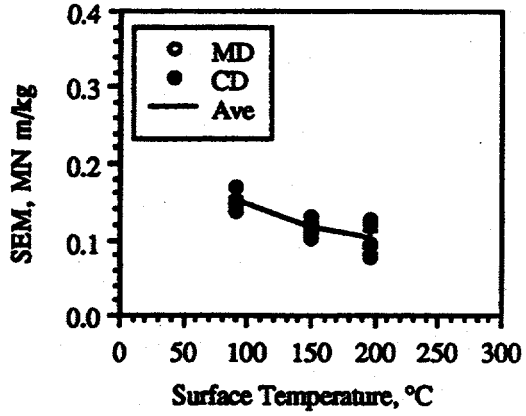

Figure C25. SEM for Furnish FD5.

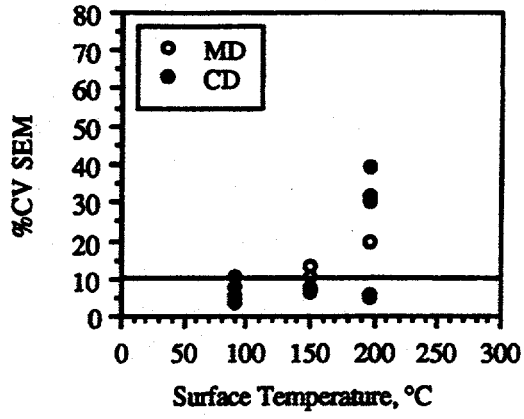

Figure C26. %CV of SEM for Furnish FD5.

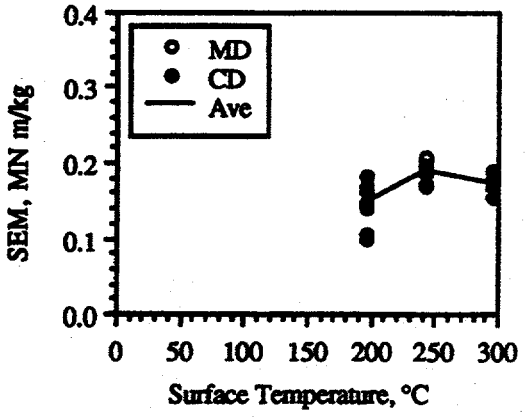

Figure C27. SEM for Furnish FD6.

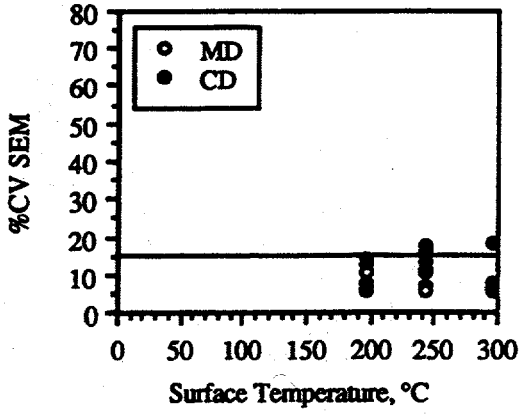

Figure C28. %CV of SEM for Furnish FD6.

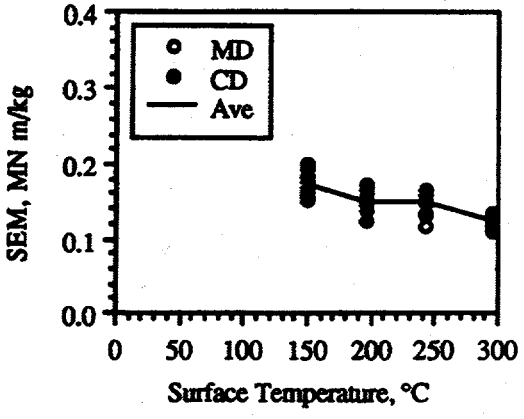

Figure C29. SEM for Furnish FD7.

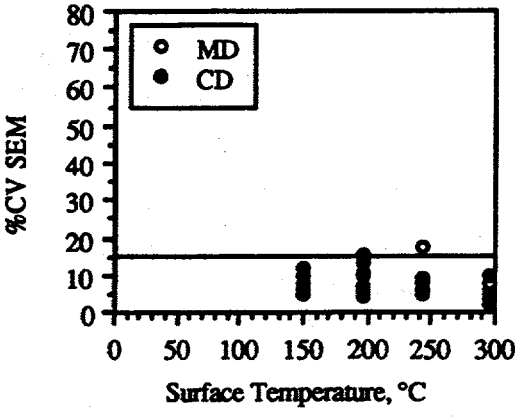

Figure C30. %CV of SEM for Furnish FD7.

Case C2- Visual Delamination Code for Impulse Drying with the IPST-C Ceramic Roll
(Felt B, 0 pivot, and 8500 pli)

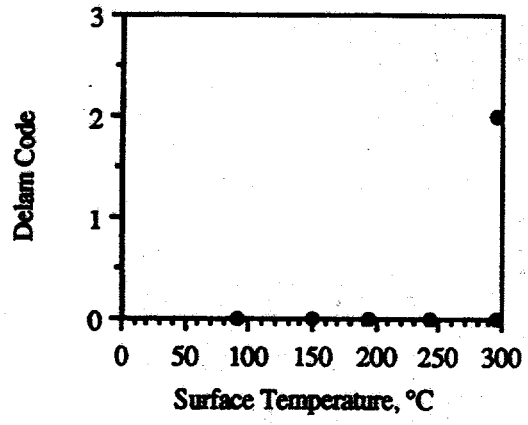

Figure C31. Furnish WF1.

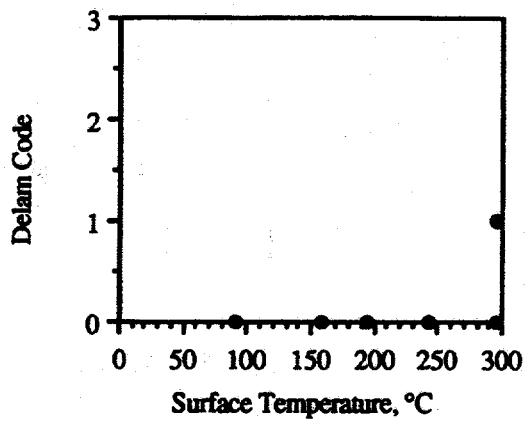

Figure C32. Furnish WF2.

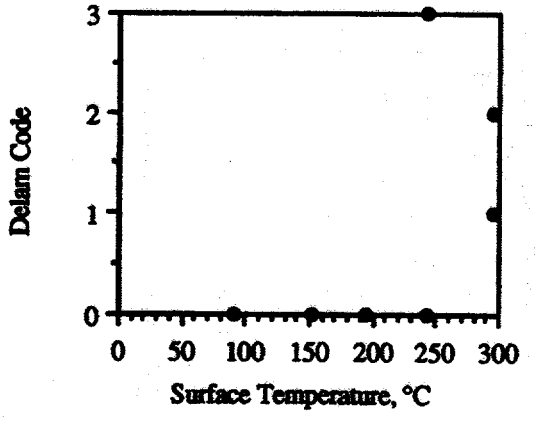

Figure C33. Furnish WF3.

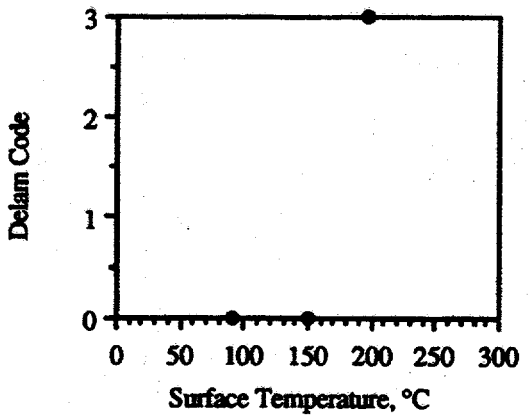

Figure C34. Furnish FD5.

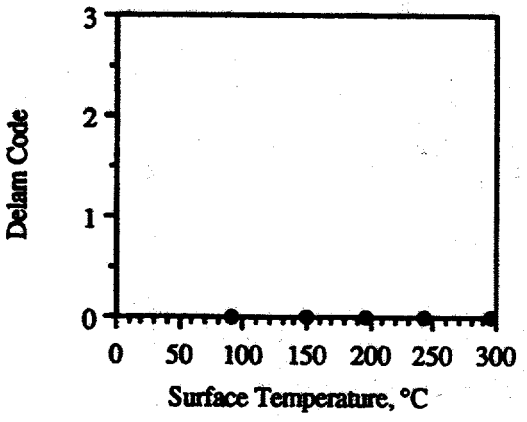

Figure C35. Furnish FD6.

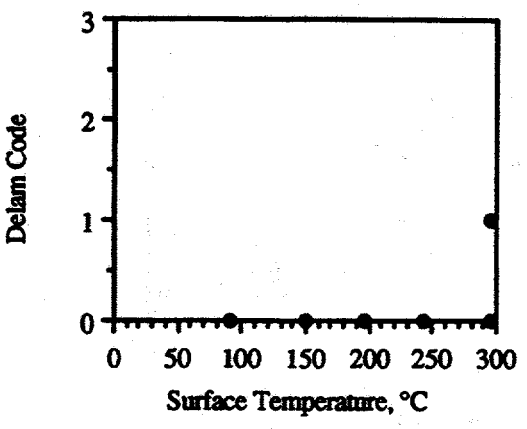

Figure C36. Furnish FD7.

Case C3- SEM and %CV of SEM for Impulse Drying with the IPST-C Ceramic Roll (Felt B, 2" pivot, and 6000 pli)

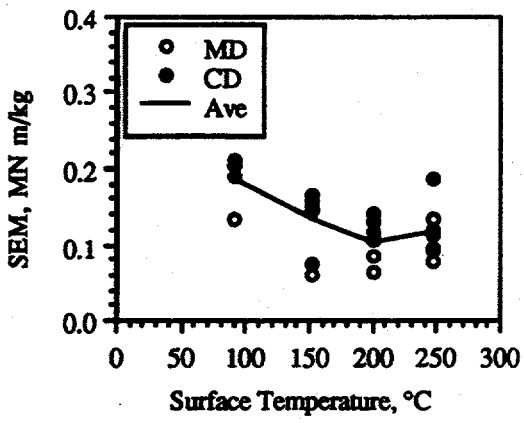

Figure C37 SEM for Furnish WF1.

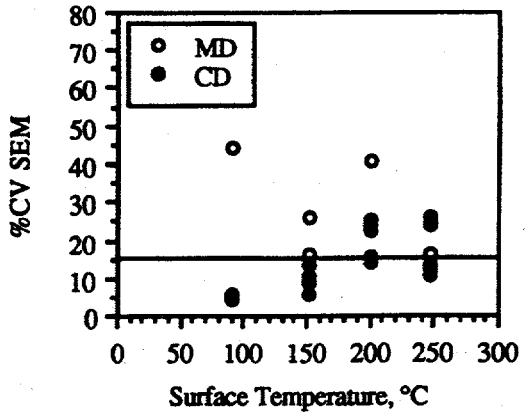

Figure C38 %CV of SEM for Furnish WF1.

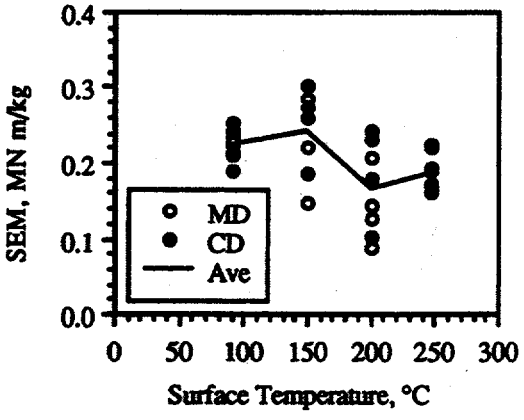

Figure C39 SEM for Furnish WF2.

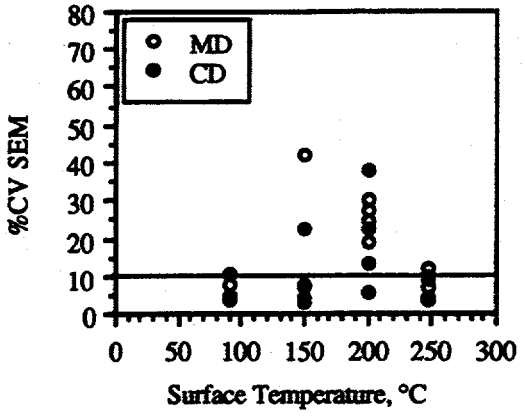

Figure C40 %CV of SEM for Furnish WF2.

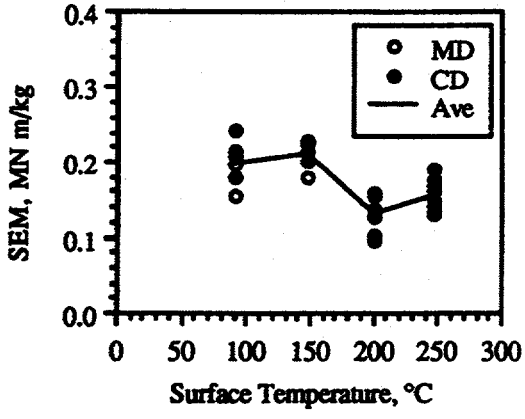

Figure C41 SEM for Furnish WF3.

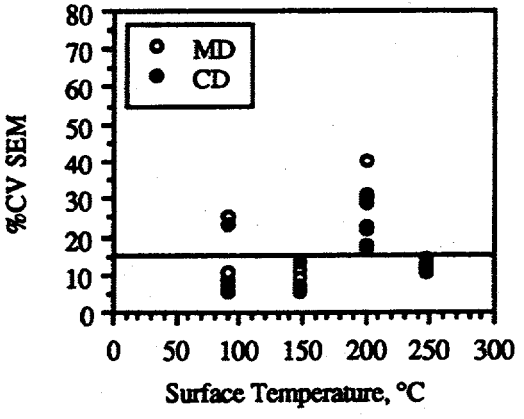

Figure C42 %CV of SEM for Furnish WF3.

Case C3- SEM and %CV of SEM for Impulse Drying with the IPST-C Ceramic Roll
(Felt B, 2" pivot, and 6000 pli)

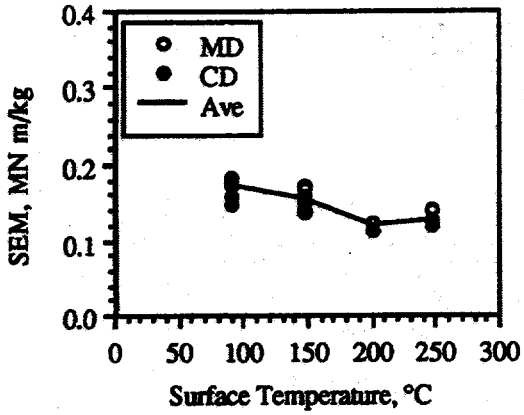

Figure C43. SEM for Furnish FD5.

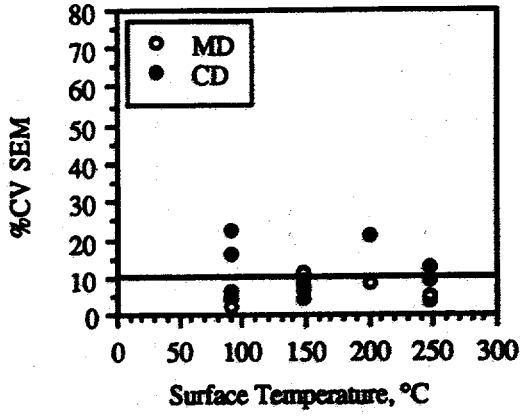

Figure C44. %CV of SEM for Furnish FD5.

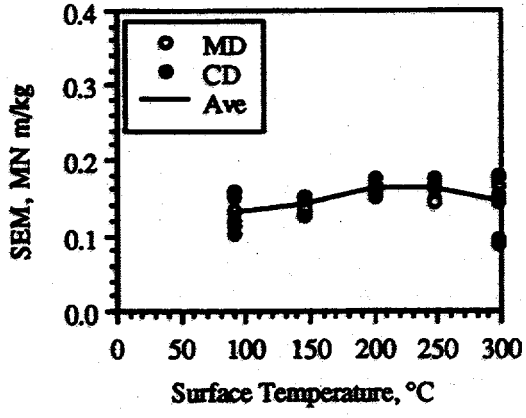

Figure C45. SEM for Furnish FD6.

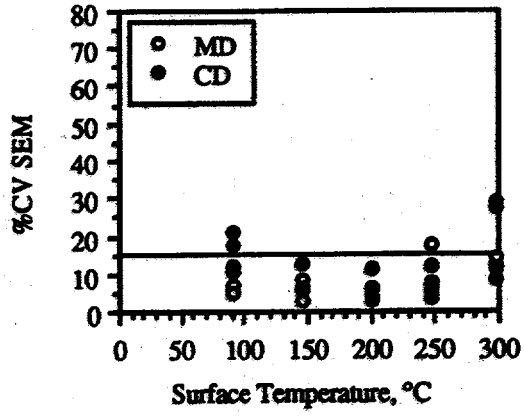

Figure C46. %CV of SEM for Furnish FD6.

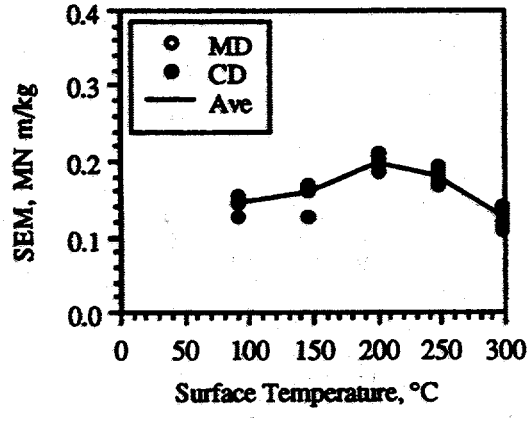

Figure C47. SEM for Furnish FD7.

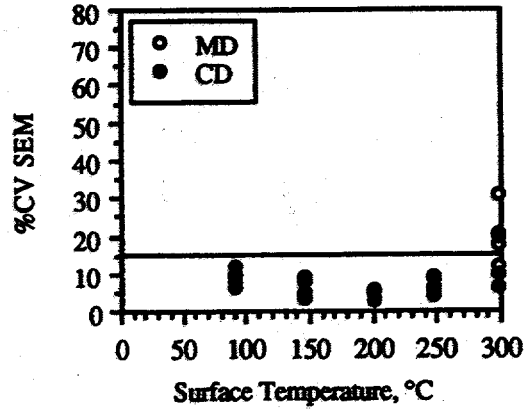

Figure C48. %CV of SEM for Furnish FD7.

Case C3- Visual Delamination Code for Impulse Drying with the IPST-C Ceramic Roll
(Felt B, 2" pivot, and 6000 pli)

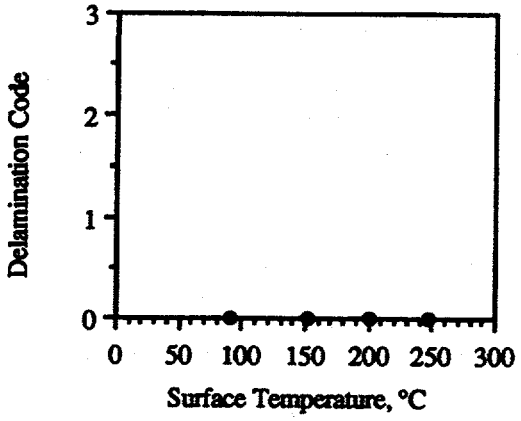

Figure C49. Furnish WF1.

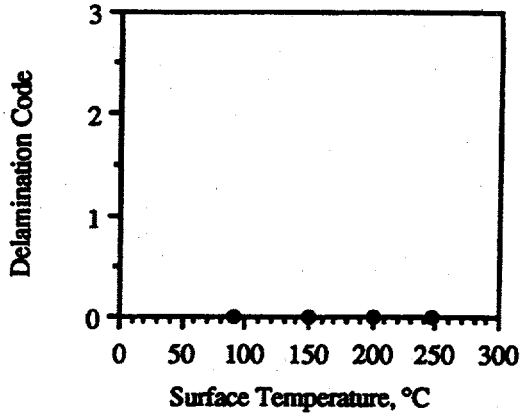

Figure C50. Furnish WF2.

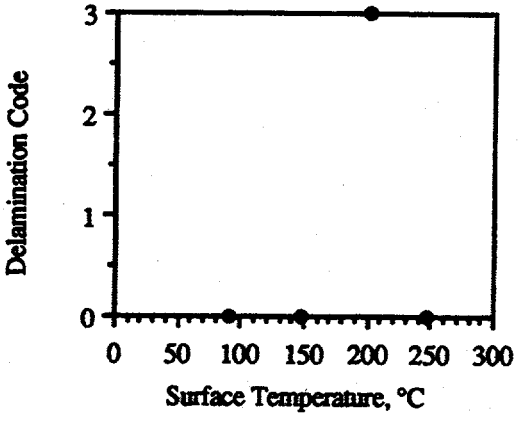

Figure C51. Furnish WF3.

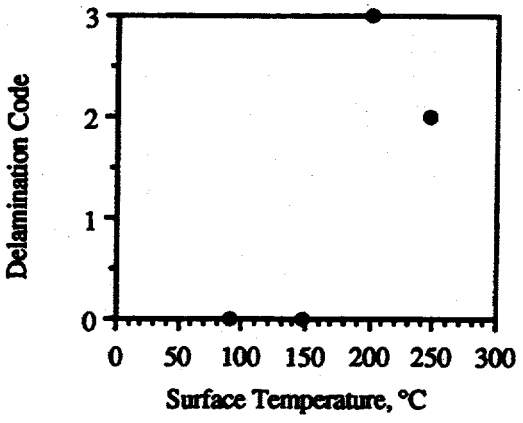

Figure C52. Furnish FD5.

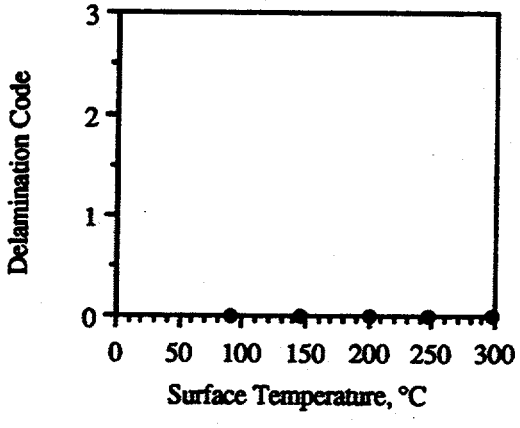

Figure C53. Furnish FD6.

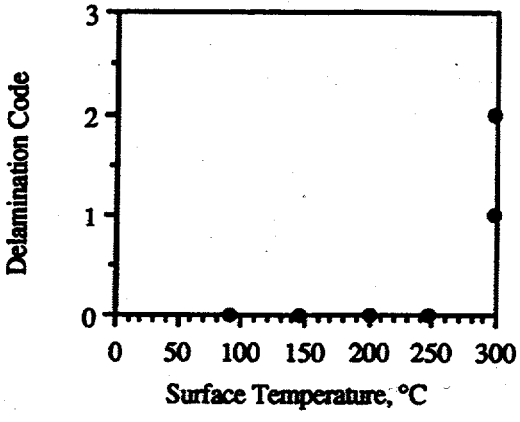

Figure C54. Furnish FD7.

Case A1- SEM and %CV of SEM for Impulse Drying with the Beloit-A Roll
(Felt B, 0 pivot, and 6000 pli)

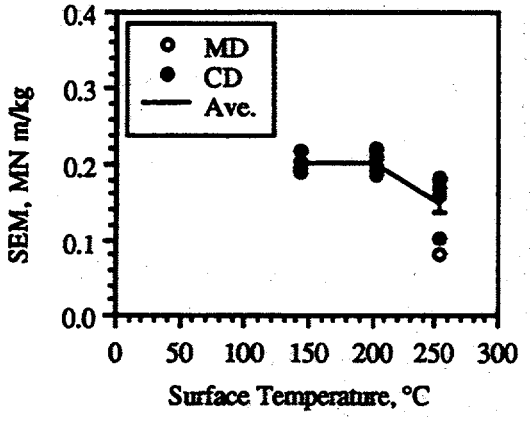

Figure C55. SEM for Furnish WF1.

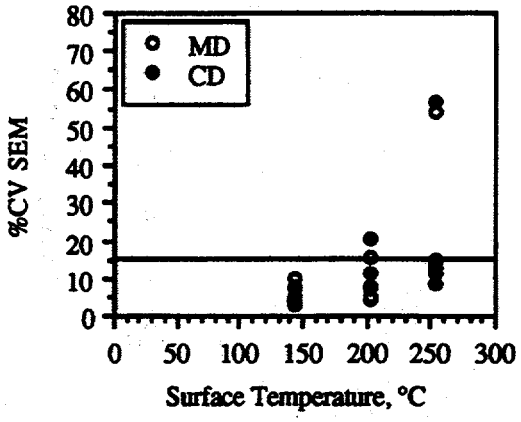

Figure C56. %CV of SEM for Furnish WF1.

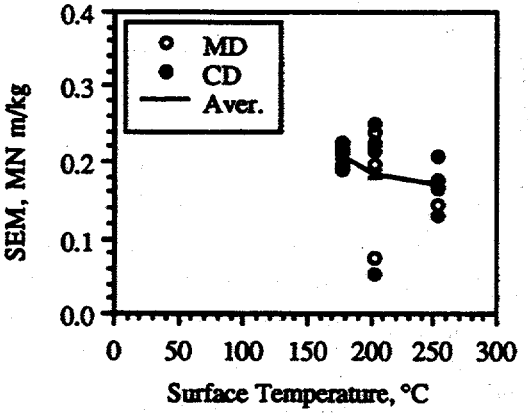

Figure C57. SEM for Furnish WF2.

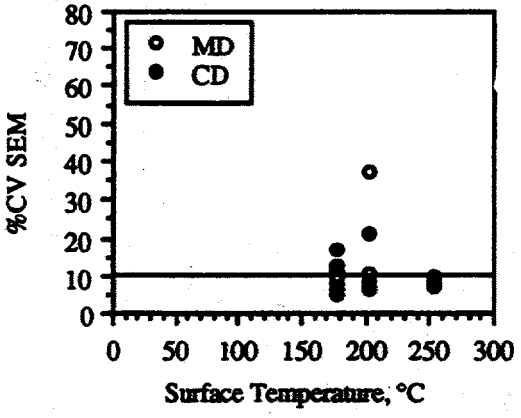

Figure C58. %CV of SEM for Furnish WF2.

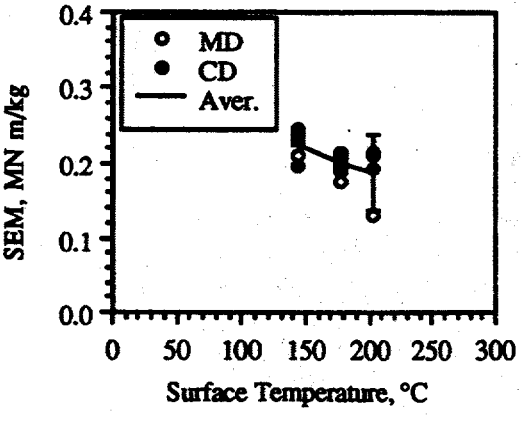

Figure C59. SEM for Furnish WF3.

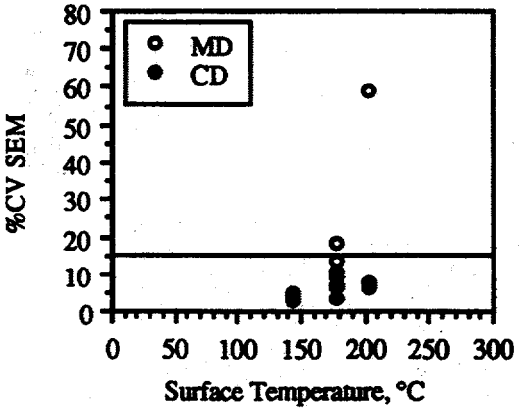

Figure C60. %CV of SEM for Furnish WF3.

Case A1- SEM and %CV of SEM for Impulse Drying with the Beloit-A Roll
(Felt B, 0 pivot, and 6000 pli)

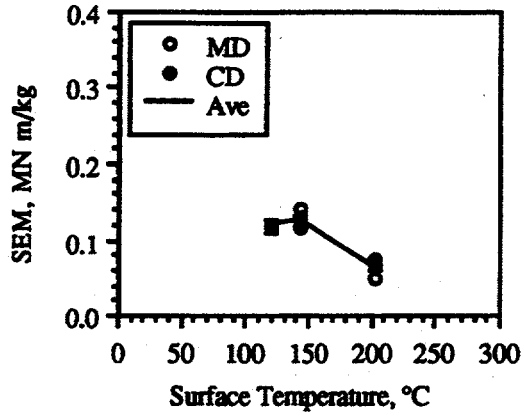

Figure C61. SEM for Furnish FD5.

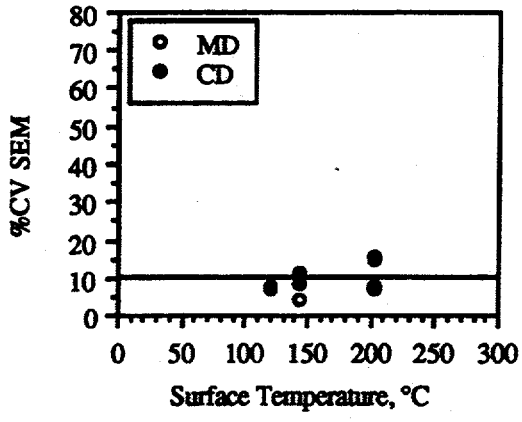

Figure C62. %CV of SEM for Furnish FD5.

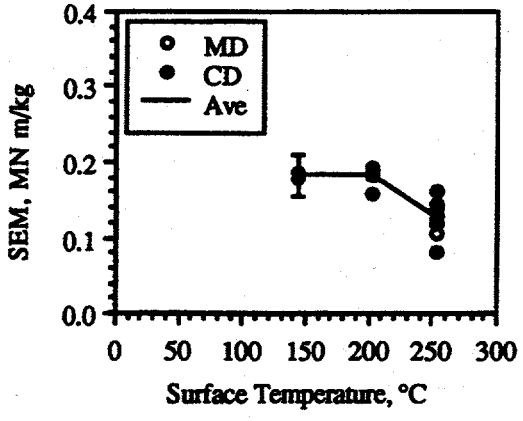

Figure C63. SEM for Furnish FD6.

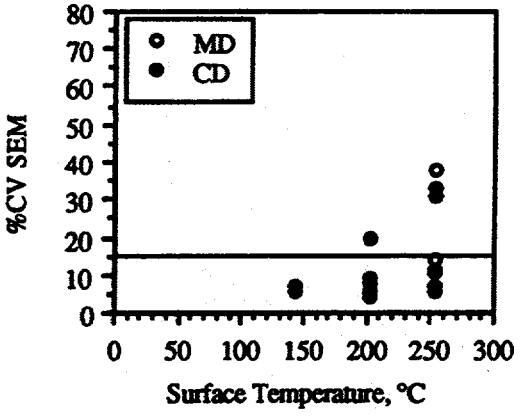

Figure C64. %CV of SEM for Furnish FD6.

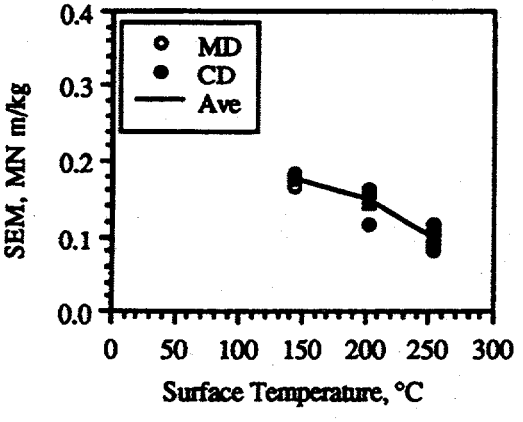

Figure C65. SEM for Furnish FD7.

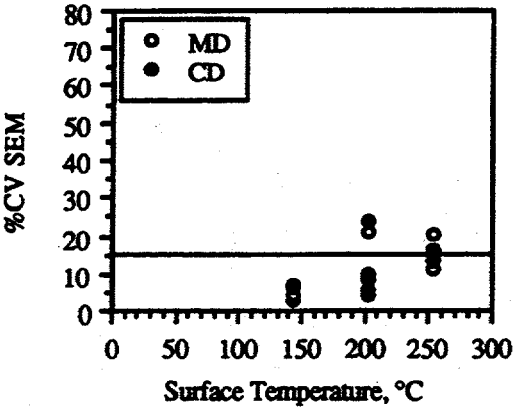

Figure C66. %CV of SEM for Furnish FD7.

Case A1- Visual Delamination Code for Impulse Drying with the Beloit-A Roll
(Felt B, 0 pivot, and 6000 pli)

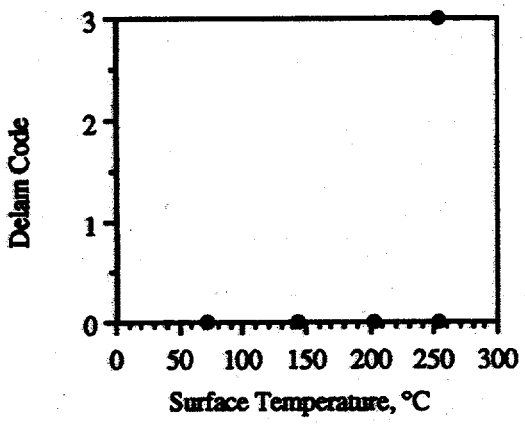

Figure C67. Furnish WF1.

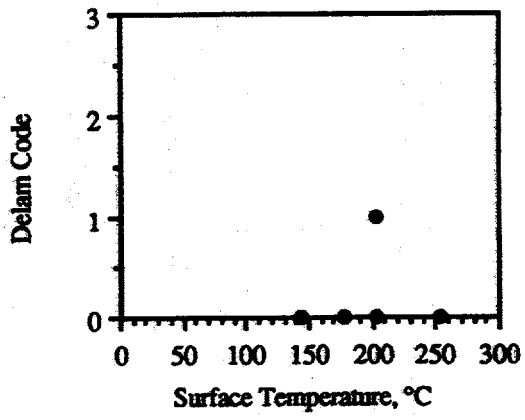

Figure C68. Furnish WF2.

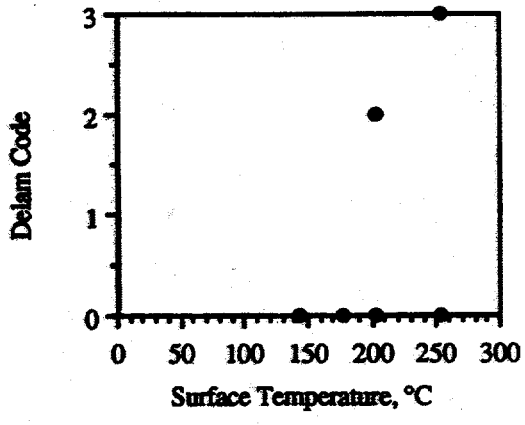

Figure C69. Furnish WF3.

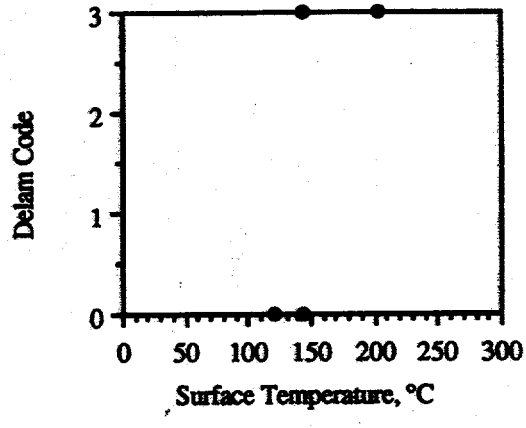

Figure C70. Furnish FD5.

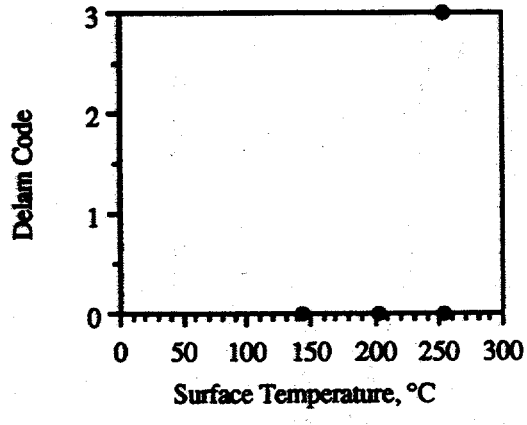

Figure C71. Furnish FD6.

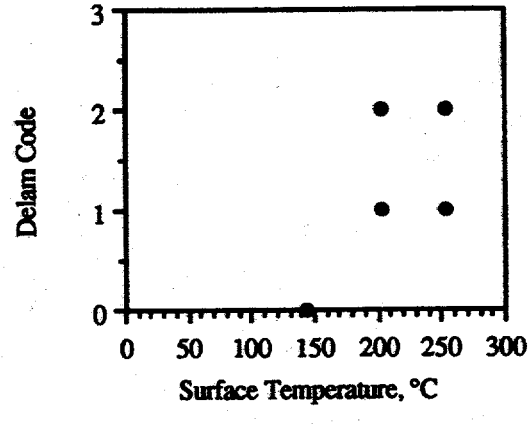

Figure C72. Furnish FD7.

Case A2- SEM and %CV of SEM for Impulse Drying with the Beloit-A Roll
(Felt B, 0 pivot, and 8500 pli)

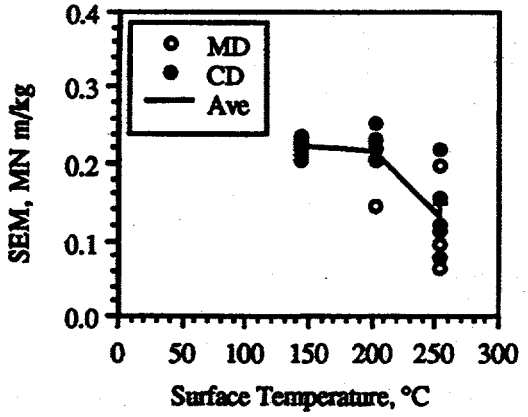

Figure C73. SEM for Furnish WF1.

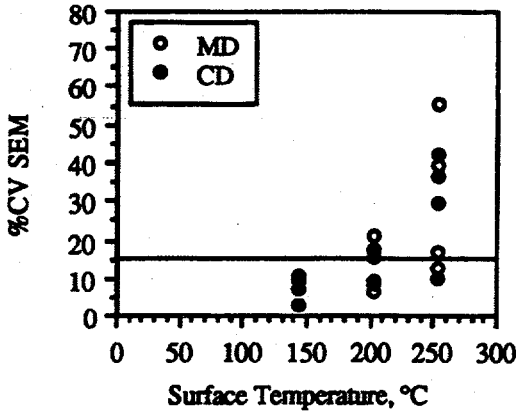

Figure C74. %CV of SEM for Furnish WF1.

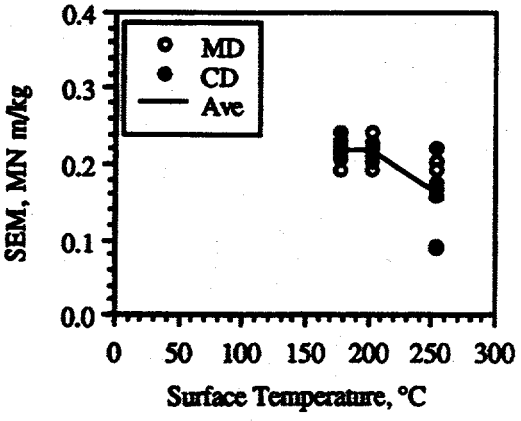

Figure C75. SEM for Furnish WF2.

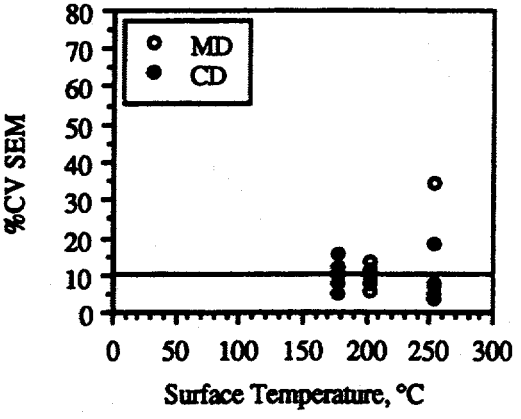

Figure C76. %CV of SEM for Furnish WF2.

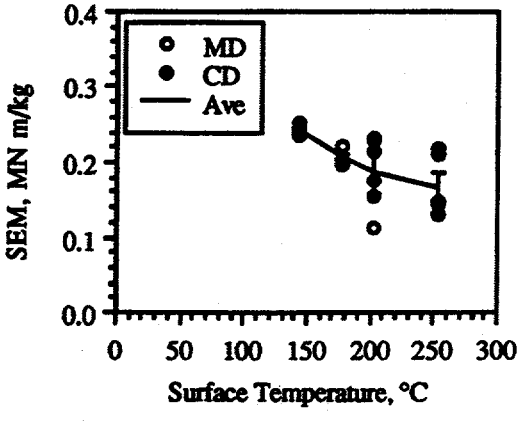

Figure C77. SEM for Furnish WF3.

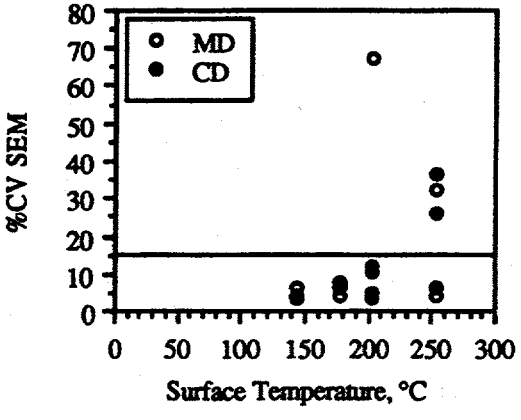

Figure C78. %CV of SEM for Furnish WF3.

Case A2- SEM and %CV of SEM for Impulse Drying with the Beloit-A Roll
(Felt B, 0 pivot, and 8500 pli)

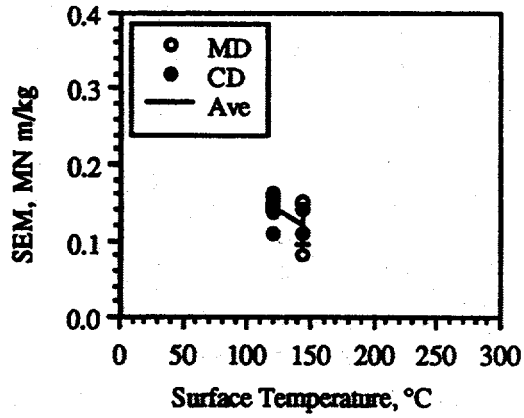

Figure C79. SEM for Furnish FD5.

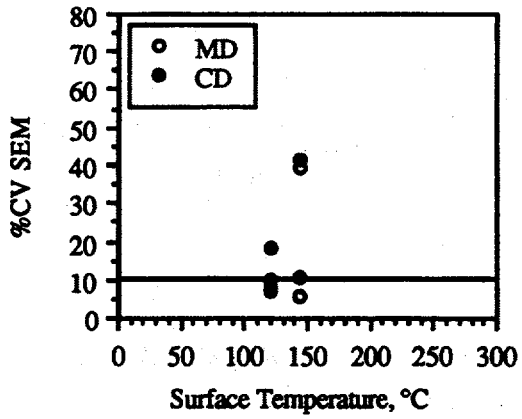

Figure C80. %CV of SEM for Furnish FD5.

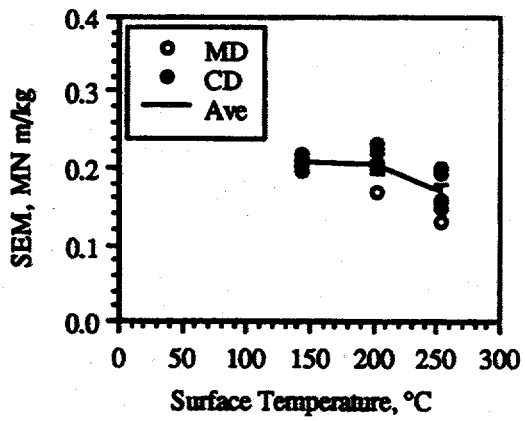

Figure C81. SEM for Furnish FD6.

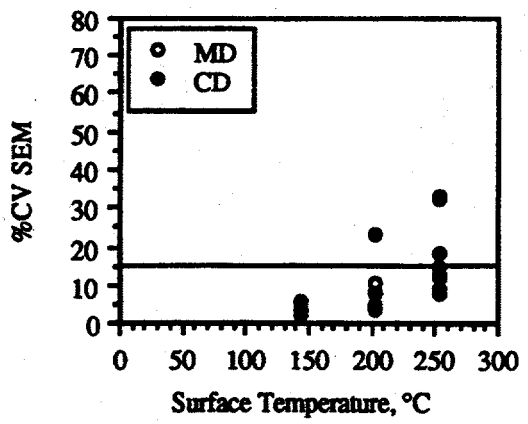

Figure C82. %CV of SEM for Furnish FD6.

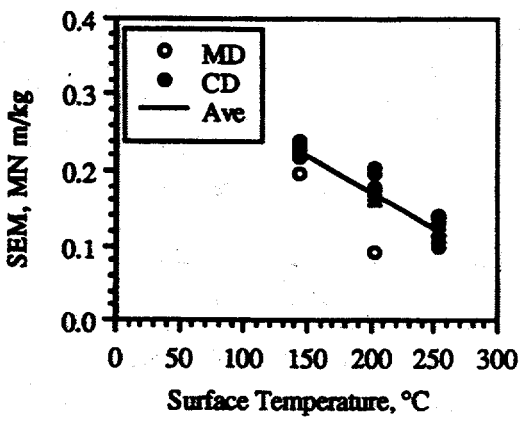

Figure C83. SEM for Furnish FD7.

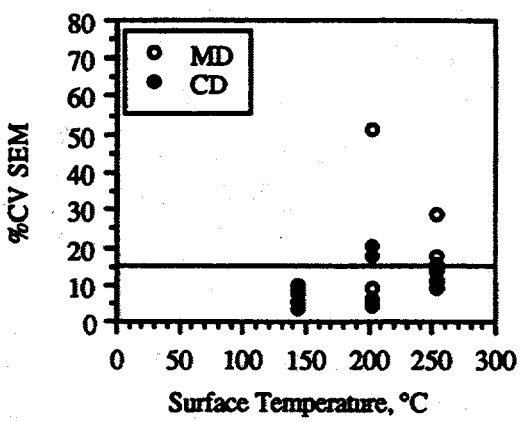

Figure C84. %CV of SEM for Furnish FD7.

Case A2- Visual Delamination Code for Impulse Drying with the Beloit-A Roll
(Felt B, 0 pivot, and 8500 pli)

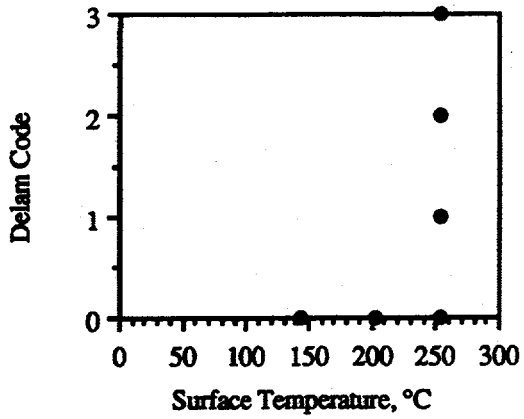

Figure C85. Furnish WF1.

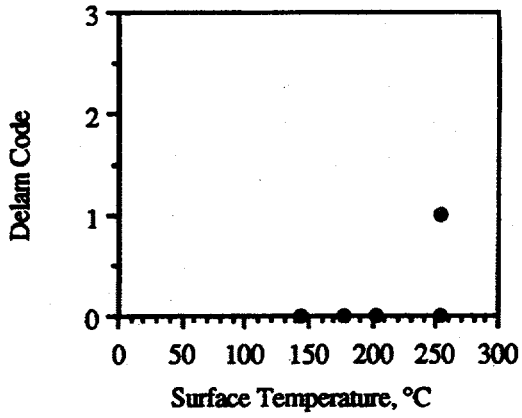

Figure C86. Furnish WF2.

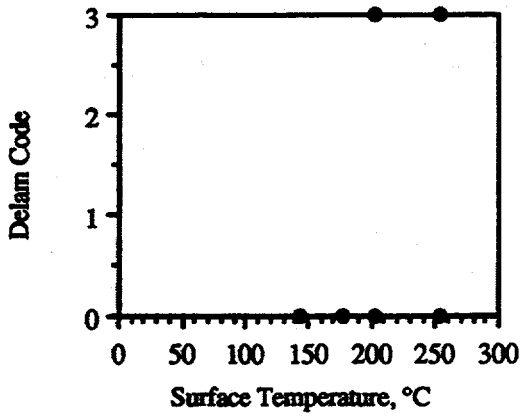

Figure C87. Furnish WF3.

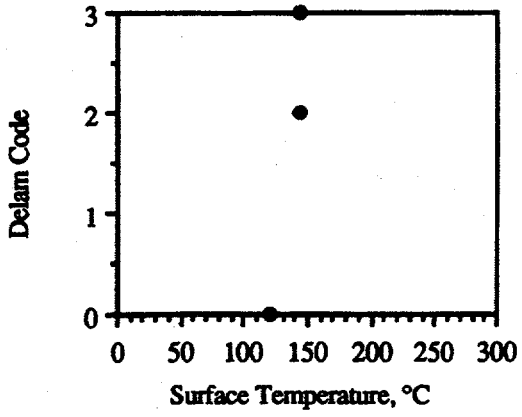

Figure C88. Furnish FD5.

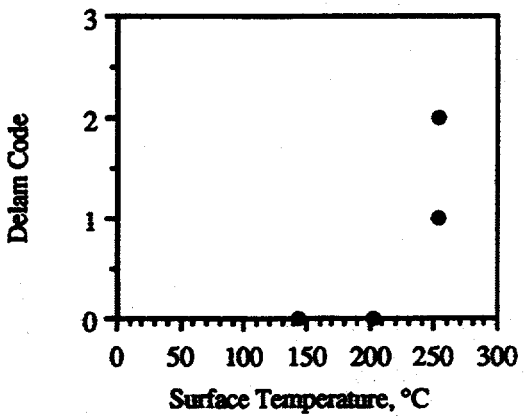

Figure C89. Furnish FD6.

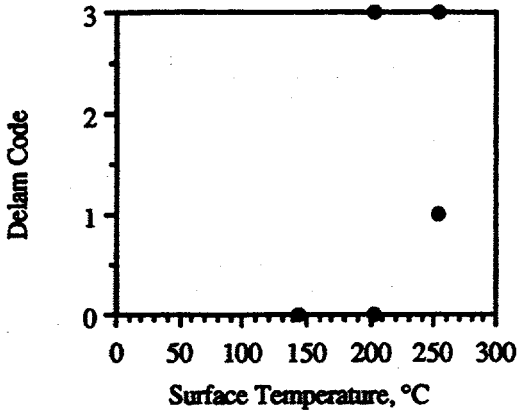

Figure C90. Furnish FD7.

Case A4- SEM and %CV of SEM for Impulse Drying with the Beloit-A Roll
(Felt S, 0 pivot, and 6000 pli)

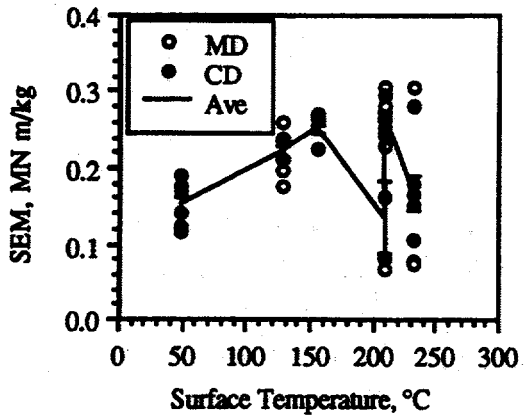

Figure C91. SEM for Furnish WF1.

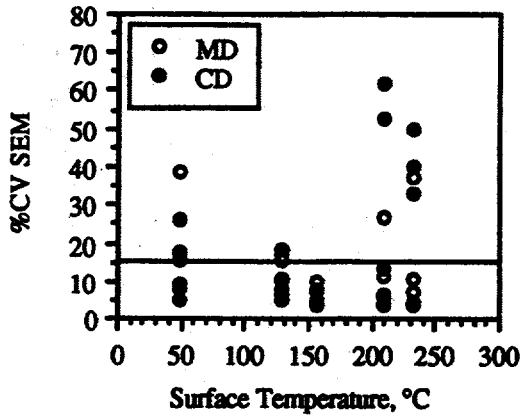

Figure C92. %CV of SEM for Furnish WF1.

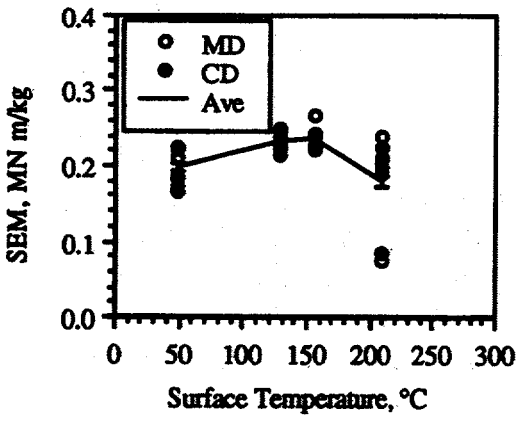

Figure C93. SEM for Furnish WF2.

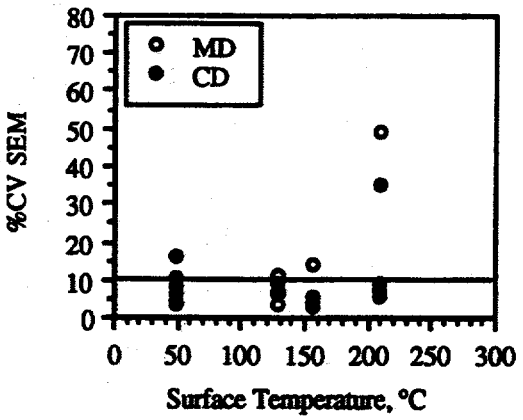

Figure C94. %CV of SEM for Furnish WF2.

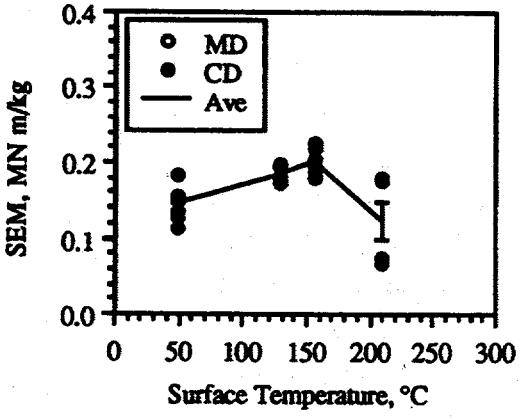

Figure C95. SEM for Furnish WF3.

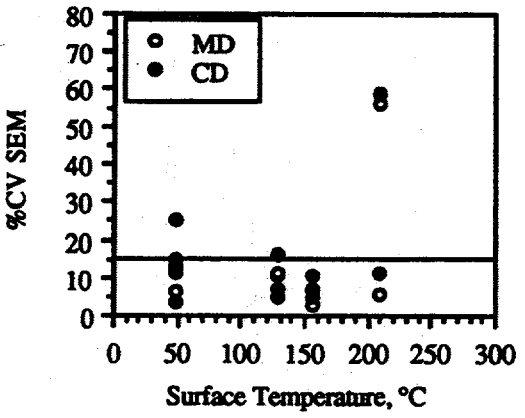

Figure C96. %CV of SEM for Furnish WF3.

Case A4- SEM and %CV of SEM for Impulse Drying with the Beloit-A Roll
(Felt S, 0 pivot, and 6000 pli)

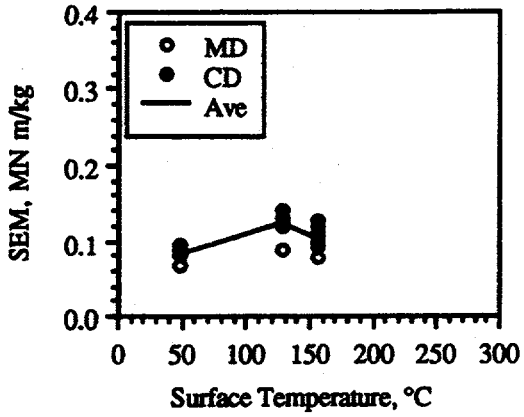

Figure C97. SEM for Furnish FD5.

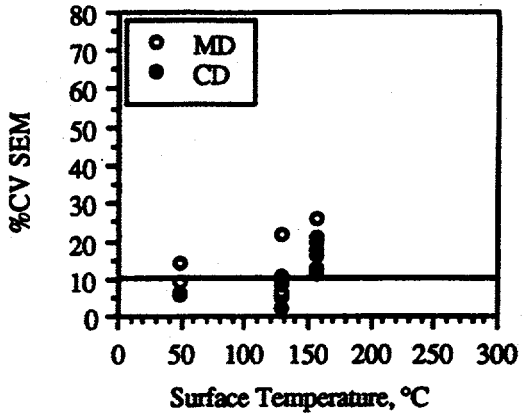

Figure C98. %CV of SEM for Furnish FD5.

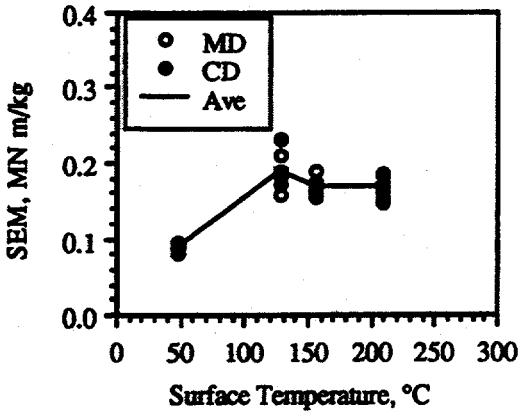

Figure C99. SEM for Furnish FD6.

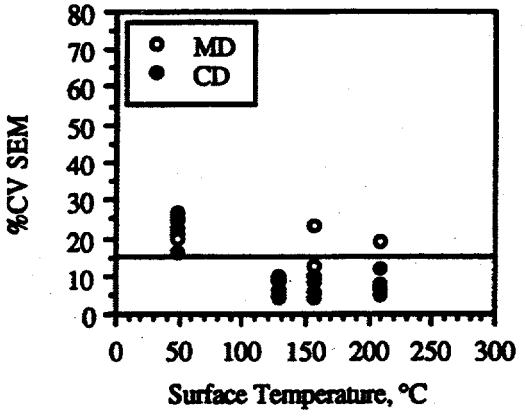

Figure C100. %CV of SEM for Furnish FD6.

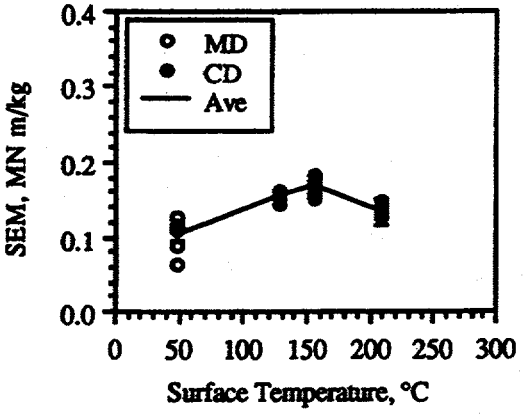

Figure C101. SEM for Furnish FD7.

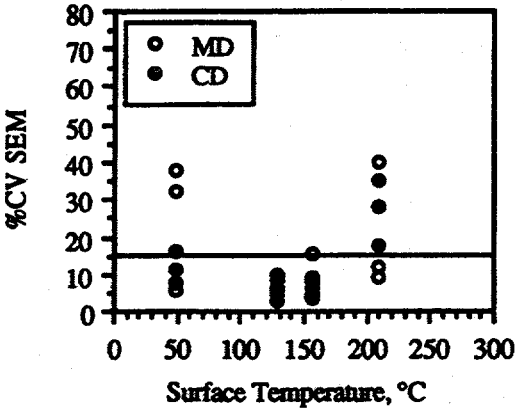

Figure C102. %CV of SEM for Furnish FD7.

Case A4- Visual Delamination Code for Impulse Drying with the Beloit-A Roll
(Felt S, 0 pivot, and 6000 pli)

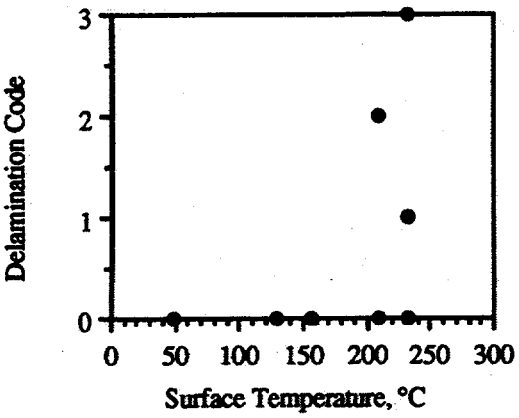

Figure C103. Furnish WF1.

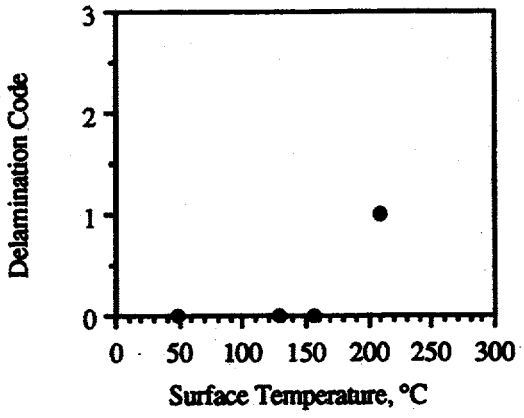

Figure C104. Furnish WF2.

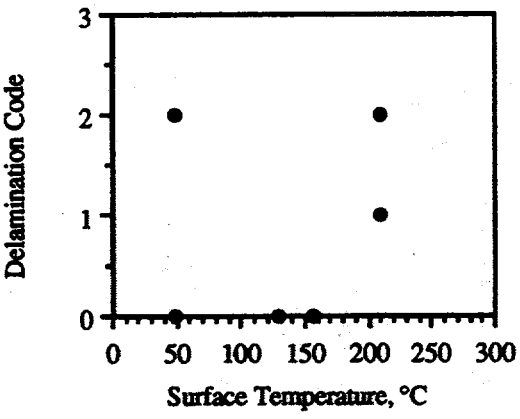

Figure C105. Furnish WF3.

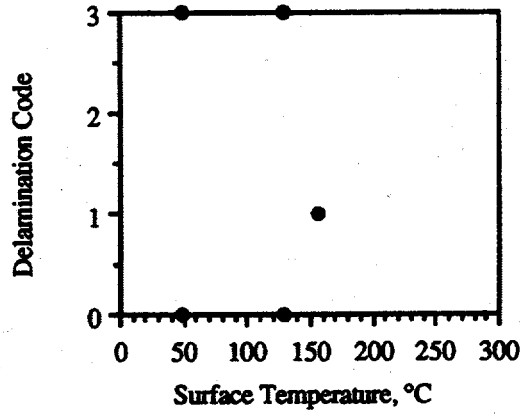

Figure C106. Furnish FD5.

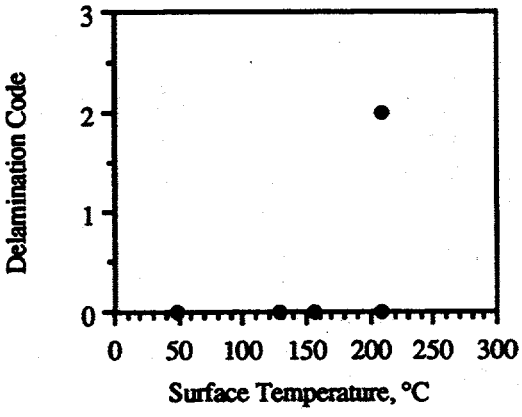

Figure C107. Furnish FD6.

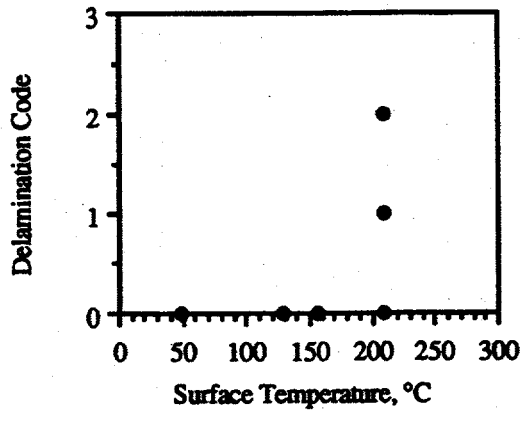

Figure C108. Furnish FD7.

Case A5- SEM and %CV of SEM for Impulse Drying with the Beloit-A Roll
(Felt S, 0 pivot, and 8500 pli)

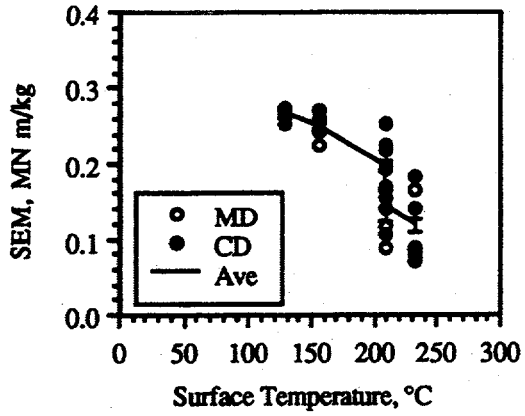

Figure C109. SEM for Furnish WF1.

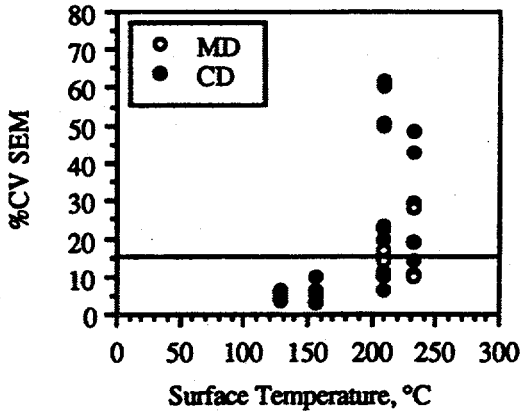

Figure C110. %CV of SEM for Furnish WF1.

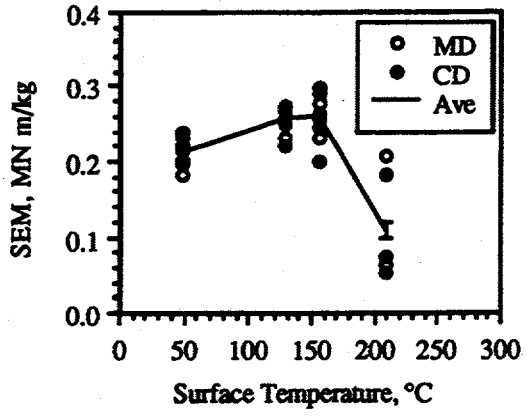

Figure C111. SEM for Furnish WF2.

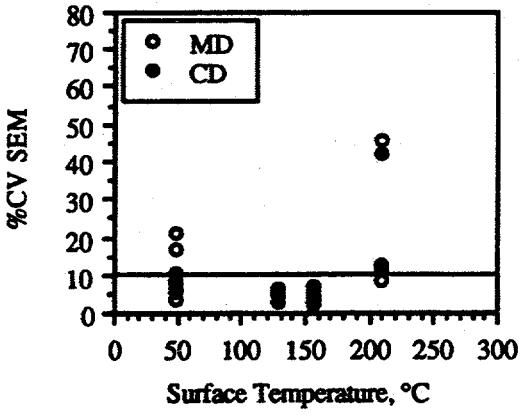

Figure C112. %CV of SEM for Furnish WF2.

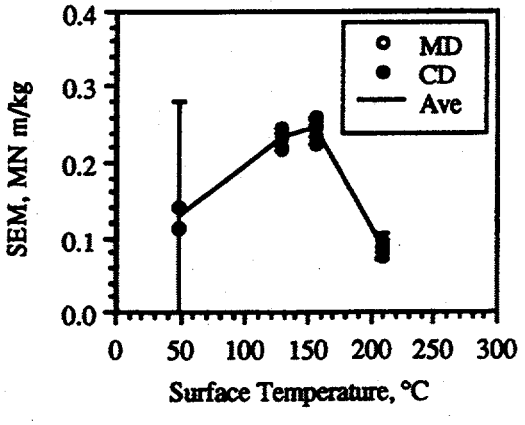

Figure C113. SEM for Furnish WF3.

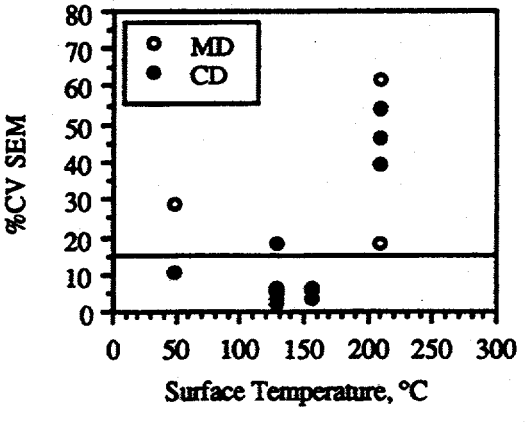

Figure C114. %CV of SEM for Furnish WF3.

Case A5- SEM and %CV of SEM for Impulse Drying with the Beloit-A Roll
(Felt S, 0 pivot, and 8500 pli)

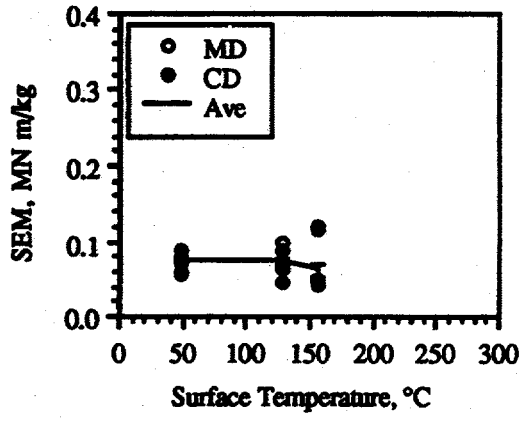

Figure C115. SEM for Furnish FD5.

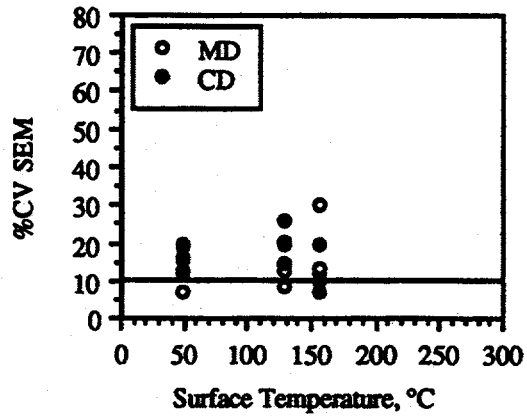

Figure C116. %CV of SEM for Furnish FD5.

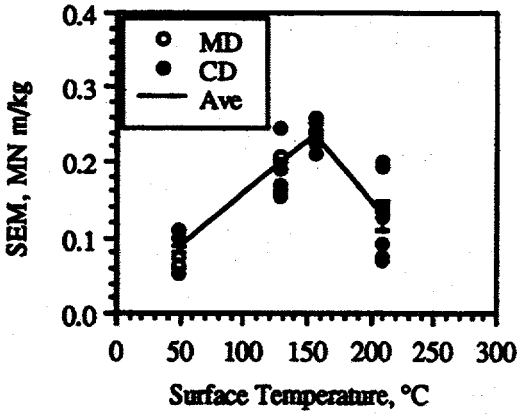

Figure C117. SEM for Furnish FD6.

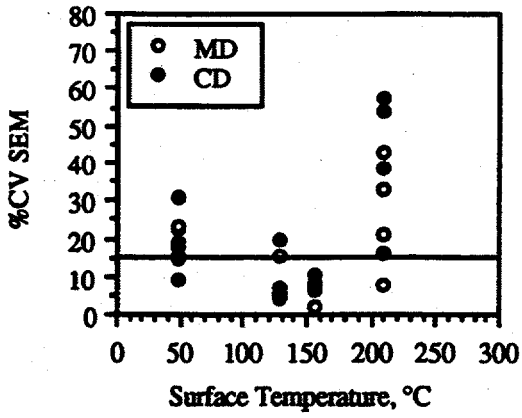

Figure C118. %CV of SEM for Furnish FD6.

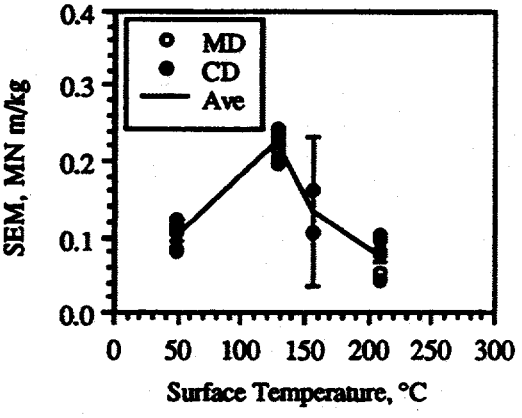

Figure C119. SEM for Furnish FD7.

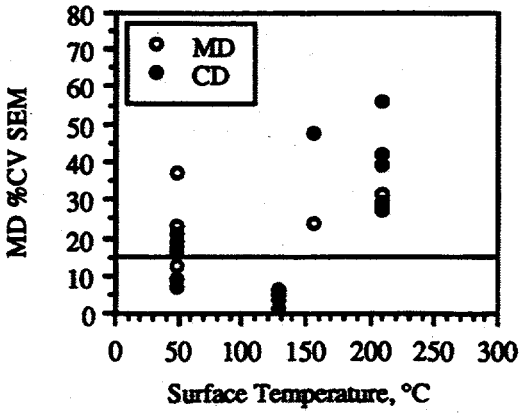

Figure C120. %CV of SEM for Furnish FD7.

Case A5- Visual delamination code for Impulse Drying with the Beloit-A Roll
(Felt S, 0 pivot, and 8500 pli)

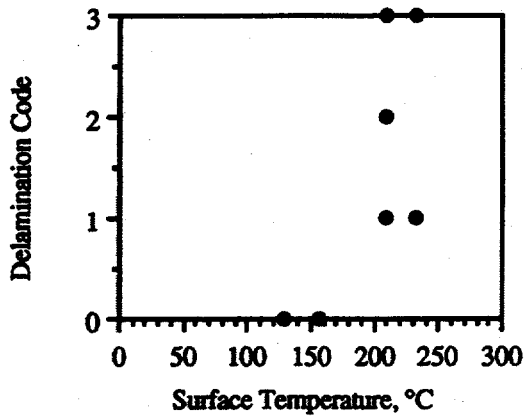

Figure C121. Furnish WF1.

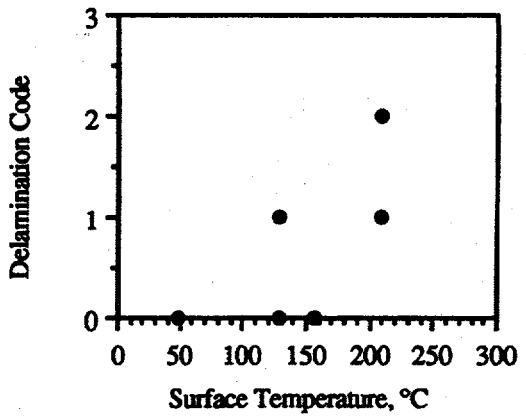

Figure C122. Furnish WF2.

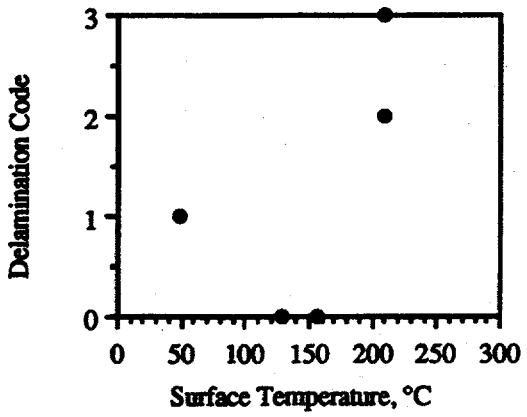

Figure C123. Furnish WF3.

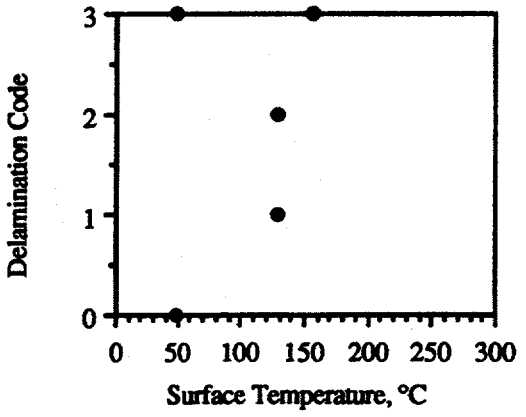

Figure C124. Furnish FD5.

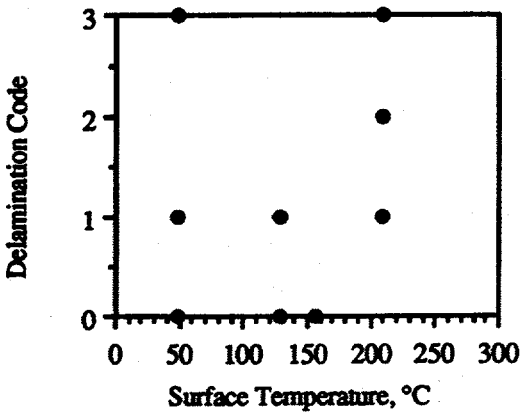

Figure C125. Furnish FD6.

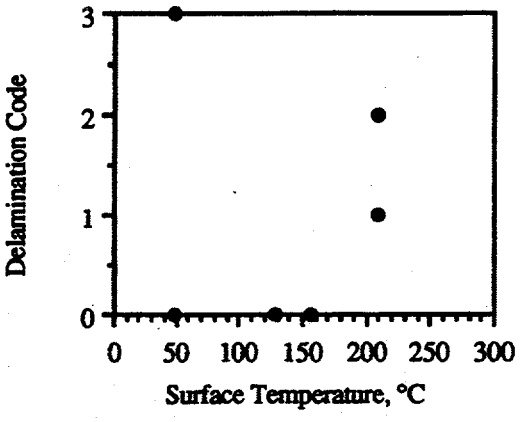

Figure C126. Furnish FD7.

Case A6- SEM and %CV of SEM for Impulse Drying with the Beloit-A Roll
(Felt S, 2" pivot, and 6000 pli)

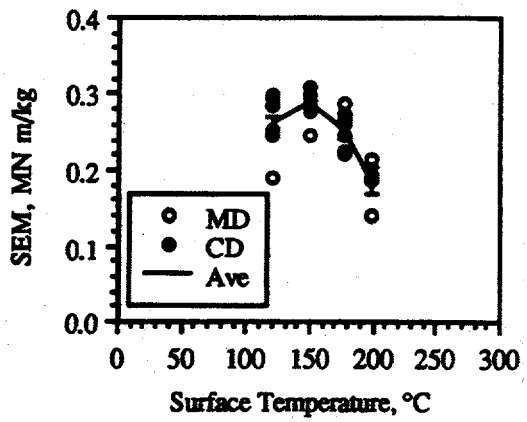

Figure C127. SEM for Furnish WF1.

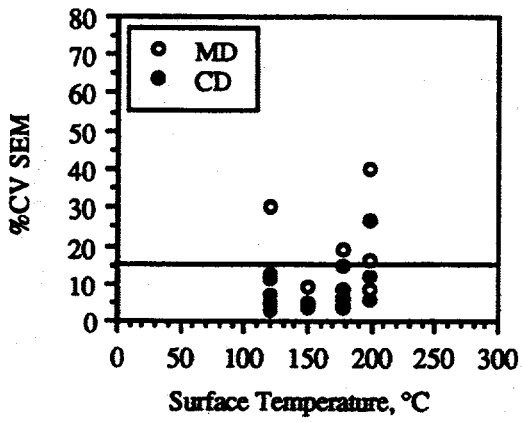

Figure C128. %CV of SEM for Furnish WF1.

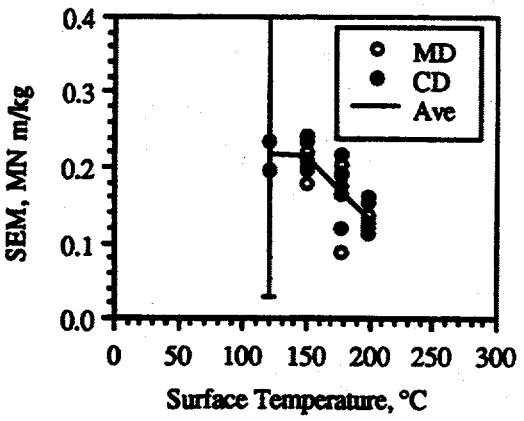

Figure C129. SEM for Furnish WF2.

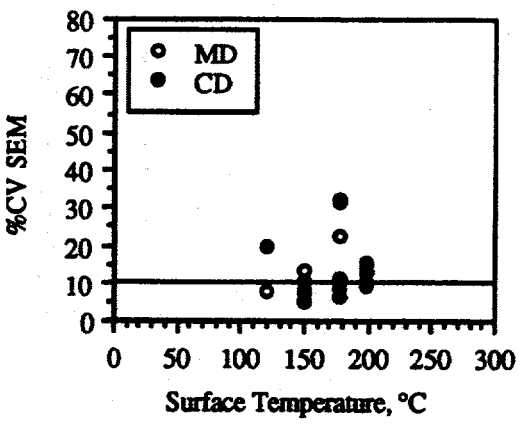

Figure C130. %CV of SEM for Furnish WF2.

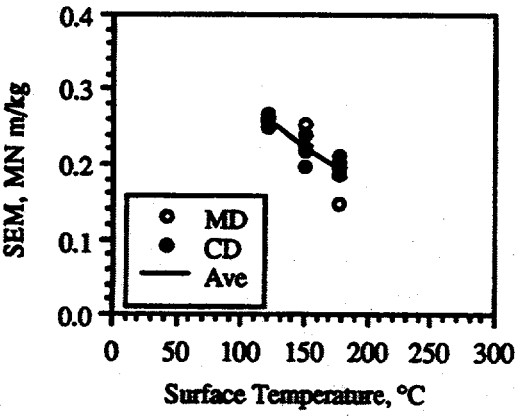

Figure C131. SEM for Furnish WF3.

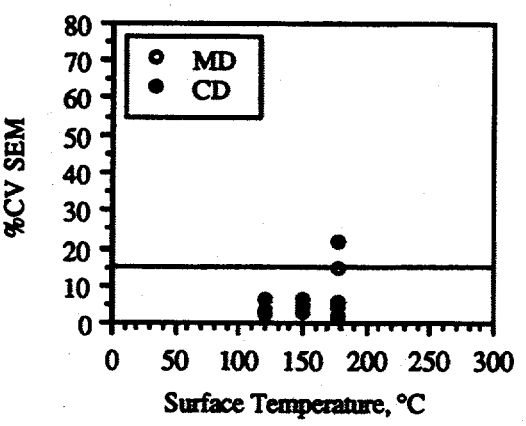

Figure C132. %CV of SEM for Furnish WF3.

Case A6- SEM and %CV of SEM for Impulse Drying with the Beloit-A Roll
(Felt S, 2" pivot, and 6000 pli)

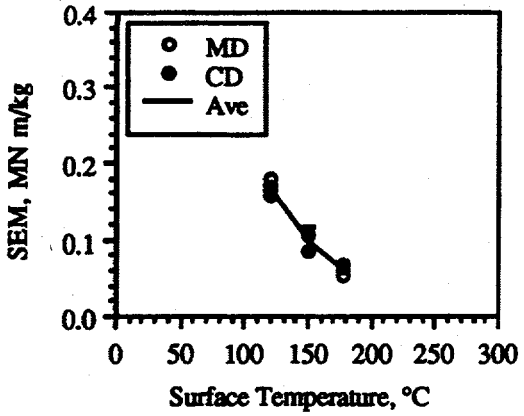

Figure C133. SEM for Furnish FD5.

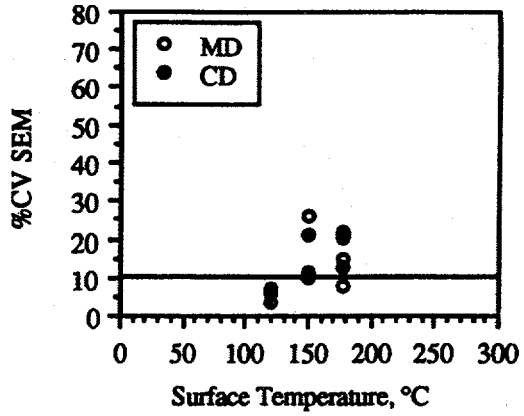

Figure C134. %CV of SEM for Furnish FD5.

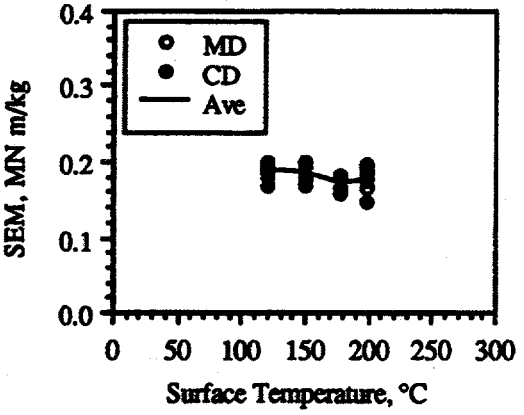

Figure C135. SEM for Furnish FD6.

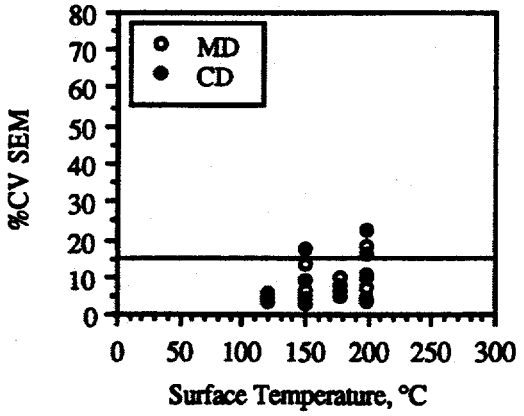

Figure C136. %CV of SEM for Furnish FD6.

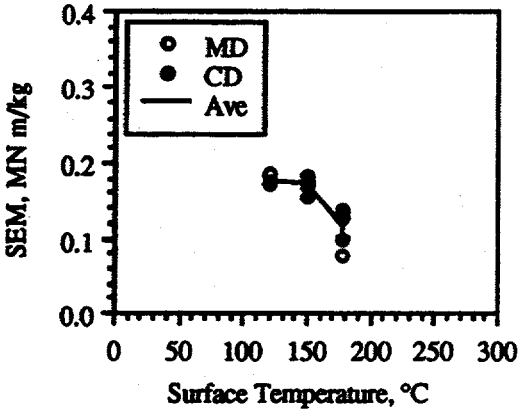

Figure C137. SEM for Furnish FD7.

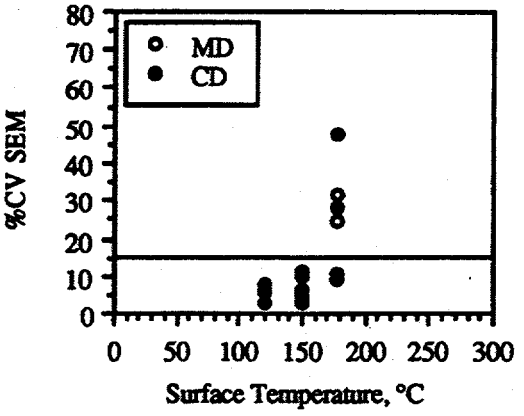

Figure C138. %CV of SEM for Furnish FD7.

Case A6- Visual Delamination Code for Impulse Drying with the Beloit-A Roll
(Felt S, 2" pivot, and 6000 pli)

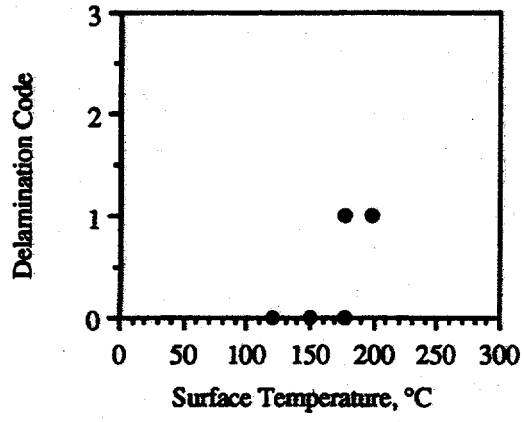

Figure C139. Furnish WF1.

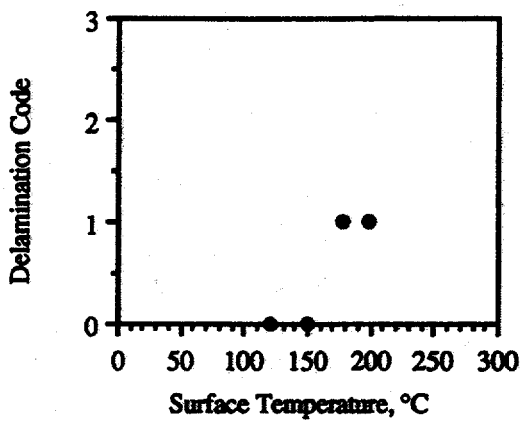

Figure C140. Furnish WF2.

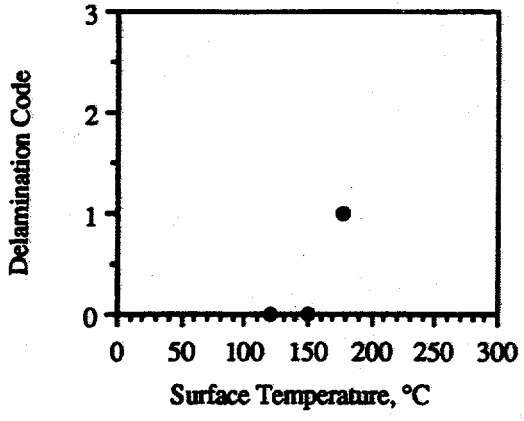

Figure C141. Furnish WF3.

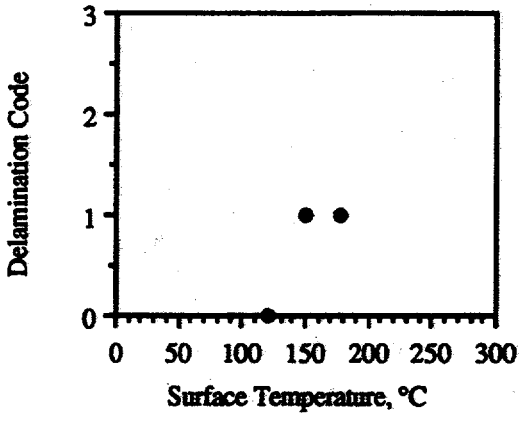

Figure C142. Furnish FD5.

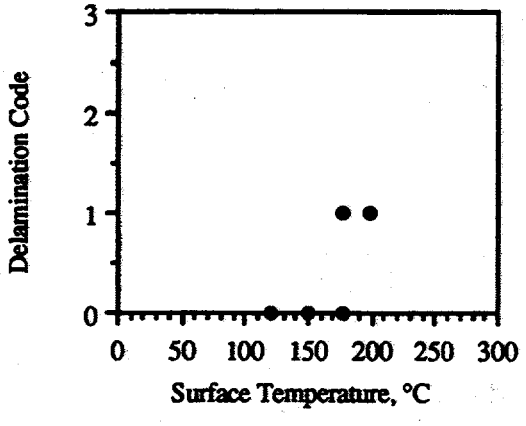

Figure C143. Furnish FD6.

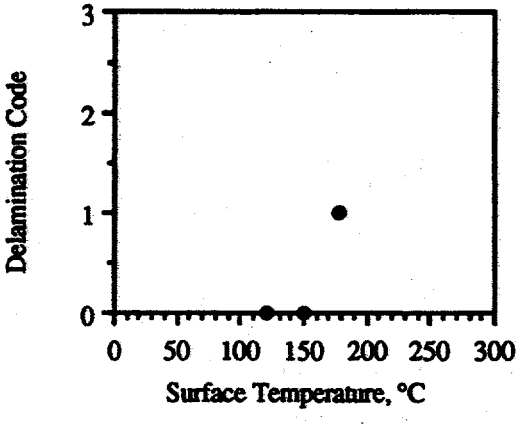

Figure C144. Furnish FD7.

Case A4F- SEM and %CV of SEM for Impulse Drying with the Beloit-A Roll
(Felt S, 0 pivot, 6000 pli, and 1500 fpm)

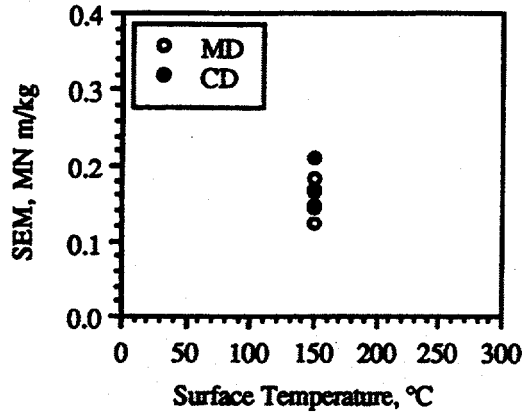

Figure C145. SEM for Furnish WF2.

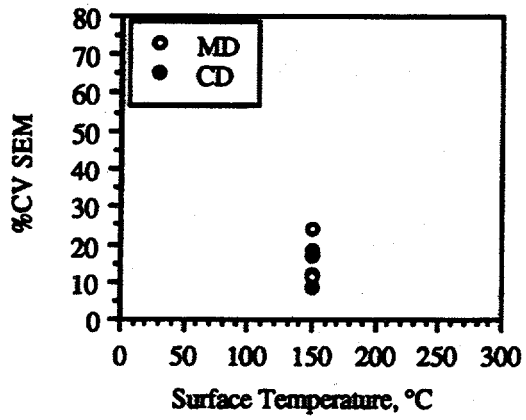

Figure C146. %CV of SEM for Furnish WF2.

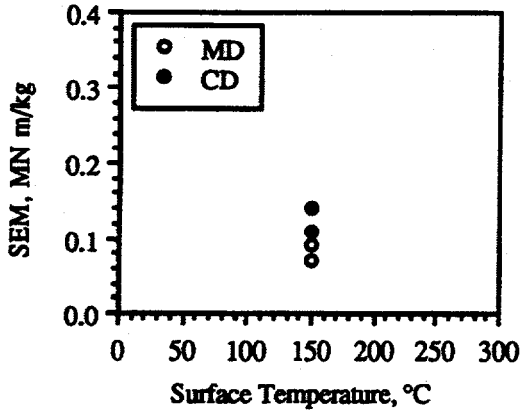

Figure C147. SEM for Furnish WF3.

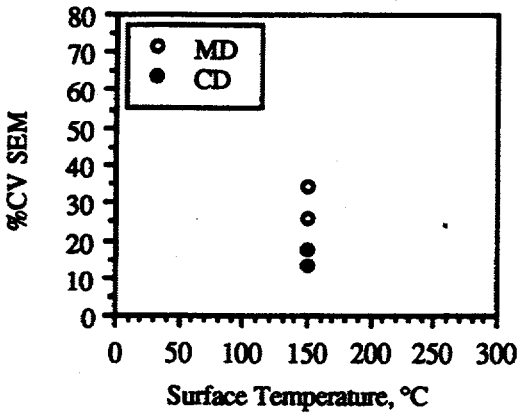

Figure C148. %CV of SEM for Furnish WF3.

Case A4F- SEM and %CV of SEM for Impulse Drying with the Beloit-A Roll
(Felt S, 0 pivot, 6000 pli, and 1500 fpm)

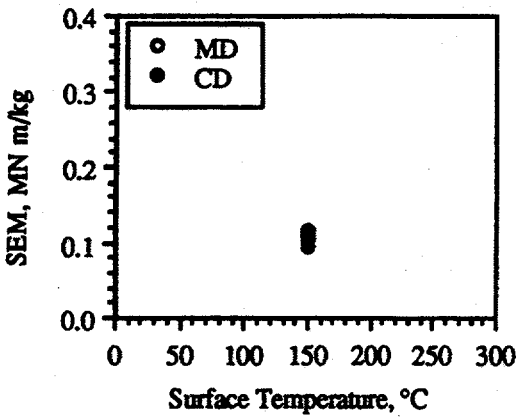

Figure C149. SEM for Furnish FD5.

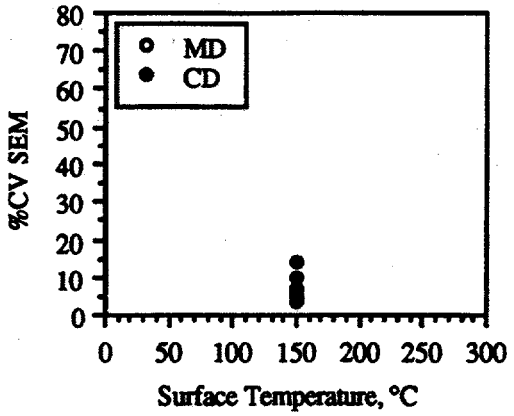

Figure C150. %CV of SEM for Furnish FD5.

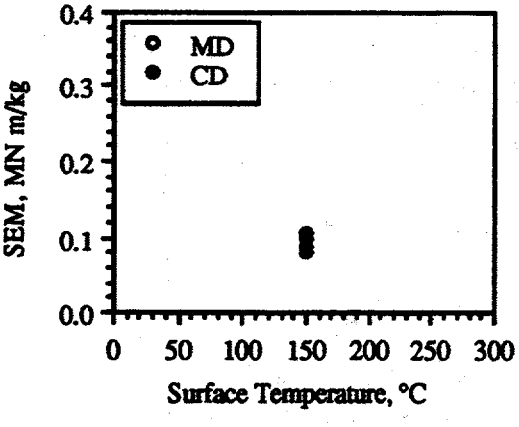

Figure C151. SEM for Furnish FD6.

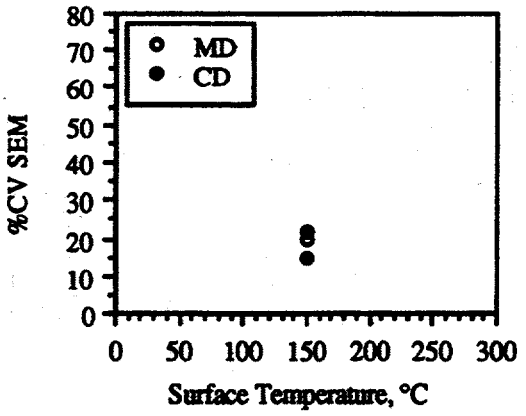

Figure C152. %CV of SEM for Furnish FD6.

Case A4F- Visual Delamination Code for Impulse Drying with the Beloit-A Roll
(Felt S, 0 pivot, 6000 pli, and 1500 fpm)

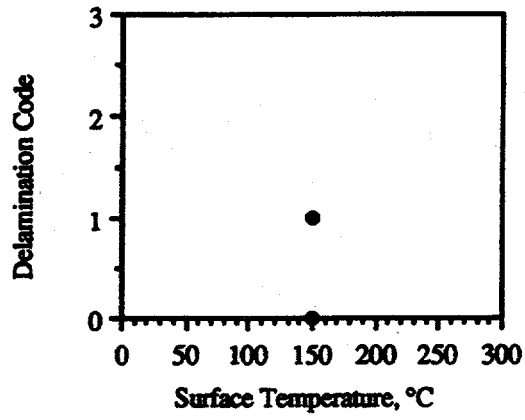

Figure C153. Furnish WF2.

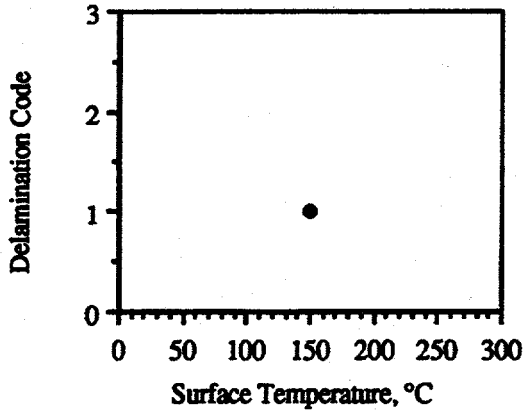

Figure C154. Furnish WF3.

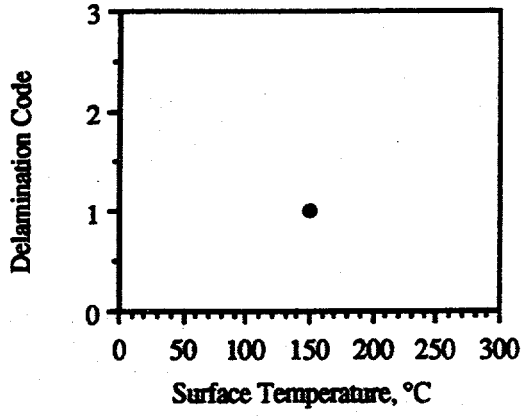

Figure C155. Furnish FD5.

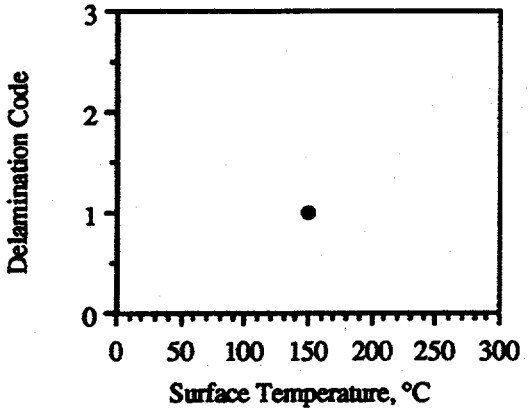

Figure C156. Furnish FD6.

Case A5F- SEM and %CV of SEM for Impulse Drying with the Beloit-A Roll
(Felt S, 0 pivot, 8500 pli, and 1500 fpm)

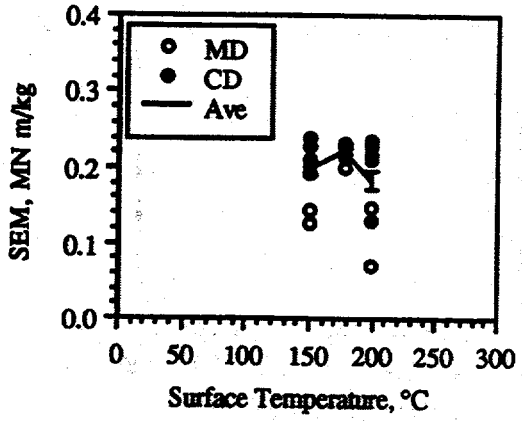

Figure C157. SEM for Furnish WF1.

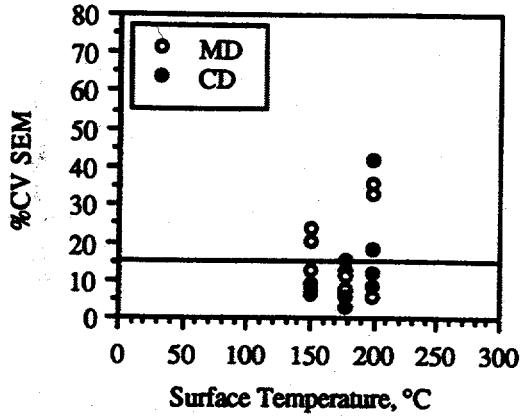

Figure C158. %CV of SEM for Furnish WF1.

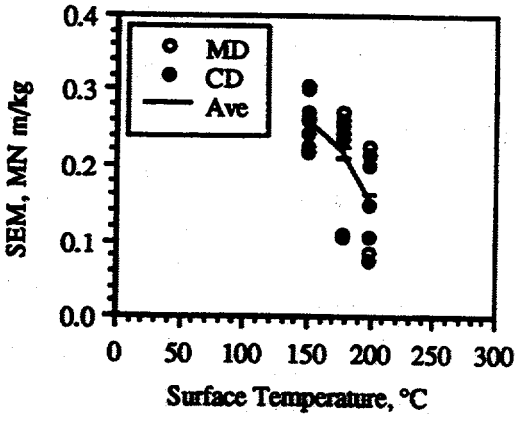

Figure C159. SEM for Furnish WF2.

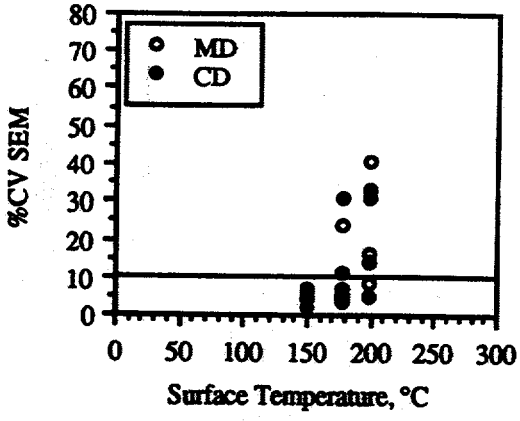

Figure C160. %CV of SEM for Furnish WF2.

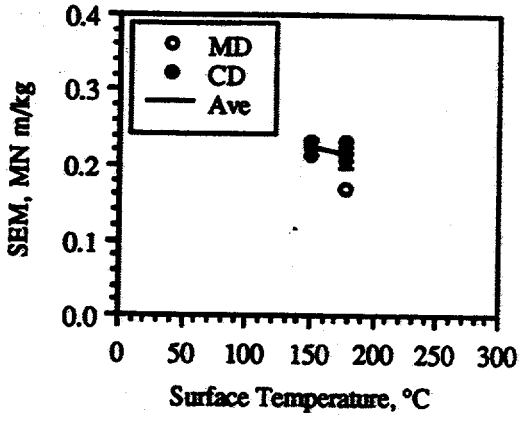

Figure C161. SEM for Furnish WF3.

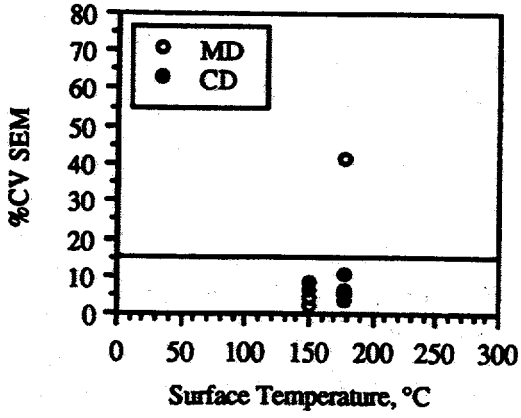

Figure C162. %CV of SEM for Furnish WF3.

Case A5F- SEM and %CV of SEM for Impulse Drying with the Beloit-A Roll
(Felt S, 0 pivot, 8500 pli, and 1500 fpm)

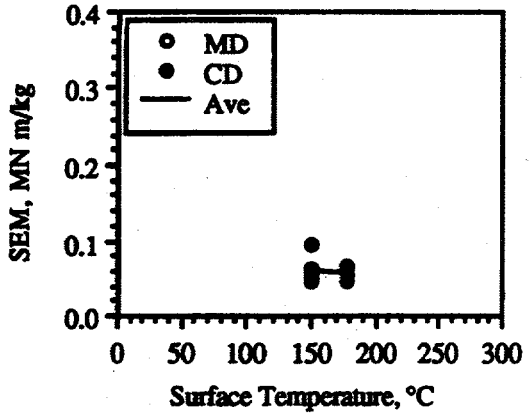

Figure C163. SEM for Furnish FD5.

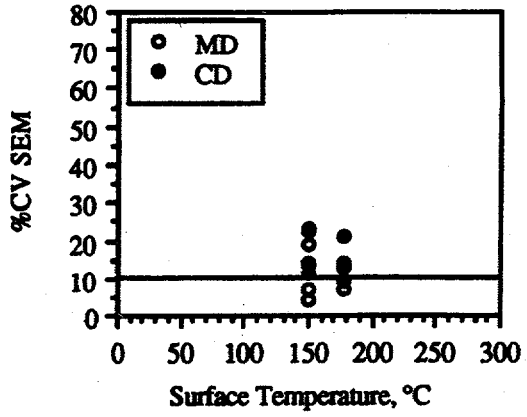

Figure C164. %CV of SEM for Furnish FD5.

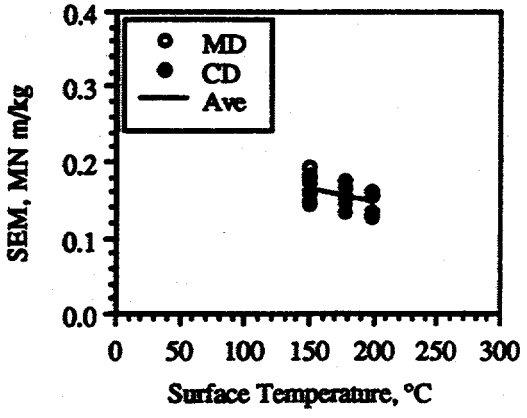

Figure C165. SEM for Furnish FD6.

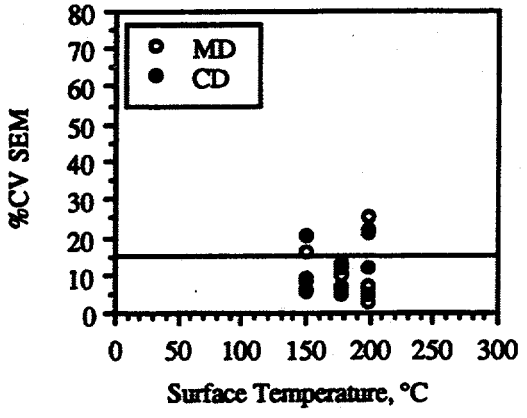

Figure C166. %CV of SEM for Furnish FD6.

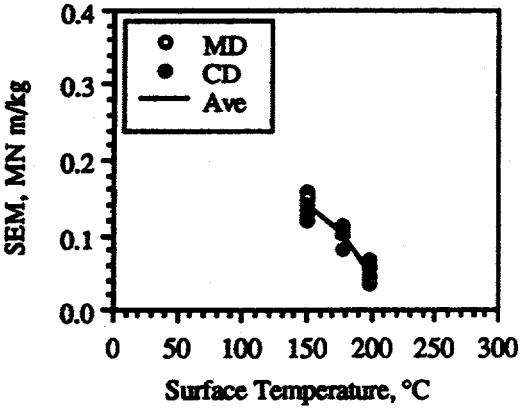

Figure C167. SEM for Furnish FD7.

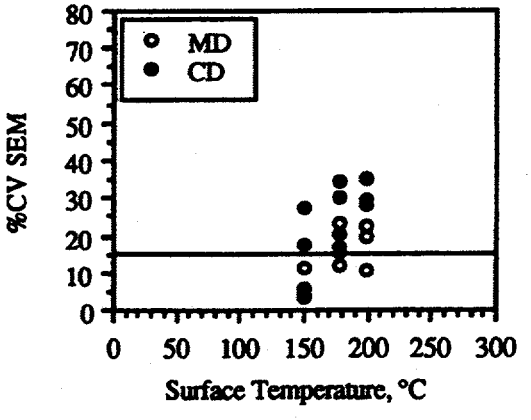

Figure C168. %CV of SEM for Furnish FD7.

Case A5F- Visual Delamination Code for Impulse Drying with the Beloit-A Roll
(Felt S, 0 pivot, 8500 pli, and 1500 fpm)

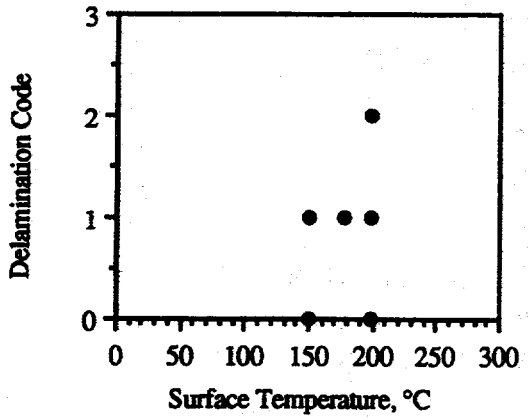

Figure C169. Furnish WF1.

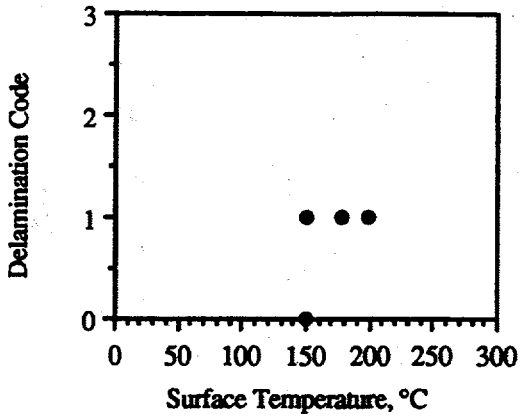

Figure C170. Furnish WF2.

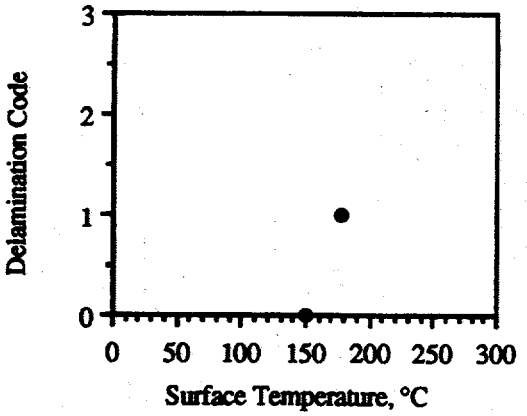

Figure C171. Furnish WF3.

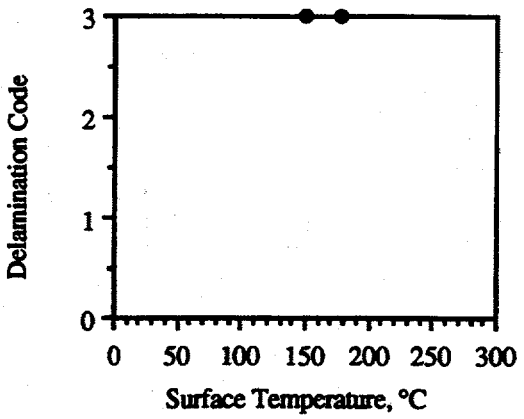

Figure C172. Furnish FD5.

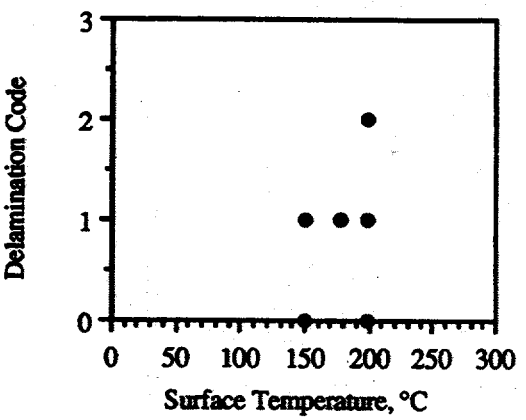

Figure C173. Furnish FD6.

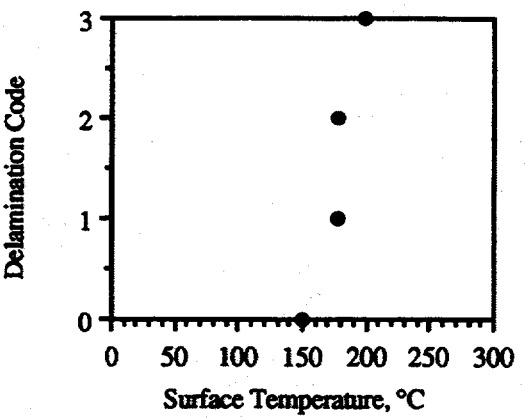

Figure C174. Furnish FD7.

Case A4H- SEM and %CV of SEM for Impulse Drying with the Beloit-A Roll
(Felt S, 0 pivot, 6000 pli, and normal building felt wash water)

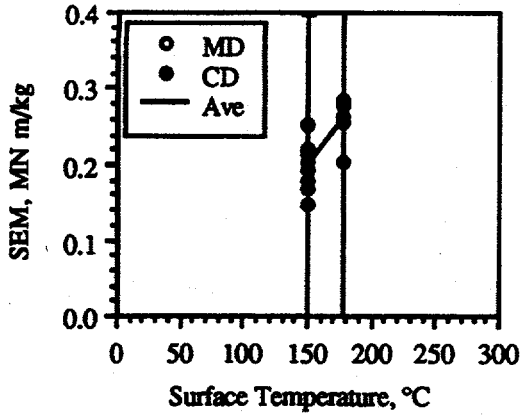

Figure C175. SEM for Furnish WF1.

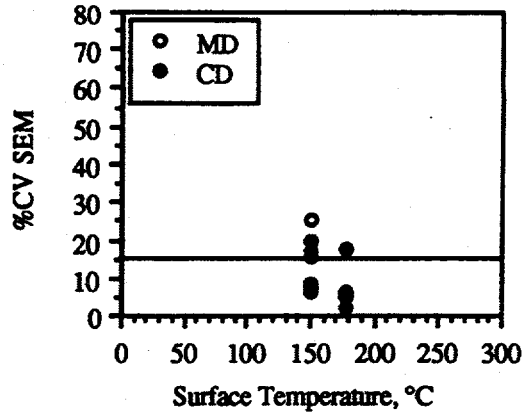

Figure C176. %CV of SEM for Furnish WF1.

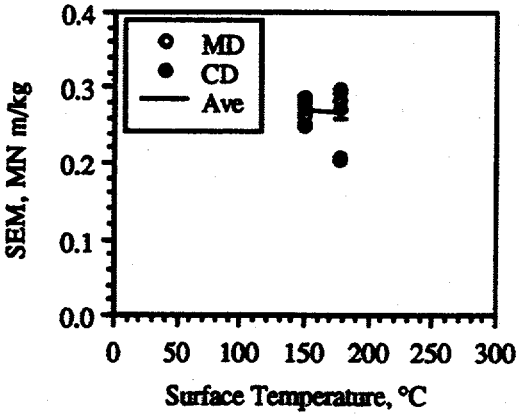

Figure C177. SEM for Furnish WF2.

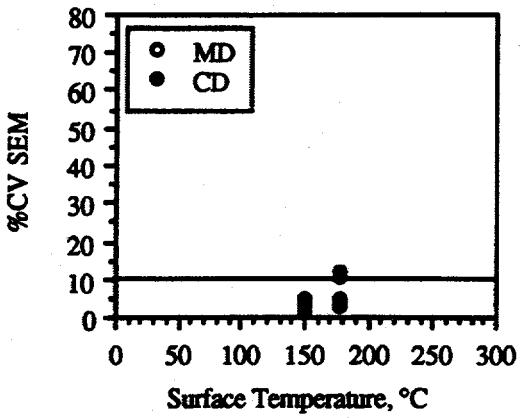

Figure C178. %CV of SEM for Furnish WF2.

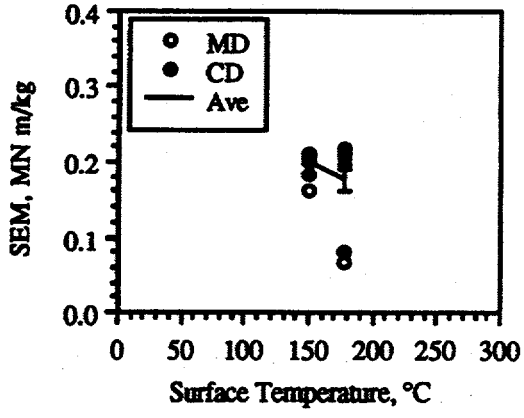

Figure C179. SEM for Furnish WF3.

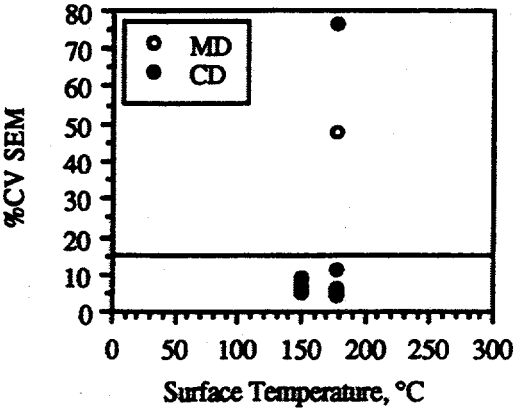

Figure C180. %CV of SEM for Furnish WF3.

Case A4H- SEM and %CV of SEM for Impulse Drying with the Beloit-A Roll
(Felt S, 0 pivot, 6000 pli, and normal building felt wash water)

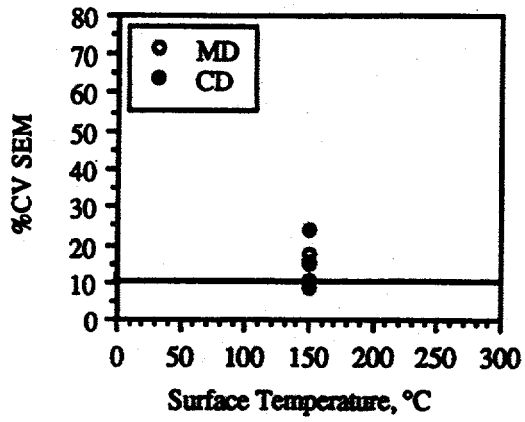

Figure C181. %CV of SEM for Furnish FD5.

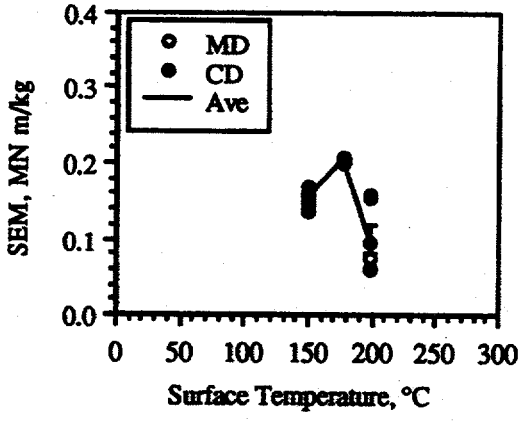

Figure C182. SEM for Furnish FD6.

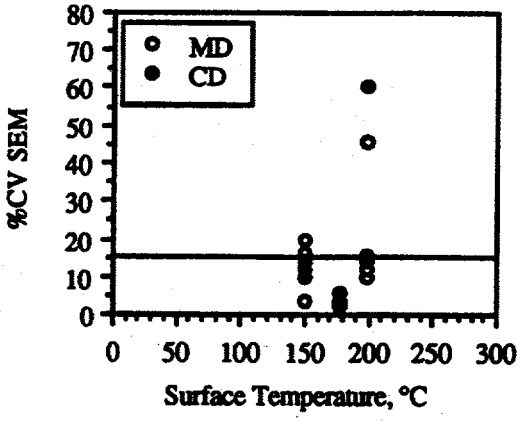

Figure C183. %CV of SEM for Furnish FD6.

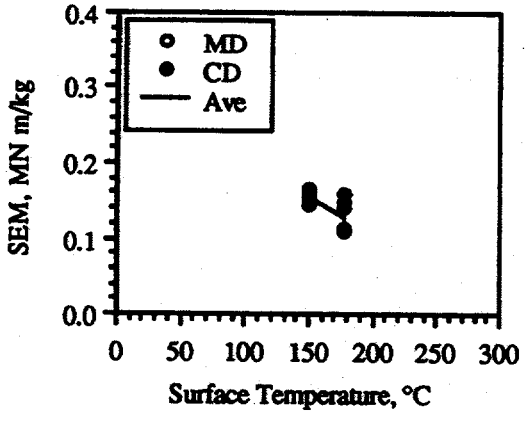

Figure C184. SEM for Furnish FD7.

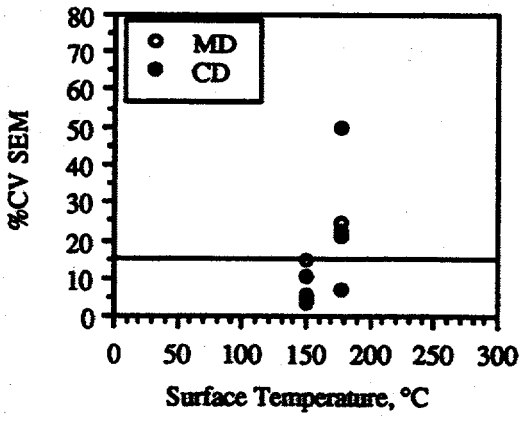

Figure C185. %CV of SEM for Furnish FD7.

Case A4H- Visual Delamination Code for Impulse Drying with the Beloit-A Roll
(Felt S, 0 pivot, 6000 pli, and normal building felt wash water)

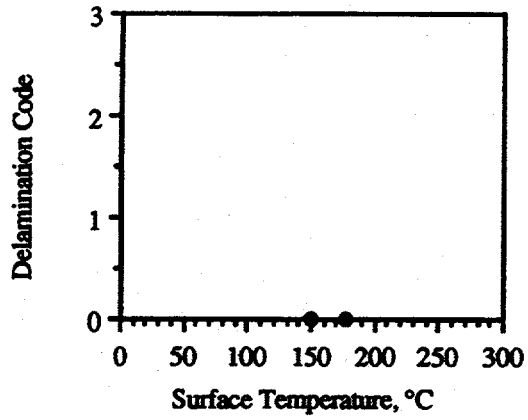

Figure C186. Furnish WF1.

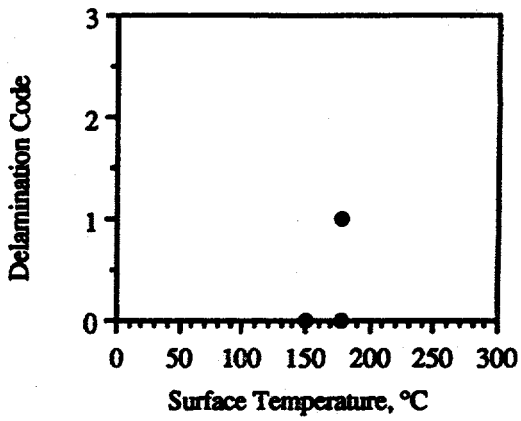

Figure C187. Furnish WF2.

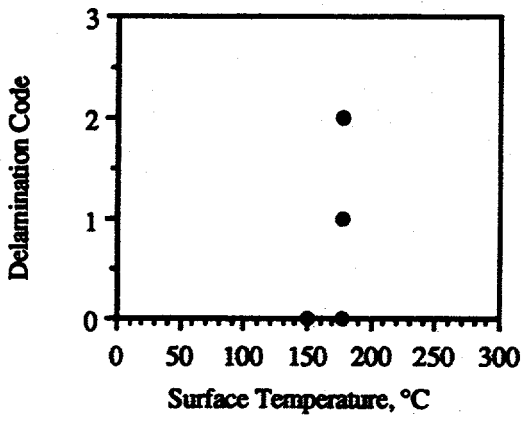

Figure C188. Furnish WF3.

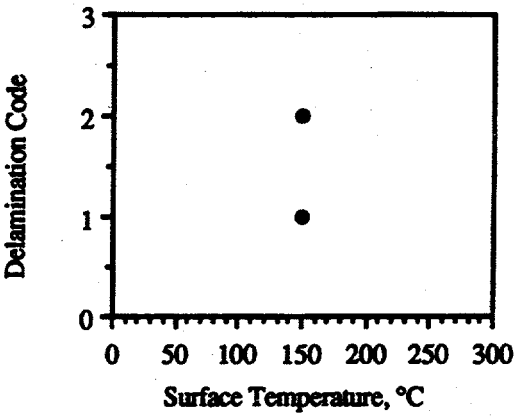

Figure C189. Furnish FD5.

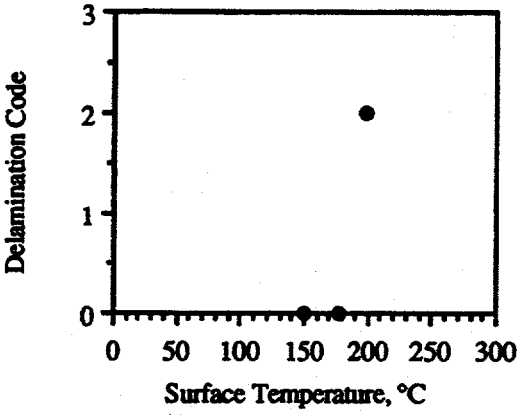

Figure C190. Furnish FD6.

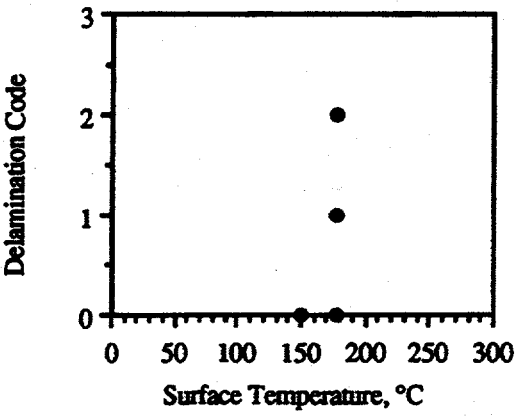

Figure C191. Furnish FD7.

Case A5H- SEM and %CV of SEM for Impulse Drying with the Beloit-A Roll
(Felt S, 0 pivot, 8500 pli, and normal building felt wash water)

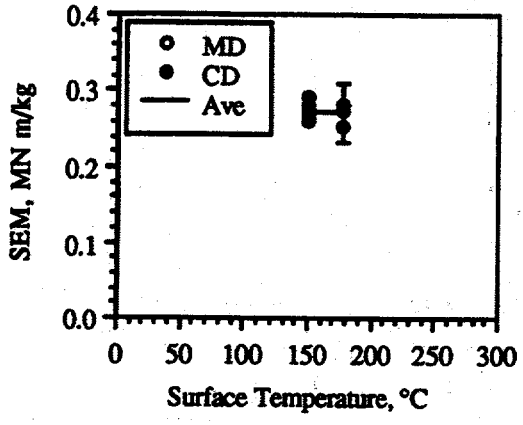

Figure C192. SEM for Furnish WF1.

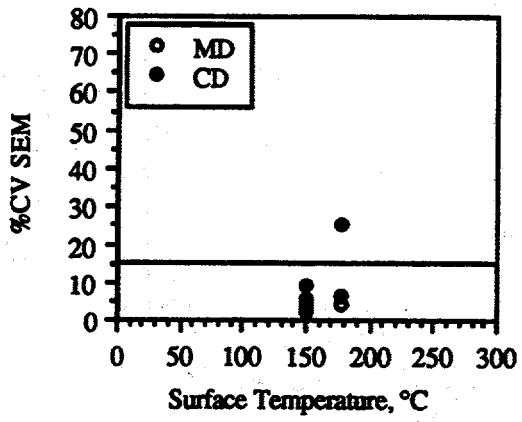

Figure C193. %CV of SEM for Furnish WF1.

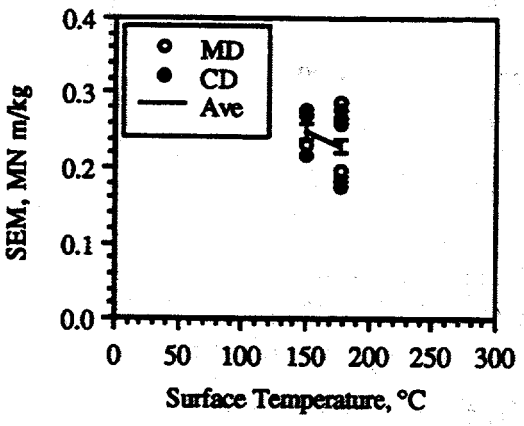

Figure C194. SEM for Furnish WF2.

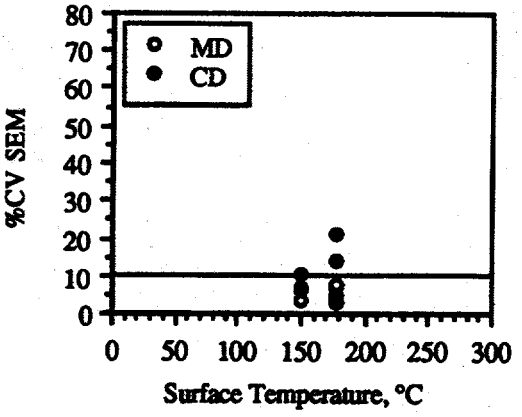

Figure C195. %CV of SEM for Furnish WF2.

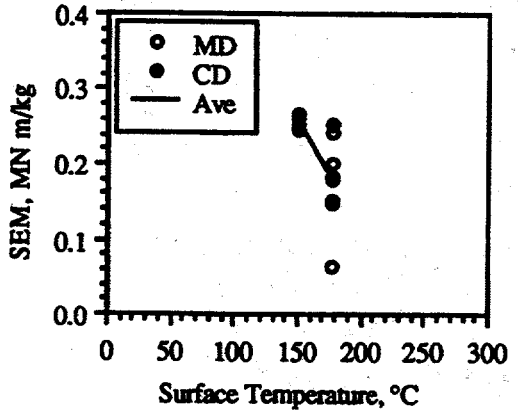

Figure C196. SEM for Furnish WF3.

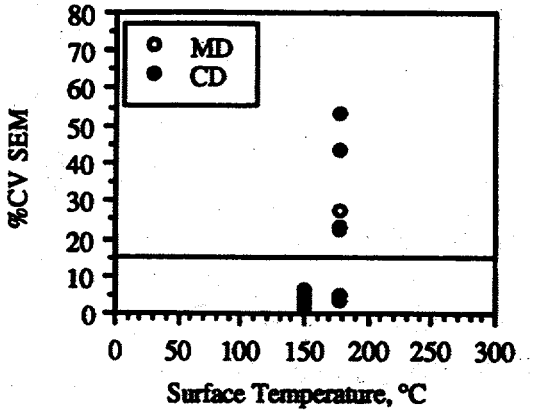

Figure C197. %CV of SEM for Furnish WF3.

Case A5H- SEM and %CV of SEM for Impulse Drying with the Beloit-A Roll
(Felt S, 0 pivot, 8500 pli, and normal building felt wash water)

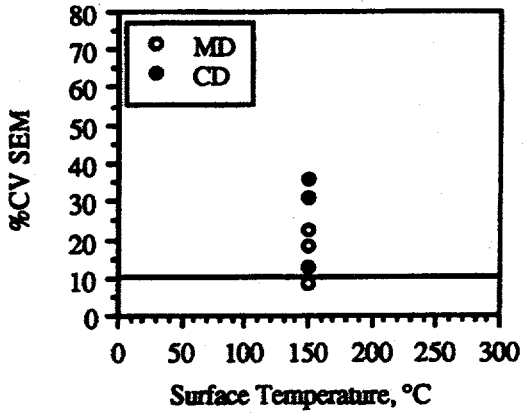

Figure C198. %CV of SEM for Furnish FD5.

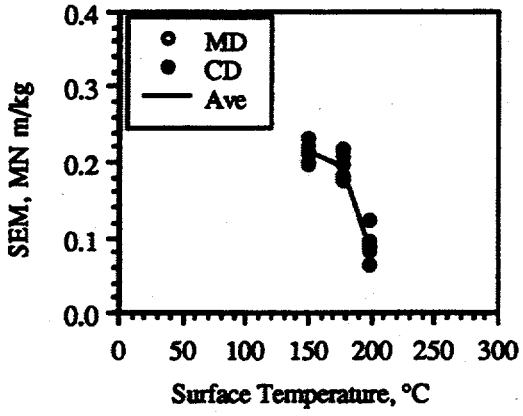

Figure C199. SEM for Furnish FD6.

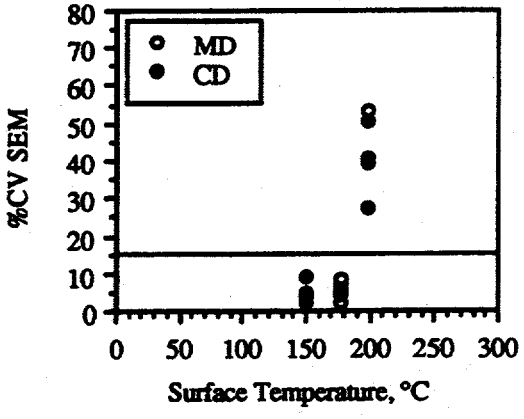

Figure C200. %CV of SEM for Furnish FD6.

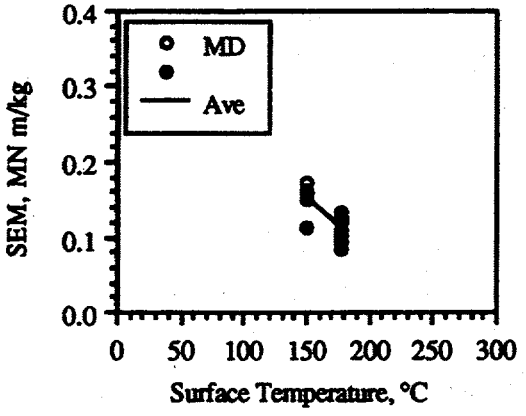

Figure C201. SEM for Furnish FD7.

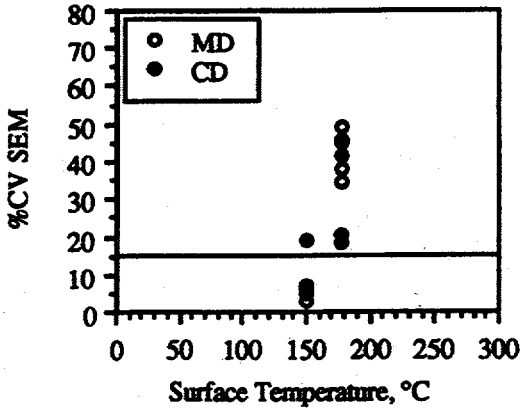

Figure C202. %CV of SEM for Furnish FD7.

Case A5H- Visual Delamination Code for Impulse Drying with the Beloit-A Roll
(Felt S, 0 pivot, 8500 pli, and normal building felt wash water)

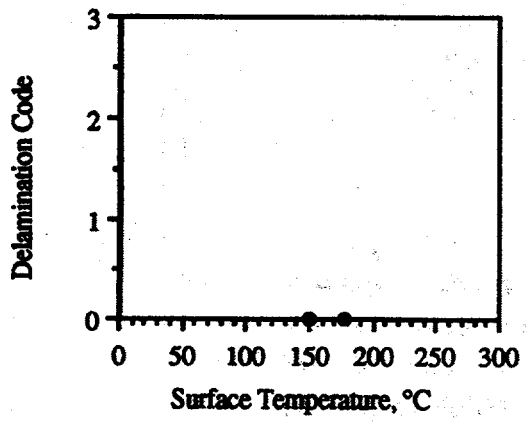

Figure C203. Furnish WF1.

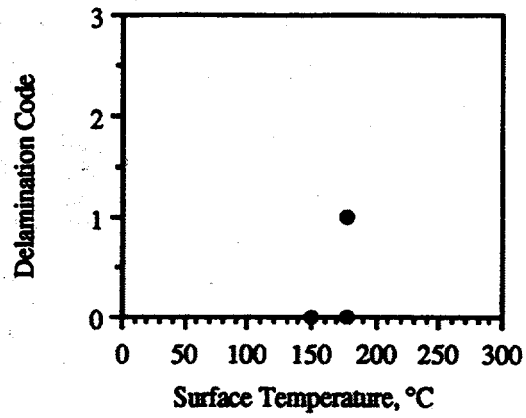

Figure C204. Furnish WF2.

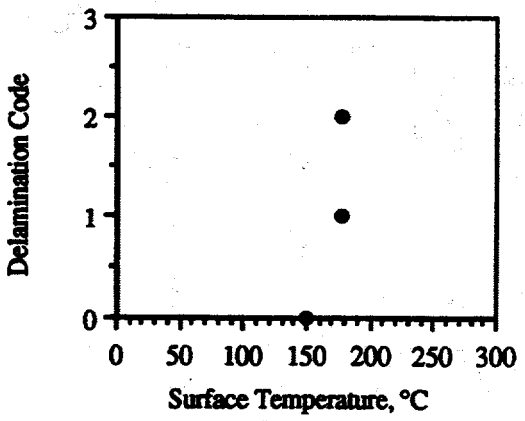

Figure C205. Furnish WF3.

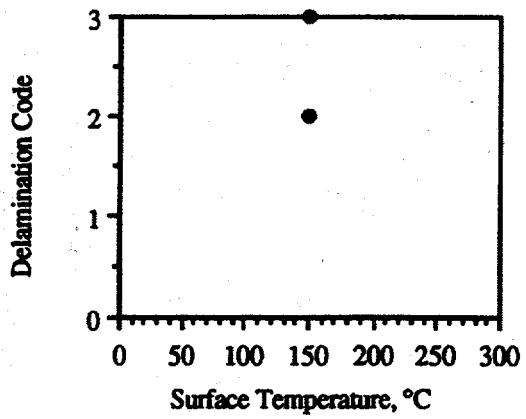

Figure C206. Furnish FD5.

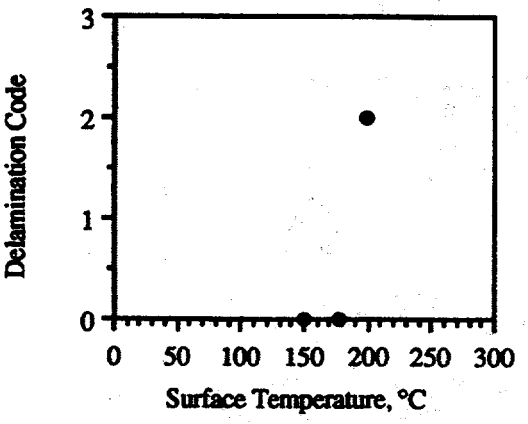

Figure C207. Furnish FD6.

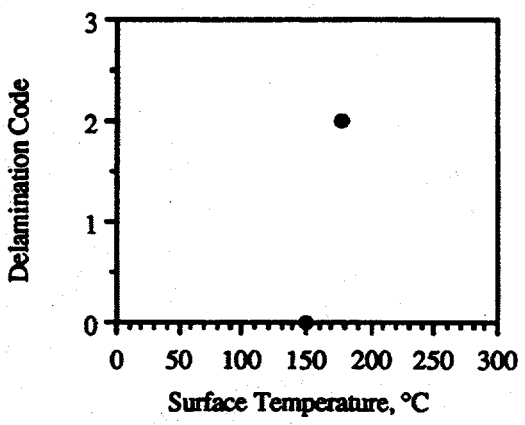

Figure C208. Furnish FD7.

APPENDIX D

The following figures show permeability versus porosity data for each furnish produced.

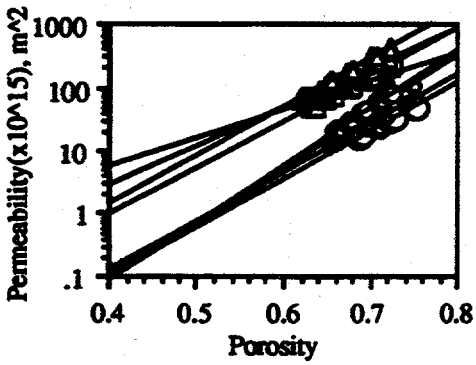

Figure D1. Furnish WF1.

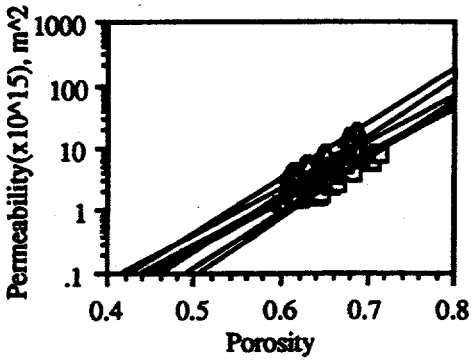

Figure D2. Furnish WF2.

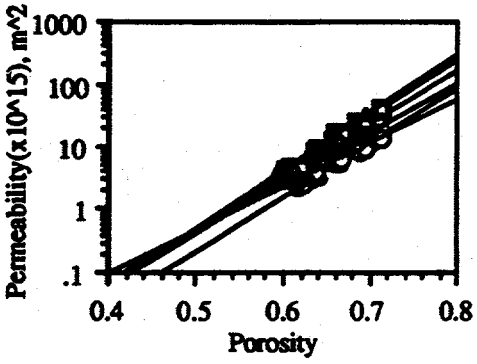

Figure D3. Furnish WF3.

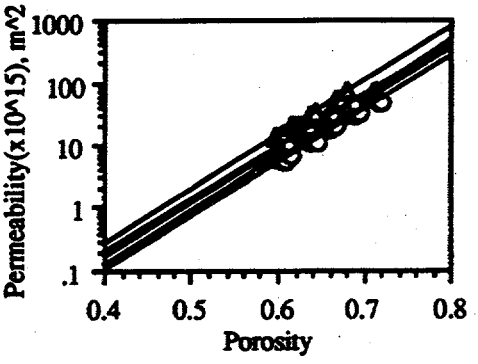

Figure D4 Furnish WF4.

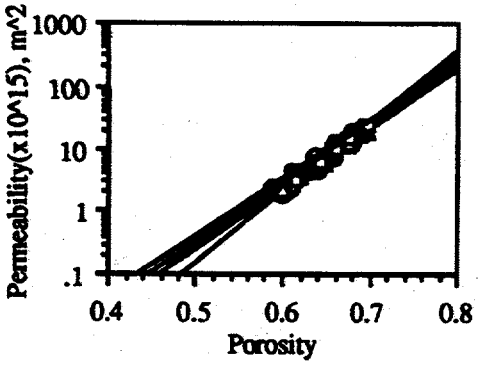

Figure D5. Furnish WF5.

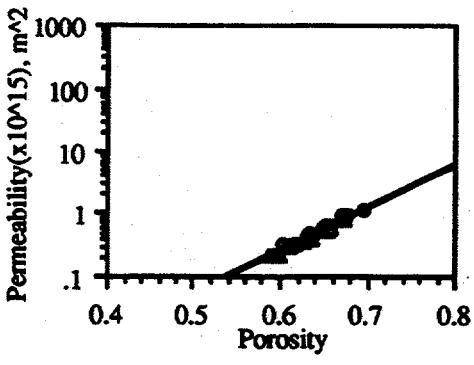

Figure D6. Furnish FD5.

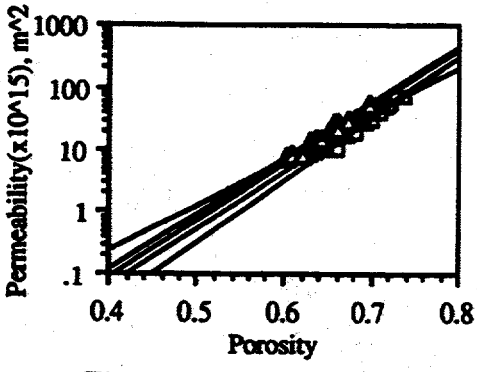

Figure D7. Furnish FD6.

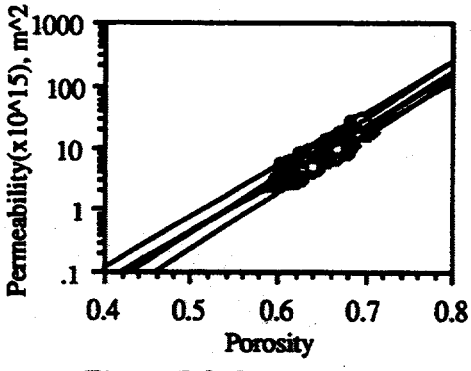

Figure D8. Furnish FD7.

APPENDIX E

APPENDIX E

Hypothesis testing results are reported in this appendix. The results from hypothesis tests are reported in the lower-left part of the tables, and are read from the top down and from left to right. The probability of the test conclusion being in error is shown in the top-right part of the tables. The probability of the conclusion being correct is then 1 minus the value in the table. For example, from the table below, Case 5 is greater than Case 2 with a probability of 0.9719 (1-0.0281).

Case	1	2	3	4	5	6	Case
1		0.273	0.3329	0.0251	0.0422		1
2	?(<)			0.7721	0.0281		2
3	?(>)			0.0278		0.5854	3
4	<	?(<)	<		0.008	0.0214	4
5	>	>		>		0.5478	5
6			?(<)	>	?(<)		6
Case	1	2	3	4	5	6	Case

If the probability of a correct conclusion is less than 0.90, then the test result is shown as a question mark with the trend shown in parentheses.

Table E1. Results of Hypothesis Test 0 for Outgoing Solids and furnish WF1.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con																										Con
D1	id																									D1
D2	id	?																								D2
D3	id	?																								D3
D4	id	?																								D4
D5	id		?		?																					D5
D6	id			?	?																					D6
C1S	id	?																								C1S
C2S	id		?					?																		C2S
C3S	id			?				?																		C3S
A1S	id	?						?																		A1S
A4S	id				?						?															A4S
A5S	id					id						id														A5S
C1	id	>						?																		C1
C2	id		?						?					?												C2
C3	id			?						?				?												C3
A1	id	>									>			?												A1
A2	id		>												?		?									A2
A4	id				>							>					?									A4
A5	id					>							id					?	?							A5
A6	id						>												?							A6
A4F	id				id														id							A4F
A5F	id					>														?		id				A5F
A4H	id				?														?							A4H
A5H	id					>														?				?		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E2. Results of Hypothesis Test 0 for Outgoing Solids and furnish WF2.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con																										Con
D1	id																									D1
D2	id	?																								D2
D3	id	?																								D3
D4	id	?																								D4
D5	id		?		?																					D5
D6	id			?	?																					D6
C1S	id	?																								C1S
C2S	id		?					?																		C2S
C3S	id			?				?																		C3S
A1S	id	id						id																		A1S
A4S	id				?						id															A4S
A5S	id					?						?														A5S
C1	id	?						?																		C1
C2	id		?						?					?												C2
C3	id			?						?				?												C3
A1	id	?									id			?												A1
A2	id		?												?		?									A2
A4	id				?							>					?									A4
A5	id					?							>					?	?							A5
A6	id						>												?							A6
A4F	id				id														id							A4F
A5F	id					?														?		id				A5F
A4H	id				?														?							A4H
A5H	id					?														?				?		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E3. Results of Hypothesis Test 0 for Outgoing Solids and furnish WF3.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con																										Con
D1	id																									D1
D2	id	>																								D2
D3	id	?																								D3
D4	id	?																								D4
D5	id		?		?																					D5
D6	id			?	?																					D6
C1S	id	?																								C1S
C2S	id		?					?																		C2S
C3S	id			?				?																		C3S
A1S	id	id						id																		A1S
A4S	id				?						id															A4S
A5S	id					?						?														A5S
C1	id	>						?																		C1
C2	id		?						?					?												C2
C3	id			?						?				?												C3
A1	id	>									id			?												A1
A2	id		?												?		?									A2
A4	id				?							>					?									A4
A5	id					>							?					?	?							A5
A6	id						>												?							A6
A4F	id				id														id							A4F
A5F	id					>														?		id				A5F
A4H	id				?														?							A4H
A5H	id					>														?				?		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E4. Results of Hypothesis Test 0 for Outgoing Solids and furnish FD5.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con																										Con
D1	id																									D1
D2	id	?																								D2
D3	id	?																								D3
D4	id	?																								D4
D5	id		?		?																					D5
D6	id			?	?																					D6
C1S	id	?																								C1S
C2S	id		?					?																		C2S
C3S	id			?				?																		C3S
A1S	id	id						id																		A1S
A4S	id				?						id															A4S
A5S	id					?						?														A5S
C1	id	?						?																		C1
C2	id		?						?					?												C2
C3	id			?						?				?												C3
A1	id	?									id			?												A1
A2	id		?												?		?									A2
A4	id				>							?					?									A4
A5	id					?							?					?	?							A5
A6	id						?												?							A6
A4F	id				id														id							A4F
A5F	id					?														?		id				A5F
A4H	id				id														id							A4H
A5H	id					id														id				id		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E5. Results of Hypothesis Test 0 for Outgoing Solids and furnish FD6.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con																										Con
D1	id																									D1
D2	id	?																								D2
D3	id	?																								D3
D4	id	?																								D4
D5	id		?		?																					D5
D6	id			?	?																					D6
C1S	id	?																								C1S
C2S	id		?					?																		C2S
C3S	id			?				?																		C3S
A1S	id	id						id																		A1S
A4S	id				?						id															A4S
A5S	id					?						?														A5S
C1	id	>						?																		C1
C2	id		>						?					?												C2
C3	id			>						>				?												C3
A1	id	>									id			?												A1
A2	id		>												?		?									A2
A4	id				?							>					<									A4
A5	id					>							>					?	?							A5
A6	id						>												?							A6
A4F	id				id														id							A4F
A5F	id					>														?		id				A5F
A4H	id				>														?							A4H
A5H	id					>														?				?		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E6. Results of Hypothesis Test 0 for Outgoing Solids and furnish FD7.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con																										Con
D1	id																									D1
D2	id	?																								D2
D3	id	?																								D3
D4	id	?																								D4
D5	id		?		>																					D5
D6	id			?	?																					D6
C1S	id	?																								C1S
C2S	id		>					?																		C2S
C3S	id			?				?																		C3S
A1S	id	id						id																		A1S
A4S	id				?						id															A4S
A5S	id					<						?														A5S
C1	id	?						?																		C1
C2	id		?						?					?												C2
C3	id			?						>				?												C3
A1	id	?									id			?												A1
A2	id		>												>		?									A2
A4	id				>							?					?									A4
A5	id					>							>					?	?							A5
A6	id						?												?							A6
A4F	id				id														id							A4F
A5F	id					?														?		id				A5F
A4H	id				>														?							A4H
A5H	id					>														?				?		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E7. Results of Hypothesis Test 0 for Outgoing Solids, comparing furnishes.

Case	Con WF1	Con WF2	Con WF3	Con FD5	Con FD6	Con FD7	D1 WF1	D1 WF2	D1 WF3	D1 FD5	D1 FD6	D1 FD7	D2 WF1	D2 WF2	D2 WF3	D2 FD5	D2 FD6	D2 FD7	Case
Con WF1																			Con WF1
Con WF2	id																		Con WF2
Con WF3	id																		Con WF3
Con FD5	id	id	id																Con FD5
Con FD6	id	id		id															Con FD6
Con FD7			id	id	id														Con FD7
D1 WF1																			D1 WF1
D1 WF2							?												D1 WF2
D1 WF3							?												D1 WF3
D1 FD5							?	?	?										D1 FD5
D1 FD6							?	?		?									D1 FD6
D1 FD7									?	?	?								D1 FD7
D2 WF1																			D2 WF1
D2 WF2													?						D2 WF2
D2 WF3													?						D2 WF3
D2 FD5													?	?	<				D2 FD5
D2 FD6													?	?		>			D2 FD6
D2 FD7															<	?	<		D2 FD7

Case	Con WF1	Con WF2	Con WF3	Con FD5	Con FD6	Con FD7	D1 WF1	D1 WF2	D1 WF3	D1 FD5	D1 FD6	D1 FD7	D2 WF1	D2 WF2	D2 WF3	D2 FD5	D2 FD6	D2 FD7	Case
	D3	D3	D3	D3	D3	D3	D4	D4	D4	D4	D4	D4	D5	D5	D5	D5	D5	D5	
D3 WF1																			D3 WF1
D3 WF2	?																		D3 WF2
D3 WF3	?																		D3 WF3
D3 FD5	?	?	?																D3 FD5
D3 FD6	?	?		>															D3 FD6
D3 FD7			?	?	?														D3 FD7
D4 WF1																			D4 WF1
D4 WF2							?												D4 WF2
D4 WF3							?												D4 WF3
D4 FD5							?	?	?										D4 FD5
D4 FD6							?	?		?									D4 FD6
D4 FD7									?	<	<								D4 FD7
D5 WF1																			D5 WF1
D5 WF2													<						D5 WF2
D5 WF3													?						D5 WF3
D5 FD5													?	?	?				D5 FD5
D5 FD6													?	>		?			D5 FD6
D5 FD7															?	?	<		D5 FD7
Case	D3 WF1	D3 WF2	D3 WF3	D3 FD5	D3 FD6	D3 FD7	D4 WF1	D4 WF2	D4 WF3	D4 FD5	D4 FD6	D4 FD7	D5 WF1	D5 WF2	D5 WF3	D5 FD5	D5 FD6	D5 FD7	Case

Table E8. Results of Hypothesis Test 0 for Outgoing Solids, comparing furnishes continued.

Case	D6 WF1	D6 WF2	D6 WF3	D6 FD5	D6 FD6	D6 FD7	C1S WF1	C1S WF2	C1S WF3	C1S FD5	C1S FD6	C1S FD7	C2S WF1	C2S WF2	C2S WF3	C2S FD5	C2S FD6	C2S FD7	Case
D6 WF1																			D6 WF1
D6 WF2	?																		D6 WF2
D6 WF3	?																		D6 WF3
D6 FD5	?	?	?																D6 FD5
D6 FD6	?	?		?															D6 FD6
D6 FD7			?	?	?														D6 FD7
C1S WF1																			C1S WF1
C1S WF2							?												C1S WF2
C1S WF3							?												C1S WF3
C1S FD5							?	?	?										C1S FD5
C1S FD6							?	?		?									C1S FD6
C1S FD7									?	?	?								C1S FD7
C2S WF1																			C2S WF1
C2S WF2													<						C2S WF2
C2S WF3													?						C2S WF3
C2S FD5													<	?	<				C2S FD5
C2S FD6													?	?		>			C2S FD6
C2S FD7															?	>	?		C2S FD7
Case	D6 WF1 C3S	D6 WF2 C3S	D6 WF3 C3S	D6 FD5 C3S	D6 FD6 C3S	D6 FD7 C3S	C1S WF1 A1S	C1S WF2 A1S	C1S WF3 A1S	C1S FD5 A1S	C1S FD6 A1S	C1S FD7 A1S	C2S WF1 A4S	C2S WF2 A4S	C2S WF3 A4S	C2S FD5 A4S	C2S FD6 A4S	C2S FD7 A4S	Case
C3S WF1																			C3S WF1
C3S WF2	?																		C3S WF2
C3S WF3	?																		C3S WF3
C3S FD5	?	?	<																C3S FD5
C3S FD6	?	?		>															C3S FD6
C3S FD7			<	?	?														C3S FD7
A1S WF1																			A1S WF1
A1S WF2							id												A1S WF2
A1S WF3							id												A1S WF3
A1S FD5							id	id	id										A1S FD5
A1S FD6							id	id		id									A1S FD6
A1S FD7									id	id	id								A1S FD7
A4S WF1																			A4S WF1
A4S WF2													?						A4S WF2
A4S WF3													?						A4S WF3
A4S FD5													?	?	?				A4S FD5
A4S FD6													?	>		?			A4S FD6
A4S FD7															?	?	?		A4S FD7
Case	C3S WF1	C3S WF2	C3S WF3	C3S FD5	C3S FD6	C3S FD7	A1S WF1	A1S WF2	A1S WF3	A1S FD5	A1S FD6	A1S FD7	A4S WF1	A4S WF2	A4S WF3	A4S FD5	A4S FD6	A4S FD7	Case

Table E9. Results of Hypothesis Test 0 for Outgoing Solids, comparing furnishes continued.

Case	A5S WF1	A5S WF2	A5S WF3	A5S FD5	A5S FD6	A5S FD7	C1 WF1	C1 WF2	C1 WF3	C1 FD5	C1 FD6	C1 FD7	C2 WF1	C2 WF2	C2 WF3	C2 FD5	C2 FD6	C2 FD7	Case
A5S WF1																			A5S WF1
A5S WF2	id																		A5S WF2
A5S WF3	id																		A5S WF3
A5S FD5	id	?	?																A5S FD5
A5S FD6	id	?		?															A5S FD6
A5S FD7			?	?	?														A5S FD7
C1 WF1																			C1 WF1
C1 WF2							?												C1 WF2
C1 WF3							?												C1 WF3
C1 FD5							?	?	?										C1 FD5
C1 FD6							?	?		>									C1 FD6
C1 FD7									?	?	?								C1 FD7
C2 WF1																			C2 WF1
C2 WF2													?						C2 WF2
C2 WF3													?						C2 WF3
C2 FD5													?	?	?				C2 FD5
C2 FD6													?	>		?			C2 FD6
C2 FD7															?	?	<		C2 FD7

Case	A5S WF1 C3	A5S WF2 C3	A5S WF3 C3	A5S FD5 C3	A5S FD6 C3	A5S FD7 C3	C1 WF1 A1	C1 WF2 A1	C1 WF3 A1	C1 FD5 A1	C1 FD6 A1	C1 FD7 A1	C2 WF1 A2	C2 WF2 A2	C2 WF3 A2	C2 FD5 A2	C2 FD6 A2	C2 FD7 A2	Case
C3 WF1																			C3 WF1
C3 WF2	?																		C3 WF2
C3 WF3	?																		C3 WF3
C3 FD5	?	?	?																C3 FD5
C3 FD6	?	>		>															C3 FD6
C3 FD7			?	?	?														C3 FD7
A1 WF1																			A1 WF1
A1 WF2							<												A1 WF2
A1 WF3							?												A1 WF3
A1 FD5							?	?	?										A1 FD5
A1 FD6							?	>		?									A1 FD6
A1 FD7									?	?	?								A1 FD7
A2 WF1																			A2 WF1
A2 WF2													<						A2 WF2
A2 WF3													?						A2 WF3
A2 FD5													<	?	?				A2 FD5
A2 FD6													?	>		>			A2 FD6
A2 FD7															?	?	?		A2 FD7
Case	C3 WF1	C3 WF2	C3 WF3	C3 FD5	C3 FD6	C3 FD7	A1 WF1	A1 WF2	A1 WF3	A1 FD5	A1 FD6	A1 FD7	A2 WF1	A2 WF2	A2 WF3	A2 FD5	A2 FD6	A2 FD7	Case

Table E10. Results of Hypothesis Test 0 for Outgoing Solids, comparing furnishes continued.

Case	A4 WF1	A4 WF2	A4 WF3	A4 FD5	A4 FD6	A4 FD7	A5 WF1	A5 WF2	A5 WF3	A5 FD5	A5 FD6	A5 FD7	A6 WF1	A6 WF2	A6 WF3	A6 FD5	A6 FD6	A6 FD7	Case
A4 WF1																			A4 WF1
A4 WF2	?																		A4 WF2
A4 WF3	?																		A4 WF3
A4 FD5	<	?	?																A4 FD5
A4 FD6	?	?		?															A4 FD6
A4 FD7			?	?	?														A4 FD7
A5 WF1																			A5 WF1
A5 WF2							?												A5 WF2
A5 WF3							?												A5 WF3
A5 FD5							<	?	<										A5 FD5
A5 FD6							?	?		>									A5 FD6
A5 FD7									?	?	?								A5 FD7
A6 WF1																			A6 WF1
A6 WF2													<						A6 WF2
A6 WF3													?						A6 WF3
A6 FD5													<	?	?				A6 FD5
A6 FD6													?	>		?			A6 FD6
A6 FD7															?	?	?		A6 FD7
Case	A4 WF1 A5F	A4 WF2 A5F	A4 WF3 A5F	A4 FD5 A5F	A4 FD6 A5F	A4 FD7 A5F	A5 WF1 A4H	A5 WF2 A4H	A5 WF3 A4H	A5 FD5 A4H	A5 FD6 A4H	A5 FD7 A4H	A6 WF1 A5H	A6 WF2 A5H	A6 WF3 A5H	A6 FD5 A5H	A6 FD6 A5H	A6 FD7 A5H	Case
A5F WF1																			A5F WF1
A5F WF2	<																		A5F WF2
A5F WF3	<																		A5F WF3
A5F FD5	?	?	?																A5F FD5
A5F FD6	?	>		>															A5F FD6
A5F FD7			?	?	?														A5F FD7
A4H WF1																			A4H WF1
A4H WF2							?												A4H WF2
A4H WF3							?												A4H WF3
A4H FD5							id	id	id										A4H FD5
A4H FD6							?	?		id									A4H FD6
A4H FD7									?	id	?								A4H FD7
A5H WF1																			A5H WF1
A5H WF2													?						A5H WF2
A5H WF3													?						A5H WF3
A5H FD5													id	id	id				A5H FD5
A5H FD6													?	?		id			A5H FD6
A5H FD7															?	id	?		A5H FD7
Case	A5F WF1	A5F WF2	A5F WF3	A5F FD5	A5F FD6	A5F FD7	A4H WF1	A4H WF2	A4H WF3	A4H FD5	A4H FD6	A4H FD7	A5H WF1	A5H WF2	A5H WF3	A5H FD5	A5H FD6	A5H FD7	Case

Table E11. Results of Hypothesis Test 1 for Outgoing Solids and furnish WF1.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	Con
D1	id		0.0056	0.1985	0.6933			0.8388			0.0775			0.0630			0.0127									D1
D2	id	>				0.3887			0.0093						0.3355			0.0079								D2
D3	id	?(<)					0.2123			0.5998						0.2215										D3
D4	id	?(<)				0.1379	0.2682					0.9010							0.0551			id		0.7702		D4
D5	id		?(<)		?(>)								id							0.0196			0.0513		0.0049	D5
D6	id			?(<)	?(<)																0.0062					D6
C1S	id	?(<)							0.1882	0.6521	0.5545			0.1769												C1S
C2S	id		>					?(>)							0.7270											C2S
C3S	id			?(>)				?(>)								0.7733										C3S
A1S	id	>						?(>)				0.1719					0.0218									A1S
A4S	id				?(<)						?(<)		id						0.0463							A4S
A5S	id					id						id								id						A5S
C1	id	>						?(>)							0.7898	0.6083	0.1804									C1
C2	id		?(>)						?(>)					?(>)				0.2605								C2
C3	id			?(>)						?(>)				?(<)												C3
A1	id	>									>			?(>)				0.9827	0.3728							A1
A2	id		>												?(>)		?(>)			0.5031						A2
A4	id				>							>					?(<)			0.6054	0.5080	id		0.9250		A4
A5	id					>							id					?(<)	?(>)				0.4783		0.7398	A5
A6	id						>												?(>)							A6
A4F	id				id														id				id			A4F
A5F	id					>														?(<)		id				A5F
A4H	id				?(>)														?(>)						0.9901	A4H
A5H	id					>														?(>)				?(<)		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E12. Results of Hypothesis Test 1 for Outgoing Solids and furnish WF2.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	Con
D1	id		0.7657	0.5761	0.1522			0.3162			id			0.6735			0.0224									D1
D2	id	?(>)				0.6580			0.2221						0.1025			0.0266								D2
D3	id	?(<)					0.5087			0.5032						0.1651										D3
D4	id	?(<)				0.2255	0.8750					0.1083							0.2006			id		0.8537		D4
D5	id		?(<)		?(>)								0.0754							0.2147			0.0410		id	D5
D6	id			?(<)	?(<)																0.0014					D6
C1S	id	?(<)							0.0807	0.2751	id			0.3078												C1S
C2S	id		?(>)					>							0.4121											C2S
C3S	id			?(>)				?(>)								0.2606										C3S
A1S	id	id						id				id					id									A1S
A4S	id				?(<)						id		0.1621						0.0624							A4S
A5S	id					<						?(>)								0.0612						A5S
C1	id	?(>)						?(>)							0.4398	0.8096	0.3677									C1
C2	id		?(>)						?(>)					?(>)				0.2759								C2
C3	id			?(>)						?(>)				?(>)												C3
A1	id	>									id			?(>)				0.5033	0.5511							A1
A2	id		>												?(>)		?(>)			0.4768						A2
A4	id				?(>)							>					?(<)			0.7737	0.5826	id		0.9274		A4
A5	id					?(>)							>					?(<)	?(>)				0.8362		id	A5
A6	id						>												?(>)							A6
A4F	id				id														id				id			A4F
A5F	id					>														?(<)		id				A5F
A4H	id				?(>)														?(>)						id	A4H
A5H	id					id														id				id		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E13. Results of Hypothesis Test 1 for Outgoing Solids and furnish WF3.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	Con
D1	id		0.0022	0.4790	0.9063			0.7801			id			0.0297			0.0003									D1
D2	id	>				0.4141			0.2282						0.2259			0.0417								D2
D3	id	?(>)					0.0234			0.2078						0.2055										D3
D4	id	?(<)				0.1368	0.0454					0.1118							0.1836			id		0.0455		D4
D5	id		?(<)		?(>)								id							0.1477			id		0.0003	D5
D6	id			<	<																0.0104					D6
C1S	id	?(>)							0.5520	0.6437	id			0.5642												C1S
C2S	id		?(>)					?(>)							0.4939											C2S
C3S	id			?(>)				?(>)								0.5881										C3S
A1S	id	id						id				id					id									A1S
A4S	id				?(<)						id		id						0.0872							A4S
A5S	id					id						id								id						A5S
C1	id	>						?(>)							0.5517	0.8221	0.0758									C1
C2	id		?(>)						?(>)					?(>)				0.3020								C2
C3	id			?(>)						?(>)				?(>)												C3
A1	id	>									id			>				0.6896	0.6466							A1
A2	id		>												?(>)		?(>)			0.7018						A2
A4	id				?(>)							>					?(<)			0.7500	0.8909	id		0.8783		A4
A5	id					?(>)							id					?(<)	?(>)				id		0.7493	A5
A6	id						>												?(>)							A6
A4F	id				id														id				id			A4F
A5F	id					id														id		id				A5F
A4H	id				>														?(<)						0.1675	A4H
A5H	id					>														?(>)				?(>)		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E14. Results of Hypothesis Test 1for Outgoing Solids and furnish FD5.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	Con
D1	id		0.7884	0.9529	0.0659			0.3519			id			0.0860			0.4533									D1
D2	id	?(>)				0.3237			0.6191						0.1769			0.1915								D2
D3	id	?(<)					0.0909			0.5228						0.4225										D3
D4	id	>				0.5576	0.5457					0.4243							0.1086			id		id		D4
D5	id		?(>)		?(<)								0.5458							0.4675			0.4313		id	D5
D6	id			>	?(<)																0.1610					D6
C1S	id	?(>)							0.9604	0.1997	id			0.2091												C1S
C2S	id		?(>)					?(>)							0.2275											C2S
C3S	id			?(<)				?(<)								0.2881										C3S
A1S	id	id						id				id					id									A1S
A4S	id				?(<)						id		0.3090						0.0650							A4S
A5S	id					?(<)						?(<)								0.1640						A5S
C1	id	>						?(>)							0.6375	0.7569	0.9120									C1
C2	id		?(>)						?(>)					?(>)				0.9606								C2
C3	id			?(>)						?(>)				?(<)												C3
A1	id	?(>)									id			?(>)				0.8656	0.8984							A1
A2	id		?(>)												?(>)		?(>)			0.5417						A2
A4	id				?(>)							>					?(>)			0.2474	0.7225	id		id		A4
A5	id					?(>)							?(>)					?(<)	?(<)				0.6628		id	A5
A6	id						?(>)												?(>)							A6
A4F	id				id														id				id			A4F
A5F	id					?(>)														?(>)		id				A5F
A4H	id				id														id						id	A4H
A5H	id					id														id				id		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E Results of Hypothesis Test 1for Outgoing Solids and furnish FD5.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	Con
D1	id		0.7884	0.9529	0.0659			0.3519			id			0.0860			0.4533									D1
D2	id	?(>)				0.3237			0.6191						0.1769			0.1915								D2
D3	id	?(<)					0.0909			0.5228						0.4225										D3
D4	id	>				0.5576	0.5457					0.4243							0.1086			id		id		D4
D5	id		?(>)		?(<)								0.5458							0.4675			0.4313		id	D5
D6	id			>	?(<)																0.1610					D6
C1S	id	?(>)							0.9604	0.1997	id			0.2091												C1S
C2S	id		?(>)					?(>)							0.2275											C2S
C3S	id			?(<)				?(<)								0.2881										C3S
A1S	id	id						id				id					id									A1S
A4S	id				?(<)						id		0.3090						0.0650							A4S
A5S	id					?(<)						?(<)								0.1640						A5S
C1	id	>						?(>)							0.6375	0.7569	0.9120									C1
C2	id		?(>)						?(>)					?(>)				0.9606								C2
C3	id			?(>)						?(>)				?(<)												C3
A1	id	?(>)									id			?(>)				0.8656	0.8984							A1
A2	id		?(>)												?(>)		?(>)			0.5417						A2
A4	id				?(>)							>					?(>)			0.2474	0.7225	id		id		A4
A5	id					?(>)							?(>)					?(<)	?(<)				0.6628		id	A5
A6	id						?(>)												?(>)							A6
A4F	id				id														id				id			A4F
A5F	id					?(>)														?(>)		id				A5F
A4H	id				id														id						id	A4H
A5H	id					id														id				id		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E16. Results of Hypothesis Test 1 for Outgoing Solids and furnish FD7.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	Con
D1	id		id	id	id			id			id			id			id									D1
D2	id	id				0.0134			0.0002						0.4582			0.0001								D2
D3	id	id					id			0.2656						0.0114										D3
D4	id	id				0.0034	id					0.9073							0.0879			id		0.0162		D4
D5	id		<		>								err							0.0867			0.3846		id	D5
D6	id			id	id																id					D6
C1S	id	id							0.0127	0.0569	id			0.0702												C1S
C2S	id		>					>							0.1190											C2S
C3S	id			?(<)				<								0.0030										C3S
A1S	id	id						id				id					id									A1S
A4S	id				?(>)						id		0.8213						0.1066							A4S
A5S	id					<						?(<)								0.0272						A5S
C1	id	id						>							0.1969	0.4236	0.5289									C1
C2	id		?(>)						?(<)					?(<)				0.0011								C2
C3	id			>						>				?(>)												C3
A1	id	id									id			?(>)				0.1159	0.5150							A1
A2	id		>												>		?(>)			0.0782						A2
A4	id				>							?(>)					?(<)			0.8530	0.6369	id		0.8832		A4
A5	id					>							>					<	?(>)				0.9785		id	A5
A6	id						id												?(>)							A6
A4F	id				id														id				id			A4F
A5F	id					?(>)														?(<)		id				A5F
A4H	id				>														?(>)						id	A4H
A5H	id					id														id				id		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E17. Results of Hypothesis Test 1 for Outgoing Solids, comparing furnishes.

Case	Con WF1	Con WF2	Con WF3	Con FD5	Con FD6	Con FD7	D1 WF1	D1 WF2	D1 WF3	D1 FD5	D1 FD6	D1 FD7	D2 WF1	D2 WF2	D2 WF3	D2 FD5	D2 FD6	D2 FD7	Case
Con WF1		id	id	id	id														Con WF1
Con WF2	id			id	id														Con WF2
Con WF3	id			id		id													Con WF3
Con FD5	id	id	id		id	id													Con FD5
Con FD6	id	id		id		id													Con FD6
Con FD7			id	id	id														Con FD7
D1 WF1								0.0363	0.5725	0.0175	0.3489								D1 WF1
D1 WF2							<			0.1972	0.0154								D1 WF2
D1 WF3							?(<)			0.0251		id							D1 WF3
D1 FD5							<	?(<)	<		0.0126	id							D1 FD5
D1 FD6							?(>)	>		>		id							D1 FD6
D1 FD7									id	id	id								D1 FD7
D2 WF1														0.0729	0.1081	0.0139	0.6907		D2 WF1
D2 WF2													<			0.4116	0.0722		D2 WF2
D2 WF3													?(<)			0.0203		0.0021	D2 WF3
D2 FD5													<	?(<)	<		0.0069	0.0665	D2 FD5
D2 FD6													?(>)	>		>		0.0013	D2 FD6
D2 FD7															<	>	<		D2 FD7

Case	Con WF1 D3	Con WF2 D3	Con WF3 D3	Con FD5 D3	Con FD6 D3	Con FD7 D3	D1 WF1 D4	D1 WF2 D4	D1 WF3 D4	D1 FD5 D4	D1 FD6 D4	D1 FD7 D4	D2 WF1 D5	D2 WF2 D5	D2 WF3 D5	D2 FD5 D5	D2 FD6 D5	D2 FD7 D5	Case
D3 WF1		0.2730	0.3329	0.0251	0.0422														D3 WF1
D3 WF2	?(<)			0.7721	0.1281														D3 WF2
D3 WF3	?(>)			0.0278		0.5854													D3 WF3
D3 FD5	<	?(<)	<		0.0080	0.0214													D3 FD5
D3 FD6	>	?(>)		>		0.5478													D3 FD6
D3 FD7			?(<)	>	?(<)														D3 FD7
D4 WF1								0.1044	0.9200	0.8065	0.2667								D4 WF1
D4 WF2							?(<)			0.0652	0.0077								D4 WF2
D4 WF3							?(>)			0.5930		0.1329							D4 WF3
D4 FD5							?(<)	>	?(<)		0.0734	0.0104							D4 FD5
D4 FD6							?(>)	>		>		0.0120							D4 FD6
D4 FD7									?(<)	<	<								D4 FD7
D5 WF1														0.0034	0.4737	0.0089	0.6918		D5 WF1
D5 WF2													<			0.5367	0.0042		D5 WF2
D5 WF3													?(<)			0.0205		0.0472	D5 WF3
D5 FD5													<	?(>)	<		0.0168	0.3932	D5 FD5
D5 FD6													?(<)	>		>		0.0028	D5 FD6
D5 FD7															<	?(>)	<		D5 FD7
Case	D3 WF1	D3 WF2	D3 WF3	D3 FD5	D3 FD6	D3 FD7	D4 WF1	D4 WF2	D4 WF3	D4 FD5	D4 FD6	D4 FD7	D5 WF1	D5 WF2	D5 WF3	D5 FD5	D5 FD6	D5 FD7	Case

Table E18. Results of Hypothesis Test 1 for Outgoing Solids, comparing furnishes continued.

Case	D6 WF1	D6 WF2	D6 WF3	D6 FD5	D6 FD6	D6 FD7	C1S WF1	C1S WF2	C1S WF3	C1S FD5	C1S FD6	C1S FD7	C2S WF1	C2S WF2	C2S WF3	C2S FD5	C2S FD6	C2S FD7	Case
D6 WF1		0.4974	0.7196	0.3696	0.7637														D6 WF1
D6 WF2	?(<)			0.0557	0.4105														D6 WF2
D6 WF3	?(<)			0.0773		id													D6 WF3
D6 FD5	?(>)	>	>		0.7143	id													D6 FD5
D6 FD6	?(>)	?(>)		?(<)		id													D6 FD6
D6 FD7			id	id	id														D6 FD7
C1S WF1								0.3365	0.7589	0.6204	0.7172								C1S WF1
C1S WF2							?(<)			0.3731	0.1148								C1S WF2
C1S WF3							?(>)			0.4843		0.9761							C1S WF3
C1S FD5							?(<)	?(>)	?(<)		0.2492	0.0151							C1S FD5
C1S FD6							?(>)	?(>)		?(>)		0.9643							C1S FD6
C1S FD7									?(<)	>	?(<)								C1S FD7
C2S WF1														0.0090	0.0644	0.0015	0.9906		C2S WF1
C2S WF2													<			0.0480	0.2700		C2S WF2
C2S WF3													<			0.0033		0.6883	C2S WF3
C2S FD5													<	<	<		0.1688	0.0073	C2S FD5
C2S FD6													?(<)	?(>)		?(>)		0.5498	C2S FD6
C2S FD7															?(>)	>	?(<)		C2S FD7

Case	D6 WF1 C3S	D6 WF2 C3S	D6 WF3 C3S	D6 FD5 C3S	D6 FD6 C3S	D6 FD7 C3S	C1S WF1 A1S	C1S WF2 A1S	C1S WF3 A1S	C1S FD5 A1S	C1S FD6 A1S	C1S FD7 A1S	C2S WF1 A4S	C2S WF2 A4S	C2S WF3 A4S	C2S FD5 A4S	C2S FD6 A4S	C2S FD7 A4S	Case
C3S WF1		0.5223	0.8625	0.3428	0.8953														C3S WF1
C3S WF2	?(<)			0.1180	0.0159														C3S WF2
C3S WF3	?(>)			0.0113		0.0168													C3S WF3
C3S FD5	?(<)	?(<)	<		0.0081	0.0821													C3S FD5
C3S FD6	?(>)	>		>		0.0055													C3S FD6
C3S FD7			<	>	<														C3S FD7
A1S WF1								id	id	id	id								A1S WF1
A1S WF2							id			id	id								A1S WF2
A1S WF3							id			id		id							A1S WF3
A1S FD5							id	id	id		id	id							A1S FD5
A1S FD6							id	id		id		id							A1S FD6
A1S FD7									id	id	id								A1S FD7
A4S WF1														0.0158	0.2779	0.7118	0.6757		A4S WF1
A4S WF2													<			0.0015	0.0014		A4S WF2
A4S WF3													?(<)			0.0824		0.9833	A4S WF3
A4S FD5													?(<)	>	>		0.8758	0.3979	A4S FD5
A4S FD6													?(<)	>		?(<)		0.4172	A4S FD6
A4S FD7															?(<)	?(<)	?(<)		A4S FD7
Case	C3S WF1	C3S WF2	C3S WF3	C3S FD5	C3S FD6	C3S FD7	A1S WF1	A1S WF2	A1S WF3	A1S FD5	A1S FD6	A1S FD7	A4S WF1	A4S WF2	A4S WF3	A4S FD5	A4S FD6	A4S FD7	Case

Table E19. Results of Hypothesis Test 1 for Outgoing Solids, comparing furnishes continued.

Case	A5S WF1	A5S WF2	A5S WF3	A5S FD5	A5S FD6	A5S FD7	C1 WF1	C1 WF2	C1 WF3	C1 FD5	C1 FD6	C1 FD7	C2 WF1	C2 WF2	C2 WF3	C2 FD5	C2 FD6	C2 FD7	Case
A5S WF1		id	id	id	id														A5S WF1
A5S WF2	id			0.0597	0.0122														A5S WF2
A5S WF3	id			id		id													A5S WF3
A5S FD5	id	>	id		0.1201	0.2959													A5S FD5
A5S FD6	id	>		?(>)		0.0245													A5S FD6
A5S FD7			id	?(<)	<														A5S FD7
C1 WF1								0.1422	0.4724	0.0671	0.5963								C1 WF1
C1 WF2							?(<)			0.9154	0.0573								C1 WF2
C1 WF3							?(<)			0.0724		0.7859							C1 WF3
C1 FD5							<	?(>)	<		0.0154	0.0598							C1 FD5
C1 FD6							?(>)	>		>		0.2405							C1 FD6
C1 FD7									?(>)	>	?(<)								C1 FD7
C2 WF1														0.2337	0.6398	0.1840	0.6071		C2 WF1
C2 WF2													?(<)			0.6744	0.0384		C2 WF2
C2 WF3													?(<)			0.2148		0.1442	C2 WF3
C2 FD5													?(<)	?(<)	?(<)		0.0430	0.8850	C2 FD5
C2 FD6													?(>)	>		>		0.0292	C2 FD6
C2 FD7															?(<)	?(>)	<		C2 FD7
Case	A5S WF1 C3	A5S WF2 C3	A5S WF3 C3	A5S FD5 C3	A5S FD6 C3	A5S FD7 C3	C1 WF1 A1	C1 WF2 A1	C1 WF3 A1	C1 FD5 A1	C1 FD6 A1	C1 FD7 A1	C2 WF1 A2	C2 WF2 A2	C2 WF3 A2	C2 FD5 A2	C2 FD6 A2	C2 FD7 A2	Case
C3 WF1		0.3605	0.8676	0.2802	0.1312														C3 WF1
C3 WF2	?(<)			0.6428	0.0008														C3 WF2
C3 WF3	?(>)			0.1715		0.5558													C3 WF3
C3 FD5	?(<)	?(<)	?(<)		0.0125	0.0581													C3 FD5
C3 FD6	?(>)	>		>		0.2165													C3 FD6
C3 FD7			?(>)	>	?(<)														C3 FD7
A1 WF1								0.0391	0.2290	0.0877	0.8756								A1 WF1
A1 WF2							<			0.6255	0.0040								A1 WF2
A1 WF3							?(<)			0.2619		0.4563							A1 WF3
A1 FD5							<	?(<)	?(<)		0.0977	0.3227							A1 FD5
A1 FD6							?(<)	>		>		0.0373							A1 FD6
A1 FD7									?(<)	?(>)	<								A1 FD7
A2 WF1														0.0131	0.2592	0.0137	0.8772		A2 WF1
A2 WF2													<			0.3734	0.0037		A2 WF2
A2 WF3													?(<)			0.0835		0.7746	A2 WF3
A2 FD5													<	?(<)	<		0.0097	0.0404	A2 FD5
A2 FD6													?(>)	>		>		0.1498	A2 FD6
A2 FD7															?(>)	>	?(<)		A2 FD7
Case	C3 WF1	C3 WF2	C3 WF3	C3 FD5	C3 FD6	C3 FD7	A1 WF1	A1 WF2	A1 WF3	A1 FD5	A1 FD6	A1 FD7	A2 WF1	A2 WF2	A2 WF3	A2 FD5	A2 FD6	A2 FD7	Case

Table E20. Results of Hypothesis Test 1 for Outgoing Solids, comparing furnishes continued.

Case	A4 WF1	A4 WF2	A4 WF3	A4 FD5	A4 FD6	A4 FD7	A5 WF1	A5 WF2	A5 WF3	A5 FD5	A5 FD6	A5 FD7	A6 WF1	A6 WF2	A6 WF3	A6 FD5	A6 FD6	A6 FD7	Case
A4 WF1		0.1638	0.6715	0.0971	0.4460														A4 WF1
A4 WF2	?(<)			0.9006	0.3234														A4 WF2
A4 WF3	?(<)			0.2922		0.6798													A4 WF3
A4 FD5	<	?(>)	?(<)		0.1291	0.4883													A4 FD5
A4 FD6	?(<)	?(>)		?(>)		0.7640													A4 FD6
A4 FD7			?(<)	?(>)	?(<)														A4 FD7
A5 WF1								0.0601	0.4540	0.0019	0.9849								A5 WF1
A5 WF2							<			0.4438	0.1564								A5 WF2
A5 WF3							?(<)			0.0417		0.4435							A5 WF3
A5 FD5							<	?(<)	<		0.0812	0.0888							A5 FD5
A5 FD6							?(>)	?(>)		>		0.2532							A5 FD6
A5 FD7									?(<)	>	?(<)								A5 FD7
A6 WF1														0.0522	0.1918	0.0379	0.6042		A6 WF1
A6 WF2													<			0.7151	0.0116		A6 WF2
A6 WF3													?(<)			0.1297		0.7625	A6 WF3
A6 FD5													<	?(<)	?(<)		0.0193	0.2292	A6 FD5
A6 FD6													?(<)	>		>		0.1768	A6 FD6
A6 FD7															?(<)	?(>)	?(<)		A6 FD7
Case	A4 WF1 A5F	A4 WF2 A5F	A4 WF3 A5F	A4 FD5 A5F	A4 FD6 A5F	A4 FD7 A5F	A5 WF1 A4H	A5 WF2 A4H	A5 WF3 A4H	A5 FD5 A4H	A5 FD6 A4H	A5 FD7 A4H	A6 WF1 A5H	A6 WF2 A5H	A6 WF3 A5H	A6 FD5 A5H	A6 FD6 A5H	A6 FD7 A5H	Case
A5F WF1		0.0196	id	0.0377	0.3498														A5F WF1
A5F WF2	<			0.7601	0.0001														A5F WF2
A5F WF3	id			id		id													A5F WF3
A5F FD5	<	?(<)	id		0.0095	0.5255													A5F FD5
A5F FD6	?(>)	>		>		0.2897													A5F FD6
A5F FD7			id	?(>)	?(<)														A5F FD7
A4H WF1								0.9233	0.8697	id	0.9660								A4H WF1
A4H WF2							?(<)			id	0.9340								A4H WF2
A4H WF3							?(<)			id		0.7881							A4H WF3
A4H FD5							id	id	id		id	id							A4H FD5
A4H FD6							?(<)	?(>)		id		0.1028							A4H FD6
A4H FD7									?(<)	id	?(<)								A4H FD7
A5H WF1														id	0.1601	id	0.6031		A5H WF1
A5H WF2													id			id	id		A5H WF2
A5H WF3													?(<)			id		id	A5H WF3
A5H FD5													id	id	id		id	id	A5H FD5
A5H FD6													?(>)	id		id		id	A5H FD6
A5H FD7															id	id	id		A5H FD7
Case	A5F WF1	A5F WF2	A5F WF3	A5F FD5	A5F FD6	A5F FD7	A4H WF1	A4H WF2	A4H WF3	A4H FD5	A4H FD6	A4H FD7	A5H WF1	A5H WF2	A5H WF3	A5H FD5	A5H FD6	A5H FD7	Case

Table E21. Results of Hypothesis Test 2 for Outgoing Solids and furnish WF1.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	Con
D1	id		0.0056	0.1985	0.6933			0.8388			0.0775			0.0041			0.0004									D1
D2	id	>				0.3887			0.0093						0.1954			0.0002								D2
D3	id	?(<)					0.2123			0.5998						0.2883										D3
D4	id	?(<)				0.1379	0.2682					0.9010							0.0023			id		0.7702		D4
D5	id		?(<)		?(>)								id							0.0002			0.0015		0.0004	D5
D6	id			?(<)	?(<)																0.0004					D6
C1S	id	?(<)							0.1882	0.6521	0.5545			0.1095												C1S
C2S	id		>					?(>)							0.5222											C2S
C3S	id			?(>)				?(>)								0.9454										C3S
A1S	id	>						?(>)				0.1719					0.0010									A1S
A4S	id				?(<)						?(<)		id						0.0014							A4S
A5S	id					id						id								id						A5S
C1	id	>						?(>)							0.9449	0.1384	0.0351									C1
C2	id		?(>)						?(>)					?(>)				0.1145								C2
C3	id			?(>)						?(>)				?(<)												C3
A1	id	>									>			>				0.8254	0.1859							A1
A2	id		>												?(>)		?(<)			0.3148						A2
A4	id				>							>					?(<)			0.5775	0.2952	id		0.9774		A4
A5	id					>							id					?(<)	?(>)				0.2096		0.9292	A5
A6	id						>												?(>)							A6
A4F	id				id														id				id			A4F
A5F	id					>														?(<)		id				A5F
A4H	id				?(>)														?(>)						0.9873	A4H
A5H	id					>														?(>)				?(>)		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E22. Results of Hypothesis Test 2 for Outgoing Solids and furnish WF2.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	Con
D1	id		0.7657	0.5761	0.1522			0.3162			id			0.1137			0.0124									D1
D2	id	?(>)				0.6580			0.2221						0.0586			0.0209								D2
D3	id	?(<)					0.5087			0.5032						0.0886										D3
D4	id	?(<)				0.2255	0.8750					0.1083							0.0154			id		0.8537		D4
D5	id		?(<)		?(>)								0.0754							0.0149			0.0136		id	D5
D6	id			?(<)	?(<)																0.0007					D6
C1S	id	?(<)							0.0807	0.2751	id			0.0632												C1S
C2S	id		?(>)					>							0.1650											C2S
C3S	id			?(>)				?(>)								0.0871										C3S
A1S	id	id						id				id					id									A1S
A4S	id				?(<)						id		0.1621						0.0027							A4S
A5S	id					<						?(>)								0.0028						A5S
C1	id	?(>)						>							0.6856	0.7156	0.6611									C1
C2	id		>						?(>)					?(>)				0.2069								C2
C3	id			>						>				?(<)												C3
A1	id	>									id			?(>)				0.3742	0.9899							A1
A2	id		>												?(>)		?(>)			0.8140						A2
A4	id				>							>					?(<)			0.7011	0.9745	id		0.9662		A4
A5	id					>							>					?(<)	?(>)				0.2694		id	A5
A6	id						>												?(<)							A6
A4F	id				id														id				id			A4F
A5F	id					>														?(<)		id				A5F
A4H	id				?(>)														?(>)						id	A4H
A5H	id					id														id				id		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E23. Results of Hypothesis Test 2 for Outgoing Solids and furnish WF3.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	Con
D1	id		0.0022	0.4790	0.9063			0.7801			id			0.0027			0.0002									D1
D2	id	>				0.4141			0.2282						0.0128			0.0406								D2
D3	id	?(>)					0.0234			0.2078						0.0341										D3
D4	id	?(<)				0.1368	0.0454					0.1118							0.0195			id		0.0061		D4
D5	id		?(<)		?(>)								id							0.0094			id		0.0005	D5
D6	id			<	<																0.0032					D6
C1S	id	?(>)							0.5520	0.6437	id			0.4676												C1S
C2S	id		?(>)					?(>)							0.0652											C2S
C3S	id			?(>)				?(>)								0.1527										C3S
A1S	id	id						id				id					id									A1S
A4S	id				?(<)						id		id						0.0102							A4S
A5S	id					id						id								id						A5S
C1	id	>						?(>)							0.2110	0.5164	0.1428									C1
C2	id		>						>					?(>)				0.7219								C2
C3	id			>						?(>)				?(>)												C3
A1	id	>									id			?(>)				0.7863	0.5532							A1
A2	id		>												?(>)		?(>)			0.5134						A2
A4	id				>							>					?(>)			0.8127	0.7691	id		0.3816		A4
A5	id					>							id					?(>)	?(>)				id		0.5861	A5
A6	id						>												?(<)							A6
A4F	id				id														id				id			A4F
A5F	id					id														id		id				A5F
A4H	id				>														?(<)						0.1691	A4H
A5H	id					>														?(<)				?(>)		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E24. Results of Hypothesis Test 2 for Outgoing Solids and furnish FD5.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	Con
D1	id		0.7884	0.9529	0.0659			0.3519			id			0.0192			0.1240									D1
D2	id	?(>)				0.3237			0.6191						0.0455			0.0309								D2
D3	id	?(<)					0.0909			0.5228						0.3514										D3
D4	id	>				0.5576	0.5457					0.4243							0.0187			id		id		D4
D5	id		?(>)		?(<)								0.5458							0.2331			0.4313		id	D5
D6	id			>	?(<)																0.1101					D6
C1S	id	?(>)							0.9604	0.1997	id			0.0487												C1S
C2S	id		?(>)					?(>)							0.0739											C2S
C3S	id			?(<)				?(<)								0.2361										C3S
A1S	id	id						id				id					id									A1S
A4S	id				?(<)						id		0.3090						0.0108							A4S
A5S	id					?(<)						?(<)								0.0526						A5S
C1	id	>						>							0.3593	0.5934	0.3450									C1
C2	id		>						>					?(>)				0.9046								C2
C3	id			?(>)						?(>)				?(<)												C3
A1	id	?(>)									id			?(>)				0.6790	0.4176							A1
A2	id		>												?(>)		?(<)			0.1853						A2
A4	id				>							>					?(<)			0.1410	0.7546	id		id		A4
A5	id					?(>)							>					?(<)	?(<)				0.8310		id	A5
A6	id						?(>)												?(>)							A6
A4F	id				id														id				id			A4F
A5F	id					?(>)														?(>)		id				A5F
A4H	id				id														id						id	A4H
A5H	id					id														id				id		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E25. Results of Hypothesis Test 2 for Outgoing Solids and furnish FD6.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	Con
D1	id		0.0151	0.6036	0.4760			0.9948			id			0.0012			Error									D1
D2	id	>				0.0868			0.4811						0.0151			0.0001								D2
D3	id	?(<)					0.2650			0.0405						Error										D3
D4	id	?(>)				0.6868	0.1505					0.0547							0.0686			id		0.0006		D4
D5	id		<		?(>)								0.0175							0.0223			0.0000		0.0000	D5
D6	id			?(<)	?(<)																0.0039					D6
C1S	id	?(<)							0.1869	0.4825	id			0.0215												C1S
C2S	id		?(>)					?(>)							0.1476											C2S
C3S	id			>				?(>)								0.0002										C3S
A1S	id	id						id				id					id									A1S
A4S	id				<						id		0.2785						0.0015							A4S
A5S	id					<						?(>)								0.0130						A5S
C1	id	>						>							0.3897	0.4576	0.1444									C1
C2	id		>						?(>)					?(>)				0.2418								C2
C3	id			>					.	>				?(>)												C3
A1	id	>									id			?(>)				0.4987	0.0021							A1
A2	id		>												?(>)		?(>)			0.9981						A2
A4	id				>							>					<			0.0350	0.0303	id		0.0121		A4
A5	id					>							>					?(<)	>				0.1922		0.4953	A5
A6	id						>												>							A6
A4F	id				id														id				id			A4F
A5F	id					>														?(<)		id				A5F
A4H	id				>														>						0.9032	A4H
A5H	id					>														?(<)				?(>)		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E26. Results of Hypothesis Test 2 for Outgoing Solids and furnish FD7.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	Con
D1	id		id	id	id			id			id			id			id									D1
D2	id	id				0.0134			0.0002						0.2124			Error								D2
D3	id	id					id			0.2656						0.0048										D3
D4	id	id				0.0034	id					0.9073							0.0056			id		0.0014		D4
D5	id		<		>								#DIV/							0.0229			0.7876		#DIV/	D5
D6	id			id	id																id					D6
C1S	id	id							0.0127	0.0569	id			0.0053												C1S
C2S	id		>					>							0.1332											C2S
C3S	id			?(<)				<								0.0009										C3S
A1S	id	id						id				id					id									A1S
A4S	id				?(>)						id		0.8213						0.0071							A4S
A5S	id					<						?(<)								0.0074						A5S
C1	id	id						>							0.0530	0.5201	0.6837									C1
C2	id		?(>)						?(<)					<				0.0003								C2
C3	id			>						>				?(>)												C3
A1	id	id									id			?(>)				0.0849	0.9220							A1
A2	id		>												>		>			0.0699						A2
A4	id				>							>					?(<)			0.8383	0.7412	id		0.7849		A4
A5	id					>							>					<	?(<)				0.2160		n/a	A5
A6	id						id												?(>)							A6
A4F	id				id														id				id			A4F
A5F	id					?(>)														?(<)		id				A5F
A4H	id				>														?(<)						n/a	A4H
A5H	id					<														<				<		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E27. Results of Hypothesis Test 2 for Outgoing Solids, comparing furnishes.

Case	Con WF1	Con WF2	Con WF3	Con FD5	Con FD6	Con FD7	D1 WF1	D1 WF2	D1 WF3	D1 FD5	D1 FD6	D1 FD7	D2 WF1	D2 WF2	D2 WF3	D2 FD5	D2 FD6	D2 FD7	Case
Con WF1		id	id	id	id														Con WF1
Con WF2	id			id	id														Con WF2
Con WF3	id			id		id													Con WF3
Con FD5	id	id	id		id	id													Con FD5
Con FD6	id	id		id		id													Con FD6
Con FD7			id	id	id														Con FD7
D1 WF1								0.0363	0.5725	0.0175	0.3489								D1 WF1
D1 WF2							<			0.1972	0.0154								D1 WF2
D1 WF3							?(<)			0.0251		id							D1 WF3
D1 FD5							<	?(<)	<		0.0126	id							D1 FD5
D1 FD6							?(>)	>		>		id							D1 FD6
D1 FD7									id	id	id								D1 FD7
D2 WF1														0.0729	0.1081	0.0139	0.6907		D2 WF1
D2 WF2													<			0.4116	0.0722		D2 WF2
D2 WF3													?(<)			0.0203		0.0021	D2 WF3
D2 FD5													<	?(<)	<		0.0069	0.0665	D2 FD5
D2 FD6													?(>)	>		>		0.0013	D2 FD6
D2 FD7															<	>	<		D2 FD7
Case	Con WF1 D3	Con WF2 D3	Con WF3 D3	Con FD5 D3	Con FD6 D3	Con FD7 D3	D1 WF1 D4	D1 WF2 D4	D1 WF3 D4	D1 FD5 D4	D1 FD6 D4	D1 FD7 D4	D2 WF1 D5	D2 WF2 D5	D2 WF3 D5	D2 FD5 D5	D2 FD6 D5	D2 FD7 D5	Case
D3 WF1		0.2730	0.3329	0.0251	0.0422														D3 WF1
D3 WF2	?(<)			0.7721	0.1281														D3 WF2
D3 WF3	?(>)			0.0278		0.5854													D3 WF3
D3 FD5	<	?(<)	<		0.0080	0.0214													D3 FD5
D3 FD6	>	?(>)		>		0.5478													D3 FD6
D3 FD7			?(<)	>	?(<)														D3 FD7
D4 WF1								0.1044	0.9200	0.8065	0.2667								D4 WF1
D4 WF2							?(<)			0.0652	0.0077								D4 WF2
D4 WF3							?(>)			0.5930		0.1329							D4 WF3
D4 FD5							?(<)	>	?(<)		0.0734	0.0104							D4 FD5
D4 FD6							?(>)	>		>		0.0120							D4 FD6
D4 FD7									?(<)	<	<								D4 FD7
D5 WF1														0.0034	0.4737	0.0089	0.6918		D5 WF1
D5 WF2													<			0.5367	0.0042		D5 WF2
D5 WF3													?(<)			0.0205		0.0472	D5 WF3
D5 FD5													<	?(>)	<		0.0168	0.3932	D5 FD5
D5 FD6													?(<)	>		>		0.0028	D5 FD6
D5 FD7															<	?(>)	<		D5 FD7
Case	D3 WF1	D3 WF2	D3 WF3	D3 FD5	D3 FD6	D3 FD7	D4 WF1	D4 WF2	D4 WF3	D4 FD5	D4 FD6	D4 FD7	D5 WF1	D5 WF2	D5 WF3	D5 FD5	D5 FD6	D5 FD7	Case

Table E28. Results of Hypothesis Test 2 for Outgoing Solids, comparing furnishes continued.

Case	D6 WF1	D6 WF2	D6 WF3	D6 FD5	D6 FD6	D6 FD7	C1S WF1	C1S WF2	C1S WF3	C1S FD5	C1S FD6	C1S FD7	C2S WF1	C2S WF2	C2S WF3	C2S FD5	C2S FD6	C2S FD7	Case
D6 WF1		0.4974	0.7196	0.3696	0.7637														D6 WF1
D6 WF2	?(<)			0.0557	0.4105														D6 WF2
D6 WF3	?(<)			0.0773		id													D6 WF3
D6 FD5	?(>)	>	>		0.7143	id													D6 FD5
D6 FD6	?(>)	?(>)		?(<)		id													D6 FD6
D6 FD7			id	id	id														D6 FD7
C1S WF1								0.3365	0.7589	0.6204	0.7172								C1S WF1
C1S WF2							?(<)			0.3731	0.1148								C1S WF2
C1S WF3							?(>)			0.4843		0.9761							C1S WF3
C1S FD5							?(<)	?(>)	?(<)		0.2492	0.0151							C1S FD5
C1S FD6							?(>)	?(>)		?(>)		0.9643							C1S FD6
C1S FD7									?(<)	>	?(<)								C1S FD7
C2S WF1														0.0090	0.0644	0.0015	0.9906		C2S WF1
C2S WF2													<			0.0480	0.2700		C2S WF2
C2S WF3													<			0.0033		0.6883	C2S WF3
C2S FD5													<	<	<		0.1688	0.0073	C2S FD5
C2S FD6													?(<)	?(>)		?(>)		0.5498	C2S FD6
C2S FD7															?(>)	>	?(<)		C2S FD7

Case	D6 WF1 C3S	D6 WF2 C3S	D6 WF3 C3S	D6 FD5 C3S	D6 FD6 C3S	D6 FD7 C3S	C1S WF1 A1S	C1S WF2 A1S	C1S WF3 A1S	C1S FD5 A1S	C1S FD6 A1S	C1S FD7 A1S	C2S WF1 A4S	C2S WF2 A4S	C2S WF3 A4S	C2S FD5 A4S	C2S FD6 A4S	C2S FD7 A4S	Case
C3S WF1		0.5223	0.8625	0.3428	0.8953														C3S WF1
C3S WF2	?(<)			0.1180	0.0159														C3S WF2
C3S WF3	?(>)			0.0113		0.0168													C3S WF3
C3S FD5	?(<)	?(<)	<		0.0081	0.0821													C3S FD5
C3S FD6	?(>)	>		>		0.0055													C3S FD6
C3S FD7			<	>	<														C3S FD7
A1S WF1								id	id	id	id								A1S WF1
A1S WF2							id			id	id								A1S WF2
A1S WF3							id			id		id							A1S WF3
A1S FD5							id	id	id		id	id							A1S FD5
A1S FD6							id	id		id		id							A1S FD6
A1S FD7									id	id	id								A1S FD7
A4S WF1														0.0158	0.2779	0.7118	0.6757		A4S WF1
A4S WF2													<			0.0015	0.0014		A4S WF2
A4S WF3													?(<)			0.0824		0.9833	A4S WF3
A4S FD5													?(<)	>	>		0.8758	0.3979	A4S FD5
A4S FD6													?(<)	>		?(<)		0.4172	A4S FD6
A4S FD7															?(<)	?(<)	?(<)		A4S FD7
Case	C3S WF1	C3S WF2	C3S WF3	C3S FD5	C3S FD6	C3S FD7	A1S WF1	A1S WF2	A1S WF3	A1S FD5	A1S FD6	A1S FD7	A4S WF1	A4S WF2	A4S WF3	A4S FD5	A4S FD6	A4S FD7	Case

Table E29. Results of Hypothesis Test 2 for Outgoing Solids, comparing furnishes continued.

Case	A5S WF1	A5S WF2	A5S WF3	A5S FD5	A5S FD6	A5S FD7	C1 WF1	C1 WF2	C1 WF3	C1 FD5	C1 FD6	C1 FD7	C2 WF1	C2 WF2	C2 WF3	C2 FD5	C2 FD6	C2 FD7	Case
A5S WF1		id	id	id	id														A5S WF1
A5S WF2	id			0.0597	0.0122														A5S WF2
A5S WF3	id			id		id													A5S WF3
A5S FD5	id	>	id		0.1201	0.2959													A5S FD5
A5S FD6	id	>		?(>)		0.0245													A5S FD6
A5S FD7			id	?(<)	<														A5S FD7
C1 WF1								0.0607	0.1592	0.0074	0.4792								C1 WF1
C1 WF2							<			0.6373	0.0160								C1 WF2
C1 WF3							?(<)			0.0292		0.6015							C1 WF3
C1 FD5							<	?(<)	<		0.0011	0.0137							C1 FD5
C1 FD6							?(>)	>		>		0.0595							C1 FD6
C1 FD7									?(>)	>	<								C1 FD7
C2 WF1														0.1717	0.7144	0.1937	0.3416		C2 WF1
C2 WF2													?(<)			0.9737	0.0032		C2 WF2
C2 WF3													?(<)			0.1462		0.0167	C2 WF3
C2 FD5													?(<)	?(<)	?(<)		0.0127	0.7007	C2 FD5
C2 FD6													?(>)	>		>		0.0025	C2 FD6
C2 FD7															<	?(<)	<		C2 FD7

Case	A5S WF1 C3	A5S WF2 C3	A5S WF3 C3	A5S FD5 C3	A5S FD6 C3	A5S FD7 C3	C1 WF1 A1	C1 WF2 A1	C1 WF3 A1	C1 FD5 A1	C1 FD6 A1	C1 FD7 A1	C2 WF1 A2	C2 WF2 A2	C2 WF3 A2	C2 FD5 A2	C2 FD6 A2	C2 FD7 A2	Case
C3 WF1		0.6458	0.3074	0.4063	0.0175														C3 WF1
C3 WF2	?(<)			0.5227	0.0000														C3 WF2
C3 WF3	?(>)			0.0670		0.7829													C3 WF3
C3 FD5	?(<)	?(<)	<		0.0066	0.0452													C3 FD5
C3 FD6	>	>		>		0.0664													C3 FD6
C3 FD7			?(>)	>	<														C3 FD7
A1 WF1								0.0015	0.0136	0.0689	0.4842								A1 WF1
A1 WF2							<			0.6492	0.0003								A1 WF2
A1 WF3							<			0.6018		0.6712							A1 WF3
A1 FD5							<	?(>)	?(<)		0.1070	0.7539							A1 FD5
A1 FD6							?(<)	>		?(>)		0.0056							A1 FD6
A1 FD7									?(<)	?(>)	<								A1 FD7
A2 WF1														0.0003	0.0192	0.0019	0.9961		A2 WF1
A2 WF2													<			0.5149	0.0001		A2 WF2
A2 WF3													<			0.1611		0.3881	A2 WF3
A2 FD5													<	?(<)	?(<)		0.0019	0.0320	A2 FD5
A2 FD6													?(<)	>		>		0.0181	A2 FD6
A2 FD7															?(>)	>	<		A2 FD7

Case	C3 WF1	C3 WF2	C3 WF3	C3 FD5	C3 FD6	C3 FD7	A1 WF1	A1 WF2	A1 WF3	A1 FD5	A1 FD6	A1 FD7	A2 WF1	A2 WF2	A2 WF3	A2 FD5	A2 FD6	A2 FD7	Case

Table E30. Results of Hypothesis Test 2 for Outgoing Solids, comparing furnishes continued.

Case	A4 WF1	A4 WF2	A4 WF3	A4 FD5	A4 FD6	A4 FD7	A5 WF1	A5 WF2	A5 WF3	A5 FD5	A5 FD6	A5 FD7	A6 WF1	A6 WF2	A6 WF3	A6 FD5	A6 FD6	A6 FD7	Case
A4 WF1		0.0412	0.6298	0.0044	0.0970														A4 WF1
A4 WF2	<			0.5399	0.3944														A4 WF2
A4 WF3	?(<)			0.0415		0.4183													A4 WF3
A4 FD5	<	?(<)	<		0.0379	0.0888													A4 FD5
A4 FD6	<	?(>)		>		0.8735													A4 FD6
A4 FD7			?(<)	>	?(>)														A4 FD7
A5 WF1								0.0113	0.3333	0.0000	0.4914								A5 WF1
A5 WF2							<			0.0728	0.0248								A5 WF2
A5 WF3							?(<)			0.0030		0.1420							A5 WF3
A5 FD5							<	<	<		0.0138	0.0282							A5 FD5
A5 FD6							?(>)	>		>		0.0374							A5 FD6
A5 FD7									?(<)	>	<								A5 FD7
A6 WF1														0.0023	0.0410	0.0031	0.1507		A6 WF1
A6 WF2													<			0.6750	0.0011		A6 WF2
A6 WF3													<			0.0359		0.5770	A6 WF3
A6 FD5													<	?(<)	<		0.0075	0.0678	A6 FD5
A6 FD6													?(<)	>		>		0.0956	A6 FD6
A6 FD7															?(<)	>	<		A6 FD7
Case	A4 WF1 A5F	A4 WF2 A5F	A4 WF3 A5F	A4 FD5 A5F	A4 FD6 A5F	A4 FD7 A5F	A5 WF1 A4H	A5 WF2 A4H	A5 WF3 A4H	A5 FD5 A4H	A5 FD6 A4H	A5 FD7 A4H	A6 WF1 A5H	A6 WF2 A5H	A6 WF3 A5H	A6 FD5 A5H	A6 FD6 A5H	A6 FD7 A5H	Case
A5F WF1		0.0007	id	0.0116	0.7248														A5F WF1
A5F WF2	<			0.6099	0.0000														A5F WF2
A5F WF3	id			id		id													A5F WF3
A5F FD5	<	?(<)	id		0.0095	0.9803													A5F FD5
A5F FD6	?(>)	>		>		0.0298													A5F FD6
A5F FD7			id	?(<)	<														A5F FD7
A4H WF1								0.9233	0.8926	id	0.9937								A4H WF1
A4H WF2							?(<)			id	0.9032								A4H WF2
A4H WF3							?(<)			id		0.7228							A4H WF3
A4H FD5							id	id	id		id	id							A4H FD5
A4H FD6							?(>)	?(>)		id		0.0136							A4H FD6
A4H FD7									?(<)	id	<								A4H FD7
A5H WF1														id	0.0357	id	0.9735		A5H WF1
A5H WF2													id			id	id		A5H WF2
A5H WF3													<			id		0.0000	A5H WF3
A5H FD5													id	id	id		id	id	A5H FD5
A5H FD6													?(<)	id		id		<.0001	A5H FD6
A5H FD7															<	id	<		A5H FD7
Case	A5F WF1	A5F WF2	A5F WF3	A5F FD5	A5F FD6	A5F FD7	A4H WF1	A4H WF2	A4H WF3	A4H FD5	A4H FD6	A4H FD7	A5H WF1	A5H WF2	A5H WF3	A5H FD5	A5H FD6	A5H FD7	Case

Table E31. Results of Hypothesis Test 3 for Outgoing Solids and furnish WF1.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	Con
D1	id		0.0056	0.1985	0.6933			0.8388			0.0775			0.0019			0.0001									D1
D2	id	>				0.3887			0.0093						0.0080			0.0001								D2
D3	id	?(<)					0.2123			0.5998						0.0299										D3
D4	id	?(<)				0.1379	0.2682					0.9010							0.0105			id		0.0022		D4
D5	id		?(<)		?(>)								id							0.0001			0.0021		0.0002	D5
D6	id			?(<)	?(<)																0.0005					D6
C1S	id	?(<)							0.1882	0.6521	0.5545			0.1883												C1S
C2S	id		>					?(>)							0.0720											C2S
C3S	id			?(>)				?(>)								0.7589										C3S
A1S	id	>						?(>)				0.1719					0.0015									A1S
A4S	id				?(<)						?(<)		id						0.0034							A4S
A5S	id					id						id								id						A5S
C1	id	>						?(>)							0.2150	0.1621	0.0022									C1
C2	id		>						>					?(>)				0.0011								C2
C3	id			>						?(>)				?(<)												C3
A1	id	>									>			>				0.9338	0.0099							A1
A2	id		>												>		?(>)			0.0192						A2
A4	id				>							>					<			0.0616	0.0409	id		0.0874		A4
A5	id					>							id					<	>				0.0156		0.2859	A5
A6	id						>												>							A6
A4F	id				id														id				id			A4F
A5F	id					>														<		id				A5F
A4H	id				>														>						0.7578	A4H
A5H	id					>														?(>)				?(<)		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E32. Results of Hypothesis Test 3 for Outgoing Solids and furnish WF2.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	Con
D1	id		0.7657	0.5761	0.1522			0.3162			id			0.2020			0.0141									D1
D2	id	?(>)				0.6580			0.2221						0.1214			0.0310								D2
D3	id	?(<)					0.5087			0.5032						0.1549										D3
D4	id	?(<)				0.2255	0.8750					0.1083							0.0161			id		0.0013		D4
D5	id		?(<)		?(>)								0.0754							0.0097			0.0150		0.0053	D5
D6	id			?(<)	?(<)	<															0.0022					D6
C1S	id	?(<)							0.0807	0.2751	id			0.1536												C1S
C2S	id		?(>)					>							0.2484											C2S
C3S	id			?(>)				?(>)								0.1588										C3S
A1S	id	id						id				id					id									A1S
A4S	id				?(<)						id		0.1621						0.0010							A4S
A5S	id					<						?(>)								0.0013						A5S
C1	id	?(>)						?(>)							0.0362	0.3990	0.0405									C1
C2	id		?(>)						?(>)					>				0.0334								C2
C3	id			?(>)						?(>)				?(>)												C3
A1	id	>									id			>				0.2850	0.1415							A1
A2	id		>												>		?(>)			0.0449						A2
A4	id				>							>					?(<)			0.3017	0.1156	id		0.0248		A4
A5	id					>							>					<	?(>)					0.5105		0.0335	A5
A6	id						>												?(>)								A6
A4F	id				id														id				id				A4F
A5F	id					>														?(<)		id					A5F
A4H	id				>														>						0.7324		A4H
A5H	id					>														>				?(>)			A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E33. Results of Hypothesis Test 3 for Outgoing Solids and furnish WF3.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	Con
D1	id		0.0022	0.4790	0.9063			0.7801			id			0.0010			0.0000									D1
D2	id	>				0.4141			0.2282						0.0048			0.0005								D2
D3	id	?(>)					0.0234			0.2078						0.0691										D3
D4	id	?(<)				0.1368	0.0454					0.1118							0.0115			id		0.0141		D4
D5	id		?(<)		?(>)								id							0.0036			0.0263		0.0026	D5
D6	id			<	<																0.0004					D6
C1S	id	?(>)							0.5520	0.6437	id			0.5427												C1S
C2S	id		?(>)					?(>)							0.1486											C2S
C3S	id			?(>)				?(>)								0.1700										C3S
A1S	id	id						id				id					id									A1S
A4S	id				?(<)						id		id						0.0030							A4S
A5S	id					id						id								id						A5S
C1	id	>						?(>)							0.0576	0.4597	0.0014									C1
C2	id		>						?(>)					>				0.0029								C2
C3	id			>						?(>)				?(>)												C3
A1	id	>									id			>				0.0798	0.1398							A1
A2	id		>												>		>			0.1360						A2
A4	id				>							>					?(<)			0.2290	0.6046	id		0.5827		A4
A5	id					>							id					?(<)	?(>)				0.1263		0.2092	A5
A6	id						>												?(>)							A6
A4F	id				id														id				id			A4F
A5F	id					>														?(<)		id				A5F
A4H	id				>														?(<)						0.0143	A4H
A5H	id					>														?(>)				>		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E34. Results of Hypothesis Test 3 for Outgoing Solids and furnish FD5.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	Con
D1	id		0.7884	0.9529	0.0659			0.3519			id			id			0.0232									D1
D2	id	?(>)				0.3237			0.6191						0.0334			0.0357								D2
D3	id	?(<)					0.0909			0.5228						0.0958										D3
D4	id	>				0.5576	0.5457					0.4243							0.0210			id		id		D4
D5	id		?(>)		?(<)								0.5458							id			id		id	D5
D6	id			>	?(<)																0.0200					D6
C1S	id	?(>)							0.9604	0.1997	id			id												C1S
C2S	id		?(>)					?(>)							0.0364											C2S
C3S	id			?(<)				?(<)								0.0883										C3S
A1S	id	id						id				id					id									A1S
A4S	id				?(<)						id		0.3090						0.0124							A4S
A5S	id					?(<)						?(<)								id						A5S
C1	id	id						id							id	id	id									C1
C2	id		>						>					id				0.8990								C2
C3	id			>						>				id												C3
A1	id	>									id			id				0.5025	0.4829							A1
A2	id		>												?(>)		?(>)			id						A2
A4	id				>							>					?(>)			id	0.2759	id		id		A4
A5	id					id							id					id	id				id		id	A5
A6	id						>												?(>)							A6
A4F	id				id														id				id			A4F
A5F	id					id														id		id				A5F
A4H	id				id														id						id	A4H
A5H	id					id														id				id		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E35. Results of Hypothesis Test 3 for Outgoing Solids and furnish FD6.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	Con
D1	id		0.0151	0.6036	0.4760			0.9948			id			0.0005			0.0000									D1
D2	id	>				0.0868			0.4811						0.0035			0.0000								D2
D3	id	?(<)					0.2650			0.0405						0.0000										D3
D4	id	?(>)				0.6868	0.1505					0.0547							0.0957			id		0.0013		D4
D5	id		<		?(>)								0.0175							0.0058			0.0000		0.0000	D5
D6	id			?(<)	?(<)																0.0151					D6
C1S	id	?(<)							0.1869	0.4825	id			0.0832												C1S
C2S	id		?(>)					?(>)							0.3447											C2S
C3S	id			>				?(>)								0.0002										C3S
A1S	id	id						id				id					id									A1S
A4S	id				<						id		0.2785						0.0019							A4S
A5S	id					<						?(>)								0.0010						A5S
C1	id	>						>							0.2040	0.0605	0.0066									C1
C2	id		>						?(>)					?(>)				0.0215								C2
C3	id			>						>				>												C3
A1	id	>									id			>				0.1754	0.0003							A1
A2	id		>												>		?(>)			0.1290						A2
A4	id				>							>					<			0.0167	0.0038	id		0.0017		A4
A5	id					>							>					?(<)	>					0.8698		0.2034	A5
A6	id						>												>							A6
A4F	id				id														id				id			A4F
A5F	id					>														?(<)		id				A5F
A4H	id				>														>						0.0180	A4H
A5H	id					>														?(>)				>		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E36. Results of Hypothesis Test 3 for Outgoing Solids and furnish FD7.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	id	Con
D1	id		id	id	id			id			id			id			id									D1
D2	id	id				0.0134			0.0002						0.1594			0.0002								D2
D3	id	id					id			0.2656						0.0017										D3
D4	id	id				0.0034	id					0.9073							0.0020			id		0.0018		D4
D5	id		<		>								#DIV/							0.0212			0.0054		0.0056	D5
D6	id			id	id																id					D6
C1S	id	id							0.0127	0.0569	id			0.0088												C1S
C2S	id		>					>							0.0244											C2S
C3S	id			?(<)				<								0.0002										C3S
A1S	id	id						id				id					id									A1S
A4S	id				?(>)						id		0.8213						0.0140							A4S
A5S	id					<						?(<)								0.0070						A5S
C1	id	id						>							0.0167	0.0276	0.0578									C1
C2	id		?(>)						<					<				0.0003								C2
C3	id			>						>				>												C3
A1	id	id									id			>				0.0083	0.0516							A1
A2	id		>												>		>			0.0101						A2
A4	id				>							>					<			0.6142	0.1292	id		0.6483		A4
A5	id					>							>					<	?(>)				0.9081		0.0565	A5
A6	id						id												?(>)							A6
A4F	id				id														id				id			A4F
A5F	id					>														?(<)		id				A5F
A4H	id				>														?(>)						0.0449	A4H
A5H	id					>														>				>		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E37. Results of Hypothesis Test 3 for Outgoing Solids, comparing furnishes.

Case	Con WF1	Con WF2	Con WF3	Con FD5	Con FD6	Con FD7	D1 WF1	D1 WF2	D1 WF3	D1 FD5	D1 FD6	D1 FD7	D2 WF1	D2 WF2	D2 WF3	D2 FD5	D2 FD6	D2 FD7	Case
Con WF1		id	id	id	id														Con WF1
Con WF2	id			id	id														Con WF2
Con WF3	id			id		id													Con WF3
Con FD5	id	id	id		id	id													Con FD5
Con FD6	id	id		id		id													Con FD6
Con FD7			id	id	id														Con FD7
D1 WF1								0.0363	0.5725	0.0175	0.3489								D1 WF1
D1 WF2							<			0.1972	0.0154								D1 WF2
D1 WF3							?(<)			0.0251		id							D1 WF3
D1 FD5							<	?(<)	<		0.0126	id							D1 FD5
D1 FD6							?(>)	>		>		id							D1 FD6
D1 FD7									id	id	id								D1 FD7
D2 WF1														0.0729	0.1081	0.0139	0.6907		D2 WF1
D2 WF2													<			0.4116	0.0722		D2 WF2
D2 WF3													?(<)			0.0203		0.0021	D2 WF3
D2 FD5													<	?(<)	<		0.0069	0.0665	D2 FD5
D2 FD6													?(>)	>		>		0.0013	D2 FD6
D2 FD7															<	>	<		D2 FD7

Case	Con WF1	Con WF2	Con WF3	Con FD5	Con FD6	Con FD7	D1 WF1	D1 WF2	D1 WF3	D1 FD5	D1 FD6	D1 FD7	D2 WF1	D2 WF2	D2 WF3	D2 FD5	D2 FD6	D2 FD7	Case
	D3	D3	D3	D3	D3	D3	D4	D4	D4	D4	D4	D4	D5	D5	D5	D5	D5	D5	
D3 WF1		0.2730	0.3329	0.0251	0.0422														D3 WF1
D3 WF2	?(<)			0.7721	0.1281														D3 WF2
D3 WF3	?(>)			0.0278		0.5854													D3 WF3
D3 FD5	<	?(<)	<		0.0080	0.0214													D3 FD5
D3 FD6	>	?(>)		>		0.5478													D3 FD6
D3 FD7			?(<)	>	?(<)														D3 FD7
D4 WF1								0.1044	0.9200	0.8065	0.2667								D4 WF1
D4 WF2							?(<)			0.0652	0.0077								D4 WF2
D4 WF3							?(>)			0.5930		0.1329							D4 WF3
D4 FD5							?(<)	>	?(<)		0.0734	0.0104							D4 FD5
D4 FD6							?(>)	>		>		0.0120							D4 FD6
D4 FD7									?(<)	<	<								D4 FD7
D5 WF1														0.0034	0.4737	0.0089	0.6918		D5 WF1
D5 WF2													<			0.5367	0.0042		D5 WF2
D5 WF3													?(<)			0.0205		0.0472	D5 WF3
D5 FD5													<	?(>)	<		0.0168	0.3932	D5 FD5
D5 FD6													?(<)	>		>		0.0028	D5 FD6
D5 FD7															<	?(>)	<		D5 FD7

Case	D3 WF1	D3 WF2	D3 WF3	D3 FD5	D3 FD6	D3 FD7	D4 WF1	D4 WF2	D4 WF3	D4 FD5	D4 FD6	D4 FD7	D5 WF1	D5 WF2	D5 WF3	D5 FD5	D5 FD6	D5 FD7	Case

Table E38. Results of Hypothesis Test 3 for Outgoing Solids, comparing furnishes continued.

Case	D6 WF1	D6 WF2	D6 WF3	D6 FD5	D6 FD6	D6 FD7	C1S WF1	C1S WF2	C1S WF3	C1S FD5	C1S FD6	C1S FD7	C2S WF1	C2S WF2	C2S WF3	C2S FD5	C2S FD6	C2S FD7	Case
D6 WF1		0.4974	0.7196	0.3696	0.7637														D6 WF1
D6 WF2	?(<)			0.0557	0.4105														D6 WF2
D6 WF3	?(<)			0.0773		id													D6 WF3
D6 FD5	?(>)	>	>		0.7143	id													D6 FD5
D6 FD6	?(>)	?(>)		?(<)		id													D6 FD6
D6 FD7			id	id	id														D6 FD7
C1S WF1								0.3365	0.7589	0.6204	0.7172								C1S WF1
C1S WF2							?(<)			0.3731	0.1148								C1S WF2
C1S WF3							?(>)			0.4843		0.9761							C1S WF3
C1S FD5							?(<)	?(>)	?(<)		0.2492	0.0151							C1S FD5
C1S FD6							?(>)	?(>)		?(>)		0.9643							C1S FD6
C1S FD7									?(<)	>	?(<)								C1S FD7
C2S WF1														0.0090	0.0644	0.0015	0.9906		C2S WF1
C2S WF2													<			0.0480	0.2700		C2S WF2
C2S WF3													<			0.0033		0.6883	C2S WF3
C2S FD5													<	<	<		0.1688	0.0073	C2S FD5
C2S FD6													?(<)	?(>)		?(>)		0.5498	C2S FD6
C2S FD7															?(>)	>	?(<)		C2S FD7

Case	D6 WF1	D6 WF2	D6 WF3	D6 FD5	D6 FD6	D6 FD7	C1S WF1	C1S WF2	C1S WF3	C1S FD5	C1S FD6	C1S FD7	C2S WF1	C2S WF2	C2S WF3	C2S FD5	C2S FD6	C2S FD7	Case
	C3S	C3S	C3S	C3S	C3S	C3S	A1S	A1S	A1S	A1S	A1S	A1S	A4S	A4S	A4S	A4S	A4S	A4S	
C3S WF1		0.5223	0.8625	0.3428	0.8953														C3S WF1
C3S WF2	?(<)			0.1180	0.0159														C3S WF2
C3S WF3	?(>)			0.0113		0.0168													C3S WF3
C3S FD5	?(<)	?(<)	<		0.0081	0.0821													C3S FD5
C3S FD6	?(>)	>		>		0.0055													C3S FD6
C3S FD7			<	>	<														C3S FD7
A1S WF1								id	id	id	id								A1S WF1
A1S WF2							id			id	id								A1S WF2
A1S WF3							id			id		id							A1S WF3
A1S FD5							id	id	id		id	id							A1S FD5
A1S FD6							id	id		id		id							A1S FD6
A1S FD7									id	id	id								A1S FD7
A4S WF1														0.0158	0.2779	0.7118	0.6757		A4S WF1
A4S WF2													<			0.0015	0.0014		A4S WF2
A4S WF3													?(<)			0.0824		0.9833	A4S WF3
A4S FD5													?(<)	>	>		0.8758	0.3979	A4S FD5
A4S FD6													?(<)	>		?(<)		0.4172	A4S FD6
A4S FD7															?(<)	?(<)	?(<)		A4S FD7
Case	C3S WF1	C3S WF2	C3S WF3	C3S FD5	C3S FD6	C3S FD7	A1S WF1	A1S WF2	A1S WF3	A1S FD5	A1S FD6	A1S FD7	A4S WF1	A4S WF2	A4S WF3	A4S FD5	A4S FD6	A4S FD7	Case

Table E39. Results of Hypothesis Test 3 for Outgoing Solids, comparing furnishes continued.

Case	A5S WF1	A5S WF2	A5S WF3	A5S FD5	A5S FD6	A5S FD7	C1 WF1	C1 WF2	C1 WF3	C1 FD5	C1 FD6	C1 FD7	C2 WF1	C2 WF2	C2 WF3	C2 FD5	C2 FD6	C2 FD7	Case
A5S WF1		id	id	id	id														A5S WF1
A5S WF2	id			0.0597	0.0122														A5S WF2
A5S WF3	id			id		id													A5S WF3
A5S FD5	id	>	id		0.1201	0.2959													A5S FD5
A5S FD6	id	>		?(>)		0.0245													A5S FD6
A5S FD7			id	?(<)	<														A5S FD7
C1 WF1								0.0012	0.0652	id	0.1177								C1 WF1
C1 WF2							<			id	0.0002								C1 WF2
C1 WF3							<			id		0.3868							C1 WF3
C1 FD5							id	id	id		id	id							C1 FD5
C1 FD6							?(>)	>		id		0.0087							C1 FD6
C1 FD7									?(>)	id	<								C1 FD7
C2 WF1														0.0020	0.0197	0.0191	0.0625		C2 WF1
C2 WF2													<			0.2974	0.0015		C2 WF2
C2 WF3													<			0.0215		0.0063	C2 WF3
C2 FD5													<	?(<)	<		0.0008	0.7125	C2 FD5
C2 FD6													>	>		>		0.0005	C2 FD6
C2 FD7															<	?(>)	<		C2 FD7
Case	A5S WF1 C3	A5S WF2 C3	A5S WF3 C3	A5S FD5 C3	A5S FD6 C3	A5S FD7 C3	C1 WF1 A1	C1 WF2 A1	C1 WF3 A1	C1 FD5 A1	C1 FD6 A1	C1 FD7 A1	C2 WF1 A2	C2 WF2 A2	C2 WF3 A2	C2 FD5 A2	C2 FD6 A2	C2 FD7 A2	Case
C3 WF1		0.0455	0.6080	0.0164	0.0073														C3 WF1
C3 WF2	<			0.2480	0.0000														C3 WF2
C3 WF3	?(>)			0.0059		0.0904													C3 WF3
C3 FD5	<	?(<)	<		0.0002	0.0012													C3 FD5
C3 FD6	>	>		>		0.0039													C3 FD6
C3 FD7			>	>	<														C3 FD7
A1 WF1								0.0006	0.0090	0.0004	0.5807								A1 WF1
A1 WF2							<			0.1069	0.0008								A1 WF2
A1 WF3							<			0.0109		0.0347							A1 WF3
A1 FD5							<	?(<)	<		0.0008	0.0779							A1 FD5
A1 FD6							?(<)	>		>		0.0007							A1 FD6
A1 FD7									<	>	<								A1 FD7
A2 WF1														0.0001	0.0026	0.0009	0.5570		A2 WF1
A2 WF2													<			0.0630	0.0000		A2 WF2
A2 WF3													<			0.0082		0.3225	A2 WF3
A2 FD5													<	<	<		0.0008	0.0017	A2 FD5
A2 FD6													?(>)	>		>		0.0056	A2 FD6
A2 FD7															?(>)	>	<		A2 FD7
Case	C3 WF1	C3 WF2	C3 WF3	C3 FD5	C3 FD6	C3 FD7	A1 WF1	A1 WF2	A1 WF3	A1 FD5	A1 FD6	A1 FD7	A2 WF1	A2 WF2	A2 WF3	A2 FD5	A2 FD6	A2 FD7	Case

Table E40. Results of Hypothesis Test 3 for Outgoing Solids, comparing furnishes continued.

Case	A4 WF1	A4 WF2	A4 WF3	A4 FD5	A4 FD6	A4 FD7	A5 WF1	A5 WF2	A5 WF3	A5 FD5	A5 FD6	A5 FD7	A6 WF1	A6 WF2	A6 WF3	A6 FD5	A6 FD6	A6 FD7	Case
A4 WF1		0.0010	0.1164	0.0008	0.0303														A4 WF1
A4 WF2	<			0.6690	0.0144														A4 WF2
A4 WF3	?(<)			0.0185		0.1422													A4 WF3
A4 FD5	<	?(>)	<		0.0104	0.0481													A4 FD5
A4 FD6	<	>		>		0.3550													A4 FD6
A4 FD7			?(<)	>	?(<)														A4 FD7
A5 WF1								0.0003	0.0116	id	0.9513								A5 WF1
A5 WF2							<			id	0.0034								A5 WF2
A5 WF3							<			id		0.0784							A5 WF3
A5 FD5							id	id	id		id	id							A5 FD5
A5 FD6							?(>)	>		id		0.0143							A5 FD6
A5 FD7									<	id	<								A5 FD7
A6 WF1														0.0003	0.0060	0.0006	0.1556		A6 WF1
A6 WF2													<			0.3469	0.0004		A6 WF2
A6 WF3													<			0.0082		0.3648	A6 WF3
A6 FD5													<	?(<)	<		0.0005	0.0073	A6 FD5
A6 FD6													?(<)	>		>		0.0039	A6 FD6
A6 FD7															?(<)	>	<		A6 FD7
Case	A4 WF1 A5F	A4 WF2 A5F	A4 WF3 A5F	A4 FD5 A5F	A4 FD6 A5F	A4 FD7 A5F	A5 WF1 A4H	A5 WF2 A4H	A5 WF3 A4H	A5 FD5 A4H	A5 FD6 A4H	A5 FD7 A4H	A6 WF1 A5H	A6 WF2 A5H	A6 WF3 A5H	A6 FD5 A5H	A6 FD6 A5H	A6 FD7 A5H	Case
A5F WF1		0.0002	0.0246	id	0.0110														A5F WF1
A5F WF2	<			id	0.0002														A5F WF2
A5F WF3	<			id		0.0863													A5F WF3
A5F FD5	id	id	id		id	id													A5F FD5
A5F FD6	>	>		id		0.0011													A5F FD6
A5F FD7			<	id	<														A5F FD7
A4H WF1								0.0194	0.0208	id	0.3141								A4H WF1
A4H WF2							<			id	0.0330								A4H WF2
A4H WF3							<			id		0.5013							A4H WF3
A4H FD5							id	id	id		id	id							A4H FD5
A4H FD6							?(<)	>		id		0.0028							A4H FD6
A4H FD7									?(<)	id	<								A4H FD7
A5H WF1														0.0166	0.0161	id	0.2148		A5H WF1
A5H WF2													<			id	0.0197		A5H WF2
A5H WF3													<			id		0.9748	A5H WF3
A5H FD5													id	id	id		id	id	A5H FD5
A5H FD6													?(>)	>		id		0.0282	A5H FD6
A5H FD7															?(<)	id	<		A5H FD7
Case	A5F WF1	A5F WF2	A5F WF3	A5F FD5	A5F FD6	A5F FD7	A4H WF1	A4H WF2	A4H WF3	A4H FD5	A4H FD6	A4H FD7	A5H WF1	A5H WF2	A5H WF3	A5H FD5	A5H FD6	A5H FD7	Case

Table E41. Results of Hypothesis Test 0 for MD STFI and furnish WF1.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con																										Con
D1	>																									D1
D2	?	?																								D2
D3	>	?																								D3
D4	>	?																								D4
D5	>		?		?																					D5
D6	>			?	?																					D6
C1S	?	?																								C1S
C2S	>		?					?																		C2S
C3S	?			?				?																		C3S
A1S	?	?						?																		A1S
A4S	>				?						?															A4S
A5S	id					id						id														A5S
C1	>	?						?																		C1
C2	>		?						?					?												C2
C3	?			?						?				?												C3
A1	>	?									?			?												A1
A2	>		?												?		?									A2
A4	>				?							?					?									A4
A5	>					?							id					?	?							A5
A6	>						?												?							A6
A4F	id				id														id							A4F
A5F	>					?														?		id				A5F
A4H	?				?														?							A4H
A5H	>					?														?				?		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E42. Results of Hypothesis Test 0 for MD STFI and furnish WF2.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con																										Con
D1	>																									D1
D2	>	?																								D2
D3	>	?																								D3
D4	>	?																								D4
D5	>		?		?																					D5
D6	>			?	?																					D6
C1S	>	?																								C1S
C2S	>		?					?																		C2S
C3S	>			?				?																		C3S
A1S	id	id						id																		A1S
A4S	>				<						id															A4S
A5S	?					<						?														A5S
C1	>	?						?																		C1
C2	>		?						?					?												C2
C3	>			?						?				?												C3
A1	>	?									id			?												A1
A2	>		?												?		?									A2
A4	>				?							>					?									A4
A5	>					?							?					?	?							A5
A6	?						?												?							A6
A4F	id				id														id							A4F
A5F	>					<														?		id				A5F
A4H	?				?														?							A4H
A5H	?					?														?				?		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E43. Results of Hypothesis Test 0 for MD STFI and furnish WF3.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con																										Con
D1	?																									D1
D2	>	?																								D2
D3	?	?																								D3
D4	>	?																								D4
D5	>		?		?																					D5
D6	>			?	?																					D6
C1S	?	?																								C1S
C2S	>		?					?																		C2S
C3S	>			?				?																		C3S
A1S	id	id						id																		A1S
A4S	>				?						id															A4S
A5S	?					?						?														A5S
C1	>	?						?																		C1
C2	>		?						?					?												C2
C3	>			?						?				?												C3
A1	>	?									id			?												A1
A2	>		?												?		?									A2
A4	>				?							>					?									A4
A5	>					?							?					?	?							A5
A6	>						?												?							A6
A4F	id				id														id							A4F
A5F	?					?														?		id				A5F
A4H	>				?														?							A4H
A5H	>					?														?				?		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E44. Results of Hypothesis Test 0 for MD STFI and furnish FD5.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con																										Con
D1	?																									D1
D2	>	?																								D2
D3	?	?																								D3
D4	?	?																								D4
D5	?		?		?																					D5
D6	?			?	?																					D6
C1S	?	?																								C1S
C2S	?		?					?																		C2S
C3S	?			?				?																		C3S
A1S	id	id						id																		A1S
A4S	?				?						id															A4S
A5S	?					<						?														A5S
C1	?	?						?																		C1
C2	?		?						?					?												C2
C3	?			?						?				?												C3
A1	?	?									id			?												A1
A2	?		?												?		?									A2
A4	?				?							?					?									A4
A5	?					?							?					?	?							A5
A6	?						?												?							A6
A4F	id				id														id							A4F
A5F	id					id														id		id				A5F
A4H	id				id														id							A4H
A5H	id					id														id				id		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E45. Results of Hypothesis Test 0 for MD STFI and furnish FD6.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con																										Con
D1	>																									D1
D2	?	?																								D2
D3	?	?																								D3
D4	?	?																								D4
D5	>		?		?																					D5
D6	?			?	?																					D6
C1S	?	?																								C1S
C2S	?		?					?																		C2S
C3S	>			?				?																		C3S
A1S	id	id						id																		A1S
A4S	?				?						id															A4S
A5S	?					?						?														A5S
C1	>	?						?																		C1
C2	>		?						?					?												C2
C3	>			?						?				?												C3
A1	?	?									id			?												A1
A2	>		?												?		?									A2
A4	>				?							?					?									A4
A5	>					?							?					?	?							A5
A6	>						?												?							A6
A4F	id				id														id							A4F
A5F	>					?														?		id				A5F
A4H	>				?														?							A4H
A5H	>					?														?				?		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E46. Results of Hypothesis Test 0 for MD STFI and furnish FD7.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con																										Con
D1	?																									D1
D2	>	?																								D2
D3	>	?																								D3
D4	>	?																								D4
D5	>		?		?																					D5
D6	?			?	?																					D6
C1S	>	?																								C1S
C2S	>		?					?																		C2S
C3S	>			?				?																		C3S
A1S	id	id						id																		A1S
A4S	?				?						id															A4S
A5S	?					<						?														A5S
C1	>	?						?																		C1
C2	>		?						?		·			?												C2
C3	>			?						?				?												C3
A1	>	?									id			?												A1
A2	>		?												>		?									A2
A4	>				?							?					?									A4
A5	>					?							>					?	?							A5
A6	>						?												?							A6
A4F	id				id														id							A4F
A5F	>					?														?		id				A5F
A4H	>				?														?							A4H
A5H	>					?														?				?		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E47. Results of Hypothesis Test 0 for MD STFI, comparing furnishes.

Case	Con WF1	Con WF2	Con WF3	Con FD5	Con FD6	Con FD7	D1 WF1	D1 WF2	D1 WF3	D1 FD5	D1 FD6	D1 FD7	D2 WF1	D2 WF2	D2 WF3	D2 FD5	D2 FD6	D2 FD7	Case
Con WF1																			Con WF1
Con WF2	>																		Con WF2
Con WF3	?																		Con WF3
Con FD5	?	?	?																Con FD5
Con FD6	?	<		?															Con FD6
Con FD7			?	?	?														Con FD7
D1 WF1																			D1 WF1
D1 WF2							?												D1 WF2
D1 WF3							?												D1 WF3
D1 FD5							?	<	?										D1 FD5
D1 FD6							<	<		?									D1 FD6
D1 FD7									?	?	?								D1 FD7
D2 WF1																			D2 WF1
D2 WF2													?						D2 WF2
D2 WF3													?						D2 WF3
D2 FD5													?	<	?				D2 FD5
D2 FD6													?	<		<			D2 FD6
D2 FD7															?	?	?		D2 FD7

Case	Con WF1 D3	Con WF2 D3	Con WF3 D3	Con FD5 D3	Con FD6 D3	Con FD7 D3	D1 WF1 D4	D1 WF2 D4	D1 WF3 D4	D1 FD5 D4	D1 FD6 D4	D1 FD7 D4	D2 WF1 D5	D2 WF2 D5	D2 WF3 D5	D2 FD5 D5	D2 FD6 D5	D2 FD7 D5	Case
D3 WF1																			D3 WF1
D3 WF2	?																		D3 WF2
D3 WF3	?																		D3 WF3
D3 FD5	?	<	?																D3 FD5
D3 FD6	?	<		?															D3 FD6
D3 FD7			?	?	?														D3 FD7
D4 WF1																			D4 WF1
D4 WF2							?												D4 WF2
D4 WF3							?												D4 WF3
D4 FD5							?	?	?										D4 FD5
D4 FD6							?	<		?									D4 FD6
D4 FD7									?	?	?								D4 FD7
D5 WF1																			D5 WF1
D5 WF2													?						D5 WF2
D5 WF3													?						D5 WF3
D5 FD5													?	<	?				D5 FD5
D5 FD6													<	<		<			D5 FD6
D5 FD7															<	?	?		D5 FD7
Case	D3 WF1	D3 WF2	D3 WF3	D3 FD5	D3 FD6	D3 FD7	D4 WF1	D4 WF2	D4 WF3	D4 FD5	D4 FD6	D4 FD7	D5 WF1	D5 WF2	D5 WF3	D5 FD5	D5 FD6	D5 FD7	Case

Table E48. Results of Hypothesis Test 0 for MD STFI, comparing furnishes continued.

Case	D6 WF1	D6 WF2	D6 WF3	D6 FD5	D6 FD6	D6 FD7	C1S WF1	C1S WF2	C1S WF3	C1S FD5	C1S FD6	C1S FD7	C2S WF1	C2S WF2	C2S WF3	C2S FD5	C2S FD6	C2S FD7	Case
D6 WF1																			D6 WF1
D6 WF2	?																		D6 WF2
D6 WF3	?																		D6 WF3
D6 FD5	?	?	?																D6 FD5
D6 FD6	?	<		?															D6 FD6
D6 FD7			?	?	?														D6 FD7
C1S WF1																			C1S WF1
C1S WF2							?												C1S WF2
C1S WF3							?												C1S WF3
C1S FD5							?	<	?										C1S FD5
C1S FD6							?	<		?									C1S FD6
C1S FD7									?	?	?								C1S FD7
C2S WF1																			C2S WF1
C2S WF2													?						C2S WF2
C2S WF3													?						C2S WF3
C2S FD5													<	<	?				C2S FD5
C2S FD6													?	<		?			C2S FD6
C2S FD7															?	?	?		C2S FD7
Case	D6 WF1 C3S	D6 WF2 C3S	D6 WF3 C3S	D6 FD5 C3S	D6 FD6 C3S	D6 FD7 C3S	C1S WF1 A1S	C1S WF2 A1S	C1S WF3 A1S	C1S FD5 A1S	C1S FD6 A1S	C1S FD7 A1S	C2S WF1 A4S	C2S WF2 A4S	C2S WF3 A4S	C2S FD5 A4S	C2S FD6 A4S	C2S FD7 A4S	Case
C3S WF1																			C3S WF1
C3S WF2	?																		C3S WF2
C3S WF3	?																		C3S WF3
C3S FD5	?	<	?																C3S FD5
C3S FD6	?	<		?															C3S FD6
C3S FD7			?	?	?														C3S FD7
A1S WF1																			A1S WF1
A1S WF2							id												A1S WF2
A1S WF3							id												A1S WF3
A1S FD5							id	id	id										A1S FD5
A1S FD6							id	id		id									A1S FD6
A1S FD7									id	id	id								A1S FD7
A4S WF1																			A4S WF1
A4S WF2													>						A4S WF2
A4S WF3													?						A4S WF3
A4S FD5													?	?	?				A4S FD5
A4S FD6													<	<		?			A4S FD6
A4S FD7															?	?	?		A4S FD7
Case	C3S WF1	C3S WF2	C3S WF3	C3S FD5	C3S FD6	C3S FD7	A1S WF1	A1S WF2	A1S WF3	A1S FD5	A1S FD6	A1S FD7	A4S WF1	A4S WF2	A4S WF3	A4S FD5	A4S FD6	A4S FD7	Case

Table E49. Results of Hypothesis Test 0 for MD STFI, comparing furnishes continued.

Case	A5S WF1	A5S WF2	A5S WF3	A5S FD5	A5S FD6	A5S FD7	C1 WF1	C1 WF2	C1 WF3	C1 FD5	C1 FD6	C1 FD7	C2 WF1	C2 WF2	C2 WF3	C2 FD5	C2 FD6	C2 FD7	Case
A5S WF1																			A5S WF1
A5S WF2	id																		A5S WF2
A5S WF3	id																		A5S WF3
A5S FD5	id	<	?																A5S FD5
A5S FD6	id	<		?															A5S FD6
A5S FD7			?	?	?														A5S FD7
C1 WF1																			C1 WF1
C1 WF2							?												C1 WF2
C1 WF3							?												C1 WF3
C1 FD5							?	?	?										C1 FD5
C1 FD6							<	<		?									C1 FD6
C1 FD7									?	?	?								C1 FD7
C2 WF1																			C2 WF1
C2 WF2													?						C2 WF2
C2 WF3													?						C2 WF3
C2 FD5													?	<	?				C2 FD5
C2 FD6													?	<		?			C2 FD6
C2 FD7															<	?	?		C2 FD7
Case	A5S WF1 C3	A5S WF2 C3	A5S WF3 C3	A5S FD5 C3	A5S FD6 C3	A5S FD7 C3	C1 WF1 A1	C1 WF2 A1	C1 WF3 A1	C1 FD5 A1	C1 FD6 A1	C1 FD7 A1	C2 WF1 A2	C2 WF2 A2	C2 WF3 A2	C2 FD5 A2	C2 FD6 A2	C2 FD7 A2	Case
C3 WF1																			C3 WF1
C3 WF2	?																		C3 WF2
C3 WF3	?																		C3 WF3
C3 FD5	?	?	?																C3 FD5
C3 FD6	?	<		?															C3 FD6
C3 FD7			?	?	?														C3 FD7
A1 WF1																			A1 WF1
A1 WF2							?												A1 WF2
A1 WF3							?												A1 WF3
A1 FD5							?	?	?										A1 FD5
A1 FD6							?	?		?									A1 FD6
A1 FD7									?	?	?								A1 FD7
A2 WF1																			A2 WF1
A2 WF2													?						A2 WF2
A2 WF3													?						A2 WF3
A2 FD5													?	<	?				A2 FD5
A2 FD6													?	<		?			A2 FD6
A2 FD7															?	?	?		A2 FD7
Case	C3 WF1	C3 WF2	C3 WF3	C3 FD5	C3 FD6	C3 FD7	A1 WF1	A1 WF2	A1 WF3	A1 FD5	A1 FD6	A1 FD7	A2 WF1	A2 WF2	A2 WF3	A2 FD5	A2 FD6	A2 FD7	Case

Table E50. Results of Hypothesis Test 0 for MD STFI, comparing furnishes continued.

Case	A4 WF1	A4 WF2	A4 WF3	A4 FD5	A4 FD6	A4 FD7	A5 WF1	A5 WF2	A5 WF3	A5 FD5	A5 FD6	A5 FD7	A6 WF1	A6 WF2	A6 WF3	A6 FD5	A6 FD6	A6 FD7	Case
A4 WF1																			A4 WF1
A4 WF2	?																		A4 WF2
A4 WF3	?																		A4 WF3
A4 FD5	?	?	?																A4 FD5
A4 FD6	?	<		?															A4 FD6
A4 FD7			?	?	?														A4 FD7
A5 WF1																			A5 WF1
A5 WF2							?												A5 WF2
A5 WF3							?												A5 WF3
A5 FD5							<	<	?										A5 FD5
A5 FD6							?	?		?									A5 FD6
A5 FD7									?	?	?								A5 FD7
A6 WF1																			A6 WF1
A6 WF2													?						A6 WF2
A6 WF3													?						A6 WF3
A6 FD5													?	?	?				A6 FD5
A6 FD6													?	?		?			A6 FD6
A6 FD7															?	?	?		A6 FD7
Case	A4 WF1 A5F	A4 WF2 A5F	A4 WF3 A5F	A4 FD5 A5F	A4 FD6 A5F	A4 FD7 A5F	A5 WF1 A4H	A5 WF2 A4H	A5 WF3 A4H	A5 FD5 A4H	A5 FD6 A4H	A5 FD7 A4H	A6 WF1 A5H	A6 WF2 A5H	A6 WF3 A5H	A6 FD5 A5H	A6 FD6 A5H	A6 FD7 A5H	Case
A5F WF1																			A5F WF1
A5F WF2	?																		A5F WF2
A5F WF3	?																		A5F WF3
A5F FD5	id	id	id																A5F FD5
A5F FD6	<	<		id															A5F FD6
A5F FD7			?	id	?														A5F FD7
A4H WF1																			A4H WF1
A4H WF2							?												A4H WF2
A4H WF3							?												A4H WF3
A4H FD5							id	id	id										A4H FD5
A4H FD6							?	?		id									A4H FD6
A4H FD7									?	id	?								A4H FD7
A5H WF1																			A5H WF1
A5H WF2													?						A5H WF2
A5H WF3													<						A5H WF3
A5H FD5													id	id	id				A5H FD5
A5H FD6													<	?		id			A5H FD6
A5H FD7															<	id	?		A5H FD7
Case	A5F WF1	A5F WF2	A5F WF3	A5F FD5	A5F FD6	A5F FD7	A4H WF1	A4H WF2	A4H WF3	A4H FD5	A4H FD6	A4H FD7	A5H WF1	A5H WF2	A5H WF3	A5H FD5	A5H FD6	A5H FD7	Case

Table E51. Results of Hypothesis Test 1 for MD STFI and furnish WF1.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		0.0022	0.1608	0.0025	0.0108	0.0007	0.0014	0.0718	0.0001	0.1797	0.2484	0.0052	id	0.0050	0.0060	0.1447	0.0136	0.0117	0.0148	0.0281	0.0044	id	0.0240	0.5932	0.0000	Con
D1	>		0.6682	0.1897	0.5344			0.7463			0.3571			0.2594			0.2279									D1
D2	?(>)	?(>)				0.6022			0.6086						0.6867			0.9068								D2
D3	>	?(>)					0.5394			0.8670						0.5618										D3
D4	>	?(>)				0.3086	0.8344					0.1156							0.6693			id		0.9390		D4
D5	>		?(>)		?(>)								id							0.6591			0.7384		0.5444	D5
D6	>			?(<)	?(<)																0.3672					D6
C1S	>	?(>)							0.4767	0.9763	0.2693			0.7502												C1S
C2S	>		?(>)					?(>)							0.8834											C2S
C3S	?(>)			?(<)				?(<)								0.7037										C3S
A1S	?(>)	?(<)						?(<)				0.7226					0.1062									A1S
A4S	>				?(<)						?(>)		id						0.0946							A4S
A5S	id					id						id								id						A5S
C1	>	?(>)						?(>)							0.7232	0.4883	0.6358									C1
C2	>		?(>)						?(<)					?(>)				0.7190								C2
C3	?(>)			?(<)						?(<)				?(<)												C3
A1	>	?(>)									?(>)			?(>)				0.6361	0.7797							A1
A2	>		?(>)												?(<)		?(<)			0.4436						A2
A4	>				?(>)							>					?(<)			0.5348	0.9838	id		0.9876		A4
A5	>					?(>)							id					?(>)	?(>)				0.5538		0.8063	A5
A6	>						?(>)												?(<)							A6
A4F	id				id														id				id			A4F
A5F	>					?(<)														?(<)		id				A5F
A4H	?(>)				?(>)														?(>)						0.9436	A4H
A5H	>					?(>)														?(<)				?(>)		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E52. Results of Hypothesis Test 1 for MD STFI and furnish WF2.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		0.0016	0.0002	0.0001	0.0001	0.0000	0.0000	0.0002	0.0001	0.0001	id	0.0023	0.0069	0.0717	0.0001	0.0007	0.0011	0.0000	0.0026	0.0077	0.0364	id	id	0.8065	id	Con
D1	>		0.8000	0.9464	0.5236			0.9108			id			0.9317			0.6723									D1
D2	>	?(>)				0.0608			0.4414						0.2411			0.9947								D2
D3	>	?(>)					0.5897			0.5339						0.2278										D3
D4	>	?(<)				0.0166	0.1524					0.0055							0.8882			id		0.9951		D4
D5	>		>		>								0.0072							0.4939			id		id	D5
D6	>			?(>)	?(>)																0.2975					D6
C1S	>	?(<)							0.4024	0.5050	id			0.9617												C1S
C2S	>		?(>)					?(>)							0.6220											C2S
C3S	>			?(>)				?(>)								0.1526										C3S
A1S	id	id						id				id					id									A1S
A4S	>				<						id		0.9510						0.1176							A4S
A5S	>					<						?(>)								0.1008						A5S
C1	>	?(<)						?(<)							0.7419	0.7360	0.9423									C1
C2	>		?(>)						?(>)					?(>)				0.3302								C2
C3	>			?(<)						?(<)				?(<)												C3
A1	>	?(<)									id			?(<)				0.4524	0.8210							A1
A2	>		?(>)												?(<)		?(>)			0.9392						A2
A4	>				?(<)							?(>)					?(<)			0.6016	0.6339	id		0.9998		A4
A5	>					?(<)							?(>)					?(<)	?(>)				id		id	A5
A6	>						?(<)												?(<)							A6
A4F	id				id														id				id			A4F
A5F	id					id														id		id				A5F
A4H	?(>)				?(<)														?(>)						id	A4H
A5H	id					id														id				id		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E53. Results of Hypothesis Test 1 for MD STFI and furnish WF3.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		0.0136	0.0007	0.0191	0.0016	0.0005	0.0007	0.1004	0.0002	0.0011	id	0.0093	id	0.0005	<.0001	0.0063	<.0001	0.0001	0.0056	0.0519	0.0022	id	id	id	id	Con
D1	>		0.5177	0.9537	0.5960			0.7301			id			0.6958			0.6435									D1
D2	>	?(>)				0.1605			0.1583						0.5744			0.6822								D2
D3	>	?(>)					0.6077			0.7980						0.4523										D3
D4	>	?(<)				0.0699	0.1622					0.2497							0.1599			id		id		D4
D5	>		?(>)		>								id							0.6648			id		id	D5
D6	>			?(>)	?(>)																0.5000					D6
C1S	?(>)	?(>)							0.4420	0.5985	id			0.9751												C1S
C2S	>		?(>)					?(>)							0.4502											C2S
C3S	>			?(<)				?(<)								0.3161										C3S
A1S	id	id						id				id					id									A1S
A4S	>				?(<)						id		id						0.0887							A4S
A5S	id					id						id								id						A5S
C1	>	?(>)						?(<)							0.3687	0.6018	0.8785									C1
C2	>		?(>)						?(<)					?(>)				0.4878								C2
C3	>			?(>)						?(>)				?(>)												C3
A1	>	?(>)									id			?(>)				0.8793	0.5701							A1
A2	>		?(<)												?(<)		?(<)			0.4351						A2
A4	>				?(>)							>					?(>)			0.6517	0.9736	id		id		A4
A5	>					?(>)							id					?(>)	?(>)				id		id	A5
A6	>						?(>)												?(<)							A6
A4F	id				id														id				id			A4F
A5F	id					id														id		id				A5F
A4H	id				id														id					id		A4H
A5H	id					id														id				id		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E54. Results of Hypothesis Test 1for MD STFI and furnish FD5.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		0.2017	0.0072	0.0103	0.1167	0.0150	0.0598	0.0378	0.0183	0.0146	id	0.7753	0.2823	id	0.0760	0.0326	0.7291	id	0.3031	0.7889	id	id	id	id	id	Con
D1	?(>)		0.0428	0.0819	0.7999			0.3168			id			id			0.9075									D1
D2	>	>				0.1112			0.2528						0.2250			id								D2
D3	>	>					0.5057			0.6063						0.4895										D3
D4	?(>)	?(>)				0.1955	0.4125					0.4704							0.7999			id		id		D4
D5	>		?(<)		?(>)								0.0100							0.0738			id		id	D5
D6	>			?(<)	?(>)																id					D6
C1S	>	?(>)							0.6861	0.5703	id			id												C1S
C2S	>		?(<)					?(>)							0.5832											C2S
C3S	>			?(<)				?(>)								0.7483										C3S
A1S	id	id						id				id					id									A1S
A4S	?(<)				?(<)						id		0.9016						0.3965							A4S
A5S	?(<)					<						?(<)								0.2552						A5S
C1	id	id						id							id	id	id									C1
C2	>		?(<)						?(<)					id				id								C2
C3	>			?(<)						?(<)				id												C3
A1	?(>)	?(>)									id			id				id	0.9950							A1
A2	id		id												id		id			id						A2
A4	?(>)				?(>)							?(>)					?(>)			0.3933	id	id		id		A4
A5	?(>)					<							?(>)					id	?(<)				id		id	A5
A6	id						id												id							A6
A4F	id				id														id				id			A4F
A5F	id					id														id		id				A5F
A4H	id				id														id						id	A4H
A5H	id					id														id				id		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E55. Results of Hypothesis Test 1 for MD STFI and furnish FD6.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		0.0038	0.0104	0.0135	0.0108	0.0029	0.0104	0.0055	0.0007	0.0009	id	0.0322	0.3696	0.0011	0.0020	0.0015	0.0722	0.0065	0.0222	0.0613	0.0001	id	0.0031	0.0737	0.0013	Con
D1	>		0.6440	0.2742	0.8314			0.7861			id			0.1482			0.3488									D1
D2	>	?(>)				0.7326			0.1200						0.1207			0.1439								D2
D3	>	?(>)					0.5213			0.9909						0.6408										D3
D4	>	?(>)				0.9142	0.7852					0.0953								0.3975			id		0.3434		D4
D5	>		?(<)		?(<)								0.0591								0.3050			0.3473		0.0600	D5
D6	>			?(<)	?(>)																	0.1000					D6
C1S	>	?(>)							0.0580	0.1814	id			0.3075												C1S
C2S	>		?(>)					>							0.6487											C2S
C3S	>			?(>)				?(>)								0.0985										C3S
A1S	id	id						id				id					id									A1S
A4S	>				<						id		0.4754						0.0731							A4S
A5S	?(>)					<						?(<)								0.0829						A5S
C1	>	?(>)						?(>)							0.2169	0.7044	0.6249									C1
C2	>		?(>)						?(>)					?(>)				0.9641								C2
C3	>			?(<)						<				?(<)												C3
A1	>	?(>)									id			?(>)				0.8651	0.7793							A1
A2	>		?(>)												?(>)		?(>)			0.9920						A2
A4	>				?(>)							>					?(<)			0.6665	0.5371	id		0.6746		A4
A5	>					?(>)							>					?(<)	?(>)				0.5615		0.8405	A5
A6	>						>												?(>)							A6
A4F	id				id														id				id			A4F
A5F	>					?(>)														?(<)		id				A5F
A4H	>				?(>)														?(>)						0.8650	A4H
A5H	>					>														?(>)				?(>)		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E56. Results of Hypothesis Test 1 for MD STFI and furnish FD7.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		id	0.0034	0.0002	0.0024	0.0001	id	0.0002	0.0008	0.0000	id	0.4728	0.3373	0.0015	0.0000	0.0011	0.0012	id	0.0719	0.0631	0.0061	id	id	0.0001	id	Con
D1	id		id	id	id			id			id			id			id									D1
D2	>	id				0.7636			0.4111						0.7295			id								D2
D3	>	id					id			0.4966						0.4076										D3
D4	>	id				0.2151	id					0.0134							0.9007			id		0.1629		D4
D5	>		?(<)		?(<)								#DIV/							0.3773			id		id	D5
D6	id			id	id																id					D6
C1S	>	id							0.8082	0.9356	id			0.1144												C1S
C2S	>		?(>)					?(<)							0.1833											C2S
C3S	>			?(>)				?(>)								0.2076										C3S
A1S	id	id						id				id					id									A1S
A4S	?(>)				<						id		0.7628						0.0962							A4S
A5S	?(>)					<						?(<)								0.0738						A5S
C1	>	id						?(<)							0.8005	0.8401	0.2194									C1
C2	>		?(<)						?(<)					?(>)				id								C2
C3	>			?(<)						?(<)				?(>)												C3
A1	>	id									id			?(>)				id	0.9590							A1
A2	id		id												id		id			id						A2
A4	>				?(<)							>					?(<)			0.6335	0.8712	id		0.5737		A4
A5	>					?(>)							>					id	?(>)				id		id	A5
A6	>						id												?(>)							A6
A4F	id				id														id				id			A4F
A5F	id					id														id		id				A5F
A4H	>				?(<)														?(<)						id	A4H
A5H	id					id														id				id		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E57. Results of Hypothesis Test 1 for MD STFI, comparing furnishes.

Case	Con WF1	Con WF2	Con WF3	Con FD5	Con FD6	Con FD7	D1 WF1	D1 WF2	D1 WF3	D1 FD5	D1 FD6	D1 FD7	D2 WF1	D2 WF2	D2 WF3	D2 FD5	D2 FD6	D2 FD7	Case
Con WF1		0.0023	0.1032	0.1402	0.2218														Con WF1
Con WF2	>			0.0921	0.0003														Con WF2
Con WF3	?(<)			0.0389		0.0476													Con WF3
Con FD5	?(>)	<	>		0.0684	0.2301													Con FD5
Con FD6	?(<)	<		<		0.0909													Con FD6
Con FD7			>	?(<)	>														Con FD7
D1 WF1								0.0156	0.4038	0.0729	0.0044								D1 WF1
D1 WF2							>			0.0037	0.0015								D1 WF2
D1 WF3							?(<)			0.4093		id							D1 WF3
D1 FD5							<	<	?(<)		0.2674	id							D1 FD5
D1 FD6							<	<		?(<)		id							D1 FD6
D1 FD7									id	id	id								D1 FD7
D2 WF1														0.4655	0.5770	0.7432	0.2612		D2 WF1
D2 WF2													?(>)			0.0004	0.0027		D2 WF2
D2 WF3													?(<)			0.1502		0.0443	D2 WF3
D2 FD5													?(<)	<	?(>)		0.0079	0.0114	D2 FD5
D2 FD6													?(<)	<		<		0.1648	D2 FD6
D2 FD7															<	<	?(>)		D2 FD7
Case	Con WF1 D3	Con WF2 D3	Con WF3 D3	Con FD5 D3	Con FD6 D3	Con FD7 D3	D1 WF1 D4	D1 WF2 D4	D1 WF3 D4	D1 FD5 D4	D1 FD6 D4	D1 FD7 D4	D2 WF1 D5	D2 WF2 D5	D2 WF3 D5	D2 FD5 D5	D2 FD6 D5	D2 FD7 D5	Case
D3 WF1		0.0171	0.2300	0.1296	0.0179														D3 WF1
D3 WF2	>			0.0064	0.0082														D3 WF2
D3 WF3	?(<)			0.4135		0.6393													D3 WF3
D3 FD5	?(<)	<	?(>)		0.0681	0.0909													D3 FD5
D3 FD6	<	<		<		0.3501													D3 FD6
D3 FD7			?(<)	<	?(>)														D3 FD7
D4 WF1								0.2945	0.1020	0.0833	0.0216								D4 WF1
D4 WF2							?(>)			0.0205	0.0010								D4 WF2
D4 WF3							?(<)			0.7516		0.4684							D4 WF3
D4 FD5							<	<	?(<)		0.2061	0.3533							D4 FD5
D4 FD6							<	<		?(<)		0.0363							D4 FD6
D4 FD7									?(>)	?(>)	>								D4 FD7
D5 WF1														0.0976	0.0205	0.0049	0.0001		D5 WF1
D5 WF2													>			0.0003	0.0000		D5 WF2
D5 WF3													<			0.1318		0.0006	D5 WF3
D5 FD5													<	<	?(<)		0.0035	0.0377	D5 FD5
D5 FD6													<	<		<		0.0307	D5 FD6
D5 FD7															<	<	>		D5 FD7
Case	D3 WF1	D3 WF2	D3 WF3	D3 FD5	D3 FD6	D3 FD7	D4 WF1	D4 WF2	D4 WF3	D4 FD5	D4 FD6	D4 FD7	D5 WF1	D5 WF2	D5 WF3	D5 FD5	D5 FD6	D5 FD7	Case

Table E58. Results of Hypothesis Test 1 for MD STFI, comparing furnishes continued.

Case	D6 WF1	D6 WF2	D6 WF3	D6 FD5	D6 FD6	D6 FD7	C1S WF1	C1S WF2	C1S WF3	C1S FD5	C1S FD6	C1S FD7	C2S WF1	C2S WF2	C2S WF3	C2S FD5	C2S FD6	C2S FD7	Case
D6 WF1		0.0157	0.2083	0.2405	0.0052														D6 WF1
D6 WF2	>			0.0331	0.0010														D6 WF2
D6 WF3	?(<)			0.7115		id													D6 WF3
D6 FD5	?(<)	<	?(<)		0.1428	id													D6 FD5
D6 FD6	<	<		?(<)		id													D6 FD6
D6 FD7			id	id	id														D6 FD7
C1S WF1								0.3860	0.5600	0.4257	0.1586								C1S WF1
C1S WF2							?(>)			0.0072	0.0002								C1S WF2
C1S WF3							?(<)			0.7101		0.6461							C1S WF3
C1S FD5							?(<)	<	?(<)		0.0490	0.8903							C1S FD5
C1S FD6							?(<)	<		<		0.0217							C1S FD6
C1S FD7									?(<)	?(<)	>								C1S FD7
C2S WF1														0.0280	0.0382	0.0144	0.0012		C2S WF1
C2S WF2													>			0.0052	0.0037		C2S WF2
C2S WF3													<			0.1757		0.0256	C2S WF3
C2S FD5													<	<	?(<)		0.1770	0.4191	C2S FD5
C2S FD6													<	<		?(<)		0.3600	C2S FD6
C2S FD7															<	?(<)	?(>)		C2S FD7
Case	D6 WF1 C3S	D6 WF2 C3S	D6 WF3 C3S	D6 FD5 C3S	D6 FD6 C3S	D6 FD7 C3S	C1S WF1 A1S	C1S WF2 A1S	C1S WF3 A1S	C1S FD5 A1S	C1S FD6 A1S	C1S FD7 A1S	C2S WF1 A4S	C2S WF2 A4S	C2S WF3 A4S	C2S FD5 A4S	C2S FD6 A4S	C2S FD7 A4S	Case
C3S WF1		0.4028	0.4871	0.6490	0.3457														C3S WF1
C3S WF2	?(>)			0.0011	0.0002														C3S WF2
C3S WF3	?(<)			0.2472		0.7405													C3S WF3
C3S FD5	?(<)	<	?(>)		0.0242	0.3070													C3S FD5
C3S FD6	?(<)	<		<		0.0091													C3S FD6
C3S FD7			?(>)	?(<)	>														C3S FD7
A1S WF1								id	id	id	id								A1S WF1
A1S WF2							id			id	id								A1S WF2
A1S WF3							id			id		id							A1S WF3
A1S FD5							id	id	id		id	id							A1S FD5
A1S FD6							id	id		id		id							A1S FD6
A1S FD7									id	id	id								A1S FD7
A4S WF1														0.0135	0.1696	0.4310	0.0036		A4S WF1
A4S WF2													>			0.2765	0.0000		A4S WF2
A4S WF3													?(<)			0.5345		0.0839	A4S WF3
A4S FD5													?(<)	?(<)	?(<)		0.9526	0.9264	A4S FD5
A4S FD6													<	<		?(>)		0.8767	A4S FD6
A4S FD7															<	?(>)	?(>)		A4S FD7
Case	C3S WF1	C3S WF2	C3S WF3	C3S FD5	C3S FD6	C3S FD7	A1S WF1	A1S WF2	A1S WF3	A1S FD5	A1S FD6	A1S FD7	A4S WF1	A4S WF2	A4S WF3	A4S FD5	A4S FD6	A4S FD7	Case

Table E59. Results of Hypothesis Test 1 for MD STFI, comparing furnishes continued.

Case	A5S WF1	A5S WF2	A5S WF3	A5S FD5	A5S FD6	A5S FD7	C1 WF1	C1 WF2	C1 WF3	C1 FD5	C1 FD6	C1 FD7	C2 WF1	C2 WF2	C2 WF3	C2 FD5	C2 FD6	C2 FD7	Case
A5S WF1		id	id	id	id														A5S WF1
A5S WF2	id			0.0022	0.0004														A5S WF2
A5S WF3	id			id		id													A5S WF3
A5S FD5	id	<	id		0.9768	0.6182													A5S FD5
A5S FD6	id	<		?(>)		0.5350													A5S FD6
A5S FD7			id	?(>)	?(>)														A5S FD7
C1 WF1								0.6032	0.1214	id	0.0182								C1 WF1
C1 WF2							?(>)			id	0.0523								C1 WF2
C1 WF3							?(<)			id		0.0488							C1 WF3
C1 FD5							id	id	id		id	id							C1 FD5
C1 FD6							<	<		id		0.5589							C1 FD6
C1 FD7									<	id	?(>)								C1 FD7
C2 WF1														0.4257	0.2479	0.0942	0.0720		C2 WF1
C2 WF2													?(>)			0.0369	0.0029		C2 WF2
C2 WF3													?(<)			0.2657		0.0064	C2 WF3
C2 FD5													<	<	?(<)		0.9170	0.4726	C2 FD5
C2 FD6													<	<		?(<)		0.4460	C2 FD6
C2 FD7															<	?(<)	?(<)		C2 FD7
Case	A5S WF1 C3	A5S WF2 C3	A5S WF3 C3	A5S FD5 C3	A5S FD6 C3	A5S FD7 C3	C1 WF1 A1	C1 WF2 A1	C1 WF3 A1	C1 FD5 A1	C1 FD6 A1	C1 FD7 A1	C2 WF1 A2	C2 WF2 A2	C2 WF3 A2	C2 FD5 A2	C2 FD6 A2	C2 FD7 A2	Case
C3 WF1		0.3941	0.8367	0.9419	0.4542														C3 WF1
C3 WF2	?(>)			0.0370	0.0003														C3 WF2
C3 WF3	?(>)			0.5373		0.1379													C3 WF3
C3 FD5	?(<)	<	?(<)		0.0964	0.2696													C3 FD5
C3 FD6	?(<)	<		<		0.2919													C3 FD6
C3 FD7			?(<)	?(<)	?(>)														C3 FD7
A1 WF1								0.9263	0.1529	0.6198	0.1180								A1 WF1
A1 WF2							?(>)			0.5980	0.0698								A1 WF2
A1 WF3							?(<)			0.8854		0.3413							A1 WF3
A1 FD5							?(<)	?(<)	?(<)		0.9776	0.9747							A1 FD5
A1 FD6							?(<)	<		?(<)		0.8187							A1 FD6
A1 FD7									?(<)	?(>)	?(>)								A1 FD7
A2 WF1														0.2908	0.2313	id	0.1306		A2 WF1
A2 WF2													?(>)			id	0.0077		A2 WF2
A2 WF3													?(<)			id		id	A2 WF3
A2 FD5													id	id	id		id	id	A2 FD5
A2 FD6													?(<)	<		id		id	A2 FD6
A2 FD7															id	id	id		A2 FD7
Case	C3 WF1	C3 WF2	C3 WF3	C3 FD5	C3 FD6	C3 FD7	A1 WF1	A1 WF2	A1 WF3	A1 FD5	A1 FD6	A1 FD7	A2 WF1	A2 WF2	A2 WF3	A2 FD5	A2 FD6	A2 FD7	Case

Table E60. Results of Hypothesis Test 1 for MD STFI, comparing furnishes continued.

Case	A4 WF1	A4 WF2	A4 WF3	A4 FD5	A4 FD6	A4 FD7	A5 WF1	A5 WF2	A5 WF3	A5 FD5	A5 FD6	A5 FD7	A6 WF1	A6 WF2	A6 WF3	A6 FD5	A6 FD6	A6 FD7	Case
A4 WF1		0.7431	0.3882	0.2524	0.0733														A4 WF1
A4 WF2	?(>)			0.1505	0.0138														A4 WF2
A4 WF3	?(<)			0.5063		0.4069													A4 WF3
A4 FD5	?(<)	?(<)	?(<)		0.7361	0.9721													A4 FD5
A4 FD6	<	<		?(<)		0.6265													A4 FD6
A4 FD7			?(<)	?(>)	?(>)														A4 FD7
A5 WF1								0.8195	0.4509	0.0493	0.1385								A5 WF1
A5 WF2							?(<)			0.0044	0.0674								A5 WF2
A5 WF3							?(<)			0.0919		0.6028							A5 WF3
A5 FD5							<	<	<		0.3136	0.1653							A5 FD5
A5 FD6							?(<)	<		?(>)		0.6441							A5 FD6
A5 FD7									?(<)	?(>)	?(>)								A5 FD7
A6 WF1														0.9640	0.2059	id	0.0338		A6 WF1
A6 WF2													?(<)			id	0.0575		A6 WF2
A6 WF3													?(<)			id		0.2644	A6 WF3
A6 FD5													id	id	id		id	id	A6 FD5
A6 FD6													<	<		id		0.6292	A6 FD6
A6 FD7															?(<)	id	?(>)		A6 FD7
Case	A4 WF1 A5F	A4 WF2 A5F	A4 WF3 A5F	A4 FD5 A5F	A4 FD6 A5F	A4 FD7 A5F	A5 WF1 A4H	A5 WF2 A4H	A5 WF3 A4H	A5 FD5 A4H	A5 FD6 A4H	A5 FD7 A4H	A6 WF1 A5H	A6 WF2 A5H	A6 WF3 A5H	A6 FD5 A5H	A6 FD6 A5H	A6 FD7 A5H	Case
A5F WF1		id	id	id	0.0913														A5F WF1
A5F WF2	id			id	id														A5F WF2
A5F WF3	id			id		id													A5F WF3
A5F FD5	id	id	id		id	id													A5F FD5
A5F FD6	<	id		id		id													A5F FD6
A5F FD7			id	id	id														A5F FD7
A4H WF1								0.9866	id	id	0.8110								A4H WF1
A4H WF2							?(>)			id	0.8371								A4H WF2
A4H WF3							id			id		id							A4H WF3
A4H FD5							id	id	id		id	id							A4H FD5
A4H FD6							?(<)	?(<)		id		0.6507							A4H FD6
A4H FD7									id	id	?(<)								A4H FD7
A5H WF1														id	id	id	0.0086		A5H WF1
A5H WF2													id			id	id		A5H WF2
A5H WF3													id			id		id	A5H WF3
A5H FD5													id	id	id		id	id	A5H FD5
A5H FD6													<	id		id		id	A5H FD6
A5H FD7															id	id	id		A5H FD7
Case	A5F WF1	A5F WF2	A5F WF3	A5F FD5	A5F FD6	A5F FD7	A4H WF1	A4H WF2	A4H WF3	A4H FD5	A4H FD6	A4H FD7	A5H WF1	A5H WF2	A5H WF3	A5H FD5	A5H FD6	A5H FD7	Case

Table E61. Results of Hypothesis Test 2 for MD STFI and furnish WF1.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		0.0022	0.1608	0.0025	0.0108	0.0007	0.0014	0.0718	0.0001	0.1797	0.2484	0.0052	id	0.0015	0.0019	0.1743	0.0032	0.0077	0.0029	0.0026	0.0027	id	0.0044	0.5932	0.0000	Con
D1	>		0.6682	0.1897	0.5344			0.7463			0.3571			0.0511			0.0290									D1
D2	?(>)	?(>)				0.6022			0.6086						0.4843			0.7150								D2
D3	>	?(>)					0.5394			0.8670						0.3047										D3
D4	>	?(>)				0.3086	0.8344					0.1156							0.1796			id		0.9390		D4
D5	>		?(>)		?(>)								id							0.0410			0.4287		0.2839	D5
D6	>			?(<)	?(<)																0.2158					D6
C1S	>	?(>)							0.4767	0.9763	0.2693			0.4934												C1S
C2S	>		?(>)					?(>)							0.6724											C2S
C3S	?(>)			?(<)				?(<)								0.4551										C3S
A1S	?(>)	?(<)						?(<)				0.7226					0.0730									A1S
A4S	>				?(<)						?(>)		id						0.0077							A4S
A5S	id					id						id								id						A5S
C1	>	>						?(>)							0.6649	0.1629	0.2935									C1
C2	>		?(>)						?(>)					?(>)				0.1232								C2
C3	?(>)			?(<)						?(<)				?(<)												C3
A1	>	>									>			?(>)				0.0487	0.7215							A1
A2	>		?(<)												?(<)		<			0.0105						A2
A4	>				?(>)							>					?(<)			0.0813	0.3995	id		0.9264		A4
A5	>					>							id					>	>				0.1278		0.0714	A5
A6	>						?(>)												?(<)							A6
A4F	id				id														id				id			A4F
A5F	>					?(>)														?(<)		id				A5F
A4H	?(>)				?(>)														?(<)						0.9243	A4H
A5H	>					?(>)														<				?(>)		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E62. Results of Hypothesis Test 2 for MD STFI and furnish WF2.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		0.0016	0.0002	0.0001	0.0001	0.0000	0.0000	0.0002	0.0001	0.0001	id	0.0023	0.0069	0.0053	0.0002	0.0004	0.0010	0.0001	0.0002	0.0005	0.0369	id	id	0.8065	id	Con
D1	>		0.8000	0.9464	0.5236			0.9108			id			0.3995			0.5801									D1
D2	>	?(>)				0.0608			0.4414						0.1720			0.7150								D2
D3	>	?(>)					0.5897			0.5339						0.0437										D3
D4	>	?(<)				0.0166	0.1524					0.0055							0.3665			id		0.9951		D4
D5	>		>		>								0.0072							0.8203			id		id	D5
D6	>			?(>)	?(>)																0.2269					D6
C1S	>	?(<)							0.4024	0.5050	id			0.3653												C1S
C2S	>		?(>)					?(>)							0.4878											C2S
C3S	>			?(>)				?(>)								0.0303										C3S
A1S	id	id						id				id					id									A1S
A4S	>				<						id		0.9510						0.0117							A4S
A5S	>					<						?(>)								0.0103						A5S
C1	>	?(>)						?(>)							0.6045	0.1151	0.2756									C1
C2	>		?(>)						?(>)					?(<)				0.1280								C2
C3	>			<						<				?(<)												C3
A1	>	?(<)									id			?(<)				0.4376	0.4580							A1
A2	>		?(<)												?(<)		?(>)			0.2420						A2
A4	>				?(>)							>					?(>)			0.3173	0.2539	id		0.9695		A4
A5	>					?(>)							>					?(>)	?(>)				id		id	A5
A6	>						?(<)												?(<)							A6
A4F	id				id														id				id			A4F
A5F	id					id														id		id				A5F
A4H	?(>)				?(<)														?(<)						id	A4H
A5H	id					id														id				id		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E63. Results of Hypothesis Test 2 for MD STFI and furnish WF3.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		0.0136	0.0007	0.0191	0.0016	0.0005	0.0007	0.1004	0.0002	0.0011	id	0.0093	id	0.0005	0.0000	0.0020	<.0001	0.0001	0.0014	0.0139	0.0004	id	id	id	id	Con
D1	>		0.5177	0.9537	0.5960			0.7301			id			0.7511			0.6424									D1
D2	>	?(>)				0.1605			0.1583						0.9951			0.7508								D2
D3	>	?(>)					0.6077			0.7980						0.1267										D3
D4	>	?(<)				0.0699	0.1622					0.2497							0.0181			id		id		D4
D5	>		?(>)		>								id							0.0966			id		id	D5
D6	>			?(>)	?(>)																0.8747					D6
C1S	?(>)	?(>)							0.4420	0.5985	id			0.9174												C1S
C2S	>		?(>)					?(>)							0.1704											C2S
C3S	>			?(<)				?(<)								0.0824										C3S
A1S	id	id						id				id					id									A1S
A4S	>				?(<)						id		id						0.0232							A4S
A5S	id					id						id								id						A5S
C1	>	?(>)						?(<)							0.5004	0.1169	0.7723									C1
C2	>		?(<)						?(<)					?(>)				0.7672								C2
C3	>			?(>)						>				?(>)												C3
A1	>	?(>)									id			?(>)				0.9509	0.0668							A1
A2	>		?(<)												?(<)		?(<)			0.0382						A2
A4	>				>							>					>			0.1572	0.0915	id		id		A4
A5	>					>							id					>	?(>)				id		id	A5
A6	>						?(>)												<							A6
A4F	id				id														id				id			A4F
A5F	id					id														id		id				A5F
A4H	id				id														id						id	A4H
A5H	id					id														id				id		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E64. Results of Hypothesis Test 2 for MD STFI and furnish FD5.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		0.2017	0.0072	0.0103	0.1167	0.0150	0.0598	0.0378	0.0183	0.0146	id	0.7753	0.2823	id	0.1093	0.0386	0.9564	id	0.1180	0.3146	id	id	id	id	id	Con
D1	?(>)		0.0428	0.0819	0.7999			0.3168			id			id			0.8457									D1
D2	>	>				0.1112			0.2528						0.0808			id								D2
D3	>	>					0.5057			0.6063						0.2786										D3
D4	?(>)	?(>)				0.1955	0.4125					0.4704							0.3907			id		id		D4
D5	>		?(<)		?(>)								0.0100							0.1013			id		id	D5
D6	>			?(<)	?(>)																id					D6
C1S	>	?(>)							0.6861	0.5703	id			id												C1S
C2S	>		?(<)					?(>)							0.3145											C2S
C3S	>			?(<)				?(>)								0.4842										C3S
A1S	id	id						id				id					id									A1S
A4S	?(<)				?(<)						id		0.9016						0.2750							A4S
A5S	?(<)					<						?(<)								0.0741						A5S
C1	id	id						id							id	id	id									C1
C2	?(>)		<						?(<)					id				id								C2
C3	>			?(<)						?(<)				id												C3
A1	?(>)	?(<)									id			id				id	0.6590							A1
A2	id		id												id		id			id						A2
A4	?(>)				?(>)							?(>)					?(>)			0.2618	id	id		id		A4
A5	?(>)					?(<)							>					id	?(<)				id		id	A5
A6	id						id												id							A6
A4F	id				id														id				id			A4F
A5F	id					id														id		id				A5F
A4H	id				id														id						id	A4H
A5H	id					id														id				id		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E65. Results of Hypothesis Test 2 for MD STFI and furnish FD6.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		0.0038	0.0104	0.0135	0.0108	0.0029	0.0104	0.0055	0.0007	0.0009	id	0.0322	0.3696	0.0004	0.0001	0.0015	0.0592	0.0015	0.0063	0.0051	0.0000	id	0.0004	0.0053	0.0012	Con
D1	>		0.6440	0.2742	0.8314			0.7861			id			0.0451			0.5505									D1
D2	>	?(>)				0.7326			0.1200						0.0254			0.0674								D2
D3	>	?(>)					0.5213			0.9909						0.5470										D3
D4	>	?(>)				0.9142	0.7852					0.0953							0.1202			id		0.0304		D4
D5	>		?(<)		?(<)								0.0591							0.0339			0.1306		0.0616	D5
D6	>			?(<)	?(>)																0.0793					D6
C1S	>	?(>)							0.0580	0.1814	id			0.1526												C1S
C2S	>		?(>)					>							0.1281											C2S
C3S	>			?(>)				?(>)								0.0280										C3S
A1S	id	id						id				id					id									A1S
A4S	>				<						id		0.4754						0.0182							A4S
A5S	?(>)					<						?(<)								0.0073						A5S
C1	>	>						?(>)							0.0426	0.1791	0.8499									C1
C2	>		>						?(>)					>				0.7874								C2
C3	>			?(<)						<				?(<)												C3
A1	>	?(>)									id			?(<)				0.3386	0.5308							A1
A2	>		>												?(<)		?(>)			0.3856						A2
A4	>				?(>)							>					?(>)			0.2392	0.8919	id		0.1940		A4
A5	>					>							>					?(>)	?(>)				0.1216		0.3924	A5
A6	>						>												?(>)							A6
A4F	id				id														id				id			A4F
A5F	>					?(>)														?(<)		id				A5F
A4H	>				>														?(>)						0.3198	A4H
A5H	>					>														?(<)				?(<)		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E66. Results of Hypothesis Test 2 for MD STFI and furnish FD7.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		id	0.0034	0.0002	0.0024	0.0001	id	0.0002	0.0008	0.0000	id	0.4728	0.3373	0.0011	0.0000	0.0006	0.0012	id	0.0122	0.0191	0.0053	id	id	0.0000	id	Con
D1	id		id	id	id			id			id			id			id									D1
D2	>	id				0.7636			0.4111						0.7295			id								D2
D3	>	id					id			0.4966						0.1616										D3
D4	>	id				0.2151	id					0.0134							0.3105			id		0.2159		D4
D5	>		?(<)		?(<)								err							0.1112			id		id	D5
D6	id			id	id																id					D6
C1S	>	id							0.8082	0.9356	id			0.0369												C1S
C2S	>		?(>)					?(<)							0.1833											C2S
C3S	>			?(>)				?(>)								0.0536										C3S
A1S	id	id						id				id					id									A1S
A4S	?(>)				<						id		0.7628						0.0086							A4S
A5S	?(>)					<						?(<)								0.0221						A5S
C1	>	id						<							0.3851	0.8136	0.1052									C1
C2	>		?(<)						?(<)					?(>)				id								C2
C3	>			?(<)						<				?(>)												C3
A1	>	id									id			?(>)				id	0.2722							A1
A2	id		id												id		id			id						A2
A4	>				?(>)							>					?(>)			0.6055	0.2759	id		0.1019		A4
A5	>					?(>)							>					id	?(>)				id		id	A5
A6	>						id												?(<)							A6
A4F	id				id														id				id			A4F
A5F	id					id														id		id				A5F
A4H	>				?(<)														?(<)						id	A4H
A5H	id					id														id				id		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E67. Results of Hypothesis Test 2 for MD STFI, comparing furnishes.

Case	Con WF1	Con WF2	Con WF3	Con FD5	Con FD6	Con FD7	D1 WF1	D1 WF2	D1 WF3	D1 FD5	D1 FD6	D1 FD7	D2 WF1	D2 WF2	D2 WF3	D2 FD5	D2 FD6	D2 FD7	Case
Con WF1		0.0023	0.1032	0.1402	0.2218														Con WF1
Con WF2	>			0.0921	0.0003														Con WF2
Con WF3	?(<)			0.0389		0.0476													Con WF3
Con FD5	?(>)	<	>		0.0684	0.2301													Con FD5
Con FD6	?(<)	<		<		0.0909													Con FD6
Con FD7			>	?(<)	>														Con FD7
D1 WF1								0.0156	0.4038	0.0729	0.0044								D1 WF1
D1 WF2							>			0.0037	0.0015								D1 WF2
D1 WF3							?(<)			0.4093		id							D1 WF3
D1 FD5							<	<	?(<)		0.2674	id							D1 FD5
D1 FD6							<	<		?(<)		id							D1 FD6
D1 FD7									id	id	id								D1 FD7
D2 WF1														0.4655	0.5770	0.7432	0.2612		D2 WF1
D2 WF2													?(>)			0.0004	0.0027		D2 WF2
D2 WF3													?(<)			0.1502		0.0443	D2 WF3
D2 FD5													?(<)	<	?(>)		0.0079	0.0114	D2 FD5
D2 FD6													?(<)	<		<		0.1648	D2 FD6
D2 FD7															<	<	?(>)		D2 FD7

Case	Con WF1 D3	Con WF2 D3	Con WF3 D3	Con FD5 D3	Con FD6 D3	Con FD7 D3	D1 WF1 D4	D1 WF2 D4	D1 WF3 D4	D1 FD5 D4	D1 FD6 D4	D1 FD7 D4	D2 WF1 D5	D2 WF2 D5	D2 WF3 D5	D2 FD5 D5	D2 FD6 D5	D2 FD7 D5	Case
D3 WF1		0.0171	0.2300	0.1296	0.0179														D3 WF1
D3 WF2	>			0.0064	0.0082														D3 WF2
D3 WF3	?(<)			0.4135		0.6393													D3 WF3
D3 FD5	?(<)	<	?(>)		0.0681	0.0909													D3 FD5
D3 FD6	<	<		<		0.3501													D3 FD6
D3 FD7			?(<)	<	?(>)														D3 FD7
D4 WF1								0.2945	0.1020	0.0833	0.0216								D4 WF1
D4 WF2							?(>)			0.0205	0.0010								D4 WF2
D4 WF3							?(<)			0.7516		0.4684							D4 WF3
D4 FD5							<	<	?(<)		0.2061	0.3533							D4 FD5
D4 FD6							<	<		?(<)		0.0363							D4 FD6
D4 FD7									?(>)	?(>)	>								D4 FD7
D5 WF1														0.0976	0.0205	0.0049	0.0001		D5 WF1
D5 WF2													>			0.0003	0.0000		D5 WF2
D5 WF3													<			0.1318		0.0006	D5 WF3
D5 FD5													<	<	?(<)		0.0035	0.0377	D5 FD5
D5 FD6													<	<		<		0.0307	D5 FD6
D5 FD7															<	<	>		D5 FD7
Case	D3 WF1	D3 WF2	D3 WF3	D3 FD5	D3 FD6	D3 FD7	D4 WF1	D4 WF2	D4 WF3	D4 FD5	D4 FD6	D4 FD7	D5 WF1	D5 WF2	D5 WF3	D5 FD5	D5 FD6	D5 FD7	Case

Table E68. Results of Hypothesis Test 2 for MD STFI, comparing furnishes continued.

Case	D6 WF1	D6 WF2	D6 WF3	D6 FD5	D6 FD6	D6 FD7	C1S WF1	C1S WF2	C1S WF3	C1S FD5	C1S FD6	C1S FD7	C2S WF1	C2S WF2	C2S WF3	C2S FD5	C2S FD6	C2S FD7	Case
D6 WF1		0.0157	0.2083	0.2405	0.0052														D6 WF1
D6 WF2	>			0.0331	0.0010														D6 WF2
D6 WF3	?(<)			0.7115		id													D6 WF3
D6 FD5	?(<)	<	?(<)		0.1428	id													D6 FD5
D6 FD6	<	<		?(<)		id													D6 FD6
D6 FD7			id	id	id														D6 FD7
C1S WF1								0.3860	0.5600	0.4257	0.1586								C1S WF1
C1S WF2							?(>)			0.0072	0.0002								C1S WF2
C1S WF3							?(<)			0.7101		0.6461							C1S WF3
C1S FD5							?(<)	<	?(<)		0.0490	0.8903							C1S FD5
C1S FD6							?(<)	<		<		0.0217							C1S FD6
C1S FD7									?(<)	?(<)	>								C1S FD7
C2S WF1														0.0280	0.0382	0.0144	0.0012		C2S WF1
C2S WF2													>			0.0052	0.0037		C2S WF2
C2S WF3													<			0.1757		0.0256	C2S WF3
C2S FD5													<	<	?(<)		0.1770	0.4191	C2S FD5
C2S FD6													<	<		?(<)		0.3600	C2S FD6
C2S FD7															<	?(<)	?(>)		C2S FD7

Case	D6 WF1	D6 WF2	D6 WF3	D6 FD5	D6 FD6	D6 FD7	C1S WF1	C1S WF2	C1S WF3	C1S FD5	C1S FD6	C1S FD7	C2S WF1	C2S WF2	C2S WF3	C2S FD5	C2S FD6	C2S FD7	Case
	C3S	C3S	C3S	C3S	C3S	C3S	A1S	A1S	A1S	A1S	A1S	A1S	A4S	A4S	A4S	A4S	A4S	A4S	
C3S WF1		0.4028	0.4871	0.6490	0.3457														C3S WF1
C3S WF2	?(>)			0.0011	0.0002														C3S WF2
C3S WF3	?(<)			0.2472		0.7405													C3S WF3
C3S FD5	?(<)	<	?(>)		0.0242	0.3070													C3S FD5
C3S FD6	?(<)	<		<		0.0091													C3S FD6
C3S FD7			?(>)	?(<)	>														C3S FD7
A1S WF1								id	id	id	id								A1S WF1
A1S WF2							id			id	id								A1S WF2
A1S WF3							id			id		id							A1S WF3
A1S FD5							id	id	id		id	id							A1S FD5
A1S FD6							id	id		id		id							A1S FD6
A1S FD7									id	id	id								A1S FD7
A4S WF1														0.0135	0.1696	0.4310	0.0036		A4S WF1
A4S WF2													>			0.2765	0.0000		A4S WF2
A4S WF3													?(<)			0.5345		0.0839	A4S WF3
A4S FD5													?(<)	?(<)	?(<)		0.9526	0.9264	A4S FD5
A4S FD6													<	<		?(>)		0.8767	A4S FD6
A4S FD7															<	?(>)	?(>)		A4S FD7
Case	C3S WF1	C3S WF2	C3S WF3	C3S FD5	C3S FD6	C3S FD7	A1S WF1	A1S WF2	A1S WF3	A1S FD5	A1S FD6	A1S FD7	A4S WF1	A4S WF2	A4S WF3	A4S FD5	A4S FD6	A4S FD7	Case

Table E69. Results of Hypothesis Test 2 for MD STFI, comparing furnishes continued.

Case	A5S WF1	A5S WF2	A5S WF3	A5S FD5	A5S FD6	A5S FD7	C1 WF1	C1 WF2	C1 WF3	C1 FD5	C1 FD6	C1 FD7	C2 WF1	C2 WF2	C2 WF3	C2 FD5	C2 FD6	C2 FD7	Case
A5S WF1		id	id	id	id														A5S WF1
A5S WF2	id			0.0022	0.0004														A5S WF2
A5S WF3	id			id		id													A5S WF3
A5S FD5	id	<	id		0.9768	0.6182													A5S FD5
A5S FD6	id	<		?(>)		0.5350													A5S FD6
A5S FD7			id	?(>)	?(>)														A5S FD7
C1 WF1								0.2490	0.0157	id	0.0022								C1 WF1
C1 WF2							?(>)			id	0.0043								C1 WF2
C1 WF3							<			id		0.0296							C1 WF3
C1 FD5							id	id	id		id	id							C1 FD5
C1 FD6							<	<		id		0.6951							C1 FD6
C1 FD7									<	id	?(<)								C1 FD7
C2 WF1														0.6501	0.0513	0.0159	0.0361		C2 WF1
C2 WF2													?(>)			0.0227	0.0014		C2 WF2
C2 WF3													<			0.1806		0.0042	C2 WF3
C2 FD5													<	<	?(<)		0.3121	0.7690	C2 FD5
C2 FD6													<	<		?(>)		0.0649	C2 FD6
C2 FD7															<	?(<)	<		C2 FD7
Case	A5S WF1 C3	A5S WF2 C3	A5S WF3 C3	A5S FD5 C3	A5S FD6 C3	A5S FD7 C3	C1 WF1 A1	C1 WF2 A1	C1 WF3 A1	C1 FD5 A1	C1 FD6 A1	C1 FD7 A1	C2 WF1 A2	C2 WF2 A2	C2 WF3 A2	C2 FD5 A2	C2 FD6 A2	C2 FD7 A2	Case
C3 WF1		0.2547	0.3037	0.8257	0.6155														C3 WF1
C3 WF2	?(>)			0.0217	0.0001														C3 WF2
C3 WF3	?(>)			0.0744		0.0097													C3 WF3
C3 FD5	?(>)	<	<		0.0894	0.2154													C3 FD5
C3 FD6	?(<)	<		<		0.3090													C3 FD6
C3 FD7			<	?(<)	?(>)														C3 FD7
A1 WF1								0.3289	0.0172	0.4015	0.0101								A1 WF1
A1 WF2							?(<)			0.4588	0.0251								A1 WF2
A1 WF3							<			0.6606		0.3398							A1 WF3
A1 FD5							?(<)	?(<)	?(<)		0.8806	0.7349							A1 FD5
A1 FD6							<	<		?(>)		0.4133							A1 FD6
A1 FD7									?(<)	?(>)	?(>)								A1 FD7
A2 WF1														0.0671	0.5198	id	0.3236		A2 WF1
A2 WF2													>			id	0.0067		A2 WF2
A2 WF3													?(<)			id		id	A2 WF3
A2 FD5													id	id	id		id	id	A2 FD5
A2 FD6													?(<)	<		id		id	A2 FD6
A2 FD7															id	id	id		A2 FD7
Case	C3 WF1	C3 WF2	C3 WF3	C3 FD5	C3 FD6	C3 FD7	A1 WF1	A1 WF2	A1 WF3	A1 FD5	A1 FD6	A1 FD7	A2 WF1	A2 WF2	A2 WF3	A2 FD5	A2 FD6	A2 FD7	Case

Table E70. Results of Hypothesis Test 2 for MD STFI, comparing furnishes continued.

Case	A4 WF1	A4 WF2	A4 WF3	A4 FD5	A4 FD6	A4 FD7	A5 WF1	A5 WF2	A5 WF3	A5 FD5	A5 FD6	A5 FD7	A6 WF1	A6 WF2	A6 WF3	A6 FD5	A6 FD6	A6 FD7	Case
A4 WF1		0.8468	0.1636	0.1239	0.0094														A4 WF1
A4 WF2	?(<)			0.1482	0.0045														A4 WF2
A4 WF3	?(<)			0.3958		0.3221													A4 WF3
A4 FD5	?(<)	?(<)	?(<)		0.5473	0.8297													A4 FD5
A4 FD6	<	<		?(<)		0.2358													A4 FD6
A4 FD7			?(<)	?(>)	?(>)														A4 FD7
A5 WF1								0.1298	0.1757	0.0019	0.0097								A5 WF1
A5 WF2							?(<)			0.0009	0.0363								A5 WF2
A5 WF3							?(<)			0.0114		0.1732							A5 WF3
A5 FD5							<	<	<		0.0776	0.0676							A5 FD5
A5 FD6							<	<		>		0.6847							A5 FD6
A5 FD7									?(<)	>	?(>)								A5 FD7
A6 WF1														0.6684	0.0538	id	0.0187		A6 WF1
A6 WF2													?(<)			id	0.0637		A6 WF2
A6 WF3													<			id		0.2836	A6 WF3
A6 FD5													id	id	id		id	id	A6 FD5
A6 FD6													<	<		id		0.9182	A6 FD6
A6 FD7															?(<)	id	?(>)		A6 FD7
Case	A4 WF1 A5F	A4 WF2 A5F	A4 WF3 A5F	A4 FD5 A5F	A4 FD6 A5F	A4 FD7 A5F	A5 WF1 A4H	A5 WF2 A4H	A5 WF3 A4H	A5 FD5 A4H	A5 FD6 A4H	A5 FD7 A4H	A6 WF1 A5H	A6 WF2 A5H	A6 WF3 A5H	A6 FD5 A5H	A6 FD6 A5H	A6 FD7 A5H	Case
A5F WF1		id	id	id	0.0085														A5F WF1
A5F WF2	id			id	id														A5F WF2
A5F WF3	id			id		id													A5F WF3
A5F FD5	id	id	id		id	id													A5F FD5
A5F FD6	<	id		id		id													A5F FD6
A5F FD7			id	id	id														A5F FD7
A4H WF1								0.9866	id	id	0.9188								A4H WF1
A4H WF2							?(>)			id	0.9213								A4H WF2
A4H WF3							id			id		id							A4H WF3
A4H FD5							id	id	id		id	id							A4H FD5
A4H FD6							?(<)	?(<)		id		0.0967							A4H FD6
A4H FD7									id	id	<								A4H FD7
A5H WF1														id	id	id	0.0031		A5H WF1
A5H WF2													id			id	id		A5H WF2
A5H WF3													id			id		id	A5H WF3
A5H FD5													id	id	id		id	id	A5H FD5
A5H FD6													<	id		id		id	A5H FD6
A5H FD7															id	id	id		A5H FD7
Case	A5F WF1	A5F WF2	A5F WF3	A5F FD5	A5F FD6	A5F FD7	A4H WF1	A4H WF2	A4H WF3	A4H FD5	A4H FD6	A4H FD7	A5H WF1	A5H WF2	A5H WF3	A5H FD5	A5H FD6	A5H FD7	Case

Table E71. Results of Hypothesis Test 3 for MD STFI and furnish WF1.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		0.0022	0.1608	0.0025	0.0108	0.0007	0.0014	0.0718	0.0001	0.1797	0.2484	0.0052	id	0.0004	0.0130	0.0161	0.0011	0.0005	0.0008	0.0001	0.0004	id	0.0009	0.0021	0.0001	Con
D1	>		0.6682	0.1897	0.5344			0.7463			0.3571			0.1049			0.0363									D1
D2	?(>)	?(>)				0.6022			0.6086						0.6665			0.8994								D2
D3	>	?(>)					0.5394			0.8670						0.1926										D3
D4	>	?(>)				0.3086	0.8344					0.1156							0.5469			id		0.4343		D4
D5	>		?(>)		?(>)								id							0.1380			0.4344		0.4521	D5
D6	>			?(<)	?(<)																0.1650					D6
C1S	>	?(>)							0.4767	0.9763	0.2693			0.7377												C1S
C2S	>		?(>)					?(>)							0.4742											C2S
C3S	?(>)			?(<)				?(<)								0.6018										C3S
A1S	?(>)	?(<)						?(<)				0.7226					0.1982									A1S
A4S	>				?(<)						?(>)		id						0.0042							A4S
A5S	id					id						id								id						A5S
C1	>	?(>)						?(>)							0.2271	0.1320	0.2918									C1
C2	>		?(>)						?(<)					?(>)				0.1803								C2
C3	>			?(<)						?(<)				?(<)												C3
A1	>	>									?(>)			?(>)				0.2541	0.4864							A1
A2	>		?(>)												?(<)		?(<)			0.0068						A2
A4	>				?(>)							>					?(<)			0.0342	0.9573	id		0.7503		A4
A5	>					?(>)							id					>	>				0.0379		0.1991	A5
A6	>						?(>)												?(<)							A6
A4F	id				id														id				id			A4F
A5F	>					?(<)														<		id				A5F
A4H	>				?(>)														?(>)						0.0980	A4H
A5H	>					?(>)														?(<)				>		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E72. Results of Hypothesis Test 3 for MD STFI and furnish WF2.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		0.0016	0.0002	0.0001	0.0001	0.0000	0.0000	0.0002	0.0001	0.0001	id	0.0023	0.0069	0.0002	0.0002	0.0001	0.0001	0.0002	0.0002	0.0001	0.0006	id	0.0003	0.0001	0.1094	Con
D1	>		0.8000	0.9464	0.5236			0.9108			id			0.7960			0.5907									D1
D2	>	?(>)				0.0608			0.4414						0.1553			0.9916								D2
D3	>	?(>)					0.5897			0.5339						0.0337										D3
D4	>	?(<)				0.0166	0.1524					0.0055							0.7903			id		0.8103		D4
D5	>		>		>								0.0072							0.1402			0.0059		0.7203	D5
D6	>			?(>)	?(>)																0.0315					D6
C1S	>	?(<)							0.4024	0.5050	id			0.8692												C1S
C2S	>		?(>)					?(>)							0.5536											C2S
C3S	>			?(>)				?(>)								0.0350										C3S
A1S	id	id						id				id					id									A1S
A4S	>				<						id		0.9510						0.0044							A4S
A5S	>					<						?(>)								0.0196						A5S
C1	>	?(<)						?(<)							0.1844	0.1934	0.7543									C1
C2	>		?(>)						?(>)					?(>)				0.1146								C2
C3	>			<						<				?(<)												C3
A1	>	?(<)									id			?(<)				0.1182	0.5683							A1
A2	>		?(>)												?(<)		?(>)			0.8444						A2
A4	>				?(<)							>					?(<)			0.2102	0.2295	id		0.9916		A4
A5	>					?(<)							>					?(<)	?(>)				0.0587		0.7780	A5
A6	>						<												?(<)							A6
A4F	id				id														id				id			A4F
A5F	>					<														<		id				A5F
A4H	>				?(<)														?(>)						0.4756	A4H
A5H	?(>)					?(<)														?(>)				?(>)		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E73. Results of Hypothesis Test 3 for MD STFI and furnish WF3.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		0.0136	0.0007	0.0191	0.0016	0.0005	0.0007	0.1004	0.0002	0.0011	id	0.0093	id	0.0009	0.0005	0.0002	0.0007	0.0039	0.0002	0.0014	0.0006	id	0.0100	0.0004	0.0004	Con
D1	>		0.5177	0.9537	0.5960			0.7301			id			0.6920			0.6244									D1
D2	>	?(>)				0.1605			0.1583						0.3141			0.2696								D2
D3	>	?(>)					0.6077			0.7980						0.4245										D3
D4	>	?(<)				0.0699	0.1622					0.2497							0.0544			id		0.2085		D4
D5	>		?(>)		>								id							0.2647			0.6587		0.3489	D5
D6	>			?(>)	?(>)																0.3903					D6
C1S	?(>)	?(>)							0.4420	0.5985	id			0.9759												C1S
C2S	>		?(>)					?(>)							0.3159											C2S
C3S	>			?(<)				?(<)								0.0349										C3S
A1S	id	id						id				id					id									A1S
A4S	>				?(<)						id		id						0.0041							A4S
A5S	id					id						id								id						A5S
C1	>	?(>)						?(<)							0.0975	0.2262	0.7454									C1
C2	>		?(>)						?(<)					>				0.0217								C2
C3	>			?(>)						>				?(>)												C3
A1	>	?(>)									id			?(>)				0.5011	0.1930							A1
A2	>		?(<)												<		?(<)			0.0888						A2
A4	>				>							>					?(>)			0.2231	0.9293	id		0.3729		A4
A5	>					?(>)							id					>	?(>)				0.2096		0.3679	A5
A6	>						?(>)												?(<)							A6
A4F	id				id														id				id			A4F
A5F	>					?(<)														?(<)		id				A5F
A4H	>				?(>)														?(<)						0.2064	A4H
A5H	>					?(>)														?(<)				?(>)		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E74. Results of Hypothesis Test 3 for MD STFI and furnish FD5.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		0.2017	0.0072	0.0103	0.1167	0.0150	0.0598	0.0378	0.0183	0.0146	id	0.7753	0.2823	id	0.0366	0.0218	0.2148	0.0241	0.1376	id	0.1913	id	id	id	id	Con
D1	?(>)		0.0428	0.0819	0.7999			0.3168			id			id			0.6277									D1
D2	>	>				0.1112			0.2528						0.0192			0.2335								D2
D3	>	>					0.5057			0.6063						0.2977										D3
D4	?(>)	?(>)				0.1955	0.4125					0.4704							0.6856			id		id		D4
D5	>		?(<)		?(>)								0.0100							id			id		id	D5
D6	>			?(<)	?(>)																0.8821					D6
C1S	>	?(>)							0.6861	0.5703	id			id												C1S
C2S	>		?(<)					?(>)							0.4205											C2S
C3S	>			?(<)				?(>)								0.6097										C3S
A1S	id	id						id				id					id									A1S
A4S	?(<)				?(<)						id		0.9016						0.4370							A4S
A5S	?(<)					<						?(<)								id						A5S
C1	id	id						id							id	id	id									C1
C2	>		<						?(<)					id				0.5273								C2
C3	>			?(<)						?(<)				id												C3
A1	?(>)	?(>)									id			id				0.6339	0.9798							A1
A2	>		?(<)												?(>)		?(>)			id						A2
A4	?(>)				?(>)							?(>)					?(>)			id	0.8903	id		id		A4
A5	id					id							id					id	id				id		id	A5
A6	?(>)						?(<)												?(>)							A6
A4F	id				id														id				id			A4F
A5F	id					id														id		id				A5F
A4H	id				id														id						id	A4H
A5H	id					id														id				id		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E75. Results of Hypothesis Test 3 for MD STFI and furnish FD6.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		0.0038	0.0104	0.0135	0.0108	0.0029	0.0104	0.0055	0.0007	0.0009	id	0.0322	0.3696	0.0006	0.0002	0.0038	0.0004	0.0001	0.0024	0.0010	0.0004	id	0.0005	0.0004	0.0001	Con
D1	>		0.6440	0.2742	0.8314			0.7861			id			0.0354			0.0266									D1
D2	>	?(>)				0.7326			0.1200						0.0707			0.0677								D2
D3	>	?(>)					0.5213			0.9909						0.6361										D3
D4	>	?(>)				0.9142	0.7852					0.0953							0.2356			id		0.0485		D4
D5	>		?(<)		?(<)								0.0591							0.0335			0.1016		0.0039	D5
D6	>			?(<)	?(>)																0.1081					D6
C1S	>	?(>)							0.0580	0.1814	id			0.2517												C1S
C2S	>		?(>)					>							0.3909											C2S
C3S	>			?(>)				?(>)								0.0527										C3S
A1S	id	id						id				id					id									A1S
A4S	>				<						id		0.4754						0.0106							A4S
A5S	?(>)					<						?(<)								0.0045						A5S
C1	>	>						?(>)							0.0179	0.4817	0.1687									C1
C2	>		>						?(>)					>				0.9042								C2
C3	>			?(<)						<				?(<)												C3
A1	>	>									id			?(>)				0.5948	0.4807							A1
A2	>		>												?(>)		?(>)			0.9777						A2
A4	>				?(>)							>					?(<)			0.3235	0.2832	id		0.2926		A4
A5	>					>							>					?(<)	?(>)				0.1403		0.5738	A5
A6	>						?(>)												?(>)							A6
A4F	id				id														id				id			A4F
A5F	>					?(>)														?(<)		id				A5F
A4H	>				>														?(>)						0.5932	A4H
A5H	>					>														?(>)				?(>)		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E76. Results of Hypothesis Test 3 for MD STFI and furnish FD7.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		id	0.0034	0.0002	0.0024	0.0001	id	0.0002	0.0008	0.0000	id	0.4728	0.3373	0.0001	0.0001	0.0001	0.0001	0.0000	0.0021	0.0142	0.0000	id	0.0050	0.0001	0.0000	Con
D1	id		id	id	id			id			id			id			id									D1
D2	>	id				0.7636			0.4111						0.7040			0.0183								D2
D3	>	id					id			0.4966						0.1883										D3
D4	>	id				0.2151	id					0.0134							0.7961			id		0.1349		D4
D5	>		?(<)		?(<)								err							0.1624			0.9575		0.0096	D5
D6	id			id	id																id					D6
C1S	>	id							0.8082	0.9356	id			0.0610												C1S
C2S	>		?(>)					?(<)							0.1618											C2S
C3S	>			?(>)				?(>)								0.0306										C3S
A1S	id	id						id				id					id									A1S
A4S	?(>)				<						id		0.7628						0.0143							A4S
A5S	?(>)					<						?(<)								0.0170						A5S
C1	>	id						<							0.6491	0.6367	0.0208									C1
C2	>		?(<)						?(<)					?(>)				0.0007								C2
C3	>			?(<)						<				?(>)												C3
A1	>	id									id			>				0.0051	0.8822							A1
A2	>		>												>		>			0.6429						A2
A4	>				?(<)							>					?(<)			0.3448	0.6595	id		0.1707		A4
A5	>					?(>)							>					?(<)	?(>)				0.1507		0.5470	A5
A6	>						id												?(>)							A6
A4F	id				id														id				id			A4F
A5F	>					?(<)														?(<)		id				A5F
A4H	>				?(<)														?(<)						0.0033	A4H
A5H	>					>														?(<)				>		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E77. Results of Hypothesis Test 3 for MD STFI comparing furnishes.

Case	Con WF1	Con WF2	Con WF3	Con FD5	Con FD6	Con FD7	D1 WF1	D1 WF2	D1 WF3	D1 FD5	D1 FD6	D1 FD7	D2 WF1	D2 WF2	D2 WF3	D2 FD5	D2 FD6	D2 FD7	Case
Con WF1		0.0023	0.1032	0.1402	0.2218														Con WF1
Con WF2	>			0.0921	0.0003														Con WF2
Con WF3	?(<)			0.0389		0.0476													Con WF3
Con FD5	?(>)	<	>		0.0684	0.2301													Con FD5
Con FD6	?(<)	<		<		0.0909													Con FD6
Con FD7			>	?(<)	>														Con FD7
D1 WF1								0.0156	0.4038	0.0729	0.0044								D1 WF1
D1 WF2							>			0.0037	0.0015								D1 WF2
D1 WF3							?(<)			0.4093		id							D1 WF3
D1 FD5							<	<	?(<)		0.2674	id							D1 FD5
D1 FD6							<	<		?(<)		id							D1 FD6
D1 FD7									id	id	id								D1 FD7
D2 WF1														0.4655	0.5770	0.7432	0.2612		D2 WF1
D2 WF2													?(>)			0.0004	0.0027		D2 WF2
D2 WF3													?(<)			0.1502		0.0443	D2 WF3
D2 FD5													?(<)	<	?(>)		0.0079	0.0114	D2 FD5
D2 FD6													?(<)	<		<		0.1648	D2 FD6
D2 FD7															<	<	?(>)		D2 FD7

Case	Con WF1 D3	Con WF2 D3	Con WF3 D3	Con FD5 D3	Con FD6 D3	Con FD7 D3	D1 WF1 D4	D1 WF2 D4	D1 WF3 D4	D1 FD5 D4	D1 FD6 D4	D1 FD7 D4	D2 WF1 D5	D2 WF2 D5	D2 WF3 D5	D2 FD5 D5	D2 FD6 D5	D2 FD7 D5	Case
D3 WF1		0.0171	0.2300	0.1296	0.0179														D3 WF1
D3 WF2	>			0.0064	0.0082														D3 WF2
D3 WF3	?(<)			0.4135		0.6393													D3 WF3
D3 FD5	?(<)	<	?(>)		0.0681	0.0909													D3 FD5
D3 FD6	<	<		<		0.3501													D3 FD6
D3 FD7			?(<)	<	?(>)														D3 FD7
D4 WF1								0.2945	0.1020	0.0833	0.0216								D4 WF1
D4 WF2							?(>)			0.0205	0.0010								D4 WF2
D4 WF3							?(<)			0.7516		0.4684							D4 WF3
D4 FD5							<	<	?(<)		0.2061	0.3533							D4 FD5
D4 FD6							<	<		?(<)		0.0363							D4 FD6
D4 FD7									?(>)	?(>)	>								D4 FD7
D5 WF1														0.0976	0.0205	0.0049	0.0001		D5 WF1
D5 WF2													>			0.0003	0.0000		D5 WF2
D5 WF3													<			0.1318		0.0006	D5 WF3
D5 FD5													<	<	?(<)		0.0035	0.0377	D5 FD5
D5 FD6													<	<		<		0.0307	D5 FD6
D5 FD7															<	<	>		D5 FD7
Case	D3 WF1	D3 WF2	D3 WF3	D3 FD5	D3 FD6	D3 FD7	D4 WF1	D4 WF2	D4 WF3	D4 FD5	D4 FD6	D4 FD7	D5 WF1	D5 WF2	D5 WF3	D5 FD5	D5 FD6	D5 FD7	Case

Table E78. Results of Hypothesis Test 3 for MD STFI comparing furnishes continued.

Case	D6 WF1	D6 WF2	D6 WF3	D6 FD5	D6 FD6	D6 FD7	C1S WF1	C1S WF2	C1S WF3	C1S FD5	C1S FD6	C1S FD7	C2S WF1	C2S WF2	C2S WF3	C2S FD5	C2S FD6	C2S FD7	Case
D6 WF1		0.0157	0.2083	0.2405	0.0052														D6 WF1
D6 WF2	>			0.0331	0.0010														D6 WF2
D6 WF3	?(<)			0.7115		id													D6 WF3
D6 FD5	?(<)	<	?(<)		0.1428	id													D6 FD5
D6 FD6	<	<		?(<)		id													D6 FD6
D6 FD7			id	id	id														D6 FD7
C1S WF1								0.3860	0.5600	0.4257	0.1586								C1S WF1
C1S WF2							?(>)			0.0072	0.0002								C1S WF2
C1S WF3							?(<)			0.7101		0.6461							C1S WF3
C1S FD5							?(<)	<	?(<)		0.0490	0.8903							C1S FD5
C1S FD6							?(<)	<		<		0.0217							C1S FD6
C1S FD7									?(<)	?(<)	>								C1S FD7
C2S WF1														0.0280	0.0382	0.0144	0.0012		C2S WF1
C2S WF2													>			0.0052	0.0037		C2S WF2
C2S WF3													<			0.1757		0.0256	C2S WF3
C2S FD5													<	<	?(<)		0.1770	0.4191	C2S FD5
C2S FD6													<	<		?(<)		0.3600	C2S FD6
C2S FD7															<	?(<)	?(>)		C2S FD7

Case	D6 WF1	D6 WF2	D6 WF3	D6 FD5	D6 FD6	D6 FD7	C1S WF1	C1S WF2	C1S WF3	C1S FD5	C1S FD6	C1S FD7	C2S WF1	C2S WF2	C2S WF3	C2S FD5	C2S FD6	C2S FD7	Case
	C3S	C3S	C3S	C3S	C3S	C3S	A1S	A1S	A1S	A1S	A1S	A1S	A4S	A4S	A4S	A4S	A4S	A4S	
C3S WF1		0.4028	0.4871	0.6490	0.3457														C3S WF1
C3S WF2	?(>)			0.0011	0.0002														C3S WF2
C3S WF3	?(<)			0.2472		0.7405													C3S WF3
C3S FD5	?(<)	<	?(>)		0.0242	0.3070													C3S FD5
C3S FD6	?(<)	<		<		0.0091													C3S FD6
C3S FD7			?(>)	?(<)	>														C3S FD7
A1S WF1								id	id	id	id								A1S WF1
A1S WF2							id			id	id								A1S WF2
A1S WF3							id			id		id							A1S WF3
A1S FD5							id	id	id		id	id							A1S FD5
A1S FD6							id	id		id		id							A1S FD6
A1S FD7									id	id	id								A1S FD7
A4S WF1														0.0135	0.1696	0.4310	0.0036		A4S WF1
A4S WF2													>			0.2765	0.0000		A4S WF2
A4S WF3													?(<)			0.5345		0.0839	A4S WF3
A4S FD5													?(<)	?(<)	?(<)		0.9526	0.9264	A4S FD5
A4S FD6													<	<		?(>)		0.8767	A4S FD6
A4S FD7															<	?(>)	?(>)		A4S FD7
Case	C3S WF1	C3S WF2	C3S WF3	C3S FD5	C3S FD6	C3S FD7	A1S WF1	A1S WF2	A1S WF3	A1S FD5	A1S FD6	A1S FD7	A4S WF1	A4S WF2	A4S WF3	A4S FD5	A4S FD6	A4S FD7	Case

Table E79. Results of Hypothesis Test 3 for MD STFI comparing furnishes continued.

Case	A5S WF1	A5S WF2	A5S WF3	A5S FD5	A5S FD6	A5S FD7	C1 WF1	C1 WF2	C1 WF3	C1 FD5	C1 FD6	C1 FD7	C2 WF1	C2 WF2	C2 WF3	C2 FD5	C2 FD6	C2 FD7	Case
A5S WF1		id	id	id	id														A5S WF1
A5S WF2	id			0.0022	0.0004														A5S WF2
A5S WF3	id			id		id													A5S WF3
A5S FD5	id	<	id		0.9768	0.6182													A5S FD5
A5S FD6	id	<		?(>)		0.5350													A5S FD6
A5S FD7			id	?(>)	?(>)														A5S FD7
C1 WF1								0.0866	0.0085	id	0.0004								C1 WF1
C1 WF2							>			id	0.0001								C1 WF2
C1 WF3							<			id		0.0051							C1 WF3
C1 FD5							id	id	id		id	id							C1 FD5
C1 FD6							<	<		id		0.2849							C1 FD6
C1 FD7									<	id	?(>)								C1 FD7
C2 WF1														0.0244	0.0011	0.0026	0.0004		C2 WF1
C2 WF2													>			0.0009	0.0001		C2 WF2
C2 WF3													<			0.0370		0.0005	C2 WF3
C2 FD5													<	<	<		0.7833	0.1307	C2 FD5
C2 FD6													<	<		?(<)		0.1072	C2 FD6
C2 FD7															<	?(<)	?(<)		C2 FD7
Case	A5S WF1 C3	A5S WF2 C3	A5S WF3 C3	A5S FD5 C3	A5S FD6 C3	A5S FD7 C3	C1 WF1 A1	C1 WF2 A1	C1 WF3 A1	C1 FD5 A1	C1 FD6 A1	C1 FD7 A1	C2 WF1 A2	C2 WF2 A2	C2 WF3 A2	C2 FD5 A2	C2 FD6 A2	C2 FD7 A2	Case
C3 WF1		0.0955	0.6067	0.8547	0.1206														C3 WF1
C3 WF2	>			0.0007	0.0001														C3 WF2
C3 WF3	?(>)			0.1349		0.0066													C3 WF3
C3 FD5	?(<)	<	?(<)		0.0090	0.0245													C3 FD5
C3 FD6	?(<)	<		<		0.0377													C3 FD6
C3 FD7			<	<	>														C3 FD7
A1 WF1								0.8261	0.0132	0.0982	0.0024								A1 WF1
A1 WF2							?(>)			0.1791	0.0015								A1 WF2
A1 WF3							<			0.5465		0.0297							A1 WF3
A1 FD5							<	?(<)	?(<)		0.8977	0.8798							A1 FD5
A1 FD6							<	<		?(<)		0.4662							A1 FD6
A1 FD7									<	?(>)	?(>)								A1 FD7
A2 WF1														0.0315	0.0172	0.0520	0.0031		A2 WF1
A2 WF2													>			0.0142	0.0002		A2 WF2
A2 WF3													<			0.9083		0.0378	A2 WF3
A2 FD5													<	<	?(<)		0.4695	0.2581	A2 FD5
A2 FD6													<	<		?(<)		0.0059	A2 FD6
A2 FD7															>	?(>)	>		A2 FD7
Case	C3 WF1	C3 WF2	C3 WF3	C3 FD5	C3 FD6	C3 FD7	A1 WF1	A1 WF2	A1 WF3	A1 FD5	A1 FD6	A1 FD7	A2 WF1	A2 WF2	A2 WF3	A2 FD5	A2 FD6	A2 FD7	Case

Table E80. Results of Hypothesis Test 3 for MD STFI comparing furnishes continued.

Case	A4 WF1	A4 WF2	A4 WF3	A4 FD5	A4 FD6	A4 FD7	A5 WF1	A5 WF2	A5 WF3	A5 FD5	A5 FD6	A5 FD7	A6 WF1	A6 WF2	A6 WF3	A6 FD5	A6 FD6	A6 FD7	Case
A4 WF1		0.3911	0.0486	0.0705	0.0021														A4 WF1
A4 WF2	?(>)			0.0543	0.0019														A4 WF2
A4 WF3	<			0.2880		0.0532													A4 WF3
A4 FD5	<	<	?(<)		0.5727	0.9478													A4 FD5
A4 FD6	<	<		?(<)		0.2798													A4 FD6
A4 FD7			<	?(>)	?(>)														A4 FD7
A5 WF1								0.2693	0.0371	id	0.0007								A5 WF1
A5 WF2							?(<)			id	0.0014								A5 WF2
A5 WF3							<			id		0.2638							A5 WF3
A5 FD5							id	id	id		id	id							A5 FD5
A5 FD6							<	<		id		0.3485							A5 FD6
A5 FD7									?(<)	id	?(>)								A5 FD7
A6 WF1														0.9085	0.0184	0.2602	0.0018		A6 WF1
A6 WF2													?(<)			0.2665	0.0021		A6 WF2
A6 WF3													<			0.4778		0.0254	A6 WF3
A6 FD5													?(<)	?(<)	?(<)		0.8311	0.9431	A6 FD5
A6 FD6													<	<		?(<)		0.2579	A6 FD6
A6 FD7															<	?(>)	?(>)		A6 FD7
Case	A4 WF1 A5F	A4 WF2 A5F	A4 WF3 A5F	A4 FD5 A5F	A4 FD6 A5F	A4 FD7 A5F	A5 WF1 A4H	A5 WF2 A4H	A5 WF3 A4H	A5 FD5 A4H	A5 FD6 A4H	A5 FD7 A4H	A6 WF1 A5H	A6 WF2 A5H	A6 WF3 A5H	A6 FD5 A5H	A6 FD6 A5H	A6 FD7 A5H	Case
A5F WF1		0.9577	0.0960	id	0.0019														A5F WF1
A5F WF2	?(>)			id	0.0001														A5F WF2
A5F WF3	<			id		0.0809													A5F WF3
A5F FD5	id	id	id		id	id													A5F FD5
A5F FD6	<	<		id		0.4738													A5F FD6
A5F FD7			<	id	?(>)														A5F FD7
A4H WF1								0.4859	0.0251	id	0.0037								A4H WF1
A4H WF2							?(>)			id	0.0020								A4H WF2
A4H WF3							<			id		0.0636							A4H WF3
A4H FD5							id	id	id		id	id							A4H FD5
A4H FD6							<	<		id		0.1920							A4H FD6
A4H FD7									<	id	?(<)								A4H FD7
A5H WF1														0.7519	0.0014	id	0.0001		A5H WF1
A5H WF2													?(>)			id	0.1349		A5H WF2
A5H WF3													<			id		0.0025	A5H WF3
A5H FD5													id	id	id		id	id	A5H FD5
A5H FD6													<	?(<)		id		0.8415	A5H FD6
A5H FD7															<	id	?(>)		A5H FD7
Case	A5F WF1	A5F WF2	A5F WF3	A5F FD5	A5F FD6	A5F FD7	A4H WF1	A4H WF2	A4H WF3	A4H FD5	A4H FD6	A4H FD7	A5H WF1	A5H WF2	A5H WF3	A5H FD5	A5H FD6	A5H FD7	Case

Table E81, Results of Hypothesis Test 0 for CD STFI and furnish WF1.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con																										Con
D1	>																									D1
D2	?	?																								D2
D3	>	?																								D3
D4	>	?																								D4
D5	>		?		?																					D5
D6	>			?	?																					D6
C1S	?	?																								C1S
C2S	>		?					?																		C2S
C3S	>			?				?																		C3S
A1S	?	?						?																		A1S
A4S	>				?						. ?															A4S
A5S	id					id						id														A5S
C1	>	?						?																		C1
C2	>		?						?					?												C2
C3	>			?						?				?												C3
A1	>	>									?			?												A1
A2	>		?												?		?									A2
A4	>				?							?					?									A4
A5	>					?							id					?	?							A5
A6	>						?												?							A6
A4F	id				id														id							A4F
A5F	>					?														?		id				A5F
A4H	?				?														?							A4H
A5H	>					?														?				?		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E82. Results of Hypothesis Test 0 for CD STFI and furnish WF2.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con																										Con
D1	?																									D1
D2	>	?																								D2
D3	>	?																								D3
D4	>	?																								D4
D5	>		?		?																					D5
D6	>			?	?																					D6
C1S	>	?																								C1S
C2S	>		?					?																		C2S
C3S	>			?				?																		C3S
A1S	id	id						id																		A1S
A4S	>				?						id															A4S
A5S	>					?						?														A5S
C1	>	?						?																		C1
C2	>		?						?					?												C2
C3	>			?						?				?												C3
A1	>	?									id			?												A1
A2	>		?												?		?									A2
A4	>				?							>					?									A4
A5	>					?							?					?	?							A5
A6	>						?												?							A6
A4F	id				id														id							A4F
A5F	>					?														?		id				A5F
A4H	?				?														?							A4H
A5H	?					?														?				?		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E83. Results of Hypothesis Test 0 for CD STFI and furnish WF3.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con																										Con
D1	>																									D1
D2	>	?																								D2
D3	>	?																								D3
D4	>	?																								D4
D5	>		?		?																					D5
D6	>			?	?																					D6
C1S	?	?																								C1S
C2S	>		?					?																		C2S
C3S	>			?				?																		C3S
A1S	id	id						id																		A1S
A4S	>				?						id															A4S
A5S	?					?						?														A5S
C1	>	?						?																		C1
C2	>		?						?					?												C2
C3	>			?						?				?												C3
A1	>	?									id			?												A1
A2	>		?												?		?									A2
A4	>				?							?					?									A4
A5	>					?							?					?	?							A5
A6	>						?												?							A6
A4F	id				id														id							A4F
A5F	>					?														?		id				A5F
A4H	>				?														?							A4H
A5H	>					?														?				?		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E84. Results of Hypothesis Test 0 for CD STFI and furnish FD5.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con																										Con
D1	?																									D1
D2	?	?																								D2
D3	?	?																								D3
D4	?	?																								D4
D5	?		?		?																					D5
D6	?			?	?																					D6
C1S	?	?																								C1S
C2S	?		?					?																		C2S
C3S	?			?				?																		C3S
A1S	id	id						id																		A1S
A4S	?				?						id															A4S
A5S	?					?						?														A5S
C1	?	?						?																		C1
C2	?		?						?					?												C2
C3	?			?						?				?												C3
A1	?	?									id			?												A1
A2	?		?												?		?									A2
A4	?				?							?					?									A4
A5	?					?							?					?	?							A5
A6	?						?												?							A6
A4F	id				id														id							A4F
A5F	id					id														id		id				A5F
A4H	id				id														id							A4H
A5H	id					id														id				id		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E85. Results of Hypothesis Test 0 for CD STFI and furnish FD6.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
0Con																										Con
D1	>																									D1
D2	>	?																								D2
D3	>	?																								D3
D4	>	?																								D4
D5	>		?		?																					D5
D6	>			?	?																					D6
C1S	?	?																								C1S
C2S	>		>					?																		C2S
C3S	>			?				?																		C3S
A1S	id	id						id																		A1S
A4S	?				?						id															A4S
A5S	?					?						?														A5S
C1	>	?						?																		C1
C2	>		?						<					?												C2
C3	>			?						>				?												C3
A1	>	?									id			?												A1
A2	?		?												?		?									A2
A4	>				?							?					?									A4
A5	>					?							>					?	?							A5
A6	?						?												?							A6
A4F	id				id														id							A4F
A5F	>					?														?		id				A5F
A4H	>				?														?							A4H
A5H	>					?														?				?		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E86. Results of Hypothesis Test 0 for CD STFI and furnish FD7.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con																										Con
D1	?																									D1
D2	>	?																								D2
D3	>	?																								D3
D4	>	?																								D4
D5	>		?		?																					D5
D6	?			?	?																					D6
C1S	>	?																								C1S
C2S	?		?					?																		C2S
C3S	>			?				?																		C3S
A1S	id	id						id																		A1S
A4S	>				?						id															A4S
A5S	>					<						?														A5S
C1	>	?						?																		C1
C2	>		?						?					?												C2
C3	>			?						?				?												C3
A1	?	?									id			?												A1
A2	>		?												?		?									A2
A4	>				?							>					?									A4
A5	>					?							>					?	?							A5
A6	>						?												?							A6
A4F	id				id														id							A4F
A5F	>					?														?		id				A5F
A4H	>				?														?							A4H
A5H	>					?														?				?		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E87. Results of Hypothesis Test 0 for CD STFI, comparing furnishes.

Case	Con WF1	Con WF2	Con WF3	Con FD5	Con FD6	Con FD7	D1 WF1	D1 WF2	D1 WF3	D1 FD5	D1 FD6	D1 FD7	D2 WF1	D2 WF2	D2 WF3	D2 FD5	D2 FD6	D2 FD7	Case
Con WF1																			Con WF1
Con WF2	>																		Con WF2
Con WF3	?																		Con WF3
Con FD5	?	?	?																Con FD5
Con FD6	?	<		?															Con FD6
Con FD7			?	?	?														Con FD7
D1 WF1																			D1 WF1
D1 WF2							?												D1 WF2
D1 WF3							>												D1 WF3
D1 FD5							?	?	?										D1 FD5
D1 FD6							?	?		?									D1 FD6
D1 FD7									?	?	?								D1 FD7
D2 WF1																			D2 WF1
D2 WF2													?						D2 WF2
D2 WF3													?						D2 WF3
D2 FD5													?	<	<				D2 FD5
D2 FD6													?	<		?			D2 FD6
D2 FD7															?	>	?		D2 FD7
Case	Con WF1 D3	Con WF2 D3	Con WF3 D3	Con FD5 D3	Con FD6 D3	Con FD7 D3	D1 WF1 D4	D1 WF2 D4	D1 WF3 D4	D1 FD5 D4	D1 FD6 D4	D1 FD7 D4	D2 WF1 D5	D2 WF2 D5	D2 WF3 D5	D2 FD5 D5	D2 FD6 D5	D2 FD7 D5	Case
D3 WF1																			D3 WF1
D3 WF2	>																		D3 WF2
D3 WF3	?																		D3 WF3
D3 FD5	?	<	?																D3 FD5
D3 FD6	?	<		?															D3 FD6
D3 FD7			?	?	?														D3 FD7
D4 WF1																			D4 WF1
D4 WF2							?												D4 WF2
D4 WF3							?												D4 WF3
D4 FD5							<	<	<										D4 FD5
D4 FD6							?	?		?									D4 FD6
D4 FD7									?	>	?								D4 FD7
D5 WF1																			D5 WF1
D5 WF2													?						D5 WF2
D5 WF3													?						D5 WF3
D5 FD5													<	<	<				D5 FD5
D5 FD6													<	<		>			D5 FD6
D5 FD7															<	>	?		D5 FD7
Case	D3 WF1	D3 WF2	D3 WF3	D3 FD5	D3 FD6	D3 FD7	D4 WF1	D4 WF2	D4 WF3	D4 FD5	D4 FD6	D4 FD7	D5 WF1	D5 WF2	D5 WF3	D5 FD5	D5 FD6	D5 FD7	Case

Table E88. Results of Hypothesis Test 0 for CD STFI, comparing furnishes continued.

Case	D6 WF1	D6 WF2	D6 WF3	D6 FD5	D6 FD6	D6 FD7	C1S WF1	C1S WF2	C1S WF3	C1S FD5	C1S FD6	C1S FD7	C2S WF1	C2S WF2	C2S WF3	C2S FD5	C2S FD6	C2S FD7	Case
D6 WF1																			D6 WF1
D6 WF2	?																		D6 WF2
D6 WF3	?																		D6 WF3
D6 FD5	?	<	?																D6 FD5
D6 FD6	<	<		?															D6 FD6
D6 FD7			?	?	?														D6 FD7
C1S WF1																			C1S WF1
C1S WF2							?												C1S WF2
C1S WF3							?												C1S WF3
C1S FD5							?	<	?										C1S FD5
C1S FD6							?	<		?									C1S FD6
C1S FD7									?	?	?								C1S FD7
C2S WF1																			C2S WF1
C2S WF2													?						C2S WF2
C2S WF3													?						C2S WF3
C2S FD5													?	<	?				C2S FD5
C2S FD6													<	<		?			C2S FD6
C2S FD7															?	?	?		C2S FD7
Case	D6 WF1 C3S	D6 WF2 C3S	D6 WF3 C3S	D6 FD5 C3S	D6 FD6 C3S	D6 FD7 C3S	C1S WF1 A1S	C1S WF2 A1S	C1S WF3 A1S	C1S FD5 A1S	C1S FD6 A1S	C1S FD7 A1S	C2S WF1 A4S	C2S WF2 A4S	C2S WF3 A4S	C2S FD5 A4S	C2S FD6 A4S	C2S FD7 A4S	Case
C3S WF1																			C3S WF1
C3S WF2	?																		C3S WF2
C3S WF3	?																		C3S WF3
C3S FD5	?	<	<																C3S FD5
C3S FD6	?	<		?															C3S FD6
C3S FD7			?	>	?														C3S FD7
A1S WF1																			A1S WF1
A1S WF2							id												A1S WF2
A1S WF3							id												A1S WF3
A1S FD5							id	id	id										A1S FD5
A1S FD6							id	id		id									A1S FD6
A1S FD7									id	id	id								A1S FD7
A4S WF1																			A4S WF1
A4S WF2													?						A4S WF2
A4S WF3													?						A4S WF3
A4S FD5													?	?	?				A4S FD5
A4S FD6													?	<		?			A4S FD6
A4S FD7															?	?	?		A4S FD7
Case	C3S WF1	C3S WF2	C3S WF3	C3S FD5	C3S FD6	C3S FD7	A1S WF1	A1S WF2	A1S WF3	A1S FD5	A1S FD6	A1S FD7	A4S WF1	A4S WF2	A4S WF3	A4S FD5	A4S FD6	A4S FD7	Case

Table E89. Results of Hypothesis Test 0 for CD STFI, comparing furnishes continued.

Case	A5S WF1	A5S WF2	A5S WF3	A5S FD5	A5S FD6	A5S FD7	C1 WF1	C1 WF2	C1 WF3	C1 FD5	C1 FD6	C1 FD7	C2 WF1	C2 WF2	C2 WF3	C2 FD5	C2 FD6	C2 FD7	Case
A5S WF1																			A5S WF1
A5S WF2	id																		A5S WF2
A5S WF3	id																		A5S WF3
A5S FD5	id	<	?																A5S FD5
A5S FD6	id	<		?															A5S FD6
A5S FD7			?	?	?														A5S FD7
C1 WF1																			C1 WF1
C1 WF2							?												C1 WF2
C1 WF3							?												C1 WF3
C1 FD5							?	<	?										C1 FD5
C1 FD6							?	?		?									C1 FD6
C1 FD7									?	?	?								C1 FD7
C2 WF1																			C2 WF1
C2 WF2													?						C2 WF2
C2 WF3													?						C2 WF3
C2 FD5													?	<	?				C2 FD5
C2 FD6													?	<		?			C2 FD6
C2 FD7															<	?	?		C2 FD7
Case	A5S WF1 C3	A5S WF2 C3	A5S WF3 C3	A5S FD5 C3	A5S FD6 C3	A5S FD7 C3	C1 WF1 A1	C1 WF2 A1	C1 WF3 A1	C1 FD5 A1	C1 FD6 A1	C1 FD7 A1	C2 WF1 A2	C2 WF2 A2	C2 WF3 A2	C2 FD5 A2	C2 FD6 A2	C2 FD7 A2	Case
C3 WF1																			C3 WF1
C3 WF2	?																		C3 WF2
C3 WF3	?																		C3 WF3
C3 FD5	?	<	<																C3 FD5
C3 FD6	?	?		>															C3 FD6
C3 FD7			?	?	?														C3 FD7
A1 WF1																			A1 WF1
A1 WF2							?												A1 WF2
A1 WF3							?												A1 WF3
A1 FD5							?	?	?										A1 FD5
A1 FD6							?	?		?									A1 FD6
A1 FD7									?	?	?								A1 FD7
A2 WF1																			A2 WF1
A2 WF2													?						A2 WF2
A2 WF3													?						A2 WF3
A2 FD5													?	<	?				A2 FD5
A2 FD6													?	?		?			A2 FD6
A2 FD7															?	?	?		A2 FD7
Case	C3 WF1	C3 WF2	C3 WF3	C3 FD5	C3 FD6	C3 FD7	A1 WF1	A1 WF2	A1 WF3	A1 FD5	A1 FD6	A1 FD7	A2 WF1	A2 WF2	A2 WF3	A2 FD5	A2 FD6	A2 FD7	Case

Table E90. Results of Hypothesis Test 0 for CD STFI, comparing furnishes continued.

Case	A4 WF1	A4 WF2	A4 WF3	A4 FD5	A4 FD6	A4 FD7	A5 WF1	A5 WF2	A5 WF3	A5 FD5	A5 FD6	A5 FD7	A6 WF1	A6 WF2	A6 WF3	A6 FD5	A6 FD6	A6 FD7	Case
A4 WF1																			A4 WF1
A4 WF2	?																		A4 WF2
A4 WF3	?																		A4 WF3
A4 FD5	<	<	<																A4 FD5
A4 FD6	?	?		?															A4 FD6
A4 FD7			?	>	?														A4 FD7
A5 WF1																			A5 WF1
A5 WF2							?												A5 WF2
A5 WF3							?												A5 WF3
A5 FD5							<	<	<										A5 FD5
A5 FD6							?	?		>									A5 FD6
A5 FD7									?	>	?								A5 FD7
A6 WF1																			A6 WF1
A6 WF2													?						A6 WF2
A6 WF3													?						A6 WF3
A6 FD5													?	?	?				A6 FD5
A6 FD6													?	?		?			A6 FD6
A6 FD7															?	?	?		A6 FD7
Case	A4 WF1	A4 WF2	A4 WF3	A4 FD5	A4 FD6	A4 FD7	A5 WF1	A5 WF2	A5 WF3	A5 FD5	A5 FD6	A5 FD7	A6 WF1	A6 WF2	A6 WF3	A6 FD5	A6 FD6	A6 FD7	Case
	A5F	A5F	A5F	A5F	A5F	A5F	A4H	A4H	A4H	A4H	A4H	A4H	A5H	A5H	A5H	A5H	A5H	A5H	
A5F WF1																			A5F WF1
A5F WF2	?																		A5F WF2
A5F WF3	?																		A5F WF3
A5F FD5	id	id	id																A5F FD5
A5F FD6	<	<		id															A5F FD6
A5F FD7			?	id	?														A5F FD7
A4H WF1																			A4H WF1
A4H WF2							?												A4H WF2
A4H WF3							?												A4H WF3
A4H FD5							id	id	id										A4H FD5
A4H FD6							?	?		id									A4H FD6
A4H FD7									?	id	?								A4H FD7
A5H WF1																			A5H WF1
A5H WF2													?						A5H WF2
A5H WF3													?						A5H WF3
A5H FD5													id	id	id				A5H FD5
A5H FD6													?	?		id			A5H FD6
A5H FD7															?	id	?		A5H FD7
Case	A5F WF1	A5F WF2	A5F WF3	A5F FD5	A5F FD6	A5F FD7	A4H WF1	A4H WF2	A4H WF3	A4H FD5	A4H FD6	A4H FD7	A5H WF1	A5H WF2	A5H WF3	A5H FD5	A5H FD6	A5H FD7	Case

Table E91. Results of Hypothesis Test 1 for CD STFI and furnish WF1.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		0.0017	0.0978	0.0053	0.0005	0.0000	0.0002	0.0471	0.0000	0.0291	0.1213	0.0032	id	0.0027	0.0111	0.0098	0.0055	0.0007	0.0045	0.0084	0.0006	id	0.0009	0.6698	0.0001	Con
D1	>		0.4262	0.3359	0.0169			0.4740			0.9326			0.3579			0.0514									D1
D2	>	?(>)				0.2713			0.3089						0.5550			0.3738								D2
D3	>	?(>)					0.0172			0.1087						0.6098										D3
D4	>	>				0.0364	0.3020					0.0627							0.6615			id		0.9854		D4
D5	>		?(>)		>								id							0.7437			0.1201		0.8451	D5
D6	>			>	?(>)																0.6319					D6
C1S	>	?(>)							0.3012	0.7487	0.5405			0.7563												C1S
C2S	>		?(>)					?(>)							0.7192											C2S
C3S	>			?(>)				?(>)								0.6604										C3S
A1S	?(>)	?(>)						?(<)				0.8910					0.1165									A1S
A4S	>				<						?(>)		id						0.1029							A4S
A5S	id					id						id								id						A5S
C1	>	?(>)						?(<)							0.3568	0.6925	0.0993									C1
C2	>		?(>)						?(<)					?(>)				0.9919								C2
C3	>			?(>)						?(<)				?(>)												C3
A1	>	>									?(>)			>				0.5555	0.5909							A1
A2	>		?(>)												?(>)		?(<)			0.3948						A2
A4	>				?(>)							?(>)					?(<)			0.4266	0.7142	id		0.9907		A4
A5	>					?(>)							id					?(>)	?(>)				0.3359		0.6927	A5
A6	>						?(>)												?(>)							A6
A4F	id				id														id				id			A4F
A5F	>					?(<)														?(<)		id				A5F
A4H	?(>)				?(>)														?(<)						0.9519	A4H
A5H	>					?(<)														?(<)				?(>)		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E92. Results of Hypothesis Test 1 for CD STFI and furnish WF2.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		0.0412	0.0000	0.0001	0.0002	0.0001	0.0000	0.0001	0.0000	0.0013	id	0.0002	0.0024	0.0393	0.0000	0.0138	0.0166	<.0001	0.0132	0.0102	0.0635	id	id	0.8478	id	Con
D1	>		0.2688	0.5342	0.8627			0.3433			id			0.5834			0.6502									D1
D2	>	?(>)				1.0000			0.0920						0.0702			0.3585								D2
D3	>	?(>)					0.1998			0.5830						0.9828										D3
D4	>	?(>)				0.0837	0.0785					0.0167							0.7700			id		0.9903		D4
D5	>		?(>)		>								0.0118							0.8525			id		id	D5
D6	>			?(>)	>																0.9339					D6
C1S	>	?(>)							0.1077	0.9927	id			0.9347												C1S
C2S	>		>					?(>)							0.9809											C2S
C3S	>			?(>)				?(<)								0.7062										C3S
A1S	id	id						id				id					id									A1S
A4S	>				<						id		0.1909						0.0881							A4S
A5S	>					<						?(>)								0.1325						A5S
C1	>	?(>)						?(>)							0.7064	0.7832	0.7865									C1
C2	>		>						?(<)					?(>)				0.8392								C2
C3	>			?(<)						?(<)				?(<)												C3
A1	>	?(>)									id			?(<)				0.3039	0.9140							A1
A2	>		?(>)												?(<)		?(>)			0.5008						A2
A4	>				?(>)							>					?(<)			0.6133	0.7720	id		0.9999		A4
A5	>					?(<)							?(>)					?(<)	?(>)				id		id	A5
A6	>						?(<)												?(>)							A6
A4F	id				id														id				id			A4F
A5F	id					id														id		id				A5F
A4H	?(>)				?(>)														?(<)						id	A4H
A5H	id					id														id				id		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E93. Results of Hypothesis Test 1 for CD STFI and furnish WF3.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		0.0000	0.0010	0.0024	0.0022	0.0006	0.0003	0.0840	0.0003	0.0000	id	0.0012	id	0.0114	<.0001	0.0097	<.0001	<.0001	0.0196	0.0098	0.0000	id	id	id	id	Con
D1	>		0.2807	0.1873	0.0216			0.9283			id			0.6525			0.9775									D1
D2	>	?(<)				0.1567			0.0482						0.2669			0.3521								D2
D3	>	?(<)					0.0607			0.9236						0.3426										D3
D4	>	<				0.0148	0.0081					0.4806							0.1152			id		id		D4
D5	>		?(>)		>								id							0.7955			id		id	D5
D6	>			>	>																0.3536					D6
C1S	>	?(>)							0.5169	0.5595	id			0.7169												C1S
C2S	>		>					?(>)							0.1922											C2S
C3S	>			?(<)				?(<)								0.3494										C3S
A1S	id	id						id				id					id									A1S
A4S	>				?(<)						id		id						0.0787							A4S
A5S	id					id						id								id						A5S
C1	>	?(<)						?(<)							0.5632	0.5915	0.6461									C1
C2	>		?(>)						?(<)					?(>)				0.8553								C2
C3	>			?(>)						?(>)				?(>)												C3
A1	>	?(>)									id			?(>)				0.9770	0.8275							A1
A2	>		?(>)												?(<)		?(>)			0.8194						A2
A4	>				?(>)							>					?(>)			0.9791	0.9521	id		id		A4
A5	>					?(<)							id					?(>)	?(<)				id		id	A5
A6	>						?(<)												?(<)							A6
A4F	id				id														id				id			A4F
A5F	id					id														id		id				A5F
A4H	id				id														id						id	A4H
A5H	id					id														id				id		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E94. Results of Hypothesis Test 1 for CD STFI and furnish FD5.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		0.1767	0.1793	0.0586	0.6828	0.8681	0.0680	0.1163	0.0231	0.2261	id	0.7267	0.6192	0.2342	0.2391	0.1933	0.7378	id	0.4544	0.4233	id	id	id	id	id	Con
D1	?(>)		0.5277	0.9605	0.2100			0.9113			id			0.6875			0.8514									D1
D2	?(>)	?(<)				0.0103			0.0868						0.6796			id								D2
D3	>	?(>)					0.7252			0.1604						0.2933										D3
D4	?(>)	?(<)				0.4669	0.0856					0.8099							0.4355			id		id		D4
D5	?(>)		<		?(<)								0.3492							0.1285			id		id	D5
D6	>			?(>)	>																id					D6
C1S	?(>)	?(<)							0.2970	0.3565	id			0.7151												C1S
C2S	>		>					?(>)							0.4084											C2S
C3S	?(>)			?(<)				?(<)								0.7187										C3S
A1S	id	id						id				id					id									A1S
A4S	?(>)				?(>)						id		0.5955						0.9372							A4S
A5S	?(<)					?(<)						?(<)								0.7184						A5S
C1	?(>)	?(<)						?(<)							0.8207	0.8638	0.9678									C1
C2	?(>)		?(>)						?(<)					?(>)				id								C2
C3	?(>)			?(<)						?(>)				?(<)												C3
A1	?(>)	?(<)									id			?(<)				id	0.8659							A1
A2	id		id												id		id			id						A2
A4	?(>)				?(>)							?(<)					?(<)			0.0424	id	id		id		A4
A5	?(<)					?(<)							?(<)					id	<				id		id	A5
A6	id						id												id							A6
A4F	id				id														id				id			A4F
A5F	id					id														id		id				A5F
A4H	id				id														id						id	A4H
A5H	id					id														id				id		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E95. Results of Hypothesis Test 1 for CD STFI and furnish FD6.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		0.0005	0.0120	0.0048	0.0153	0.0001	0.0001	0.0697	0.0002	0.0001	id	0.0213	0.2335	0.0029	0.0037	0.0009	0.0785	0.0672	0.0352	0.0545	0.0406	id	0.0001	0.0545	0.0078	Con
D1	>		0.2539	0.3834	0.5927			0.2600			id			0.3208			0.4895									D1
D2	>	?(<)				0.4396			0.0257						0.1854			0.2794								D2
D3	>	?(<)					0.3854			0.9451						0.0368										D3
D4	>	?(<)				0.8586	0.5743					0.1040							0.3141			id		0.3959		D4
D5	>		?(>)		?(>)								0.0404							0.3530			0.1601		0.2072	D5
D6	>			?(>)	?(>)																0.7743					D6
C1S	>	?(<)							0.0584	0.4766	id			0.1083												C1S
C2S	>		>					>							0.1604											C2S
C3S	>			?(>)				?(>)								0.0315										C3S
A1S	id	id						id				id					id									A1S
A4S	>				?(<)						id		0.5321						0.0696							A4S
A5S	?(>)					<						?(<)								0.0803						A5S
C1	>	?(>)						?(>)							0.7511	0.4390	0.7226									C1
C2	>		?(>)						?(<)					?(<)				0.5956								C2
C3	>			>						>				?(>)												C3
A1	>	?(>)									id			?(>)				0.9884	0.9060							A1
A2	>		?(>)												?(>)		?(>)			0.9863						A2
A4	>				?(>)							>					?(<)			0.8963	0.6542	id		0.9813		A4
A5	>					?(>)							>					?(<)	?(>)				0.6565		0.9455	A5
A6	>						?(>)												?(<)							A6
A4F	id				id														id				id			A4F
A5F	>					?(>)														?(<)		id				A5F
A4H	>				?(>)														?(<)						0.8208	A4H
A5H	>					?(>)														?(>)				?(>)		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E96. Results of Hypothesis Test 1 for CD STFI and furnish FD7.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		id	0.0001	0.0013	0.0015	0.0000	id	0.0002	0.0375	0.0000	id	0.0007	0.0001	0.0002	<.0001	<.0001	id	id	0.0224	0.0212	0.0516	id	id	id	id	Con
D1	id		id	id	id			id			id			id			id									D1
D2	>	id				0.1255			0.2183						0.9367			id								D2
D3	>	id					id			0.7061						0.7298										D3
D4	>	id				0.8987	id					0.0417							0.3855			id		id		D4
D5	>		?(<)		?(>)								0.0008							0.2498			id		id	D5
D6	id			id	id																id					D6
C1S	>	id							0.3025	0.9314	id			0.2191												C1S
C2S	>		?(<)					?(<)							0.2434											C2S
C3S	>			?(>)				?(>)								0.9537										C3S
A1S	id	id						id				id					id									A1S
A4S	>				<						id		0.9323						0.0944							A4S
A5S	>					<						?(>)								0.0755						A5S
C1	>	id						?(<)							0.1682	0.2204	id									C1
C2	>		?(<)						?(>)					?(>)				id								C2
C3	>			?(>)						?(>)				?(>)												C3
A1	id	id									id			id				id	id							A1
A2	id		id												id		id			id						A2
A4	>				?(>)							>					id			0.6879	0.9430	id		id		A4
A5	>					?(>)							>					id	?(>)				id		id	A5
A6	>						id												?(<)							A6
A4F	id				id														id				id			A4F
A5F	id					id														id		id				A5F
A4H	id				id														id						id	A4H
A5H	id					id														id				id		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E97. Results of Hypothesis Test 1 for CD STFI, comparing furnishes.

Case	Con WF1	Con WF2	Con WF3	Con FD5	Con FD6	Con FD7	D1 WF1	D1 WF2	D1 WF3	D1 FD5	D1 FD6	D1 FD7	D2 WF1	D2 WF2	D2 WF3	D2 FD5	D2 FD6	D2 FD7	Case
Con WF1		0.0003	0.0238	0.0455	0.0453														Con WF1
Con WF2	>			0.1148	0.0001														Con WF2
Con WF3	>			0.1540		0.2619													Con WF3
Con FD5	>	?(<)	?(>)		0.1095	0.2487													Con FD5
Con FD6	>	<		?(<)		0.1783													Con FD6
Con FD7			?(>)	?(<)	?(>)														Con FD7
D1 WF1								0.0490	0.0095	0.6753	0.6884								D1 WF1
D1 WF2							>			0.0507	0.0571								D1 WF2
D1 WF3							>			0.0824		id							D1 WF3
D1 FD5							?(<)	<	<		0.7829	id							D1 FD5
D1 FD6							?(<)	<		?(>)		id							D1 FD6
D1 FD7									id	id	id								D1 FD7
D2 WF1														0.2266	0.8146	0.2247	0.1684		D2 WF1
D2 WF2													?(>)			0.0001	0.0046		D2 WF2
D2 WF3													?(>)			0.0202		0.1583	D2 WF3
D2 FD5													?(<)	<	<		0.7954	0.0031	D2 FD5
D2 FD6													?(<)	<		?(>)		0.0574	D2 FD6
D2 FD7															?(<)	>	>		D2 FD7

Case	Con WF1 D3	Con WF2 D3	Con WF3 D3	Con FD5 D3	Con FD6 D3	Con FD7 D3	D1 WF1 D4	D1 WF2 D4	D1 WF3 D4	D1 FD5 D4	D1 FD6 D4	D1 FD7 D4	D2 WF1 D5	D2 WF2 D5	D2 WF3 D5	D2 FD5 D5	D2 FD6 D5	D2 FD7 D5	Case
D3 WF1		0.0057	0.1160	0.1614	0.0924														D3 WF1
D3 WF2	>			0.0016	0.0011														D3 WF2
D3 WF3	?(>)			0.0218		0.0704													D3 WF3
D3 FD5	?(<)	<	<		0.7157	0.2579													D3 FD5
D3 FD6	<	<		?(<)		0.1471													D3 FD6
D3 FD7			<	?(>)	?(>)														D3 FD7
D4 WF1								0.1520	0.0330	0.0021	0.0300								D4 WF1
D4 WF2							?(>)			0.0007	0.0143								D4 WF2
D4 WF3							<			0.0246		0.6483							D4 WF3
D4 FD5							<	<	<		0.1508	0.0128							D4 FD5
D4 FD6							<	<		?(>)		0.4634							D4 FD6
D4 FD7									?(<)	>	?(>)								D4 FD7
D5 WF1														0.2800	0.1563	0.0000	0.0000		D5 WF1
D5 WF2													?(>)			0.0000	0.0002		D5 WF2
D5 WF3													?(<)			0.0016		0.0105	D5 WF3
D5 FD5													<	<	<		0.0008	0.0002	D5 FD5
D5 FD6													<	<		>		0.0462	D5 FD6
D5 FD7															<	>	>		D5 FD7
Case	D3 WF1	D3 WF2	D3 WF3	D3 FD5	D3 FD6	D3 FD7	D4 WF1	D4 WF2	D4 WF3	D4 FD5	D4 FD6	D4 FD7	D5 WF1	D5 WF2	D5 WF3	D5 FD5	D5 FD6	D5 FD7	Case

Table E98. Results of Hypothesis Test 1 for CD STFI, comparing furnishes continued.

Case	D6 WF1	D6 WF2	D6 WF3	D6 FD5	D6 FD6	D6 FD7	C1S WF1	C1S WF2	C1S WF3	C1S FD5	C1S FD6	C1S FD7	C2S WF1	C2S WF2	C2S WF3	C2S FD5	C2S FD6	C2S FD7	Case
D6 WF1		0.0174	0.6890	0.0376	0.0008														D6 WF1
D6 WF2	>			0.0193	0.0002														D6 WF2
D6 WF3	?(>)			0.0311		id													D6 WF3
D6 FD5	<	<	<		0.9478	id													D6 FD5
D6 FD6	<	<		?(<)		id													D6 FD6
D6 FD7			id	id	id														D6 FD7
C1S WF1								0.2269	0.5566	0.3014	0.1941								C1S WF1
C1S WF2							?(>)			0.0055	0.0082								C1S WF2
C1S WF3							?(>)			0.0702		0.2998							C1S WF3
C1S FD5							?(<)	<	<		0.5481	0.1953							C1S FD5
C1S FD6							?(<)	<		?(<)		0.0989							C1S FD6
C1S FD7									?(<)	?(>)	>								C1S FD7
C2S WF1														0.0045	0.9428	0.0191	0.0037		C2S WF1
C2S WF2													>			0.0049	0.0010		C2S WF2
C2S WF3													?(<)			0.0249		0.0162	C2S WF3
C2S FD5													<	<	<		0.2226	0.4403	C2S FD5
C2S FD6													<	<		?(>)		0.0972	C2S FD6
C2S FD7															<	?(<)	<		C2S FD7
Case	D6 WF1 C3S	D6 WF2 C3S	D6 WF3 C3S	D6 FD5 C3S	D6 FD6 C3S	D6 FD7 C3S	C1S WF1 A1S	C1S WF2 A1S	C1S WF3 A1S	C1S FD5 A1S	C1S FD6 A1S	C1S FD7 A1S	C2S WF1 A4S	C2S WF2 A4S	C2S WF3 A4S	C2S FD5 A4S	C2S FD6 A4S	C2S FD7 A4S	Case
C3S WF1		0.0358	0.7076	0.0135	0.0088														C3S WF1
C3S WF2	>			0.0009	0.0019														C3S WF2
C3S WF3	?(<)			0.0001		0.0169													C3S WF3
C3S FD5	<	<	<		0.0781	0.0010													C3S FD5
C3S FD6	<	<		>		0.0110													C3S FD6
C3S FD7			<	>	>														C3S FD7
A1S WF1								id	id	id	id								A1S WF1
A1S WF2							id			id	id								A1S WF2
A1S WF3							id			id		id							A1S WF3
A1S FD5							id	id	id		id	id							A1S FD5
A1S FD6							id	id		id		id							A1S FD6
A1S FD7									id	id	id								A1S FD7
A4S WF1														0.1383	0.5933	0.4689	0.0129		A4S WF1
A4S WF2													?(>)			0.3159	0.0004		A4S WF2
A4S WF3													?(<)			0.5366		0.0607	A4S WF3
A4S FD5													?(<)	?(<)	?(<)		0.7330	0.9065	A4S FD5
A4S FD6													<	<		?(<)		0.0966	A4S FD6
A4S FD7															<	?(>)	>		A4S FD7
Case	C3S WF1	C3S WF2	C3S WF3	C3S FD5	C3S FD6	C3S FD7	A1S WF1	A1S WF2	A1S WF3	A1S FD5	A1S FD6	A1S FD7	A4S WF1	A4S WF2	A4S WF3	A4S FD5	A4S FD6	A4S FD7	Case

Table E99. Results of Hypothesis Test 1 for CD STFI, comparing furnishes continued.

Case	A5S WF1	A5S WF2	A5S WF3	A5S FD5	A5S FD6	A5S FD7	C1 WF1	C1 WF2	C1 WF3	C1 FD5	C1 FD6	C1 FD7	C2 WF1	C2 WF2	C2 WF3	C2 FD5	C2 FD6	C2 FD7	Case
A5S WF1		id	id	id	id														A5S WF1
A5S WF2	id			0.0002	0.0014														A5S WF2
A5S WF3	id			id		id													A5S WF3
A5S FD5	id	<	id		0.9783	0.0455													A5S FD5
A5S FD6	id	<		?(<)		0.1168													A5S FD6
A5S FD7			id	>	?(>)														A5S FD7
C1 WF1								0.1368	0.2413	0.1194	0.8676								C1 WF1
C1 WF2							?(>)			0.0351	0.1247								C1 WF2
C1 WF3							?(>)			0.0279		0.0627							C1 WF3
C1 FD5							?(<)	<	<		0.1608	0.3052							C1 FD5
C1 FD6							?(<)	?(<)		?(>)		0.4180							C1 FD6
C1 FD7									<	?(>)	?(<)								C1 FD7
C2 WF1														0.2938	0.9216	0.1458	0.2609		C2 WF1
C2 WF2													?(>)			0.0071	0.0085		C2 WF2
C2 WF3													?(<)			0.0501		0.0177	C2 WF3
C2 FD5													?(<)	<	<		0.4779	0.2932	C2 FD5
C2 FD6													?(<)	<		?(>)		0.6058	C2 FD6
C2 FD7															<	?(>)	?(>)		C2 FD7
Case	A5S WF1 C3	A5S WF2 C3	A5S WF3 C3	A5S FD5 C3	A5S FD6 C3	A5S FD7 C3	C1 WF1 A1	C1 WF2 A1	C1 WF3 A1	C1 FD5 A1	C1 FD6 A1	C1 FD7 A1	C2 WF1 A2	C2 WF2 A2	C2 WF3 A2	C2 FD5 A2	C2 FD6 A2	C2 FD7 A2	Case
C3 WF1		0.1628	0.3873	0.0901	0.9609														C3 WF1
C3 WF2	?(>)			0.0039	0.0919														C3 WF2
C3 WF3	?(>)			0.0084		0.0819													C3 WF3
C3 FD5	<	<	<		0.0115	0.0174													C3 FD5
C3 FD6	?(>)	<		>		0.3816													C3 FD6
C3 FD7			<	>	?(<)														C3 FD7
A1 WF1								0.9835	0.4071	0.3728	0.4488								A1 WF1
A1 WF2							?(<)			0.3655	0.4413								A1 WF2
A1 WF3							?(<)			0.4369		id							A1 WF3
A1 FD5							?(<)	?(<)	?(<)		0.5273	id							A1 FD5
A1 FD6							?(<)	?(<)		?(>)		id							A1 FD6
A1 FD7									id	id	id								A1 FD7
A2 WF1														0.0265	0.6562	id	0.6239		A2 WF1
A2 WF2													>			id	0.2338		A2 WF2
A2 WF3													?(<)			id		id	A2 WF3
A2 FD5													id	id	id		id	id	A2 FD5
A2 FD6													?(<)	?(<)		id		id	A2 FD6
A2 FD7															id	id	id		A2 FD7
Case	C3 WF1	C3 WF2	C3 WF3	C3 FD5	C3 FD6	C3 FD7	A1 WF1	A1 WF2	A1 WF3	A1 FD5	A1 FD6	A1 FD7	A2 WF1	A2 WF2	A2 WF3	A2 FD5	A2 FD6	A2 FD7	Case

Table E100. Results of Hypothesis Test 1 for CD STFI, comparing furnishes continued.

Case	A4 WF1	A4 WF2	A4 WF3	A4 FD5	A4 FD6	A4 FD7	A5 WF1	A5 WF2	A5 WF3	A5 FD5	A5 FD6	A5 FD7	A6 WF1	A6 WF2	A6 WF3	A6 FD5	A6 FD6	A6 FD7	Case
A4 WF1		0.5925	0.9695	0.0136	0.4421														A4 WF1
A4 WF2	?(>)			0.0020	0.2425														A4 WF2
A4 WF3	?(<)			0.0220		0.3854													A4 WF3
A4 FD5	<	<	<		0.1104	0.0584													A4 FD5
A4 FD6	?(<)	?(<)		?(>)		0.9853													A4 FD6
A4 FD7			?(<)	>	?(>)														A4 FD7
A5 WF1								0.8964	0.3702	0.0165	0.2982								A5 WF1
A5 WF2							?(<)			0.0013	0.2880								A5 WF2
A5 WF3							?(<)			0.0015		0.6715							A5 WF3
A5 FD5							<	<	<		0.0827	0.0161							A5 FD5
A5 FD6							?(<)	?(<)		>		0.8575							A5 FD6
A5 FD7									?(<)	>	?(>)								A5 FD7
A6 WF1														0.6548	0.3938	id	0.1111		A6 WF1
A6 WF2													?(>)			id	0.1319		A6 WF2
A6 WF3													?(<)			id		0.4108	A6 WF3
A6 FD5													id	id	id		id	id	A6 FD5
A6 FD6													?(<)	?(<)		id		0.6973	A6 FD6
A6 FD7															?(<)	id	?(>)		A6 FD7

Case	A4 WF1 A5F	A4 WF2 A5F	A4 WF3 A5F	A4 FD5 A5F	A4 FD6 A5F	A4 FD7 A5F	A5 WF1 A4H	A5 WF2 A4H	A5 WF3 A4H	A5 FD5 A4H	A5 FD6 A4H	A5 FD7 A4H	A6 WF1 A5H	A6 WF2 A5H	A6 WF3 A5H	A6 FD5 A5H	A6 FD6 A5H	A6 FD7 A5H	Case
A5F WF1		id	id	id	0.0626														A5F WF1
A5F WF2	id			id	id														A5F WF2
A5F WF3	id			id		id													A5F WF3
A5F FD5	id	id	id		id	id													A5F FD5
A5F FD6	<	id		id		id													A5F FD6
A5F FD7			id	id	id														A5F FD7
A4H WF1								0.9729	id	id	0.9388								A4H WF1
A4H WF2							?(>)			id	0.9203								A4H WF2
A4H WF3							id			id		id							A4H WF3
A4H FD5							id	id	id		id	id							A4H FD5
A4H FD6							?(<)	?(<)		id		id							A4H FD6
A4H FD7									id	id	id								A4H FD7
A5H WF1														id	id	id	0.3325		A5H WF1
A5H WF2													id			id	id		A5H WF2
A5H WF3													id			id		id	A5H WF3
A5H FD5													id	id	id		id	id	A5H FD5
A5H FD6													?(<)	id		id		id	A5H FD6
A5H FD7															id	id	id		A5H FD7
Case	A5F WF1	A5F WF2	A5F WF3	A5F FD5	A5F FD6	A5F FD7	A4H WF1	A4H WF2	A4H WF3	A4H FD5	A4H FD6	A4H FD7	A5H WF1	A5H WF2	A5H WF3	A5H FD5	A5H FD6	A5H FD7	Case

Table E101. Results of Hypothesis Test 2 for CD STFI and furnish WF1.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		0.0017	0.0978	0.0053	0.0005	0.0000	0.0002	0.0471	0.0000	0.0291	0.1213	0.0032	id	0.0023	0.0070	0.0081	0.0013	0.0006	0.0010	0.0014	0.0006	id	0.0003	0.6698	0.0000	Con
D1	>		0.4262	0.3359	0.0169			0.4740			0.9326			0.4274			0.0046									D1
D2	>	?(>)				0.2713			0.3089						0.4217			0.3873								D2
D3	>	?(>)					0.0172			0.1087						0.8733										D3
D4	>	>				0.0364	0.3020					0.0627							0.1194			id		0.9854		D4
D5	>		?(>)		>								id							0.1038			0.1939		0.6413	D5
D6	>			>	?(>)																0.5608					D6
C1S	>	?(>)							0.3012	0.7487	0.5405			0.6918												C1S
C2S	>		?(>)					?(>)							0.8650											C2S
C3S	>			?(>)				?(>)								0.3615										C3S
A1S	?(>)	?(>)						?(<)				0.8910					0.0733									A1S
A4S	>				<						?(>)		id						0.0108							A4S
A5S	id					id						id								id						A5S
C1	>	?(>)						?(<)							0.2173	0.8622	0.0111									C1
C2	>		?(>)						?(<)					?(>)				0.8133								C2
C3	>			?(>)						?(<)				?(>)												C3
A1	>	>									>			>				0.0921	0.3834							A1
A2	>		?(>)												?(<)		<			0.0289						A2
A4	>				?(>)							>					?(<)			0.1113	0.5756	id		0.9439		A4
A5	>					?(>)							id					>	?(>)				0.0453		0.1433	A5
A6	>						?(>)												?(<)							A6
A4F	id				id														id				id			A4F
A5F	>					?(<)														<		id				A5F
A4H	?(>)				?(>)														?(<)						0.9285	A4H
A5H	>					?(>)														?(<)				?(>)		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E102. Results of Hypothesis Test 2 for CD STFI and furnish WF2.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		0.0412	0.0000	0.0001	0.0002	0.0001	0.0000	0.0001	0.0000	0.0013	id	0.0002	0.0024	0.0037	0.0000	0.0055	0.0141	<.0001	0.0009	0.0007	0.0152	id	id	0.8478	id	Con
D1	>		0.2688	0.5342	0.8627			0.3433			id			0.1226			0.9349									D1
D2	>	?(>)				1.0000			0.0920						0.0618			0.6454								D2
D3	>	?(>)					0.1998			0.5830						0.6727										D3
D4	>	?(>)				0.0837	0.0785					0.0167							0.1678			id		0.9903		D4
D5	>		?(>)		>								0.0118							0.4089			id		id	D5
D6	>			?(>)	>																0.3905					D6
C1S	>	?(>)							0.1077	0.9927	id			0.2641												C1S
C2S	>		>					?(>)							0.9653											C2S
C3S	>			?(>)				?(<)								0.4519										C3S
A1S	id	id						id				id					id									A1S
A4S	>				<						id		0.1909						0.0109							A4S
A5S	>					<						?(>)								0.0165						A5S
C1	>	?(>)						?(>)							0.6026	0.1412	0.1237									C1
C2	>		>						?(>)					?(<)				0.2843								C2
C3	>			?(<)						?(<)				?(<)												C3
A1	>	?(>)									id			?(<)				0.1693	0.2701							A1
A2	>		?(>)												?(<)		?(>)			0.5717						A2
A4	>				?(>)							>					?(>)			0.4791	0.4224	id		0.9719		A4
A5	>					?(>)							>					?(>)	?(>)				id		id	A5
A6	>						?(>)												?(>)							A6
A4F	id				id														id				id			A4F
A5F	id					id														id		id				A5F
A4H	?(>)				?(>)														?(<)						id	A4H
A5H	id					id														id				id		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E103. Results of Hypothesis Test 2 for CD STFI and furnish WF3.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		0.0000	0.0010	0.0024	0.0022	0.0006	0.0003	0.0840	0.0003	0.0000	id	0.0012	id	0.0100	<.0001	0.0047	<.0001	<.0001	0.0069	0.0004	0.0000	id	id	id	id	Con
D1	>		0.2807	0.1873	0.0216			0.9283			id			0.3718			0.9877									D1
D2	>	?(<)				0.1567			0.0482						0.1110			0.3130								D2
D3	>	?(<)					0.0607			0.9236						0.0742										D3
D4	>	<				0.0148	0.0081					0.4806							0.0202			id		id		D4
D5	>		?(>)		>								id							0.2908			id		id	D5
D6	>			>	>																0.3935					D6
C1S	>	?(>)							0.5169	0.5595	id			0.5301												C1S
C2S	>		>					?(>)							0.3179											C2S
C3S	>			?(<)				?(<)								0.0623										C3S
A1S	id	id						id				id					id									A1S
A4S	>				?(<)						id		id						0.0074							A4S
A5S	id					id						id								id						A5S
C1	>	?(<)						?(<)							0.1628	0.1068	0.3624									C1
C2	>		?(>)						?(<)					?(>)				0.5167								C2
C3	>			>						>				?(>)												C3
A1	>	?(>)									id			?(>)				0.9066	0.1263							A1
A2	>		?(>)												?(<)		?(>)			0.1204						A2
A4	>				>							>					?(>)			0.7021	0.2053	id		id		A4
A5	>					?(>)							id					?(>)	?(<)				id		id	A5
A6	>						?(<)												?(<)							A6
A4F	id				id														id				id			A4F
A5F	id					id														id		id				A5F
A4H	id				id														id						id	A4H
A5H	id					id														id				id		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E104. Results of Hypothesis Test 2 for CD STFI and furnish FD5.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		0.1767	0.1793	0.0586	0.6828	0.8681	0.0680	0.1163	0.0231	0.2261	id	0.7267	0.6192	0.2747	0.2541	0.1305	0.4639	id	0.4551	0.3413	id	id	id	id	id	Con
D1	?(>)		0.5277	0.9605	0.2100			0.9113			id			0.5836			0.7652									D1
D2	?(>)	?(<)				0.0103			0.0868						0.7300			id								D2
D3	>	?(>)					0.7252			0.1604						0.4003										D3
D4	?(>)	?(<)				0.4669	0.0856					0.8099							0.4366			id		id		D4
D5	?(>)		<		?(<)								0.3492							0.0670			id		id	D5
D6	>			?(>)	>																id					D6
C1S	?(>)	?(<)							0.2970	0.3565	id			0.5826												C1S
C2S	>		>					?(>)							0.3568											C2S
C3S	?(>)			?(<)				?(<)								0.4236										C3S
A1S	id	id						id				id					id									A1S
A4S	?(>)				?(>)						id		0.5955						0.9366							A4S
A5S	?(<)					?(<)						?(<)								0.5584						A5S
C1	?(>)	?(<)						?(<)							0.7669	0.8122	0.6244									C1
C2	?(>)		?(>)						?(<)					?(>)				id								C2
C3	?(>)			?(<)						?(>)				?(>)												C3
A1	?(>)	?(>)									id			?(>)				id	0.5331							A1
A2	id		id												id		id			id						A2
A4	?(>)				?(>)							?(<)					?(<)			0.0222	id	id		id		A4
A5	?(<)					<							?(<)					id	<				id		id	A5
A6	id						id												id							A6
A4F	id				id														id				id			A4F
A5F	id					id														id		id				A5F
A4H	id				id														id						id	A4H
A5H	id					id														id				id		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E105. Results of Hypothesis Test 2 for CD STFI and furnish FD6.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		0.0005	0.0120	0.0048	0.0153	0.0001	0.0001	0.0697	0.0002	0.0001	id	0.0213	0.2335	0.0007	0.0024	0.0001	0.0153	0.0727	0.0116	0.0093	0.0400	id	0.0000	0.0119	0.0075	Con
D1	>		0.2539	0.3834	0.5927			0.2600			id			0.0720			0.0922										D1
D2	>	?(<)				0.4396			0.0257						0.3451			0.4643								D2
D3	>	?(<)					0.3854			0.9451						0.0096										D3
D4	>	?(<)				0.8586	0.5743					0.1040							0.0848			id		0.0725		D4
D5	>		?(>)		?(>)								0.0404							0.0521			0.2168		0.2017	D5
D6	>			?(>)	?(>)																0.9754					D6
C1S	>	?(<)							0.0584	0.4766	id			0.0470												C1S
C2S	>		>					>							0.0360											C2S
C3S	>			?(>)				?(>)								0.0041										C3S
A1S	id	id						id				id					id									A1S
A4S	>				?(<)						id		0.5321						0.0172							A4S
A5S	?(>)					<						?(<)								0.0064						A5S
C1	>	>						>							0.0876	0.3714	0.2245									C1
C2	>		?(>)						<					<				0.7569								C2
C3	>			>						>				?(>)												C3
A1	>	>									id			?(>)				0.2000	0.5095							A1
A2	>		?(>)												?(>)		?(<)			0.1840						A2
A4	>				>							>					?(<)			0.5038	0.2036	id		0.7847		A4
A5	>					>							>					?(>)	?(>)				0.0806		0.4142	A5
A6	>						?(>)												?(<)							A6
A4F	id				id														id				id			A4F
A5F	>					?(>)														<		id				A5F
A4H	>				>														?(>)						0.6304	A4H
A5H	>					?(>)														?(<)				?(<)		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E106. Results of Hypothesis Test 2 for CD STFI and furnish FD7.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		id	0.0001	0.0013	0.0015	0.0000	id	0.0002	0.0375	0.0000	id	0.0007	0.0001	0.0001	<.0001	<.0001	id	id	0.0044	0.0071	0.0166	id	id	id	id	Con
D1	id		id	id	id			id			id			id			id								D1
D2	>	id				0.1255			0.2183						0.9367			id							D2
D3	>	id					id			0.7061						0.8504									D3
D4	>	id				0.8987	id					0.0417							0.0445			id		id	D4
D5	>		?(<)		?(>)								0.0008							0.0722			id		id	D5
D6	id			id	id																id				D6
C1S	>	id							0.3025	0.9314	id			0.1247											C1S
C2S	>		?(<)					?(<)							0.2434										C2S
C3S	>			?(>)				?(>)								0.8609									C3S
A1S	id	id						id				id					id								A1S
A4S	>				<						id		0.9323						0.0147						A4S
A5S	>					<						?(>)								0.0228					A5S
C1	>	id						?(<)							0.0880	0.1402	id								C1
C2	>		?(<)						?(>)					>				id							C2
C3	>			?(>)						?(<)				?(>)											C3
A1	id	id									id			id				id	id						A1
A2	id		id												id		id			id					A2
A4	>				>							>					id			0.7269	0.8690	id		id	A4
A5	>					>							>					id	?(>)				id		id	A5
A6	>						id												?(<)							A6
A4F	id				id														id				id			A4F
A5F	id					id														id		id				A5F
A4H	id				id														id						id	A4H
A5H	id					id														id				id		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E107. Results of Hypothesis Test 2 for CD STFI, comparing furnishes.

Case	Con WF1	Con WF2	Con WF3	Con FD5	Con FD6	Con FD7	D1 WF1	D1 WF2	D1 WF3	D1 FD5	D1 FD6	D1 FD7	D2 WF1	D2 WF2	D2 WF3	D2 FD5	D2 FD6	D2 FD7	Case
Con WF1		0.0003	0.0238	0.0455	0.0453														Con WF1
Con WF2	>			0.1148	0.0001														Con WF2
Con WF3	>			0.1540		0.2619													Con WF3
Con FD5	>	?(<)	?(>)		0.1095	0.2487													Con FD5
Con FD6	>	<		?(<)		0.1783													Con FD6
Con FD7			?(>)	?(<)	?(>)														Con FD7
D1 WF1								0.0490	0.0095	0.6753	0.6884								D1 WF1
D1 WF2							>			0.0507	0.0571								D1 WF2
D1 WF3							>			0.0824		id							D1 WF3
D1 FD5							?(<)	<	<		0.7829	id							D1 FD5
D1 FD6							?(<)	<		?(>)		id							D1 FD6
D1 FD7									id	id	id								D1 FD7
D2 WF1														0.2266	0.8146	0.2247	0.1684		D2 WF1
D2 WF2													?(>)			0.0001	0.0046		D2 WF2
D2 WF3													?(>)			0.0202		0.1583	D2 WF3
D2 FD5													?(<)	<	<		0.7954	0.0031	D2 FD5
D2 FD6													?(<)	<		?(>)		0.0574	D2 FD6
D2 FD7															?(<)	>	>		D2 FD7

Case	Con WF1 D3	Con WF2 D3	Con WF3 D3	Con FD5 D3	Con FD6 D3	Con FD7 D3	D1 WF1 D4	D1 WF2 D4	D1 WF3 D4	D1 FD5 D4	D1 FD6 D4	D1 FD7 D4	D2 WF1 D5	D2 WF2 D5	D2 WF3 D5	D2 FD5 D5	D2 FD6 D5	D2 FD7 D5	Case
D3 WF1		0.0057	0.1160	0.1614	0.0924														D3 WF1
D3 WF2	>			0.0016	0.0011														D3 WF2
D3 WF3	?(>)			0.0218		0.0704													D3 WF3
D3 FD5	?(<)	<	<		0.7157	0.2579													D3 FD5
D3 FD6	<	<		?(<)		0.1471													D3 FD6
D3 FD7			<	?(>)	?(>)														D3 FD7
D4 WF1								0.1520	0.0330	0.0021	0.0300								D4 WF1
D4 WF2							?(>)			0.0007	0.0143								D4 WF2
D4 WF3							<			0.0246		0.6483							D4 WF3
D4 FD5							<	<	<		0.1508	0.0128							D4 FD5
D4 FD6							<	<		?(>)		0.4634							D4 FD6
D4 FD7									?(<)	>	?(>)								D4 FD7
D5 WF1														0.2800	0.1563	0.0000	0.0000		D5 WF1
D5 WF2													?(>)			0.0000	0.0002		D5 WF2
D5 WF3													?(<)			0.0016		0.0105	D5 WF3
D5 FD5													<	<	<		0.0008	0.0002	D5 FD5
D5 FD6													<	<		>		0.0462	D5 FD6
D5 FD7															<	>	>		D5 FD7
Case	D3 WF1	D3 WF2	D3 WF3	D3 FD5	D3 FD6	D3 FD7	D4 WF1	D4 WF2	D4 WF3	D4 FD5	D4 FD6	D4 FD7	D5 WF1	D5 WF2	D5 WF3	D5 FD5	D5 FD6	D5 FD7	Case

Table E108. Results of Hypothesis Test 2 for CD STFI, comparing furnishes continued.

Case	D6 WF1	D6 WF2	D6 WF3	D6 FD5	D6 FD6	D6 FD7	C1S WF1	C1S WF2	C1S WF3	C1S FD5	C1S FD6	C1S FD7	C2S WF1	C2S WF2	C2S WF3	C2S FD5	C2S FD6	C2S FD7	Case
D6 WF1		0.0174	0.6890	0.0376	0.0008														D6 WF1
D6 WF2	>			0.0193	0.0002														D6 WF2
D6 WF3	?(>)			0.0311		id													D6 WF3
D6 FD5	<	<	<		0.9478	id													D6 FD5
D6 FD6	<	<		?(<)		id													D6 FD6
D6 FD7			id	id	id														D6 FD7
C1S WF1								0.2269	0.5566	0.3014	0.1941								C1S WF1
C1S WF2							?(>)			0.0055	0.0082								C1S WF2
C1S WF3							?(>)			0.0702		0.2998							C1S WF3
C1S FD5							?(<)	<	<		0.5481	0.1953							C1S FD5
C1S FD6							?(<)	<		?(<)		0.0989							C1S FD6
C1S FD7									?(<)	?(>)	>								C1S FD7
C2S WF1														0.0045	0.9428	0.0191	0.0037		C2S WF1
C2S WF2													>			0.0049	0.0010		C2S WF2
C2S WF3													?(<)			0.0249		0.0162	C2S WF3
C2S FD5													<	<	<		0.2226	0.4403	C2S FD5
C2S FD6													<	<		?(>)		0.0972	C2S FD6
C2S FD7															<	?(<)	<		C2S FD7
Case	D6 WF1 C3S	D6 WF2 C3S	D6 WF3 C3S	D6 FD5 C3S	D6 FD6 C3S	D6 FD7 C3S	C1S WF1 A1S	C1S WF2 A1S	C1S WF3 A1S	C1S FD5 A1S	C1S FD6 A1S	C1S FD7 A1S	C2S WF1 A4S	C2S WF2 A4S	C2S WF3 A4S	C2S FD5 A4S	C2S FD6 A4S	C2S FD7 A4S	Case
C3S WF1		0.0358	0.7076	0.0135	0.0088														C3S WF1
C3S WF2	>			0.0009	0.0019														C3S WF2
C3S WF3	?(<)			0.0001		0.0169													C3S WF3
C3S FD5	<	<	<		0.0781	0.0010													C3S FD5
C3S FD6	<	<		>		0.0110													C3S FD6
C3S FD7			<	>	>														C3S FD7
A1S WF1								id	id	id	id								A1S WF1
A1S WF2							id			id	id								A1S WF2
A1S WF3							id			id		id							A1S WF3
A1S FD5							id	id	id		id	id							A1S FD5
A1S FD6							id	id		id		id							A1S FD6
A1S FD7									id	id	id								A1S FD7
A4S WF1														0.1383	0.5933	0.4689	0.0129		A4S WF1
A4S WF2													?(>)			0.3159	0.0004		A4S WF2
A4S WF3													?(<)			0.5366		0.0607	A4S WF3
A4S FD5													?(<)	?(<)	?(<)		0.7330	0.9065	A4S FD5
A4S FD6													<	<		?(<)		0.0966	A4S FD6
A4S FD7															<	?(>)	>		A4S FD7
Case	C3S WF1	C3S WF2	C3S WF3	C3S FD5	C3S FD6	C3S FD7	A1S WF1	A1S WF2	A1S WF3	A1S FD5	A1S FD6	A1S FD7	A4S WF1	A4S WF2	A4S WF3	A4S FD5	A4S FD6	A4S FD7	Case

Table E109. Results of Hypothesis Test 2 for CD STFI, comparing furnishes continued.

Case	A5S WF1	A5S WF2	A5S WF3	A5S FD5	A5S FD6	A5S FD7	C1 WF1	C1 WF2	C1 WF3	C1 FD5	C1 FD6	C1 FD7	C2 WF1	C2 WF2	C2 WF3	C2 FD5	C2 FD6	C2 FD7	Case
A5S WF1		id	id	id	id														A5S WF1
A5S WF2	id			0.0002	0.0014														A5S WF2
A5S WF3	id			id		id													A5S WF3
A5S FD5	id	<	id		0.9783	0.0455													A5S FD5
A5S FD6	id	<		?(<)		0.1168													A5S FD6
A5S FD7			id	>	?(>)														A5S FD7
C1 WF1								0.0095	0.2672	0.0890	0.5010								C1 WF1
C1 WF2							>			0.0017	0.0151								C1 WF2
C1 WF3							?(>)			0.0225		0.0543							C1 WF3
C1 FD5							<	<	<		0.0380	0.2549							C1 FD5
C1 FD6							?(>)	<		>		0.0671							C1 FD6
C1 FD7									<	?(>)	<								C1 FD7
C2 WF1														0.3386	0.8748	0.0852	0.1039		C2 WF1
C2 WF2													?(>)			0.0057	0.0007		C2 WF2
C2 WF3													?(<)			0.0268		0.0039	C2 WF3
C2 FD5													<	<	<		0.6597	0.2511	C2 FD5
C2 FD6													?(<)	<		?(>)		0.1735	C2 FD6
C2 FD7															<	?(>)	?(>)		C2 FD7
Case	A5S WF1 C3	A5S WF2 C3	A5S WF3 C3	A5S FD5 C3	A5S FD6 C3	A5S FD7 C3	C1 WF1 A1	C1 WF2 A1	C1 WF3 A1	C1 FD5 A1	C1 FD6 A1	C1 FD7 A1	C2 WF1 A2	C2 WF2 A2	C2 WF3 A2	C2 FD5 A2	C2 FD6 A2	C2 FD7 A2	Case
C3 WF1		0.0994	0.0903	0.1280	0.3829														C3 WF1
C3 WF2	>			0.0036	0.1856														C3 WF2
C3 WF3	>			0.0024		0.0093													C3 WF3
C3 FD5	?(<)	<	<		0.0025	0.0193													C3 FD5
C3 FD6	?(>)	?(<)		>		0.0652													C3 FD6
C3 FD7			<	>	<														C3 FD7
A1 WF1								0.1888	0.0577	0.4004	0.5418								A1 WF1
A1 WF2							?(<)			0.5627	0.7786								A1 WF2
A1 WF3							<			0.6536		id							A1 WF3
A1 FD5							?(<)	?(<)	?(<)		0.4611	id							A1 FD5
A1 FD6							?(<)	?(>)		?(>)		id							A1 FD6
A1 FD7									id	id	id								A1 FD7
A2 WF1														0.0348	0.7457	id	0.2461		A2 WF1
A2 WF2													>			id	0.0960		A2 WF2
A2 WF3													?(<)			id		id	A2 WF3
A2 FD5													id	id	id		id	id	A2 FD5
A2 FD6													?(<)	<		id		id	A2 FD6
A2 FD7															id	id	id		A2 FD7
Case	C3 WF1	C3 WF2	C3 WF3	C3 FD5	C3 FD6	C3 FD7	A1 WF1	A1 WF2	A1 WF3	A1 FD5	A1 FD6	A1 FD7	A2 WF1	A2 WF2	A2 WF3	A2 FD5	A2 FD6	A2 FD7	Case

Table E110. Results of Hypothesis Test 2 for CD STFI, comparing furnishes continued.

Case	A4 WF1	A4 WF2	A4 WF3	A4 FD5	A4 FD6	A4 FD7	A5 WF1	A5 WF2	A5 WF3	A5 FD5	A5 FD6	A5 FD7	A6 WF1	A6 WF2	A6 WF3	A6 FD5	A6 FD6	A6 FD7	Case
A4 WF1		0.5895	0.8612	0.0005	0.3195														A4 WF1
A4 WF2	?(>)			0.0000	0.1944														A4 WF2
A4 WF3	?(>)			0.0018		0.1985													A4 WF3
A4 FD5	<	<	<		0.0272	0.0043													A4 FD5
A4 FD6	?(<)	?(<)		>		0.9086													A4 FD6
A4 FD7			?(<)	>	?(>)														A4 FD7
A5 WF1								0.3396	0.0817	0.0008	0.1594								A5 WF1
A5 WF2							?(<)			0.0001	0.3826								A5 WF2
A5 WF3							<			0.0002		0.5496							A5 WF3
A5 FD5							<	<	<		0.0061	0.0037							A5 FD5
A5 FD6							?(<)	?(<)		>		0.7243							A5 FD6
A5 FD7									?(<)	>	?(<)								A5 FD7
A6 WF1														0.1760	0.3656	id	0.0621		A6 WF1
A6 WF2													?(>)			id	0.0179		A6 WF2
A6 WF3													?(<)			id		0.7307	A6 WF3
A6 FD5													id	id	id		id	id	A6 FD5
A6 FD6													<	<		id		0.2262	A6 FD6
A6 FD7															?(<)	id	?(>)		A6 FD7
Case	A4 WF1 A5F	A4 WF2 A5F	A4 WF3 A5F	A4 FD5 A5F	A4 FD6 A5F	A4 FD7 A5F	A5 WF1 A4H	A5 WF2 A4H	A5 WF3 A4H	A5 FD5 A4H	A5 FD6 A4H	A5 FD7 A4H	A6 WF1 A5H	A6 WF2 A5H	A6 WF3 A5H	A6 FD5 A5H	A6 FD6 A5H	A6 FD7 A5H	Case
A5F WF1		id	id	id	0.0032														A5F WF1
A5F WF2	id			id	id														A5F WF2
A5F WF3	id			id		id													A5F WF3
A5F FD5	id	id	id		id	id													A5F FD5
A5F FD6	<	id		id		id													A5F FD6
A5F FD7			id	id	id														A5F FD7
A4H WF1								0.9729	id	id	0.9894								A4H WF1
A4H WF2							?(>)			id	0.9756								A4H WF2
A4H WF3							id			id		id							A4H WF3
A4H FD5							id	id	id		id	id							A4H FD5
A4H FD6							?(>)	?(<)		id		id							A4H FD6
A4H FD7									id	id	id								A4H FD7
A5H WF1														id	id	id	0.2075		A5H WF1
A5H WF2													id			id	id		A5H WF2
A5H WF3													id			id		id	A5H WF3
A5H FD5													id	id	id		id	id	A5H FD5
A5H FD6													?(<)	id		id		id	A5H FD6
A5H FD7															id	id	id		A5H FD7
Case	A5F WF1	A5F WF2	A5F WF3	A5F FD5	A5F FD6	A5F FD7	A4H WF1	A4H WF2	A4H WF3	A4H FD5	A4H FD6	A4H FD7	A5H WF1	A5H WF2	A5H WF3	A5H FD5	A5H FD6	A5H FD7	Case

Table E111. Results of Hypothesis Test 3 for CD STFI and furnish WF1.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		0.0017	0.0978	0.0053	0.0005	0.0000	0.0002	0.0471	0.0000	0.0291	0.1213	0.0032	id	0.0006	0.0175	0.0007	0.0004	0.0001	0.0002	0.0001	0.0001	id	0.0000	0.0024	0.0002	Con
D1	>		0.4262	0.3359	0.0169			0.4740			0.9326			0.2451			0.0019										D1
D2	>	?(>)				0.2713			0.3089						0.4328			0.4295									D2
D3	>	?(>)					0.0172			0.1087						0.3347											D3
D4	>	>				0.0364	0.3020					0.0627							0.4038			id		0.6094			D4
D5	>		?(>)		>								id							0.1549			0.0061		0.6899		D5
D6	>			>	?(>)																0.4618						D6
C1S	>	?(>)							0.3012	0.7487	0.5405			0.7541													C1S
C2S	>		?(>)					?(>)							0.1088												C2S
C3S	>			?(>)				?(>)								0.3626											C3S
A1S	?(>)	?(>)						?(<)				0.8910					0.2004										A1S
A4S	>				<						?(>)		id						0.0225								A4S
A5S	id					id						id								id							A5S
C1	>	?(>)						?(<)							0.0137	0.4006	0.0045										C1
C2	>		?(>)						?(<)					>				0.9548									C2
C3	>			?(>)						?(<)				?(>)													C3
A1	>	>									?(>)			>				0.1883	0.1901								A1
A2	>		?(>)												?(>)		?(<)			0.0048							A2
A4	>				?(>)							>					?(<)			0.0172	0.3649	id		0.7142			A4
A5	>					?(>)							id					>	>				0.0017		0.1634		A5
A6	>						?(>)												?(>)								A6
A4F	id				id														id				id				A4F
A5F	>					<														<		id					A5F
A4H	>				?(>)														?(<)						0.0985		A4H
A5H	>					?(<)														?(<)				>			A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E112. Results of Hypothesis Test 3 for CD STFI and furnish WF2.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		0.0412	0.0000	0.0001	0.0002	0.0001	0.0000	0.0001	0.0000	0.0013	id	0.0002	0.0024	0.0001	0.0000	0.0001	0.0001	0.0000	0.0001	0.0001	0.0007	id	0.0003	0.0001	0.0076	Con
D1	>		0.2688	0.5342	0.8627			0.3433			id			0.2809			0.5480									D1
D2	>	?(>)				1.0000			0.0920						0.0635			0.0901								D2
D3	>	?(>)					0.1998			0.5830						0.9671										D3
D4	>	?(>)				0.0837	0.0785					0.0167							0.5883			id		0.5989		D4
D5	>		?(>)		>								0.0118							0.7235			0.0561		0.8103	D5
D6	>			?(>)	>																0.7884					D6
C1S	>	?(>)							0.1077	0.9927	id			0.7743												C1S
C2S	>		>					?(>)							0.9790											C2S
C3S	>			?(>)				?(<)								0.5757										C3S
A1S	id	id						id				id					id									A1S
A4S	>				<						id		0.1909						0.0025							A4S
A5S	>					<						?(>)								0.0170						A5S
C1	>	?(>)						?(>)							0.1367	0.3108	0.2905									C1
C2	>		>						?(<)					?(>)				0.6118								C2
C3	>			?(<)						?(<)				?(<)												C3
A1	>	?(>)									id			?(<)				0.0226	0.7669							A1
A2	>		>												?(<)		>			0.1331						A2
A4	>				?(>)							>					?(<)			0.2182	0.3518	id		0.9965		A4
A5	>					?(<)							>					?(<)	?(>)				0.0867		0.9397	A5
A6	>						?(<)												?(>)							A6
A4F	id				id														id				id			A4F
A5F	>					<														<		id				A5F
A4H	>				?(>)														?(<)						0.3174	A4H
A5H	>					?(<)														?(>)				?(>)		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E113. Results of Hypothesis Test 3 for CD STFI and furnish WF3.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		0.0000	0.0010	0.0024	0.0022	0.0006	0.0003	0.0840	0.0003	0.0000	id	0.0012	id	0.0005	0.0000	0.0002	0.0000	0.0006	0.0004	0.0000	0.0001	id	0.0027	0.0003	0.0000	Con
D1	>		0.2807	0.1873	0.0216			0.9283			id			0.4207			0.9647									D1
D2	>	?(<)				0.1567			0.0482						0.1973			0.2812								D2
D3	>	?(<)					0.0607			0.9236						0.1084										D3
D4	>	<				0.0148	0.0081					0.4806							0.0152			id		0.1196		D4
D5	>		?(>)		>								id							0.6727			0.1376		0.8359	D5
D6	>			>	>																0.3374					D6
C1S	>	?(>)							0.5169	0.5595	id			0.7119												C1S
C2S	>		>					?(>)							0.1257											C2S
C3S	>			?(<)				?(<)								0.0522										C3S
A1S	id	id						id				id					id									A1S
A4S	>				?(<)						id		id						0.0053							A4S
A5S	id					id						id								id						A5S
C1	>	?(<)						?(<)							0.2684	0.2639	0.4159									C1
C2	>		?(>)						?(<)					?(>)				0.5030								C2
C3	>			?(>)						>				?(>)												C3
A1	>	?(>)									id			?(>)				0.9018	0.5859							A1
A2	>		?(>)												?(<)		?(>)			0.4545						A2
A4	>				>							>					?(>)			0.9438	0.8777	id		0.1268		A4
A5	>					?(<)							id					?(>)	?(<)					0.1467		0.2898	A5
A6	>						?(<)												?(<)								A6
A4F	id				id														id				id				A4F
A5F	>					?(<)														?(<)		id					A5F
A4H	>				?(>)														?(<)						0.0506		A4H
A5H	>					?(>)														?(>)				>			A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E114. Results of Hypothesis Test 3 for CD STFI and furnish FD5.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		0.1767	0.1793	0.0586	0.6828	0.8681	0.0680	0.1163	0.0231	0.2261	id	0.7267	0.6192	id	0.0841	0.1821	0.2338	0.1994	0.4241	id	0.3030	id	id	id	id	Con
D1	?(>)		0.5277	0.9605	0.2100			0.9113			id			id			0.5819									D1
D2	?(>)	?(<)				0.0103			0.0868						0.2526			0.7444								D2
D3	>	?(>)					0.7252			0.1604						0.2248										D3
D4	?(>)	?(<)				0.4669	0.0856					0.8099							0.2572			id		id		D4
D5	?(>)		<		?(<)								0.3492							id			id		id	D5
D6	>			?(>)	>																0.7480					D6
C1S	?(>)	?(<)							0.2970	0.3565	id			id												C1S
C2S	>		>					?(>)							0.1838											C2S
C3S	?(>)			?(<)				?(<)								0.5232										C3S
A1S	id	id						id				id					id									A1S
A4S	?(>)				?(>)						id		0.5955						0.9360							A4S
A5S	?(<)					?(<)						?(<)								id						A5S
C1	id	id						id							id	id	id									C1
C2	>		?(>)						?(<)					id				0.7893							C2
C3	?(>)			?(<)						?(>)				id												C3
A1	?(>)	?(<)									id			id				0.8119	0.5087							A1
A2	?(>)		?(>)												?(<)		?(>)			id						A2
A4	?(>)				?(>)							?(<)					?(<)			id	0.4947	id		id		A4
A5	id					id							id					id	id				id		id	A5
A6	?(>)						?(<)												?(>)							A6
A4F	id				id														id				id			A4F
A5F	id					id														id		id				A5F
A4H	id				id														id						id	A4H
A5H	id					id														id				id		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E115. Results of Hypothesis Test 3 for CD STFI and furnish FD6.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		0.0005	0.0120	0.0048	0.0153	0.0001	0.0001	0.0697	0.0002	0.0001	id	0.0213	0.2335	0.0000	0.0000	0.0000	0.0007	0.0014	0.0031	0.0012	0.0019	id	0.0000	0.0010	0.0006	Con
D1	>		0.2539	0.3834	0.5927			0.2600			id			0.0901			0.0562									D1
D2	>	?(<)				0.4396			0.0257						0.1187			0.0309								D2
D3	>	?(<)					0.3854			0.9451						0.0258										D3
D4	>	?(<)				0.8586	0.5743					0.1040							0.1575			id		0.1316		D4
D5	>		?(>)		?(>)								0.0404							0.0555			0.0034		0.0295	D5
D6	>			?(>)	?(>)																0.5561					D6
C1S	>	?(<)							0.0584	0.4766	id			0.0926												C1S
C2S	>		>					>							0.0229											C2S
C3S	>			?(>)				?(>)								0.0019										C3S
A1S	id	id						id				id					id									A1S
A4S	>				?(<)						id		0.5321						0.0098							A4S
A5S	?(>)					<						?(<)								0.0033						A5S
C1	>	>						>							0.4913	0.1347	0.2400									C1
C2	>		?(>)						<					?(<)				0.1741								C2
C3	>			>						>				?(>)												C3
A1	>	>									id			?(>)				0.9611	0.7554							A1
A2	>		>												?(>)		?(>)			0.9602						A2
A4	>				?(>)							>					?(<)			0.7686	0.3975	id		0.9579		A4
A5	>					>							>					?(<)	?(>)				0.2565		0.8458	A5
A6	>						?(>)												?(<)							A6
A4F	id				id														id				id			A4F
A5F	>					>														?(<)		id				A5F
A4H	>				?(>)														?(<)						0.5151	A4H
A5H	>					>														?(>)				?(>)		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E116. Results of Hypothesis Test 3 for CD STFI and furnish FD7.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		id	0.0001	0.0013	0.0015	0.0000	id	0.0002	0.0375	0.0000	id	0.0007	0.0001	0.0000	0.0002	0.0000	0.0694	0.0006	0.0001	0.0014	0.0011	id	0.0002	0.0004	0.0024	Con
D1	id		id	id	id			id			id			id			id									D1
D2	>	id				0.1255			0.2183						0.9168			0.1759								D2
D3	>	id					id			0.7061						0.6686										D3
D4	>	id				0.8987	id					0.0417							0.0935			id		0.7900		D4
D5	>		?(<)		?(>)								0.0008							0.0656			0.3964		0.2870	D5
D6	id			id	id																id					D6
C1S	>	id							0.3025	0.9314	id			0.1789												C1S
C2S	>		?(<)					?(<)							0.2196											C2S
C3S	>			?(>)				?(>)								0.9211										C3S
A1S	id	id						id				id					id									A1S
A4S	>				<						id		0.9323						0.0067							A4S
A5S	>					<						?(>)								0.0180						A5S
C1	>	id						?(<)							0.0570	0.0365	0.2394									C1
C2	>		?(<)						?(>)					>				0.1566								C2
C3	>			?(>)						?(>)				>												C3
A1	>	id									id			?(>)				0.5727	0.9035							A1
A2	>		?(>)												?(>)		?(>)			0.8539						A2
A4	>				>							>					?(<)			0.4123	0.8375	id		0.0490		A4
A5	>					>							>					?(>)	?(>)				0.0467		0.3431	A5
A6	>						id												?(<)							A6
A4F	id				id														id				id			A4F
A5F	>					?(<)														<		id				A5F
A4H	>				?(<)														<						0.2159	A4H
A5H	>					?(>)														?(<)				?(>)		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E117. Results of Hypothesis Test 3 for CD STFI, comparing furnishes.

Case	Con WF1	Con WF2	Con WF3	Con FD5	Con FD6	Con FD7	D1 WF1	D1 WF2	D1 WF3	D1 FD5	D1 FD6	D1 FD7	D2 WF1	D2 WF2	D2 WF3	D2 FD5	D2 FD6	D2 FD7	Case
Con WF1		0.0003	0.0238	0.0455	0.0453														Con WF1
Con WF2	>			0.1148	0.0001														Con WF2
Con WF3	>			0.1540		0.2619													Con WF3
Con FD5	>	?(<)	?(>)		0.1095	0.2487													Con FD5
Con FD6	>	<		?(<)		0.1783													Con FD6
Con FD7			?(>)	?(<)	?(>)														Con FD7
D1 WF1								0.0490	0.0095	0.6753	0.6884								D1 WF1
D1 WF2							>			0.0507	0.0571								D1 WF2
D1 WF3							>			0.0824		id							D1 WF3
D1 FD5							?(<)	<	<		0.7829	id							D1 FD5
D1 FD6							?(<)	<		?(>)		id							D1 FD6
D1 FD7									id	id	id								D1 FD7
D2 WF1														0.2266	0.8146	0.2247	0.1684		D2 WF1
D2 WF2													?(>)			0.0001	0.0046		D2 WF2
D2 WF3													?(>)			0.0202		0.1583	D2 WF3
D2 FD5													?(<)	<	<		0.7954	0.0031	D2 FD5
D2 FD6													?(<)	<		?(>)		0.0574	D2 FD6
D2 FD7															?(<)	>	>		D2 FD7
Case	Con WF1 D3	Con WF2 D3	Con WF3 D3	Con FD5 D3	Con FD6 D3	Con FD7 D3	D1 WF1 D4	D1 WF2 D4	D1 WF3 D4	D1 FD5 D4	D1 FD6 D4	D1 FD7 D4	D2 WF1 D5	D2 WF2 D5	D2 WF3 D5	D2 FD5 D5	D2 FD6 D5	D2 FD7 D5	Case
D3 WF1		0.0057	0.1160	0.1614	0.0924														D3 WF1
D3 WF2	>			0.0016	0.0011														D3 WF2
D3 WF3	?(>)			0.0218		0.0704													D3 WF3
D3 FD5	?(<)	<	<		0.7157	0.2579													D3 FD5
D3 FD6	<	<		?(<)		0.1471													D3 FD6
D3 FD7			<	?(>)	?(>)														D3 FD7
D4 WF1								0.1520	0.0330	0.0021	0.0300								D4 WF1
D4 WF2							?(>)			0.0007	0.0143								D4 WF2
D4 WF3							<			0.0246		0.6483							D4 WF3
D4 FD5							<	<	<		0.1508	0.0128							D4 FD5
D4 FD6							<	<		?(>)		0.4634							D4 FD6
D4 FD7									?(<)	>	?(>)								D4 FD7
D5 WF1														0.2800	0.1563	0.0000	0.0000		D5 WF1
D5 WF2													?(>)			0.0000	0.0002		D5 WF2
D5 WF3													?(<)			0.0016		0.0105	D5 WF3
D5 FD5													<	<	<		0.0008	0.0002	D5 FD5
D5 FD6													<	<		>		0.0462	D5 FD6
D5 FD7															<	>	>		D5 FD7
Case	D3 WF1	D3 WF2	D3 WF3	D3 FD5	D3 FD6	D3 FD7	D4 WF1	D4 WF2	D4 WF3	D4 FD5	D4 FD6	D4 FD7	D5 WF1	D5 WF2	D5 WF3	D5 FD5	D5 FD6	D5 FD7	Case

Table E118. Results of Hypothesis Test 3 for CD STFI, comparing furnishes continued.

Case	D6 WF1	D6 WF2	D6 WF3	D6 FD5	D6 FD6	D6 FD7	C1S WF1	C1S WF2	C1S WF3	C1S FD5	C1S FD6	C1S FD7	C2S WF1	C2S WF2	C2S WF3	C2S FD5	C2S FD6	C2S FD7	Case
D6 WF1		0.0174	0.6890	0.0376	0.0008														D6 WF1
D6 WF2	>			0.0193	0.0002														D6 WF2
D6 WF3	?(>)			0.0311		id													D6 WF3
D6 FD5	<	<	<		0.9478	id													D6 FD5
D6 FD6	<	<		?(<)		id													D6 FD6
D6 FD7			id	id	id														D6 FD7
C1S WF1								0.2269	0.5566	0.3014	0.1941								C1S WF1
C1S WF2							?(>)			0.0055	0.0082								C1S WF2
C1S WF3							?(>)			0.0702		0.2998							C1S WF3
C1S FD5							?(<)	<	<		0.5481	0.1953							C1S FD5
C1S FD6							?(<)	<		?(<)		0.0989							C1S FD6
C1S FD7									?(<)	?(>)	>								C1S FD7
C2S WF1														0.0045	0.9428	0.0191	0.0037		C2S WF1
C2S WF2													>			0.0049	0.0010		C2S WF2
C2S WF3													?(<)			0.0249		0.0162	C2S WF3
C2S FD5													<	<	<		0.2226	0.4403	C2S FD5
C2S FD6													<	<		?(>)		0.0972	C2S FD6
C2S FD7															<	?(<)	<		C2S FD7
Case	D6 WF1 C3S	D6 WF2 C3S	D6 WF3 C3S	D6 FD5 C3S	D6 FD6 C3S	D6 FD7 C3S	C1S WF1 A1S	C1S WF2 A1S	C1S WF3 A1S	C1S FD5 A1S	C1S FD6 A1S	C1S FD7 A1S	C2S WF1 A4S	C2S WF2 A4S	C2S WF3 A4S	C2S FD5 A4S	C2S FD6 A4S	C2S FD7 A4S	Case
C3S WF1		0.0358	0.7076	0.0135	0.0088														C3S WF1
C3S WF2	>			0.0009	0.0019														C3S WF2
C3S WF3	?(<)			0.0001		0.0169													C3S WF3
C3S FD5	<	<	<		0.0781	0.0010													C3S FD5
C3S FD6	<	<		>		0.0110													C3S FD6
C3S FD7			<	>	>														C3S FD7
A1S WF1								id	id	id	id								A1S WF1
A1S WF2							id			id	id								A1S WF2
A1S WF3							id			id		id							A1S WF3
A1S FD5							id	id	id		id	id							A1S FD5
A1S FD6							id	id		id		id							A1S FD6
A1S FD7									id	id	id								A1S FD7
A4S WF1														0.1383	0.5933	0.4689	0.0129		A4S WF1
A4S WF2													?(>)			0.3159	0.0004		A4S WF2
A4S WF3													?(<)			0.5366		0.0607	A4S WF3
A4S FD5													?(<)	?(<)	?(<)		0.7330	0.9065	A4S FD5
A4S FD6													<	<		?(<)		0.0966	A4S FD6
A4S FD7															<	?(>)	>		A4S FD7
Case	C3S WF1	C3S WF2	C3S WF3	C3S FD5	C3S FD6	C3S FD7	A1S WF1	A1S WF2	A1S WF3	A1S FD5	A1S FD6	A1S FD7	A4S WF1	A4S WF2	A4S WF3	A4S FD5	A4S FD6	A4S FD7	Case

Table E119. Results of Hypothesis Test 3 for CD STFI, comparing furnishes continued.

Case	A5S WF1	A5S WF2	A5S WF3	A5S FD5	A5S FD6	A5S FD7	C1 WF1	C1 WF2	C1 WF3	C1 FD5	C1 FD6	C1 FD7	C2 WF1	C2 WF2	C2 WF3	C2 FD5	C2 FD6	C2 FD7	Case
A5S WF1		id	id	id	id														A5S WF1
A5S WF2	id			0.0002	0.0014														A5S WF2
A5S WF3	id			id		id													A5S WF3
A5S FD5	id	<	id		0.9783	0.0455													A5S FD5
A5S FD6	id	<		?(<)		0.1168													A5S FD6
A5S FD7			id	>	?(>)														A5S FD7
C1 WF1								0.0009	0.0670	id	0.7601								C1 WF1
C1 WF2							>			id	0.0005								C1 WF2
C1 WF3							>			id		0.0118							C1 WF3
C1 FD5							id	id	id		id	id							C1 FD5
C1 FD6							?(<)	<		id		0.1257							C1 FD6
C1 FD7									<	id	?(<)								C1 FD7
C2 WF1														0.0129	0.5491	0.0031	0.0030		C2 WF1
C2 WF2													>			0.0005	0.0002		C2 WF2
C2 WF3													?(<)			0.0029		0.0100	C2 WF3
C2 FD5													<	<	<		0.0613	0.0214	C2 FD5
C2 FD6													<	<		>		0.2981	C2 FD6
C2 FD7															<	>	?(>)		C2 FD7
Case	A5S WF1 C3	A5S WF2 C3	A5S WF3 C3	A5S FD5 C3	A5S FD6 C3	A5S FD7 C3	C1 WF1 A1	C1 WF2 A1	C1 WF3 A1	C1 FD5 A1	C1 FD6 A1	C1 FD7 A1	C2 WF1 A2	C2 WF2 A2	C2 WF3 A2	C2 FD5 A2	C2 FD6 A2	C2 FD7 A2	Case
C3 WF1		0.0081	0.0720	0.0049	0.9069														C3 WF1
C3 WF2	>			0.0003	0.0036														C3 WF2
C3 WF3	>			0.0002		0.0022													C3 WF3
C3 FD5	<	<	<		0.0005	0.0004													C3 FD5
C3 FD6	?(>)	<		>		0.0954													C3 FD6
C3 FD7			<	>	<														C3 FD7
A1 WF1								0.9575	0.0947	0.0246	0.0325								A1 WF1
A1 WF2							?(<)			0.0198	0.0265								A1 WF2
A1 WF3							<			0.1068		0.2919							A1 WF3
A1 FD5							<	<	?(<)		0.0429	0.0818							A1 FD5
A1 FD6							<	<		>		0.8070							A1 FD6
A1 FD7									?(<)	>	?(<)								A1 FD7
A2 WF1														0.0010	0.2623	0.0226	0.1896		A2 WF1
A2 WF2													>			0.0066	0.0217		A2 WF2
A2 WF3													?(<)			0.0262		0.3164	A2 WF3
A2 FD5													<	<	<		0.0537	0.0351	A2 FD5
A2 FD6													?(<)	<		>		0.8167	A2 FD6
A2 FD7															?(<)	>	?(>)		A2 FD7
Case	C3 WF1	C3 WF2	C3 WF3	C3 FD5	C3 FD6	C3 FD7	A1 WF1	A1 WF2	A1 WF3	A1 FD5	A1 FD6	A1 FD7	A2 WF1	A2 WF2	A2 WF3	A2 FD5	A2 FD6	A2 FD7	Case

Table E120. Results of Hypothesis Test 3 for CD STFI, comparing furnishes continued.

Case	A4 WF1	A4 WF2	A4 WF3	A4 FD5	A4 FD6	A4 FD7	A5 WF1	A5 WF2	A5 WF3	A5 FD5	A5 FD6	A5 FD7	A6 WF1	A6 WF2	A6 WF3	A6 FD5	A6 FD6	A6 FD7	Case
A4 WF1		0.1730	0.9184	0.0001	0.1726														A4 WF1
A4 WF2	?(>)			0.0000	0.0637														A4 WF2
A4 WF3	?(<)			0.0005		0.0473													A4 WF3
A4 FD5	<	<	<		0.0218	0.0011													A4 FD5
A4 FD6	?(<)	<		>		0.9706													A4 FD6
A4 FD7			<	>	?(>)														A4 FD7
A5 WF1								0.5970	0.0042	id	0.0180								A5 WF1
A5 WF2							?(<)			id	0.0275								A5 WF2
A5 WF3							<			id		0.4211							A5 WF3
A5 FD5							id	id	id		id	id							A5 FD5
A5 FD6							<	<		id		0.6721							A5 FD6
A5 FD7									?(<)	id	?(>)								A5 FD7
A6 WF1														0.1772	0.1106	0.2081	0.0101		A6 WF1
A6 WF2													?(>)			0.1796	0.0025		A6 WF2
A6 WF3													?(<)			0.2379		0.0723	A6 WF3
A6 FD5													?(<)	?(<)	?(<)		0.6257	0.4239	A6 FD5
A6 FD6													<	<		?(>)		0.3339	A6 FD6
A6 FD7															<	?(>)	?(>)		A6 FD7
Case	A4 WF1 A5F	A4 WF2 A5F	A4 WF3 A5F	A4 FD5 A5F	A4 FD6 A5F	A4 FD7 A5F	A5 WF1 A4H	A5 WF2 A4H	A5 WF3 A4H	A5 FD5 A4H	A5 FD6 A4H	A5 FD7 A4H	A6 WF1 A5H	A6 WF2 A5H	A6 WF3 A5H	A6 FD5 A5H	A6 FD6 A5H	A6 FD7 A5H	Case
A5F WF1		0.3503	0.1818	id	0.0004														A5F WF1
A5F WF2	?(>)			id	0.0055														A5F WF2
A5F WF3	?(<)			id		0.0163													A5F WF3
A5F FD5	id	id	id		id	id													A5F FD5
A5F FD6	<	<		id		0.0829													A5F FD6
A5F FD7			<	id	<														A5F FD7
A4H WF1								0.1288	0.1782	id	0.1097								A4H WF1
A4H WF2							?(>)			id	0.0184								A4H WF2
A4H WF3							?(<)			id		0.0340							A4H WF3
A4H FD5							id	id	id		id	id							A4H FD5
A4H FD6							?(<)	<		id		0.1315							A4H FD6
A4H FD7									<	id	?(<)								A4H FD7
A5H WF1														0.3889	0.1959	id	0.0381		A5H WF1
A5H WF2													?(>)			id	0.0244		A5H WF2
A5H WF3													?(<)			id		0.0623	A5H WF3
A5H FD5													id	id	id		id	id	A5H FD5
A5H FD6													<	<		id		0.4253	A5H FD6
A5H FD7															<	id	?(<)		A5H FD7
Case	A5F WF1	A5F WF2	A5F WF3	A5F FD5	A5F FD6	A5F FD7	A4H WF1	A4H WF2	A4H WF3	A4H FD5	A4H FD6	A4H FD7	A5H WF1	A5H WF2	A5H WF3	A5H FD5	A5H FD6	A5H FD7	Case

Table E121. Results of Hypothesis Test 0 for Density and furnish WF1.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con																										Con
D1	>																									D1
D2	>	>																								D2
D3	>	>																								D3
D4	>	?																								D4
D5	>		?		>																					D5
D6	>			>	>																					D6
C1S	>	?																								C1S
C2S	>		>					>																		C2S
C3S	>			?				?																		C3S
A1S	>	?						?																		A1S
A4S	>				?						?															A4S
A5S	id					id						id														A5S
C1	>	>						?																		C1
C2	>		?						?					?												C2
C3	>			?						?				?												C3
A1	>	>									>			?												A1
A2	>		>												?		?									A2
A4	>				>							>					?									A4
A5	>					>							id					?	?							A5
A6	>						?												?							A6
A4F	id				id														id							A4F
A5F	>					?														<		id				A5F
A4H	?				?														?							A4H
A5H	>					<														<				?		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E122. Results of Hypothesis Test 0 for Density and furnish WF2.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con																										Con
D1	>																									D1
D2	>	>																								D2
D3	>	?																								D3
D4	>	<																								D4
D5	>		?		>																					D5
D6	>			<	>																					D6
C1S	>	?																								C1S
C2S	>		>					>																		C2S
C3S	>			>				?																		C3S
A1S	id	id						id																		A1S
A4S	>				<						id															A4S
A5S	>					<						>														A5S
C1	>	>						?																		C1
C2	>		?						<					?												C2
C3	>			?						<				?												C3
A1	>	>									id			?												A1
A2	>		?												?		?									A2
A4	>				>							>					?									A4
A5	>					?							>					?	?							A5
A6	>						>												?							A6
A4F	id				id														id							A4F
A5F	>					<														<		id				A5F
A4H	?				?														?							A4H
A5H	>					?														?				?		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E123. Results of Hypothesis Test 0 for Density and furnish WF3.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con																										Con
D1	>																									D1
D2	>	>																								D2
D3	>	>																								D3
D4	>	?																								D4
D5	>		?		>																					D5
D6	>			<	?																					D6
C1S	>	>																								C1S
C2S	>		>					>																		C2S
C3S	>			?				?																		C3S
A1S	id	id						id																		A1S
A4S	>				?						id															A4S
A5S	?					?						?														A5S
C1	>	>						?																		C1
C2	>		>						?					?												C2
C3	>			?						>				?												C3
A1	>	?									id			?												A1
A2	>		?												<		?									A2
A4	>				>							>					?									A4
A5	>					?							?					>	?							A5
A6	>						>												?							A6
A4F	id				id														id							A4F
A5F	>					<														<		id				A5F
A4H	>				?														?							A4H
A5H	>					<														<				?		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E124. Results of Hypothesis Test 0 for Density and furnish FD5.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con																										Con
D1	>																									D1
D2	>	?																								D2
D3	>	>																								D3
D4	>	<																								D4
D5	>		?		>																					D5
D6	>			<	>																					D6
C1S	>	>																								C1S
C2S	>		>					?																		C2S
C3S	>			?				<																		C3S
A1S	id	id						id																		A1S
A4S	>				?						id															A4S
A5S	>					<						>														A5S
C1	>	>						?																		C1
C2	>		>						?					?												C2
C3	>			?						?				?												C3
A1	>	?									id			?												A1
A2	>		?												?		?									A2
A4	>				?							?					?									A4
A5	>					?							>					?	?							A5
A6	>						?												?							A6
A4F	id				id														id							A4F
A5F	id					id														id		id				A5F
A4H	id				id														id							A4H
A5H	id					id														id				id		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E125. Results of Hypothesis Test 0 for Density and furnish FD6.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con																										Con
D1	>																									D1
D2	>	>																								D2
D3	>	>																								D3
D4	>	<																								D4
D5	>		?		>																					D5
D6	>			<	>																					D6
C1S	>	?																								C1S
C2S	>		>					>																		C2S
C3S	>			>				?																		C3S
A1S	id	id						id																		A1S
A4S	>				?						id															A4S
A5S	>					<						?														A5S
C1	>	>						?																		C1
C2	>		?						<					?												C2
C3	>			>						>				?												C3
A1	>	>									id			?												A1
A2	>		?												?		?									A2
A4	>				>							>					?									A4
A5	>					?							>					?	?							A5
A6	>						>												?							A6
A4F	id				id														id							A4F
A5F	>					?														?		id				A5F
A4H	>				>														?							A4H
A5H	>					?														?				?		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E126. Results of Hypothesis Test 0 for Density and furnish FD7.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con																										Con
D1	>																									D1
D2	>	?																								D2
D3	>	?																								D3
D4	>	?																								D4
D5	>		?		>																					D5
D6	>			?	>																					D6
C1S	>	?																								C1S
C2S	>		>					>																		C2S
C3S	>			?				?																		C3S
A1S	id	id						id																		A1S
A4S	>				?						id															A4S
A5S	>					<						?														A5S
C1	>	?						?																		C1
C2	>		?						?					?												C2
C3	>			?						?				?												C3
A1	>	?									id			?												A1
A2	>		<												?		<									A2
A4	>				>							>					?									A4
A5	>					<							?					<	<							A5
A6	>						>												?							A6
A4F	id				id														id							A4F
A5F	>					>														>		id				A5F
A4H	>				>														?							A4H
A5H	>					>														>				>		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E127. Results of Hypothesis Test 0 for Density, comparing furnishes.

Case	Con WF1	Con WF2	Con WF3	Con FD5	Con FD6	Con FD7	D1 WF1	D1 WF2	D1 WF3	D1 FD5	D1 FD6	D1 FD7	D2 WF1	D2 WF2	D2 WF3	D2 FD5	D2 FD6	D2 FD7	Case
Con WF1																			Con WF1
Con WF2	>																		Con WF2
Con WF3	>																		Con WF3
Con FD5	>	>	>																Con FD5
Con FD6	>	<		<															Con FD6
Con FD7			>	<	>														Con FD7
D1 WF1																			D1 WF1
D1 WF2							?												D1 WF2
D1 WF3							?												D1 WF3
D1 FD5							?	?	?										D1 FD5
D1 FD6							?	?		?									D1 FD6
D1 FD7									?	?	?								D1 FD7
D2 WF1																			D2 WF1
D2 WF2													>						D2 WF2
D2 WF3													?						D2 WF3
D2 FD5													?	<	<				D2 FD5
D2 FD6													?	<		?			D2 FD6
D2 FD7															?	>	?		D2 FD7

Case	Con WF1 D3	Con WF2 D3	Con WF3 D3	Con FD5 D3	Con FD6 D3	Con FD7 D3	D1 WF1 D4	D1 WF2 D4	D1 WF3 D4	D1 FD5 D4	D1 FD6 D4	D1 FD7 D4	D2 WF1 D5	D2 WF2 D5	D2 WF3 D5	D2 FD5 D5	D2 FD6 D5	D2 FD7 D5	Case
D3 WF1																			D3 WF1
D3 WF2	?																		D3 WF2
D3 WF3	>																		D3 WF3
D3 FD5	?	?	<																D3 FD5
D3 FD6	<	<		<															D3 FD6
D3 FD7			?	?	>														D3 FD7
D4 WF1																			D4 WF1
D4 WF2							?												D4 WF2
D4 WF3							?												D4 WF3
D4 FD5							?	<	<										D4 FD5
D4 FD6							<	<		?									D4 FD6
D4 FD7									<	?	>								D4 FD7
D5 WF1																			D5 WF1
D5 WF2													?						D5 WF2
D5 WF3													?						D5 WF3
D5 FD5													<	<	<				D5 FD5
D5 FD6													<	<		?			D5 FD6
D5 FD7															<	?	?		D5 FD7
Case	D3 WF1	D3 WF2	D3 WF3	D3 FD5	D3 FD6	D3 FD7	D4 WF1	D4 WF2	D4 WF3	D4 FD5	D4 FD6	D4 FD7	D5 WF1	D5 WF2	D5 WF3	D5 FD5	D5 FD6	D5 FD7	Case

Table E128. Results of Hypothesis Test 0 for Density, comparing furnishes continued.

Case	D6 WF1	D6 WF2	D6 WF3	D6 FD5	D6 FD6	D6 FD7	C1S WF1	C1S WF2	C1S WF3	C1S FD5	C1S FD6	C1S FD7	C2S WF1	C2S WF2	C2S WF3	C2S FD5	C2S FD6	C2S FD7	Case
D6 WF1																			D6 WF1
D6 WF2	<																		D6 WF2
D6 WF3	<																		D6 WF3
D6 FD5	<	<	<																D6 FD5
D6 FD6	<	<		?															D6 FD6
D6 FD7			?	>	>														D6 FD7
C1S WF1																			C1S WF1
C1S WF2							?												C1S WF2
C1S WF3							?												C1S WF3
C1S FD5							?	?	?										C1S FD5
C1S FD6							?	?		?									C1S FD6
C1S FD7									?	>	>								C1S FD7
C2S WF1																			C2S WF1
C2S WF2													>						C2S WF2
C2S WF3													>						C2S WF3
C2S FD5													<	<	<				C2S FD5
C2S FD6													?	?		>			C2S FD6
C2S FD7															?	>	?		C2S FD7
Case	D6 WF1 C3S	D6 WF2 C3S	D6 WF3 C3S	D6 FD5 C3S	D6 FD6 C3S	D6 FD7 C3S	C1S WF1 A1S	C1S WF2 A1S	C1S WF3 A1S	C1S FD5 A1S	C1S FD6 A1S	C1S FD7 A1S	C2S WF1 A4S	C2S WF2 A4S	C2S WF3 A4S	C2S FD5 A4S	C2S FD6 A4S	C2S FD7 A4S	Case
C3S WF1																			C3S WF1
C3S WF2	?																		C3S WF2
C3S WF3	?																		C3S WF3
C3S FD5	<	<	?																C3S FD5
C3S FD6	?	<		>															C3S FD6
C3S FD7			?	>	?														C3S FD7
A1S WF1																			A1S WF1
A1S WF2							id												A1S WF2
A1S WF3							id												A1S WF3
A1S FD5							id	id	id										A1S FD5
A1S FD6							id	id		id									A1S FD6
A1S FD7									id	id	id								A1S FD7
A4S WF1																			A4S WF1
A4S WF2													<						A4S WF2
A4S WF3													?						A4S WF3
A4S FD5													<	<	<				A4S FD5
A4S FD6													<	<		?			A4S FD6
A4S FD7															<	?	?		A4S FD7
Case	C3S WF1	C3S WF2	C3S WF3	C3S FD5	C3S FD6	C3S FD7	A1S WF1	A1S WF2	A1S WF3	A1S FD5	A1S FD6	A1S FD7	A4S WF1	A4S WF2	A4S WF3	A4S FD5	A4S FD6	A4S FD7	Case

Table E129. Results of Hypothesis Test 0 for Density, comparing furnishes continued.

Case	A5S WF1	A5S WF2	A5S WF3	A5S FD5	A5S FD6	A5S FD7	C1 WF1	C1 WF2	C1 WF3	C1 FD5	C1 FD6	C1 FD7	C2 WF1	C2 WF2	C2 WF3	C2 FD5	C2 FD6	C2 FD7	Case
A5S WF1																			A5S WF1
A5S WF2	id																		A5S WF2
A5S WF3	id																		A5S WF3
A5S FD5	id	?	?																A5S FD5
A5S FD6	id	<		?															A5S FD6
A5S FD7			?	<	?														A5S FD7
C1 WF1																			C1 WF1
C1 WF2							?												C1 WF2
C1 WF3							?												C1 WF3
C1 FD5							?	?	?										C1 FD5
C1 FD6							?	?		?									C1 FD6
C1 FD7									?	?	?								C1 FD7
C2 WF1																			C2 WF1
C2 WF2													?						C2 WF2
C2 WF3													?						C2 WF3
C2 FD5													?	<	<				C2 FD5
C2 FD6													?	<		?			C2 FD6
C2 FD7															?	?	?		C2 FD7
Case	A5S WF1 C3	A5S WF2 C3	A5S WF3 C3	A5S FD5 C3	A5S FD6 C3	A5S FD7 C3	C1 WF1 A1	C1 WF2 A1	C1 WF3 A1	C1 FD5 A1	C1 FD6 A1	C1 FD7 A1	C2 WF1 A2	C2 WF2 A2	C2 WF3 A2	C2 FD5 A2	C2 FD6 A2	C2 FD7 A2	Case
C3 WF1																			C3 WF1
C3 WF2	?																		C3 WF2
C3 WF3	?																		C3 WF3
C3 FD5	?	?	?																C3 FD5
C3 FD6	?	?		?															C3 FD6
C3 FD7			?	?	?														C3 FD7
A1 WF1																			A1 WF1
A1 WF2							?												A1 WF2
A1 WF3							<												A1 WF3
A1 FD5							<	<	?										A1 FD5
A1 FD6							?	?		>									A1 FD6
A1 FD7									?	>	?								A1 FD7
A2 WF1																			A2 WF1
A2 WF2													?						A2 WF2
A2 WF3													<						A2 WF3
A2 FD5													<	?	?				A2 FD5
A2 FD6													<	?		?			A2 FD6
A2 FD7															?	?	?		A2 FD7
Case	C3 WF1	C3 WF2	C3 WF3	C3 FD5	C3 FD6	C3 FD7	A1 WF1	A1 WF2	A1 WF3	A1 FD5	A1 FD6	A1 FD7	A2 WF1	A2 WF2	A2 WF3	A2 FD5	A2 FD6	A2 FD7	Case

Table E130. Results of Hypothesis Test 0 for Density, comparing furnishes continued.

Case	A4 WF1	A4 WF2	A4 WF3	A4 FD5	A4 FD6	A4 FD7	A5 WF1	A5 WF2	A5 WF3	A5 FD5	A5 FD6	A5 FD7	A6 WF1	A6 WF2	A6 WF3	A6 FD5	A6 FD6	A6 FD7	Case
A4 WF1																			A4 WF1
A4 WF2	?																		A4 WF2
A4 WF3	?																		A4 WF3
A4 FD5	<	<	<																A4 FD5
A4 FD6	?	?		?															A4 FD6
A4 FD7			?	>	?														A4 FD7
A5 WF1																			A5 WF1
A5 WF2							?												A5 WF2
A5 WF3							?												A5 WF3
A5 FD5							<	<	<										A5 FD5
A5 FD6							?	?		?									A5 FD6
A5 FD7									<	?	<								A5 FD7
A6 WF1																			A6 WF1
A6 WF2													?						A6 WF2
A6 WF3													?						A6 WF3
A6 FD5													?	<	<				A6 FD5
A6 FD6													?	?		>			A6 FD6
A6 FD7															?	>	?		A6 FD7
Case	A4 WF1	A4 WF2	A4 WF3	A4 FD5	A4 FD6	A4 FD7	A5 WF1	A5 WF2	A5 WF3	A5 FD5	A5 FD6	A5 FD7	A6 WF1	A6 WF2	A6 WF3	A6 FD5	A6 FD6	A6 FD7	Case
	A5F	A5F	A5F	A5F	A5F	A5F	A4H	A4H	A4H	A4H	A4H	A4H	A5H	A5H	A5H	A5H	A5H	A5H	
A5F WF1																			A5F WF1
A5F WF2	?																		A5F WF2
A5F WF3	?																		A5F WF3
A5F FD5	id	id	id																A5F FD5
A5F FD6	?	?		id															A5F FD6
A5F FD7			?	id	?														A5F FD7
A4H WF1																			A4H WF1
A4H WF2							?												A4H WF2
A4H WF3							?												A4H WF3
A4H FD5							id	id	id										A4H FD5
A4H FD6							?	?		id									A4H FD6
A4H FD7									?	id	?								A4H FD7
A5H WF1																			A5H WF1
A5H WF2													?						A5H WF2
A5H WF3													<						A5H WF3
A5H FD5													id	id	id				A5H FD5
A5H FD6													?	?		id			A5H FD6
A5H FD7															>	id	?		A5H FD7
Case	A5F WF1	A5F WF2	A5F WF3	A5F FD5	A5F FD6	A5F FD7	A4H WF1	A4H WF2	A4H WF3	A4H FD5	A4H FD6	A4H FD7	A5H WF1	A5H WF2	A5H WF3	A5H FD5	A5H FD6	A5H FD7	Case

Table E131. Results of Hypothesis Test 1 for Density and furnish WF1.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		0.0000	0.0001	0.0000	0.0000	<.0001	0.0000	0.0000	<.0001	0.0003	0.0008	<.0001	id	<.0001	0.0006	<.0001	0.0000	0.0000	0.0000	0.0003	0.0000	id	0.0000	0.9939	id	Con
D1	>		0.0006	0.0003	1.0000			0.0720			0.4725			0.0014			0.0103									D1
D2	>	>				0.0325			0.0007						0.1764			0.0020								D2
D3	>	>					0.0006			0.0519						0.2615										D3
D4	>	?(>)				0.0001	0.0000					0.5748							0.0363			id		0.9995		D4
D5	>		>		>								id							0.4861			0.2398		id	D5
D6	>			>	>																0.0450					D6
C1S	>	>							0.0075	0.0350	0.2800			0.0943												C1S
C2S	>		>					>							0.5122											C2S
C3S	>			>				>								0.4630										C3S
A1S	>	?(>)						?(<)				0.6879					0.0201									A1S
A4S	>				?(>)						?(<)		id						0.0499							A4S
A5S	id					id						id								id						A5S
C1	>	>						>							0.3731	0.7094	0.4259									C1
C2	>		?(>)						?(>)					?(>)				0.5155								C2
C3	>			?(>)						?(<)				?(<)												C3
A1	>	>									>			?(>)				0.7003	0.3271							A1
A2	>		>												?(<)		?(<)			0.9107						A2
A4	>				>							>					?(<)			0.5076	0.6371	id		0.9984		A4
A5	>					?(>)							id					?(>)	?(>)					0.2704		id	A5
A6	>						<												?(<)							A6
A4F	id				id														id				id			A4F
A5F	>					?(<)														?(<)		id				A5F
A4H	?(>)				?(>)														?(<)						id	A4H
A5H	id					id														id				id		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E132. Results of Hypothesis Test 1 for Density and furnish WF2.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		0.0000	0.0000	<.0001	<.0001	<.0001	<.0001	0.0000	<.0001	<.0001	id	<.0001	<.0001	0.0001	0.0000	<.0001	0.0000	<.0001	0.0026	0.0004	0.0000	id	id	0.9960	id	Con
D1	>		0.0001	0.0156	0.0191			0.0773			id			0.1826			0.0003									D1
D2	>	>				0.0057			0.0001						0.3033			0.6248								D2
D3	>	>					0.0014			0.0005						0.9516										D3
D4	>	<				<.0001	0.0002					0.0000							0.0949			id		0.9998		D4
D5	>		<		>								err							0.6025			id		id	D5
D6	>			<	>																0.0040					D6
C1S	>	>							0.0002	0.0440	id			0.5972												C1S
C2S	>		>					>							0.0301											C2S
C3S	>			>				>								0.0361										C3S
A1S	id	id						id				id					id									A1S
A4S	>				<						id		0.0005						0.0486							A4S
A5S	>					<						>								0.0439						A5S
C1	>	?(>)						?(>)							0.4217	0.6133	0.6307									C1
C2	>		?(>)						<					?(>)				0.2116								C2
C3	>			?(>)						<				?(<)												C3
A1	>	>									id			?(>)				0.5880	0.9584							A1
A2	>		?(<)												?(<)		?(<)			0.9678						A2
A4	>				>							>					?(>)			0.8425	0.8847	id		0.9974		A4
A5	>					?(>)							>					?(<)	?(<)				id		id	A5
A6	>						>												?(>)							A6
A4F	id				id														id				id			A4F
A5F	id					id														id		id				A5F
A4H	?(>)				?(>)														?(<)						id	A4H
A5H	id					id														id				id		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E133. Results of Hypothesis Test 1 for Density and furnish WF3.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		0.0000	0.0000	0.0000	<.0001	<.0001	0.0000	0.0000	<.0001	0.0000	id	<.0001	0.0587	0.0000	<.0001	0.0029	<.0001	<.0001	0.0027	0.0027	0.0001	id	id	0.0000	id	Con
D1	>		0.0027	0.0017	0.1327			0.0013			id			0.0005			0.0124									D1
D2	>	>				0.0293			0.0000						0.0003			0.0628								D2
D3	>	>					0.0028			0.0069						0.5603										D3
D4	>	?(<)				<.0001	0.0680					0.0061							0.0959			id		0.8079		D4
D5	>		>		>								0.0714							0.9075			id		id	D5
D6	>			<	>																0.0269					D6
C1S	>	>							0.0014	0.0053	id			0.8054												C1S
C2S	>		>					>							0.0623											C2S
C3S	>			<				<								0.2561										C3S
A1S	id	id						id				id					id									A1S
A4S	>				<						id		0.4204						0.0559							A4S
A5S	>					<						?(<)								0.0432						A5S
C1	>	>						?(>)							0.0080	0.7279	0.1767									C1
C2	>		>						<					>				<.0001								C2
C3	>			?(>)						?(>)				?(>)												C3
A1	>	>									id			?(<)				0.1944	0.3626							A1
A2	>		<												<		?(<)			0.3174						A2
A4	>				>							>					?(>)			0.7963	0.9377	id		0.1319		A4
A5	>					?(>)							>					?(>)	?(<)					id		id	A5
A6	>						>												?(<)							A6
A4F	id				id														id				id			A4F
A5F	id					id														id		id				A5F
A4H	>				?(>)														?(<)						id	A4H
A5H	id					id														id				id		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E134. Results of Hypothesis Test 1 for Density and furnish FD5.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		<.0001	<.0001	<.0001	0.0001	<.0001	<.0001	<.0001	<.0001	<.0001	id	0.0073	<.0001	0.0000	<.0001	<.0001	0.0144	0.0237	0.0006	0.0002	0.0113	id	id	id	id	Con
D1	>		0.1700	0.0080	0.0011			0.0047			id			0.0006			0.8025									D1
D2	>	?(>)				0.1852			0.0007						0.0138			0.5818								D2
D3	>	>					<.0001			0.0074						0.6709										D3
D4	>	<				0.0002	0.0027					0.1010							0.3766			id		id		D4
D5	>		?(<)		>								0.0004							0.9688			id		id	D5
D6	>			<	>																0.9179					D6
C1S	>	>							0.5039	0.0013	id			0.0275												C1S
C2S	>		>					?(>)							0.6967											C2S
C3S	>			<				<								0.4807										C3S
A1S	id	id						id				id					id									A1S
A4S	>				?(<)						id		0.0041						0.0607							A4S
A5S	>					<						>								0.1231						A5S
C1	>	>						>							0.4923	0.0907	0.1329									C1
C2	>		>						?(>)					?(<)				0.2082								C2
C3	>			?(<)						?(>)				<												C3
A1	>	?(>)									id			?(<)				0.7628	0.1688							A1
A2	>		?(<)												?(<)		?(<)			0.7268						A2
A4	>				?(>)							>					?(<)			0.0684	0.4481	id		id		A4
A5	>					?(>)							?(>)					?(>)	>				id		id	A5
A6	>						?(>)												?(>)							A6
A4F	id				id														id				id			A4F
A5F	id					id														id		id				A5F
A4H	id				id														id						id	A4H
A5H	id					id														id				id		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E135. Results of Hypothesis Test 1 for Density and furnish FD6.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		<.0001	<.0001	<.0001	<.0001	<.0001	<.0001	0.0000	0.0000	<.0001	id	<.0001	<.0001	<.0001	<.0001	<.0001	0.0000	0.0007	0.0003	0.0007	<.0001	id	0.0000	0.0000	0.0000	Con
D1	>		0.0029	0.0016	err			0.0349			id			0.0000			0.0163									D1
D2	>	>				0.8813			0.0001						0.1370			0.5900								D2
D3	>	>					0.0002			0.0002						0.0014										D3
D4	>	<				<.0001	0.0077					0.2573							0.0479			id		0.0054		D4
D5	>		?(<)		>								0.0000							0.6354			0.3550		0.2918	D5
D6	>			<	>																<.0001					D6
C1S	>	>							0.0001	0.1757	id			0.0717												C1S
C2S	>		>					>							0.0013											C2S
C3S	>			>				?(>)								0.0268										C3S
A1S	id	id						id				id					id									A1S
A4S	>				?(<)						id		0.1394						0.0378							A4S
A5S	>					<						?(>)								0.0654						A5S
C1	>	>						>							0.8249	0.0844	0.5542									C1
C2	>		?(>)						<					?(<)				0.9666								C2
C3	>			>						>				>												C3
A1	>	>									id			?(>)				0.7617	0.3493							A1
A2	>		?(>)												?(>)		?(<)			0.9350						A2
A4	>				>							>					?(<)			0.7321	0.0614	id		0.8627		A4
A5	>					?(>)							>					?(<)	?(>)				0.7872		0.6361	A5
A6	>						>												>							A6
A4F	id				id														id				id			A4F
A5F	>					?(>)														?(>)		id				A5F
A4H	>				>														?(<)						0.2777	A4H
A5H	>					?(>)														?(>)				?(>)		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E136. Results of Hypothesis Test 1 for Density and furnish FD7.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		0.0006	<.0001	<.0001	<.0001	<.0001	0.0000	<.0001	0.0000	<.0001	id	0.0000	<.0001	<.0001	0.0005	0.0000	<.0001	id	0.0026	0.0000	0.0000	id	id	id	id	Con
D1	>		0.0017	0.0011	0.0008			0.0002			id			0.0000			0.0004									D1
D2	>	>				0.0009			<.0001						0.7144			id								D2
D3	>	>					0.5945			0.0474						0.4623										D3
D4	>	<				<.0001	<.0001					0.0130							0.0977			id		id		D4
D5	>		<		>								<.0001							0.0149			id		id	D5
D6	>			?(<)	>																0.0091					D6
C1S	>	>							0.0003	0.0139	id			0.8044												C1S
C2S	>		>					>							0.0292											C2S
C3S	>			>				<								0.2794										C3S
A1S	id	id						id				id					id									A1S
A4S	>				<						id		0.5120						0.0490							A4S
A5S	>					<						?(>)								0.0666						A5S
C1	>	>						?(<)							0.2420	0.1424	0.7303									C1
C2	>		?(<)						<					?(<)				id								C2
C3	>			?(<)						?(<)				?(<)												C3
A1	>	>									id			?(<)				id	0.7155							A1
A2	id		id												id		id			id						A2
A4	>				>							>					?(<)			0.1600	0.2080	id		id		A4
A5	>					<							>					id	?(<)				id		id	A5
A6	>						>												?(>)							A6
A4F	id				id														id				id			A4F
A5F	id					id														id		id				A5F
A4H	id				id														id						id	A4H
A5H	id					id														id				id		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E137. Results of Hypothesis Test 1 for Density, comparing furnishes.

Case	Con WF1	Con WF2	Con WF3	Con FD5	Con FD6	Con FD7	D1 WF1	D1 WF2	D1 WF3	D1 FD5	D1 FD6	D1 FD7	D2 WF1	D2 WF2	D2 WF3	D2 FD5	D2 FD6	D2 FD7	Case
Con WF1		<.0001	0.0000	<.0001	<.0001														Con WF1
Con WF2	>			<.0001	<.0001														Con WF2
Con WF3	>			<.0001		<.0001													Con WF3
Con FD5	>	>	>		<.0001	<.0001													Con FD5
Con FD6	>	<		<		<.0001													Con FD6
Con FD7			>	<	>														Con FD7
D1 WF1								0.0069	0.0139	0.1173	0.0791								D1 WF1
D1 WF2							>			0.1335	0.0495								D1 WF2
D1 WF3							>			0.2865		0.2664							D1 WF3
D1 FD5							?(>)	?(<)	?(<)		0.7772	0.7799							D1 FD5
D1 FD6							>	<		?(<)		0.2736							D1 FD6
D1 FD7									?(<)	?(>)	?(>)								D1 FD7
D2 WF1														0.0014	0.1190	0.0444	0.1251		D2 WF1
D2 WF2													>			<.0001	0.0000		D2 WF2
D2 WF3													?(>)			0.0012		0.0171	D2 WF3
D2 FD5													<	<	<		0.2840	0.0037	D2 FD5
D2 FD6													?(<)	<		?(>)		0.1557	D2 FD6
D2 FD7															<	>	?(>)		D2 FD7
Case	Con WF1	Con WF2	Con WF3	Con FD5	Con FD6	Con FD7	D1 WF1	D1 WF2	D1 WF3	D1 FD5	D1 FD6	D1 FD7	D2 WF1	D2 WF2	D2 WF3	D2 FD5	D2 FD6	D2 FD7	Case
	D3	D3	D3	D3	D3	D3	D4	D4	D4	D4	D4	D4	D5	D5	D5	D5	D5	D5	
D3 WF1		0.0104	0.0074	0.8990	0.0023														D3 WF1
D3 WF2	>			0.0126	0.0001														D3 WF2
D3 WF3	>			0.0060		0.0324													D3 WF3
D3 FD5	?(>)	<	<		0.0014	0.1068													D3 FD5
D3 FD6	<	<		<		0.0000													D3 FD6
D3 FD7			<	?(>)	>														D3 FD7
D4 WF1								0.3618	0.1727	0.0504	0.0167								D4 WF1
D4 WF2							?(>)			0.0034	<.0001								D4 WF2
D4 WF3							?(>)			0.0005		0.0002							D4 WF3
D4 FD5							<	<	<		0.3225	0.1968							D4 FD5
D4 FD6							<	<		?(<)		0.0020							D4 FD6
D4 FD7									<	?(>)	>								D4 FD7
D5 WF1														0.2861	0.0401	<.0001	0.0002		D5 WF1
D5 WF2													?(<)			<.0001	0.0003		D5 WF2
D5 WF3													>			<.0001		0.0000	D5 WF3
D5 FD5													<	<	<		0.1170	0.2246	D5 FD5
D5 FD6													<	<		?(>)		0.3361	D5 FD6
D5 FD7															<	?(>)	?(<)		D5 FD7
Case	D3 WF1	D3 WF2	D3 WF3	D3 FD5	D3 FD6	D3 FD7	D4 WF1	D4 WF2	D4 WF3	D4 FD5	D4 FD6	D4 FD7	D5 WF1	D5 WF2	D5 WF3	D5 FD5	D5 FD6	D5 FD7	Case

Table E138. Results of Hypothesis Test 1 for Density, comparing furnishes continued.

Case	D6 WF1	D6 WF2	D6 WF3	D6 FD5	D6 FD6	D6 FD7	C1S WF1	C1S WF2	C1S WF3	C1S FD5	C1S FD6	C1S FD7	C2S WF1	C2S WF2	C2S WF3	C2S FD5	C2S FD6	C2S FD7	Case
D6 WF1		0.0002	0.0001	<.0001	<.0001														D6 WF1
D6 WF2	<			0.0001	0.0000														D6 WF2
D6 WF3	<			0.0130		0.0531													D6 WF3
D6 FD5	<	<	<		0.0344	<.0001													D6 FD5
D6 FD6	<	<		<		<.0001													D6 FD6
D6 FD7			>	>	>														D6 FD7
C1S WF1								0.2213	0.0498	0.5018	0.9746								C1S WF1
C1S WF2							?(>)			0.2835	0.1033								C1S WF2
C1S WF3							>			0.0186		0.5706							C1S WF3
C1S FD5							?(>)	?(<)	<		0.2318	0.0001							C1S FD5
C1S FD6							?(>)	?(<)		?(<)		0.0039							C1S FD6
C1S FD7									?(<)	>	>								C1S FD7
C2S WF1														0.0000	0.0045	<.0001	0.3767		C2S WF1
C2S WF2													>			<.0001	0.0174		C2S WF2
C2S WF3													>			<.0001		0.0525	C2S WF3
C2S FD5													<	<	<		0.0009	<.0001	C2S FD5
C2S FD6													?(>)	<		>		1.0000	C2S FD6
C2S FD7															<	>	?(>)		C2S FD7
Case	D6 WF1 C3S	D6 WF2 C3S	D6 WF3 C3S	D6 FD5 C3S	D6 FD6 C3S	D6 FD7 C3S	C1S WF1 A1S	C1S WF2 A1S	C1S WF3 A1S	C1S FD5 A1S	C1S FD6 A1S	C1S FD7 A1S	C2S WF1 A4S	C2S WF2 A4S	C2S WF3 A4S	C2S FD5 A4S	C2S FD6 A4S	C2S FD7 A4S	Case
C3S WF1		1.0000	0.0319	0.0284	0.0716														C3S WF1
C3S WF2	?(>)			<.0001	0.0000														C3S WF2
C3S WF3	<			0.3669		0.0187													C3S WF3
C3S FD5	<	<	?(<)		0.0007	<.0001													C3S FD5
C3S FD6	<	<		>		0.0236													C3S FD6
C3S FD7			>	>	>														C3S FD7
A1S WF1								id	id	id	id								A1S WF1
A1S WF2							id			id	id								A1S WF2
A1S WF3							id			id		id							A1S WF3
A1S FD5							id	id	id		id	id							A1S FD5
A1S FD6							id	id		id		id							A1S FD6
A1S FD7									id	id	id								A1S FD7
A4S WF1														0.0013	0.0678	0.0018	<.0001		A4S WF1
A4S WF2													<			0.0156	0.0001		A4S WF2
A4S WF3													<			0.0062		0.0008	A4S WF3
A4S FD5													<	<	<		0.4695	0.4235	A4S FD5
A4S FD6													<	<		?(>)		0.8413	A4S FD6
A4S FD7															<	?(>)	?(>)		A4S FD7
Case	C3S WF1	C3S WF2	C3S WF3	C3S FD5	C3S FD6	C3S FD7	A1S WF1	A1S WF2	A1S WF3	A1S FD5	A1S FD6	A1S FD7	A4S WF1	A4S WF2	A4S WF3	A4S FD5	A4S FD6	A4S FD7	Case

Table E139. Results of Hypothesis Test 1 for Density, comparing furnishes continued.

Case	A5S WF1	A5S WF2	A5S WF3	A5S FD5	A5S FD6	A5S FD7	C1 WF1	C1 WF2	C1 WF3	C1 FD5	C1 FD6	C1 FD7	C2 WF1	C2 WF2	C2 WF3	C2 FD5	C2 FD6	C2 FD7	Case
A5S WF1		id	id	id	id														A5S WF1
A5S WF2	id			0.1013	0.0035														A5S WF2
A5S WF3	id			0.3584		0.6245													A5S WF3
A5S FD5	id	?(<)	?(>)		0.0271	0.0007													A5S FD5
A5S FD6	id	<		<		0.4694													A5S FD6
A5S FD7			?(<)	<	?(<)														A5S FD7
C1 WF1								0.9516	0.9068	0.3113	0.2522								C1 WF1
C1 WF2							?(<)			0.5430	0.4772								C1 WF2
C1 WF3							?(<)			0.0445		0.3364							C1 WF3
C1 FD5							?(<)	?(<)	<		0.5837	0.0586							C1 FD5
C1 FD6							?(<)	?(<)		?(<)		0.0616							C1 FD6
C1 FD7									?(<)	>	>								C1 FD7
C2 WF1														0.5774	0.5947	0.1958	0.1947		C2 WF1
C2 WF2													?(<)			0.0027	0.0040		C2 WF2
C2 WF3													?(<)			0.0001		0.0296	C2 WF3
C2 FD5													?(<)	<	<		0.9495	0.5011	C2 FD5
C2 FD6													?(<)	<		?(<)		0.5260	C2 FD6
C2 FD7															<	?(<)	?(<)		C2 FD7
Case	A5S WF1 C3	A5S WF2 C3	A5S WF3 C3	A5S FD5 C3	A5S FD6 C3	A5S FD7 C3	C1 WF1 A1	C1 WF2 A1	C1 WF3 A1	C1 FD5 A1	C1 FD6 A1	C1 FD7 A1	C2 WF1 A2	C2 WF2 A2	C2 WF3 A2	C2 FD5 A2	C2 FD6 A2	C2 FD7 A2	Case
C3 WF1		0.7602	0.6225	0.2301	0.7298														C3 WF1
C3 WF2	?(<)			0.1579	0.3014														C3 WF2
C3 WF3	?(>)			0.2613		0.2518													C3 WF3
C3 FD5	?(<)	?(<)	?(<)		0.0177	0.8314													C3 FD5
C3 FD6	?(>)	?(>)		>		0.0946													C3 FD6
C3 FD7			?(<)	?(<)	<														C3 FD7
A1 WF1								0.6042	0.1741	0.0369	0.2371								A1 WF1
A1 WF2							?(<)			0.0163	0.1666								A1 WF2
A1 WF3							?(<)			0.1140		0.6909							A1 WF3
A1 FD5							<	<	?(<)		0.1059	0.0898							A1 FD5
A1 FD6							?(<)	?(<)		?(>)		0.9925							A1 FD6
A1 FD7									?(>)	>	?(>)								A1 FD7
A2 WF1														0.3919	0.0007	0.0194	0.2464		A2 WF1
A2 WF2													?(<)			0.0378	0.3874		A2 WF2
A2 WF3													<			0.3399		id	A2 WF3
A2 FD5													<	<	?(<)		0.3607	id	A2 FD5
A2 FD6													?(<)	?(<)		?(>)		id	A2 FD6
A2 FD7															id	id	id		A2 FD7
Case	C3 WF1	C3 WF2	C3 WF3	C3 FD5	C3 FD6	C3 FD7	A1 WF1	A1 WF2	A1 WF3	A1 FD5	A1 FD6	A1 FD7	A2 WF1	A2 WF2	A2 WF3	A2 FD5	A2 FD6	A2 FD7	Case

Table E140. Results of Hypothesis Test 1 for Density, comparing furnishes continued.

Case	A4 WF1	A4 WF2	A4 WF3	A4 FD5	A4 FD6	A4 FD7	A5 WF1	A5 WF2	A5 WF3	A5 FD5	A5 FD6	A5 FD7	A6 WF1	A6 WF2	A6 WF3	A6 FD5	A6 FD6	A6 FD7	Case
A4 WF1		0.6150	0.4889	0.0206	0.3897														A4 WF1
A4 WF2	?(>)			0.0488	0.2727														A4 WF2
A4 WF3	?(>)			0.0425		0.3627													A4 WF3
A4 FD5	<	<	<		0.1359	0.1200													A4 FD5
A4 FD6	?(<)	?(<)		?(>)		0.7081													A4 FD6
A4 FD7			?(<)	?(>)	?(>)														A4 FD7
A5 WF1								0.7331	0.8330	0.1119	0.3433								A5 WF1
A5 WF2							?(<)			0.0996	0.4579								A5 WF2
A5 WF3							?(<)			0.1749		0.0690							A5 WF3
A5 FD5							?(<)	<	?(<)		0.4625	0.1308							A5 FD5
A5 FD6							?(<)	?(<)		?(>)		0.1502							A5 FD6
A5 FD7									<	?(<)	?(<)								A5 FD7
A6 WF1														0.0616	0.1271	0.1517	0.0572		A6 WF1
A6 WF2													>			0.0055	0.6500		A6 WF2
A6 WF3													?(>)			0.0146		0.9616	A6 WF3
A6 FD5													?(<)	<	<		0.0069	0.0050	A6 FD5
A6 FD6													>	?(<)		>		0.5940	A6 FD6
A6 FD7															?(>)	>	?(>)		A6 FD7
Case	A4 WF1	A4 WF2	A4 WF3	A4 FD5	A4 FD6	A4 FD7	A5 WF1	A5 WF2	A5 WF3	A5 FD5	A5 FD6	A5 FD7	A6 WF1	A6 WF2	A6 WF3	A6 FD5	A6 FD6	A6 FD7	Case
	A5F	A5F	A5F	A5F	A5F	A5F	A4H	A4H	A4H	A4H	A4H	A4H	A5H	A5H	A5H	A5H	A5H	A5H	
A5F WF1		id	id	id	0.6995														A5F WF1
A5F WF2	id			id	id														A5F WF2
A5F WF3	id			id		id													A5F WF3
A5F FD5	id	id	id		id	id													A5F FD5
A5F FD6	?(>)	id		id		id													A5F FD6
A5F FD7			id	id	id														A5F FD7
A4H WF1								1.0000	0.9999	id	0.9996								A4H WF1
A4H WF2							?(<)			id	0.9995								A4H WF2
A4H WF3							?(>)			id		id							A4H WF3
A4H FD5							id	id	id		id	id							A4H FD5
A4H FD6							?(>)	?(>)		id		id							A4H FD6
A4H FD7									id	id	id								A4H FD7
A5H WF1														id	id	id	id		A5H WF1
A5H WF2													id			id	id		A5H WF2
A5H WF3													id			id		id	A5H WF3
A5H FD5													id	id	id		id	id	A5H FD5
A5H FD6													id	id		id		id	A5H FD6
A5H FD7															id	id	id		A5H FD7
Case	A5F WF1	A5F WF2	A5F WF3	A5F FD5	A5F FD6	A5F FD7	A4H WF1	A4H WF2	A4H WF3	A4H FD5	A4H FD6	A4H FD7	A5H WF1	A5H WF2	A5H WF3	A5H FD5	A5H FD6	A5H FD7	Case

Table E141. Results of Hypothesis Test 2 for Density and furnish WF1.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		0.0000	0.0001	0.0000	0.0000	<.0001	0.0000	0.0000	<.0001	0.0003	0.0008	<.0001	id	<.0001	0.0001	<.0001	0.0000	0.0000	0.0000	0.0000	0.0000	id	0.0000	0.9939	id	Con
D1	>		0.0006	0.0003	1.0000			0.0720			0.4725			<.0001			0.0003									D1
D2	>	>				0.0325			0.0007						0.0439			0.0006								D2
D3	>	>					0.0006			0.0519						0.3217										D3
D4	>	?(>)				0.0001	0.0000					0.5748							0.0006			id		0.9995		D4
D5	>		>		>								id							0.0165			0.3596		id	D5
D6	>			>	>																0.0600					D6
C1S	>	>							0.0075	0.0350	0.2800			0.0137												C1S
C2S	>		>					>							0.2019											C2S
C3S	>			>				>								0.3003										C3S
A1S	>	?(>)						?(<)				0.6879					0.0007									A1S
A4S	>				?(>)						?(<)		id						0.0011							A4S
A5S	id					id						id								id						A5S
C1	>	>						>							0.1869	0.1989	0.1161									C1
C2	>		>						?(>)					?(>)				0.2251								C2
C3	>			?(>)						?(<)				?(<)												C3
A1	>	>									>			?(>)				0.1644	0.1215							A1
A2	>		>												?(<)		?(<)			0.1062						A2
A4	>				>							>					?(<)			0.0788	0.2913	id		0.9977		A4
A5	>					>							id					?(>)	>					0.0079		id	A5
A6	>						<												?(<)								A6
A4F	id				id														id				id				A4F
A5F	>					?(<)														<		id					A5F
A4H	?(>)				?(>)														?(<)						id		A4H
A5H	id					id														id				id			A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E142. Results of Hypothesis Test 2 for Density and furnish WF2.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		0.0000	0.0000	<.0001	<.0001	<.0001	<.0001	0.0000	<.0001	<.0001	id	<.0001	<.0001	<.0001	0.0000	<.0001	<.0001	<.0001	0.0001	0.0000	0.0000	id	id	0.9960	id	Con
D1	>		0.0001	0.0156	0.0191			0.0773			id			0.0031			0.0001									D1
D2	>	>				0.0057			0.0001						0.5731			0.1398								D2
D3	>	>					0.0014			0.0005						0.5779										D3
D4	>	<				<.0001	0.0002					0.0000							0.0036			id		0.9998		D4
D5	>		<		>								err							0.0696			id		id	D5
D6	>			<	>																0.0002					D6
C1S	>	>							0.0002	0.0440	id			0.0578												C1S
C2S	>		>					>							0.0021											C2S
C3S	>			>				>								0.0018										C3S
A1S	id	id						id				id					id									A1S
A4S	>				<						id		0.0005						0.0016							A4S
A5S	>					<						>								0.0015						A5S
C1	>	>						>							0.7133	0.0263	0.7162									C1
C2	>		?(>)						<					?(<)				0.0865								C2
C3	>			?(<)						<				<												C3
A1	>	>									id			?(<)				0.0934	0.2524							A1
A2	>		?(<)												<		<			0.1666						A2
A4	>				>							>					?(>)			0.5293	0.5196	id		0.9962		A4
A5	>					>							>					?(>)	?(<)					id		id	A5
A6	>						>												?(<)							A6
A4F	id				id														id				id			A4F
A5F	id					id														id		id				A5F
A4H	?(>)				?(>)														?(<)						id	A4H
A5H	id					id														id				id		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E143. Results of Hypothesis Test 2 for Density and furnish WF3.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		0.0000	0.0000	0.0000	<.0001	<.0001	0.0000	0.0000	<.0001	0.0000	id	<.0001	0.0587	0.0000	<.0001	0.0002	<.0001	<.0001	0.0002	0.0001	0.0000	id	id	<.0001	id	Con
D1	>		0.0027	0.0017	0.1327			0.0013			id			0.0003			0.0120									D1
D2	>	>				0.0293			0.0000						0.0004			0.0666								D2
D3	>	>					0.0028			0.0069						0.0618										D3
D4	>	?(<)				<.0001	0.0680					0.0061							0.0065			id		0.3744		D4
D5	>		>		>								0.0714							0.1474			id		id	D5
D6	>			<	>																0.0010					D6
C1S	>	>							0.0014	0.0053	id			0.6804												C1S
C2S	>		>					>							0.0222											C2S
C3S	>			<				<								0.0148										C3S
A1S	id	id						id				id					id									A1S
A4S	>				<						id		0.4204						0.0036							A4S
A5S	>					<						?(<)								0.0018						A5S
C1	>	>						?(>)							0.0102	0.1026	0.1324									C1
C2	>		>						<					>				<.0001								C2
C3	>			>						>				?(>)												C3
A1	>	>									id			?(<)				0.2034	0.0314							A1
A2	>		<												<		?(<)			0.0197						A2
A4	>				>							>					>			0.6883	0.4902	id		0.0085		A4
A5	>					?(>)							>					>	?(<)				id		id	A5
A6	>						>												?(<)							A6
A4F	id				id														id				id			A4F
A5F	id					id														id		id				A5F
A4H	>				?(>)														<						id	A4H
A5H	id					id														id				id		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E144. Results of Hypothesis Test 2 for Density and furnish FD5.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		<.0001	<.0001	<.0001	0.0001	<.0001	<.0001	<.0001	<.0001	<.0001	id	0.0073	<.0001	<.0001	<.0001	<.0001	0.0043	0.0003	0.0000	<.0001	0.0004	id	id	id	id	Con
D1	>		0.1700	0.0080	0.0011			0.0047			id			0.0002			0.4547									D1
D2	>	?(>)				0.1852			0.0007						0.0047			0.7912								D2
D3	>	>					<.0001			0.0074						0.9121										D3
D4	>	<				0.0002	0.0027					0.1010							0.0876			id		id		D4
D5	>		?(<)		>								0.0004							0.3372			id		id	D5
D6	>			<	>																0.2917					D6
C1S	>	>							0.5039	0.0013	id			0.0013												C1S
C2S	>		>					?(>)							0.4405											C2S
C3S	>			<				<								0.1379										C3S
A1S	id	id						id				id					id									A1S
A4S	>				?(<)						id		0.0041						0.0091							A4S
A5S	>					<						>								0.0090						A5S
C1	>	>						>							0.1795	0.0299	0.0173									C1
C2	>		>						?(>)					?(<)				0.3302								C2
C3	>			?(>)						?(>)				<												C3
A1	>	?(<)									id			<				0.2432	0.5253							A1
A2	>		?(>)												?(<)		?(>)			0.9434						A2
A4	>				>							>					?(<)			0.0094	0.1321	id		id		A4
A5	>					?(>)							>					?(<)	>					id		id	A5
A6	>						?(>)												?(>)								A6
A4F	id				id														id				id			A4F
A5F	id					id														id		id				A5F
A4H	id				id														id						id	A4H
A5H	id					id														id				id		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E145. Results of Hypothesis Test 2 for Density and furnish FD6.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		<.0001	<.0001	<.0001	<.0001	<.0001	<.0001	0.0000	0.0000	<.0001	id	<.0001	<.0001	<.0001	<.0001	<.0001	<.0001	0.0001	0.0000	0.0000	<.0001	id	<.0001	<.0001	0.0000	Con
D1	>		0.0029	0.0016	err			0.0349			id			<.0001			0.0002									D1
D2	>	>				0.8813			0.0001						0.1832			0.6086								D2
D3	>	>					0.0002			0.0002						0.0003										D3
D4	>	<				<.0001	0.0077					0.2573							0.0052			id		0.0001		D4
D5	>		?(<)		>								0.0000							0.1025			0.1209		0.1185	D5
D6	>			<	>																<.0001					D6
C1S	>	>							0.0001	0.1757	id			0.0320												C1S
C2S	>		>					>							0.0004											C2S
C3S	>			>				?(>)								0.0052										C3S
A1S	id	id						id				id					id									A1S
A4S	>				?(<)						id		0.1394						0.0040							A4S
A5S	>					<						?(>)								0.0030						A5S
C1	>	>						>							0.2795	0.0331	0.0638									C1
C2	>		?(>)						<					?(<)				0.2993								C2
C3	>			>						>				>												C3
A1	>	>									id			>				0.0318	0.2146							A1
A2	>		?(<)												?(<)		<			0.1069						A2
A4	>				>							>					?(<)			0.4273	0.0869	id		0.7171		A4
A5	>					?(>)							>					?(>)	?(>)					0.9576		0.8008	A5
A6	>						>												>							A6
A4F	id				id														id				id			A4F
A5F	>					?(>)														?(<)		id				A5F
A4H	>				>														?(<)						0.2067	A4H
A5H	>					?(>)														?(>)				?(>)		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E146. Results of Hypothesis Test 2 for Density and furnish FD7.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		0.0006	<.0001	<.0001	<.0001	<.0001	0.0000	<.0001	0.0000	<.0001	id	0.0000	<.0001	<.0001	0.0000	0.0000	<.0001	id	0.0001	<.0001	0.0000	id	id	id	id	Con
D1	>		0.0017	0.0011	0.0008			0.0002			id			0.0000			0.0000									D1
D2	>	>				0.0009			<.0001						0.8327			id								D2
D3	>	>					0.5945			0.0474						0.1778										D3
D4	>	<				<.0001	<.0001					0.0130							0.0037			id		id		D4
D5	>		<		>								<.0001							0.0112			id		id	D5
D6	>			?(<)	>																0.0004					D6
C1S	>	>							0.0003	0.0139	id			0.9428												C1S
C2S	>		>					>							0.0252											C2S
C3S	>			>				<								0.0812										C3S
A1S	id	id						id				id					id									A1S
A4S	>				<						id		0.5120						0.0011							A4S
A5S	>					<						?(>)								0.0082						A5S
C1	>	>						?(<)							0.3544	0.0277	0.9646									C1
C2	>		?(>)						<					?(<)				id								C2
C3	>			?(<)						<				<												C3
A1	>	>									id			?(>)				id	0.6330							A1
A2	id		id												id		id			id						A2
A4	>				>							>					?(>)			0.0079	0.2098	id		id		A4
A5	>					<							>					id	<				id		id	A5
A6	>						>												?(>)							A6
A4F	id				id														id				id			A4F
A5F	id					id														id		id				A5F
A4H	id				id														id						id	A4H
A5H	id					id														id				id		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E147. Results of Hypothesis Test 2 for Density, comparing furnishes.

Case	Con WF1	Con WF2	Con WF3	Con FD5	Con FD6	Con FD7	D1 WF1	D1 WF2	D1 WF3	D1 FD5	D1 FD6	D1 FD7	D2 WF1	D2 WF2	D2 WF3	D2 FD5	D2 FD6	D2 FD7	Case
Con WF1		<.0001	0.0000	<.0001	<.0001														Con WF1
Con WF2	>			<.0001	<.0001														Con WF2
Con WF3	>			<.0001		<.0001													Con WF3
Con FD5	>	>	>		<.0001	<.0001													Con FD5
Con FD6	>	<		<		<.0001													Con FD6
Con FD7			>	<	>														Con FD7
D1 WF1								0.0069	0.0139	0.1173	0.0791								D1 WF1
D1 WF2							>			0.1335	0.0495								D1 WF2
D1 WF3							>			0.2865		0.2664							D1 WF3
D1 FD5							?(>)	?(<)	?(<)		0.7772	0.7799							D1 FD5
D1 FD6							>	<		?(<)		0.2736							D1 FD6
D1 FD7									?(<)	?(>)	?(>)								D1 FD7
D2 WF1														0.0014	0.1190	0.0444	0.1251		D2 WF1
D2 WF2													>			<.0001	0.0000		D2 WF2
D2 WF3													?(>)			0.0012		0.0171	D2 WF3
D2 FD5													<	<	<		0.2840	0.0037	D2 FD5
D2 FD6													?(<)	<		?(>)		0.1557	D2 FD6
D2 FD7															<	>	?(>)		D2 FD7
Case	Con WF1 D3	Con WF2 D3	Con WF3 D3	Con FD5 D3	Con FD6 D3	Con FD7 D3	D1 WF1 D4	D1 WF2 D4	D1 WF3 D4	D1 FD5 D4	D1 FD6 D4	D1 FD7 D4	D2 WF1 D5	D2 WF2 D5	D2 WF3 D5	D2 FD5 D5	D2 FD6 D5	D2 FD7 D5	Case
D3 WF1		0.0104	0.0074	0.8990	0.0023														D3 WF1
D3 WF2	>			0.0126	0.0001														D3 WF2
D3 WF3	>			0.0060		0.0324													D3 WF3
D3 FD5	?(>)	<	<		0.0014	0.1068													D3 FD5
D3 FD6	<	<		<		0.0000													D3 FD6
D3 FD7			<	?(>)	>														D3 FD7
D4 WF1								0.3618	0.1727	0.0504	0.0167								D4 WF1
D4 WF2							?(>)			0.0034	<.0001								D4 WF2
D4 WF3							?(>)			0.0005		0.0002							D4 WF3
D4 FD5							<	<	<		0.3225	0.1968							D4 FD5
D4 FD6							<	<		?(<)		0.0020							D4 FD6
D4 FD7									<	?(>)	>								D4 FD7
D5 WF1														0.2861	0.0401	<.0001	0.0002		D5 WF1
D5 WF2													?(<)			<.0001	0.0003		D5 WF2
D5 WF3													>			<.0001		0.0000	D5 WF3
D5 FD5													<	<	<		0.1170	0.2246	D5 FD5
D5 FD6													<	<		?(>)		0.3361	D5 FD6
D5 FD7															<	?(>)	?(<)		D5 FD7
Case	D3 WF1	D3 WF2	D3 WF3	D3 FD5	D3 FD6	D3 FD7	D4 WF1	D4 WF2	D4 WF3	D4 FD5	D4 FD6	D4 FD7	D5 WF1	D5 WF2	D5 WF3	D5 FD5	D5 FD6	D5 FD7	Case

Table E148. Results of Hypothesis Test 2 for Density, comparing furnishes continued.

Case	D6 WF1	D6 WF2	D6 WF3	D6 FD5	D6 FD6	D6 FD7	C1S WF1	C1S WF2	C1S WF3	C1S FD5	C1S FD6	C1S FD7	C2S WF1	C2S WF2	C2S WF3	C2S FD5	C2S FD6	C2S FD7	Case
D6 WF1		0.0002	0.0001	<.0001	<.0001														D6 WF1
D6 WF2	<			0.0001	0.0000														D6 WF2
D6 WF3	<			0.0130		0.0531													D6 WF3
D6 FD5	<	<	<		0.0344	<.0001													D6 FD5
D6 FD6	<	<		<		<.0001													D6 FD6
D6 FD7			>	>	>														D6 FD7
C1S WF1								0.2213	0.0498	0.5018	0.9746								C1S WF1
C1S WF2							?(>)			0.2835	0.1033								C1S WF2
C1S WF3							>			0.0186		0.5706							C1S WF3
C1S FD5							?(>)	?(<)	<		0.2318	0.0001							C1S FD5
C1S FD6							?(>)	?(<)		?(<)		0.0039							C1S FD6
C1S FD7									?(<)	>	>								C1S FD7
C2S WF1														0.0000	0.0045	<.0001	0.3767		C2S WF1
C2S WF2													>			<.0001	0.0174		C2S WF2
C2S WF3													>			<.0001		0.0525	C2S WF3
C2S FD5													<	<	<		0.0009	<.0001	C2S FD5
C2S FD6													?(>)	<		>		1.0000	C2S FD6
C2S FD7															<	>	?(>)		C2S FD7
Case	D6 WF1 C3S	D6 WF2 C3S	D6 WF3 C3S	D6 FD5 C3S	D6 FD6 C3S	D6 FD7 C3S	C1S WF1 A1S	C1S WF2 A1S	C1S WF3 A1S	C1S FD5 A1S	C1S FD6 A1S	C1S FD7 A1S	C2S WF1 A4S	C2S WF2 A4S	C2S WF3 A4S	C2S FD5 A4S	C2S FD6 A4S	C2S FD7 A4S	Case
C3S WF1		1.0000	0.0319	0.0284	0.0716														C3S WF1
C3S WF2	?(>)			<.0001	0.0000														C3S WF2
C3S WF3	<			0.3669		0.0187													C3S WF3
C3S FD5	<	<	?(<)		0.0007	<.0001													C3S FD5
C3S FD6	<	<		>		0.0236													C3S FD6
C3S FD7			>	>	>														C3S FD7
A1S WF1								id	id	id	id								A1S WF1
A1S WF2							id			id	id								A1S WF2
A1S WF3							id			id		id							A1S WF3
A1S FD5							id	id	id		id	id							A1S FD5
A1S FD6							id	id		id		id							A1S FD6
A1S FD7									id	id	id								A1S FD7
A4S WF1														0.0013	0.0678	0.0018	<.0001		A4S WF1
A4S WF2													<			0.0156	0.0001		A4S WF2
A4S WF3													<			0.0062		0.0008	A4S WF3
A4S FD5													<	<	<		0.4695	0.4235	A4S FD5
A4S FD6													<	<		?(>)		0.8413	A4S FD6
A4S FD7															<	?(>)	?(>)		A4S FD7
Case	C3S WF1	C3S WF2	C3S WF3	C3S FD5	C3S FD6	C3S FD7	A1S WF1	A1S WF2	A1S WF3	A1S FD5	A1S FD6	A1S FD7	A4S WF1	A4S WF2	A4S WF3	A4S FD5	A4S FD6	A4S FD7	Case

Table E149. Results of Hypothesis Test 2 for Density, comparing furnishes continued.

Case	A5S WF1	A5S WF2	A5S WF3	A5S FD5	A5S FD6	A5S FD7	C1 WF1	C1 WF2	C1 WF3	C1 FD5	C1 FD6	C1 FD7	C2 WF1	C2 WF2	C2 WF3	C2 FD5	C2 FD6	C2 FD7	Case
A5S WF1		id	id	id	id														A5S WF1
A5S WF2	id			0.1013	0.0035														A5S WF2
A5S WF3	id			0.3584		0.6245													A5S WF3
A5S FD5	id	?(<)	?(>)		0.0271	0.0007													A5S FD5
A5S FD6	id	<		<		0.4694													A5S FD6
A5S FD7			?(<)	<	?(<)														A5S FD7
C1 WF1								0.6573	0.3366	0.0568	0.0235								C1 WF1
C1 WF2							?(>)			0.0587	0.0314								C1 WF2
C1 WF3							?(<)			0.0882		0.2633							C1 WF3
C1 FD5							<	<	<		0.1619	0.2768							C1 FD5
C1 FD6							<	<		?(<)		0.0512							C1 FD6
C1 FD7									?(<)	?(>)	>								C1 FD7
C2 WF1														0.1958	0.2381	0.0545	0.0432		C2 WF1
C2 WF2													?(<)			0.0016	0.0007		C2 WF2
C2 WF3													?(<)			0.0000		0.0303	C2 WF3
C2 FD5													<	<	<		0.4436	0.7486	C2 FD5
C2 FD6													<	<		?(<)		0.9913	C2 FD6
C2 FD7															<	?(<)	?(>)		C2 FD7
Case	A5S WF1 C3	A5S WF2 C3	A5S WF3 C3	A5S FD5 C3	A5S FD6 C3	A5S FD7 C3	C1 WF1 A1	C1 WF2 A1	C1 WF3 A1	C1 FD5 A1	C1 FD6 A1	C1 FD7 A1	C2 WF1 A2	C2 WF2 A2	C2 WF3 A2	C2 FD5 A2	C2 FD6 A2	C2 FD7 A2	Case
C3 WF1		0.7094	0.0617	0.3864	0.3844														C3 WF1
C3 WF2	?(<)			0.3740	0.0380														C3 WF2
C3 WF3	>			0.0207		0.0082													C3 WF3
C3 FD5	?(<)	?(<)	<		0.0059	0.3297													C3 FD5
C3 FD6	?(>)	>		>		0.0110													C3 FD6
C3 FD7			<	?(<)	<														C3 FD7
A1 WF1								0.1155	0.0097	0.0004	0.0403								A1 WF1
A1 WF2							?(<)			0.0016	0.2259								A1 WF2
A1 WF3							<			0.0094		0.4162							A1 WF3
A1 FD5							<	<	<		0.0020	0.0056							A1 FD5
A1 FD6							<	?(<)		>		0.3994							A1 FD6
A1 FD7									?(>)	>	?(<)								A1 FD7
A2 WF1														0.0447	0.0001	0.0088	0.0068		A2 WF1
A2 WF2													<			0.0567	0.0334		A2 WF2
A2 WF3													<			0.6664		id	A2 WF3
A2 FD5													<	<	?(<)		0.7171	id	A2 FD5
A2 FD6													<	<		?(<)		id	A2 FD6
A2 FD7															id	id	id		A2 FD7
Case	C3 WF1	C3 WF2	C3 WF3	C3 FD5	C3 FD6	C3 FD7	A1 WF1	A1 WF2	A1 WF3	A1 FD5	A1 FD6	A1 FD7	A2 WF1	A2 WF2	A2 WF3	A2 FD5	A2 FD6	A2 FD7	Case

Table E150. Results of Hypothesis Test 2 for Density, comparing furnishes continued.

Case	A4 WF1	A4 WF2	A4 WF3	A4 FD5	A4 FD6	A4 FD7	A5 WF1	A5 WF2	A5 WF3	A5 FD5	A5 FD6	A5 FD7	A6 WF1	A6 WF2	A6 WF3	A6 FD5	A6 FD6	A6 FD7	Case
A4 WF1		0.2330	0.1404	0.0005	0.1484														A4 WF1
A4 WF2	?(>)			0.0017	0.0370														A4 WF2
A4 WF3	?(>)			0.0024		0.1104													A4 WF3
A4 FD5	<	<	<		0.0273	0.0054													A4 FD5
A4 FD6	?(<)	<		>		0.3234													A4 FD6
A4 FD7			?(<)	>	?(>)														A4 FD7
A5 WF1								0.2627	0.6392	0.0016	0.0444								A5 WF1
A5 WF2							?(<)			0.0055	0.2555								A5 WF2
A5 WF3							?(<)			0.0123		0.0031							A5 WF3
A5 FD5							<	<	<		0.1026	0.0239							A5 FD5
A5 FD6							<	?(<)		?(>)		0.0110							A5 FD6
A5 FD7									<	<	<								A5 FD7
A6 WF1														0.0212	0.0190	0.0460	0.1030		A6 WF1
A6 WF2													>			0.0009	0.1355		A6 WF2
A6 WF3													>			0.0009		0.7033	A6 WF3
A6 FD5													<	<	<		0.0043	0.0005	A6 FD5
A6 FD6													?(>)	?(<)		>		0.0606	A6 FD6
A6 FD7															?(<)	>	>		A6 FD7
Case	A4 WF1 A5F	A4 WF2 A5F	A4 WF3 A5F	A4 FD5 A5F	A4 FD6 A5F	A4 FD7 A5F	A5 WF1 A4H	A5 WF2 A4H	A5 WF3 A4H	A5 FD5 A4H	A5 FD6 A4H	A5 FD7 A4H	A6 WF1 A5H	A6 WF2 A5H	A6 WF3 A5H	A6 FD5 A5H	A6 FD6 A5H	A6 FD7 A5H	Case
A5F WF1		id	id	id	0.5734														A5F WF1
A5F WF2	id			id	id														A5F WF2
A5F WF3	id			id		id													A5F WF3
A5F FD5	id	id	id		id	id													A5F FD5
A5F FD6	?(>)	id		id		id													A5F FD6
A5F FD7			id	id	id														A5F FD7
A4H WF1								1.0000	0.9995	id	0.9992								A4H WF1
A4H WF2							?(<)			id	0.9991								A4H WF2
A4H WF3							?(>)			id		id							A4H WF3
A4H FD5							id	id	id		id	id							A4H FD5
A4H FD6							?(>)	?(>)		id		id							A4H FD6
A4H FD7									id	id	id								A4H FD7
A5H WF1														id	id	id	id		A5H WF1
A5H WF2													id			id	id		A5H WF2
A5H WF3													id			id		id	A5H WF3
A5H FD5													id	id	id		id	id	A5H FD5
A5H FD6													id	id		id		id	A5H FD6
A5H FD7															id	id	id		A5H FD7
Case	A5F WF1	A5F WF2	A5F WF3	A5F FD5	A5F FD6	A5F FD7	A4H WF1	A4H WF2	A4H WF3	A4H FD5	A4H FD6	A4H FD7	A5H WF1	A5H WF2	A5H WF3	A5H FD5	A5H FD6	A5H FD7	Case

Table E151. Results of Hypothesis Test 3 for Density and furnish WF1.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		0.0000	0.0001	0.0000	0.0000	<.0001	0.0000	0.0000	<.0001	0.0003	0.0008	<.0001	id	<.0001	0.0002	0.0000	0.0000	<.0001	0.0000	<.0001	<.0001	id	<.0001	0.0000	0.0000	Con
D1	>		0.0006	0.0003	1.0000			0.0720			0.4725			<.0001			<.0001									D1
D2	>	>				0.0325			0.0007						0.0050			0.0012								D2
D3	>	>					0.0006			0.0519						0.0408										D3
D4	>	?(>)				0.0001	0.0000					0.5748							0.0001			id		0.1218		D4
D5	>		>		>								id							0.0003			0.0085		0.0185	D5
D6	>			>	>																0.0019					D6
C1S	>	>							0.0075	0.0350	0.2800			0.0314												C1S
C2S	>		>					>							0.0726											C2S
C3S	>			>				>								0.3033										C3S
A1S	>	?(>)						?(<)				0.6879					0.0007									A1S
A4S	>				?(>)						?(<)		id						0.0000							A4S
A5S	id					id						id								id						A5S
C1	>	>						>							0.0207	0.3710	0.0312									C1
C2	>		>						>					>				0.0710								C2
C3	>			>						?(<)				?(<)												C3
A1	>	>									>			>				0.2752	0.0075							A1
A2	>		>												<		?(<)			0.4502						A2
A4	>				>							>					<			0.0023	0.1075	id		0.0001		A4
A5	>					>							id					?(>)	>				0.0000		0.0001	A5
A6	>						<												?(<)							A6
A4F	id				id														id				id			A4F
A5F	>					<														<		id				A5F
A4H	>				?(>)														<						0.0001	A4H
A5H	>					<														<				>		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E152. Results of Hypothesis Test 3 for Density and furnish WF2.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		0.0000	0.0000	<.0001	<.0001	<.0001	<.0001	0.0000	<.0001	<.0001	id	<.0001	<.0001	<.0001	0.0000	<.0001	<.0001	<.0001	0.0000	0.0000	<.0001	id	<.0001	<.0001	0.0018	Con
D1	>		0.0001	0.0156	0.0191			0.0773			id			0.0009			0.0002									D1
D2	>	>				0.0057			0.0001						0.0920			0.3906								D2
D3	>	>					0.0014			0.0005						0.9142										D3
D4	>	<				<.0001	0.0002					0.0000							0.0003			id		0.0556		D4
D5	>		<		>								err							0.1020			0.0000		0.8381	D5
D6	>			<	>																<.0001					D6
C1S	>	>							0.0002	0.0440	id			0.2024												C1S
C2S	>		>					>							0.0004											C2S
C3S	>			>				>								0.0009										C3S
A1S	id	id						id				id					id									A1S
A4S	>				<						id		0.0005						0.0001							A4S
A5S	>					<						>								0.0000						A5S
C1	>	>						?(>)							0.0035	0.0477	0.0421									C1
C2	>		>						<					>				0.0068								C2
C3	>			?(>)						<				<												C3
A1	>	>									id			>				0.1048	0.8575							A1
A2	>		?(<)												<		?(<)			0.8882						A2
A4	>				>							>					?(>)			0.4926	0.6161	id		0.0005		A4
A5	>					?(>)							>					?(<)	?(<)				0.0007		0.3181	A5
A6	>						>												?(>)							A6
A4F	id				id														id				id			A4F
A5F	>					<														<		id				A5F
A4H	>				>														<						0.0613	A4H
A5H	>					?(<)														?(<)				>		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E153. Results of Hypothesis Test 3 for Density and furnish WF3.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		0.0000	0.0000	0.0000	<.0001	<.0001	0.0000	0.0000	<.0001	0.0000	id	<.0001	0.0587	<.0001	<.0001	0.0000	<.0001	<.0001	0.0000	0.0000	0.0000	id	0.0000	<.0001	<.0001	Con
D1	>		0.0027	0.0017	0.1327			0.0013			id			0.0002			0.0036									D1
D2	>	>				0.0293			0.0000						0.0005			0.0164								D2
D3	>	>					0.0028			0.0069						0.0803										D3
D4	>	?(<)				<.0001	0.0680					0.0061							0.0006			id		0.6452		D4
D5	>		>		>								0.0714							0.6679			0.0006		0.0000	D5
D6	>			<	>																0.0000					D6
C1S	>	>							0.0014	0.0053	id			0.7611												C1S
C2S	>		>					>							0.0278											C2S
C3S	>			<				<								0.0036										C3S
A1S	id	id						id				id					id									A1S
A4S	>				<						id		0.4204						0.0002							A4S
A5S	>					<						?(<)								0.0052						A5S
C1	>	>						?(>)							0.0001	0.2494	0.0102									C1
C2	>		>						<					>				<.0001								C2
C3	>			>						>				?(>)												C3
A1	>	>									id			<				0.0033	0.0176							A1
A2	>		<												<		<			0.0066						A2
A4	>				>							>					>			0.3670	0.8002	id		0.0007		A4
A5	>					?(>)							>					>	?(<)				0.0137		0.0037	A5
A6	>						>												?(<)							A6
A4F	id				id														id				id			A4F
A5F	>					<														<		id				A5F
A4H	>				?(>)														<						0.2635	A4H
A5H	>					<														<				?(>)		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E154. Results of Hypothesis Test 3 for Density and furnish FD5.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		<.0001	<.0001	<.0001	0.0001	<.0001	<.0001	<.0001	<.0001	<.0001	id	0.0073	<.0001	<.0001	<.0001	<.0001	<.0001	<.0001	<.0001	id	0.0002	id	id	id	id	Con
D1	>		0.1700	0.0080	0.0011			0.0047			id			0.0008			0.5292									D1
D2	>	?(>)				0.1852			0.0007						0.0001			0.1032								D2
D3	>	>					<.0001			0.0074						0.3070										D3
D4	>	<				0.0002	0.0027					0.1010							0.1506			id		id		D4
D5	>		?(<)		>								0.0004							id			id		id	D5
D6	>			<	>																0.7539					D6
C1S	>	>							0.5039	0.0013	id			0.0068												C1S
C2S	>		>					?(>)							0.5317											C2S
C3S	>			<				<								0.0664										C3S
A1S	id	id						id				id					id									A1S
A4S	>				?(<)						id		0.0041						0.0147							A4S
A5S	>					<						>								id						A5S
C1	>	>						>							0.1643	0.0003	0.0002									C1
C2	>		>						?(>)					?(<)				0.0018								C2
C3	>			?(<)						>				<												C3
A1	>	?(>)									id			<				0.2827	0.0002							A1
A2	>		?(<)												<		?(<)			id						A2
A4	>				?(>)							>					<			id	0.0548	id		id		A4
A5	id					id							id					id	id				id		id	A5
A6	>						?(>)												>							A6
A4F	id				id														id				id			A4F
A5F	id					id														id		id				A5F
A4H	id				id														id						id	A4H
A5H	id					id														id				id		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E155. Results of Hypothesis Test 3 for Density and furnish FD6.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		<.0001	<.0001	<.0001	<.0001	<.0001	<.0001	0.0000	0.0000	<.0001	id	<.0001	<.0001	<.0001	<.0001	<.0001	<.0001	<.0001	0.0000	<.0001	<.0001	id	<.0001	<.0001	<.0001	Con
D1	>		0.0029	0.0016	err			0.0349			id			<.0001			<.0001									D1
D2	>	>				0.8813			0.0001						0.0177			0.0590								D2
D3	>	>					0.0002			0.0002						0.0000										D3
D4	>	<				<.0001	0.0077					0.2573							0.0019			id		<.0001		D4
D5	>		?(<)		>								0.0000							0.2205			0.0193		0.0027	D5
D6	>			<	>																<.0001					D6
C1S	>	>							0.0001	0.1757	id			0.0547												C1S
C2S	>		>					>							0.0007											C2S
C3S	>			>				?(>)								0.0012										C3S
A1S	id	id						id				id					id									A1S
A4S	>				?(<)						id		0.1394						0.0009							A4S
A5S	>					<						?(>)								0.0002						A5S
C1	>	>						>							0.6349	0.0061	0.0311									C1
C2	>		>						<					?(<)				0.8702								C2
C3	>			>						>				>												C3
A1	>	>									id			>				0.2036	0.0555							A1
A2	>		>												?(>)		?(<)			0.7799						A2
A4	>				>							>					<			0.4063	0.0029	id		0.7013		A4
A5	>					?(>)							>					?(<)	?(>)				0.4149		0.1256	A5
A6	>						>												>							A6
A4F	id				id														id				id			A4F
A5F	>					>														?(>)		id				A5F
A4H	>				>														?(<)						0.0013	A4H
A5H	>					>														?(>)				>		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E156. Results of Hypothesis Test 3 for Density and furnish FD7.

Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case
Con		0.0006	<.0001	<.0001	<.0001	<.0001	0.0000	<.0001	0.0000	<.0001	id	0.0000	<.0001	<.0001	0.0001	<.0001	0.0000	<.0001	0.0000	<.0001	<.0001	id	<.0001	<.0001	<.0001	Con
D1	>		0.0017	0.0011	0.0008			0.0002			id			0.0007			0.0003									D1
D2	>	>				0.0009			<.0001						0.4180			0.0004								D2
D3	>	>					0.5945			0.0474						0.1025										D3
D4	>	<				<.0001	<.0001					0.0130							0.0002			id		<.0001		D4
D5	>		<		>								<.0001							0.0003			<.0001		<.0001	D5
D6	>			?(<)	>																<.0001					D6
C1S	>	>							0.0003	0.0139	id			0.7477												C1S
C2S	>		>					>							0.0010											C2S
C3S	>			>				<								0.0247										C3S
A1S	id	id						id				id					id									A1S
A4S	>				<						id		0.5120						0.0000							A4S
A5S	>					<						?(>)								0.0058						A5S
C1	>	>						?(<)							0.0341	0.0049	0.4345									C1
C2	>		?(<)						<					<				0.6462								C2
C3	>			?(<)						<				<												C3
A1	>	>									id			?(<)				0.0001	0.2244							A1
A2	>		<												?(<)		<			0.0006							A2
A4	>				>							>					?(<)			0.0004	0.0008	id		0.1125		A4
A5	>					<							>					<	<				<.0001		<.0001	A5
A6	>						>												>							A6
A4F	id				id														id				id			A4F
A5F	>					>														>		id				A5F
A4H	>				>														?(<)						<.0001	A4H
A5H	>					>														>				>		A5H
Case	Con	D1	D2	D3	D4	D5	D6	C1S	C2S	C3S	A1S	A4S	A5S	C1	C2	C3	A1	A2	A4	A5	A6	A4F	A5F	A4H	A5H	Case

Table E157. Results of Hypothesis Test 3 for Density, comparing furnishes.

Case	Con WF1	Con WF2	Con WF3	Con FD5	Con FD6	Con FD7	D1 WF1	D1 WF2	D1 WF3	D1 FD5	D1 FD6	D1 FD7	D2 WF1	D2 WF2	D2 WF3	D2 FD5	D2 FD6	D2 FD7	Case
Con WF1		<.0001	0.0000	<.0001	<.0001														Con WF1
Con WF2	>			<.0001	<.0001														Con WF2
Con WF3	>			<.0001		<.0001													Con WF3
Con FD5	>	>	>		<.0001	<.0001													Con FD5
Con FD6	>	<		<		<.0001													Con FD6
Con FD7			>	<	>														Con FD7
D1 WF1								0.0069	0.0139	0.1173	0.0791								D1 WF1
D1 WF2							>			0.1335	0.0495								D1 WF2
D1 WF3							>			0.2865		0.2664							D1 WF3
D1 FD5							?(>)	?(<)	?(<)		0.7772	0.7799							D1 FD5
D1 FD6							>	<		?(<)		0.2736							D1 FD6
D1 FD7									?(<)	?(>)	?(>)								D1 FD7
D2 WF1														0.0014	0.1190	0.0444	0.1251		D2 WF1
D2 WF2													>			<.0001	0.0000		D2 WF2
D2 WF3													?(>)			0.0012		0.0171	D2 WF3
D2 FD5													<	<	<		0.2840	0.0037	D2 FD5
D2 FD6													?(<)	<		?(>)		0.1557	D2 FD6
D2 FD7															<	>	?(>)		D2 FD7
Case	Con WF1	Con WF2	Con WF3	Con FD5	Con FD6	Con FD7	D1 WF1	D1 WF2	D1 WF3	D1 FD5	D1 FD6	D1 FD7	D2 WF1	D2 WF2	D2 WF3	D2 FD5	D2 FD6	D2 FD7	Case
	D3	D3	D3	D3	D3	D3	D4	D4	D4	D4	D4	D4	D5	D5	D5	D5	D5	D5	
D3 WF1		0.0104	0.0074	0.8990	0.0023														D3 WF1
D3 WF2	>			0.0126	0.0001														D3 WF2
D3 WF3	>			0.0060		0.0324													D3 WF3
D3 FD5	?(>)	<	<		0.0014	0.1068													D3 FD5
D3 FD6	<	<		<		0.0000													D3 FD6
D3 FD7			<	?(>)	>														D3 FD7
D4 WF1								0.3618	0.1727	0.0504	0.0167								D4 WF1
D4 WF2							?(>)			0.0034	<.0001								D4 WF2
D4 WF3							?(>)			0.0005		0.0002							D4 WF3
D4 FD5							<	<	<		0.3225	0.1968							D4 FD5
D4 FD6							<	<		?(<)		0.0020							D4 FD6
D4 FD7									<	?(>)	>								D4 FD7
D5 WF1														0.2861	0.0401	<.0001	0.0002		D5 WF1
D5 WF2													?(<)			<.0001	0.0003		D5 WF2
D5 WF3													>			<.0001		0.0000	D5 WF3
D5 FD5													<	<	<		0.1170	0.2246	D5 FD5
D5 FD6													<	<		?(>)		0.3361	D5 FD6
D5 FD7															<	?(>)	?(<)		D5 FD7
Case	D3 WF1	D3 WF2	D3 WF3	D3 FD5	D3 FD6	D3 FD7	D4 WF1	D4 WF2	D4 WF3	D4 FD5	D4 FD6	D4 FD7	D5 WF1	D5 WF2	D5 WF3	D5 FD5	D5 FD6	D5 FD7	Case

Table E158. Results of Hypothesis Test 3 for Density, comparing furnishes continued.

Case	D6 WF1	D6 WF2	D6 WF3	D6 FD5	D6 FD6	D6 FD7	C1S WF1	C1S WF2	C1S WF3	C1S FD5	C1S FD6	C1S FD7	C2S WF1	C2S WF2	C2S WF3	C2S FD5	C2S FD6	C2S FD7	Case
D6 WF1		0.0002	0.0001	<.0001	<.0001														D6 WF1
D6 WF2	<			0.0001	0.0000														D6 WF2
D6 WF3	<			0.0130		0.0531													D6 WF3
D6 FD5	<	<	<		0.0344	<.0001													D6 FD5
D6 FD6	<	<		<		<.0001													D6 FD6
D6 FD7			>	>	>														D6 FD7
C1S WF1								0.2213	0.0498	0.5018	0.9746								C1S WF1
C1S WF2							?(>)			0.2835	0.1033								C1S WF2
C1S WF3							>			0.0186		0.5706							C1S WF3
C1S FD5							?(>)	?(<)	<		0.2318	0.0001							C1S FD5
C1S FD6							?(>)	?(<)		?(<)		0.0039							C1S FD6
C1S FD7									?(<)	>	>								C1S FD7
C2S WF1														0.0000	0.0045	<.0001	0.3767		C2S WF1
C2S WF2													>			<.0001	0.0174		C2S WF2
C2S WF3													>			<.0001		0.0525	C2S WF3
C2S FD5													<	<	<		0.0009	<.0001	C2S FD5
C2S FD6													?(>)	<		>		1.0000	C2S FD6
C2S FD7															<	>	?(>)		C2S FD7

Case	D6 WF1 C3S	D6 WF2 C3S	D6 WF3 C3S	D6 FD5 C3S	D6 FD6 C3S	D6 FD7 C3S	C1S WF1 A1S	C1S WF2 A1S	C1S WF3 A1S	C1S FD5 A1S	C1S FD6 A1S	C1S FD7 A1S	C2S WF1 A4S	C2S WF2 A4S	C2S WF3 A4S	C2S FD5 A4S	C2S FD6 A4S	C2S FD7 A4S	Case
C3S WF1		1.0000	0.0319	0.0284	0.0716														C3S WF1
C3S WF2	?(>)			<.0001	0.0000														C3S WF2
C3S WF3	<			0.3669		0.0187													C3S WF3
C3S FD5	<	<	?(<)		0.0007	<.0001													C3S FD5
C3S FD6	<	<		>		0.0236													C3S FD6
C3S FD7			>	>	>														C3S FD7
A1S WF1								id	id	id	id								A1S WF1
A1S WF2							id			id	id								A1S WF2
A1S WF3							id			id		id							A1S WF3
A1S FD5							id	id	id		id	id							A1S FD5
A1S FD6							id	id		id		id							A1S FD6
A1S FD7									id	id	id								A1S FD7
A4S WF1														0.0013	0.0678	0.0018	<.0001		A4S WF1
A4S WF2													<			0.0156	0.0001		A4S WF2
A4S WF3													<			0.0062		0.0008	A4S WF3
A4S FD5													<	<	<		0.4695	0.4235	A4S FD5
A4S FD6													<	<		?(>)		0.8413	A4S FD6
A4S FD7															<	?(>)	?(>)		A4S FD7
Case	C3S WF1	C3S WF2	C3S WF3	C3S FD5	C3S FD6	C3S FD7	A1S WF1	A1S WF2	A1S WF3	A1S FD5	A1S FD6	A1S FD7	A4S WF1	A4S WF2	A4S WF3	A4S FD5	A4S FD6	A4S FD7	Case

Table E159. Results of Hypothesis Test 3 for Density, comparing furnishes continued.

Case	A5S WF1	A5S WF2	A5S WF3	A5S FD5	A5S FD6	A5S FD7	C1 WF1	C1 WF2	C1 WF3	C1 FD5	C1 FD6	C1 FD7	C2 WF1	C2 WF2	C2 WF3	C2 FD5	C2 FD6	C2 FD7	Case
A5S WF1		id	id	id	id														A5S WF1
A5S WF2	id			0.1013	0.0035														A5S WF2
A5S WF3	id			0.3584		0.6245													A5S WF3
A5S FD5	id	?(<)	?(>)		0.0271	0.0007													A5S FD5
A5S FD6	id	<		<		0.4694													A5S FD6
A5S FD7			?(<)	<	?(<)														A5S FD7
C1 WF1								0.8015	0.7412	0.0141	0.0061								C1 WF1
C1 WF2							?(<)			0.0153	0.0056								C1 WF2
C1 WF3							?(<)			0.0032		0.0988							C1 WF3
C1 FD5							<	<	<		0.2568	0.0046							C1 FD5
C1 FD6							<	<		?(<)		0.0016							C1 FD6
C1 FD7									<	>	>								C1 FD7
C2 WF1														0.0808	0.1097	0.0108	0.0050		C2 WF1
C2 WF2													<			<.0001	<.0001		C2 WF2
C2 WF3													?(<)			<.0001		0.0023	C2 WF3
C2 FD5													<	<	<		0.8915	0.1533	C2 FD5
C2 FD6													<	<		?(<)		0.1780	C2 FD6
C2 FD7															<	?(<)	?(<)		C2 FD7
Case	A5S WF1 C3	A5S WF2 C3	A5S WF3 C3	A5S FD5 C3	A5S FD6 C3	A5S FD7 C3	C1 WF1 A1	C1 WF2 A1	C1 WF3 A1	C1 FD5 A1	C1 FD6 A1	C1 FD7 A1	C2 WF1 A2	C2 WF2 A2	C2 WF3 A2	C2 FD5 A2	C2 FD6 A2	C2 FD7 A2	Case
C3 WF1		0.5152	0.1448	0.0226	0.4842														C3 WF1
C3 WF2	?(<)			0.0024	0.0524														C3 WF2
C3 WF3	?(>)			0.0045		0.0025													C3 WF3
C3 FD5	<	<	<		0.0001	0.5847													C3 FD5
C3 FD6	?(>)	>		>		0.0015													C3 FD6
C3 FD7			<	?(<)	<														C3 FD7
A1 WF1								0.1521	0.0020	0.0001	0.0042								A1 WF1
A1 WF2							?(<)			<.0001	0.0001								A1 WF2
A1 WF3							<			<.0001		0.3348							A1 WF3
A1 FD5							<	<	<		<.0001	0.0000							A1 FD5
A1 FD6							<	<		>		0.9711							A1 FD6
A1 FD7									?(>)	>	?(>)								A1 FD7
A2 WF1														0.0213	<.0001	<.0001	0.0005		A2 WF1
A2 WF2													<			0.0001	0.0045		A2 WF2
A2 WF3													<			0.0094		0.0008	A2 WF3
A2 FD5													<	<	<		0.0030	0.1538	A2 FD5
A2 FD6													<	<		>		0.0077	A2 FD6
A2 FD7															<	?(>)	<		A2 FD7
Case	C3 WF1	C3 WF2	C3 WF3	C3 FD5	C3 FD6	C3 FD7	A1 WF1	A1 WF2	A1 WF3	A1 FD5	A1 FD6	A1 FD7	A2 WF1	A2 WF2	A2 WF3	A2 FD5	A2 FD6	A2 FD7	Case

Table E160. Results of Hypothesis Test 3 for Density, comparing furnishes continued.

Case	A4 WF1	A4 WF2	A4 WF3	A4 FD5	A4 FD6	A4 FD7	A5 WF1	A5 WF2	A5 WF3	A5 FD5	A5 FD6	A5 FD7	A6 WF1	A6 WF2	A6 WF3	A6 FD5	A6 FD6	A6 FD7	Case
A4 WF1		0.0966	0.0404	<.0001	0.0486														A4 WF1
A4 WF2	>			0.0000	0.0054														A4 WF2
A4 WF3	>			0.0001		0.0089													A4 WF3
A4 FD5	<	<	<		0.0087	0.0001													A4 FD5
A4 FD6	<	<		>		0.3225													A4 FD6
A4 FD7			<	>	?(>)														A4 FD7
A5 WF1								0.1053	0.3005	id	0.0016								A5 WF1
A5 WF2							?(<)			id	0.0321								A5 WF2
A5 WF3							?(<)			id		<.0001							A5 WF3
A5 FD5							id	id	id		id	id							A5 FD5
A5 FD6							<	<		id		0.0013							A5 FD6
A5 FD7									<	id	<								A5 FD7
A6 WF1														0.0000	0.0004	0.0020	0.0000		A6 WF1
A6 WF2													>			0.0000	0.1547		A6 WF2
A6 WF3													>			<.0001		0.8805	A6 WF3
A6 FD5													<	<	<		0.0003	0.0000	A6 FD5
A6 FD6													>	?(<)		>		0.1109	A6 FD6
A6 FD7															?(>)	>	?(>)		A6 FD7

Case	A4 WF1 A5F	A4 WF2 A5F	A4 WF3 A5F	A4 FD5 A5F	A4 FD6 A5F	A4 FD7 A5F	A5 WF1 A4H	A5 WF2 A4H	A5 WF3 A4H	A5 FD5 A4H	A5 FD6 A4H	A5 FD7 A4H	A6 WF1 A5H	A6 WF2 A5H	A6 WF3 A5H	A6 FD5 A5H	A6 FD6 A5H	A6 FD7 A5H	Case
A5F WF1		0.1503	0.5947	id	0.2418														A5F WF1
A5F WF2	?(<)			id	0.0288														A5F WF2
A5F WF3	?(>)			id		0.2208													A5F WF3
A5F FD5	id	id	id		id	id													A5F FD5
A5F FD6	?(>)	>		id		0.7357													A5F FD6
A5F FD7			?(>)	id	?(<)														A5F FD7
A4H WF1								0.8164	0.7689	id	0.0352								A4H WF1
A4H WF2							?(<)			id	0.0044								A4H WF2
A4H WF3							?(>)			id		0.3101							A4H WF3
A4H FD5							id	id	id		id	id							A4H FD5
A4H FD6							>	>		id		0.2686							A4H FD6
A4H FD7									?(>)	id	?(>)								A4H FD7
A5H WF1														0.9367	<.0001	id	0.2559		A5H WF1
A5H WF2													?(>)			id	0.6279		A5H WF2
A5H WF3													<			id		<.0001	A5H WF3
A5H FD5													id	id	id		id	id	A5H FD5
A5H FD6													?(>)	?(>)		id		0.1041	A5H FD6
A5H FD7															>	id	?(>)		A5H FD7

Case	A5F WF1	A5F WF2	A5F WF3	A5F FD5	A5F FD6	A5F FD7	A4H WF1	A4H WF2	A4H WF3	A4H FD5	A4H FD7	A5H WF1	A5H WF2	A5H WF3	A5H FD5	A5H FD6	A5H FD7	Case

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