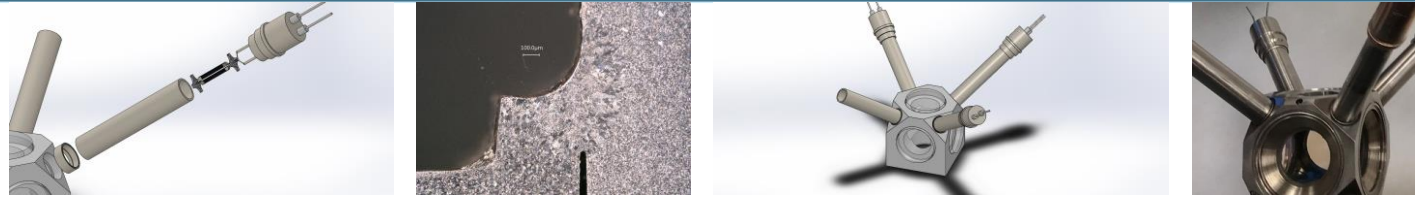
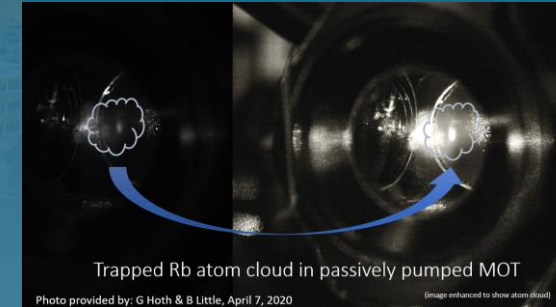




Fabricating a passively pumped vacuum chamber for cold-atom experiments



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Vision/Motivation

“Build the world’s first truly portable, compact atom interferometer inertial sensor.”

Because quantum sensors generally have at least 1-2 orders of magnitude better resolution than current state of the art techniques, they are uniquely suited to be used in such applications as:

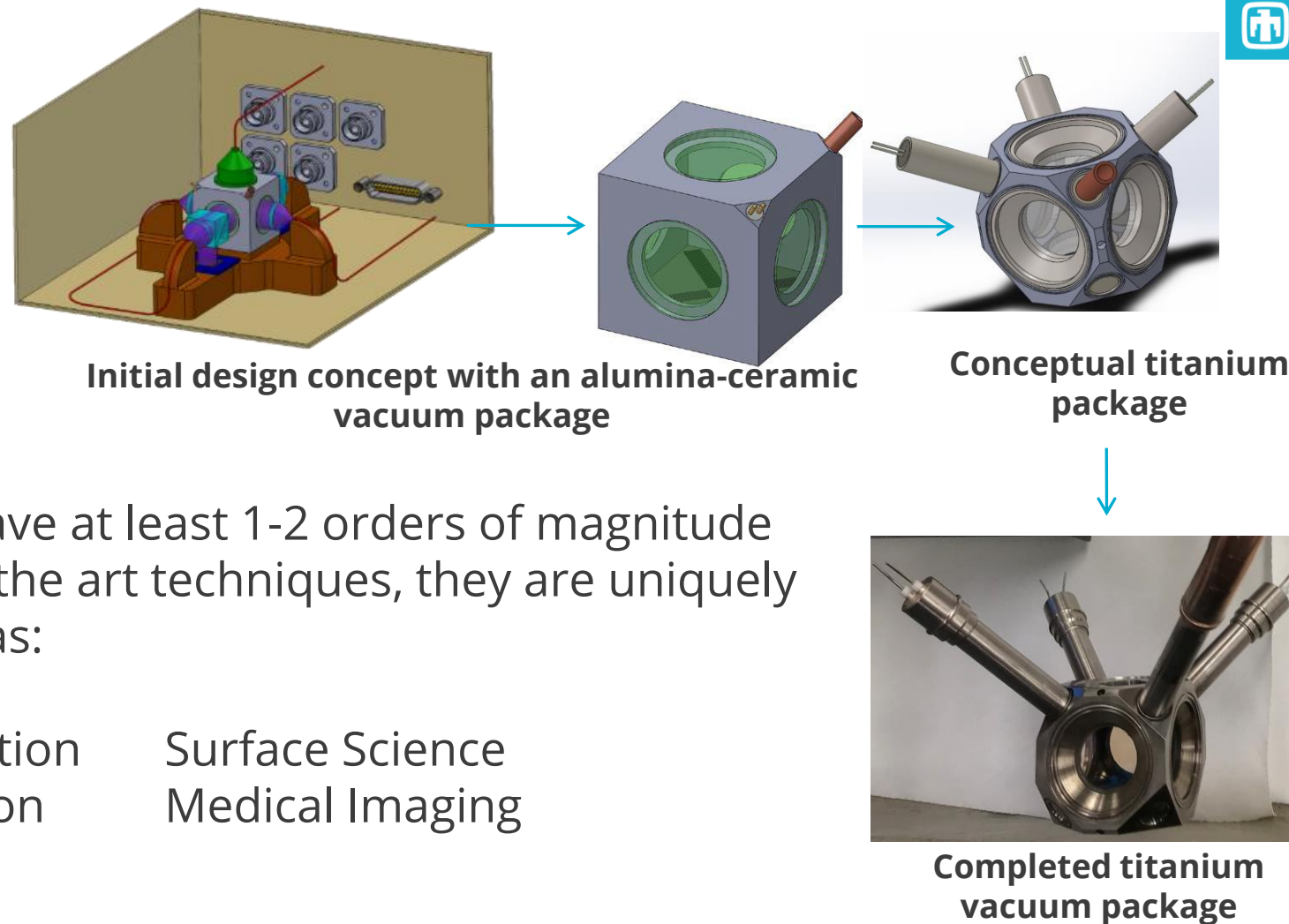
Timing
Navigation
Gravimetry

Non Destructive Evaluation
Trace Chemical Detection

Surface Science
Medical Imaging

This presentation, approximately 15 minutes in duration, will summarize a 3-year multi-person effort, describing how small vacuum chambers, capable of supporting a magneto optical trap (MOT), via laser-cooling*, were successfully fabricated.

*Temperature: $\sim 5\mu\text{K}$ (5×10^{-6} Kelvin)

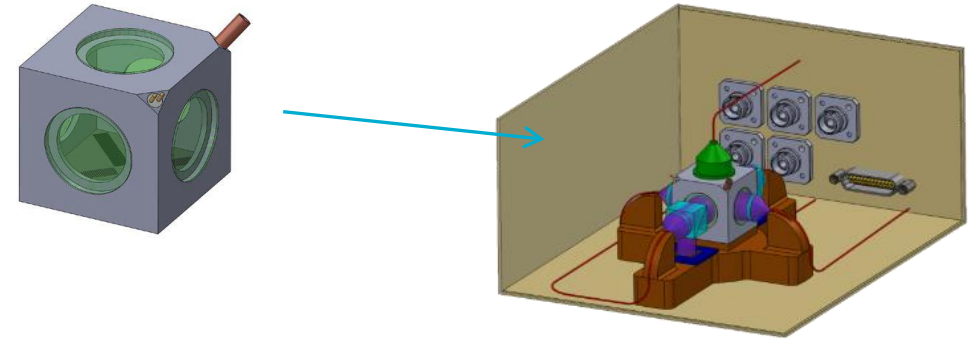


Background: High-vacuum Chamber Features

Required features

- Supply alkali metal (Rb) atoms
- Non or nearly nonmagnetic chamber and feedthroughs
- Small footprint, $\sim 5 \text{ cm}^3$ volume to function as an atom interferometer (AI) accelerometer
- Must provide optical windows for laser access
- Must have negligible helium permeation
- ***Maintain high-vacuum for months**
 - $P_{\text{Rb}} \sim 10^{-7} \text{ Torr}$; $P_{\text{background}} \sim 10^{-8} \text{ Torr}$

*Key Vacuum System Challenges



Desired Features

- ***Electrically activated contaminant-free alkali metal source.**
- 100% glass-free
- Windows with nearly zero helium permeability, AR coating, and no birefringence
 - Include passive (getter) pumping
 - Support up to 6 months “pumpless” vacuum package operation.
- MOT diffraction grating internal to vacuum package
- Copper pinch-off tube for sealing
- Bakeable to $\sim 400^\circ \text{C}$.
- Zero/low electrical conductivity ($\ll \ll$ eddy currents)

Materials & Components Selection



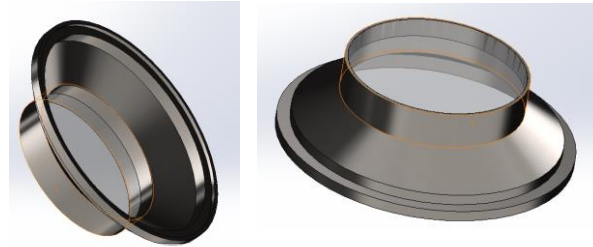
Component	Material	Heat sensitive	Atmosphere sensitive	Notes
Chamber	Titanium*	No	No	Grade-2 (commercially pure). Can be welded without the formation of intermetallics
Chamber	Alumina Ceramic	No	No	94% - 98% Al_2O_3
Non-evaporable getters (NEG)	NEG, St 172*	Yes	Yes	Sensitive above 250°C in O_2 containing environments
Alkali Metal Dispenser (AMD)	AMD, Rb*	Yes	Yes	Sensitive above 250°C in O_2 containing environments
Window	Sapphire w/Ti frame*	No	No	Brazed into frames. Able to withstand 450°C+ temperatures
Window	Sapphire w/o frame	Yes	No	CTE mismatch with Ti body could be problematic
Window	Fused Silica w/Ti frame	No	No	Brazed into frames. Able to withstand 450°C+ temperatures
Window	Fused Silica w/o frame	Yes	No	CTE mismatch with Ti body could be problematic
Grating MOT	Si wafer*	Yes	No	Need to keep below 250°C
Electrical feedthroughs	Ti bodies, Mo* conductors	No	No	Grade-2 Ti, brazed to Al_2O_3 insulators and Mo pins
Electrical feedthroughs	Stainless-steel bodies	No	No	Used initially until Ti bodies became available. Pins are Mo.
NEG & AMD bodies	Ti tubing*	No	No	Grade-2 Ti
Exhaust tubing	Ti and/or Ti/Cu*	No	No	Brazed to adapters as needed.

*Candidate materials selected for first iteration of vacuum chamber assemblies

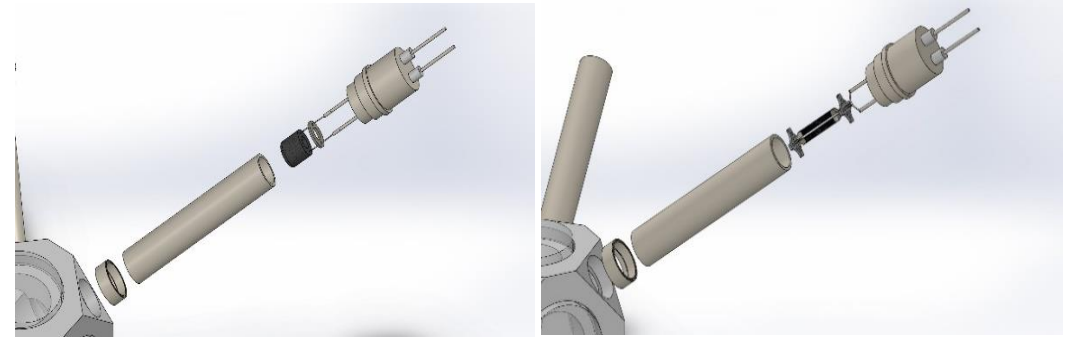
Chamber Components Construction



Window Assemblies
Getter Assemblies
Alkali Metal
Dispensers
Exhaust Manifolds



Sapphire window/CP titanium flanges



Non-evaporable getter assembly (L), Alkali metal dispenser assembly (R)

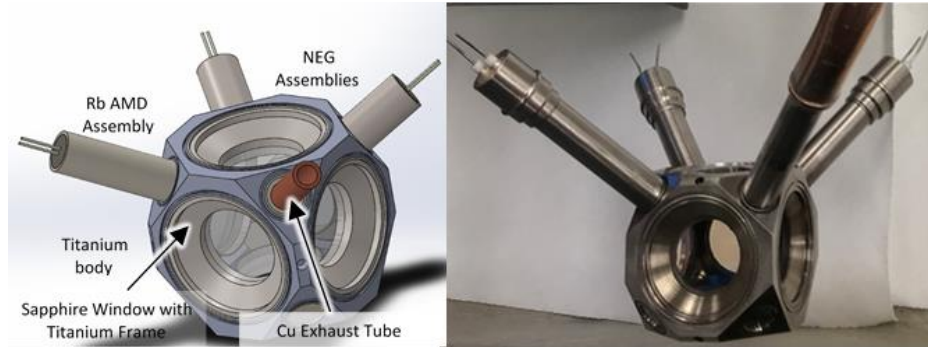
Joining Processes

Welding Processes

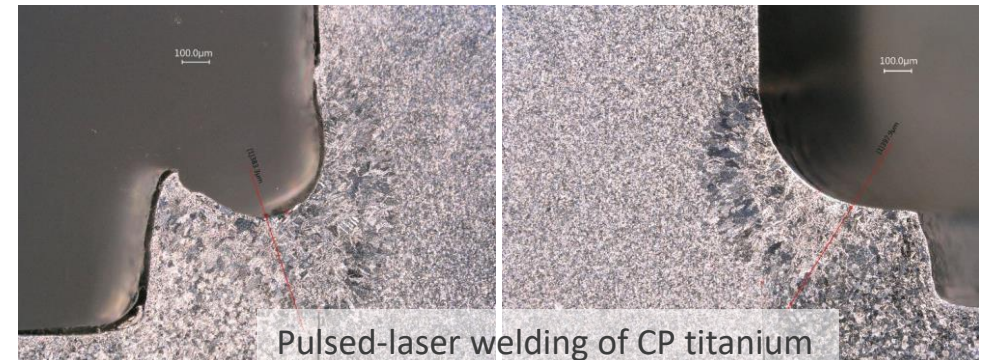
- Pulsed-laser
- Resistance
- Orbital
- TIG

Brazing Processes

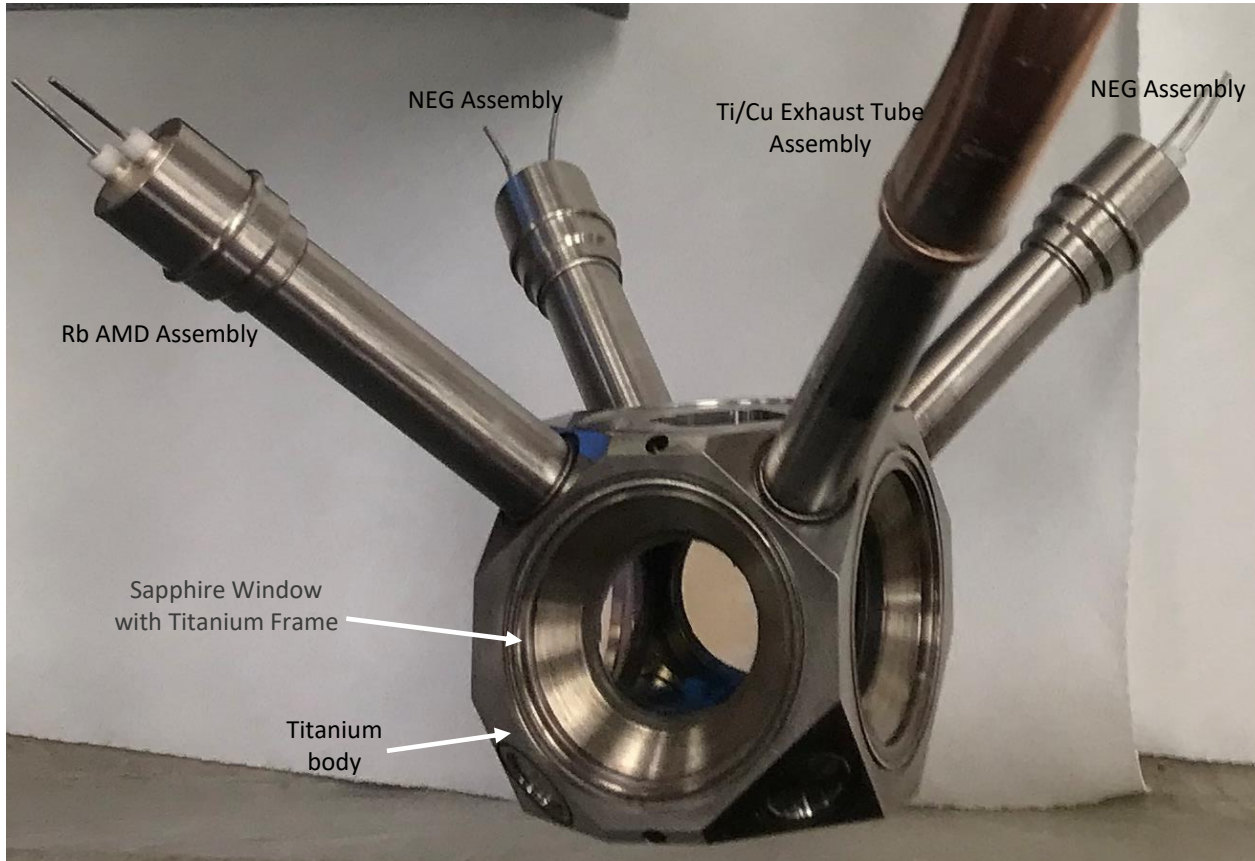
- Vacuum Furnace
- Hydrogen/Oxygen Torch
- Hand-held Induction



Sapphire window/CP titanium flanges



Pulsed-laser welding of CP titanium



Completed Titanium Vacuum Package



Solid-model of Titanium chamber/UHV manifold assembly

Sapphire-Alumina Ceramic Braze Development

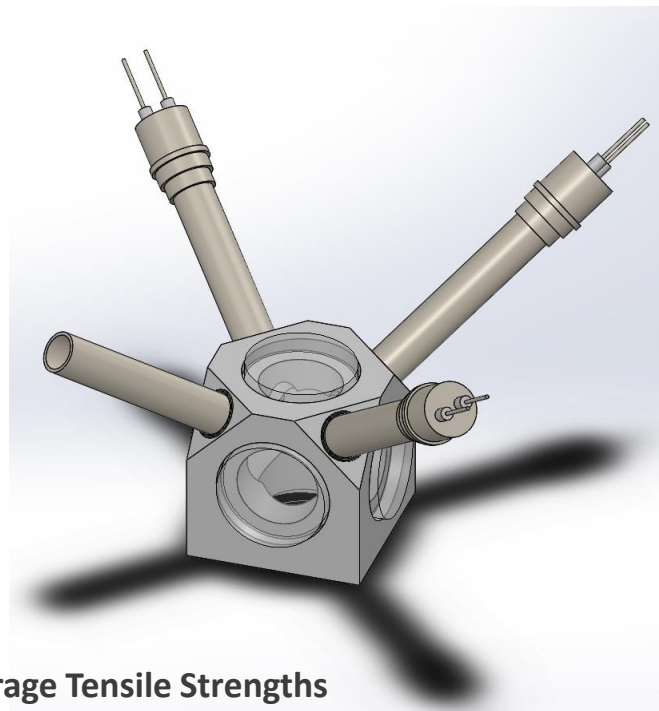
Alumina-ceramic chamber design restrictions:

- Ten simultaneous active filler metal brazements (6 ea. sapphire window, 4 titanium weld sleeves) was determined to be too risky, as any leaks detected would be difficult to repair.
- The requirement that any metallization system used be nonmagnetic eliminated those utilizing nickel plating.

Solution:

A COTS titanium-hydride/organic carrier metallization system (Tiger Ink) was selected for use after robust testing using with conventional silver-based brazing filler metals (BVAg-0, BVAg-8, and BVAg-29).

All of the ceramic tensile button samples and sapphire window-ceramic window frame samples fabricated using the Tiger-Ink metallization were hermetic (Helium leak rate <5E-12 atm/cc-sec).



Average Tensile Strengths

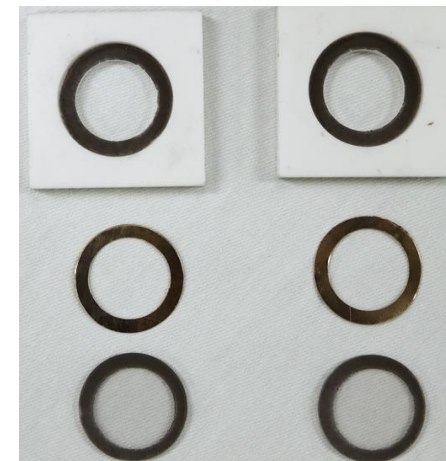
96% Alumina Ceramic ASTM F-19
Tensile Buttons w/TiH₂ metallization.
No metal interlayers.

Braze Filler Metal AWS Classification	Stress at failure KSI / MPa
BVAg-0	21.4 / 147.5
BVAg-8	23.7 / 163.4
BVAg-29	22.8 / 157.2

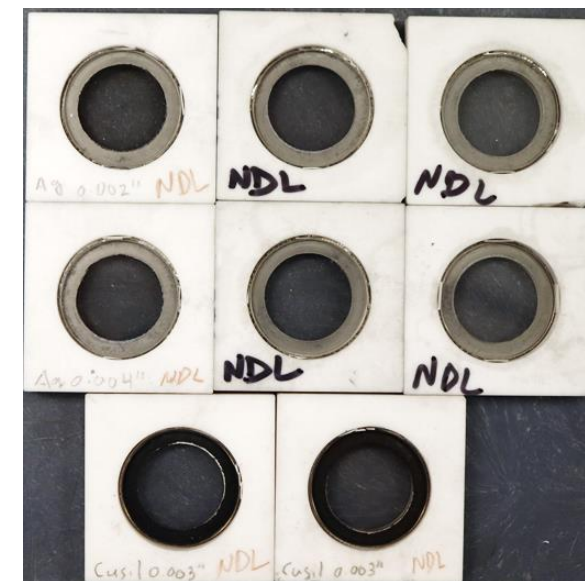
Tensile testing (ASTM F-19)
Instron 5969, Rate: 3×10^{-4} inch/sec



Fractured ASTM F-19 Tensile Buttons.

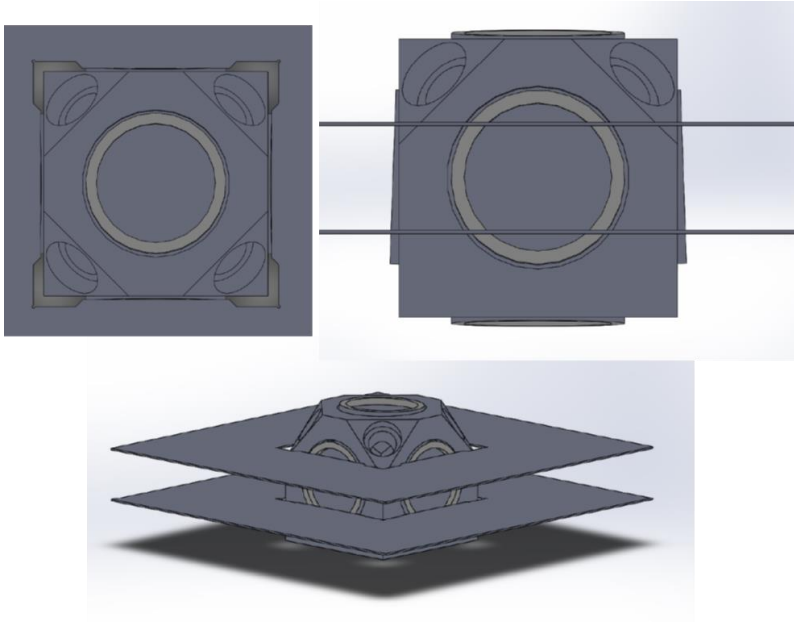


Metallized ceramic and sapphire windows with BFM preforms

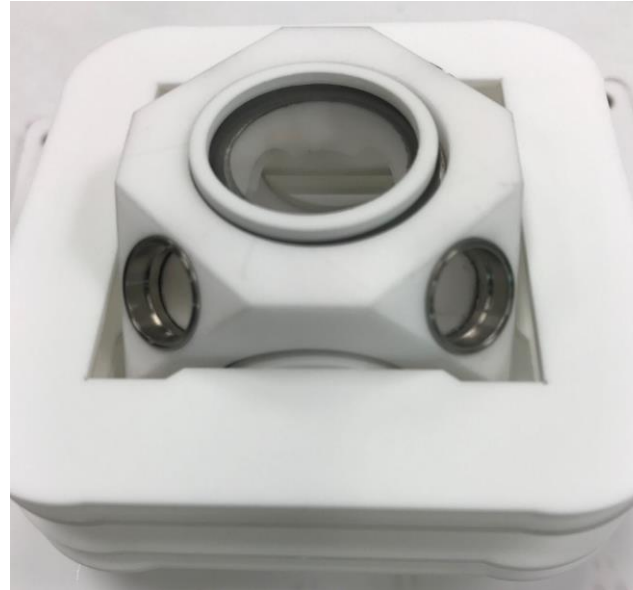


Brazed Alumina ceramic-sapphire window samples.

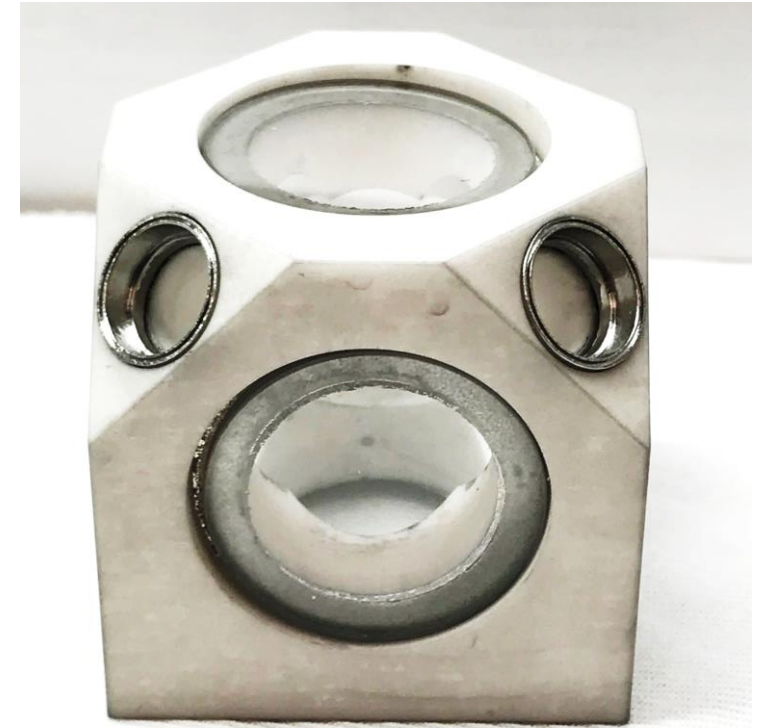
Alumina-Ceramic Vacuum Chamber Assembly



Solid Model of Ceramic Chamber with
Laser-Machined Alumina Ceramic
Fixturing



Alumina Ceramic Chamber with Laser-
Machined Alumina Ceramic Fixturing Prior
to Brazing

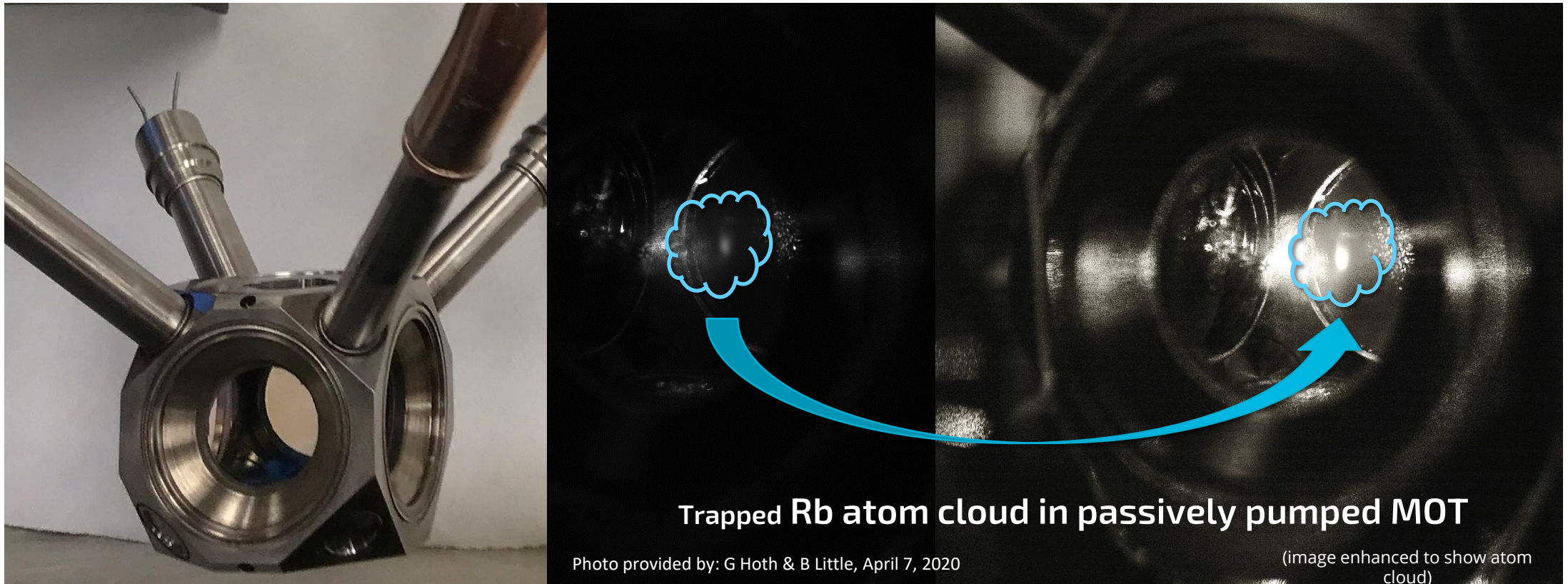


Brazed Ceramic
Chamber

Conclusion



- Multiple small titanium vacuum chambers, capable of supporting a magneto optical trap (MOT), via laser-cooling were successfully fabricated and tested.
- Alumina ceramic chambers were partially constructed, but not completed.
- Chambers removed from external vacuum sources have been supporting a MOT for over 450 days.



Thank you for your time & attention!



Acknowledgements

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