

# Analysis to support revised distance between bulk liquid hydrogen systems and exposures

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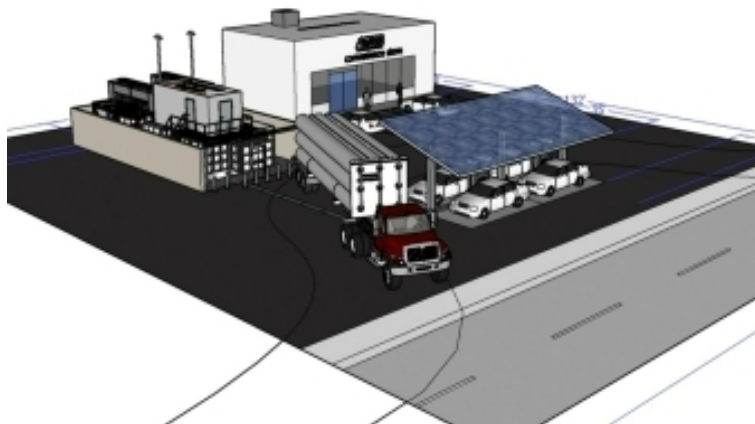
Edinburgh, Scotland, September 21-24, 2021



# Current separation distances for liquid hydrogen systems in NFPA 2 are based on consensus without a documented scientific analysis

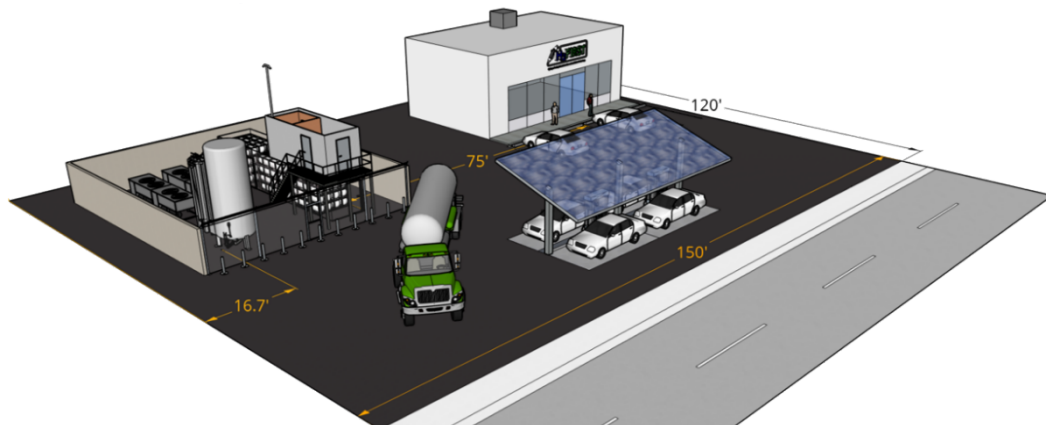
## Compressed H<sub>2</sub> storage

- Previous work by Sandia led to science-based gaseous H<sub>2</sub> separation distances



## Liquid H<sub>2</sub> storage

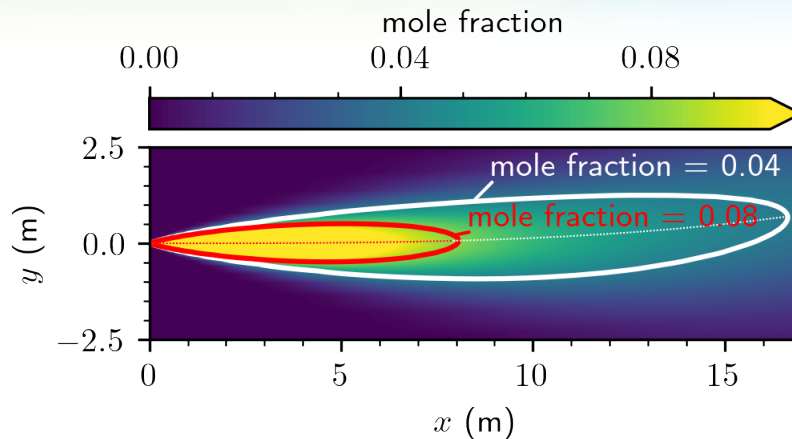
- Even with credits for insulation and fire-rated barrier wall, 75 ft. offset to building intakes and parking make footprint large



## Lab-scale validated models have been used to perform an analysis for updated LH<sub>2</sub> separation distances in NFPA 2

- Same criteria as for bulk gaseous setbacks
  - Aside from cryogenic burns, hazards from liquid hydrogen leaks/flames are similar to gaseous hydrogen
  - Considers flammable region (dispersion of unignited hydrogen), and hazards from jet flames
  - Added unconfined overpressure from a delayed ignition
- Leak scenario
  - 1% of flow area (same as current gaseous setbacks)
  - Multiple pipe sizes (0.1" – 3", 2.5 - 76mm) and pressures (60 – 180 psi, 414 – 1240 kPa)
- Distance criteria
  - Group 1: greater of the distances to 8% concentration or 4.732 kW/m<sup>2</sup>
  - Group 2: distance to a heat flux of 4.732 kW/m<sup>2</sup>
  - Group 3: distance to visible flame length or heat flux of 20 kW/m<sup>2</sup>
- Safety factor of 2 (current gaseous setbacks use 1.5)

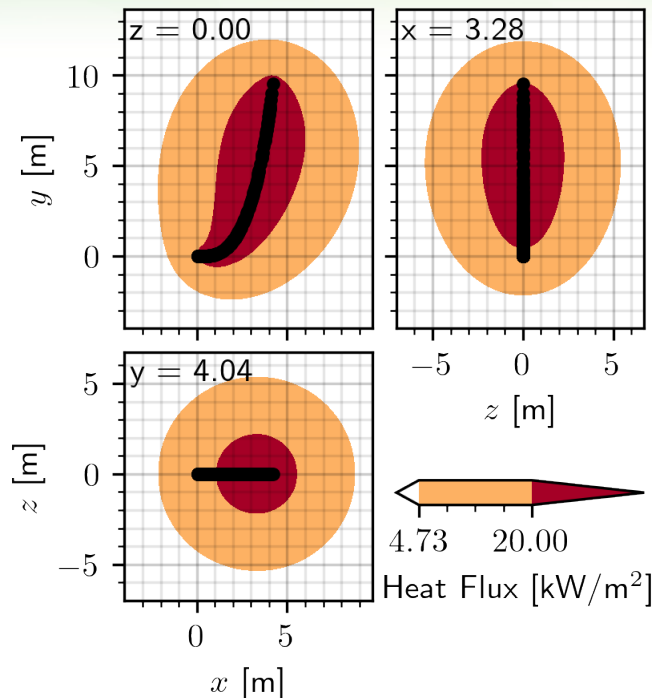
# Unignited dispersion simulations show that jets are neutrally buoyant



1% area of 76 mm (3") diameter pipe, 414 kPa (30 psi), saturated vapor release

- Even for the lowest momentum release, jets do not curve significantly either up or down due to buoyancy
- Conservative streamline (curved) distance to 8% concentration level used to calculate hazard distance

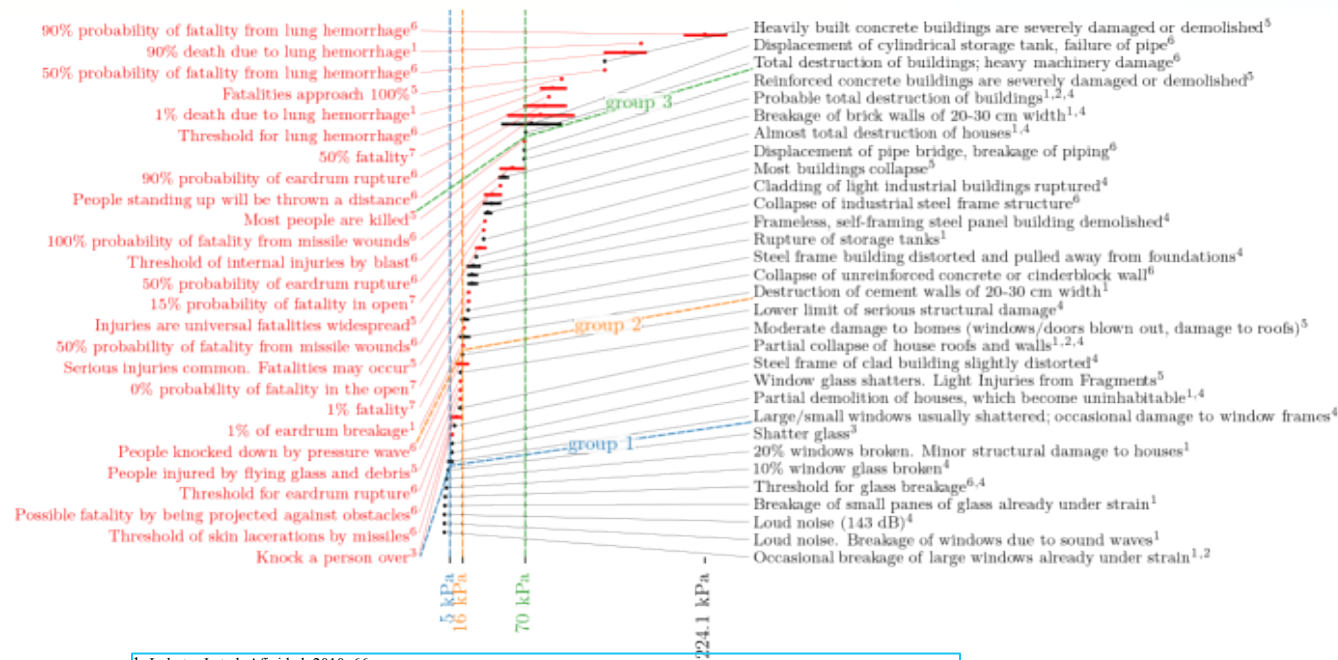
## Even high momentum flames are quite buoyant



- A flame with high momentum curves significantly upwards due to buoyancy
- Flame length and heat flux values for separation distances calculated from bird's eye view ( $xz$ -plane)

1% area of 76 mm (3") diameter pipe, 1.2 MPa (180 psi), critical temperature (33.1 K)

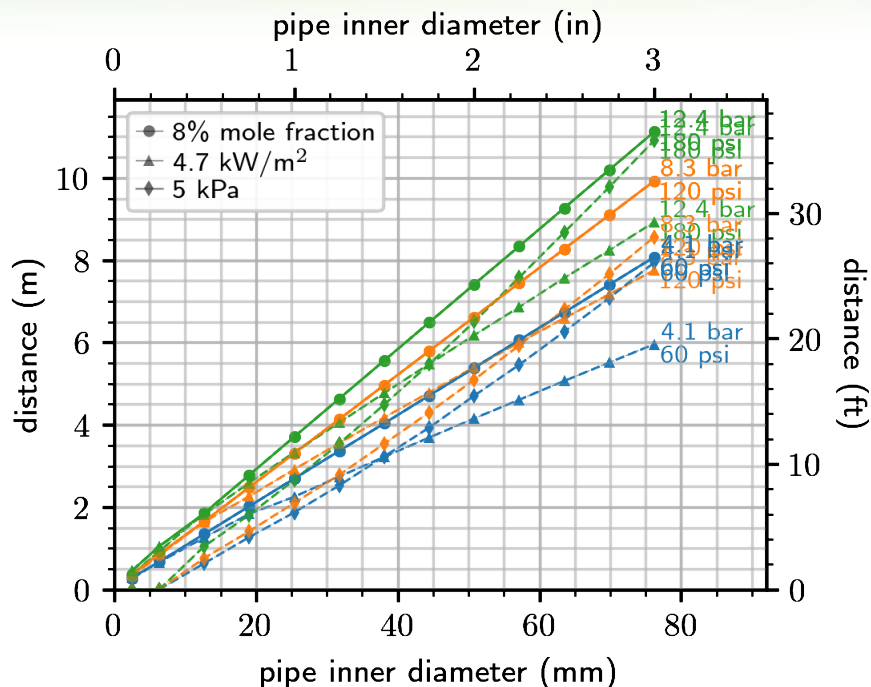
# Overpressure harm criteria were reviewed, with selection of Groups 1, 2, and 3 criteria



- Group 1: no harm to people, small chance of property damage
  - Selected criteria: 5 kPa
- Group 2: small risk of injury to people but negligible risk of fatality, minor property damage
  - Selected criteria: 16 kPa
- Group 3: moderate risk of fatalities, major (but not complete) property damage
  - Selected criteria: 70 kPa

1. Lobato, J. et al. Afinidad, 2010, 66
2. Huang, Ma. Int. J. Hydrog. Energy, 2018, 43, 442-454
3. Jallais et al. Proc. Safety Prog., 2018, 37, 397-410
4. "Preliminary Quantitative Risk Analysis (QRA) of the Texas Clean Energy Project", 2010
5. Argo, & Sandstrom, "Separation Distances in NFPA Codes and Standards" 2014
6. LaChance et al. Int. J. Hydrog. Energy, 2011, 36, 2381-2388
7. "Methods of approximation and determination of human vulnerability for offshore major accident hazard assessment." 2010

# The distance to an 8% mole fraction is limiting for group 1 exposures



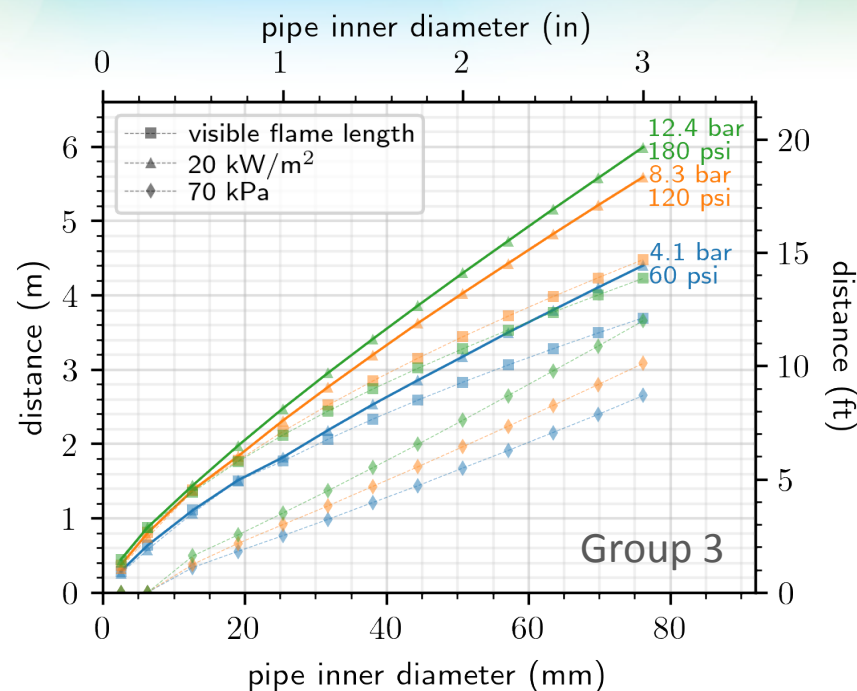
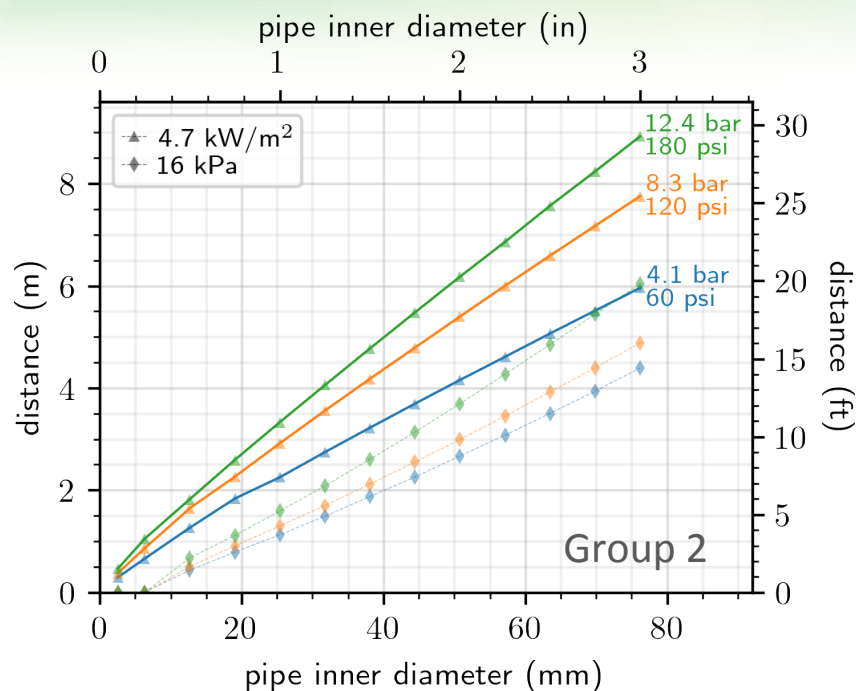
- Distance is the largest of:

- Mole fraction of 8%
- Heat flux of 4.7 kW/m<sup>2</sup>
- Overpressure of 5 kPa

➤ Even at maximum system pressure and diameter, hazard distance (11 m) is less than current air intake/parking distance (23 m)

- Most systems have smaller pipes ( $\leq 38$  mm) and operate at lower pressures ( $\leq 8$  bar)
- Safety factor increases for actual exposure distance

# Similar calculations result in hazard distances for groups 2 and 3

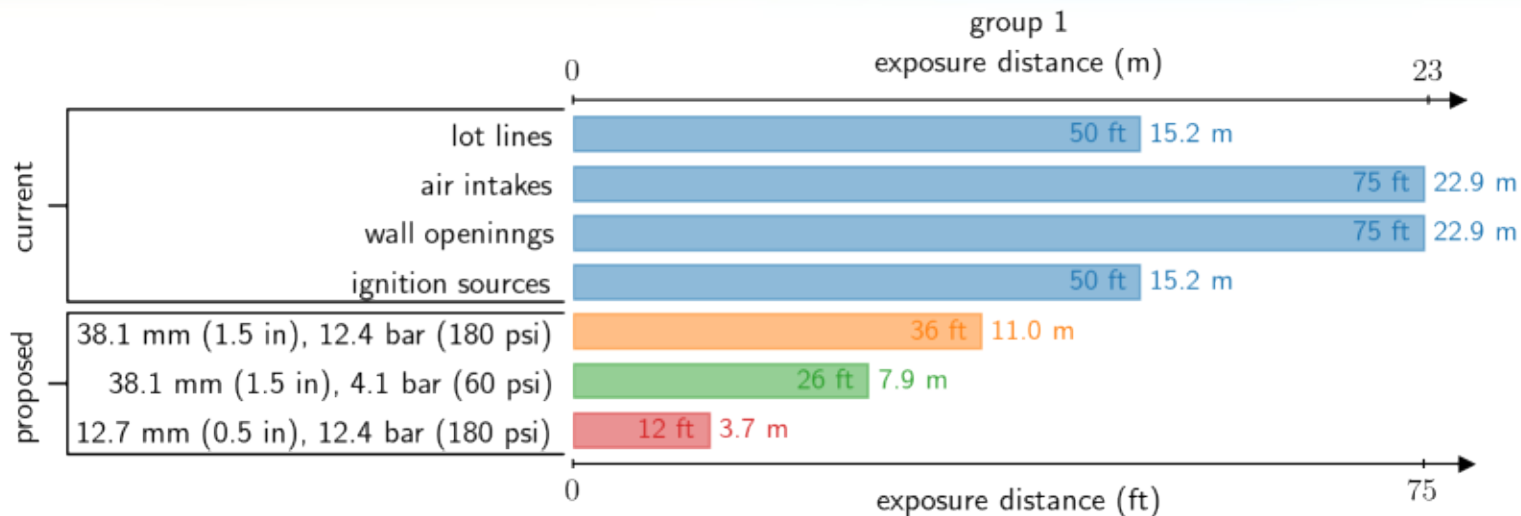


- Distances to specified heat flux tends to be the largest
- Hazard distances for group 3 can be significant



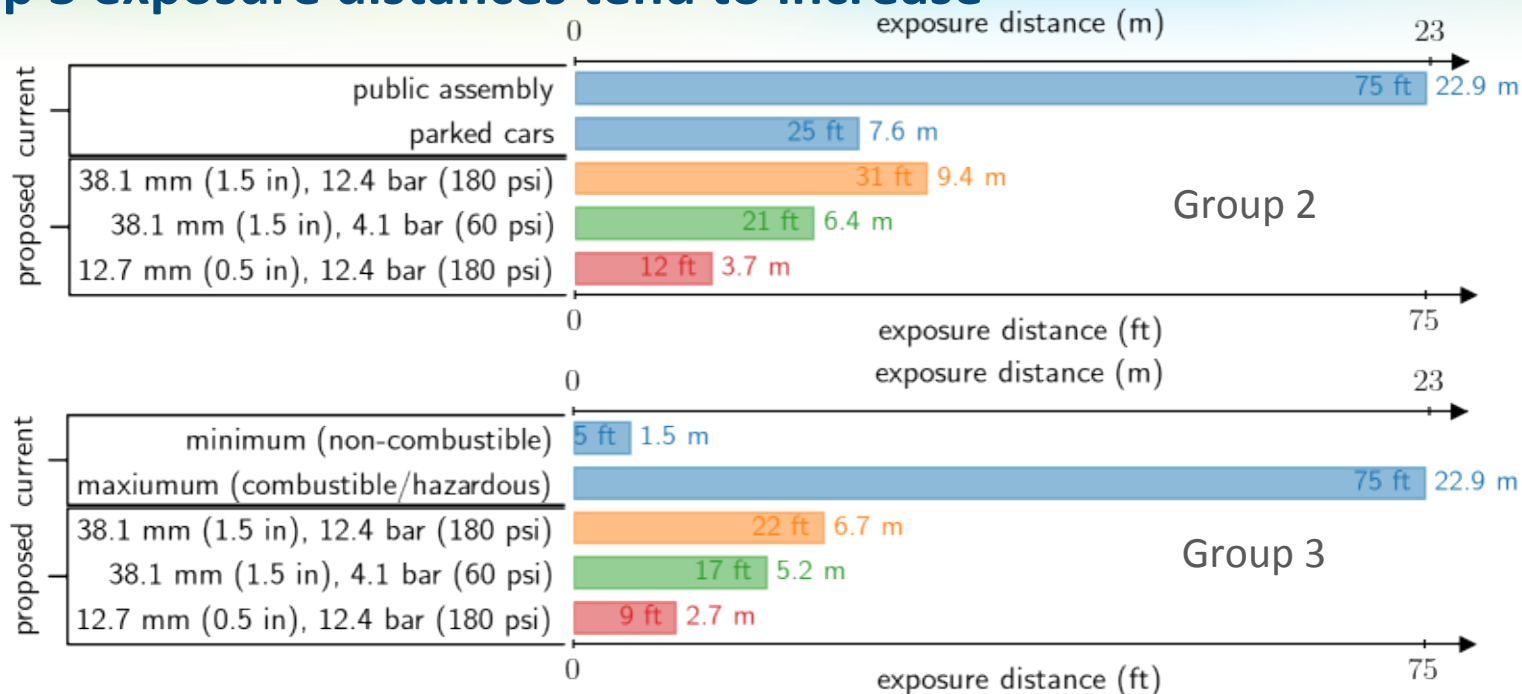


## The new group 1 exposure distances can be significantly reduced, depending on the system parameters



- Proposed exposure distances include safety factor of 2 over hazard distances
- Proposed distances based on line size and maximum allowable working pressure of tank
- Typical liquid hydrogen systems (for FCEV refueling) will have reduced group 1 exposure distances

## Group 2 exposure distances are generally similar or reduced, while group 3 exposure distances tend to increase

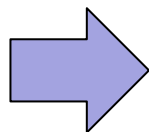


- Group 3 hazard of fire spread (and hence exposure distance) can be mitigated and reduced using fire-rated walls

# Proposed changes to NFPA 2 enable flexibility in siting and potentially reduced footprints for liquid hydrogen infrastructure

current

Type of Exposure	Total Bulk Liquefied Hydrogen (LH <sub>2</sub> ) Storage					
	30.7 gal to 3300 gal	150 L to 13,258 L	3301 gal to 15,000 gal	15,251 L to 56,781 L	15,001 gal to 75,899 gal	56,782 L to 285,996 L
	ft	m	ft	m	ft	m
<b>Group 1</b>						
1. Lot lines	25	7.6	50	15	75	23
2. Air intakes (heating, ventilating, or air-conditioning equipment (HVAC), compressors, other)	75	23	75	23	75	23
3. Wall openings	75	23	75	23	75	23
Operable openings in buildings and structures	50	15	50	15	50	15
4. Ignition sources such as open flames and welding	50	15	50	15	50	15
<b>Group 2</b>						
5. Places of public assembly	75	23	75	23	75	23
6. Parked cars (distance shall be measured from the container fill connection)	25	7.6	25	7.6	25	7.6
<b>Group 3</b>						
7. Building or structure						
(a) Buildings constructed of noncombustible or limited-combustible materials	5'	1.5	5'	1.5	5'	1.5
(1) Sprinklered building or structure or unsprinklered building or structure having noncombustible contents						
(2) Unsprinklered building or structure with combustible contents	25	7.6	50	15	75	23
8. Adjacent wall(s) with fire resistance rating less than 3 hours	5	1.5	5	1.5	5	1.5
9. Adjacent wall(s) with fire resistance rating of 3 hours or greater <sup>b</sup>						
(b) Buildings of combustible construction	50	15	50	15	50	15
(1) Sprinklered building or structure	50	15	75	23	100	30.5
(2) Unsprinklered building or structure	50	15	75	23	75	23
8. Flammable gas storage or systems (other than hydrogen) above or below ground	5	1.5	5	1.5	5	1.5
9. Between stationary liquefied hydrogen containers	50	15	75	23	100	30.5
10. All classes of flammable and combustible liquids (above ground and vent or fill openings if below ground) <sup>c</sup>	75	23	75	23	75	23
11. Hazardous materials storage or systems including liquid oxygen storage and other oxidizers, above or below ground	50	15	75	23	100	30.5
12. Heavy timber, coal, or other slow-burning combustible solids	25	7.6	50	15	50	15
13. Wall openings	25	7.6	50	15	50	15
Unopenable openings in buildings and structures	25	7.6	50	15	50	15
14. Inlets to underground sewers	5	1.5	5	1.5	5	1.5
15. Utilities overhead, including electric power, building services, or hazardous materials piping systems						
(a) Horizontal distance from the vertical plane below the nearest overhead wire of an electric trolley, train, or bus line	50	15	50	15	50	15
(b) Horizontal distance from the vertical plane below the nearest overhead electrical wire	25	7.5	25	7.5	25	7.5
(c) Piping containing other hazardous materials	15	4.6	15	4.6	15	4.6
16. Flammable gas metering and regulating stations above grade	15	4.6	15	4.6	15	4.6



proposed

MAWP (gauge)	< 60 psig		61 to 120 psig		121 to 180 psig	
	< 414 kPa		415 to 827 kPa		828 to 1,241 kPa	
Exposures Group 1	m	ft	m	ft	m	ft
Lot lines						
Air intakes (HVAC, compressors, other)	8.1	26.5	9.9	32.6	11.1	36.5
Operable openings in buildings and structures						
Ignition sources such as open flames and welding						
Exposures Group 2	m	ft	m	ft	m	ft
Exposed persons other than those servicing the system	6.4	21.1	8.4	27.4	9.5	31.3
Parked Cars						
Exposures Group 3	m	ft	m	ft	m	ft
Buildings of non-combustible non-fire-rated construction						
Buildings of combustible construction						
Flammable gas storage systems above or below ground						
Hazardous materials storage systems above or below ground						
Heavy timber, coal, or other slow-burning combustible solids						
Ordinary combustibles, including fast-burning solids such as ordinary lumber, excelsior, paper, or combustible waste and vegetation other than that found in maintained landscaped areas	5.1	16.6	6.4	21.0	6.8	22.4
Unopenable openings in buildings and structures						
Encroachment by overhead utilities (horizontal distance from the vertical plane below the nearest overhead electrical wire of building service)						
Piping containing other hazardous materials						
Flammable gas metering and regulating stations such as natural gas or propane						

MAWP (gauge)	< 60 psi						61 to 120 psi						121 to 180 psi					
	< 414 kPa						415 to 827 kPa						828 to 1,241 kPa					
	Group 1		Group 2		Group 3		Group 1		Group 2		Group 3		Group 1		Group 2		Group 3	
	Internal Pipe Diameter																	
	in	mm	m	ft	m	ft	m	ft	m	ft	m	ft	m	ft	m	ft	m	ft
0.1	2.54		0.6	1.9	0.6	1.9	0.6	1.8	0.8	2.5	0.8	2.5	0.7	2.4	0.9	3.0	0.9	3.0
0.25	6.35		1.3	4.4	1.3	4.3	1.3	4.2	1.7	5.7	1.7	5.7	1.6	5.3	2.1	6.9	2.1	6.9
0.5	12.7		2.7	8.8	2.5	8.3	2.2	7.2	3.3	10.9	3.3	10.8	2.8	9.0	3.7	12.2	3.6	12.0
0.75	19		4.0	13.3	3.7	12.0	3.0	9.9	5.0	16.3	4.5	14.8	3.7	12.0	5.6	18.3	5.2	17.0
1	25.4		5.4	17.7	4.5	14.8	3.6	11.9	6.6	21.7	5.8	19.1	4.6	15.1	7.4	24.3	6.7	21.9
1.25	31.8		6.7	22.1	5.5	18.0	4.4	14.3	8.3	27.1	7.1	23.3	5.5	18.1	9.3	30.4	8.1	26.6
1.5	38.1		8.1	26.5	6.4	21.1	5.1	16.6	9.9	32.6	8.4	27.4	6.4	21.0	11.1	36.5	9.5	31.3
1.75	44.4		9.4	30.9	7.4	24.2	5.7	18.7	11.6	38.0	9.6	31.4	7.2	23.8	13.0	42.6	10.9	35.9
2	50.8		10.8	35.3	8.3	27.3	6.3	20.8	13.2	43.4	10.8	35.4	8.0	26.4	14.8	48.7	12.3	40.5
2.25	57.1		12.1	39.8	9.2	30.3	7.0	22.9	14.9	48.9	12.0	39.4	8.9	29.0	16.7	54.7	13.7	45.0
2.5	63.5		13.5	44.2	10.1	33.3	7.6	24.9	16.5	54.3	13.2	43.3	9.6	31.6	18.5	60.8	15.1	49.6
2.75	69.8		14.8	48.6	11.0	36.2	8.2	26.8	18.2	59.7	14.3	47.0	10.4	34.2	20.4	66.9	16.5	54.1
3	76.2		16.2	53.0	11.9	39.1	8.8	28.8	19.8	65.1	15.6	51.0	11.2	36.6	22.2	73.0	17.8	58.6



## Summary and conclusions

- HyRAM models have been used, with assumptions on leak size, to quantify exposure distances for LH<sub>2</sub> systems
  - Distances related to relief pressure and pipe size
  - Included unconfined overpressure criteria (not limiting for any of the groups)
  - Largest separation distances reduced for typical system
  - Smallest separation distances sometimes increase, but mitigations can be used
  - New tables have been proposed to NFPA 2
- Methods and updated code language currently being reviewed/revised by NFPA 2 storage task group as a committee input



**QUESTIONS  
OR  
COMMENTS:**  
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- United States Department of Energy, Energy Efficiency & Renewable Energy, Hydrogen and Fuel Cell Technologies Office, Safety, Codes, and Standards subprogram managed by Laura Hill
- Air Liquide and partners

# Recent experiments under PreSLHy project show that rainout/pooling unlikely except for vertically downward releases near ground level

- Releases through ¼" – 1" orifices, 0.5m – 1.5m from ground, 1 and 5 bar<sub>g</sub>
  - Rainout/pooling only observed for vertically downward releases through ½" pipe 0.5m from ground (105/265 g/s)



Figure 3-18. Visible cloud during dispersion and rainout tests at HSE facility.

Rainout did not occur during the established flow of these releases, but there was evidence of rainout soon after valve closure (probably liquid air). Further to this, condensed components of air formed around the release point and on impingements for releases from the 6 and 12 mm nozzles. Pools were only formed with low, vertically downward releases. These pools potentially comprised of LH<sub>2</sub>, condensed components of air, or a mixture of the two.

[https://hysafe.info/wp-content/uploads/sites/3/2021/04/D39\\_2021-01-PRESLHY\\_ChapterLH2-v3.pdf](https://hysafe.info/wp-content/uploads/sites/3/2021/04/D39_2021-01-PRESLHY_ChapterLH2-v3.pdf)

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➤ Pooling is a credible, but unlikely scenario

# Verification of HyRAM models against lab-scale and literature data has been completed and published

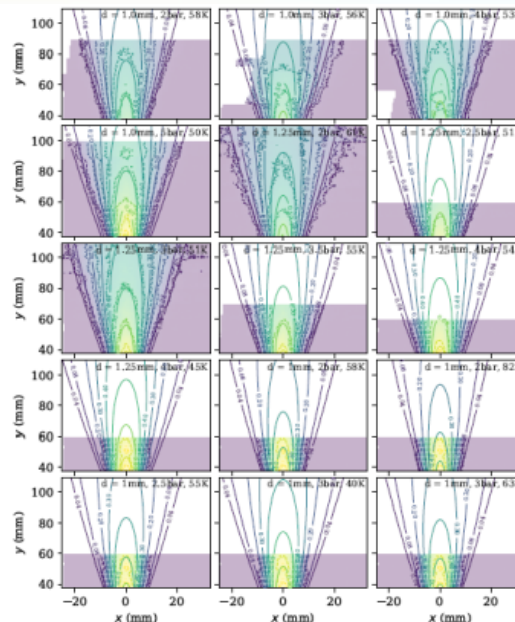
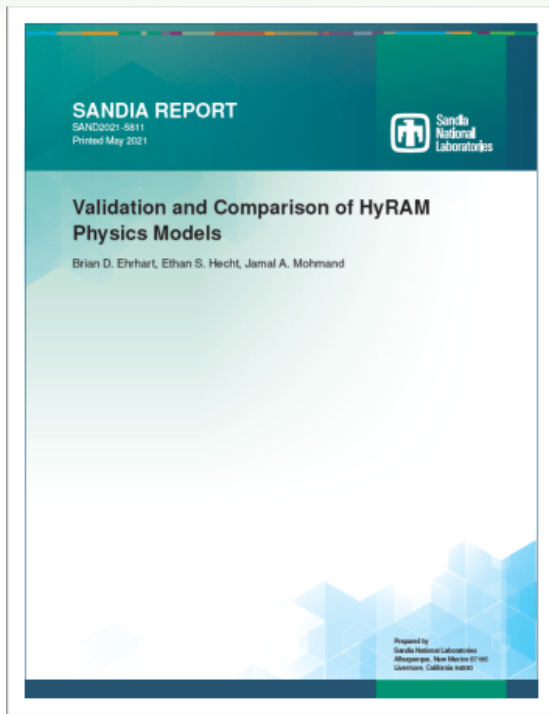


Figure 3-26 Comparison of mole fraction calculated by HyRAM 3.1 (thin, solid lines) to cryogenic hydrogen dispersion data reported by Hecht and Panda [13] (shading and thick, dashed lines) as well as some previously unreported data

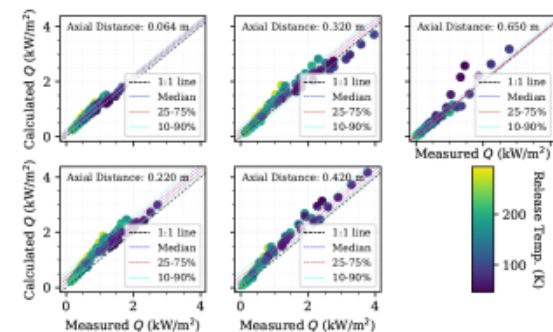


Figure 3-32 Comparison of heat flux ( $Q$ ) calculated by HyRAM 3.1 to those measured by Panda and Hecht [12]

- Distance calculations locked to a specific (3.1), retrievable version of the models



## How does the distance change for a 3% leak area vs a 1% leak area?

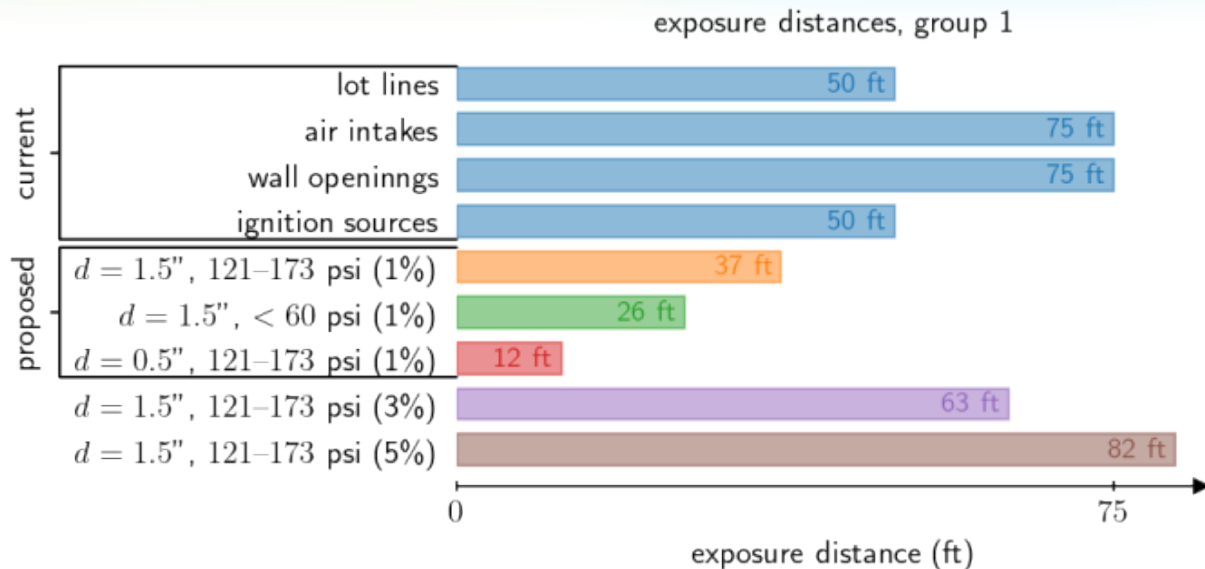
Group	Criteria	Distance increase
1	8% mole fraction	1.7 times
1	0.7 psi overpressure	2.5-3.3 times
1/2	4.7 kW/m <sup>2</sup>	1.7 times
2	2.3 psi overpressure	2.5-3.3 times
3	20 kW/m <sup>2</sup>	1.6 times
3	Visible flame length	1.4-1.6 times
3	10.2 psi overpressure	2.5-3.3 times

- Safety factor of 2 on 1% leak area is equivalent to safety factor of 0.15 on 3% leak area
- As calculated distances are conservative for 1% or 3% leak area





## Group 1 proposed distances, and calculations with larger leak sizes



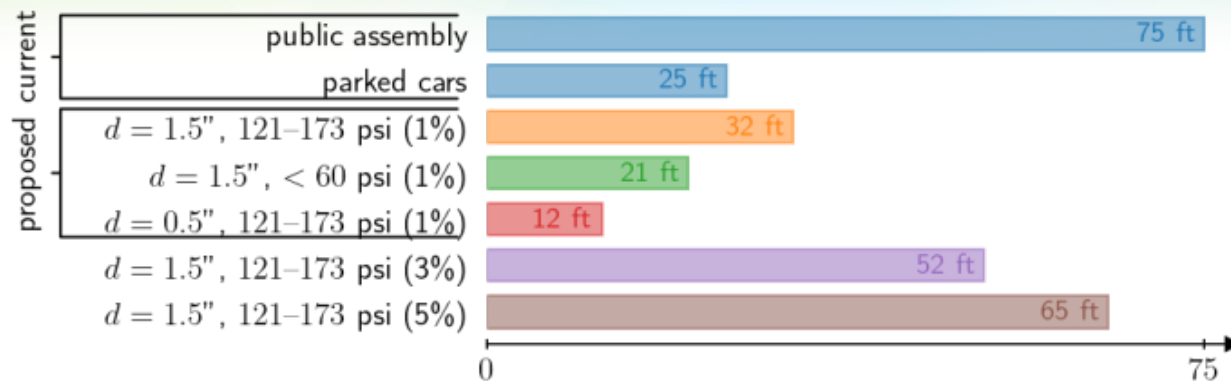
Calculations with same safety factor (2)

- 3% leak is 1.54 – 1.77 times further than 1% leak
- 5% leak is 1.91 – 2.40 times further than 1% leak



## Groups 2 and 3 proposed distances, and calculations with larger leak sizes

Group 2 →



Group 3 →

