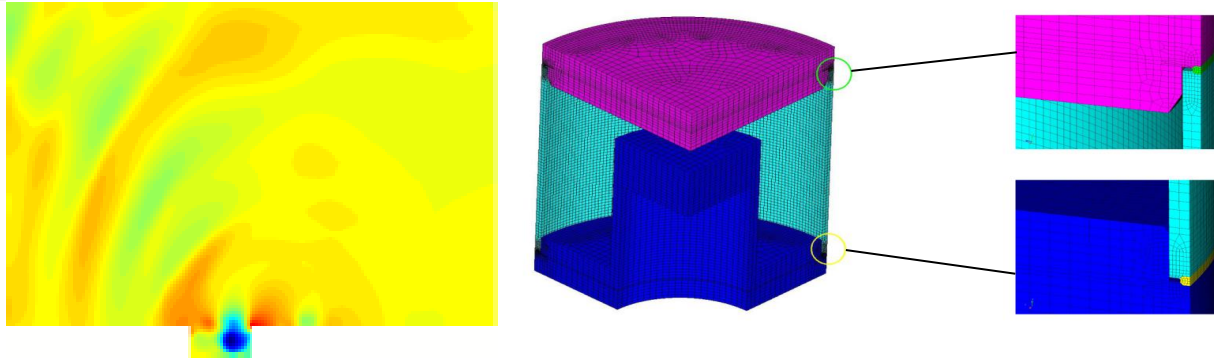




# Preconditioned Least-Squares Petrov-Galerkin Reduced Order Models for Fluid and Solid Mechanics Problems



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MMLDT-CSET2021

Wednesday, September 28, 2021

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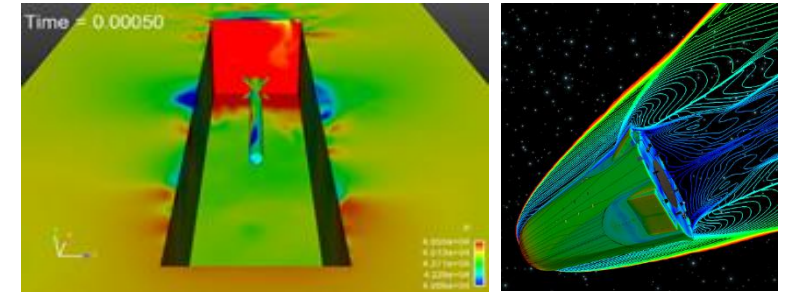


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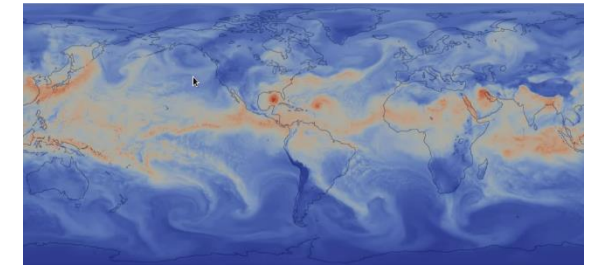
Despite improved algorithms and powerful supercomputers, “**high-fidelity**” models are often too expensive for use in a design or analysis setting.

## Sandia application areas in which this situation arises:

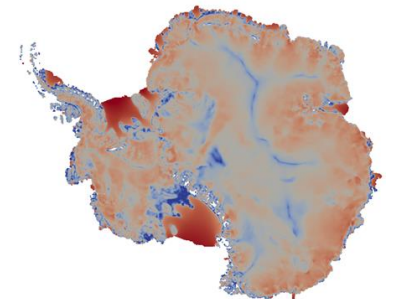
- **Captive-carry and re-entry environments:** Large Eddy Simulations (LES) runs require very fine meshes and can take on the order of *weeks*.



- **Fastener failure modeling:** modeling fastener behavior in a full system presents meshing and computational challenges, which limits the number of configurations that can be studied.



- **Climate modeling** (e.g., land-ice, atmosphere): high-fidelity simulations too costly for uncertainty quantification (UQ); Bayesian inference of high-dimensional parameter fields is intractable.

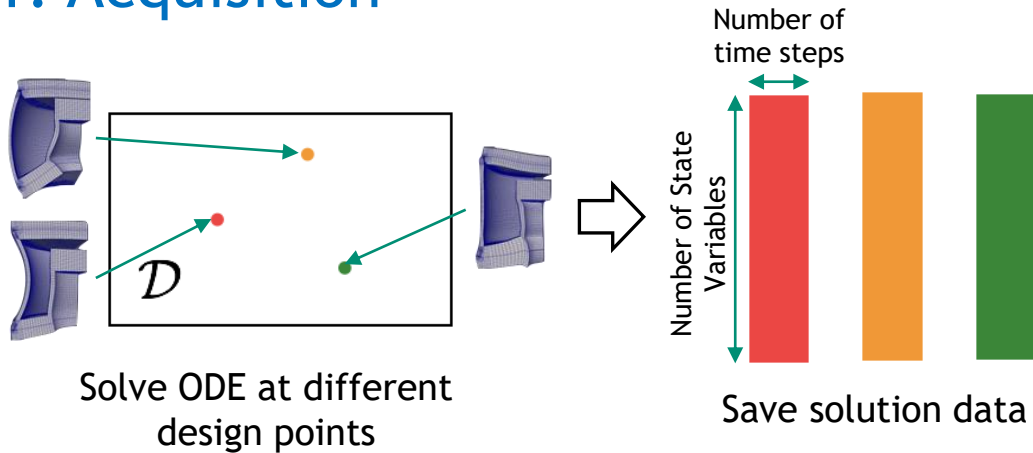


# POD/LSPG\* Approach to Model Reduction



Full Order Model (FOM) = Ordinary Differential Equation (ODE):  $\frac{d\mathbf{x}}{dt} = \mathbf{f}(\mathbf{x}; t, \mu)$

## 1. Acquisition



## 2. Learning

Proper Orthogonal Decomposition (POD):

$$\mathbf{X} = \begin{bmatrix} \text{red bar} & \text{orange bar} & \text{green bar} \end{bmatrix} = \begin{bmatrix} \text{brown bar} & \text{blue bar} \end{bmatrix} \mathbf{U} \quad \Sigma \quad \mathbf{V}^T$$

## 3. Reduction

Choose ODE  
Temporal  
Discretization

$$\frac{d\mathbf{x}}{dt} = \mathbf{f}(\mathbf{x}; t, \mu)$$

$$\Downarrow$$

$$\mathbf{r}^n(\mathbf{x}^n; \mu) = \mathbf{0}, \quad n = 1, \dots, T$$

Reduce the  
number of  
unknowns

$$\mathbf{x}(t) \approx \tilde{\mathbf{x}}(t) = \Phi \hat{\mathbf{x}}(t)$$

Minimize  
the Residual

minimize  $\|\hat{\mathbf{v}}\|$

Hyper-reduction/sample mesh

$$\mathbf{r}^n(\Phi \hat{\mathbf{v}}; \mu) \Big|_2$$

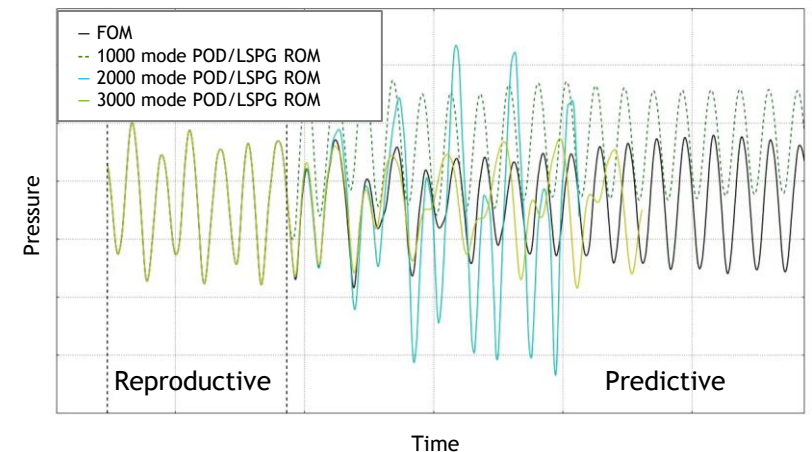
\*Least-Squares Petrov-Galerkin Projection [K. Carlberg *et al.*, 2011; K. Carlberg *et al.*, 2017]

## Advantages of POD/LSPG projection:

- Computes a solution that **minimizes the  $l_2$ -norm** of the time-discrete residual arising in each  $\Delta t$ 
  - Ensures that adding basis vectors yields a **monotonic decrease** in the least-squares objective function defining the underlying minimization problem [Carlberg *et al.*, 2011]
- Possesses **better stability and accuracy** than POD/Galerkin for certain classes of problems (e.g., compressible flow) [Carlberg *et al.*, 2013, Carlberg *et al.*, 2017, Tezaur *et al.*, 2018].

## Room for improvement for realistic predictive applications:

- Accuracy for **time-predictive problems** can be inadequate
- Method may **fail to converge** for some realistic problems run in the predictive regime
- Method may struggle when applied to **multi-physics problems** with disparate scales [Washabaugh, 2016]



**Solution:** introduction of preconditioning into LSPG/ROM formulation.



### LSPG Formulation:

$$\hat{\mathbf{x}} = \operatorname{argmin}_{\mathbf{y} \in \mathbb{R}^M} \|\mathbf{r}(\Phi \mathbf{y})\|_2^2$$

Optimization problem

$$\delta \hat{\mathbf{x}}_{\text{PG}}^{(k)} = \operatorname{argmin}_{\mathbf{y} \in \mathbb{R}^M} \|\mathbf{J}^{(k)} \Phi \mathbf{y} + \mathbf{r}^{(k)}\|_2^2$$

$$\hat{\mathbf{x}}_{\text{PG}}^{(k)} = \hat{\mathbf{x}}_{\text{PG}}^{(k-1)} + \alpha_k \delta \hat{\mathbf{x}}_{\text{PG}}^{(k)}$$

$$\tilde{\mathbf{x}}_{\text{PG}}^{(k)} = \Phi \hat{\mathbf{x}}_{\text{PG}}^{(k)}$$

Gauss-Newton iteration

Normal equations

$$\begin{aligned} \mathbf{J}_{\text{PG}}^{(k)} \delta \hat{\mathbf{x}}_{\text{PG}}^{(k)} &= -\mathbf{r}_{\text{PG}}^{(k)} \\ \mathbf{J}_{\text{PG}}^{(k)} &:= \Phi^T \mathbf{J}^{(k)T} \mathbf{J}^{(k)} \Phi \\ \mathbf{r}_{\text{PG}}^{(k)} &:= \Phi^T \mathbf{J}^{(k)T} \mathbf{r}^{(k)} \end{aligned}$$

### Preconditioned LSPG Formulation:

$$\hat{\mathbf{x}} = \operatorname{argmin}_{\mathbf{y} \in \mathbb{R}^M} \|\mathbf{M} \mathbf{r}(\Phi \mathbf{y})\|_2^2$$

Optimization problem

$$\delta \hat{\mathbf{x}}_{\text{PPG}}^{(k)} = \operatorname{argmin}_{\mathbf{y} \in \mathbb{R}^M} \|\mathbf{M}^{(k)} (\mathbf{J}^{(k)} \Phi \mathbf{y} + \mathbf{r}^{(k)})\|_2^2$$

$$\hat{\mathbf{x}}_{\text{PPG}}^{(k)} = \hat{\mathbf{x}}_{\text{PPG}}^{(k-1)} + \alpha_k \delta \hat{\mathbf{x}}_{\text{PPG}}^{(k)}$$

$$\tilde{\mathbf{x}}_{\text{PPG}}^{(k)} = \Phi \hat{\mathbf{x}}_{\text{PPG}}^{(k)}$$

Gauss-Newton iteration

Normal equations

$$\begin{aligned} \mathbf{J}_{\text{PPG}}^{(k)} \delta \hat{\mathbf{x}}_{\text{PG}}^{(k)} &= -\mathbf{r}_{\text{PG}}^{(k)} \\ \mathbf{J}_{\text{PPG}}^{(k)} &:= \Phi^T \mathbf{J}^{(k)T} \mathbf{M}^{(k)T} \mathbf{M}^{(k)} \mathbf{J}^{(k)} \Phi \\ \mathbf{r}_{\text{PPG}}^{(k)} &:= \Phi^T \mathbf{J}^{(k)T} \mathbf{M}^{(k)T} \mathbf{M}^{(k)} \mathbf{r}^{(k)} \end{aligned}$$





Adding preconditioning to the POD/LSPG formulation can **improve** not only ROM efficiency but also **ROM accuracy**.

**Ideal preconditioned ROM emulates projection of FOM solution increment onto POD basis.**

- Upper limit on ROM accuracy is obtained by taking **solution increment** computed by FOM,  $\delta x^{(k)}$ , at each time step  $k$  and **projecting it** onto the **POD basis**:

$$\delta \tilde{x}^{(k)} = \Phi (\Phi^T \Phi)^{-1} \Phi^T \delta x^{(k)} \quad (1)$$

- **Ideal preconditioned ROM** ( $M^{(k)} = (J^{(k)})^{-1}$ ) gives rise to “projected solution increment” solution (1)
- As quality of preconditioner is improved ( $M^{(k)} \rightarrow (J^{(k)})^{-1}$ ), the ROM solution **approaches** the most accurate ROM solution possible for a given basis  $\Phi$ .

**Preconditioning ensures all residual components are on approximately the same scale.**

- Minimizing the raw (unweighted) residual  $r$  can be problematic for systems of PDEs where different variables have **drastically different magnitudes** (e.g., dimensional PDEs, multi-physics) [Washabaugh, 2016].
- Adding a preconditioner amounts to **scaling** the ROM residual to get all the equations to be roughly the same order.



multi-physics finite  
element code

- Open-source<sup>1</sup>, parallel, C++ code
- Component-based design for rapid development
- Contains a wide variety of constitutive models for mechanical/thermo-mechanical problems.
- Makes extensive use of libraries from the open-source Trilinos project<sup>2</sup>, including preconditioners from the Ifpack library

**Problems tested:** quasi-static mechanical and thermo-mechanical with prediction across material parameter space.

<sup>1</sup>[https://github.com/SNLComputation/Albany/releases/tag/MOR\\_support\\_end](https://github.com/SNLComputation/Albany/releases/tag/MOR_support_end)

<sup>2</sup><https://github.com/trilinos/trilinos>

## SPARC<sup>3</sup> Flow Solver

- Next-generation transonic and hypersonic C++ CFD code developed at Sandia
- Simulates compressible flow
- Used for analyses involving captive carry and reentry vehicles
- Primary discretization is cell-centered finite volume method
- Leverages libraries from the Trilinos project<sup>2</sup>

**Problems tested:** transient compressible laminar flow over an open cavity with prediction in time

<sup>3</sup>Sandia Parallel Aerodynamics and Reentry Code

# Thermo-Mechanical Beam (Albany)

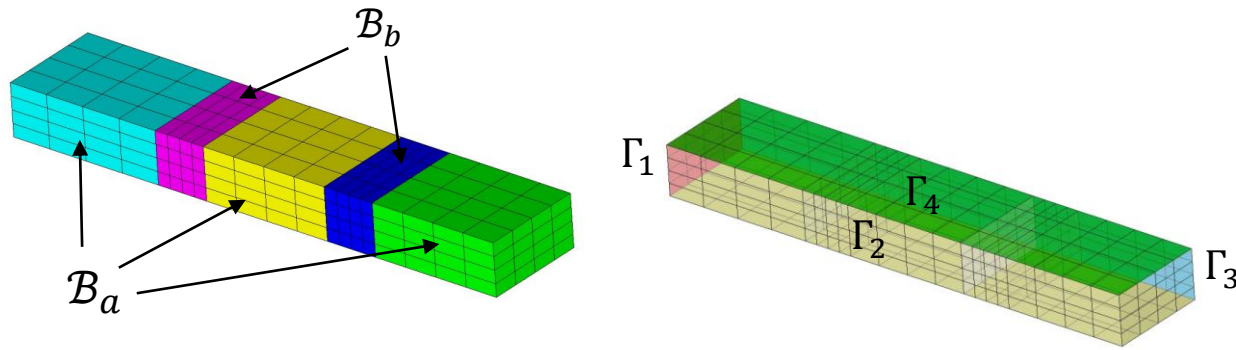
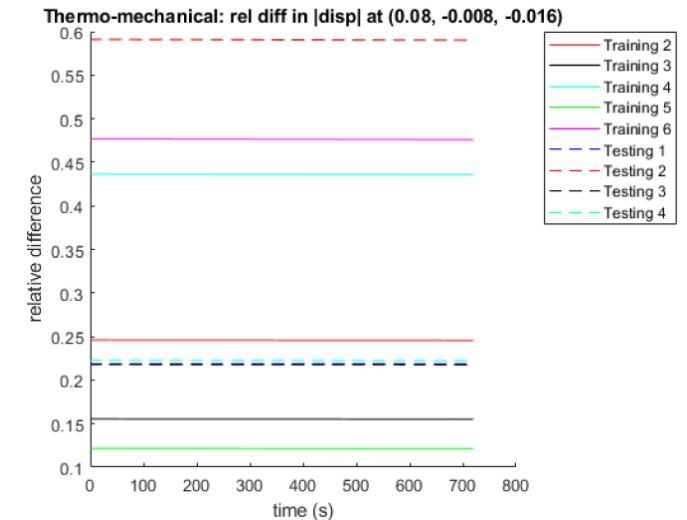


Table 1. Parameters in block  $\mathcal{B}_b$  for thermo-mechanical beam problem.

| Regime   | Case | $E_b (\times 10^9)$ [Pa] | $\nu_b$  | $\rho_b (\times 10^{-5})$ [kg/m <sup>3</sup> ] | $T_{b,ref}$ [K] |
|----------|------|--------------------------|----------|--|-----------------|
| training | 1    | 2.01313                  | 0.285907 | 7.94827  | 273.657         |
|          | 2    | 1.71637                  | 0.332083 | 6.93965  | 318.406         |
|          | 3    | 1.96881                  | 0.3478   | 9.37181  | 301.406         |
|          | 4    | 1.28954                  | 0.29427  | 9.14636  | 365.378         |
|          | 5    | 1.61326                  | 0.262464 | 6.32164  | 223.434         |
|          | 6    | 1.54724                  | 0.374118 | 7.31561  | 245.778         |
| testing  | 1    | 1.52473                  | 0.27925  | 8.80694  | 266.674         |
|          | 2    | 1.31153                  | 0.345538 | 7.58234  | 333.462         |
|          | 3    | 1.37015                  | 0.246513 | 7.73303  | 345.942         |
|          | 4    | 1.703                    | 0.32     | 7.92   | 293             |

- Coupled thermo-mechanical problem involving **Neohookean** material
- 2 sets of material blocks,  $\mathcal{B}_a$  and  $\mathcal{B}_b$ , each having set of material parameters
  - Material parameters in block  $\mathcal{B}_a$  are fixed
  - Material parameters in block  $\mathcal{B}_b$  are varied (see Table 1)
- Linearly varying **time-dependent pressure** and **temperature BC** is prescribed on  $\Gamma_2$ ; other boundaries are fixed
- Problem is run **quasi-statically** to pseudo-time  $t = 7200s$  with 2100 dofs
- Training** is performed for 6 sets of parameters; **testing/prediction** is performed for 4 sets of parameters (see Table 1)
  - **Significant variations** in displacement (up to 60%) are observed with the parameter variations considered (right figure)



[Lindsay *et al.*, in prep.]



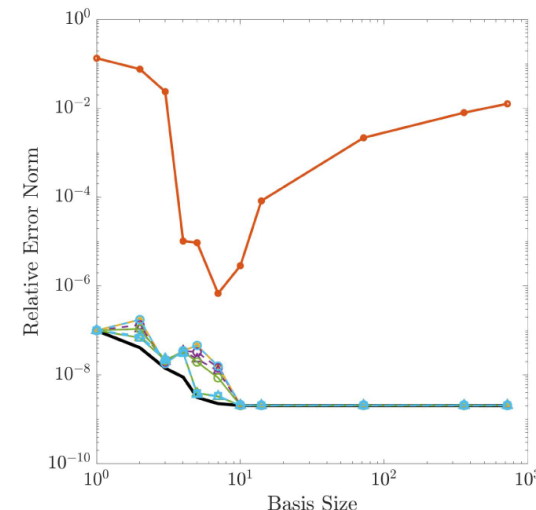
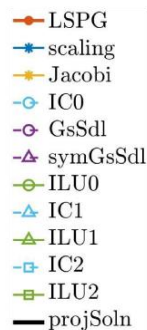
# Thermo-Mechanical Beam (Albany)



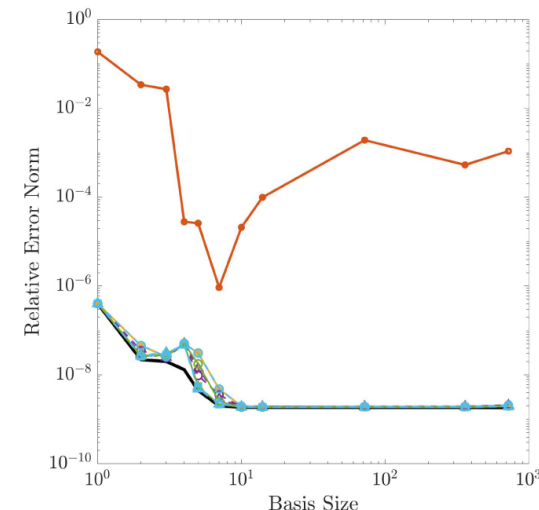
- Figure plots **global relative error** in approximate ROM solutions:

$$\epsilon := \frac{\sum_{i=0}^P \|x_i - \tilde{x}_i\|_2}{\sum_{i=0}^P \|x_i\|_2}$$

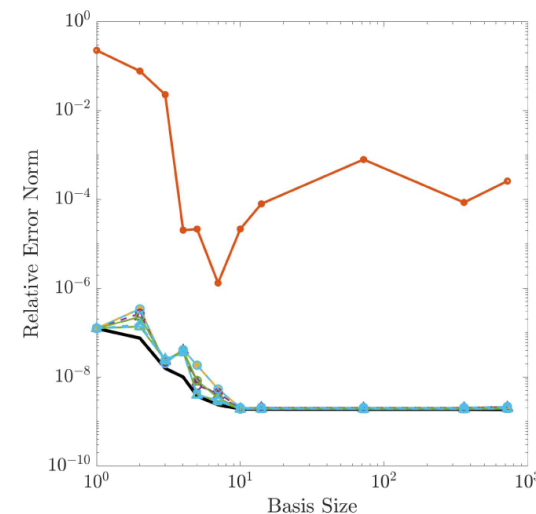
- Preconditioners evaluated:** Jacobi, Gauss-Seidel, Symmetric Gauss-Seidel, Incomplete Cholesky, ILU and  $(J^{(k)})^{-1}$  (denoted by projSoln)
- By introducing preconditioning, it is possible to reduce  $\epsilon$  by **2-6 orders of magnitude**
- All preconditioned LSPG ROMs achieve **errors close to** (less than one order of magnitude greater than) the error obtained by the **projected solution increment model**



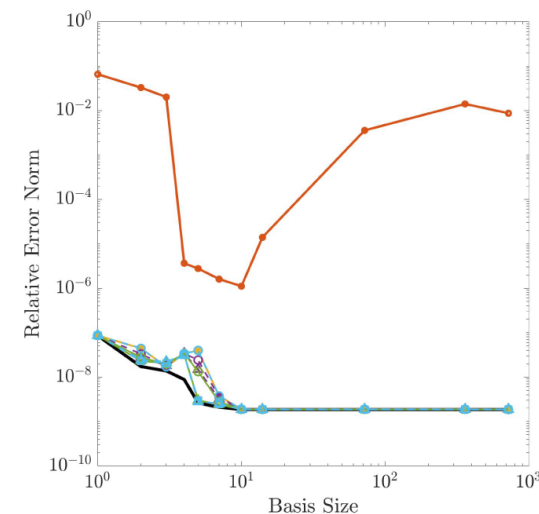
(a) Testing case 1



(b) Testing case 2



(c) Testing case 3

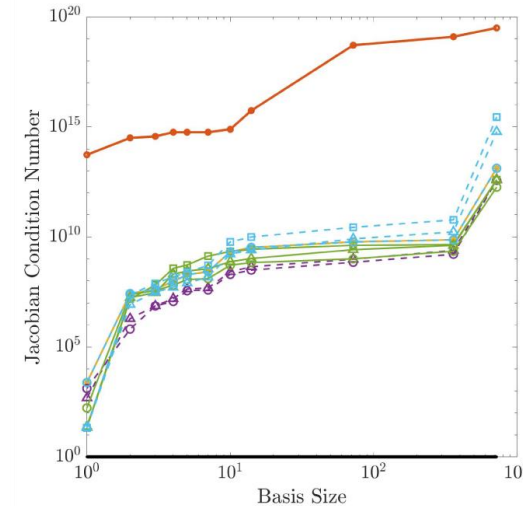
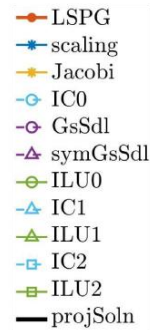


(d) Testing case 4

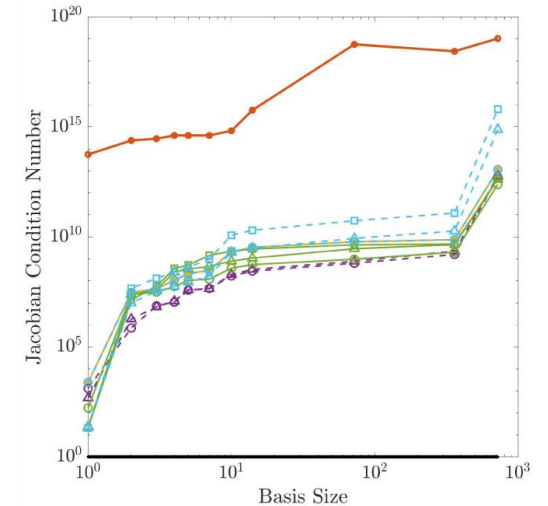
# Thermo-Mechanical Beam (Albany)



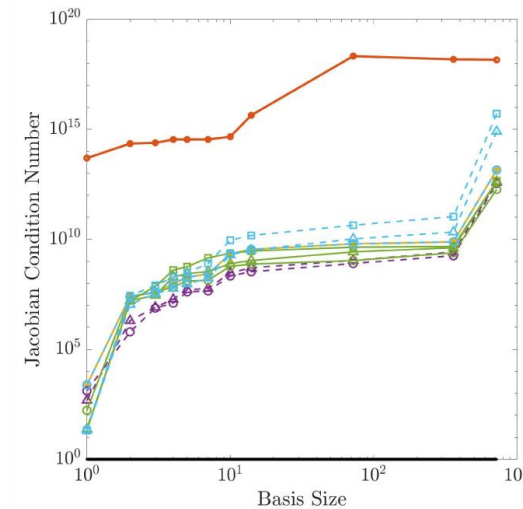
- Figure plots **condition numbers** of reduced Jacobian ( $J_{PPG}^{(k)}$  or  $J_{PG}^{(k)}$ ) for each ROM.
- Reduced Jacobians for regular LSPG ROM are **very ill-conditioned** ( $O(10^{14}) - O(10^{16})$ )
  - Ill-conditioning is due to extreme differences in scale b/w displacement and temperature solutions (9 orders of magnitude)
- Results demonstrate that **simple preconditioning** strategy can reduce condition numbers by as many as **10 orders of magnitude**
  - Gauss-Seidel** preconditioners produce the **lowest condition number**
- As expected, projected solution increment reduced Jacobian has **perfect condition number**



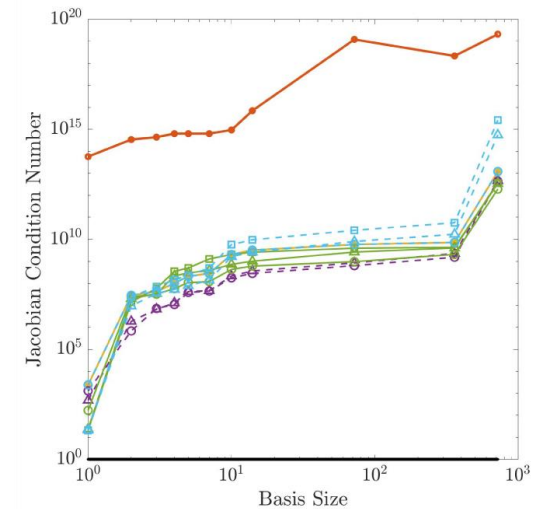
(a) Testing case 1



(b) Testing case 2



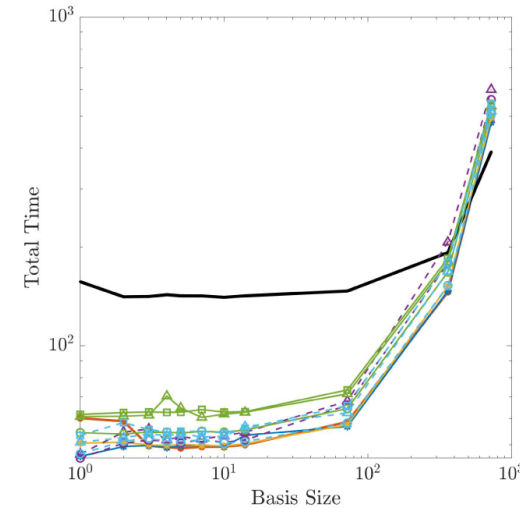
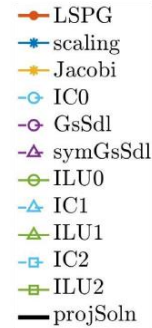
(c) Testing case 3



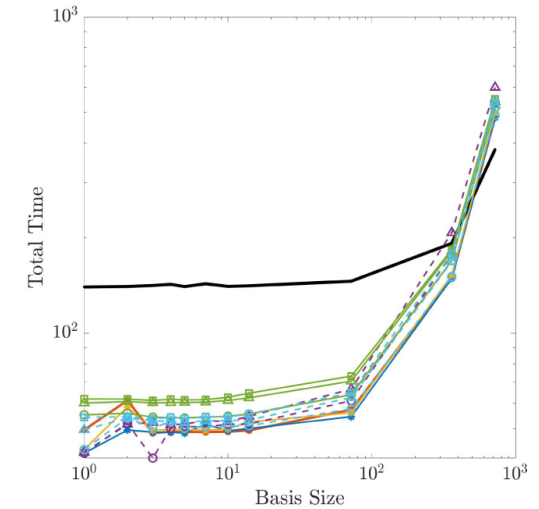
(d) Testing case 4

# Thermo-Mechanical Beam (Albany)

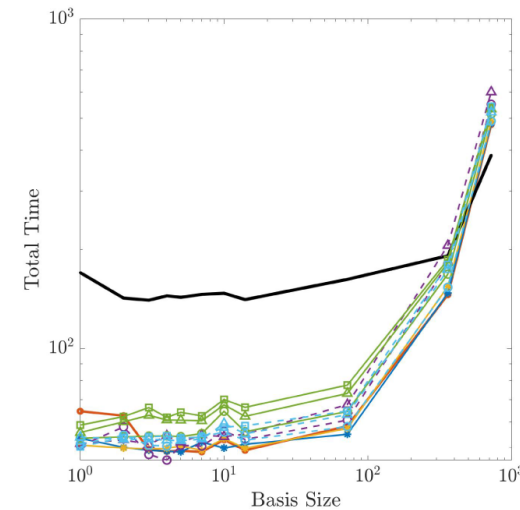
- Figures shows **CPU-times** for all ROMs considered
- Preconditioned LSPG ROMs** achieve CPU-times that are **comparable** or **marginally larger** than unpreconditioned LSPG ROM
- Since preconditioned ROMs are substantially more accurate than vanilla LSPG, there is a **significant computational advantage** in applying preconditioning
- Gauss-Seidel** preconditioners give rise to **lowest CPU-times** of preconditioned ROMs
- As expected, the **projected solution increment** is the **most expensive** to compute



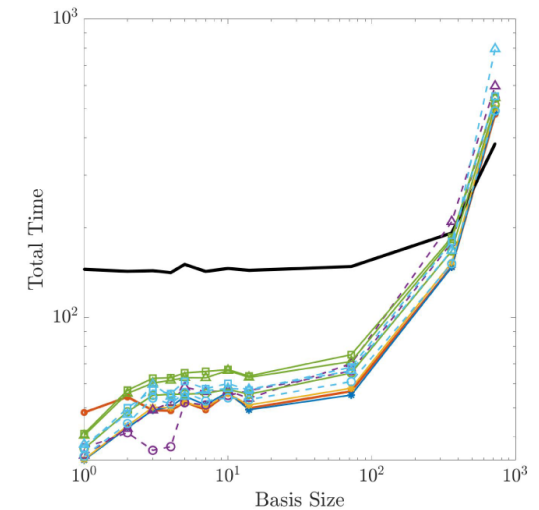
(a) Testing case 1



(b) Testing case 2



(c) Testing case 3



(d) Testing case 4

# Thermo-Mechanical Pressure Vessel (Albany)

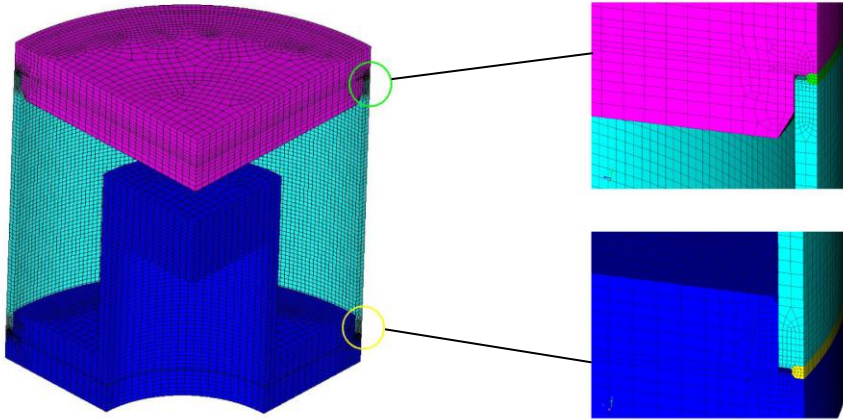


Table 2. Parameters in block  $\mathcal{B}_b$  for thermo-mechanical pressure vessel problem.

| Regime   | Case | $E_b (\times 10^9)$ [Pa] | $\nu_b$  | $\rho_b (\times 10^{-3})$ [kg/m <sup>3</sup> ] | $T_{b,\text{ref}}$ [K] |
|----------|------|--------------------------|----------|--|------------------------|
| training | 1    | 1.64424                  | 0.39524  | 8.33058  | 311.094                |
|          | 2    | 1.77118                  | 0.300065 | 9.67843  | 267.396                |
|          | 3    | 1.9893                   | 0.32161  | 7.17625  | 223.746                |
|          | 4    | 1.45551                  | 0.266385 | 6.67746  | 331.116                |
| testing  | 1    | 2.06416                  | 0.391368 | 7.79804  | 252.102                |
|          | 2    | 1.703                    | 0.32     | 7.92   | 293                    |

- Coupled **thermo-mechanical** problem involving **Neohookean** material
- 2 sets of **material blocks**,  $\mathcal{B}_a$  and  $\mathcal{B}_b$ , each having set of material parameters
  - Material parameters in block  $\mathcal{B}_a$  (magenta, cyan) are fixed
  - Material parameters in block  $\mathcal{B}_b$  (green, yellow, blue) are varied (see Table 2)
- Pressure vessel is **heated** and **pressurized** from the lateral side
- Problem is run **quasi-statically** to pseudo-time  $t = 720\text{s}$  with 370K dofs
- **Training** is performed for 4 sets of parameters; **testing/prediction** is performed for 2 sets of parameters (see Table 2)

[Lindsay *et al.*, in prep.]

# Thermo-Mechanical Pressure Vessel (Albany)



Table 3. Errors  $\epsilon$  for thermo-mechanical pressure vessel problem

| Testing case | Method                    | Basis size $M$       |                      |                      |
|--------------|---------------------------|----------------------|----------------------|----------------------|
|              |                           | 8                    | 79                   | 790                  |
| 1            | LSPG                      | $2.6 \times 10^{-1}$ | —                    | —                    |
|              | GsSd1 Preconditioned LSPG | $1.4 \times 10^{-5}$ | $1.9 \times 10^{-6}$ | $1.7 \times 10^{-6}$ |
| 2            | LSPG                      | $1.8 \times 10^{-2}$ | —                    | —                    |
|              | GsSd1 Preconditioned LSPG | $1.1 \times 10^{-5}$ | $2.2 \times 10^{-6}$ | $2.0 \times 10^{-6}$ |

- **Three basis sizes considered:  $M = 8, 79, 790$  modes**
- **One preconditioner considered: Gauss-Seidel**

Table 4. CPU-times for thermo-mechanical pressure vessel problem

| Testing case | Method                    | Basis size $M$ |      |        |
|--------------|---------------------------|----------------|------|--------|
|              |                           | 8              | 79   | 790    |
| 1            | LSPG                      | 19,490         | —    | —      |
|              | GsSd1 Preconditioned LSPG | 5449           | 6903 | 44,400 |
| 2            | LSPG                      | 9785           | —    | —      |
|              | GsSd1 Preconditioned LSPG | 4670           | 5057 | 14,620 |

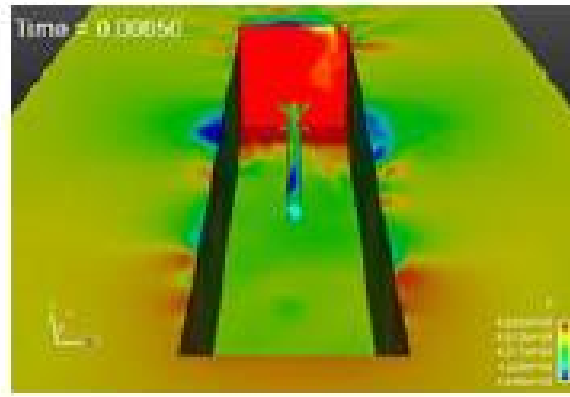
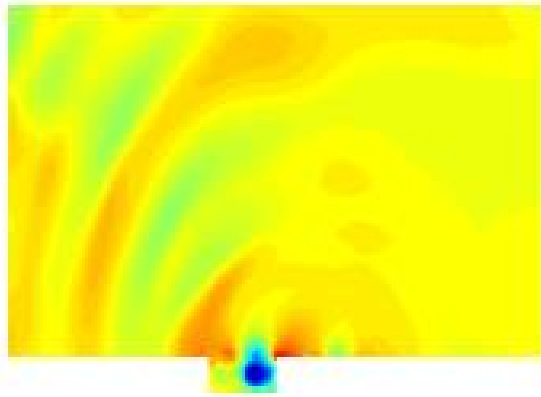
- **Vanilla LSPG ROM results are unsatisfactory**
  - LSPG ROM did not converge for larger basis sizes ( $M = 79$  and  $M = 790$ )
  - For smaller basis size ( $M = 8$ ), the LSPG ROM was only able to achieve a global error of  $O(10^{-1}) - O(10^{-2})$
- **Preconditioned LSPG ROM converges for all basis sizes and achieves errors of  $O(10^{-5}) - O(10^{-6})$**
- **For  $M = 8$  case, the preconditioned LSPG ROM achieved a speedup of up to 3.6x over LSPG ROM**
- **Preconditioned LSPG ROM reduces the total number of nonlinear iterations by a factor of 3-4x**

Table 5. Number nonlinear iterations for thermo-mechanical pressure vessel problem

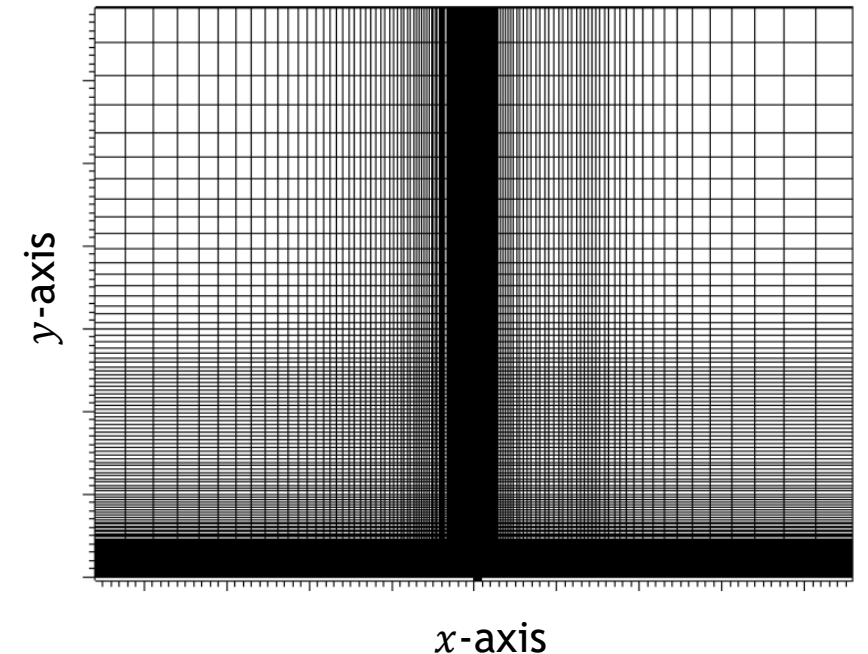
| Testing case | Method                    | Basis size $M$ |      |      |
|--------------|---------------------------|----------------|------|------|
|              |                           | 8              | 79   | 790  |
| 1            | LSPG                      | 7849           | —    | —    |
|              | GsSd1 Preconditioned LSPG | 2104           | 1963 | 1971 |
| 2            | LSPG                      | 4963           | —    | —    |
|              | GsSd1 Preconditioned LSPG | 1628           | 1700 | 1717 |



# Compressible Cavity Flow (SPARC)

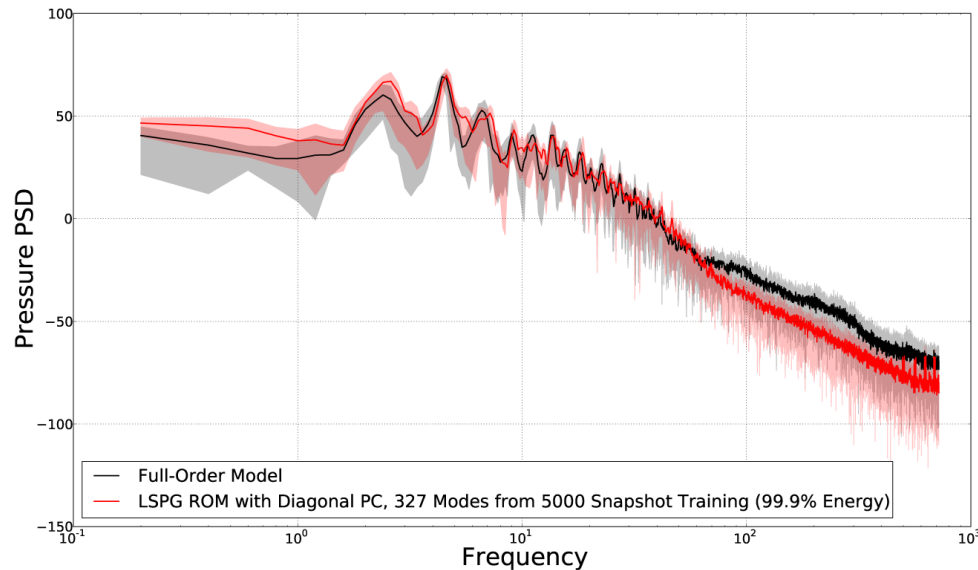
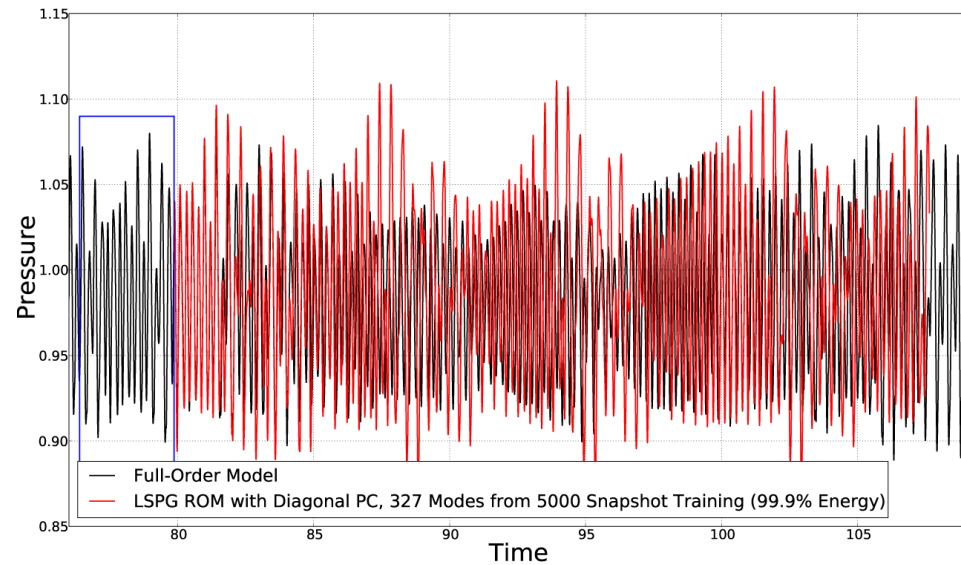


- 2D viscous laminar flow around an open cavity geometry
  - Simple model for the **captive carry scenario**
- Mach number = 0.6, Reynolds number  $\approx 3000$
- Problem is run **non-dimensionally**
- Domain is discretized using 104,500 hexahedral cells (right)
- Of primary interest are **long-time predictive simulations**
  - ROM is run at **same parameters** as FOM but **much longer in time**
  - **Relevant QOIs:** statistics of the flow (e.g., pressure power spectral densities or PSDs)



[Tezaur *et al.* 2017, Fike *et al.* 2018]

# Compressible Cavity Flow (SPARC)



- **Figure top left:** pressure time history for a point halfway up the downstream wall of the cavity for an LSPG ROM having 327 modes with a Jacobi preconditioner (PC)
- **Figure bottom left:** pressure PSD for the signal in the top left figure (solid line is mean PSD, shaded regions indicate range of values used to construct the mean)
- **Preconditioned LSPG ROM** captures well the **pressure PSD**, including its peaks (Rossiter modes) and the **RMS OASPL<sup>1</sup>**
- **Vanilla LSPG ROM did not run successfully**

| Method           | RMS OASPL <sup>1</sup> in dB | % Difference from FOM in dB |
|------------------|------------------------------|-----------------------------|
| FOM              | 66.176                       | —                           |
| projSoln         | 67.552                       | 2.08%                       |
| LSPG             | N/A                          | N/A                         |
| LSPG + Jacobi PC | 68.033                       | 2.80%                       |

<sup>1</sup>Overall sound pressure level



## Summary:

- Adding **preconditioning** to the LSPG formulation gives rise to ROMs with **improved accuracy and stability**, especially in the predictive regime
  - Preconditioning attempts to **emulate projection of FOM solution increment onto POD basis** (the ROM “best-case scenario” for a given basis)
  - Preconditioning **ensures all components of residual** being minimized are of the **same magnitude**
  - Results on **predictive (across parameter space) thermo-mechanical and predictive (in time) compressible flow** problems are **compelling**

## Ongoing/future work:

- **Two manuscripts** on this work are in preparation
  - P. Lindsay, J. Fike, K. Carlberg, I. Tezaur. “Preconditioned LSPG Reduced Order Models”, *in prep.*
  - J. Fike, P. Lindsay, K. Carlberg, I. Tezaur. “Preconditioned Least-Squares Petrov-Galerkin Reduced Order Models for Compressible Flows”, *in prep.*
- **Application** of preconditioned LSPG approach to **more sophisticated problems** relevant to Sandia’s mission spaces
  - Preconditioning LSPG ROMs has been helpful for **hypersonic aero, thermal/ablation and reacting hypersonic flow** problems



1. Motivation
2. POD/LSPG Approach to Model Reduction
3. Preconditioned LSPG ROMs
4. Numerical Results
  - Thermo-Mechanical Beam
  - Thermo-Mechanical Pressure Vessel
  - Compressible Cavity Flow
5. Summary & Future Work