

Sandia RANS Solutions for the Axisymmetric Transonic Hump

Mary McWherter-Payne, Matthew Barone, Nathan Miller
Sandia National Laboratories

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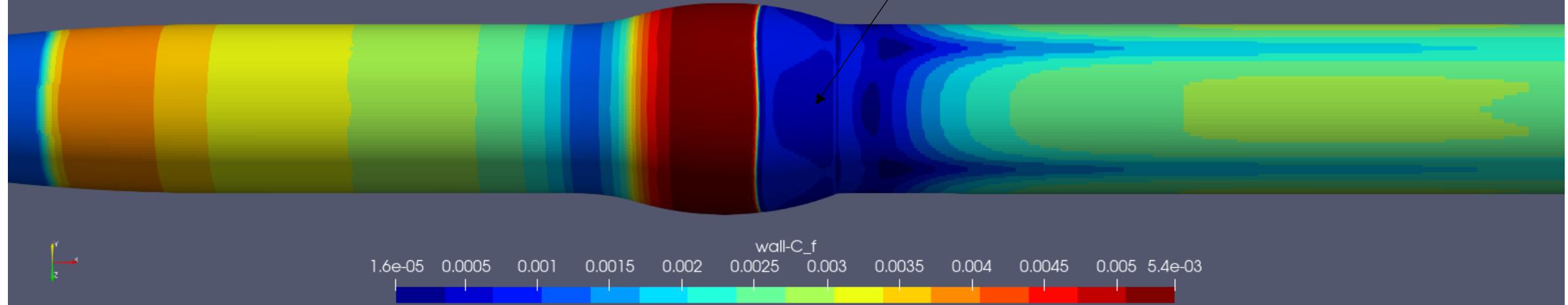
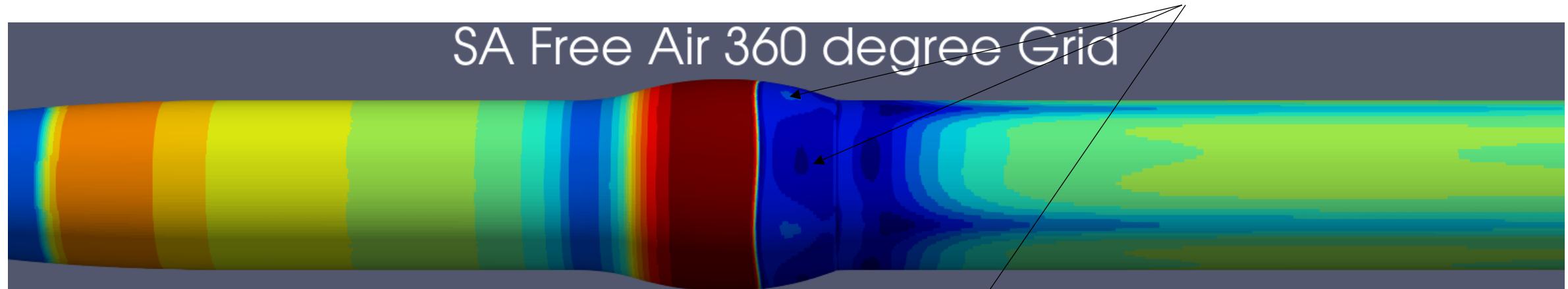
SPARC ATH Simulations

- Solutions obtained using the SPARC code
 - 2nd order, structured grid, finite volume numerical scheme
 - Standard SA and SST-2003 models
- The following plots attempt to show the effects of:
 - Turbulence model; SA and SST – non-axisymmetry?
 - Tunnel walls (in-tunnel solutions compared to free air)
 - Symmetry planes (90° grids vs 180° grids vs 360° grids)
- Some plot titles show (Reflected) – This means the solution is on a 90° or 180° grid and has been reflected/mirrored to appear as a full 360° solution in order to compare with the actual 360° grid solution.

SA Free Air Grids

SA Free Air Solutions are not Axisymmetric

Very slight differences



90° (previous slide) and 180 ° look the same

Very slight differences

SA Free Air 360 Degree Grid



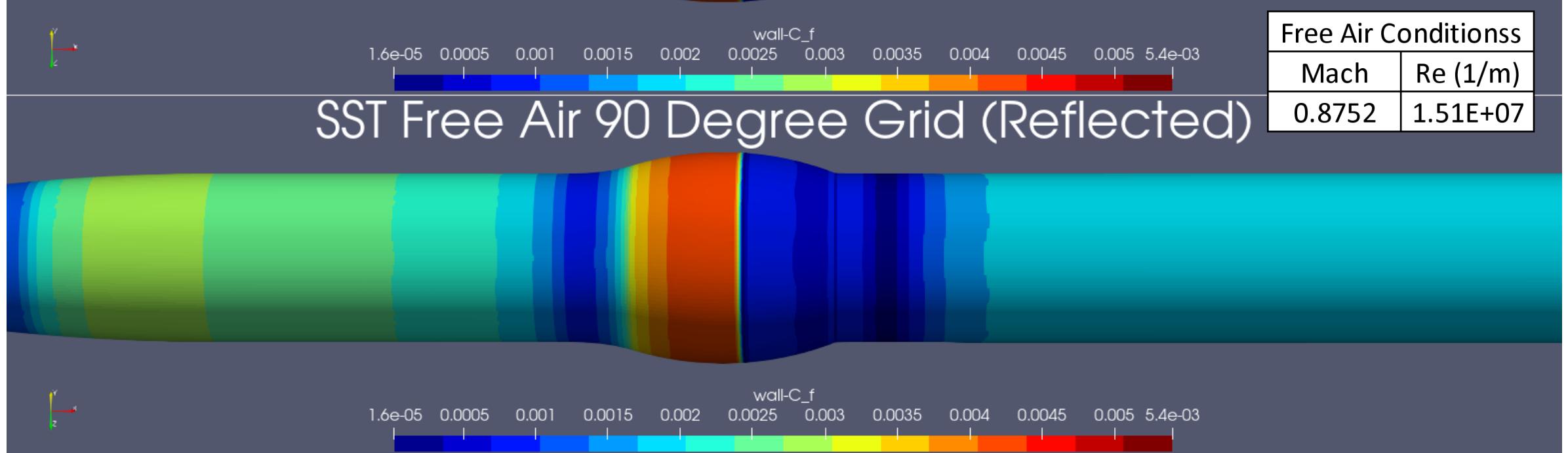
Free Air Conditions	
Mach	Re (1/m)
0.8752	1.51E+07

SA Free Air 180 Degree Grid (Reflected)

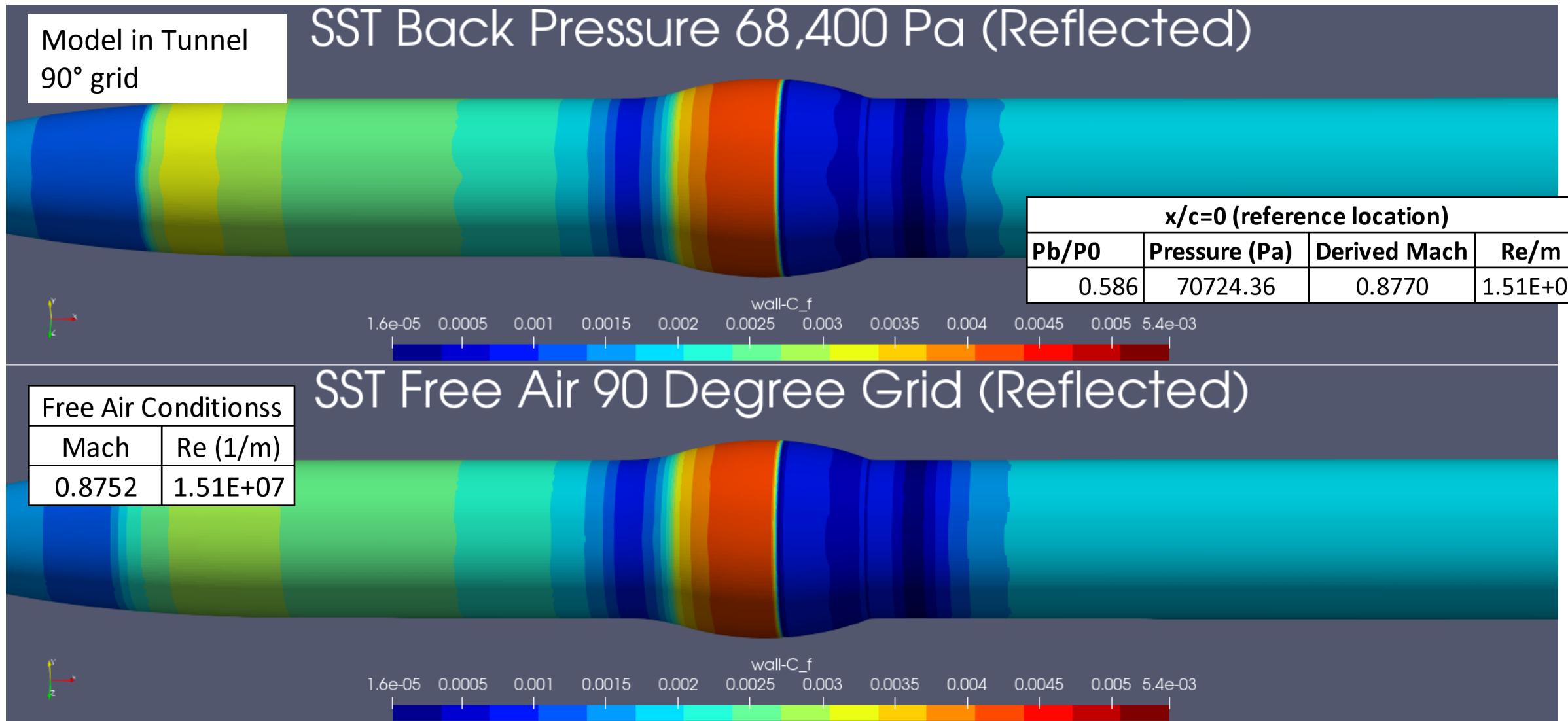


Sparc ATH **SST** Sims
90°, 180° and 360° grids

SST Free Air Solutions Show Axisymmetry



SST: Model in Tunnel vs. Free Air

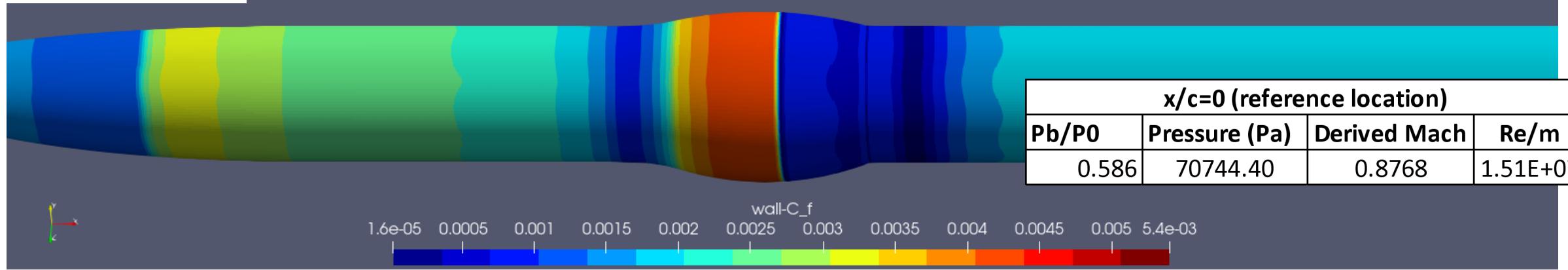


Model-in-Tunnel Grids: 90° and 180°

*Neither solution/plot is reflected for better distinction between them

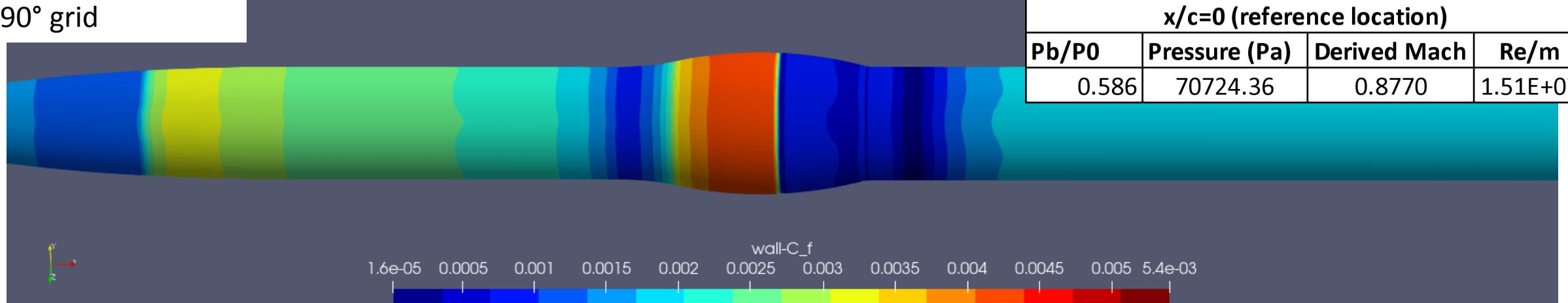
Model in Tunnel
180° grid

SST Back Pressure 68,400 Pa 180 degree grid



Model in Tunnel
90° grid

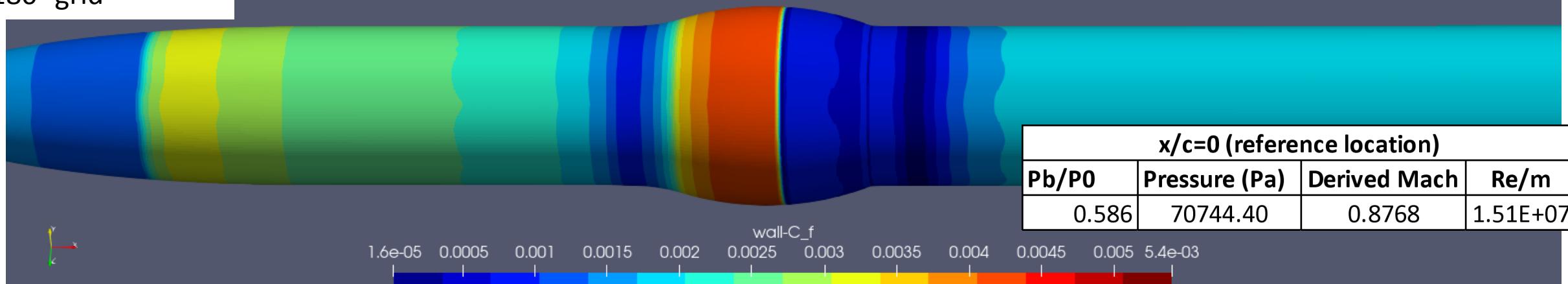
SST Back Pressure 68,400 Pa 90 degree grid



Model-in-Tunnel Grids: 360° and 180°

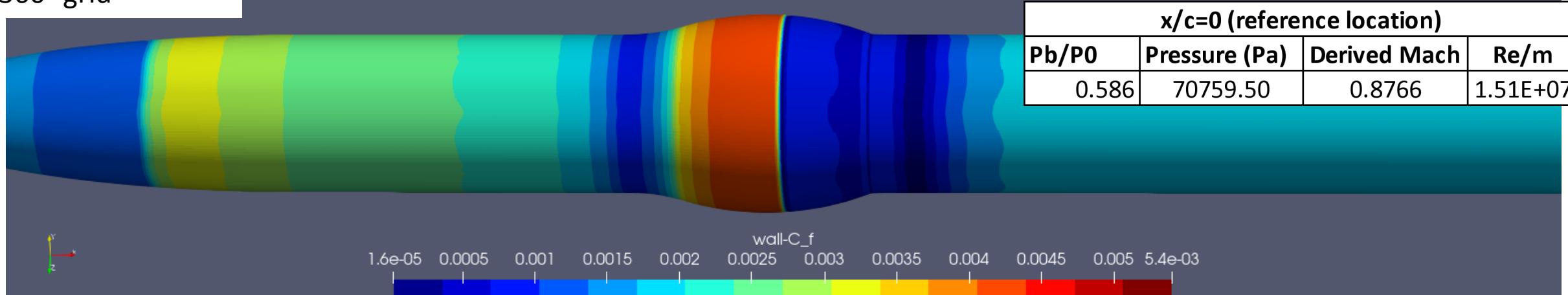
Model in Tunnel
180° grid

SST Back Pressure 68,400 Pa 180 degree grid



Model in Tunnel
360° grid

SST Back Pressure 68,400 Pa 360 degree grid

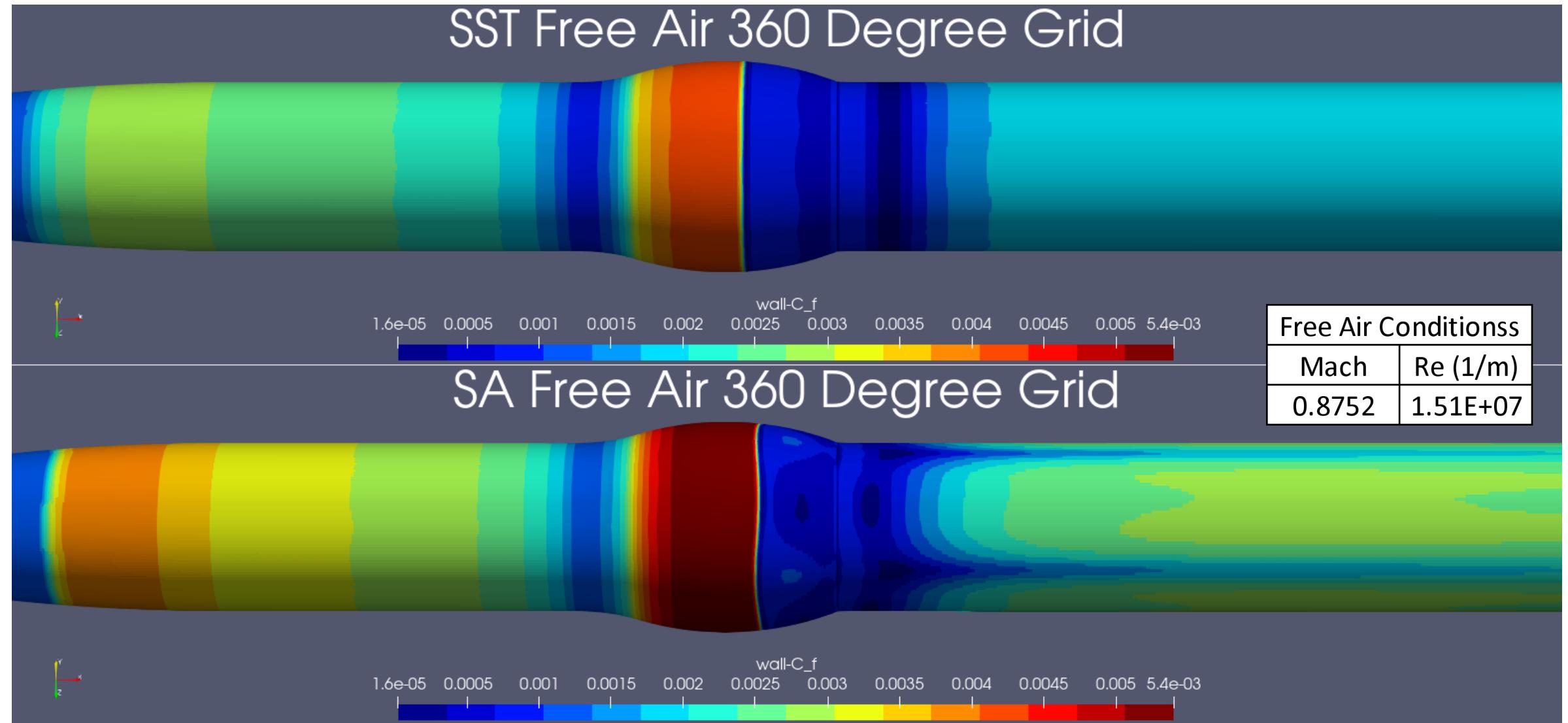


Sparc ATH **SA** and **SST** Sims

Free air grid

360° grid

SST and SA C_f Compared

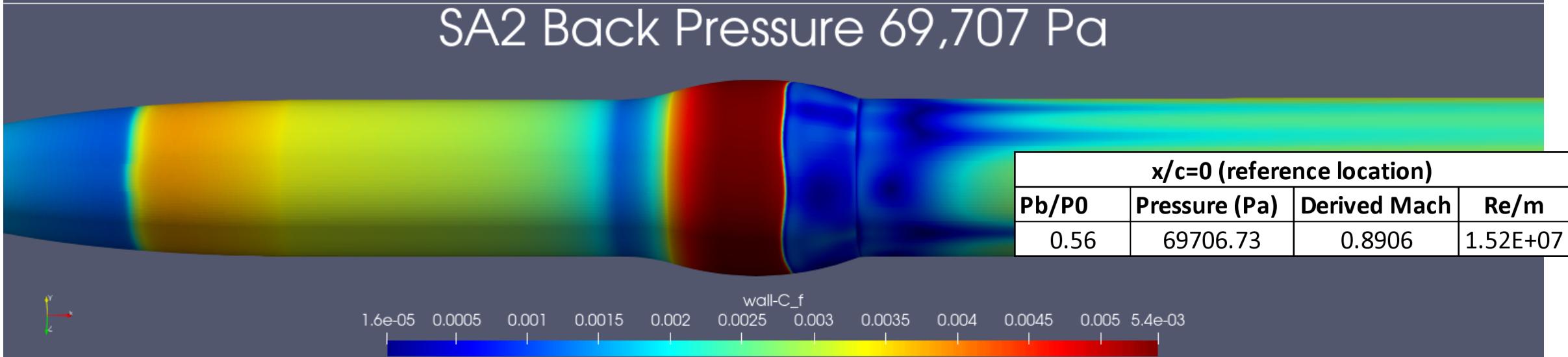
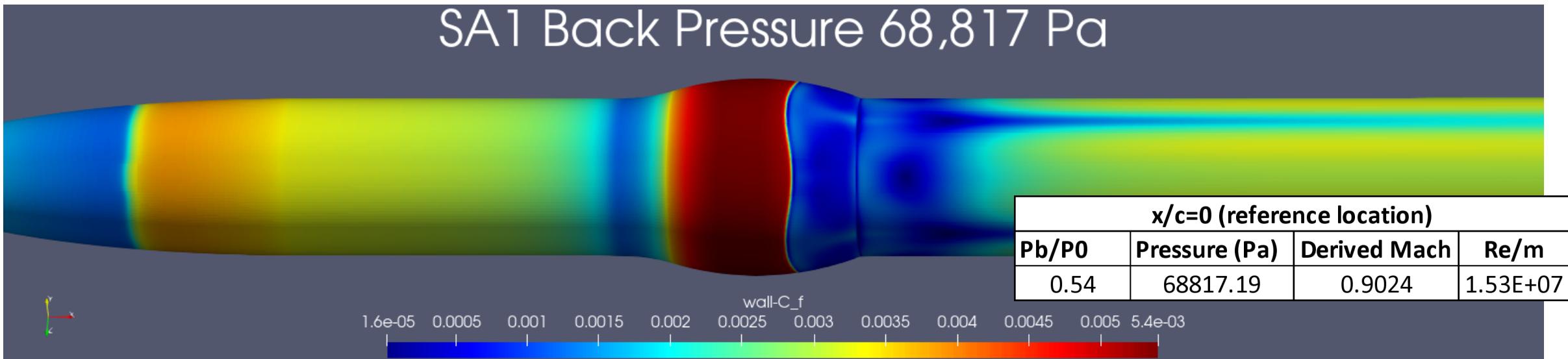


Sparc ATH **SA** Sims
Tunnel grid
90° grid

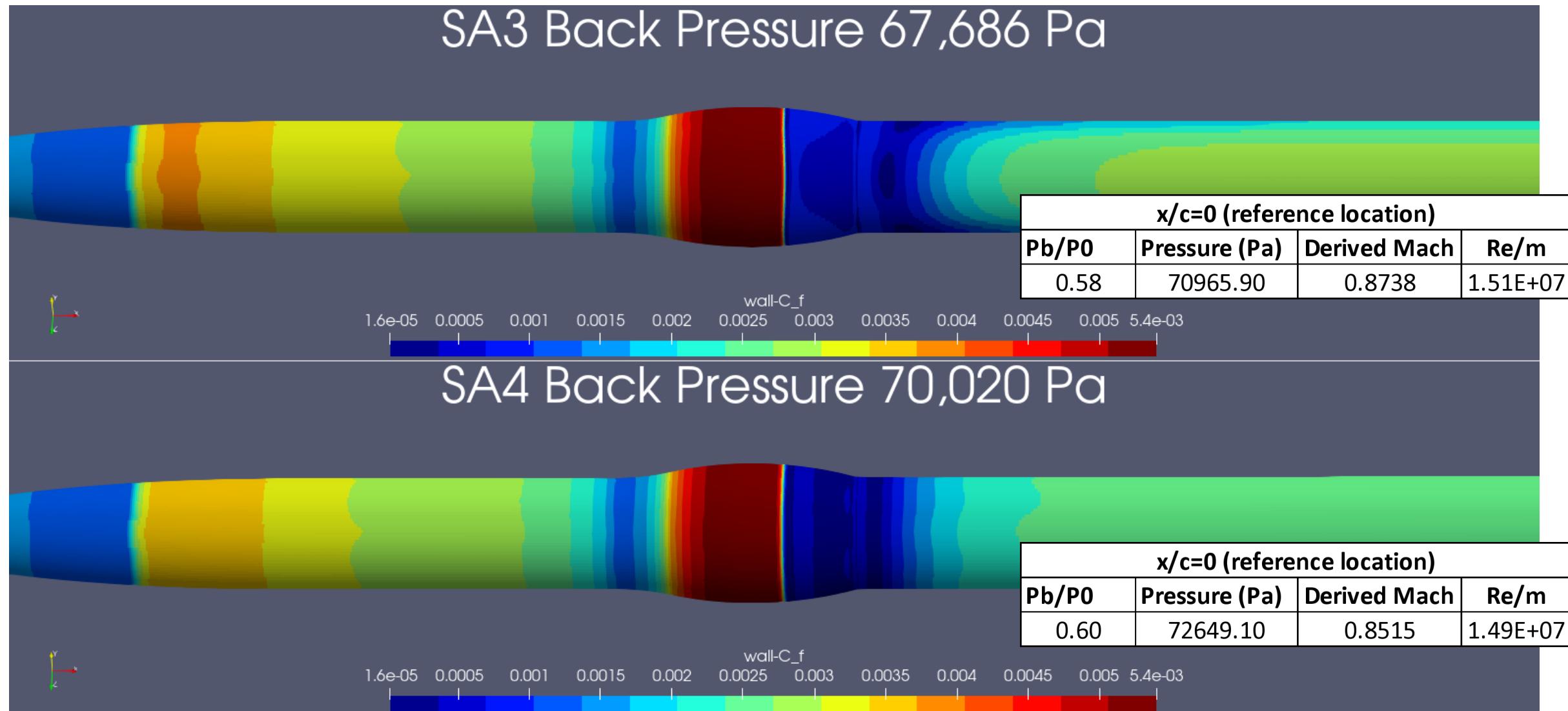
Model-in-tunnel grids: SA Back Pressure Variations

						$x/c=0$	$x/c=0$	
Turbulence Model	Case Name	P_0 (Pa)	T_0 (K)	P_b/P_0	P_b (Pa)	pressure	derived Mach	Re/m
Spalart-Allmaras	SA1	116700	318	0.54	63018	68817.19	0.902	15265796
Spalart-Allmaras	SA2	116700	318	0.56	65352	69706.73	0.891	15187704
Spalart-Allmaras	SA3	116700	318	0.58	67686	70965.90	0.874	15071730
Spalart-Allmaras	SA4	116700	318	0.6	70020	72649.10	0.852	14906631

90 degree quadrants, reflected



90 degree quadrants, reflected

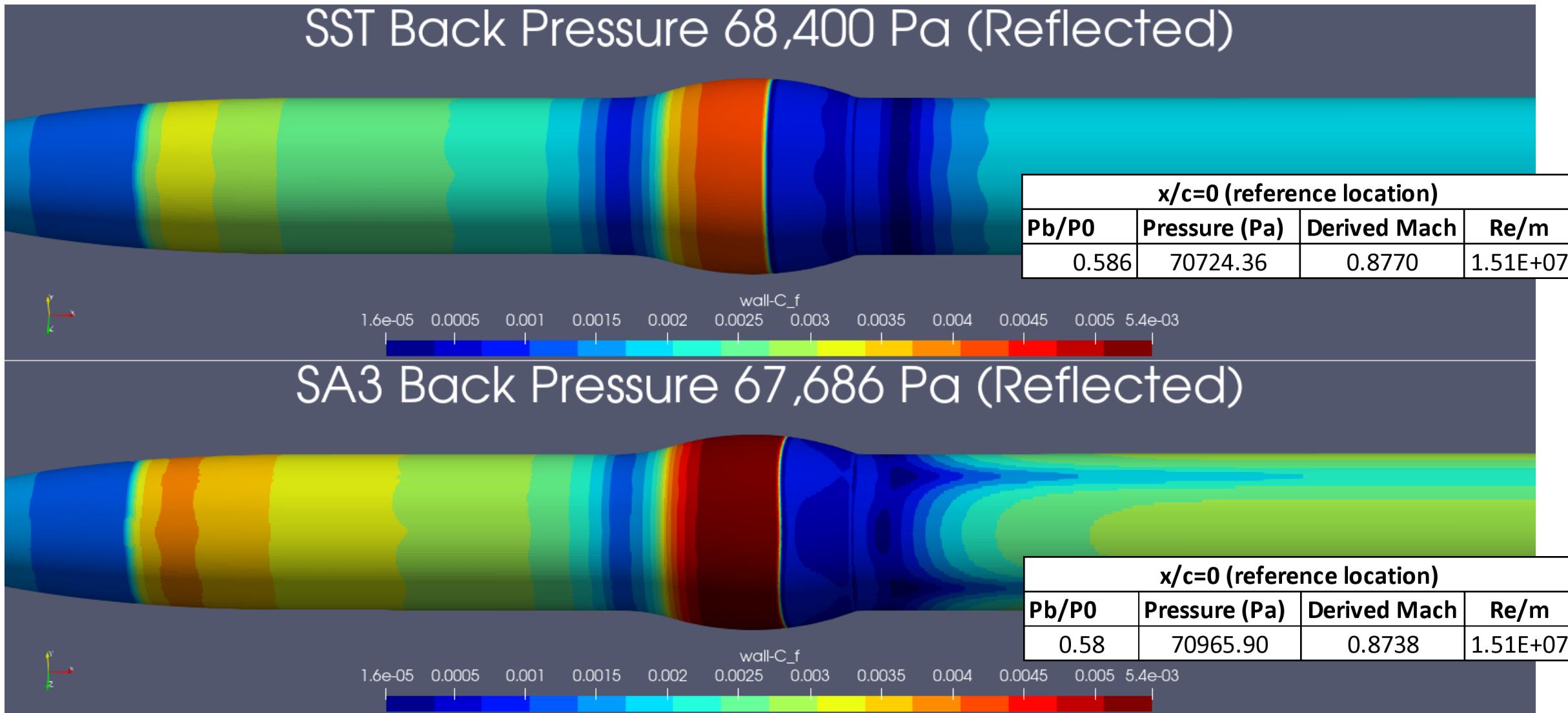


Model-in-tunnel grids

SA and SST with predictions ~Mach 0.875 at x/c=0

Case Name	Turbulence Model	P0 (Pa)	T0 (K)	Pb/P0	Pb (Pa)	pressure	x/c=0	x/c=0	T	mu	Re/m	
SA3	Spalart-Allmaras	116700	318	0.58	67686	70965.90	0.874	275.871	1.73E-05	1.5072E+07		
SST1	SST	116700	318	0.5861	68400	70724.36	0.877	275.603	1.73E-05	1.5094E+07		

90 degree grids, reflected



Sparc ATH: More **SA** Sims
Tunnel grid
90° grid

Reynolds Number Studies

Reynolds Number Calculated using Reference Conditions Derived from Pressure at $x/c=0$

						$x/c=0$	$x/c=0$		Percent
Turbulence Model	Case Name	P_0 (Pa)	T_0 (K)	P_b/P_0	P_b (Pa)	pressure	derived Mach	Re/m	Change Re/m
Spalart-Allmaras	SA5	105030	318	0.56	58817	62816	0.889	13661740	8.92%
Spalart-Allmaras	SA6	93360	318	0.56	52282	55888	0.889	12139160	19.07%
Spalart-Allmaras	SA7	81690	318	0.56	45746	48922	0.888	10619945	29.20%
Spalart-Allmaras	SA8	128370	318	0.56	71887	76681	0.891	16706143	-11.37%

Reference Values ($x/c=0$) SI Units:						
Turbulence Model	Case Name	T	μ	U	ρ	q
Spalart-Allmaras	SA5	274.56	1.7235E-05	295.43	0.79702	34781
Spalart-Allmaras	SA6	274.64	1.7239E-05	295.18	0.70893	30886
Spalart-Allmaras	SA7	274.67	1.7240E-05	295.07	0.62049	27013
Spalart-Allmaras	SA8	274.47	1.7230E-05	295.76	0.97328	42567

Previous slides showed results with a Reynolds number 1.5×10^7 per meter

These four SA solutions result in Reynolds number variation of about -11% to 29%

Each calculated value of C_f , for SA5 through SA8, has a unique **dynamic pressure** calculated after extracting pressure at $x/c=0$

90 degree grids

SA5 Back Pressure 58,817 Pa



$x/c=0$

Derived Mach	Re/m
0.8894	1.37×10^7

SA6 Back Pressure 52,282 Pa



$x/c=0$

Derived Mach	Re/m
0.8885	1.21×10^7

90 degree grids

