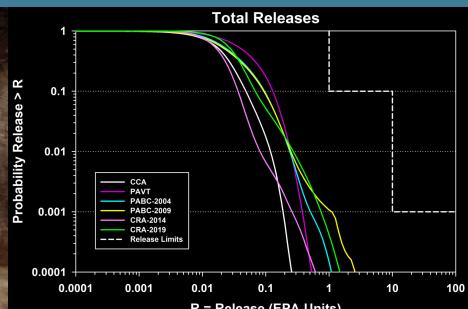
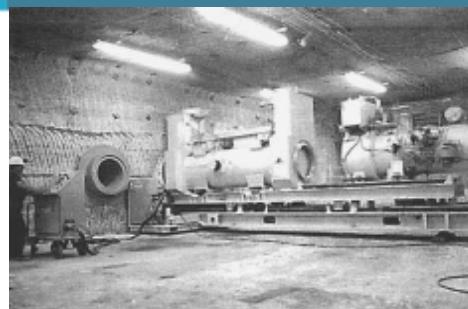




Sandia  
National  
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# Porosity Surface and Fracture Model for the Salado Flow Model



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July 2021



Sandia National Laboratories is a multimission laboratory managed and operated by National Technology & Engineering Solutions of Sandia, LLC, a wholly owned subsidiary of Honeywell International Inc., for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-NA0003525. This research is funded by WIPP programs administered by the Office of Environmental Management (EM) of the U.S. Department of Energy

# Gas generation and pressure for Porosity Surface.

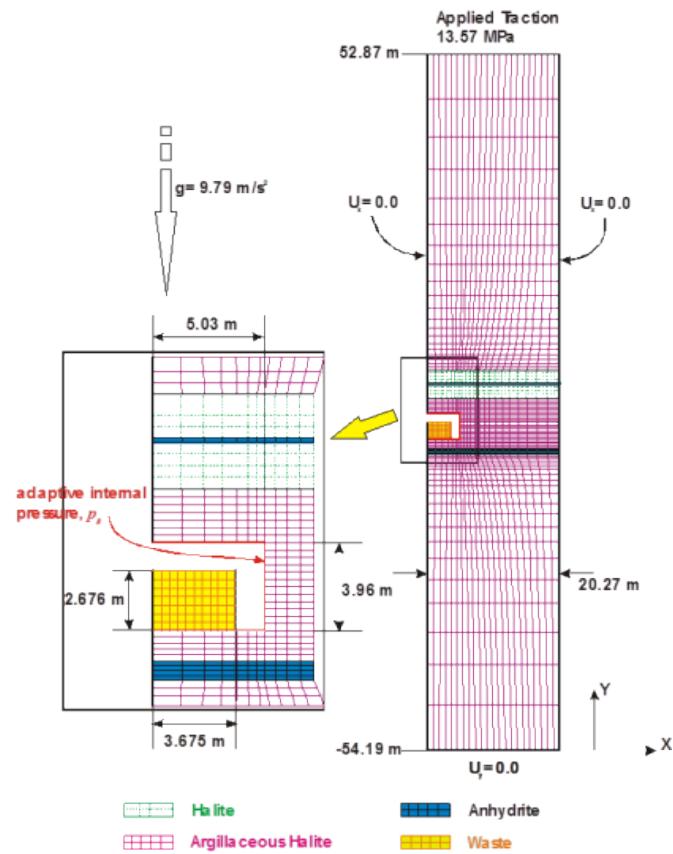


Figure PORSURF- 2. Mesh Discretization and Boundary Conditions Used for the Porosity Surface Calculations

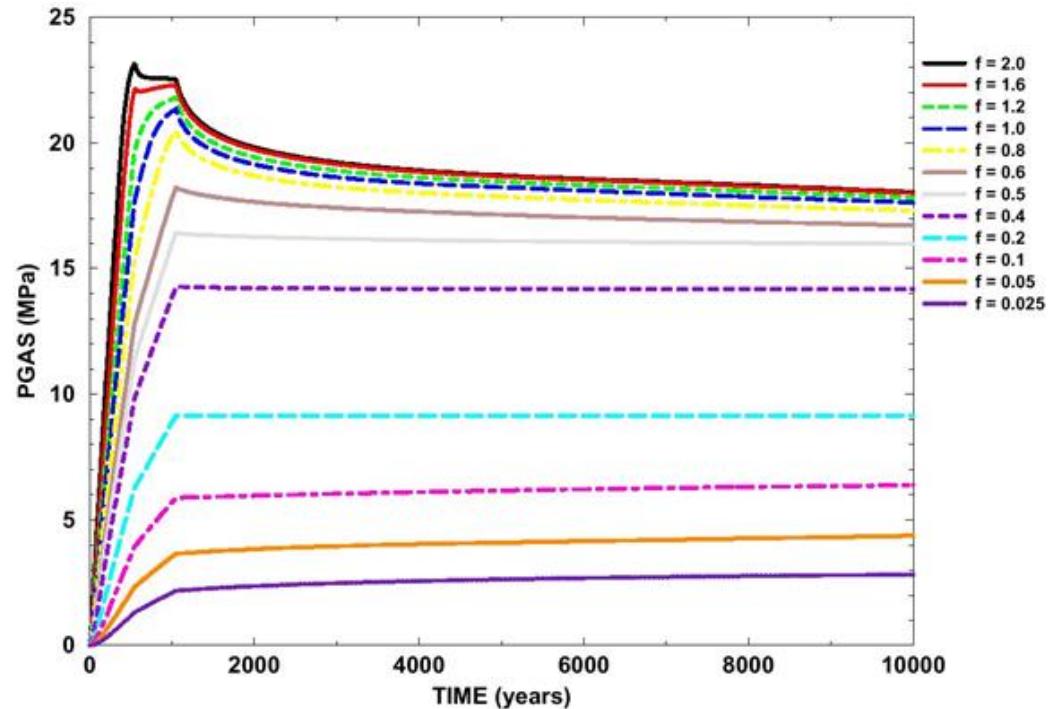


Figure PORSURF- 4. Disposal Room Pressure for Various Values of the Scaling Factor  $f$

DOE(2014) CRA-2014 Appendix-PORSURF -  
[https://wipp.energy.gov/library/CRA/CRA-2014/CRA/Appendix\\_PORSURF/Appendix\\_PORSURF.htm](https://wipp.energy.gov/library/CRA/CRA-2014/CRA/Appendix_PORSURF/Appendix_PORSURF.htm)

# Porosity Surface

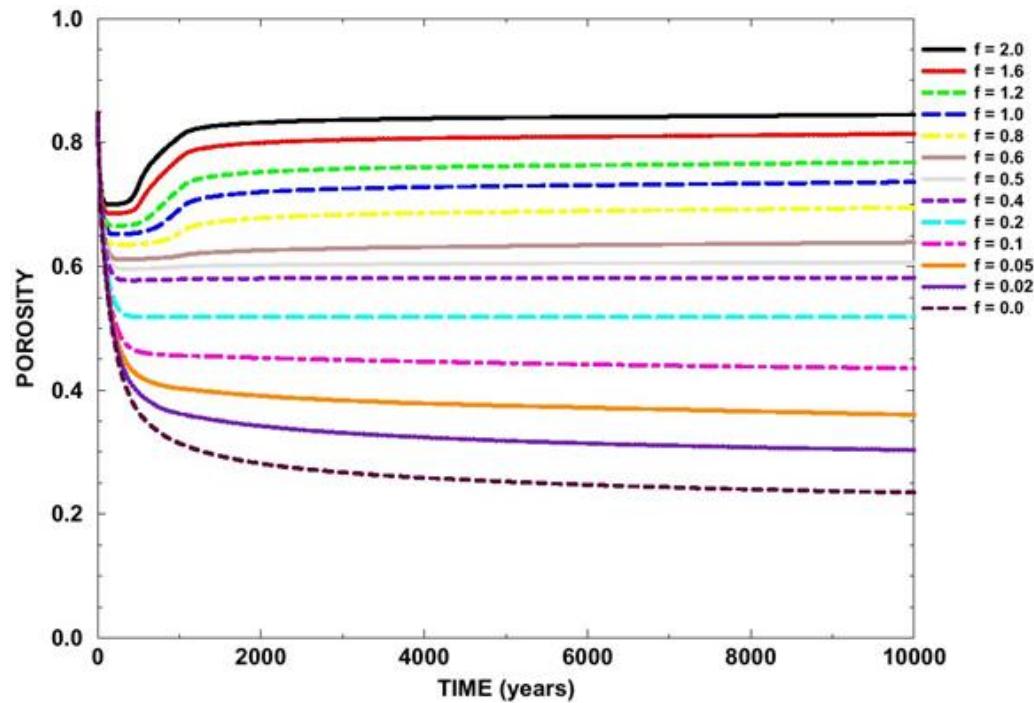
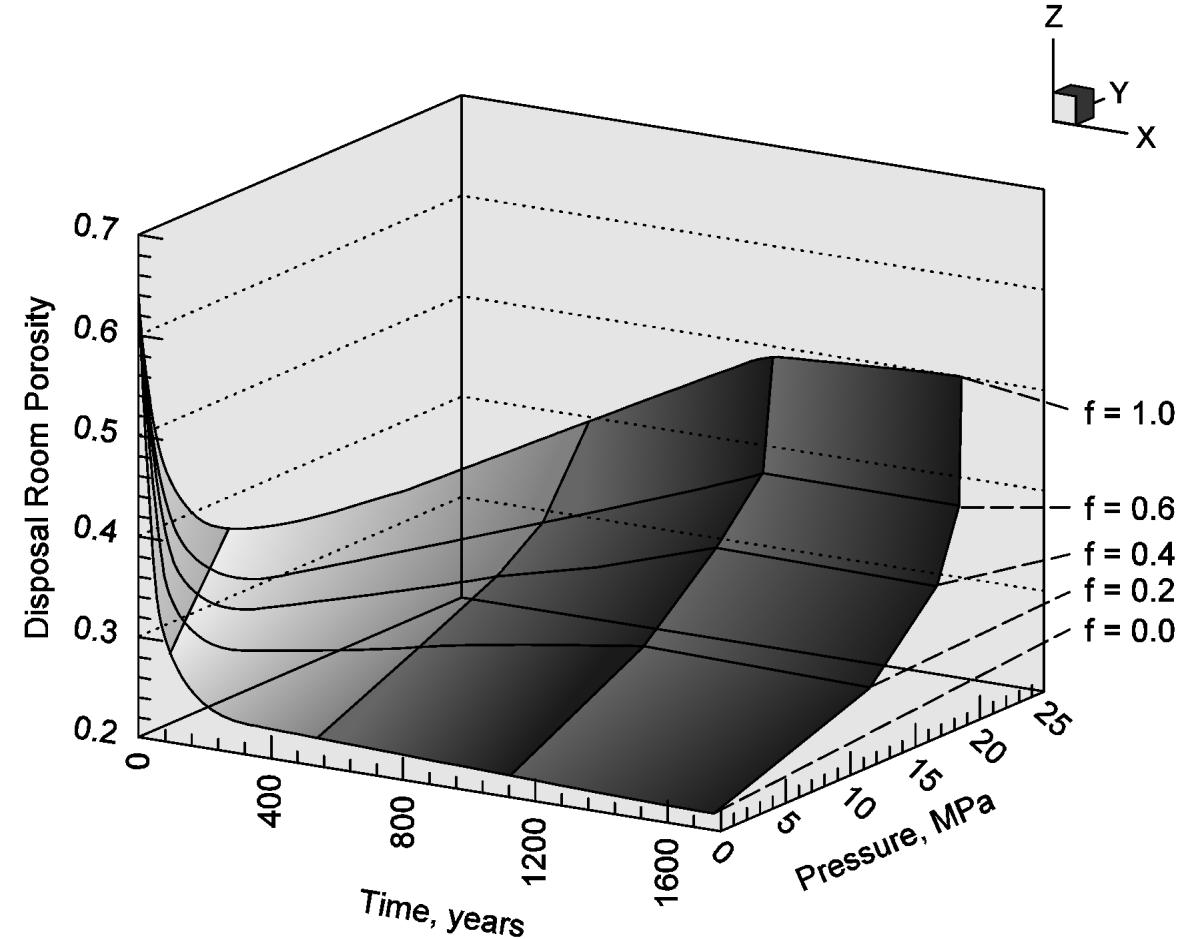


Figure PORSURF- 3. Disposal Room Porosity for Various Values of the Scaling Factor  $f$



**Pressure driven porosity function generated from SANTOS structural mechanics code. (Park and Hansen, 2003).**

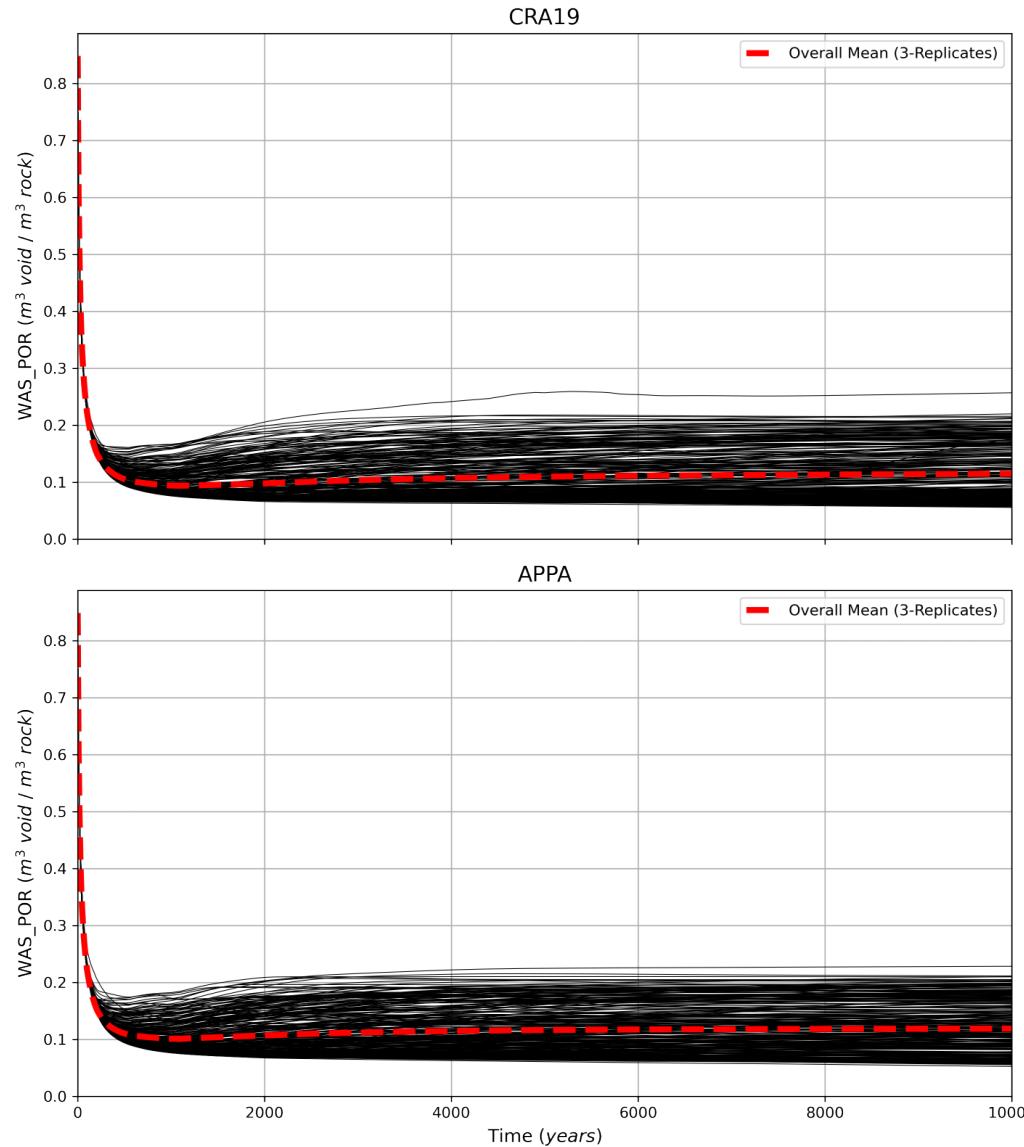
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Park, B. and F. Hansen, 2003. Determination of the Porosity Surface of the Disposal Room Containing Various Waste Inventories. Sandia National Laboratories. Carlsbad, NM. <https://wipp.energy.gov/library/CRA/CRA-2019/N%20-%20S/Park%20and%20Hansen%20%202003%20%20ERMS%20533216.pdf>

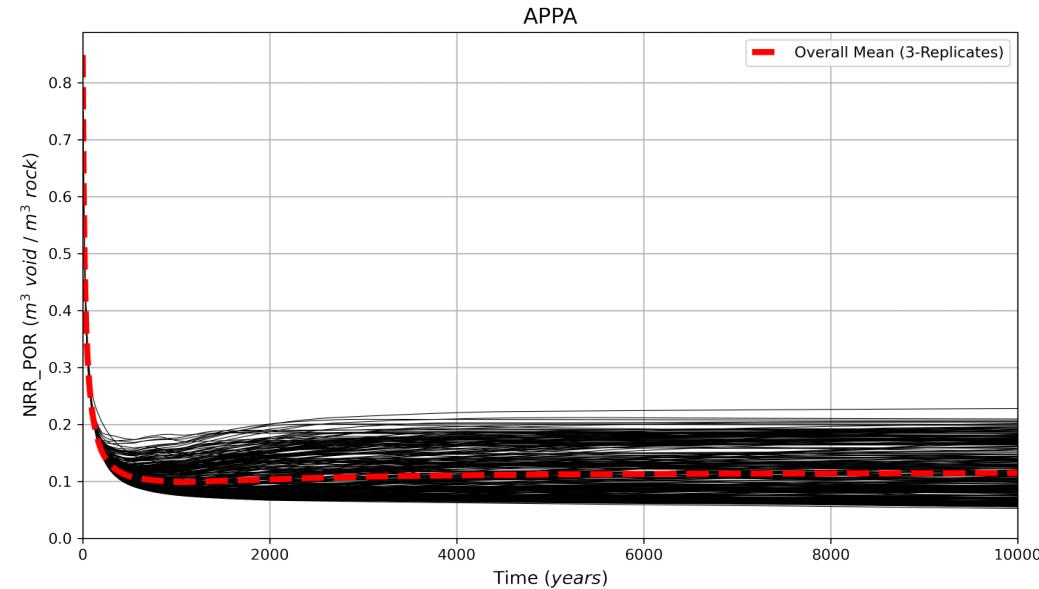
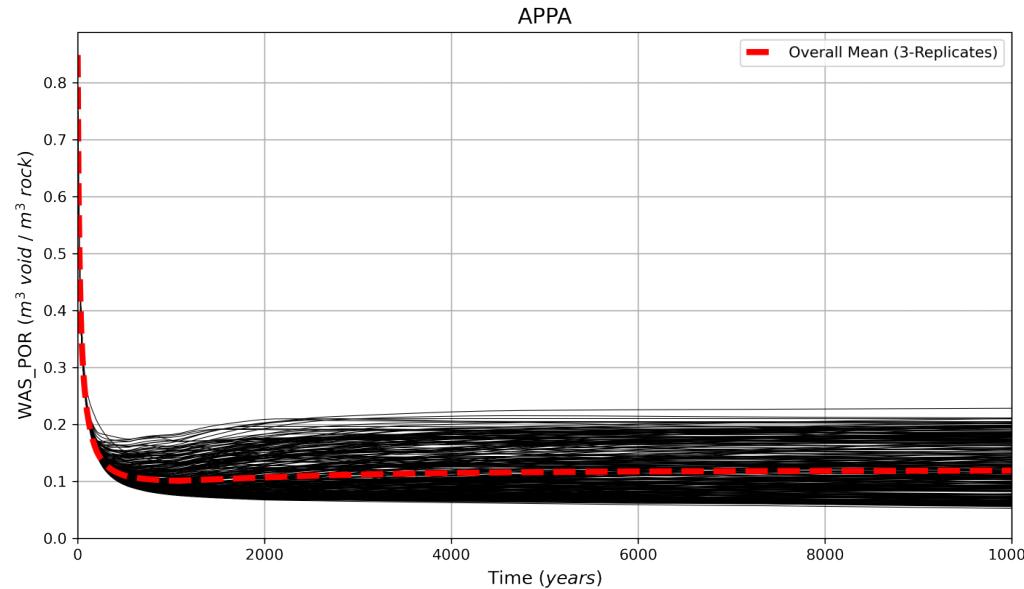
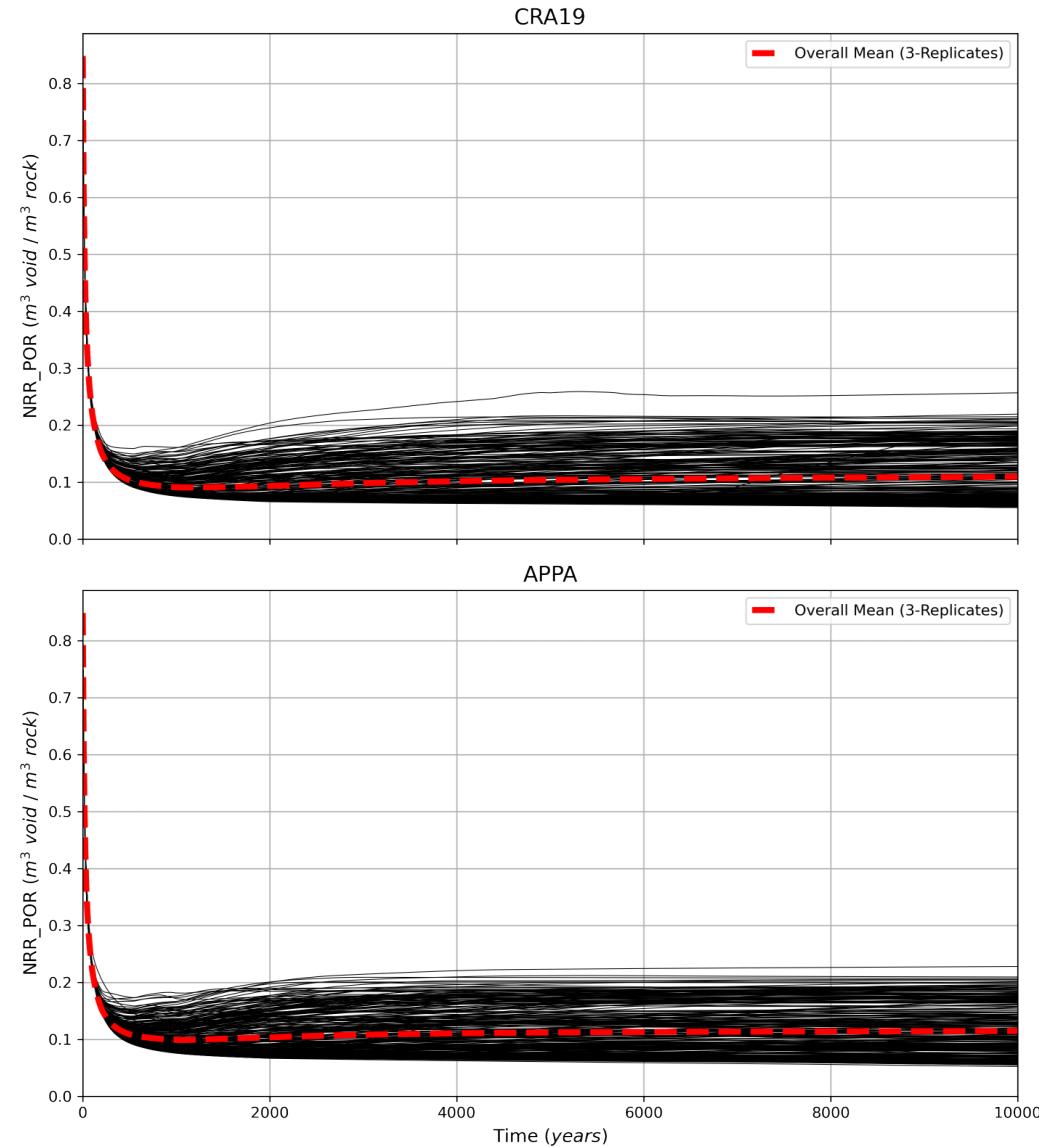
# Waste Area Porosity Evolution



Scenario S1-BF  
Porosity in Waste Panel



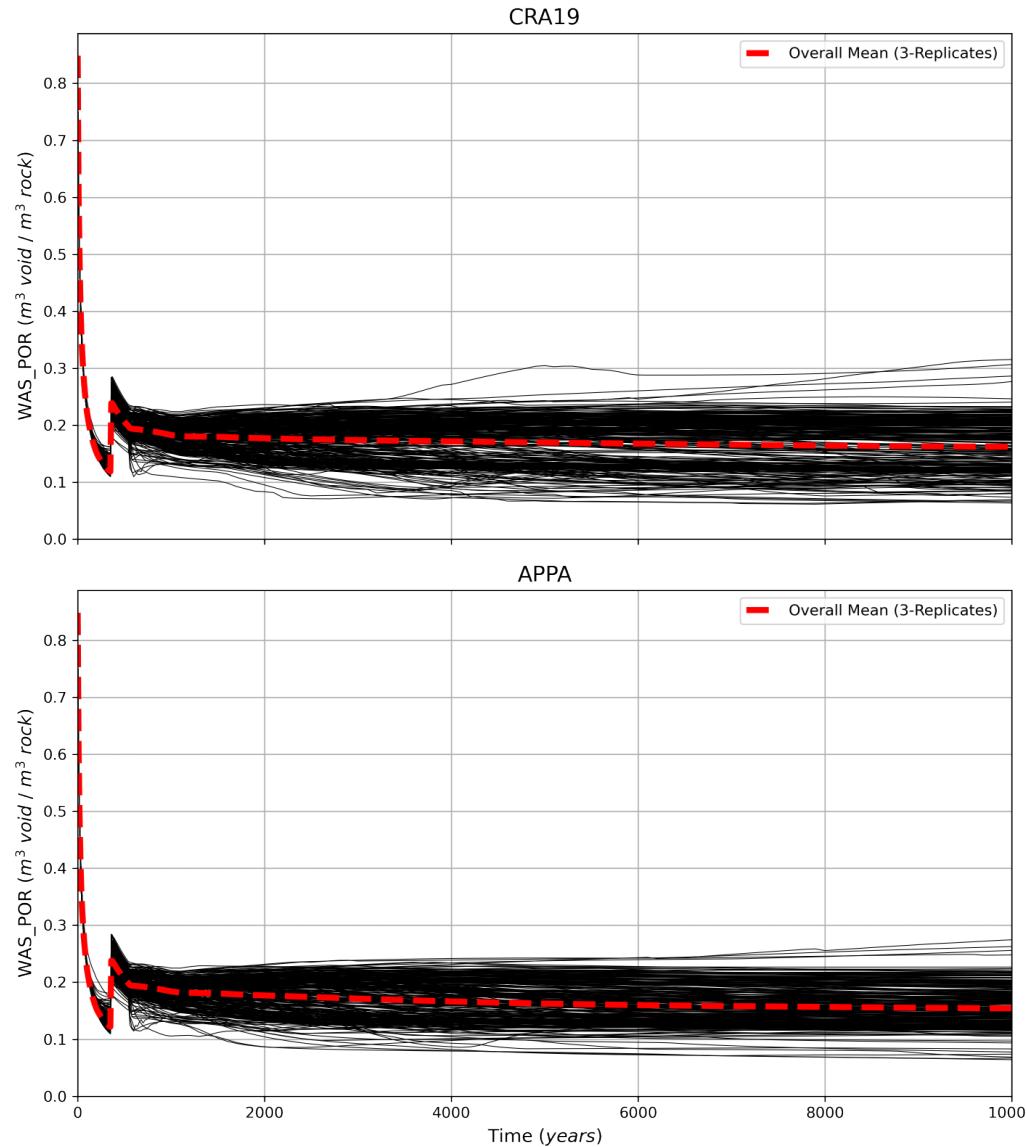
Scenario S1-BF  
Porosity in North Rest-of-Repository



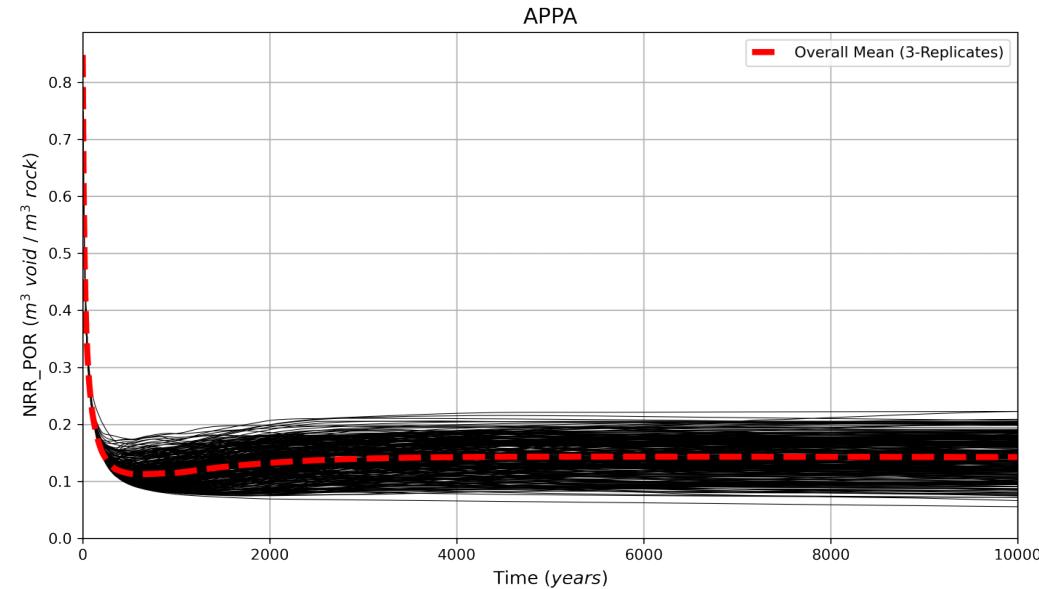
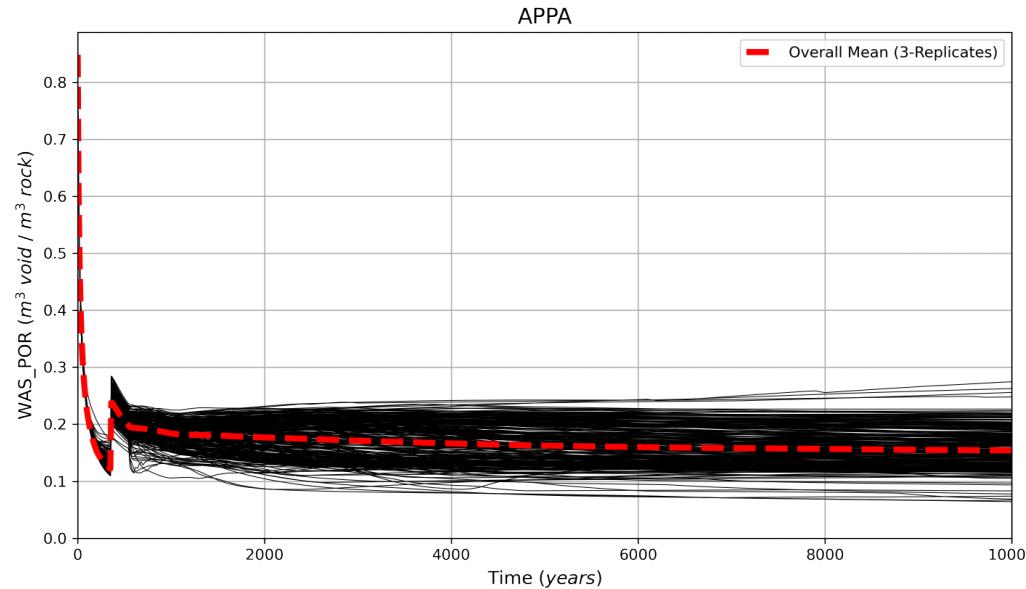
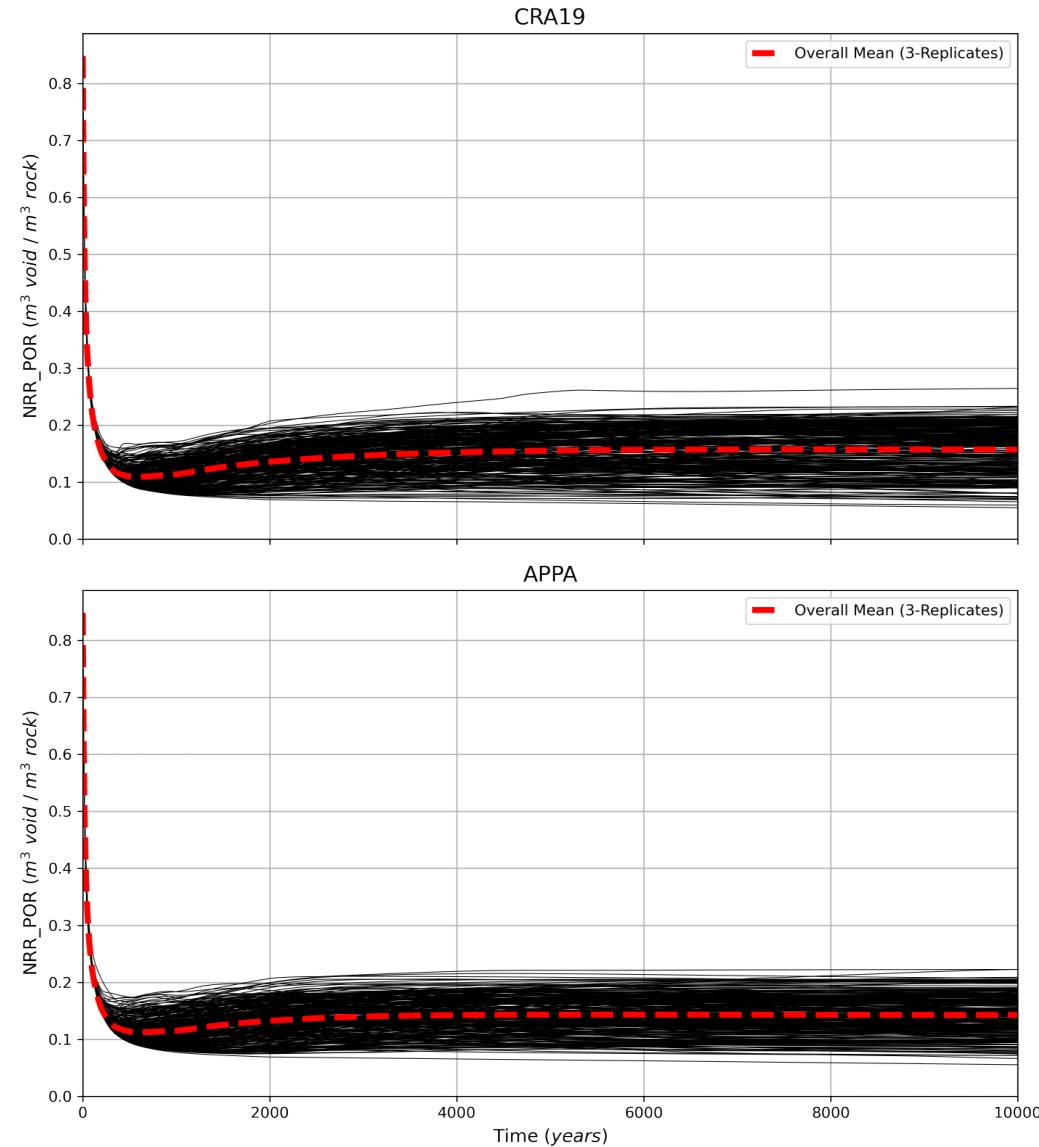
# Waste Area Porosity Evolution



Scenario S2-BF  
Porosity in Waste Panel



Scenario S2-BF  
Porosity in North Rest-of-Repository



# Fracturing model



Pressure-driven fracturing applies to DRZ and anhydrite interbeds (above and below DRZ)

Conceptualized as dilating natural or excavation-caused fractures that are assumed to not fully heal with creep closure

Initiate at  $p_{bi}=12.7\text{ MPa}$ , fully dilate at  $p_{ba}=15.5\text{ MPa}$

Before fracturing:

- Porosity 0.6 – 1.7% (interbeds), 0.04 – 3.3% (DRZ)
- Permeability  $10^{-21} – 7.9 \times 10^{-18} \text{ m}^2$  (interbeds),  $3.98 \times 10^{-20} – 3.16 \times 10^{-13} \text{ m}^2$  (DRZ)

- Linear change in porosity (up to +4% for MB138, MB139, +24% for A/B)
- Power law change in permeability

$$k_f(p_b) = \left[ \frac{\phi(p_b)}{\phi(p_{bi})} \right]^n k,$$

- $k$  – non-fractured permeability
- $\phi$  – porosity (function of pressure)
- $n$  – empirical exponent so that

$$k_f(p_{ba}) = 1 \times 10^{-9} \text{ m}^2 \text{ at full dilation}$$

Reference: DOE (2004) CRA 2004, Appendix PA, Section 6.4.5.2 and 6.4.5.3

# CRA-2019 DBR simulation of upper intrusion animation

