

NUCLEAR WASTEFORM AND BARRIER MATRIXES INTERACTIONS WITH GEOLOGIC STRATA

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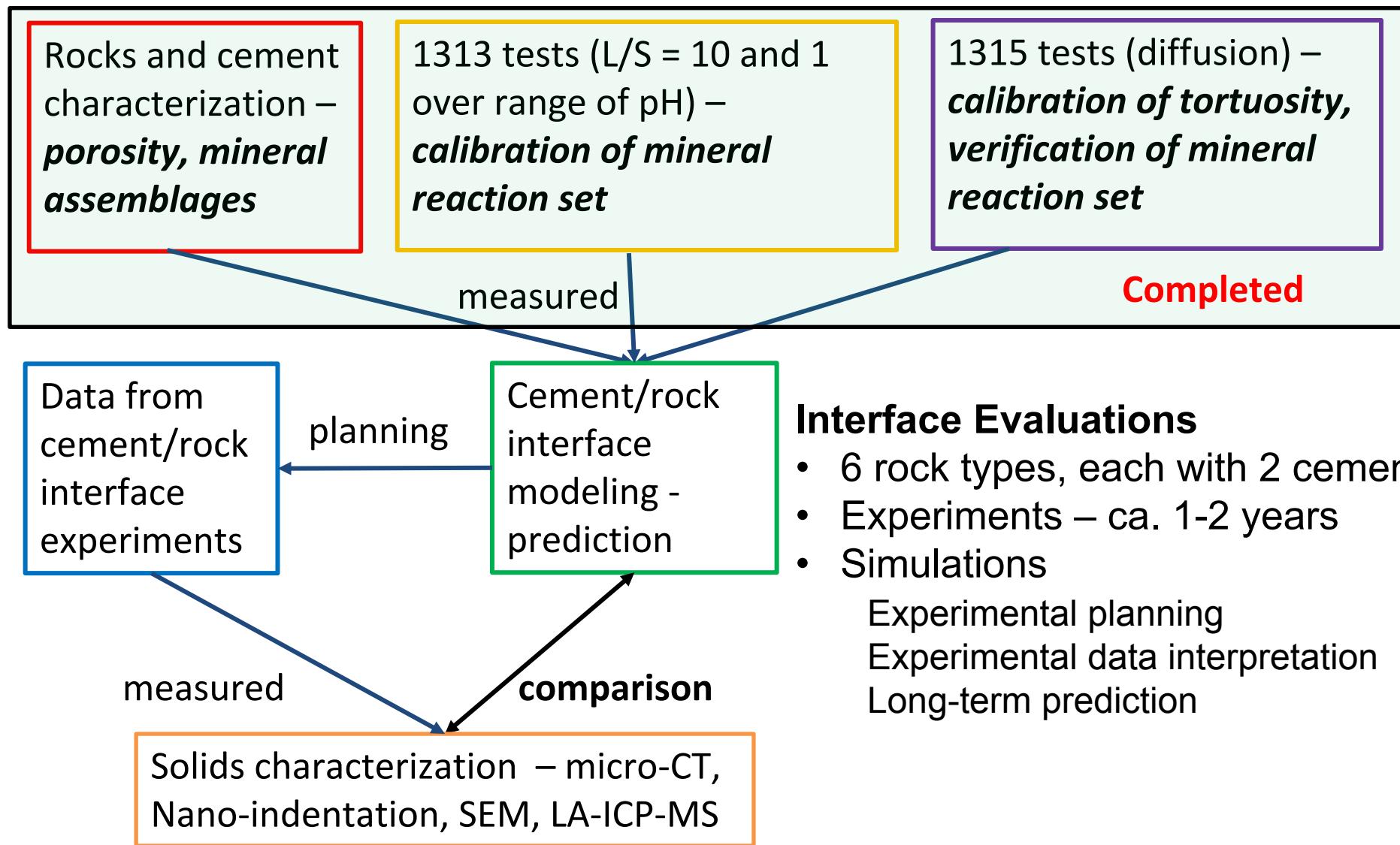
Objectives

Project goal: Characterize interactions of doped cement materials (Low pH cements and CEM I) with carbonate geologic strata (e.g., limestone, marl, chalk, oil shale).

Specific objectives:

- i) Use laboratory experiments to characterize the reactions and transport of radionuclides (dopants) and primary matrix constituents at the interface between carbonate rock types and cementitious barriers; and,
- ii) Demonstrate and benchmark multiphase diffusion reactive transport models for parameter estimation and to simulate long-term interactions considering potential intermediate depth borehole disposal.

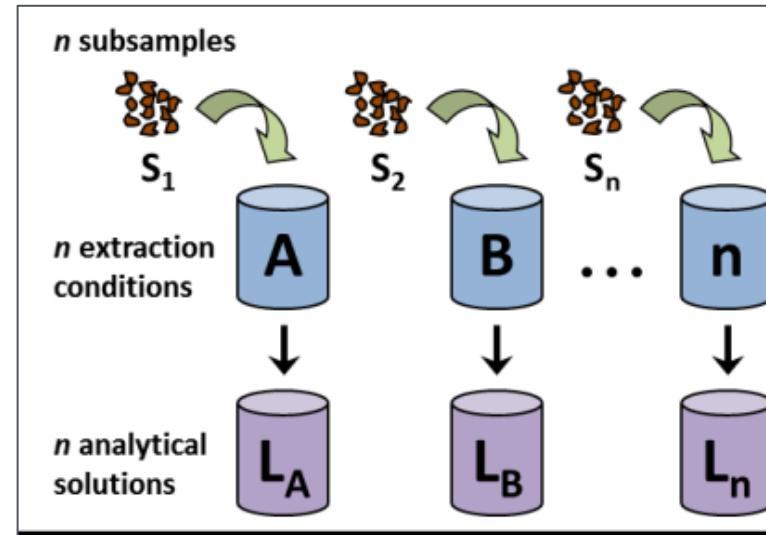
Project Approach



EPA Method 1313

Method 1313

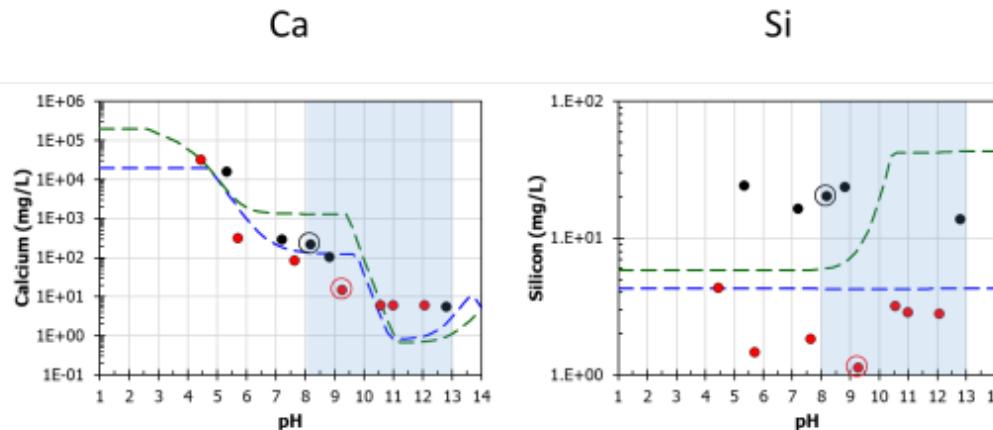
- pH dependent leaching test
 - L/S (ml g^{-1}) of 10 and 1 for rock samples and two cement types.
 - 10 parallel extractions at different target end-point pH
- Analysis
 - Extracts analyzed using ICP-OES, ICP-MS, TOC, and IC. Additional measurements include pH, conductivity.



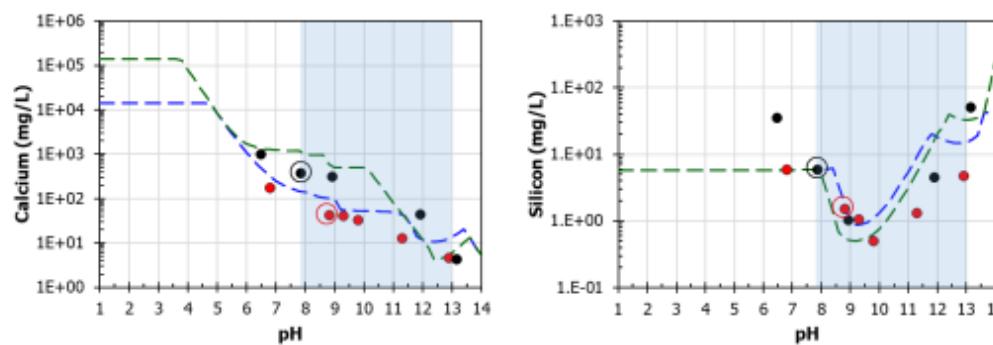
Mineral Reaction Set Calibration

Data from USEPA
Method 1313

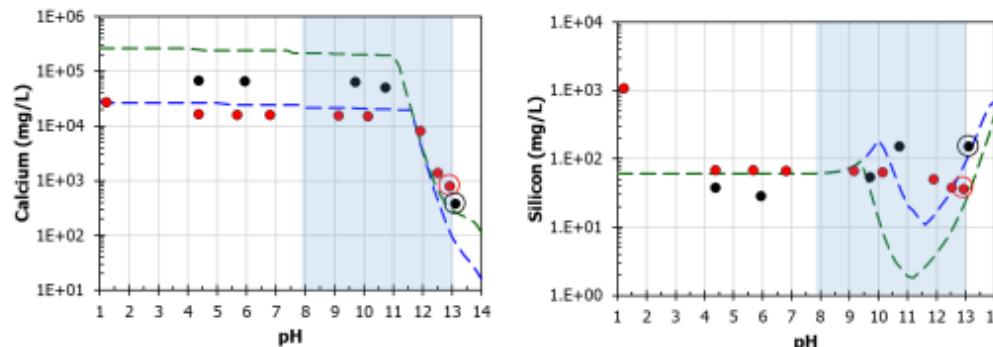
Limestone



Marl



OPC paste

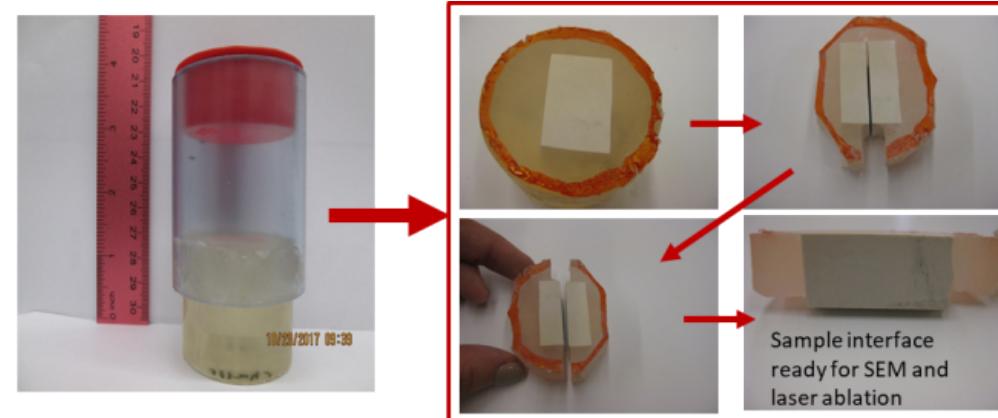


- Experimental L/S=10 mL/g-dry
- Experimental L/S=1 mL/g-dry
- Modeled L/S=10
- Modeled L/S=1
- Natural pH L/S=10
- ◊ Natural pH L/S=1

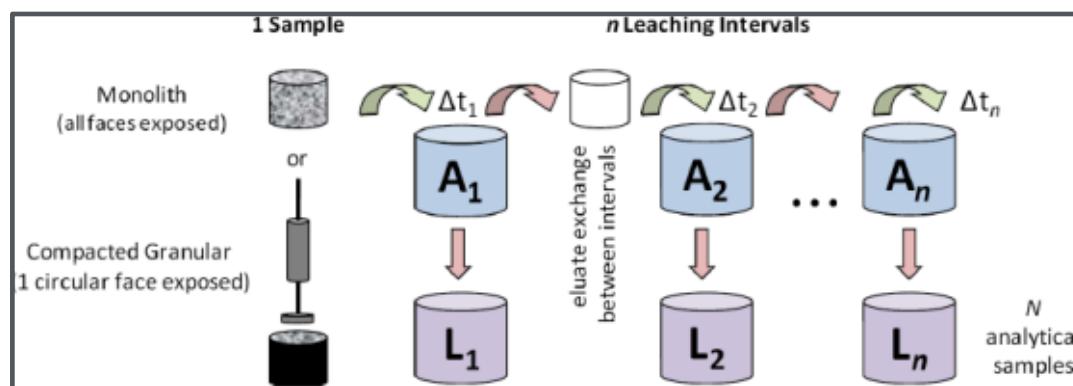
Experimental Methods (EPA 1315)

Method 1315

- Mass transfer rate tank leaching test - modified for post-test profile characterization

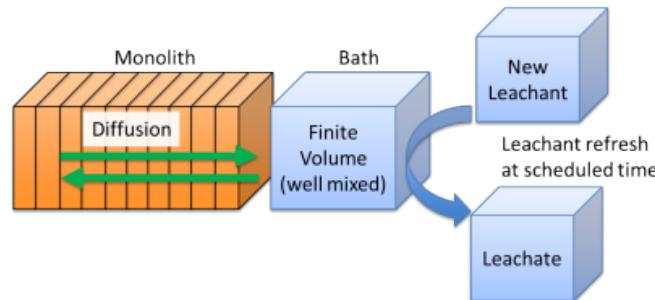


Method 1315 – Experimental set up and sample processing



Comparison of Diffusion Leaching Test to Field Conditions

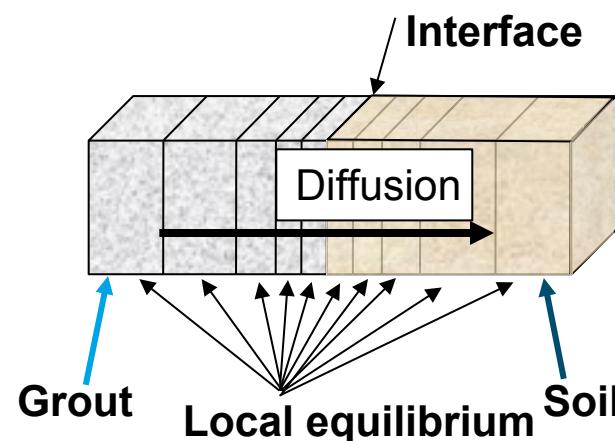
Test Conditions



Diffusion Leaching Test

- 10 mL/cm² liquid volume-to-surface area (L/S_A)
- Leachant refreshed frequently to maximize leaching (dilute boundary condition)
- Saturated conditions

Simulation Conditions



Field Conditions

- \approx 0.02 to 0.1 mL/cm² liquid volume-to-surface area (L/S_A), based on saturation
- Unsaturated conditions; slow porewater displacement

➤ **Leaching under field conditions is several orders-of-magnitude slower than lab test conditions**

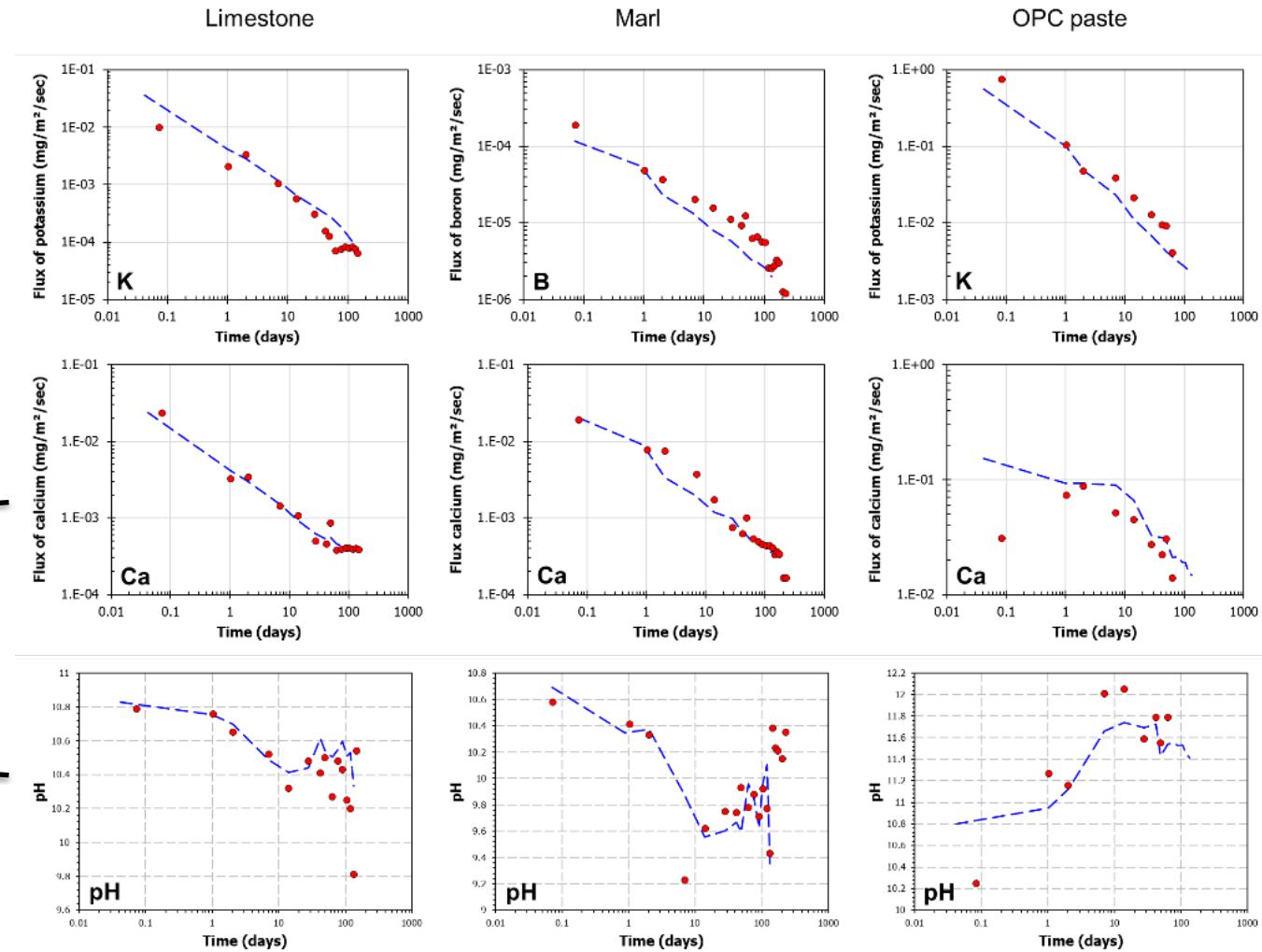
Tortuosity Calibration

Calibration and
Validation of mineral
reaction set

Prediction of 1315
results based on
mineral reaction set
calibrated by 1313 test

calibration

Validation



$$\frac{\text{porosity}}{\text{tortuosity}} = \frac{\phi}{\tau^2} = 0.0007$$

$$0.003$$

$$0.0006$$

Interface Experiments

Current Status:

Cements were cast on saturated rock (Oct. 2019)

6 rock types - limestone, chalk, marl, oil shale,
LOM and HOM

2 cements - OPC and low pH cement

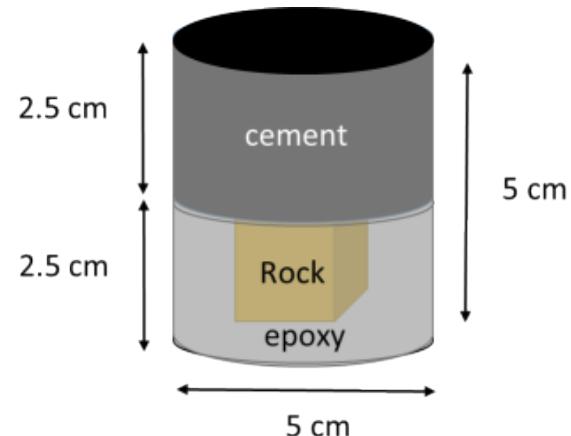
6 samples per rock/cement interface

Curing and aging conditions:

30 °C and 100% relative humidity

**Sampling time to be
based on simulation &
micro-CT results**

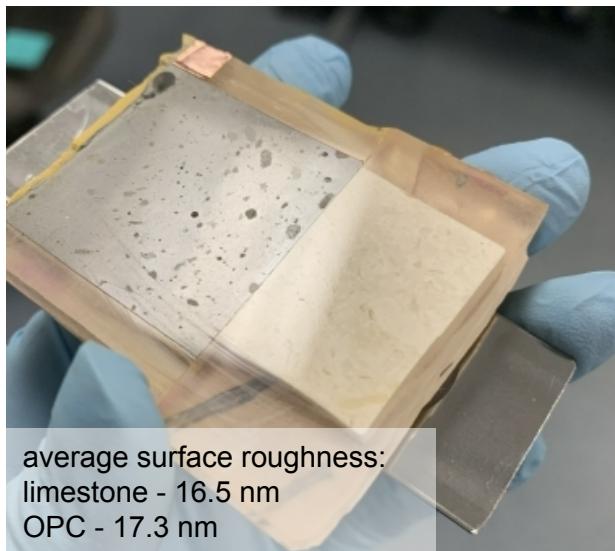
**Current curing
time: ~12 months**



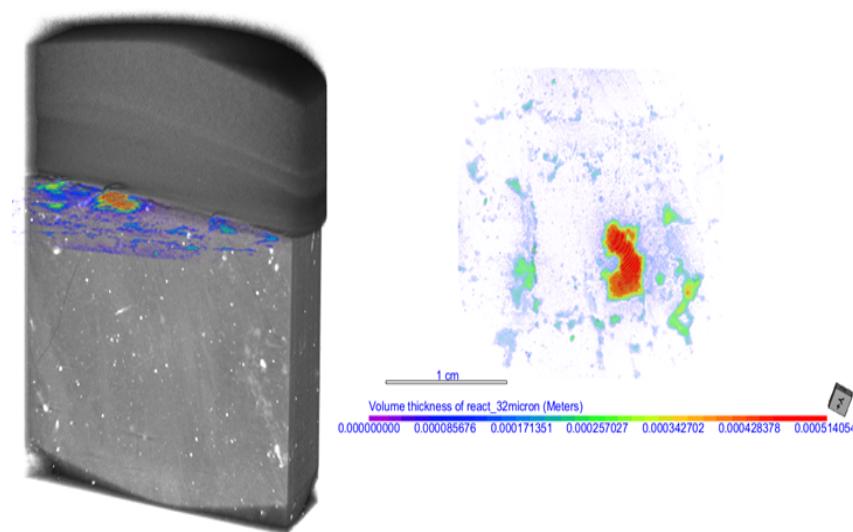
Advanced Characterization of Interfaces

Interfaces are characterized for:

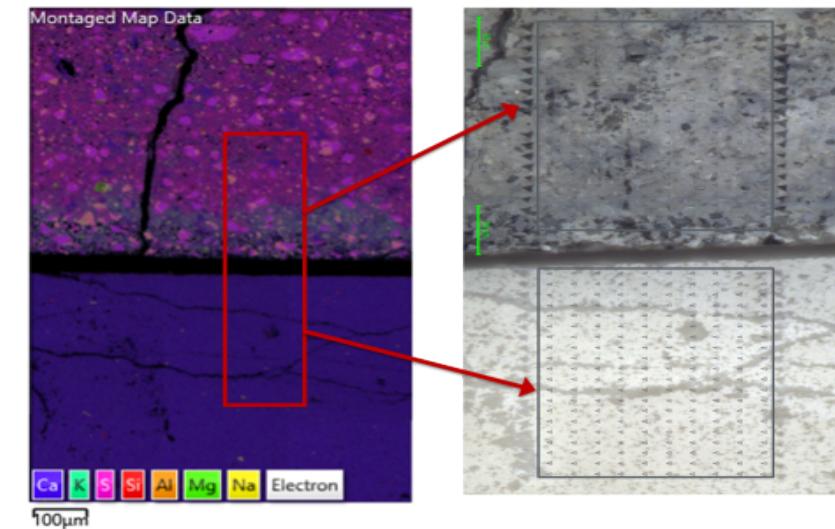
- Leaching and interface characterization – SEM-EDS and LA-ICP-MS
- Volume and porosity change - micro-CT
- Changes in material mechanical properties as a result of interface reactions - Nano indentation



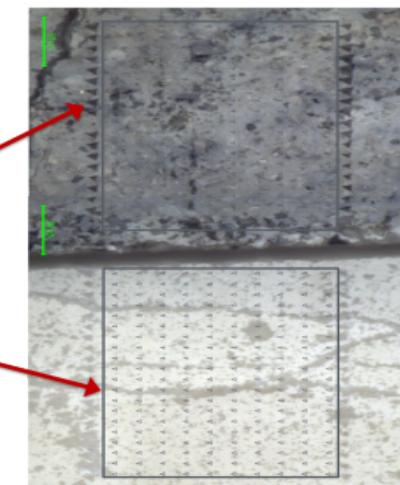
**Polishin
g**



**Micro-
CT**

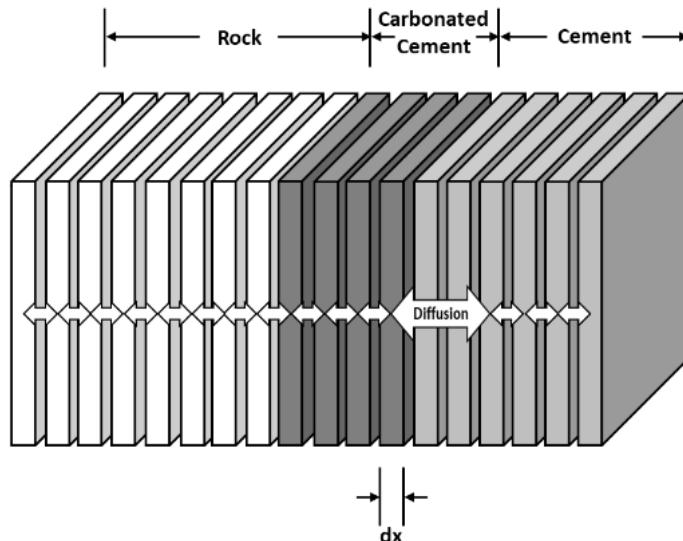


**SEM-
EDS**



**Nano-
indentation**

Conceptual Model – Rock/Cement interface



Model assumptions:

- Each cell is well mixed
- Local equilibrium
- C-(N-)A-S-H solid solutions
- Multi-ionic diffusion only

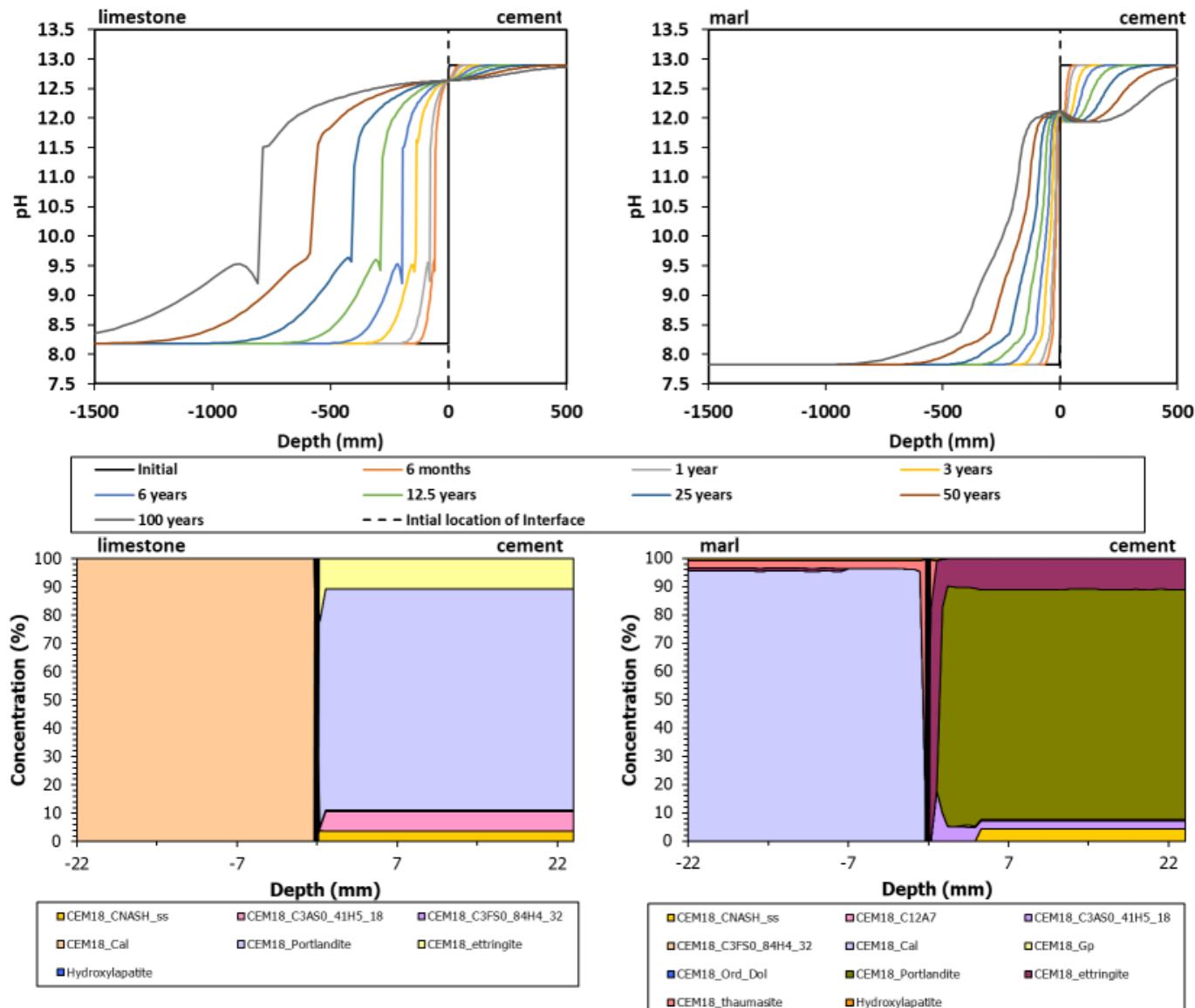
Modeling platforms:

- LeachXS/ORCHESTRA
- PFLOTTRAN

Model conditions for experimental case:

- 100 years simulated, saturated conditions, 30 C
- 1-D, 378 cells, Finite volume
- No fluxes at external boundaries
- Thermodynamic databases – Minteq v4; LLNL, CEMDATA18 (Lothenbach et al. (2018))
- Initial carbonate content – based on 1313 test
- Tortuosity – calibrated values
- Porosity – measured values

Interface Models Results



Interface Models Results – carbonation front progress prediction

The location, X_C , of the moving carbonation front as a function of cement composition and conditions, when the relative humidity is above 50%, is (Papadakis et al., 1989):

$$X_C = A\sqrt{t}$$

X_C - the location, of the moving carbonation front (mm)

A - proportionality constant (mm $\text{yr}^{-0.5}$)

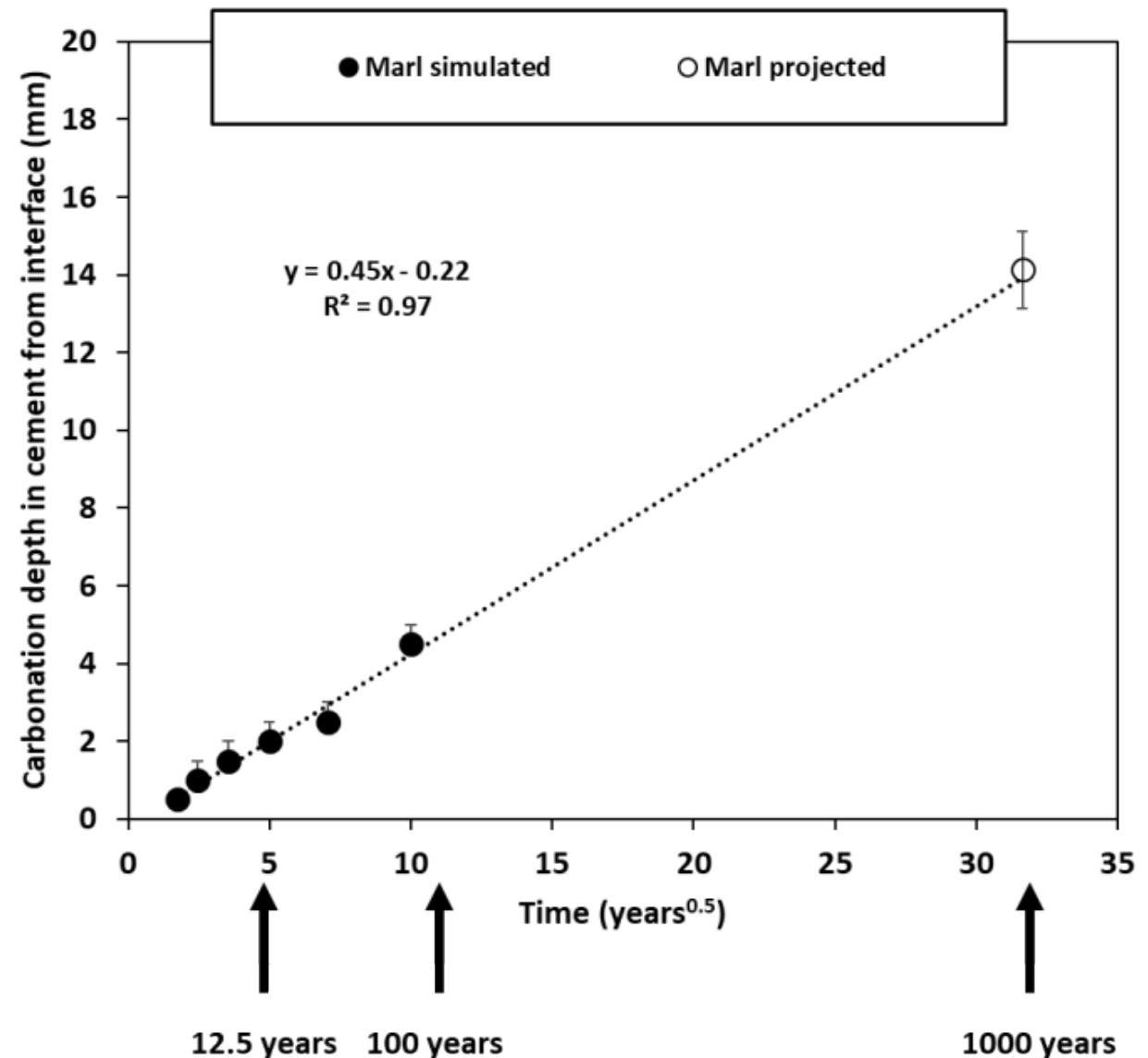
t - time (years)

1,000 years scenario (saturated):

- 14 mm OPC are carbonated

10,000 years scenario (saturated):

- 45 mm OPC are carbonated



Interface Models Results – effect of water saturation

- water relative saturation in vadose zone:
10%-40% at depths deeper than 2m
- The diffusivity under saturated conditions is about 21 and 2150 time greater than at 40% and 10% water relative saturation, respectively.
- Incorporating these factors into the proportionality constant (A) results in:
 - under 40% water relative saturation:
435,000 years and 4.5 million years for the carbonation front to penetrate to a depth of 14mm and 45mm (from 1,000 and 10,000 year scenarios) into cement.
 - Under 10% water relative saturation,
4.5 million years and 46 million years are required to penetrate depth of 14mm and 45mm.

