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Conference Paper Session #1

Impact of COVID-19 on Energy Consumption and Grid-Interactive
Efficient Buildings

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***Institutional Climate Analysis for
Future Heat Wave Scenarios: Sandia
National Laboratories California Site***



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Learning Objectives

- Describe the attributes of a load profile.
- Explain why weather-normalization is useful in analyzing electricity consumption.
- Describe how a data-driven grey-box model can be used for modeling classrooms in a school building
- Quantify capability of a school building to provide energy flexibility for a period of time when needed by the grid
- **Understand a method for conducting peak load and energy use analyses for a heat-wave using Building Energy Modeling.**
- **Discern the advantages and disadvantages of using detailed Building Energy Models for heat wave analyses.**
- Describe the requirements and potential approaches to modeling large populations of buildings to investigate coordination of grid flexible loads.
- Describe the possible causes leading to systematic errors in the prediction of aggregate grid loads

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Acknowledgements

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Thanks for support from my wife Marina. Soli Deo Gloria et Christi.

Outline/Agenda

Introduction

Methods and Data Input

Results and Discussion

Conclusions

Introduction

Background

- **Heat waves** are a prolonged period of abnormally hot weather that cause:
 - Heat related deaths or hospitalization
 - Abnormally high demand on the electrical grid via elevated Air Conditioning (AC) loads
 - AC is the dominant source of increased electricity demand during a heat wave (Choobineh et. al., 2019).
 - Degradation of efficiency for power generation
 - Solar Photo-voltaic efficiency degrades,
 - Line losses increase
 - Heat rejection at thermal plants is less efficient
 - Power outages
 - Directly – equipment failure
 - Indirectly – High temperatures and dryness leads to a fire that damages infrastructure
 - Crop failure
- Global warming is increasing magnitude, duration, and frequency of heat waves (Perkins, 2015; Horton et. al., 2016; IPCC, 2014)
 - Urban environments can expect +14°C (25°F) peak waves from normal average (Santamouris, 2020)



<https://www.pinterest.com/pin/155303887119794294/>

AC/Global Warming/Heat Wave Hazard Causal Loop

In urban environments, heat rejection from AC systems can give positive feedback that elevates external ambient temperatures even further (Viguié et. al., 2020).

HVAC coolant leaks and increased fossil fuel- based power increases green house gasses (GHG)

Increased GHG drives Global warming



Public Domain

Positive feedback between increasing AC use and heat waves calls for a need for clean energy and energy efficient systems

HVAC heat rejection and heat absorbing surfaces creates urban heat island

More HVAC installed to keep population cool

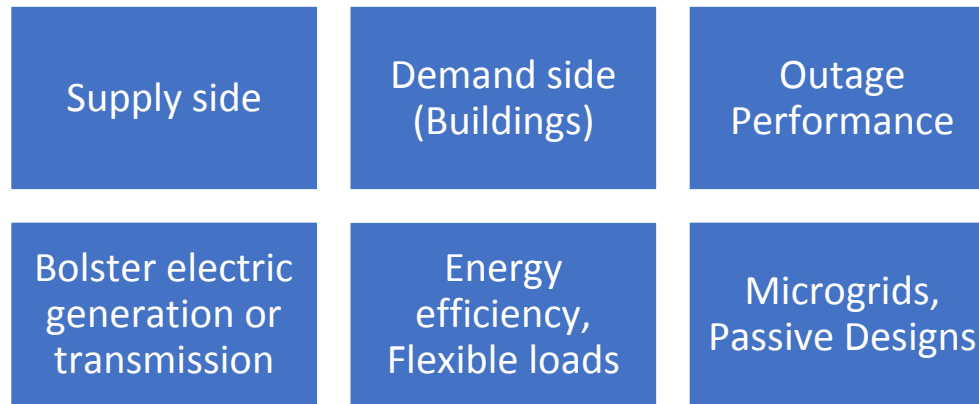
Un-conditioned spaces are more likely to be hazardous during heat waves



Figure obtained from ASHRAE Kansas City 2019 presentation background

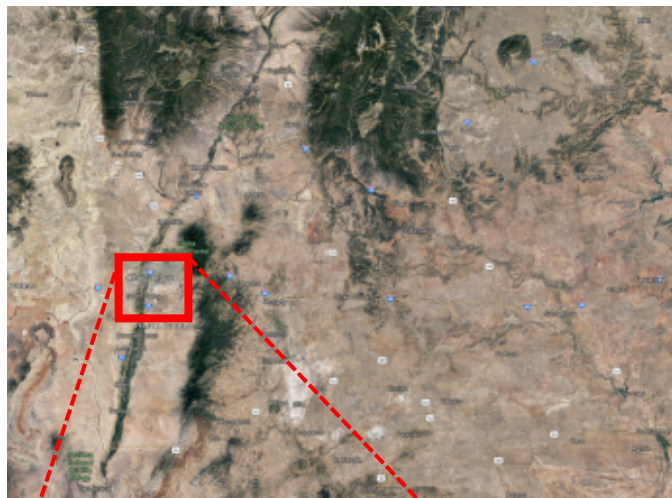
Resilience to Heat Waves

- Resilience to heat wave events can be enhanced by several approaches:

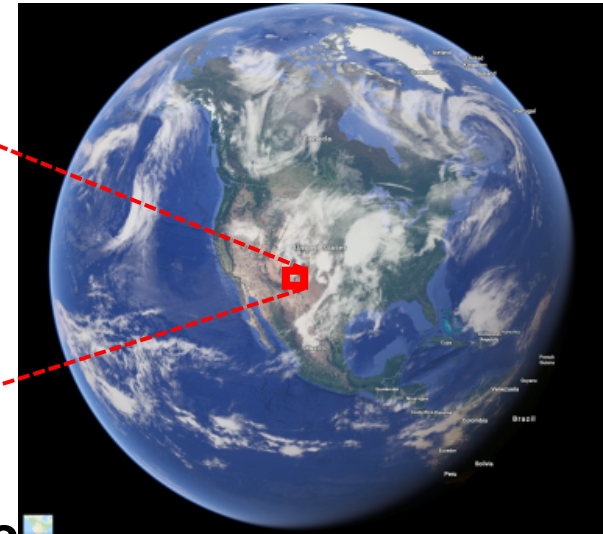


- Resilience is costly and not always positively correlated to energy efficiency (Sun et. al, 2020)
- The focus here is a necessary step toward any of these approaches: **Quantify heat waves effects on power demand from the built environment**

Scales for resilience analyses



Regional scale

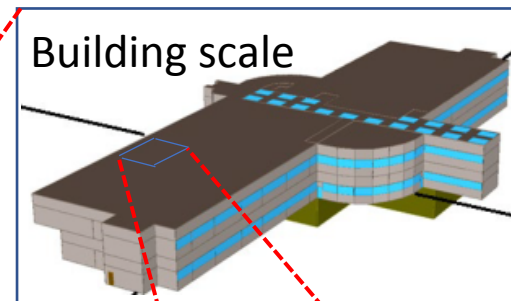
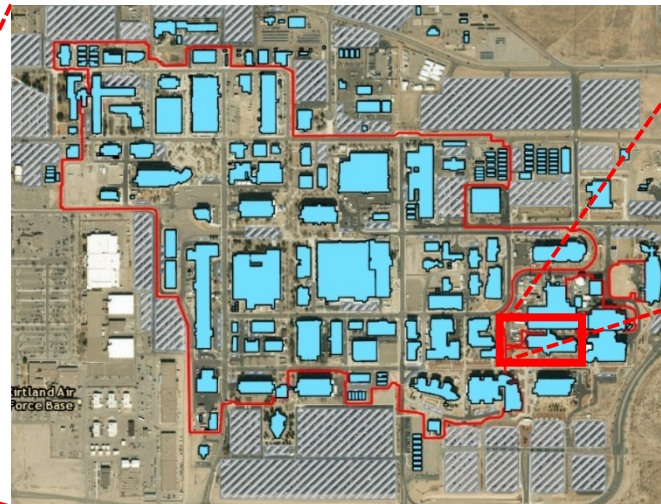


Global scale



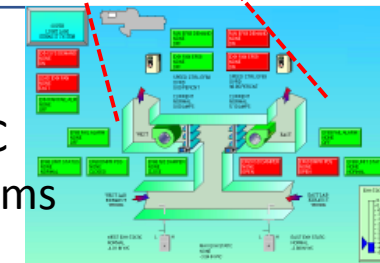
Urban scale

Institutional scale



Building scale

HVAC
Systems
Scale



Institutional Heat Wave Analyses

Large institutions often have buildings that support critical operations for which interruption due to a heat wave could cause:

- Economic losses
- Infrastructure downtimes for large populations
- Loss of one-of-a-kind assets that are irreplaceable
- Loss of critical or confidential information
- Damage to the environment
- Injury or death for personnel

Assuring these operations are resilient to heat waves is import to avoid such consequences

NM SNL Heat wave study

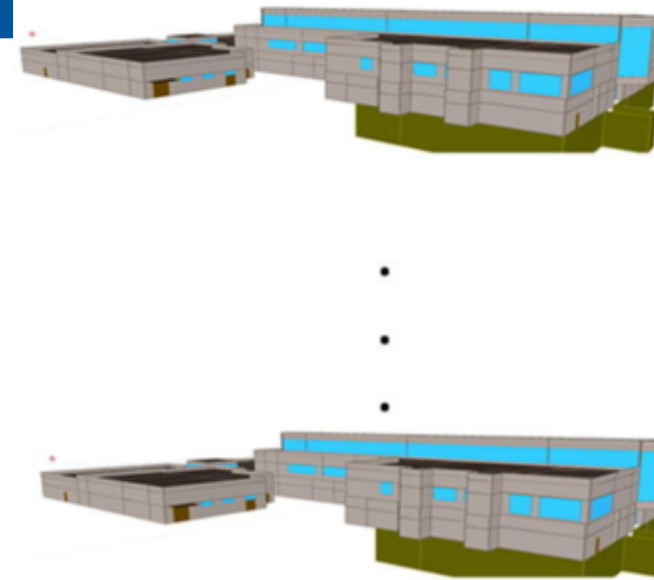
The New Mexico (NM) site heat wave study was conducted rapidly with no need for calibration of any of the individual 97 BEM used.

The NM study has been published in *Energy and Buildings* (Villa, 2021)

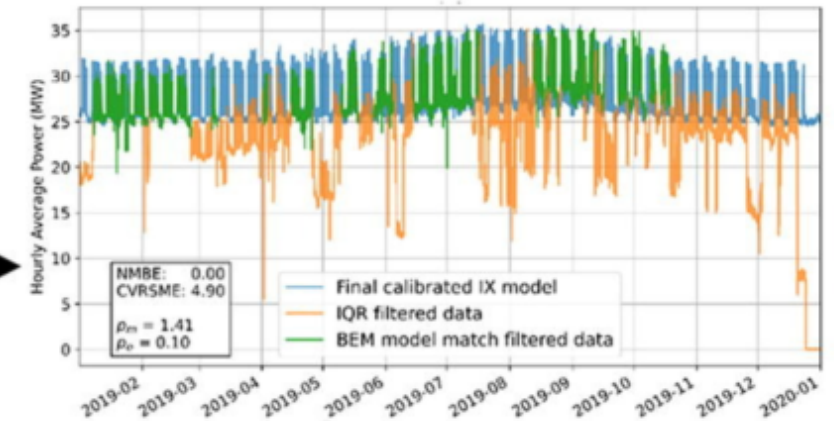
The California (CA) site study is the focus of this presentation. **It ended up being much more difficult even though it only involved 23 buildings**

Both studies' objective was to quantify the effect on peak electric load due to heat waves at their respective sites

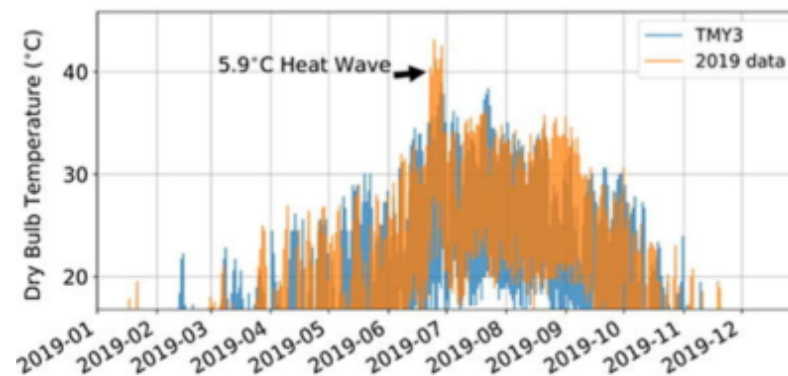
97 Building Energy Models



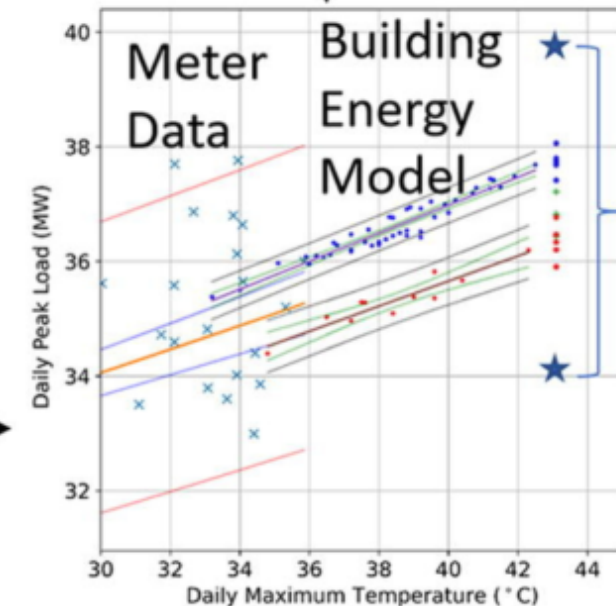
Site-wide calibration to meters



Local weather + NEX-DCP30



Parameterized Heat wave



Institutional heat wave analysis

Methods and Data Input

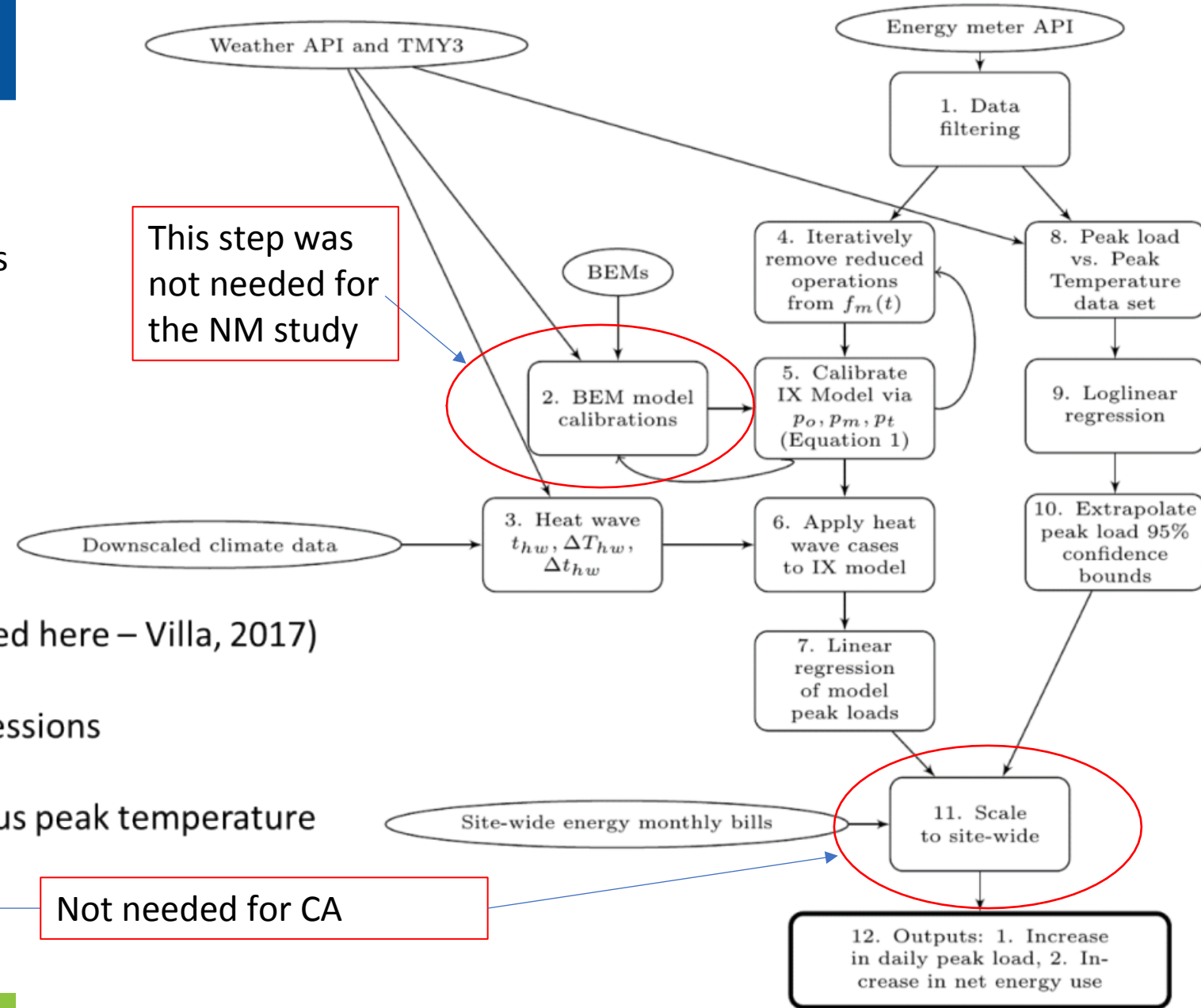
Methods

Data input:

- 1) Energy meter data for the most recent year.
- 2) Weather data for BEM
- 3) Downscaled climate model future temperatures
- 4) Monthly institution-wide energy use bills

Procedure:

- 1) Filtering meter data
- 2) Calibration of individual BEM models
- 3) Deriving the heat wave parameters
 t_{hw} , T_{hw} , Δt_{hw} .
- 4) Removing non-applicable time steps
- 5) Calibrating the aggregate model (IX = model used here – Villa, 2017)
- 6) Performing heat wave cases.
- 7) Calculating model output peak load linear regressions
- 8) Curating data-driven peak-load dataset
- 9) Create a log-linear regression of peak load versus peak temperature
- 10) Extrapolation of the data driven regression
- 11) Scale the meter results to site-wide results.
- 12) Compare data and model driven predictions



Calibration function

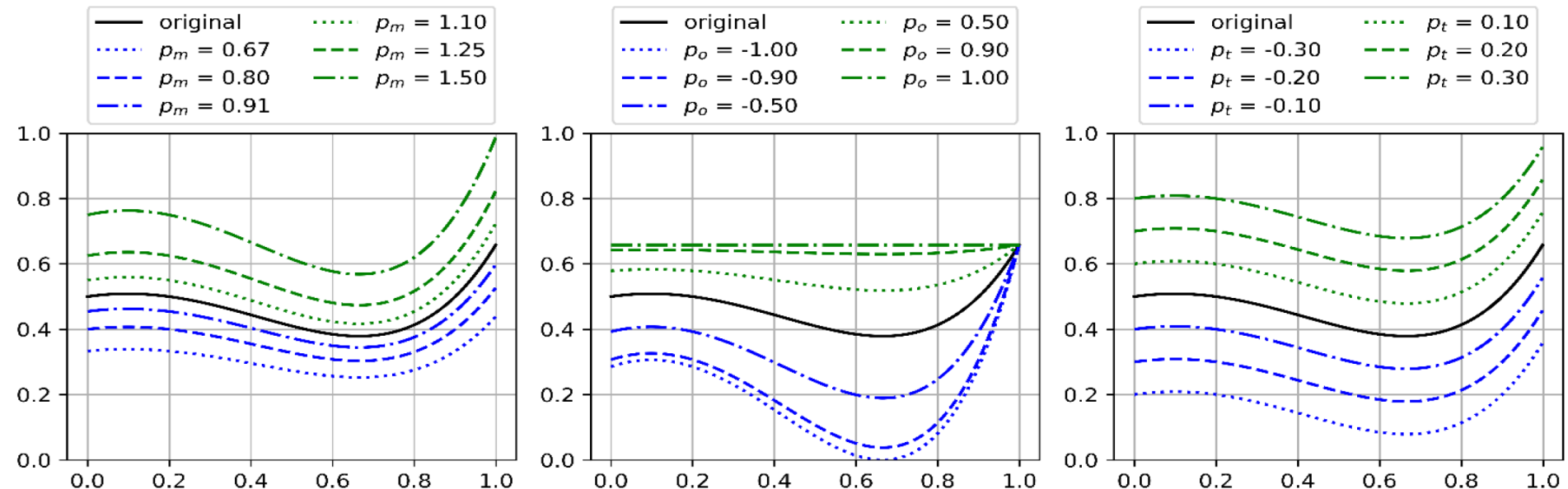
A scaling function is applied to the institution-wide power signal (Step 5)

$$f_{new}(t, p_o, p_m, p_t) = \begin{cases} p_m[(1 - p_o)f(t) + f_{max}p_o] + p_t & 1 \geq p_o \geq 0 \\ p_m[-p_o f_{new-1}(t) + (p_o + 1)f(t)] + p_t & -1 \leq p_o < 0 \end{cases}$$

$$f_{new-1}(t) = \frac{f_{max}}{f_{max} - f_{min}} f(t) - \frac{f_{max}f_{min}}{f_{max} - f_{min}}$$

The calibration function provides scaling (p_m), stretching (p_o), and translation (p_t)

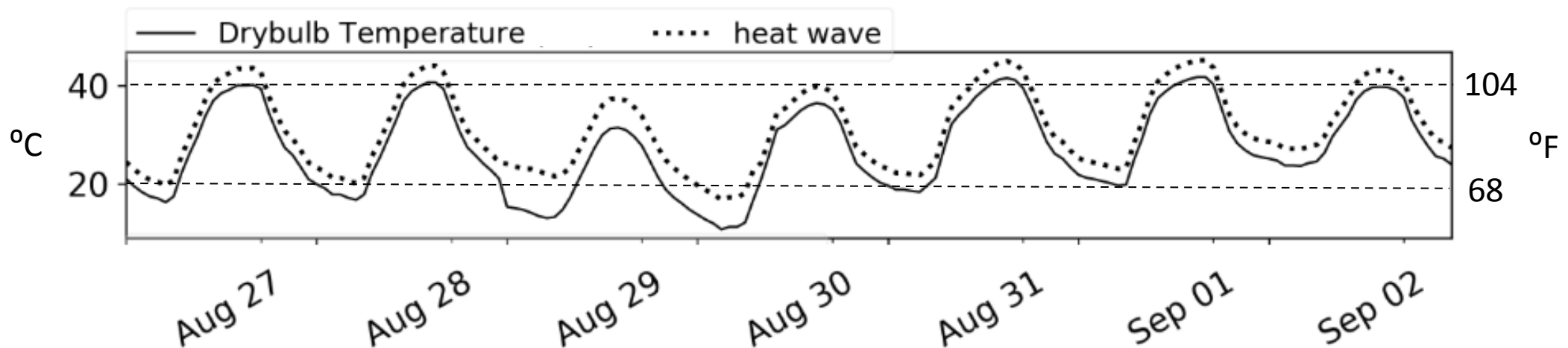
Only p_m and p_o were needed for the NM study



example function used to illustrate parameter effects: $f(t) = t(t + 1)(t - 0.9)(t - 0.2) + 0.5$

Data Input

- Weather data came from the Lawrence Livermore National Laboratory (LLNL) (LLNL, 2020) directly adjacent to the SNL CA site.
 - Missing Total horizontal solar radiation, cloud type, and cloud were filled in with Typical Meteorological Year 3 (TMY3) (Wilcox and Marion, 2008).
- Meter data came from the SNL energy analytics database through a Python API.
 - Verified to be 0.32% variation between the yearly sum of energy between 2019 monthly bills and the 15 min meter data.
- The heat wave scenario from NEX-DCP30 model results (Thrasher et. al., 2013).
 - $\Delta T_{hw} = 3.4^{\circ}\text{C}$ (6.1°F), $t_{hw} = \text{August } 27^{\text{th}}$, $\Delta t_{hw} = 7$ days
 - Unlike the NM case, the 2.0°C (3.6°F) volatility was not used due to lack of information about CA concerning increased volatility.
 - The resulting scenario peak temperature of 45.1°C did not even break the current record high of 46.1°C , yet is still representative of future heat waves according to NEX-DCP30 model results.



Results

Individual model calibration results –Much more work for CA vs NM!

| | NMBE (%) | | CVRSME (%) | | Data Mean Power | | Model Mean Power | | | |
|----------------------------|------------|--------------|------------|--------------|-----------------|-----------|--------------------|--------------------------|-------|-----------|
| | Calibrated | Uncalibrated | Calibrated | Uncalibrated | (kW) | (kBTU/h) | Calibrated (kW) | UnCalibrated (kBTU/h) | (kW) | (kBTU/h) |
| 1 | -3414 | -5209 | 4.228E+04 | 4.26E+04 | 1.013 | 3.458 | 35.6 | 121.5 | 53.79 | 121.5 |
| 2 | -5.5 | 11.41 | 206.7 | 206.7 | 225.3 | 768.8 | 237.7 | 811 | 199.6 | 811 |
| 3 | 92.86 | 87.31 | 101.9 | 97.15 | 193.4 | 659.9 | 13.83 | 47.17 | 24.56 | 47.17 |
| 4* | 8.967 | 17.57 | 11.05 | 21.1 | 488.4 | 1667 | 444.6 | 1517 | 402.6 | 1517 |
| 5* | -0.7239 | 37.61 | 23.05 | 45.59 | 37.98 | 129.6 | 38.25 | 130.5 | 23.7 | 130.5 |
| 6 | -474 | -178.6 | 476.9 | 226.6 | 102.7 | 350.3 | 589.3 | 2011 | 286.1 | 2011 |
| 7* | 0.6584 | 51.78 | 7.819 | 56.5 | 593.2 | 2024 | 589.3 | 2011 | 286.1 | 2011 |
| 8* | 0.6287 | -8.661 | 17.98 | 81.37 | 101.6 | 346.7 | 101 | 344.5 | 110.4 | 344.5 |
| 9* | 0.4323 | -3.088 | 25.85 | 35.3 | 420.1 | 1433 | 418.3 | 1427 | 433.1 | 1427 |
| 10 | -191.6 | -260.1 | 198.1 | 282.5 | 106 | 361.7 | 309.1 | 1055 | 381.7 | 1055 |
| 11 | -44.67 | -78.66 | 69.07 | 105.9 | 213.7 | 729.1 | 309.1 | 1055 | 381.7 | 1055 |
| 12* | -0.2531 | -49.1 | 23.21 | 99.81 | 21.09 | 71.96 | 21.14 | 72.14 | 31.44 | 72.14 |
| 13 | -18.89 | 31.5 | 42.31 | 49.83 | 31.95 | 109 | 37.98 | 129.6 | 21.89 | 129.6 |
| 14 | -90.59 | -93.12 | 147.9 | 190.1 | 15.07 | 51.42 | 28.72 | 98 | 29.1 | 98 |
| 15 | -98.79 | -192.5 | 163 | 310.9 | 16.69 | 56.96 | 33.19 | 113.2 | 48.82 | 113.2 |
| 16 | -116.7 | -120.6 | 170.5 | 162.3 | 70.1 | 239.2 | 151.9 | 518.3 | 154.6 | 518.3 |
| 17 | -42.3 | -41.2 | 51.58 | 111.2 | 118 | 402.6 | 167.9 | 572.8 | 166.6 | 572.8 |
| 18 | 0.1673 | 77.76 | 57.42 | 97.75 | 129.7 | 442.5 | 129.5 | 441.8 | 28.86 | 441.8 |
| 19 | 24.57 | 24.57 | 61.26 | 61.26 | 32.91 | 112.3 | 24.82 | 84.69 | 24.82 | 84.69 |
| 20 | 27.77 | 27.77 | 48.57 | 48.57 | 14.73 | 50.25 | 10.64 | 36.3 | 10.64 | 36.3 |
| 21* | -1.07 | 47.08 | 14.6 | 58.97 | 36.19 | 123.5 | 36.58 | 124.8 | 19.15 | 124.8 |
| 22* | -1.371 | -43.79 | 18.49 | 60.07 | 110.1 | 375.7 | 111.6 | 380.9 | 158.3 | 380.9 |
| 23* | -2.128 | 31.99 | 27.39 | 47.27 | 90.29 | 308.1 | 92.22 | 314.7 | 61.42 | 314.7 |
| Unscaled total | 27.38 | 35.9 | 27.91 | 40.4 | | | 3059 | 1.044E+04 | 2700 | 9214 |
| Scaled total all data | 2.563E-08 | 3.006E-07 | 5.242 | 7.202 | 4213 | 1.437E+04 | 4213 | 1.437E+04 | 4213 | 1.437E+04 |
| Scaled total filtered data | 4.418E-08 | 1.469E-08 | 5.121 | 6.74 | 4213 | 1.437E+04 | 4231 | 1.444E+04 | 4236 | 1.445E+04 |

* BEM that were G-14 compliant (NMBE < 10, CVRSME < 30) after calibration.

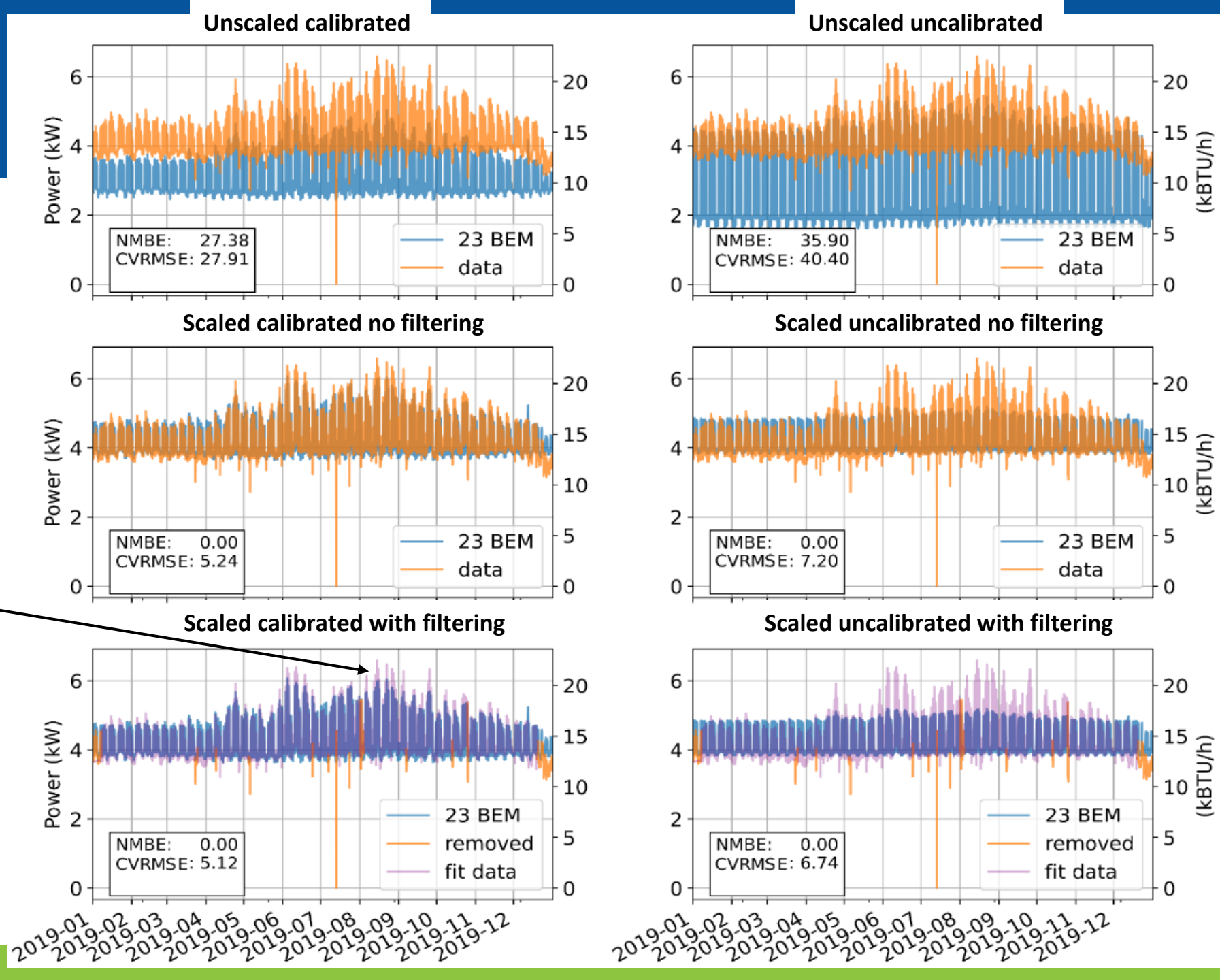
Data Curation

Effects of:

- 1) Scaling,
- 2) Individual BEM model calibration,
- 3) Data filtering

Peak loads model still could use improvement even though NMBE, CVRMSE greatly exceed ASHRAE Guideline 14 requirements!

NMBE = Normalized Mean Bias Error
CVRMSE = Coefficient for Root Mean Square Error (ASHRAE, 2014)



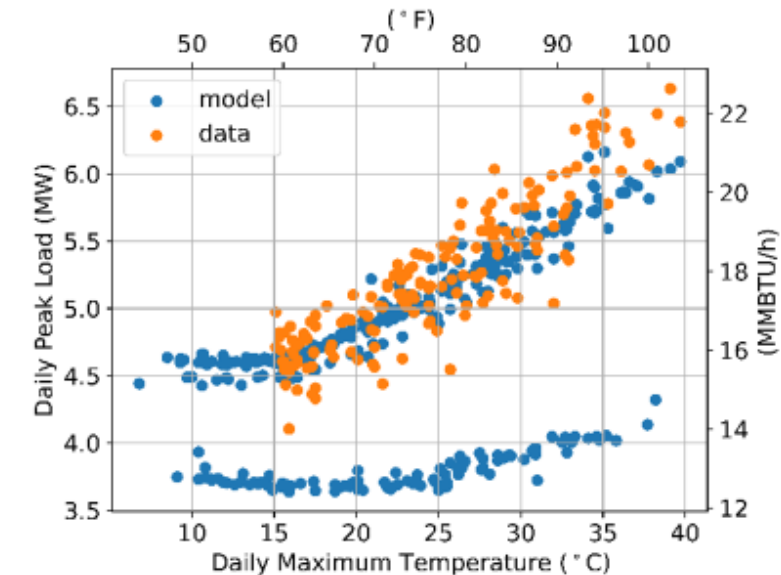
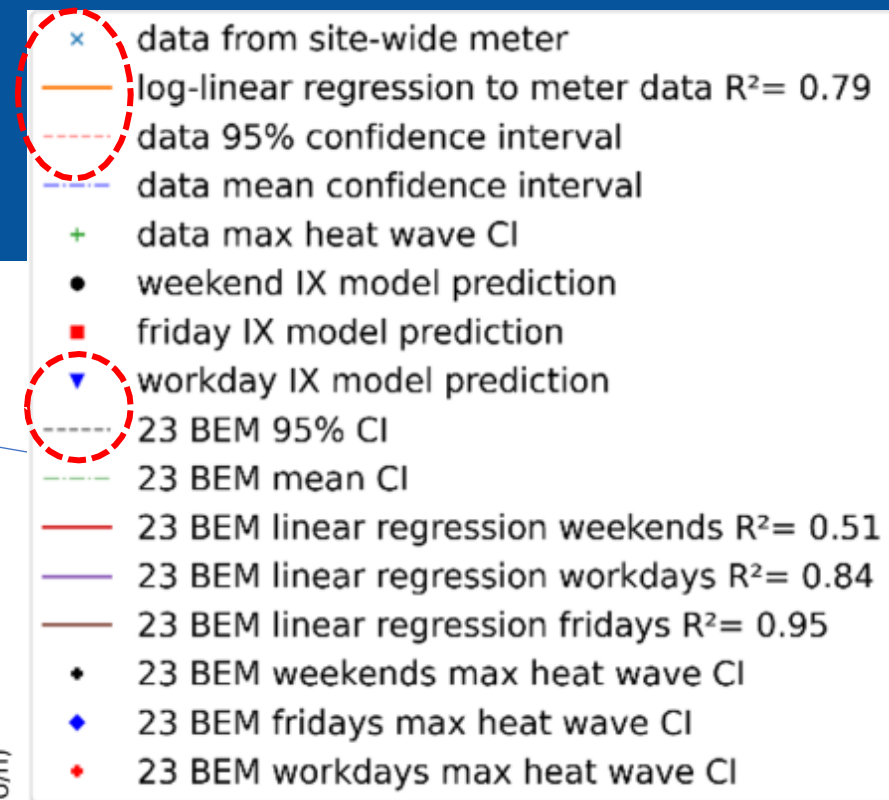
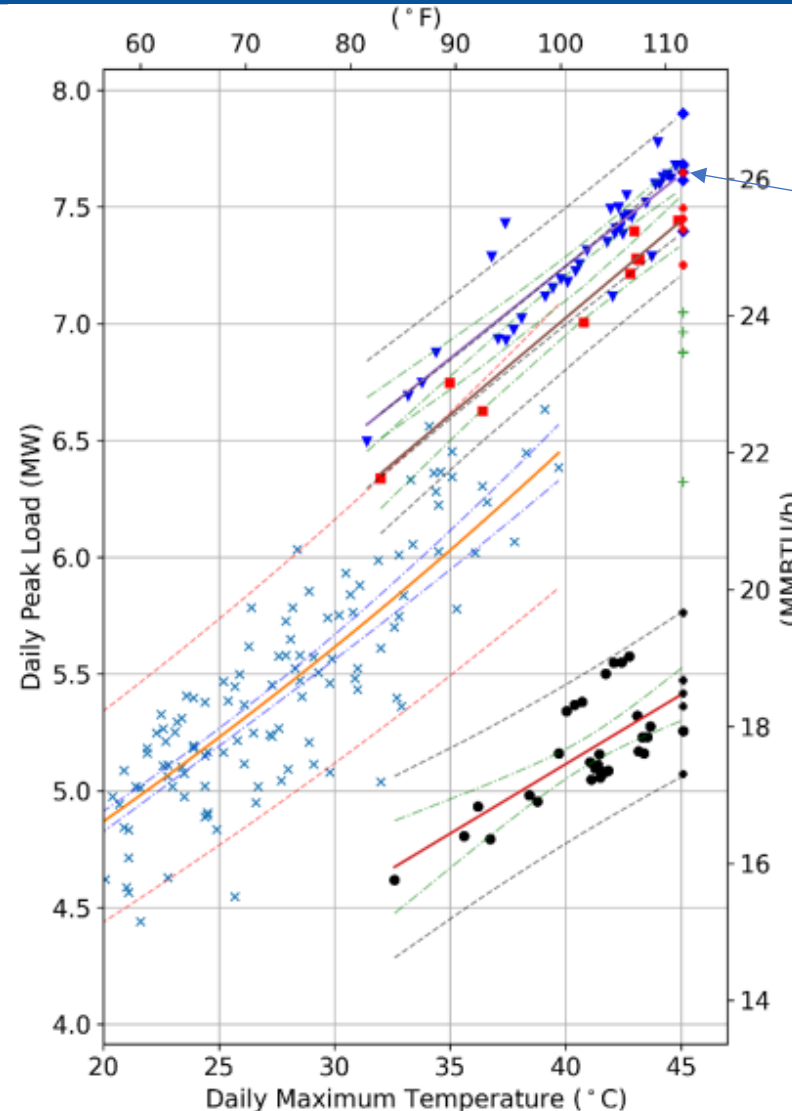
Peak Load Regressions

Even after the manual BEM calibrations the results between data and 23 BEM were not as well aligned.

The right-hand figure shows the 2019 weather data calibration

The left hand shows the model projection based on the heat wave which has been linearly scaled in 10 steps from normal weather to the heat wave shown on slide 15

Note: Confidence intervals help estimate uncertainty but give no information about probability of the occurrence of a given peak load!



Peak Load Regression Results

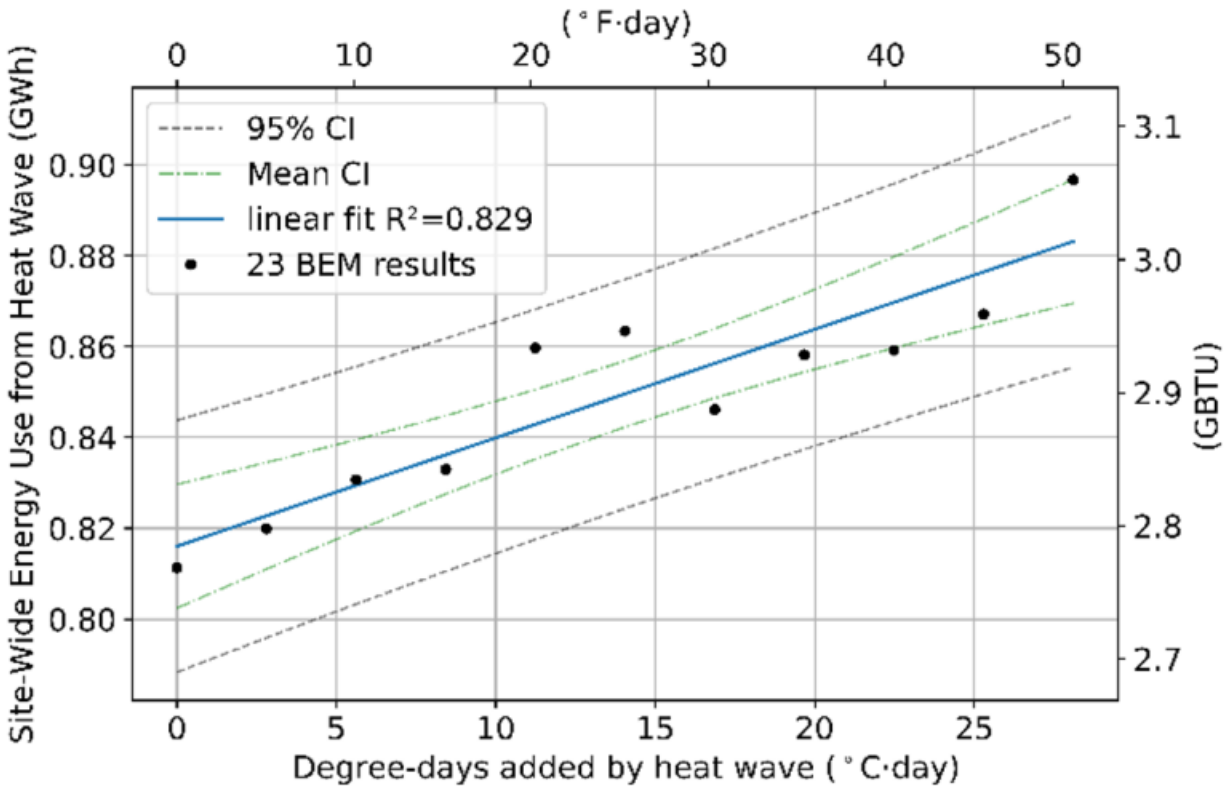
| Description | Data (workdays) | | Workdays | | Fridays | | Weekends | |
|---|-----------------|-----------|----------|---------|---------|---------|----------|---------|
| | SI | English | SI | English | SI | English | SI | English |
| 43.1°C mean predicted peak (MW/MMBTU) | 6.962 | 23.76 | 7.647 | 26.09 | 7.448 | 25.42 | 5.417 | 18.48 |
| — +95% CI | 7.669 | 26.17 | 7.899 | 26.95 | 7.647 | 26.09 | 5.762 | 19.66 |
| — +50% CI | 7.049 | 24.05 | 7.68 | 26.2 | 7.494 | 25.57 | 5.473 | 18.67 |
| — -50% CI | 6.877 | 23.47 | 7.614 | 25.98 | 7.403 | 25.26 | 5.361 | 18.29 |
| — -95% CI | 6.321 | 21.57 | 7.395 | 25.23 | 7.25 | 24.74 | 5.072 | 17.31 |
| 37.2°C mean predicted peak (MW/MMBTU) | 6.633 | 22.63 | 7.379 | 25.18 | 7.165 | 24.45 | 5.215 | 17.79 |
| Heat wave to baseline % difference | 4.965 | | 3.631 | | 3.949 | | 3.879 | |
| Mean slope (MW/°C or 1/°C) (MMBTU/°F or 1/°F) | 0.01425* | 0.007918* | 0.07881 | 0.1494 | 0.08322 | 0.1578 | 0.0595 | 0.1128 |
| — +95% CI | 0.01539* | 0.00855* | 0.09057 | 0.1717 | 0.09958 | 0.1888 | 0.0823 | 0.156 |
| — -95% CI | 0.01312* | 0.007286* | 0.06706 | 0.1271 | 0.06687 | 0.1268 | 0.0823 | 0.156 |
| Intercept (MW or unitless) (MMBTU or unitless) | 8.205 | | 4.093 | 13.96 | 3.695 | 12.61 | 2.733 | 9.327 |
| — +95% intercept | 8.234 | | 4.572 | 15.6 | 4.355 | 14.86 | 3.668 | 12.51 |
| — -95% intercept | 8.177 | | 3.614 | 12.33 | 3.035 | 10.36 | 1.799 | 6.14 |
| R ² value | 0.7929 | | 0.837 | | 0.9539 | | 0.5051 | |
| Model to data sensitivity % difference | 0 | | -16.64 | | -11.97 | | -37.06 | |
| Mean normalized slope (%/°C or %/°F) | 1.46 | 0.8113 | 1.068 | 0.5934 | 1.161 | 0.6452 | 1.141 | 0.6339 |

* The data regression model was calculated as log-linear [$\ln(y/1 \text{ MW}) = ax + b$) or $\ln(y/1 \text{ MMBTU}) = ax + b$) where y is peak power in MW and x is daily maximum temperature. All others are for a linear model ($y = ax + b$).

Increased Energy Use

The analysis was also used to project increased energy use from a heat wave at the site given the heat-content of a heat wave

This information can be very helpful for variable rate price structures during peak demand



| Description | Mean | +95% CI | -95% CI |
|--------------------------------------|----------|----------|----------|
| Maximum heat wave 28.10°C·day (GWh) | 0.8832 | 0.9109 | 0.8554 |
| Maximum heat wave 50.59°F·day (GBTU) | 3.014 | 3.108 | 2.919 |
| Slope (GWh/°C·day) | 0.002389 | 0.003209 | 0.00157 |
| Slope (GBTU/°F·day) | 0.004529 | 0.006083 | 0.002976 |
| Intercept (GWh) | 0.816 | 0.8297 | 0.8024 |
| Intercept (GBTU) | 2.784 | 2.831 | 2.738 |

Conclusions

Conclusions

- The CA analysis has **higher sensitivity to heat waves** equal to 1.46 %/°C (0.81 %/ °F) but **less expected increase in heat wave severity** equal to 3.4°C (6.1°F) than the NM results of 0.61 %/°C (0.34 %/°F) and 5.9 °C (10.6°F) leading to maximum expected percent increases in peak load of 5.0% for CA and 3.6% for NM.
 - Both these sensitivities are on the low end of values reported in the literature (Santamouris, 2020)
 - This underscores the need for thoroughness in assessing both climate changes and sensitivity to those changes – one size does not fit all for these kinds of analysis!
- The difficulties in the CA analysis suggest that detailed BEM modeling is not always a good approach for heat wave assessments. Though the NM site analysis was easily conducted the models had been maintained more thoroughly (Villa, 2019). This CA analysis showed use of a low-order RC model would have been easier. The best approach to use depends on the purposes of the analysis.
- The reduction of the BEM and data to regression parameters with CI's provides a low-order method with uncertainty for incorporating heat waves into energy master planning analyses (Jeffers, 2020) that consider additional forcing events such as human-attacks, earthquakes, floods, draughts, and fires.

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Questions?

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