

1 Characterisation of nano-scale precipitates in BOR60 irradiated T91 steel using atom probe  
2 tomography

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16 Highlights

- 17 • T91 steel was irradiated in BOR60 reactor at five different temperature/dose  
18 conditions.

- 19 • The number density, volume fraction, size and composition of the early stage Mn,  
20 Ni, Si -rich clusters have been characterised by atom probe tomography.
- 21 • After irradiation, Ni, Mn, Si and P segregation to carbide/matrix interface has  
22 been observed.
- 23 • Fe clustering inside a carbide was observed after irradiation at 524 °C:15.4dpa,  
24 which has not been reported before.

25

## 26 Abstract

27 Atom probe tomography has characterised the microstructural changes in T91 steel  
28 after BOR60 reactor irradiation at five temperatures between 376 °C and 524 °C to  
29 doses between 14.6 dpa and 35.1 dpa. Irradiation-induced precipitation and  
30 segregation to carbide/matrix interface induced by neutron irradiation has been  
31 characterised. Atom probe tomography characterisation shows that Mn, Ni, Si -rich  
32 (MNS-rich) clusters form in T91 steel irradiated in BOR60 reactor at temperatures  
33 between 376 °C and 415 °C, which is not observed at higher temperatures 460 °C and  
34 524 °C. The number density, volume fraction and composition of MNS-rich clusters  
35 have been characterised. Ni, Mn, Si and P is found to segregate at carbide matrix  
36 interface after irradiation at lower temperature and only P segregation is observed at  
37 524 °C.

**Keywords:** T91 steel, BOR60 reactor, MNS-rich clusters, atom probe tomography

## 1 Introduction

One of the key factors for safe operation of current reactors and implementation of advanced nuclear energy systems is the long term stability of structural components exposed to a combination of both high temperature and high neutron flux [1]. To this end, ferritic/martensitic (F/M) steels are appealing structural materials for high dose structural components because of their outstanding resistance to radiation-induced swelling, high thermal conductivities and low thermal expansion coefficients [2–4].

Among various commercial F/M steels, T91, a modified 9Cr-1Mo steel has found a rising number of applications as a structural material for fission reactors in recent years. However, prolonged exposure to neutron irradiation drives microstructural evolution in T91 steel, which has detrimental effects on the mechanical properties. For example, irradiation can alter the distribution and composition of the pre-existing carbide/nitrides. In their tempered state, the main precipitates in F/M steels are carbides and/or nitrides [5–7]. The pre-existing carbides and nitrides contribute to strengthen the material and are expected to be stable under service conditions. However, research has shown that modification of structure, density, size and composition of pre-existing precipitates can occur when exposed to irradiation [8–10].  $M_{23}C_6$  was previously shown to increase in size and grain boundary coverage in an

58 11Cr F/M steel after neutron irradiation at temperatures between 500 °C - 650 °C [10].  
59 Amorphization of  $M_{23}C_6$  carbides has been observed in various F/M steels exposed to  
60 neutron irradiation [5,11]. The composition of the carbides can also be altered by  
61 irradiation [12]. In T91 steel, when the ion irradiation dose increased from 1 dpa to 10  
62 dpa, the carbide size first slightly increased and then decreased [13]. Radiation  
63 induced segregation (RIS) of solutes to grain boundaries has been observed in F/M  
64 steels. Jiao et al. [14] using scanning transmission electron microscopy (STEM)  
65 studied RIS in a set of T91 steel samples subject to a range of irradiation conditions in  
66 the BOR60 fast research reactor. Their analyses showed a temperature dependence of  
67 RIS magnitude.

68

69 In addition to the modification of pre-existing carbide/nitride precipitates and RIS, the  
70 local solute concentration in the vicinity of a defect sink can reach the solubility limit,  
71 leading to radiation-induced precipitation. In T91, Mn, Ni, Si -rich (MNS-rich)  
72 clusters are known to form under irradiation, leading to embrittlement [9,14–24].  
73 Various studies on MNS-rich clustering specific to T91 have been carried out using a  
74 variety of characterisation techniques to investigate a range of irradiation conditions.  
75 Table 1 summarises results in the literature from previous studies measuring number  
76 density, volume fraction and averaged diameter of MNS-rich precipitates resulting  
77 from different irradiation experiments. In addition to investigating RIS, in the same

BOR 60 irradiated T91 samples Jiao et al. [14] used TEM to measure the number density of MNS-rich precipitates to be in the order of  $10^{21} \text{ m}^{-3}$ . T91 samples proton irradiated to 7 dpa at 400 - 500 °C ([25]) have also been shown to produce MNS-rich precipitates and copper-rich precipitates (CRPs). The absence of MNS-rich precipitates under a lower proton irradiation dose in the same study suggests that the cluster formation is enhanced by irradiation. Analysis of neutron irradiated T91 by several methods suggests an increase in diameter as temperature and dose are increased.

Table 1 Summary of MNS-rich precipitates analysis in T91 from literature.  $d$  = averaged diameter,  $f$  = volume fraction and  $N$  = number density.

Study:	Technique	Irradiation	Conditions	$d$ (nm)	$f$ (%)	$N$ ( $\text{m}^{-3}$ )
Jiao [14]	TEM	BOR60-neutron	17.1dpa,376°C	5.8	0.037	$3.6 \times 10^{21}$
			35.1dpa,378°C	7.0	0.043	$2.4 \times 10^{21}$
			18.6dpa,415°C	6.7	0.047	$3.0 \times 10^{21}$
Jiao [12]	TEM	Proton-2MeV	7dpa, 400°C	4.4	/	$1.27 \times 10^{23}$
			7dpa,500°C	8.0	/	$0.14 \times 10^{23}$
Pareige [26]	APT	Self-ion irradiated	0.5dpa, 300°C	3.0	/	$2.8 \times 10^{23}$
			0.5dpa, 420°C	3.8	/	$0.52 \times 10^{23}$
Kuksenko [27]	APT	MTR-neutron	0.6dpa, 300°C	3.2	/	$2.4 \times 10^{23}$
Wharry [25]	APT	Proton-2MeV	7dpa, 400°C	4.1	/	$7.4 \times 10^{22}$

From the literature, behaviour of MNS-rich precipitates in T91 under both neutron and ion irradiation is inconclusive. In particular, the compositional analysis of MNS

-precipitates is lacking. To further understand and determine the suitability of T91 for generation IV reactors, compositional analysis on the nanoscale and a correlative view of how this affects materials properties is required. An integrated research project (IRP) has been initiated between different universities and research institutes in US and UK. A fuller description of this project can be found in [28]. One of the main goals of the program was to understand the microstructural evolution of T91 steel under reactor irradiation. The main aim of the present study is to better understand the nano-scale MNS-rich cluster formation at different temperatures and doses and provide compositional data of the irradiated microstructure. As such, atom probe tomography (APT) analyses were carried out to study the microstructure of T91 steel subjected to BOR60 reactor irradiation. The MNS-rich cluster formation, carbide/nitride compositions and solute segregation on the carbide/matrix interface have been examined. The temperature dependence of cluster formation and solute segregation have been characterised and the results are compared with the STEM results from Jiao et al. [14] and previous data from the literature.

## 2 Materials and Experimental Methods

All APT analyses were carried out on a Cameca LEAP 5000 XR instrument. Voltage pulsing mode with a 20 % pulse fraction was utilised for the atom probe experiments. The specimen temperature and pulse repetition rate were set to 50 - 55 K and 200 kHz,

respectively. CAMECA IVAS software was used to reconstruct the detected information into 3D positions and chemical identity of each ion.

T91 steel used in this study was received from Pacific Northwest National Laboratory (PNNL). As-received T91 steel sample for APT analyses were prepared from 3 mm TEM disks after diamond lapping to 0.25  $\mu\text{m}$  at the University of Michigan. The composition of as-received T91 measured by APT and chemical composition provided by PNNL are both listed in Table 2. Compared to the bulk chemistry, the Cr and V contents are lower in APT measurements. The loss of Cr and V is about 1.25 at. % and 0.09 at. % respectively. Also, the majority of the expected Nb, C and N atoms were not detected in the APT analysed regions. The loss of these elements in the composition measurement is most likely due to the formation of nitrides and carbides outside the analysed region. From previous studies, Cr-rich carbide ( $\sim 100$  nm) were present along prior austenite grain boundaries (PAGBs) and lath boundaries. The finer V, Cr- rich nitrides ( $\sim 40$  nm) were both in the matrix and adjacent to the carbides [12]. Due to the small analysed volumes by APT, such large carbides/nitride were not captured in any of the as-received T91 data. Hence, it is not surprising that contents of carbide/nitride formers obtained via APT are lower.

Table 2 Composition of T91 from APT and bulk composition provided by PNNL. The error in APT composition is obtained by averaging data from three different analysed specimens.

	Alloy Chemistry (at. %)									
	Cr	Ni	C	N	Mn	Mo	Nb	Si	V	Fe
Bulk composition provided by PNNL	9.16	0.08	0.37	0.21	0.37	0.51	0.04	0.22	0.23	Bal.
Composition measured via APT	7.91	0.10	0.04	0.05	0.40	0.40	-	0.27	0.14	Bal.
Error ( $\pm$ )	0.05	0.02	0.01	0.05	0.04	0.04	-	0.05	0.06	-

The neutron irradiations were conducted in the BOR60 test reactor in Russia. Due to the radioactive nature of the resulting samples, lamellas were made using a lift-out process [29] for BOR60 irradiated T91 at the Low Activation Materials Development and Analysis (LAMDA) laboratory at Oak Ridge National Laboratory (ORNL). A dual beam microscope FEI Helios NanoLab 600i at Culham Centre for Fusion Energy (CCFE) was used to prepare BOR60 irradiated T91 for APT analysis. The unirradiated T91 specimen were also prepared using the FEI Helios Nano Lab 600i at CCFE. A detailed description of BOR60 irradiation conditions and methods for dose and temperature calculation can be found in Ref. [14]. The average irradiation temperatures and the accumulated irradiation doses at retrieval were calculated as 376 °C:17.1dpa (irradiation temperature: final irradiation dose), 378 °C:35.1dpa, 415 °C:18.6dpa, 460 °C:14.6dpa and 524 °C:15.4dpa. The dose rate was  $6 - 9 \times 10^{-7}$  dpa/s. The neutron damage profile is relatively flat. All the BOR60 irradiated samples were taken from a depth between 200 - 600 nm from the surface.



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145 In the reconstructed APT data, the identification and characterisation of Mn, Ni, Si  
146 -rich clusters was undertaken based on the maximum separation method [30,31]. In  
147 simple terms, the distance separating a solute atom (defined as Ni, Si and Mn in this  
148 case) from its  $K^{th}$  ( $10^{th}$  in this study) nearest solute neighbour is measured within the  
149 data. If this distance is less than a defined value,  $d_{max}$ , the two solute atoms are  
150 determined to be “core” of the same cluster. Any cluster containing less than a  
151 defined number of atoms,  $N_{min}$ , is removed from the analysis to remove contributions  
152 from very small clusters statistically likely to form from random fluctuations in the  
153 matrix. After solute clusters are defined, matrix atoms within a distance  $L$ , of the  
154 clustered solute atoms, are included in the cluster. This selection of atoms is then  
155 eroded back a distance of  $E$  (erosion parameter). The parameters chosen to define the  
156 maximum separation were  $d_{max} = 0.7$  nm,  $N_{min} = 20$  atoms,  $L = e = 0.5$  nm. The  
157 number density,  $N$ , of clusters identified within the reconstruction was calculated  
158 using the following formula:

$$N = \frac{n\eta}{N_{tot}\Omega} \quad (1)$$

159 where  $n$  is the total number of clusters and  $N_{tot}$  is total number of atoms in the  
160 analysed volume,  $\Omega$  is the volume of one solute atom, taken as  $1.094 \times 10^{-2}$  nm<sup>3</sup>,  
161 assuming the solutes have a similar atomic volume as Ni.  $\eta$  is the ion detection  
162 efficiency of the atom probe instrument, which has been estimated to be 0.52 for the

LEAP 5000 XR. The volume fraction of clusters is an important factor to estimate their influence on strength and hardness. The volume fraction,  $f$ , is estimated by:

$$f = \frac{\sum_{i=1}^n N_{sol}}{N_{tot}} \quad (2)$$

where  $N_{sol}$  is the total number of solute atoms incorporated within a cluster.

The radius,  $r$ , of a precipitate was equated to that of the volume equivalent sphere:

$$r = \sqrt[3]{\frac{3N_{sol}\Omega}{4\pi\eta}} \quad (3)$$

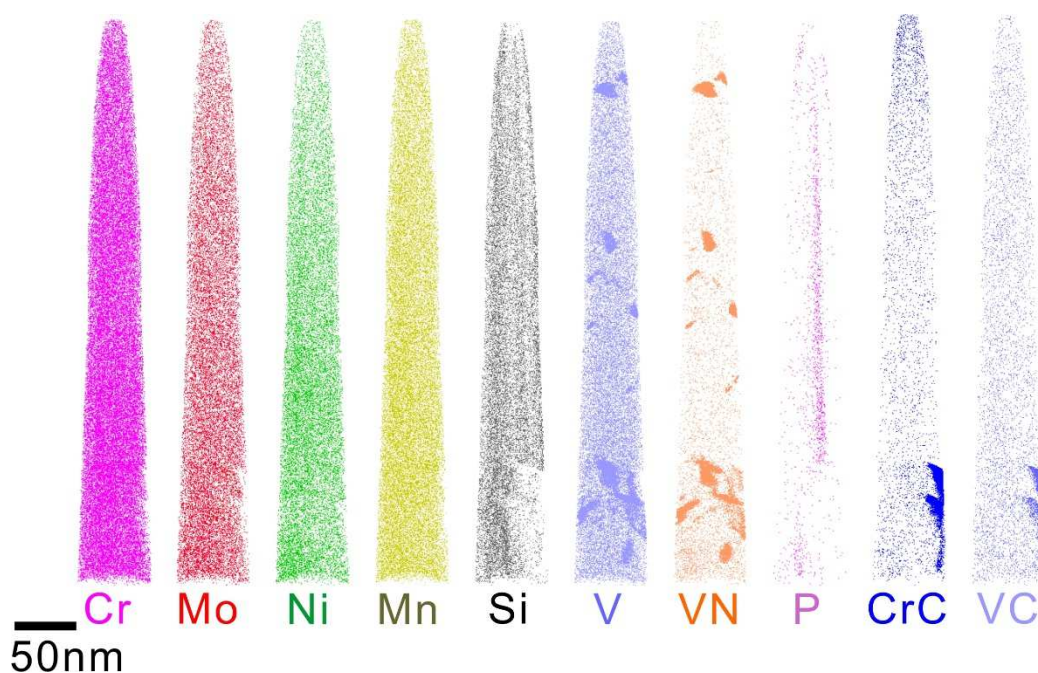
Excluding the matrix atoms could lead to under-estimation of the size and volume fraction. However, previous studies have provided evidence that the majority of Fe atoms in the clusters, as observed by APT, are due to trajectory aberrations [32]. Hence, the systematic method described above was used to estimate the volume fraction  $f$  and radius  $r$ .

### 3 Results

#### 3.1 As-received T91

Three tip-shaped specimens of as-received T91 steel were analysed. The obtained datasets included 33.0M, 7.2M and 17.1M ions, respectively. Atom maps of individual elements from Tip 1 are shown in Figure 1. Atom maps from Tip 2 and Tip 3 are included in the supplementary materials. Precipitates enriched with V, Cr and VN ions are observed in the as-received T91 samples. From compositional analysis

179 (included in the supplementary materials), the precipitates contain approximately 40  
 180 at. % V, 20 at. % Cr and 30 at. % N. CrC ions are also found at the bottom edge of the  
 181 tip.



182 50nm  
 183 Figure 1 Atom maps of individual elements, nitride and carbide ions in as-received  
 184 T91

### 185 3.2 Elemental distributions of T91 steel irradiated in BOR60

186 From each irradiation condition, 2 - 4 needles were analysed using APT. Datasets  
 187 including between 2.2M - 12.4M ions were analysed. Figure 2 (a) - (e) presents the  
 188 APT atom maps obtained from the analysis of T91 steel irradiated in BOR60 at the  
 189 different conditions. Compared to the unirradiated T91, the V-rich nitride particles  
 190 were not observed in any T91 specimen after irradiation. In all the specimen irradiated  
 191 at temperature ranges between 376 °C and 415 °C, distinct solute clusters containing

Ni, Mn, and Si were detected. However, such clusters were not observed when the temperature was raised to 460 °C and 524 °C, respectively. Cu and P was also found to cluster together with some of these MNS-rich clusters. As shown in Figure 1, this clustering was not present in the as-received T91.

Cr-rich carbide particles were also captured in some specimens, i.e. Figure 2 (a), (c) and (e). A range of behaviours were observed with respect to the incorporation of these carbides. Ni, Si, Mn and P was found to segregate to the carbide/matrix interface at 415 °C (Figure 2 (c)), whereas at the higher temperature of 524 °C, only P was found to segregate to the interface (Figure 2 (e)). Mn was found to be enriched inside the carbide at 524 °C. As shown in Figure 2 (e), Fe appeared to deplete at the interface and cluster inside the carbide. Clustering of Fe inside the carbide has not been well-documented. V-rich nitride particles were also observed inside the carbide. Except from the specimen containing carbides (i.e the one in Figure 2 (e)), solute elements were found to be randomly distributed after irradiation at higher temperatures (460 °C and 524 °C).

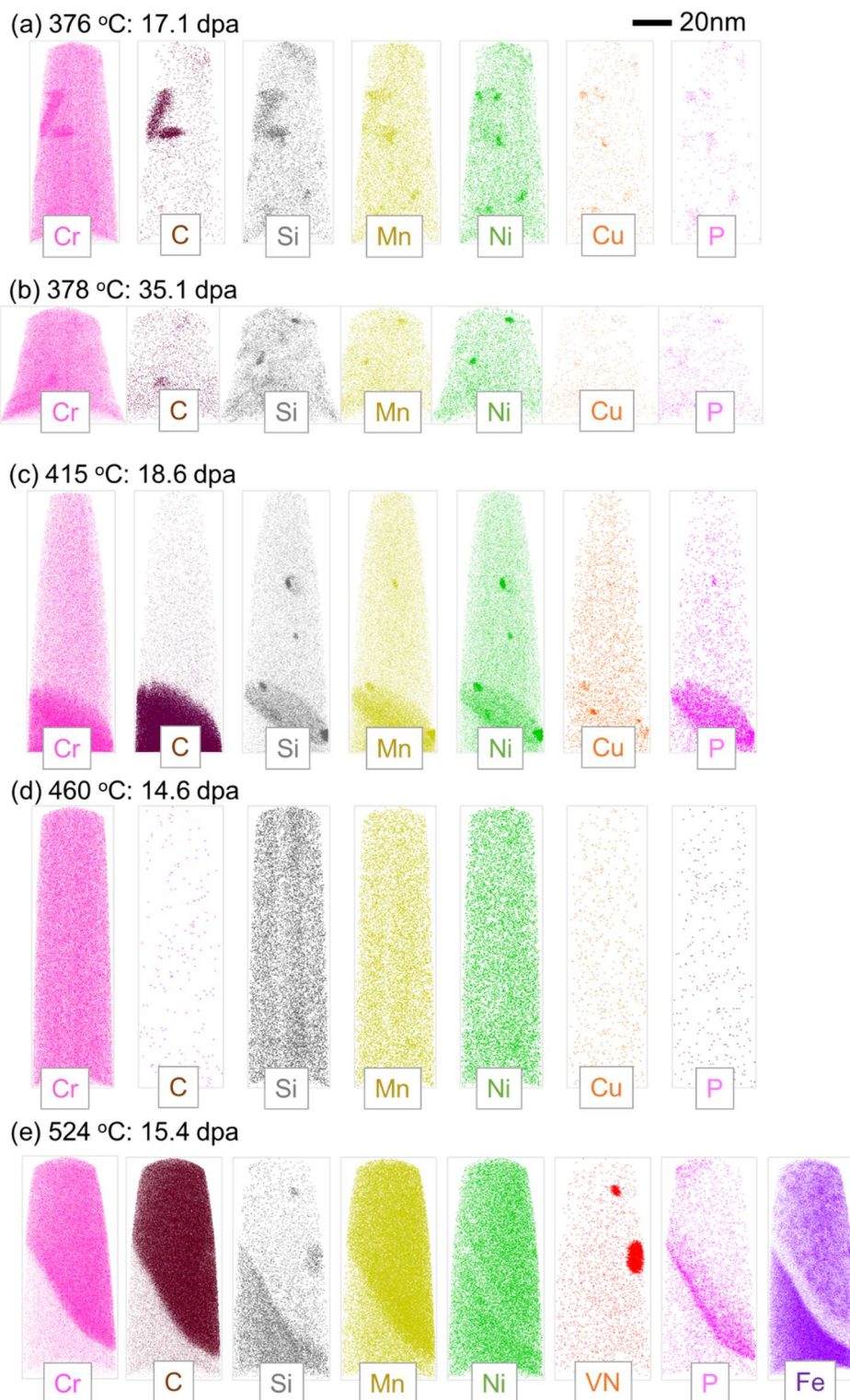


Figure 2 Atom maps of T91 steel irradiated in BOR60 (a) 376 °C:17.1dpa, (b) 378 °C:35.1dpa, (c) 415 °C:18.6dpa, (d) 460 °C:14.6dpa and (e) 524 °C:15.4dpa. Note that due to the mass-to-charge-state ratio overlap at 14 and 15 Da, which for the purposes of this figure have been assigned to be Si, the majority of the Si enrichment associated to the carbide and nitride are in fact misidentified N ions

3.3 Number density, volume fraction and composition of MNS-rich precipitates

The MNS-rich precipitates were analysed using methods described in Section 2. Table 3 presents the measured number density,  $N$ , volume fraction,  $f$ , and averaged diameter,  $d$ , of the clusters at different irradiation conditions. The error is obtained by averaging the results of the analyses across multiple APT reconstructions. It needs to be pointed out that there are still systematical errors caused by the selection of cluster analysis parameter. The same data analysis parameters were used to minimize the effect of cluster selection parameters when comparing between datasets. The measured number densities were all in the order of  $10^{23}/\text{m}^3$ . It should be noted that, due to the relatively small volumes of microstructure sample in each APT and the limited number of clusters observed that the uncertainty of the number density, volume fraction and diameter might be quite large. This is consistent with the observations from atom maps such that even at the same irradiation condition, the distributions of clusters vary significantly analysis to analysis. Hence, no clear trend with temperature and dose level can be ascertained when considering the relatively large error. When the irradiation temperature was higher than 460 °C, no clusters were identified using the same search algorithm applied to all the APT data.

Table 3 Number density ( $N$ ), volume fraction ( $f$ ) and diameter ( $d$ ) of MNS-rich precipitates. The error is obtained by averaging different specimen at the same irradiation condition.

Alloy	$N (\text{m}^{-3})$	$\pm$	$f (\%)$	$\pm$	$d (\text{nm})$	$\pm$
<b>376 °C:17.1dpa</b>	1.37E+23	4.66E+22	0.12	0.04	2.0	0.5
<b>378 °C:35.1dpa</b>	3.00E+23	4.34E+22	0.09	0.06	1.8	0.4
<b>415 °C:18.6dpa</b>	1.53E+23	6.05E+22	0.09	0.1	1.8	0.5
<b>460 °C:14.6dpa &amp;</b>	-	-	-	-	-	-

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**524 °C:15.4dpa**

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Table 4 lists the concentration of the main elements in MNS-rich clusters formed after BOR60 irradiation in T91. When the irradiation dose was increased from 376 °C:17.1 dpa to 378 °C:35.1 dpa, the Ni and Mn contents were very similar. However, the Si content in the clusters almost doubled, increasing from 6.9 at. % to 13.3 at. %. It has previously been reported that Si has the highest affinity for vacancies compared to Ni and Mn [33]. At higher doses, the number of defects is higher than that of lower dose level. Thus it is not surprising that the clusters at 378 °C:35.1dpa are more enriched in Si.

Table 4 The averaged concentration of the main elements in NMS-rich clusters. The uncertainty is the standard error of different clusters.

Alloy	Composition (at. %)						
	Ni	Si	Mn	Cu	Fe	Cr	P
<b>376 °C:17.1dpa</b>	11.9±4.5	6.9±4.8	8.0±2.4	0.6±0.4	61.1±9.5	8.0±3.2	0.4±0.4
<b>378 °C:35.1dpa</b>	11.8±5.5	13.3±5.9	8.1±2.8	0.2±0.4	56.6±8.5	8.6±5.1	0.3±0.5
<b>415 °C:18.6dpa</b>	12.4±5.3	11.1±6.3	7.4±2.7	0.2±0.4	59.4±9.2	8.7±3.8	0.3±0.5

### 3.4 Carbide composition

As shown in Figure 2 (c) and (e), large (several tens of nm) carbide particles were captured in the APT analyses of BOR60 irradiated T91. A close-up of elemental distributions and a 1D concentration profile across the matrix-particle interface in T91 irradiated at 415 °C:18.6dpa is shown in Figure 3. The carbide particle is enriched in Cr, Mo and C. The composition matches  $M_{23}C_6$  type carbide. Ni, Si, Mn and P is observed to segregate to the carbide/matrix interface. The peak concentration of Ni, Si and Mn is all around 2.5 at. % at the interface and P content is ~ 1 at. %.

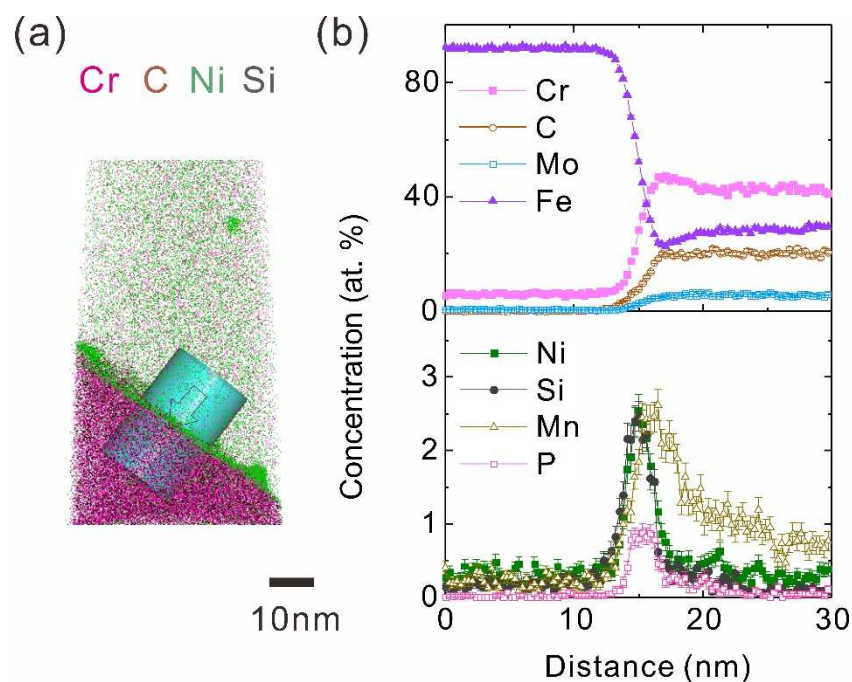


Figure 3 (a) Close-up of atom maps at the carbide/matrix interface in BOR60 irradiated T91 at 415 °C:18.6dpa. The analysed sample is the same as in Figure 2 (c); (b) 1 D concentration profile across the interface

When the irradiation temperature was raised to 524 °C, as shown in Figure 4, only P segregation was observed at the carbide/matrix interface. Instead of segregation at the interface, Mn was enriched by ~ 1 at. % inside the carbide and Si was rejected from it. Also, an Fe depleted zone was observed near the interface. Then Fe content increased again inside the carbide. This is due to the formation of small Fe-rich clusters inside the carbide particle. These Fe-rich clusters are highlighted using 40 at. % Fe isoconcentration surface in Figure 5 (a) and the concentration proxigram is displayed in Figure 5 (b). The clusters are 2 - 3 nm in radius and the Fe content in the core regions exceeds 80 at. %. The formation of Fe-rich clusters inside the carbide particles in this material has not been reported before.



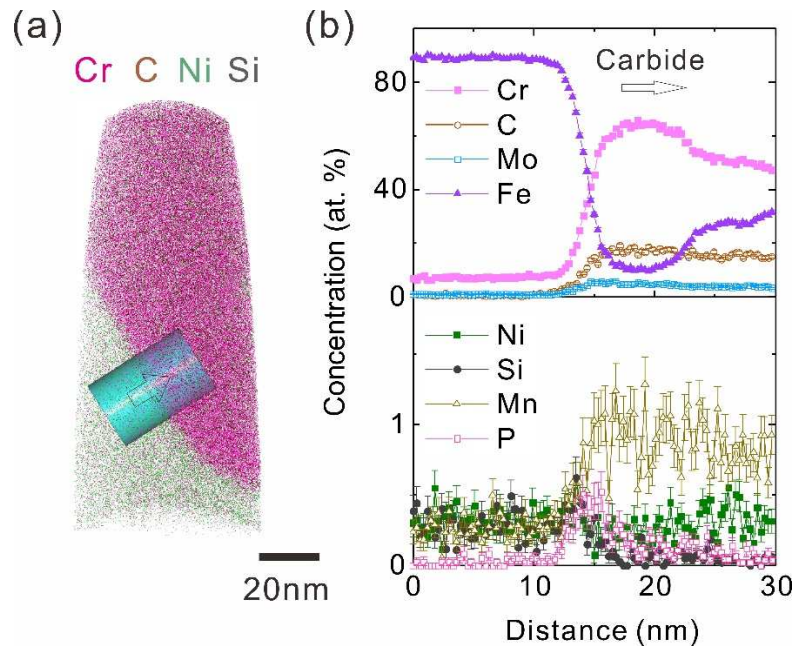


Figure 4 (a) Close-up of atom maps at the carbide/matrix interface in BOR60 irradiated T91 at 524 °C:15.4dpa. The analysed volume is the same as in Figure 2 (e); (b) 1 D concentration profile across the interface

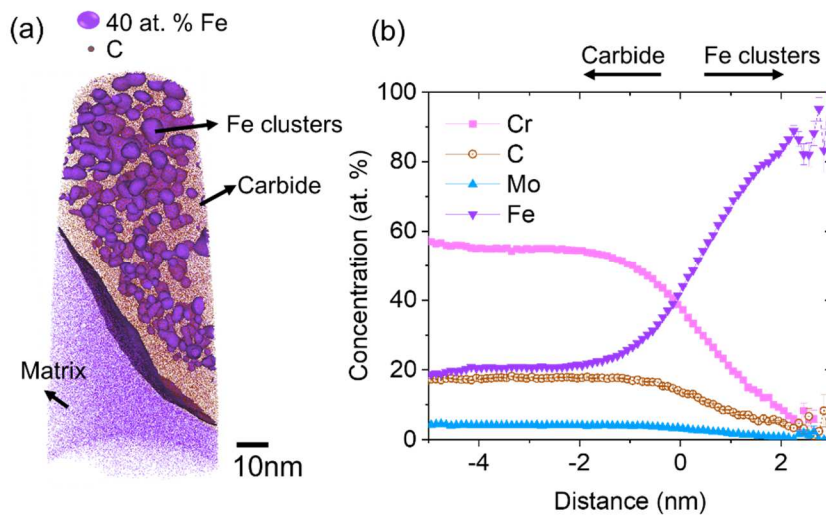


Figure 5 (a) 40 at. % Fe isoconcentration surface in BOR60 irradiated T91 at 524 °C:15.4dpa. The analysed volume is the same as in Figure 2 (e); (b) Averaged concentration proxigram across the 40 at. % Fe isoconcentration surface

## 273 4 Discussion

### 274 4.1 MNS-rich cluster formation

275 Distinct MNS-rich clusters were observed in all the samples irradiated below 415 °C.  
276 MNS clusters were not observed at 460 °C and 524 °C. The results from APT analysis  
277 are consistent with the STEM observation on the same set of materials, even though a  
278 clear grain boundary segregation of Ni and Si is observed at 460 °C [14]. From Table  
279 1, the radius of the detected clusters by TEM was 5 - 7 nm, with a number density in  
280 the order of  $10^{21} \text{ m}^{-3}$ . In the present study, the averaged diameter and number density  
281 obtained via APT were  $\sim 2 \text{ nm}$  and  $\sim 10^{23} \text{ m}^{-3}$ , respectively. The size measured by  
282 APT is much smaller than that of TEM and the number density is much higher. In the  
283 present study, matrix atoms were excluded to calculate the cluster size. This is based  
284 on the findings of previous studies which lead to the assumption that most matrix  
285 atoms incorporated into the detected MNS-rich clusters in this steel arise from  
286 trajectory aberration and limitations of the atom probe image reconstruction protocols  
287 [32,34]. Another possible reason is the difference in resolution limits of TEM  
288 compared to APT. It is highly likely that larger clusters occurring with lower number  
289 density measured via TEM are in fact present in the specimen studied here, but were  
290 statistically unlikely to be captured in the APT analyses due to its more limited  
291 sampling volume. Conversely, the much more abundant very small clusters detected  
292 via APT were not seen in TEM. These two techniques can be complementary to better

understand irradiation induced damage in materials and to underpin modelling efforts with microstructural data across a range of scales.

In this study APT analyses have characterised the compositions of MNS-rich clusters in T91. Previously Gupta [35] summarised several stable MNS-rich phases, namely G ( $\text{Mn}_6\text{Ni}_{16}\text{Si}_7$ ), E ( $\text{MnNiSi}$ ),  $\Gamma_1$  ( $\text{Mn}_3\text{Ni}_3\text{Si}_2$ ),  $\Gamma_2$  ( $\text{Mn}_2\text{Ni}_3\text{Si}_2$ ),  $\Omega$  ( $\text{Mn}_3\text{Ni}_2\text{Si}$ ). Among them, G phase and  $\Gamma_2$  phase have been reported to be thermally stable in various RPV steels [36–39]. Figure 6 summarises the Ni-Mn-Si relative composition of all the detected MNS-rich clusters in T91. The radius of each circle indicates the size of the corresponding cluster. In the present study, since the clusters are still in their early stage of formation, a large scatter is observed in cluster composition at all the irradiation conditions. Compared to the known Mn-Ni-Si phase, the composition of small clusters was closer to  $\Gamma_2$  phase. However, the larger clusters contain more Ni than the smaller ones and the composition shifted away from  $\Gamma_2$ . The larger precipitates possessed a Ni-Mn-Si composition closer to G-phase. The Ni-Mn-Si relative composition of the larger clusters were ~ 54 at. % Ni, 30 at. % Si and 16 at. % Mn. The Si content in the large clusters was still slightly higher than that of G phase and Mn content is slightly lower. Thus the clusters are likely precursors of G phase.

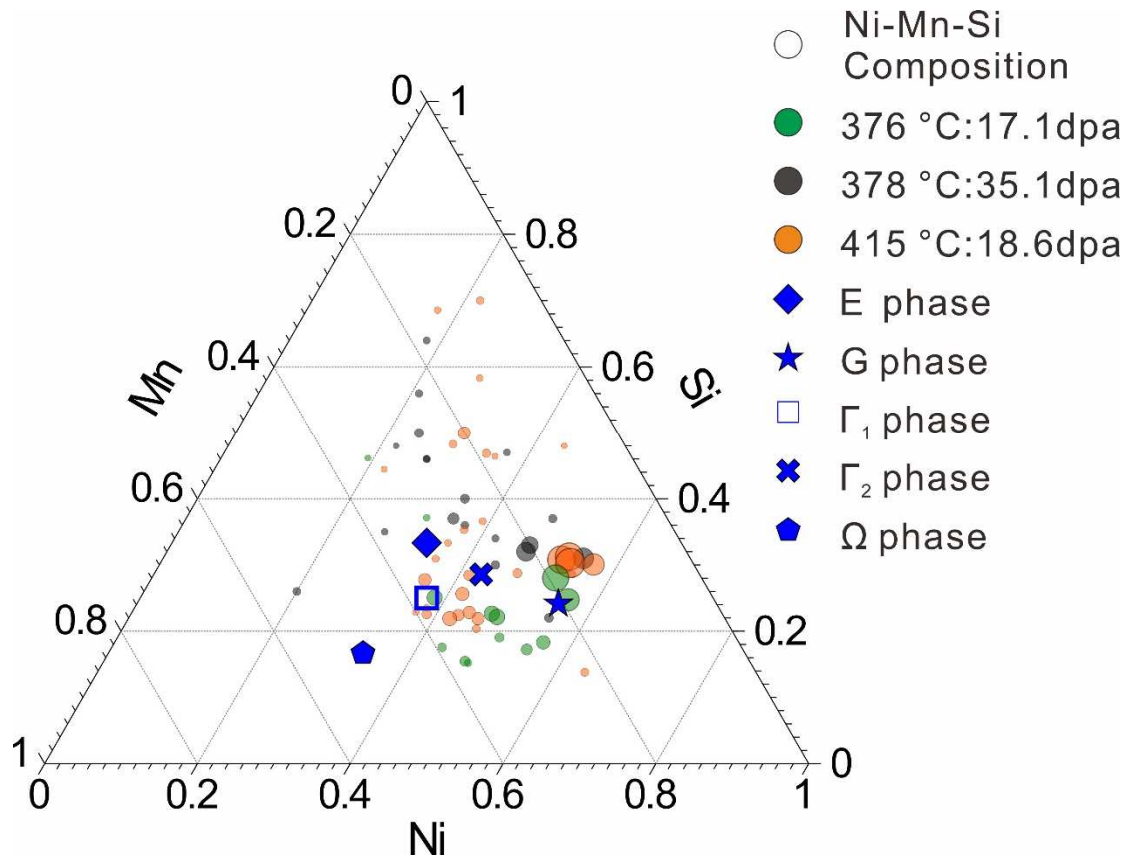


Figure 6 Gibbs triangle plot of APT Mn-Ni-Si compositions observed in BOR60 compared to known MNS phase

#### 4.2 Carbide matrix interface

In Figure 2 (c), a clear Ni, Mn, Si and P segregation to carbide matrix interface is seen in BOR60 irradiated T91 at 415 °C:18.6dpa. At higher temperature 524 °C, only P segregation was observed (Figure 2 (e)). The magnitude of depletion/enrichment are given in Table 5. At 415 °C Ni, Si, Mn and P at the observed grain boundary were enriched by 2.1 at. %, 2.2 at. %, 2.0 at. % and 0.8 at. %, respectively. At higher temperature 524 °C, the segregation of Ni, Si and Mn was not observed and the P segregation was decreased to 0.4 at. %. The grain boundary segregation of Ni and Si

on the same sample has been studied using STEM in Reference [14]. The magnitude of RIS of Ni and Si peaked around 415 °C and decreased at higher temperatures. At 524 °C, no clear segregation of Ni and Si was observed using STEM. Results from the APT analyses of the carbide matrix interface were similar to those of the grain boundary segregation behaviour. The segregation of Ni and Si to grain boundaries has been consistently reported in irradiated austenitic steel and F-M steels [14,40–43]. The segregation of Ni can be attributed to the Inverse-Kirkendall mechanism. Si is an undersized solute and binds strongly to interstitials, leading to enrichment at the sink. It is known that phosphorus has strong segregation tendency at grain boundaries, which is thought to reduce cohesion, causing the material to fail through inter-granular embrittlement [44–47]. P segregation was also reported at the interface boundaries of precipitate/matrix type [48]. Fraction of brittle intergranular fracture correlates with P segregation level [49]. In this study, P is present in T91 as an impurity. Similarly to the previous experimental and theoretical study, P segregates to the carbide/matrix interface and its contents at the interface decreased with the increasing temperature [50,51].

Table 5 Ni, Si, Mn and P grain boundary peak concentrations (at. %) and changes ( $\Delta$ ) from nominal values in T91 irradiated in BOR60. The error was obtained by averaging the concentration value in the range of  $\pm 0.6$  nm from the peak position.

<b>Irradiation condition</b>	<b>Ni</b>	<b><math>\Delta</math>Ni</b>	<b>Si</b>	<b><math>\Delta</math>Si</b>	<b>Mn</b>	<b><math>\Delta</math>Mn</b>	<b>P</b>	<b><math>\Delta</math>P</b>
<b>415 °C:18.6dpa</b>	2.4 $\pm$ 0.2	2.1	2.3 $\pm$ 0.2	2.2	2.5 $\pm$ 0.1	2.0	0.8 $\pm$ 0.0	0.8
<b>524 °C:15.4dpa</b>	-	-	-	-	-	-	0.4 $\pm$ 0.0	0.4

### 4.3 Fe clustering inside carbide

Fe-rich clusters were observed to form inside the carbide particle at 524 °C. This was not seen at lower temperatures. In previous studies, APT analyses of carbides after ion or neutron irradiation at temperature between 377 °C - 470 °C were shown [52,53]. Fe clustering inside carbide particles has not been reported. In the present study, the core composition of the Fe-rich clusters exceeded 80 at. %. These clusters were believed to be ferrite clusters. A noticeable difference is that the C concentration inside the carbide particle was ~ 17 at. % when irradiated at 524 °C (Figure 4 (b)). The ratio of metal/carbon exceeded the equilibrium value [54]. It is possible that the supersaturation of Fe inside carbide have caused the Fe clustering. It is known that prior to irradiation, the  $M_{23}C_6$  particles were along PAGBs and lath boundaries [14]. The radiation induced enrichment/depletion of elements at PAGBs may have led to change in the Fe concentration of grain boundary and hence altering the composition of carbide particles. Irradiation has also been suggested to alter the composition of carbides [12]. Alternatively, the supersaturation of Fe inside the carbide may also exist prior to irradiation due to the fluctuation in carbide composition. Thermo-Calc with the TCFE6 database has been used to calculate the equilibrium phase inside the carbide. The actual carbide composition (~ 55 at. % Cr, 17 at. % C, 4 at. % Mo and Fe as balance) after irradiation at 524 °C was used to estimate the thermally stable phases at 524 °C. The

results confirmed the presence of ferrite under equilibrium. Irradiation could also accelerate the formation process of the Fe-rich clusters.

## 5 Conclusions

Atom probe tomography has offered insight into the detailed clustering and segregation behaviour of T91 steel irradiated in BOR60 reactor. The following conclusions can be drawn:

- MNS-rich clusters were observed after BOR60 irradiation at temperatures lower than 415 °C, which were not seen at higher temperatures (460 °C and 524 °C). More abundant and much smaller MNS-rich clusters were captured via APT than that of previous STEM observation, which complements the previous STEM study to provide microstructural information from different scales.
- The composition of the early stage MNS-rich clusters was characterised and compared with the thermally stable Ni-Mn-Si phases. The clusters were likely G phase precursors.
- Segregation of Ni, Si, Mn and P to the Cr-rich carbide/matrix interface was observed after BOR60 irradiation. The segregation magnitude decreased with increasing temperature. At the highest irradiation temperature 524 °C, only P segregation was detected.
- Clustering of Fe atoms inside a carbide was observed at 524 °C:15.6dpa under BOR60 irradiation.

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