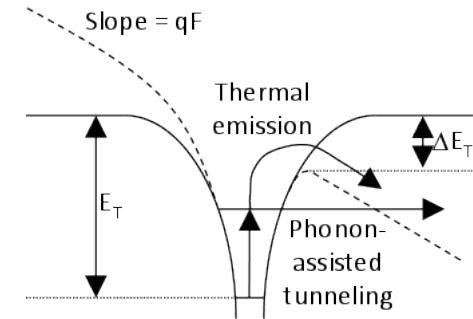
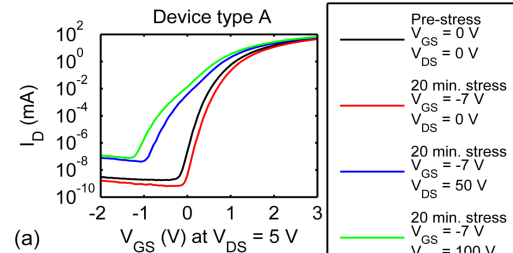
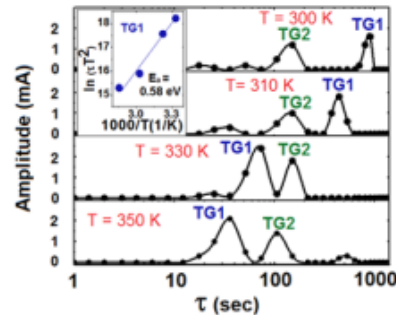
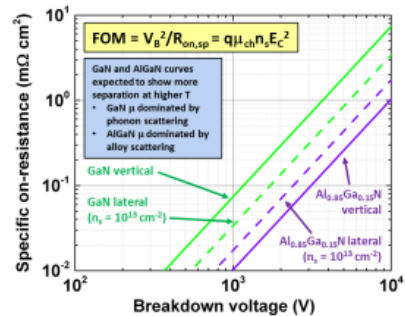


Exceptional service in the national interest



GaN Power HEMT Reliability Work at Sandia National Labs



Presentation to 5N Plus
Bob Kaplan, December 22, 2020

This work was supported by DOE OE (Drs. Imre Gyuk and Mike Soboroff)



Sandia National Laboratories is a multimission laboratory managed and operated by National Technology & Engineering Solutions of Sandia, LLC, a wholly owned subsidiary of Honeywell International Inc., for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-NA0003525.

Outline

- 1. Introduction**
- 2. Work with MIT on AlGa_N/Ga_N HEMT reliability**
- 3. Work with HRL on AlGa_N/Ga_N HEMT reliability**

Outline

1. Introduction

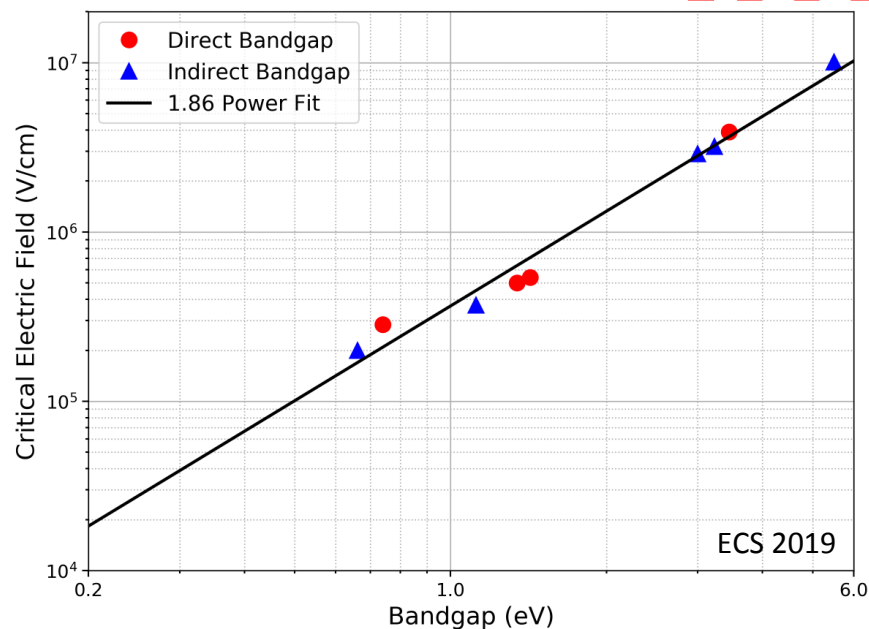
2. Work with MIT on AlGa_N/Ga_N HEMT reliability

3. Work with HRL on AlGa_N/Ga_N HEMT reliability

Critical Electric Field Scales with Bandgap and Determines Unipolar FOM

- Critical electric field is believed to follow a power-law with bandgap*: $\epsilon_{\text{crit}} \sim E_{\text{g}}^{1.86}$
- Normalizing to doping and DT/NDT yields ~ 1
- Implies strong de

No Image



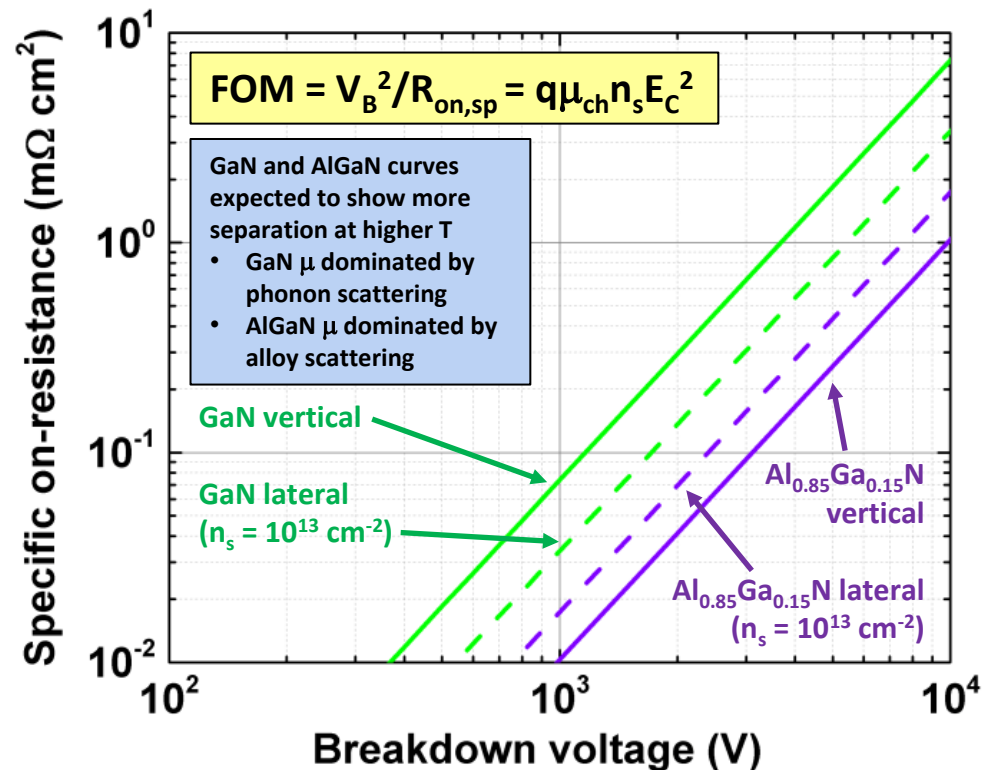
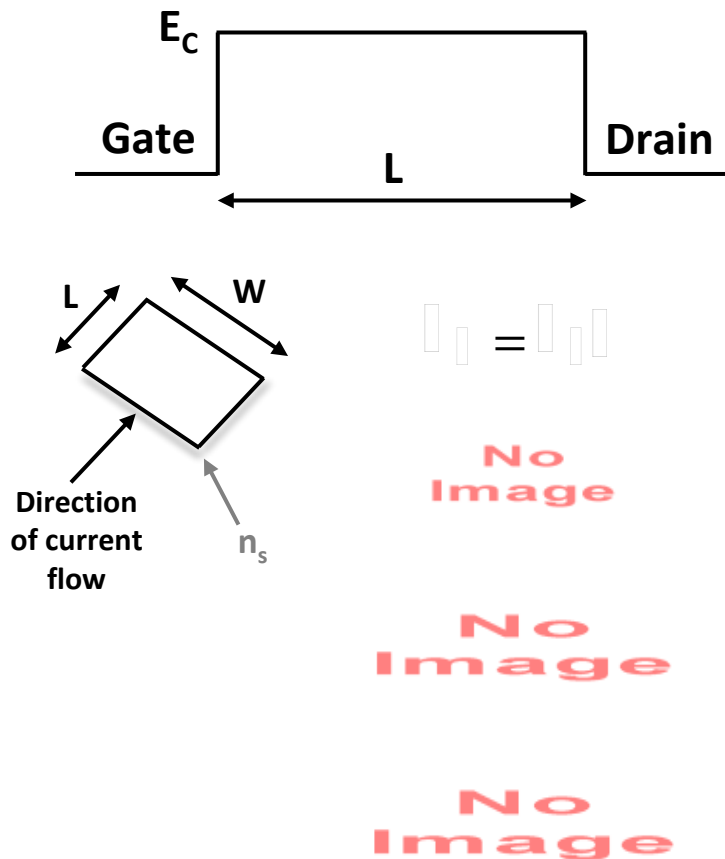
* Hudgins et al., *IEEE Trans. Power Elec.* **18(3)**, 907 (2003)



Tsao et al., *Adv. Elec. Mat.* **4**, 1600501 (2018)

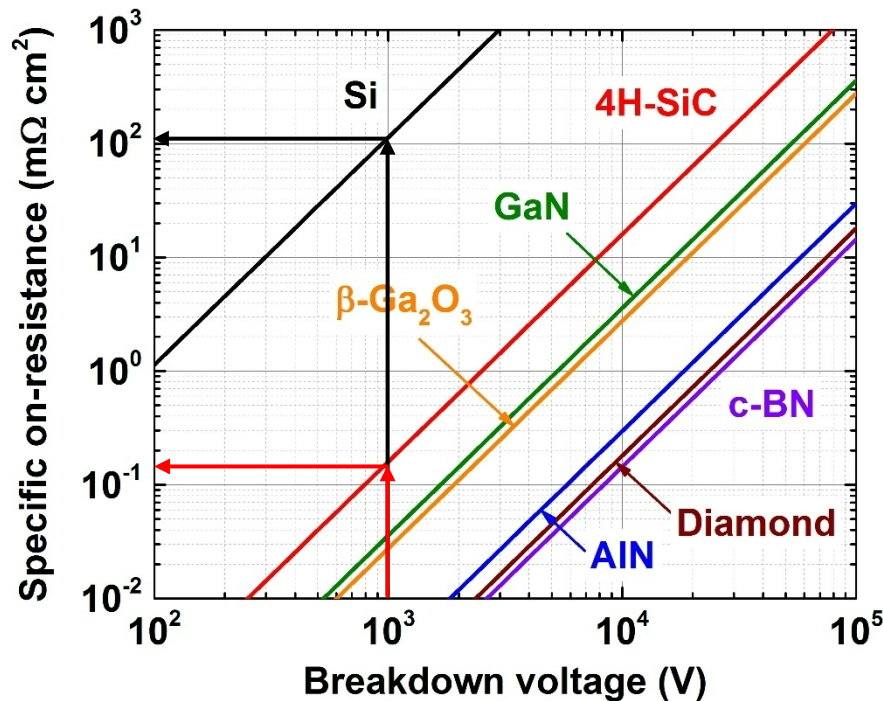
Lateral Power Device Figure of Merit (Applicable to HEMTs)

- Not as widely known as the unipolar FOM
- Unipolar (vertical) FOM is often incorrectly used for lateral devices



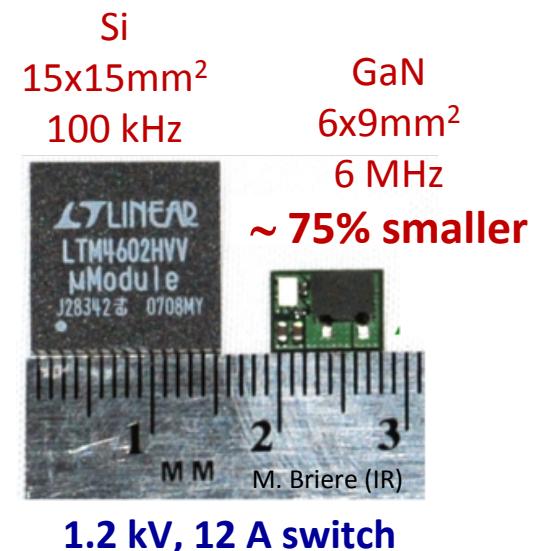
- Proportional to E_C^2 rather than E_C^3 , but high n_s can result in high FOM

How Do WBGs and UWBGs Lead to Higher Switching Frequency and Lower Loss?



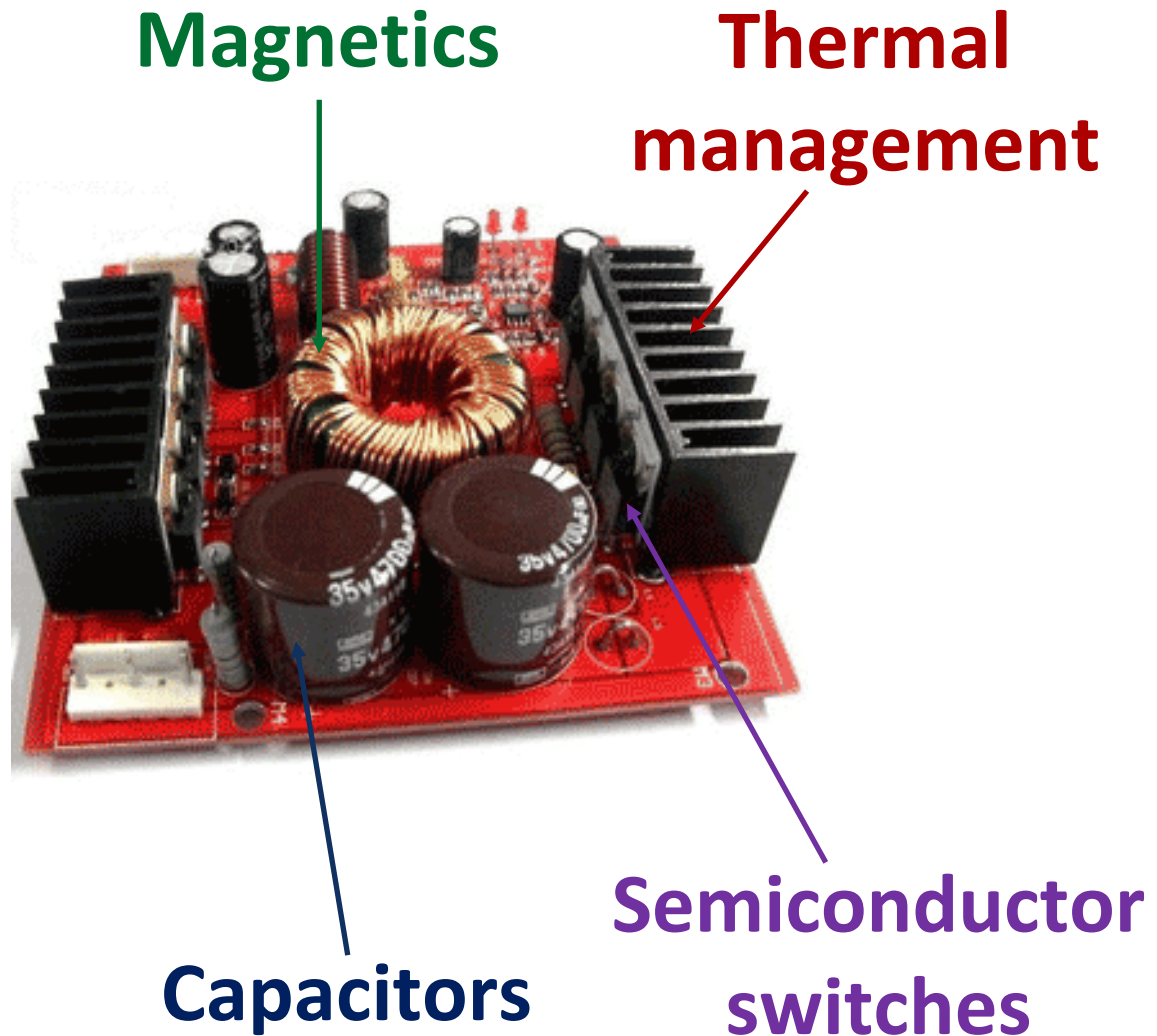
- For equivalent breakdown voltage, get lower R_{on} for (U)WBG device
 - For same R_{on} , (U)WBG device can have *smaller area*
 - Smaller area results in *less capacitance*
 - Gives a *faster switching transient* and *lower loss per switching cycle*

The scaling that results from the properties of WBG and UWBG materials can be utilized to optimize for switching frequency, conduction loss, and switching loss

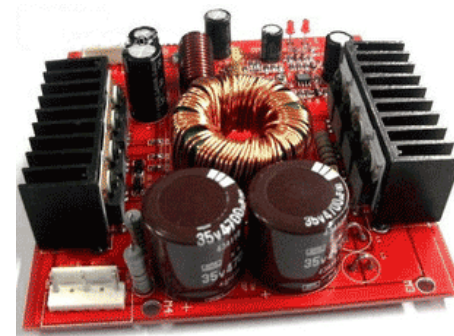
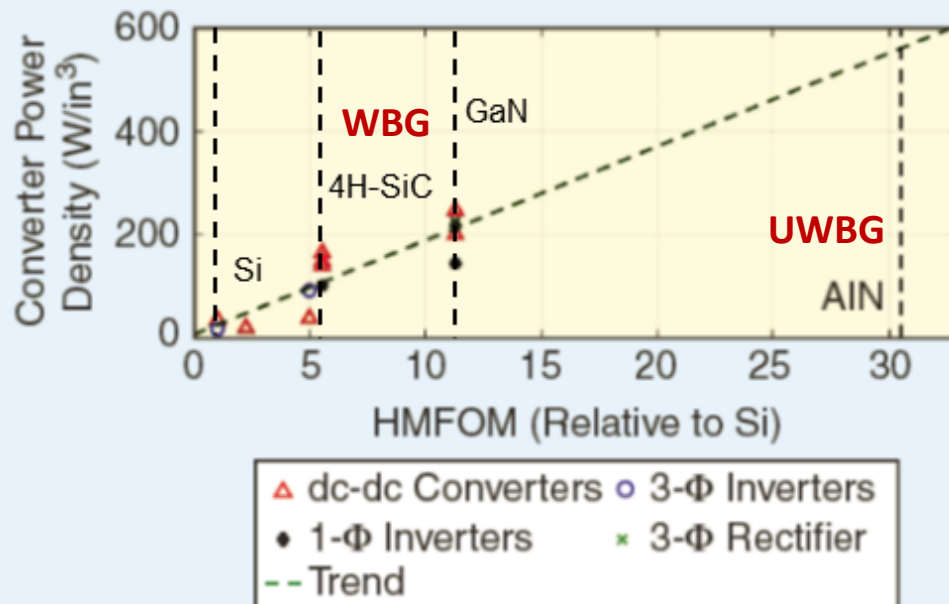


Power Converter Size is Determined by Passive Elements

- Passive elements and thermal management comprise the bulk of the volume and mass of a power converter
- These can be reduced in size using WBG semiconductors due to faster switching and reduced loss



Power Density Scaling with Semiconductor Material Properties



Si



WBG



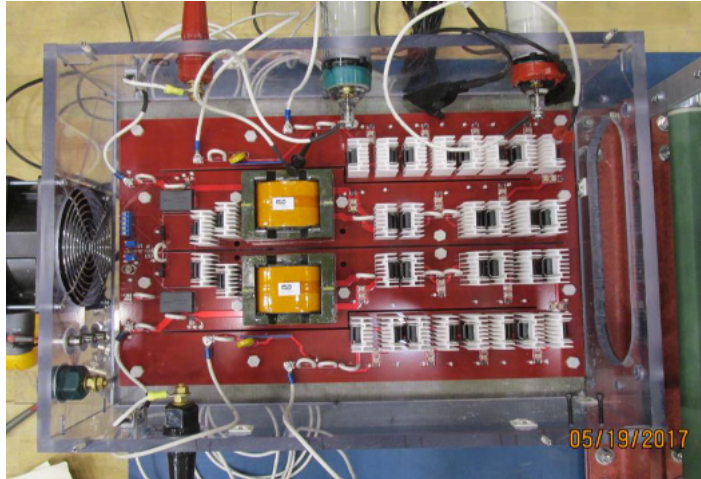
UWBG

Relative Figures of Merit:

- Vertical UFOM = $\epsilon \mu_n E_c^3$
- Huang Material FOM = $E_c \mu_n^{1/2}$
- HM-FOM seems to be a good predictor of power density

R. J. Kaplar, J. C. Neely, et al., *IEEE Power Electronics Magazine* (March 2017)

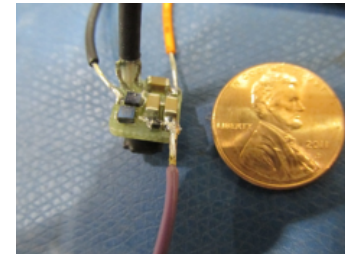
Efficient and Compact Power Conversion Enabled by WBG Semiconductors



SNL SiC hybrid switched-capacitor boost converter (ARPA-E)

- First prototype: 0.5 kV \rightarrow 10.1 kV (gain = 16.8) at 2.6 kW, 95.3% efficient, 410 in³
- Second prototype: +2% efficiency, 55% volume

Over an order of magnitude
improvement in power density is
enabled by use of GaN power
transistors compared to Si



SNL GaN HEMT "Coin Converter"
90 V, 90 mA \rightarrow 215 W/in³



SNL GaN HEMT microinverter
400 W in 2.4 in³ \rightarrow 167 W/in³



SOA commercial microinverter
250 W in 59 in³ \rightarrow 4.2 W/in³

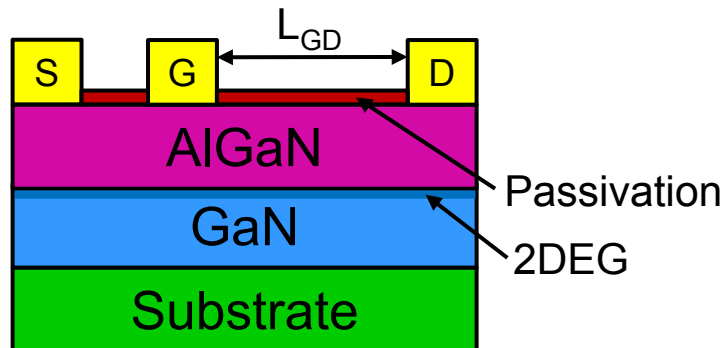
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High-Voltage AlGa_N/Ga_N HEMTs Fabricated at MIT



High Electron Mobility Transistor:

- Designed and fabricated at MIT
- Polarization induces high- μ channel
- Normally-on device
- L_{GD} and Al% control V_{BD}

	Device 1	Device 2	Device 3	Device 4
Maximum V_{BD}	1800 V	1800 V	500 V	500 V
V_{TH}	-3.6 V	-3.6 V	-1.8 V	-1.8 V
Barrier	50 nm $Al_{0.15}Ga_{0.85}N$	50 nm $Al_{0.15}Ga_{0.85}N$	20 nm $Al_{0.26}Ga_{0.74}N$	20 nm $Al_{0.26}Ga_{0.74}N$
Passivation	$Al_2O_3/SiO_2/Al_2O_3$	None	$Al_2O_3/SiO_2/Al_2O_3$	None
C-doped buffer	Yes	Yes	No	No

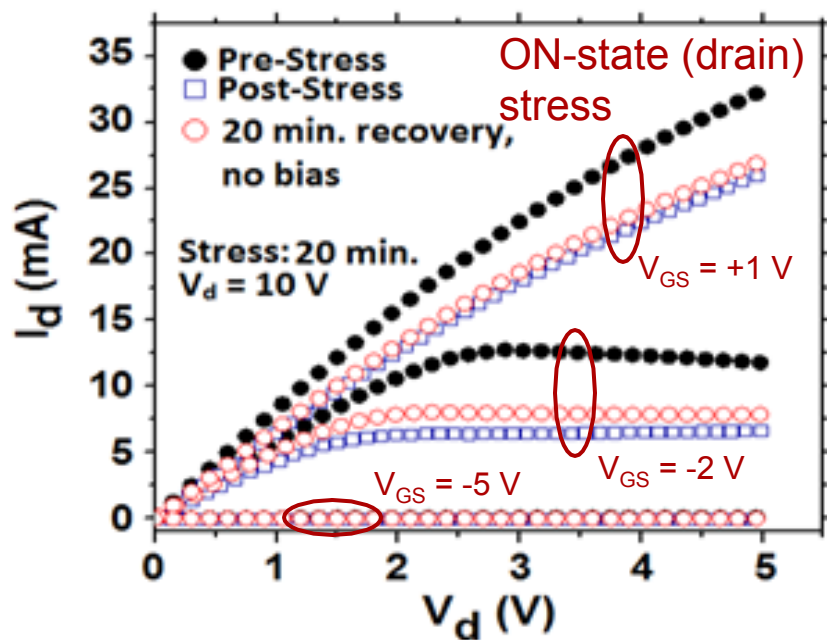
$$L_G = 2 \mu m, L_{GS} = 1.5 \mu m, L_{GD} = 1.5 \text{ to } 40 \mu m$$

All devices grown on (111) Si by MOCVD

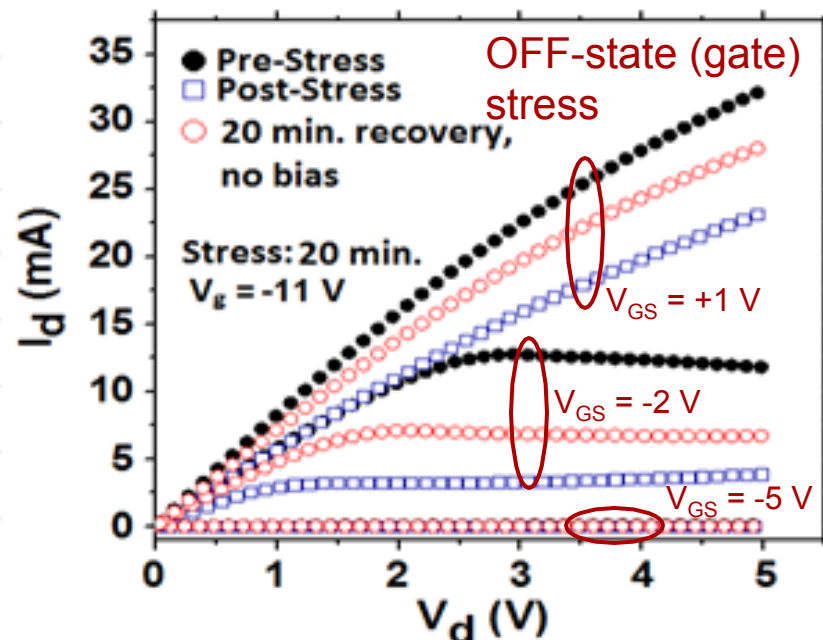
S. DasGupta et al., IEEE TED 59(8), 2115 (2012)

ON-State vs. OFF-State Stress

Passivated $\text{Al}_{0.15}\text{Ga}_{0.85}\text{N}/\text{GaN}$ sample



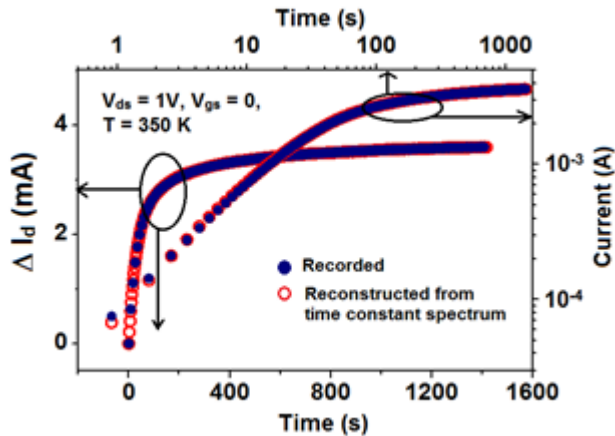
Stress: $V_{DS} = 10$ V, $V_{GS} = 0$ V (ON)



Stress: $V_{DS} = 0$ V, $V_{GS} = -11$ V (OFF)

ON-state stress (drain bias) results in much slower recovery than OFF-state stress (gate bias)

Recovery Current Transient Analysis Following Gate Stress



Fitting of recovery transient amplitudes

A_i with fixed τ_i :

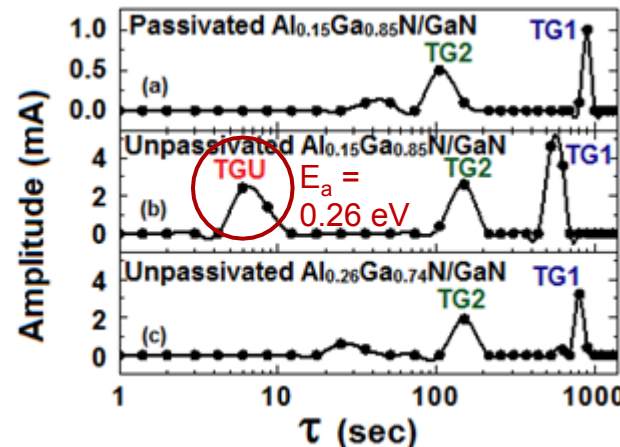
$$\Delta I_d = \sum_i A_i \left[1 - \exp\left(-\frac{t}{\tau_i}\right) \right]$$

Peaks in time constant spectra are indicative of different traps in different samples

$$\Delta I_d = \sum_i A_i \left[1 - \exp\left(-\frac{t}{\tau_i}\right) \right]$$

Passivated $\text{Al}_{0.26}\text{Ga}_{0.74}\text{N}/\text{GaN}$ temperature dependence

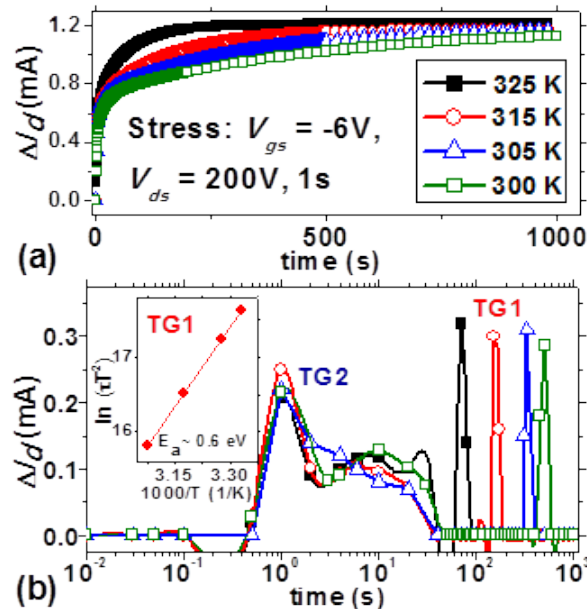
TG1 is thermally activated; TG2 is not. Why?



Comparison of other samples; note TGU only for unstable sample

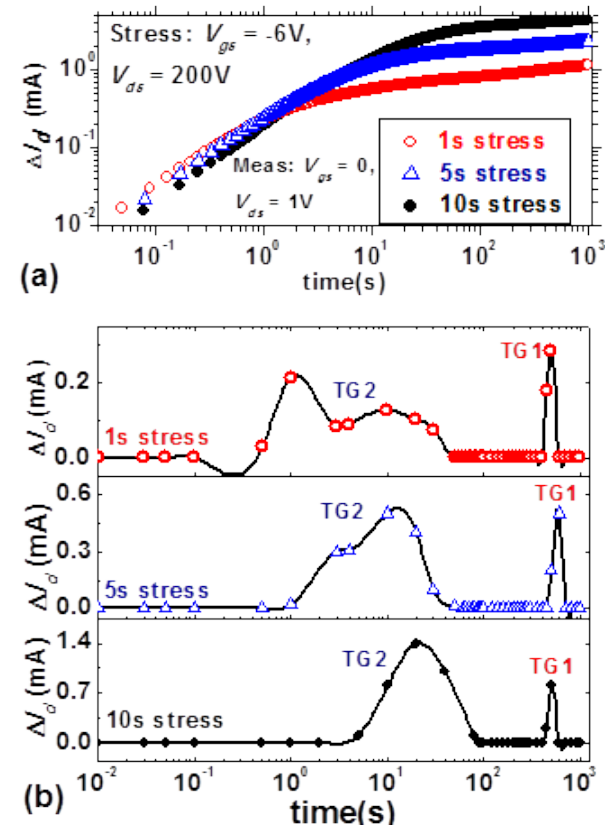
Temperature- and Stress-Time-Dependence of Degradation

Newer samples: 50 nm barrier, thicker passivation, $V_T = -4.1$ V



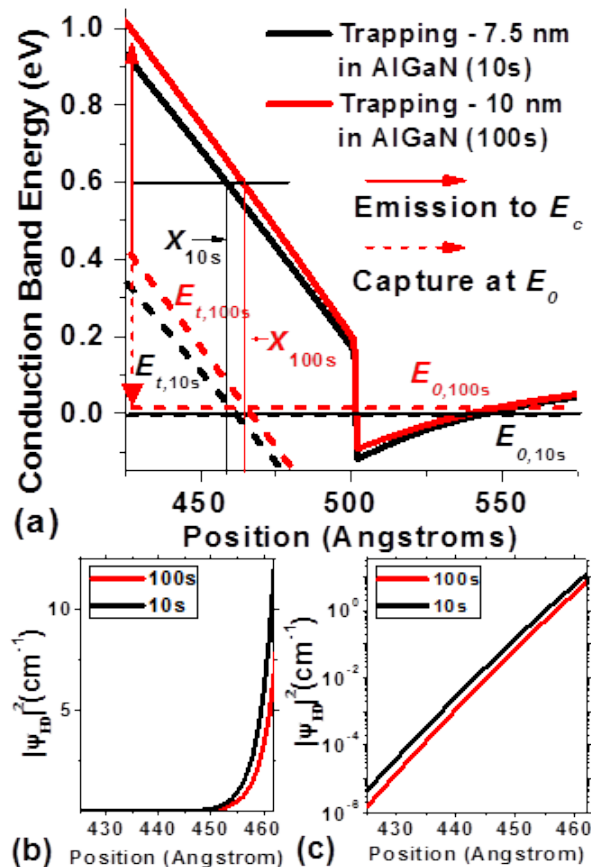
**Stress time fixed,
vary temperature**

**TG1 shows clear thermally activated behavior,
but TG2 is insensitive to temperature**



**Vary stress time,
temperature fixed**

Deep-Level / 2DEG Quantum Well Interaction Model

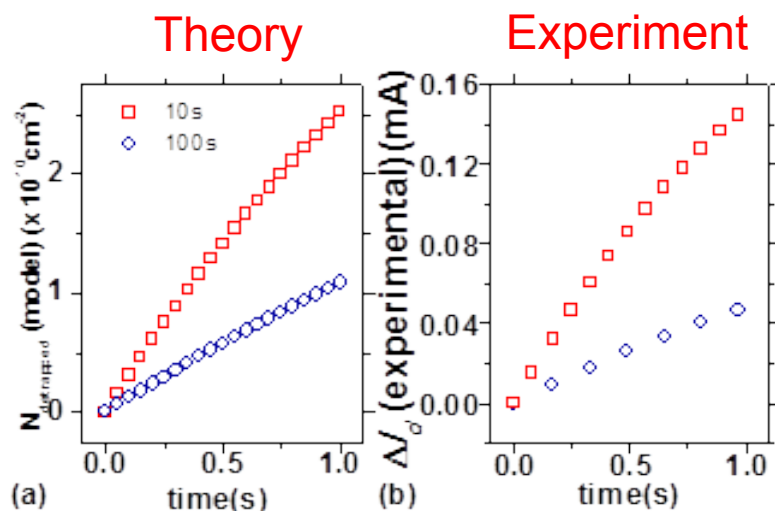


Our model proposes that a single deep level in the AlGa_N barrier ($E_c - 0.6$ eV) may emit electrons in two different ways, resulting in two different peaks:

1. To the AlGa_N CB (Arrhenius)
2. To the 2DEG wavefunction (insensitive to temperature)

Longer stress times raise the CB edge in the AlGa_N, reducing the spatial depth over which the 2DEG wavefunction overlaps with the deep level

Proposal: Electrons Are Directly Captured Into Multiple 2DEG QW States



Time constant for capture of electron from deep level to 2DEG tail:

$$1/\tau_n(x) = |\psi_n(x)|^2 D_{2D} \sigma v_{th}$$

ψ_n = nth QW wavefunction (cm^{-1/2})

D_{2D} = In-plane 2DEG DOS (cm⁻²)

σ = Capture cross section (cm²)

v_{th} = Thermal velocity (cm/s)

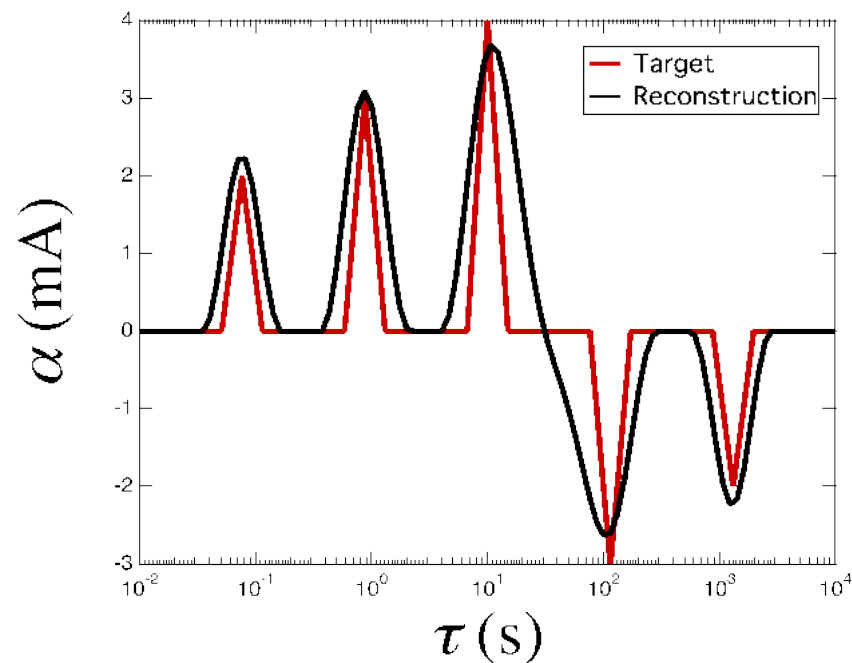
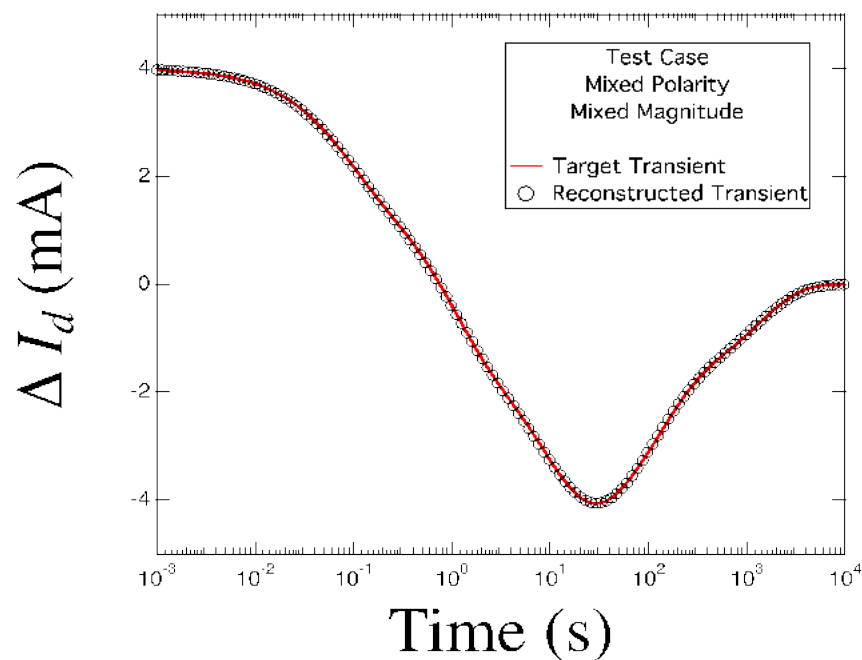
Overall recovery time constant may be tuned by wavefunction engineering (barrier height, etc.) to be much shorter than the bulk emission time; *reliability may thus be controlled by device design*

Sum time constants for each 2DEG level plus thermal term to get overall emission rate:

$$\frac{1}{\tau(x)} = \frac{1}{\tau_e} + \sum_n \frac{1}{\tau_n(x)}$$

What About Negative Peaks Due to Trapping?

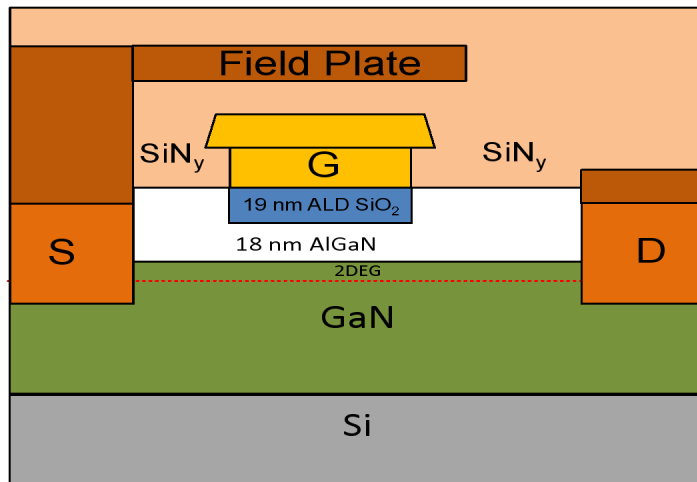
$$\Delta I_d = \sum \alpha_i (1 - e^{-t/\tau_i}) \implies y_{fit} = \min \left(|y - A\alpha|^2 + \left| \frac{d}{dt} A\alpha \right|^2 \right)$$



- Artificial transient representative of simultaneous trapping and emission of electrons
- Corresponding time-constant spectrum shows both trapping and emission processes are recoverable

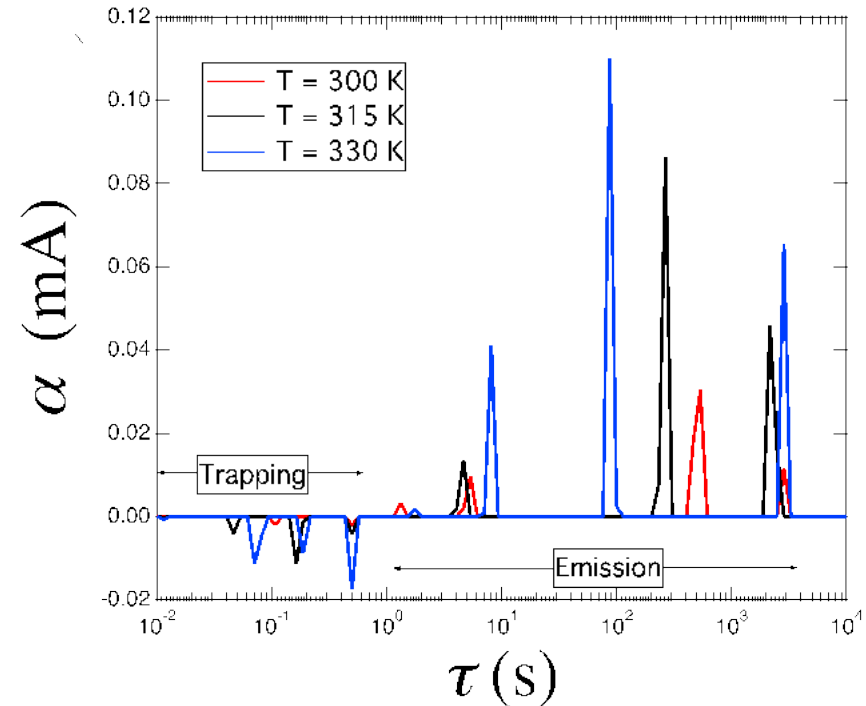
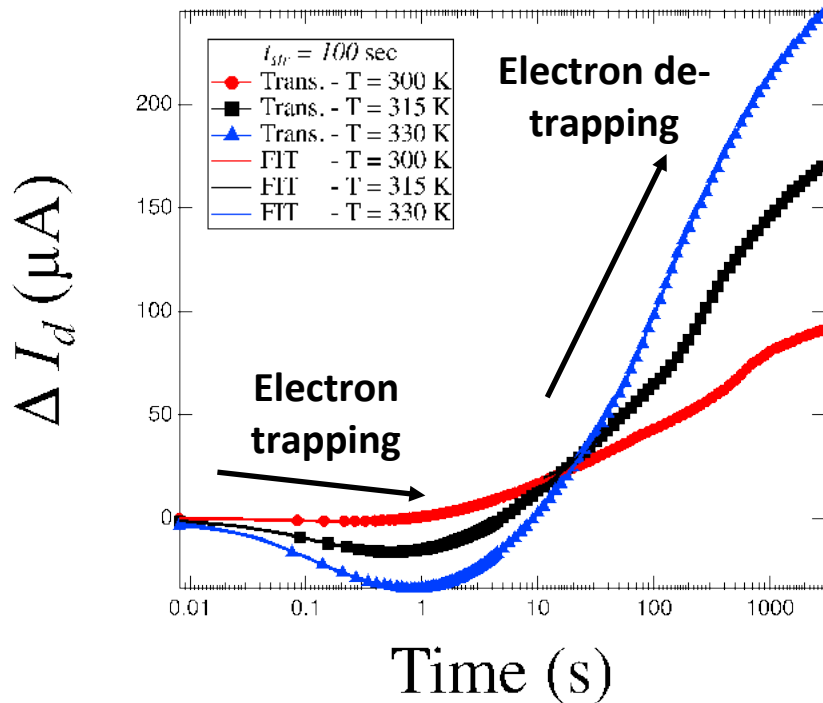
M. P. King et al., Proc. 53rd IRPS (2015)

Off-State Stress MOS-HEMT Devices



- Stress-time and temperature dependent off-state parametric shifts in I_d
- Off-state stress conditions
 $V_{gs} = -5 \text{ V}$
 $V_{ds} = 100 \text{ V}$
- Recovery-state
 $V_{gs} = 1 \text{ V}$
 $V_{ds} = 0.1 \text{ V}$

Temperature Dependent Off-State Parametric Shifts



- Electron trapping decreases I_d
- De-trapping (emission) increases I_d
- Suggests electron trapping dominates at short recovery times (< 10 s) and emission dominates for longer times
- Time constant spectrum reveals the presence of concurrent trapping and emission processes
- Temperature dependent peak present with $E_a = 0.58$ eV

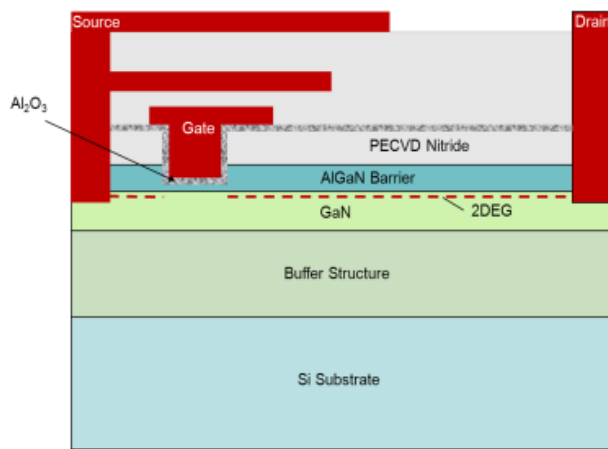
M. P. King et al., Proc. 53rd IRPS (2015)

Outline

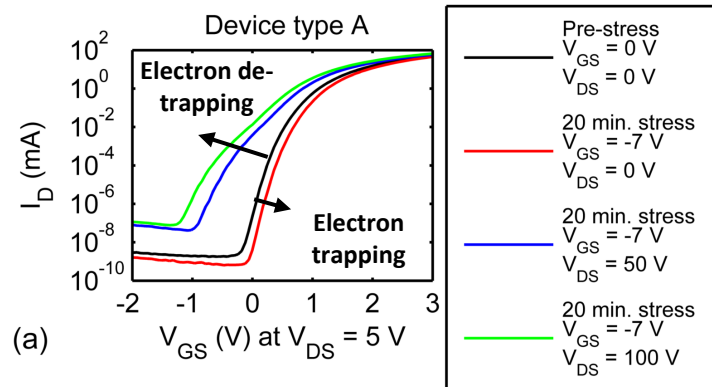
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Different stresses on different devices

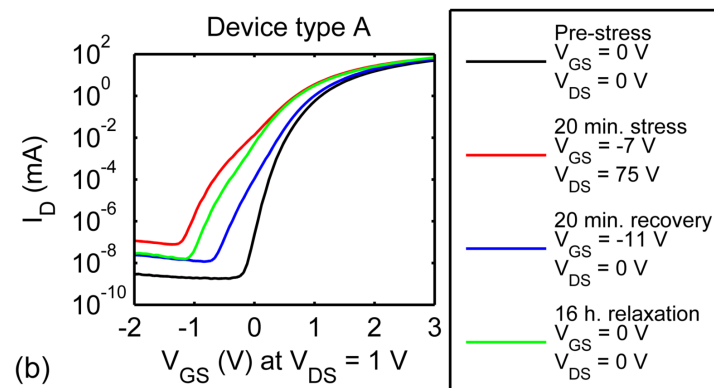


Gate stack process splits

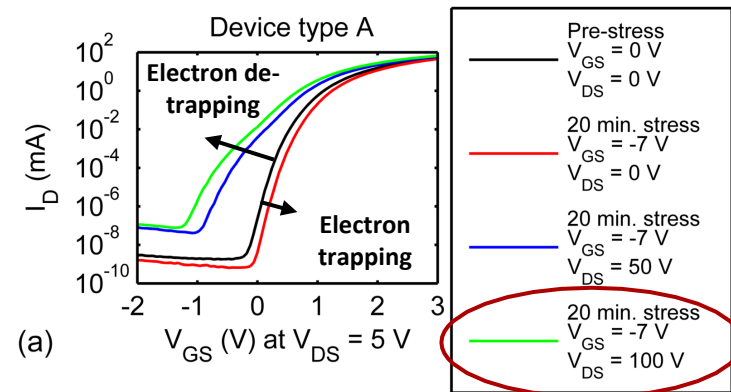
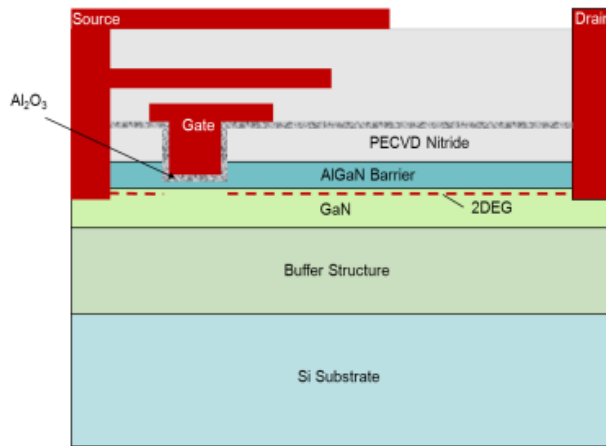
Device Type	Gate Oxide (Al_2O_3)	Gate Stack AlGaN
A	Yes	Present ($t \sim 5$ nm)
B	No	Residual ($t < 1$ nm)
C	No	Present ($t \sim 5$ nm)

Different electrical stress may results in both electron trapping and de-trapping (i.e. emission)

Sequential stresses on the same device



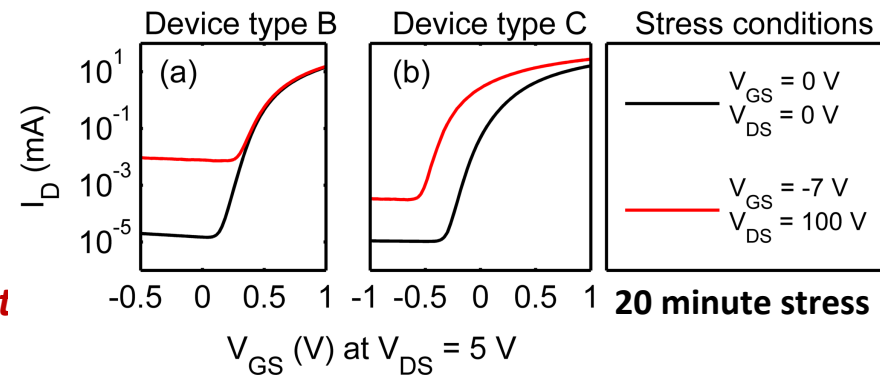
Different Process Splits Have Different Responses to Off-State Stress



Gate stack process splits

Device Type	Gate Oxide (Al_2O_3)	Gate Stack AlGaN
A	Yes	Present ($t \sim 5$ nm)
B	No	Residual ($t < 1$ nm)
C	No	Present ($t \sim 5$ nm)

The lack of a V_T shift in device type B suggests that the defects responsible for instability are in the AlGaN portion of the gate stack



A Reversal from Electron Trapping to De-Trapping is Observed

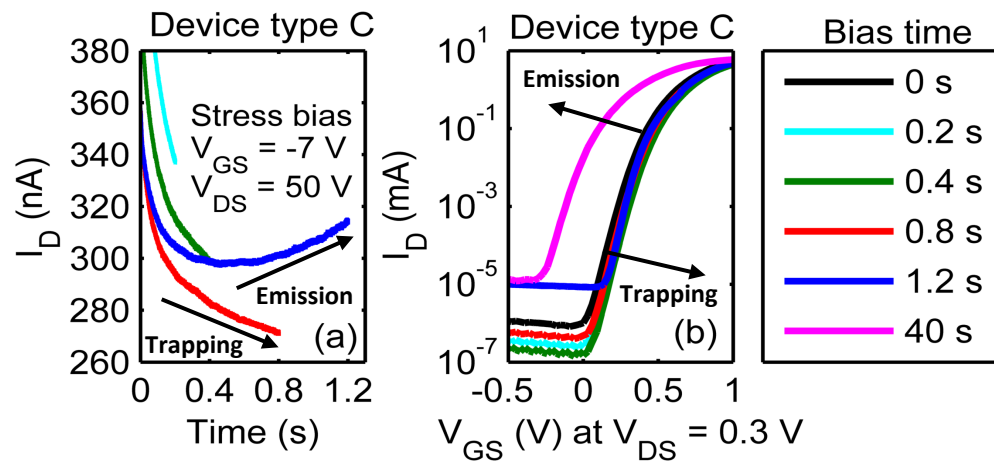
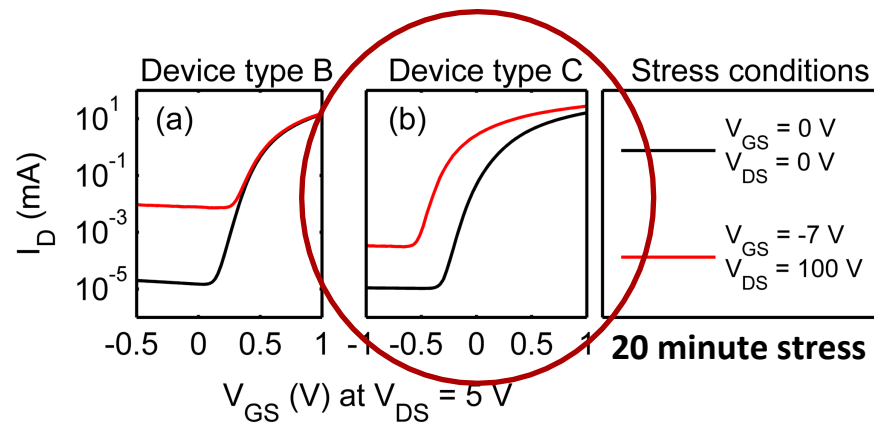
Gate stack process splits

Device Type	Gate Oxide (Al_2O_3)	Gate Stack AlGaIn
A	Yes	Present ($t \sim 5$ nm)
B	No	Residual ($t < 1$ nm)
C	No	Present ($t \sim 5$ nm)

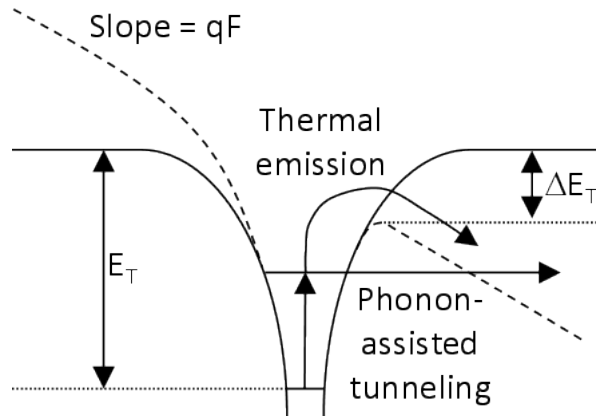
Blocking stress at short times results in **reduction in $I_D \rightarrow$ Positive V_T shift** (electron trapping)

This is in contrast to stress for long times, which shows an increase in $I_D \rightarrow$ **Negative V_T shift** (electron de-trapping)

This is explained by a transition from electron trapping to emission with prolonged stress



Field-Enhanced Emission Model to Explain Trapping to De-Trapping Transition



Poisson equation

$$\frac{\partial^2 \phi(t, x)}{\partial x^2} = \frac{qn_T(t, x)}{\epsilon}$$

Capture / emission rate equation

$$\frac{dn_T}{dt} = \left. \frac{dn_T}{dt} \right|_{\text{capture}} + \left. \frac{dn_T}{dt} \right|_{\text{Thermal Emission}} + \left. \frac{dn_T}{dt} \right|_{\text{Phonon-assisted Tunneling}}$$

Expressions
for capture
and emission
mechanisms

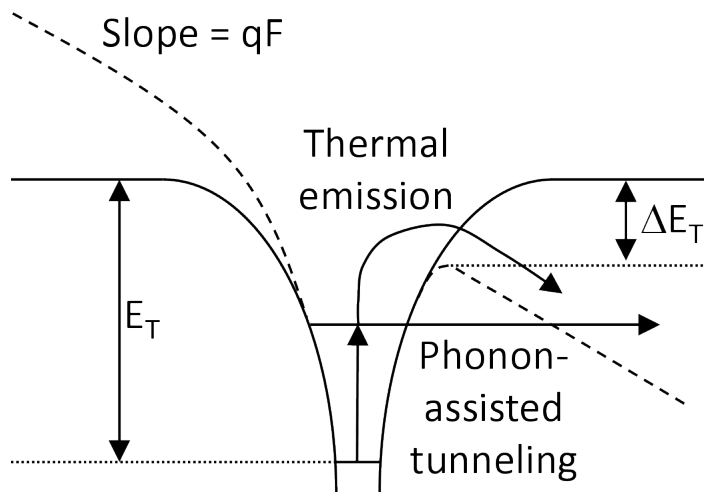
$$\left. \frac{dn_T}{dt} \right|_{\text{capture}} = \sigma_n v_{th} (N_T - n_T) n = \sigma_n v_{th} (N_T - n_T) n_0 \exp\left(\frac{-E_B}{kT}\right)$$

$$\left. \frac{dn_T}{dt} \right|_{\text{Thermal Emission}} = -\sigma_n v_{th} N_C \exp\left(\frac{-(E_T - \Delta E_T)}{kT}\right) n_T(t, x) \text{ with } \Delta E_T = q \sqrt{q \left| \frac{\partial \phi}{\partial x} \right| / \pi \epsilon}$$

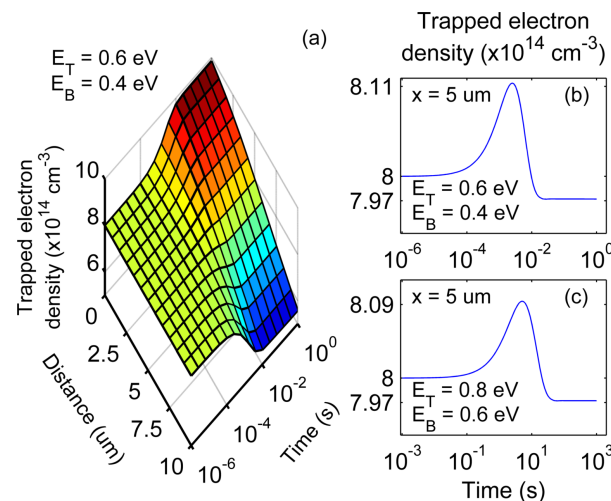
$$\left. \frac{dn_T}{dt} \right|_{\text{Phonon-assisted Tunneling}} = -\sigma_n v_{th} N_C \exp\left(\frac{-E_T}{kT}\right) \left[\int_{\Delta E_T/kT}^{E_T/kT} \exp\left[z - z^{3/2} \left(\frac{8\pi \sqrt{m_n^* (kT)^3}}{3qh |\partial \phi / \partial x|} \right) \left(1 - \left(\frac{\Delta E_T}{zkT} \right)^{5/3} \right) \right] dz \right] n_T(t, x)$$

R. J. Kaplar et al., Proc. 26th ISPSD, 209 (2014); S. G. Khalil et al., Proc. 52nd IRPS, CD.4 (2014)

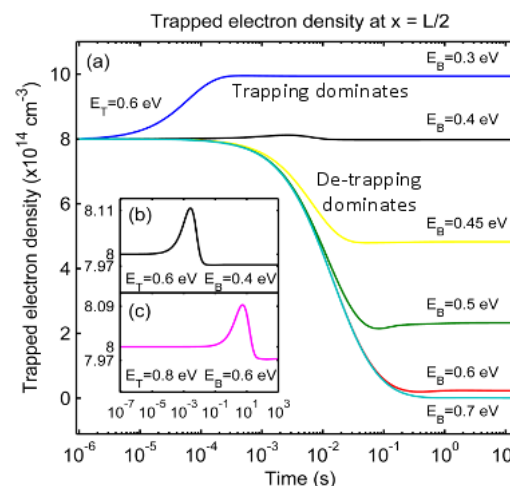
1D Field-Enhanced Emission Model Results



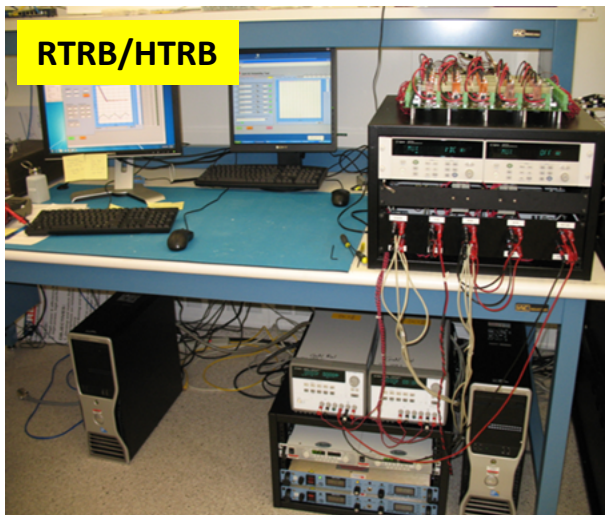
Simplified 1D model is able to qualitatively explain trapping to de-trapping transition!



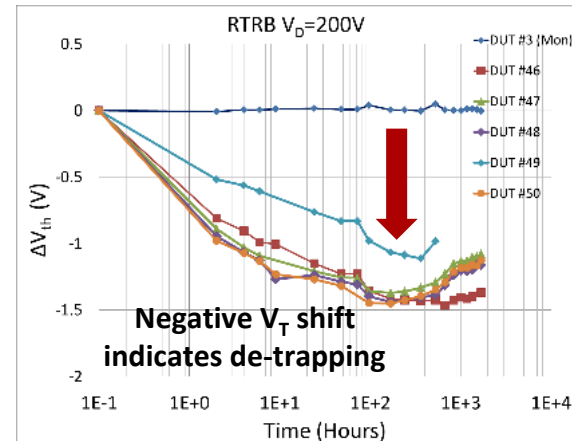
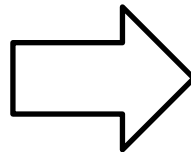
Trapped electron density vs. position and time



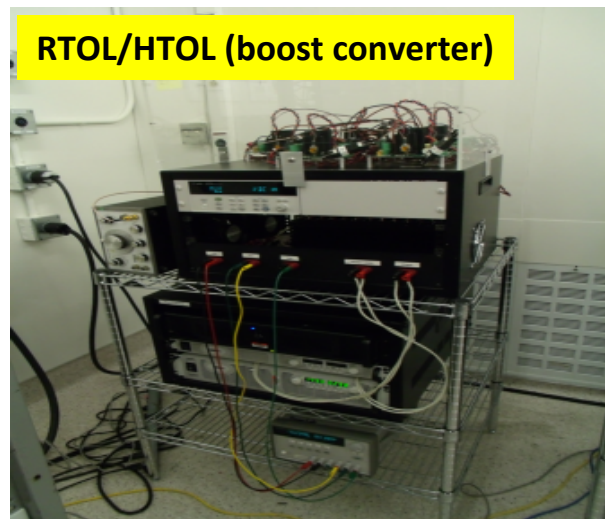
Correlation with Reverse Bias and Operating Life Testing



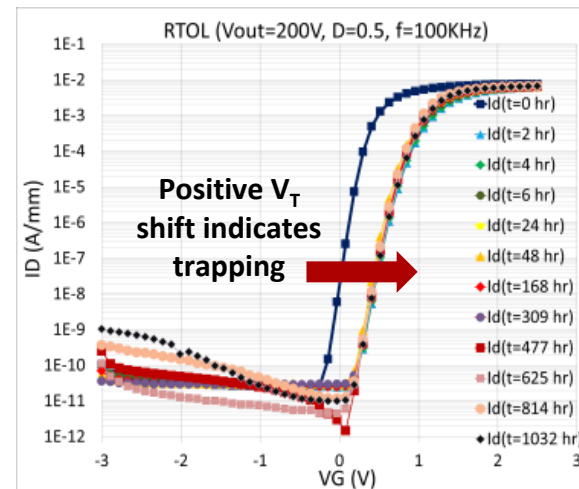
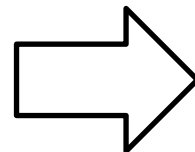
RTRB



DC stress

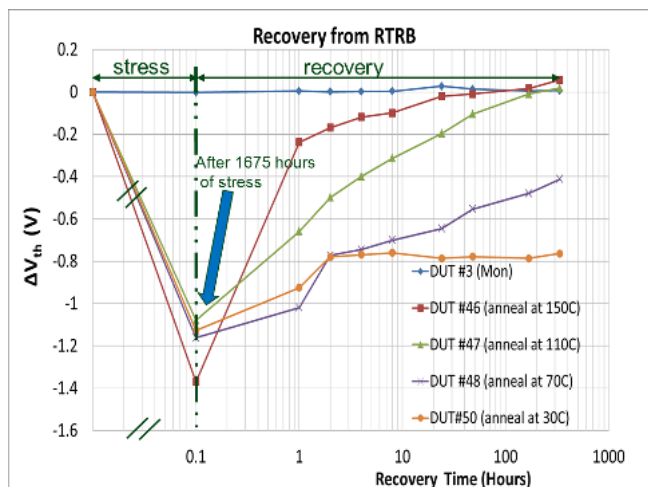


RTOL



AC stress

Temperature-Dependence of Reliability Stress



Recovery from RTRB stress:

- Positive V_T shift indicates electron capture
- Temperature dependence indicates a barrier to electron capture, consistent with model

Working theory

- *For RTRB/HTRB, the stress time is long so a negative V_T shift resulting from electron de-trapping is observed*
- *For RTOL/HTOL, the effective stress time is short (during blocking bias conditions) so a positive V_T shift resulting from electron trapping is observed*

Summary

- **Physics-based investigations of AlGaIn/GaN HEMT reliability with MIT and HRL, in both cases focused on parametric shifts due to electron capture and emission**
- **Temperature-dependent and independent signatures are observed**
- **A transition from electron capture to emission explains many observations**
- **Coupling of device design and electric field distribution to defects is of critical importance**

The contributions of all past and present collaborators are gratefully acknowledged