



DOE Stress Corrosion Cracking Research at Sandia National Labs

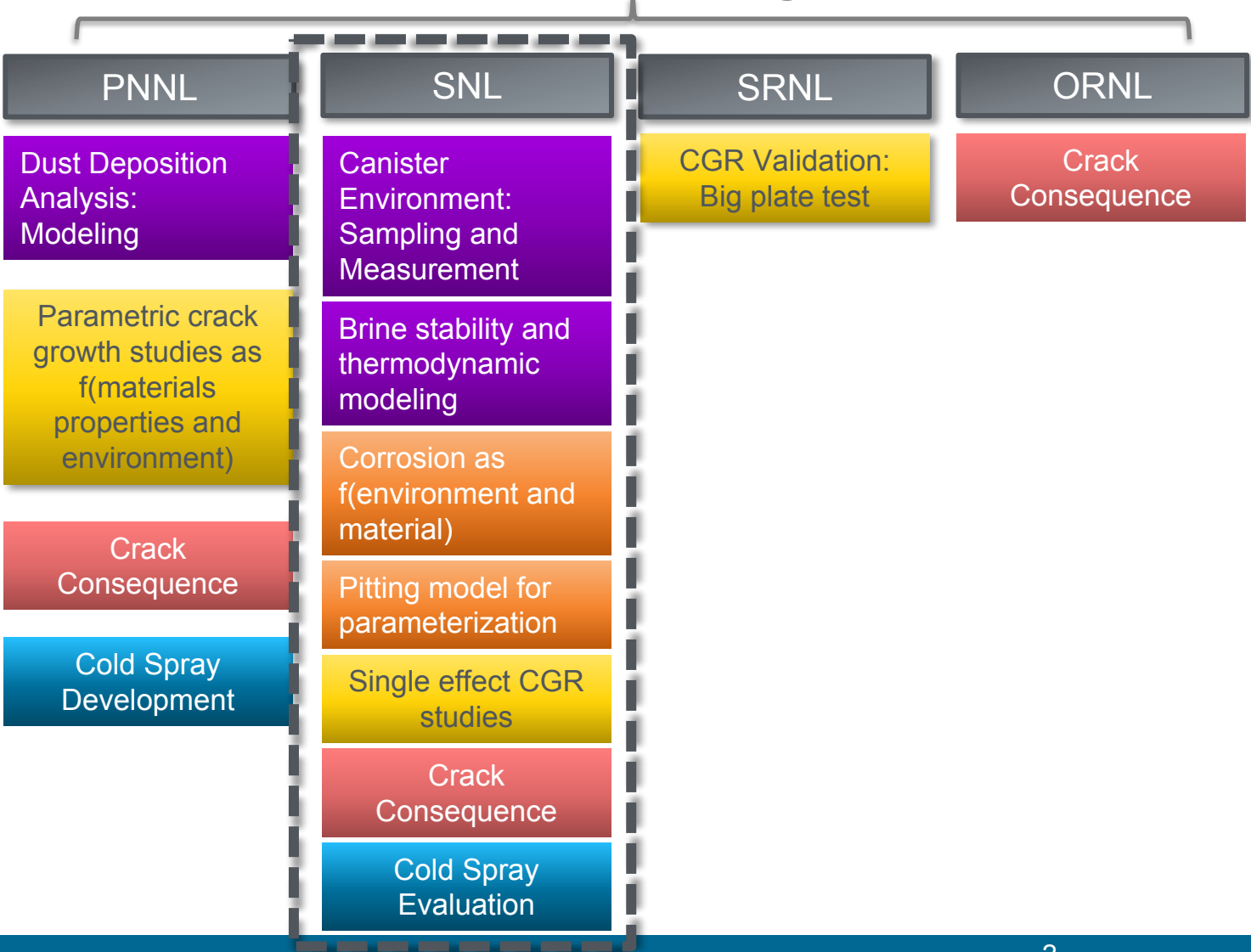
Charles Bryan, Rebecca Schaller

ESCP Fall Workshop
Virtual Meeting
November 9, 2020

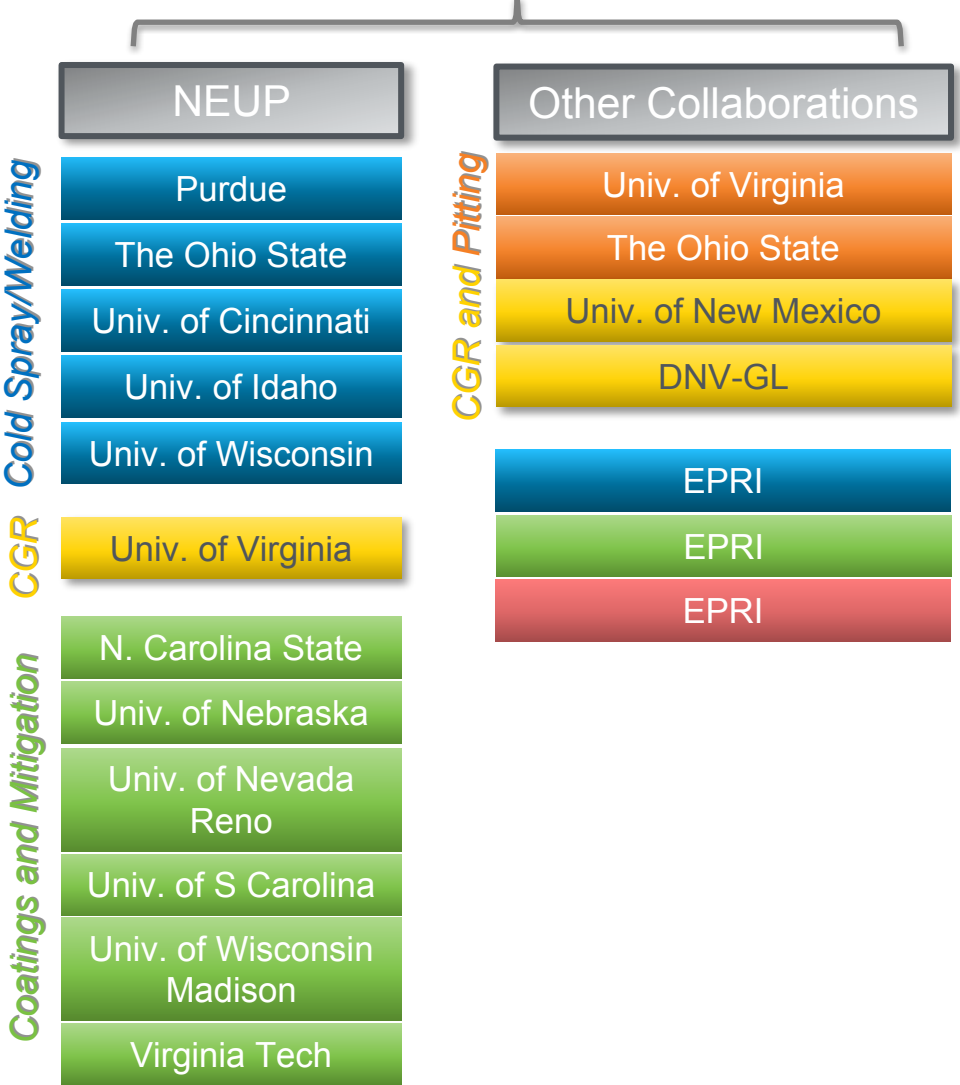
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Overview Slide: CISCC Program

DOE CISCC Program



DOE Collaborations



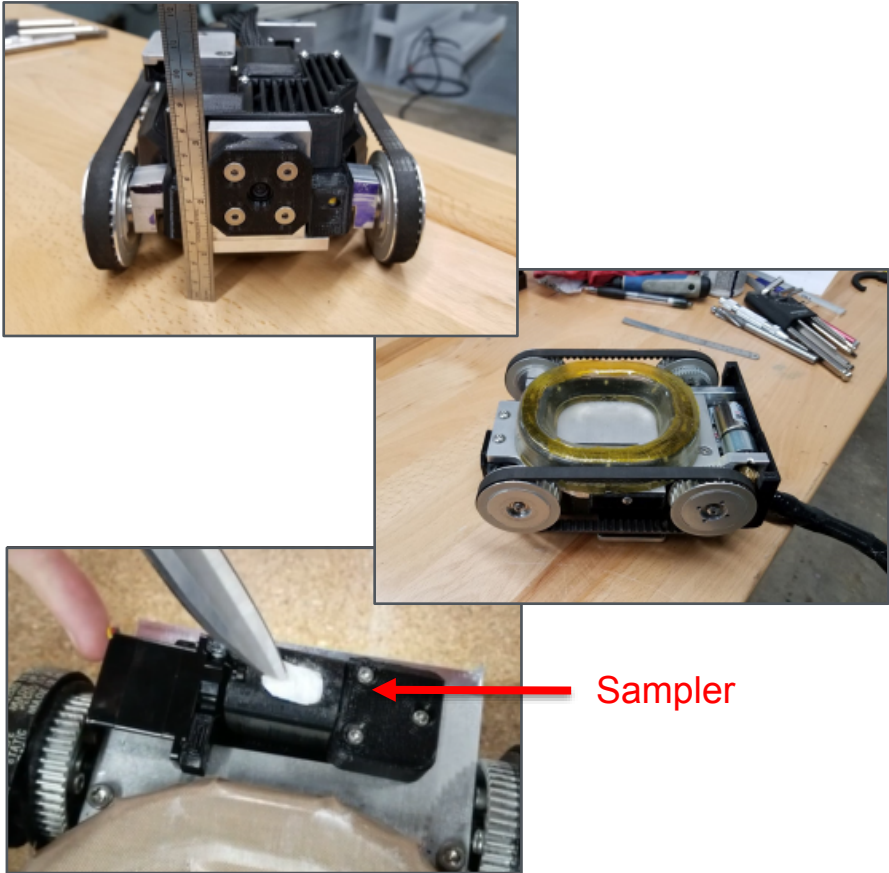
ISFSI Site Sampling – Orano Site “A”

First dust and salt data available from an inland site.

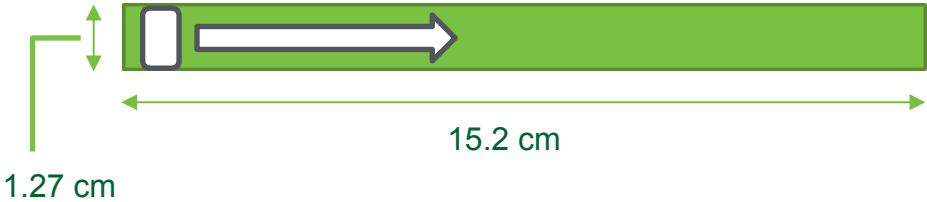
Horizontal Storage System
Sampled 12, 2, and 4 o'clock,
and above the rail.

Samples were collected using
the RTT vacuum crawler.

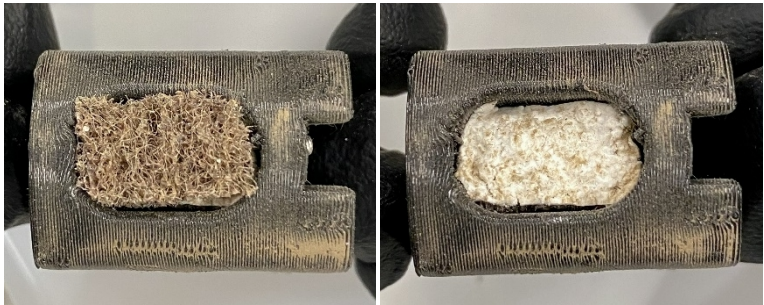
Sample #	
Block A	2 o'clock
	Above HSM rail
Block B	4 o'clock (missing filter)
	None
Block C	10 o'clock
	HSM rail - left
Block D	12 o'clock - front third
	12 o'clock - back third
Block A	
Block B	
Block C	
Block D	
Scotchbrite	Average of 3
Filter blank #1	
Filter blank #2	



Sample was collected by moving
crawler 6". Sampled area = 19.35 cm²



12 o'clock position – front third



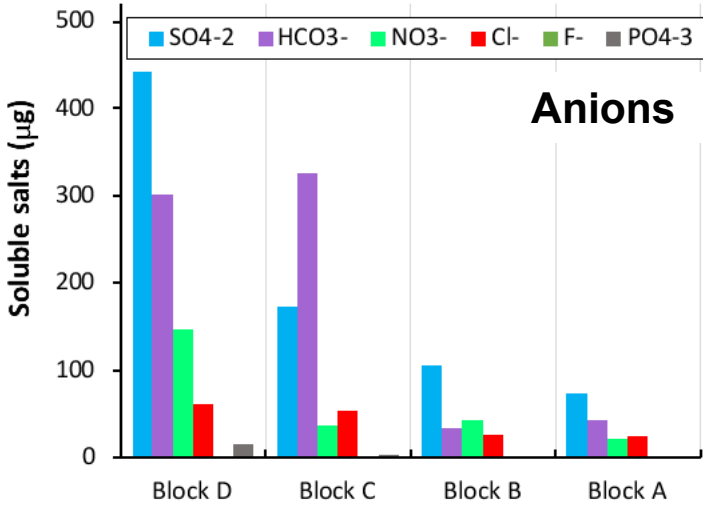
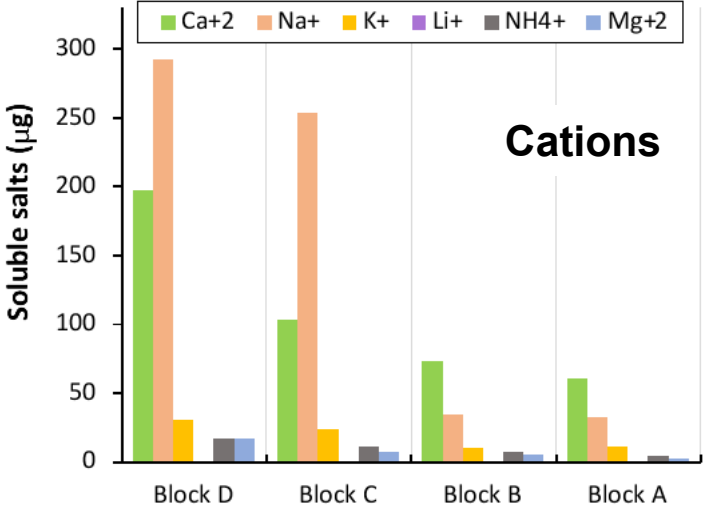
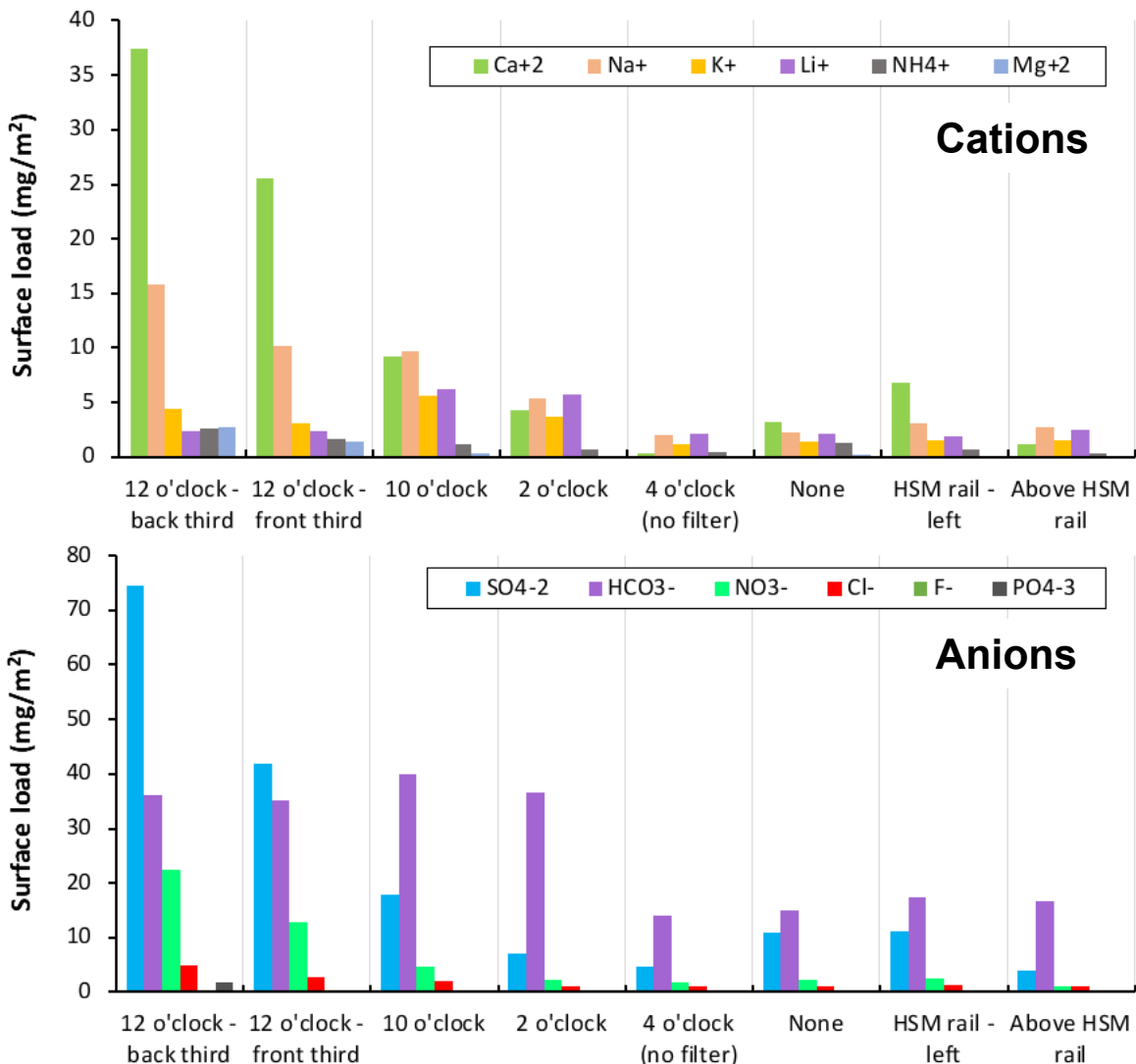
2 o'clock position



ISFSI Site Sampling – Orano Site “A”

Chemistry:

- Li leached from the Scotchbrite® pads. Not present in dust!
- Cations:
 $Ca^{+2} \gg Na^{+} > K^{+} > NH_4^{+} > Mg^{+2}$
- Anions:
 $SO_4^{-2} > HCO_3^{-} \gg NO_3^{-} > Cl^{-}$
- Chloride concentrations all < 5 mg/m²



Samples

Blocks

Definition of Canister-Relevant Testing Environments

Testing to date:

- Sea-salts or individual sea-salt components
- Isolated or coalesced droplets on metal surface (corrosion tests) *or* immersed conditions (SCC testing)
- Constant T and RH

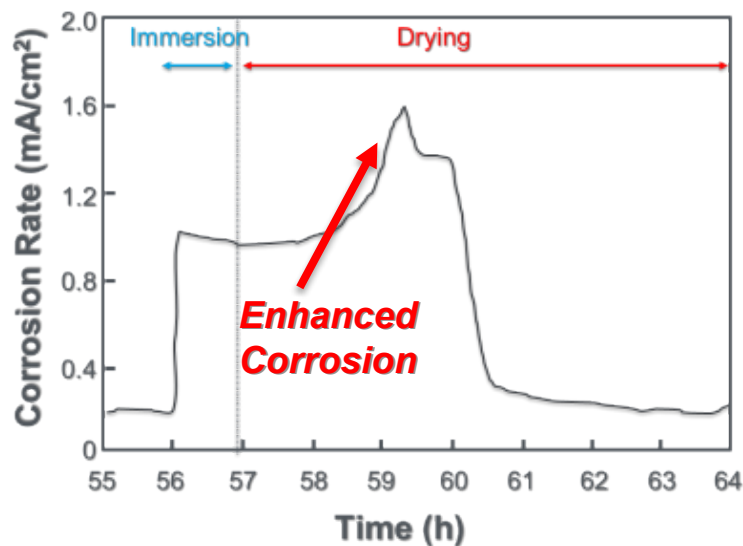
Canister-relevant testing environments:

- Diurnal cycles in T and RH
- More complex salt chemistry, even at near-marine sites (e.g., presence of nitrate)
- Presence of inert mineral grains (most abundant grains in dust, even at near-marine sites)

Definition of Canister-Relevant Testing Environments

Why significant? → Potential Influence on Corrosion:

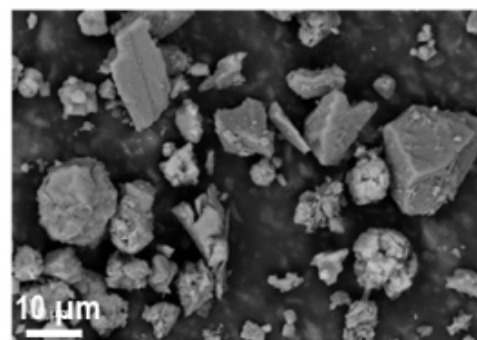
Diurnal Cycles



Changes in the corrosion rate, i_{corr} and potential during a wet/dry cycle of carbon steel.¹

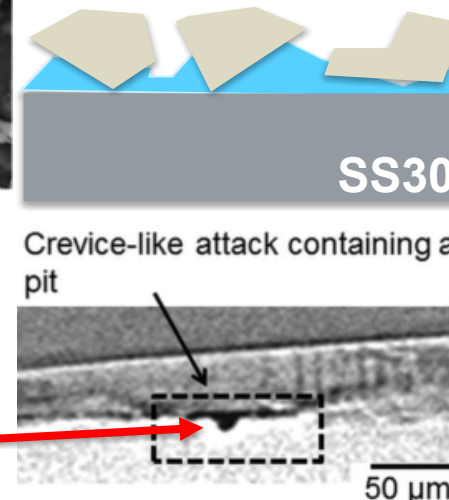
Corrosion rate increases upon initial drying (highly concentrated brine)

Dust/Precipitates



Dust at Diablo Canyon

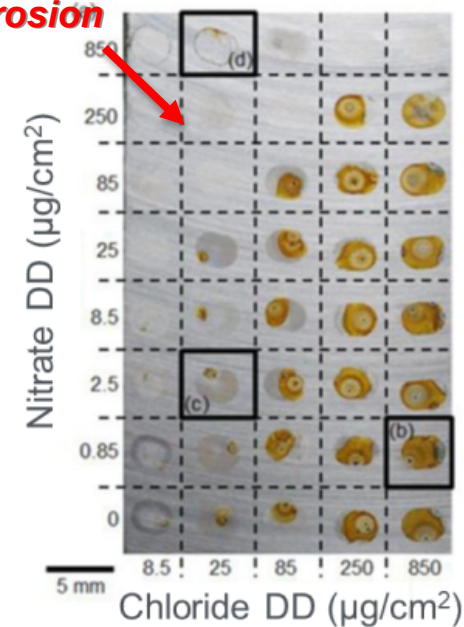
Dust may act to spread water layer/enhance corrosion



Observation of crevice-like on a SS304 sample with surface deposits²

Chemistry

Inhibited Corrosion



304L plate with mixed droplets of $MgCl_2 + Mg(NO_3)_2$.³

Other chemistries may mitigate corrosion

¹ Nishikata, A., Yamashita, Y., Katayama, H., Tsuru, T., Tanabe, K., & Mabuchi, H. (1995). *Corrosion science*, 37(12), 2059-2069.

² Guo, L., Mi, N., Mohammed-Ali, H., Ghahari, M., Du Plessis, A., Cook, A., ... & Davenport, A. J. (2019).

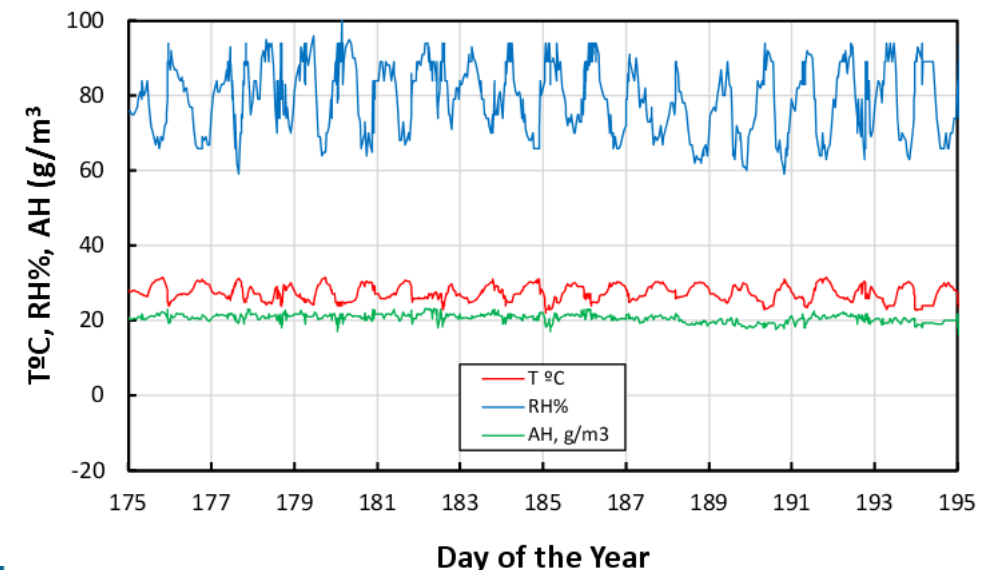
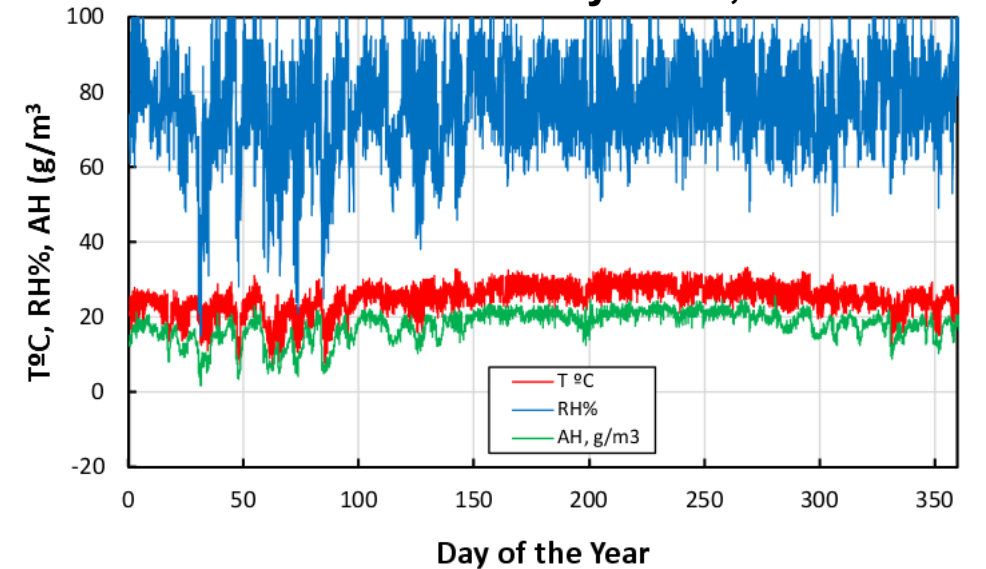
³ Cook, A. J., Padovani, C., & Davenport, A. J. (2017). *Journal of The Electrochemical Society*, 164(4), C148.

Diurnal Cycles in Temperature and RH

Evaluated ambient weather data representing several ISFSI sites. Daily cycles in T and RH vary with location, but show great similarities:

- Diurnal cycles are very regular, especially during summer months.
- T and RH strongly correlate, with $\uparrow T = \downarrow RH$.
- Absolute humidity (AH) varies significantly over seasonal cycles, but little over a day-night period

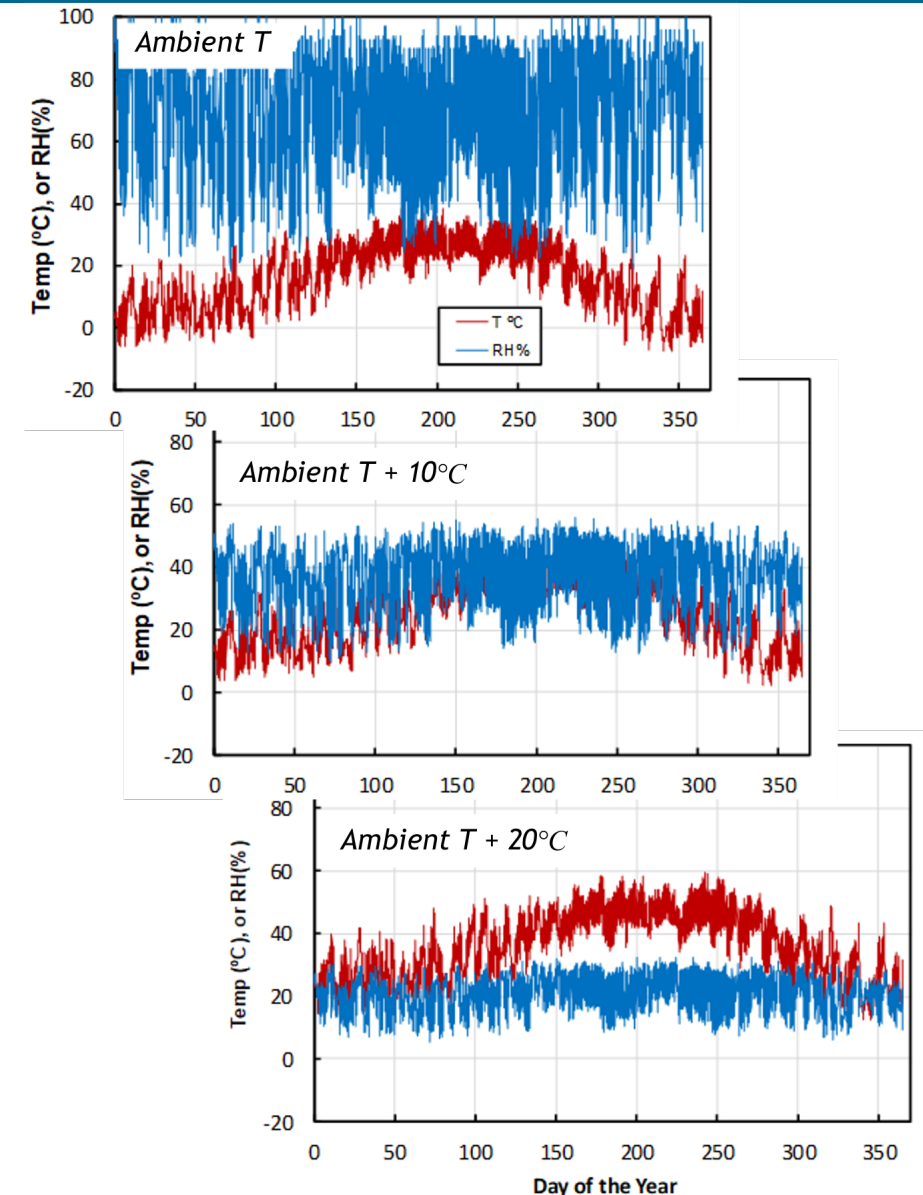
Weather at Turkey Point, FL



Diurnal Cycles in Temperature and RH

Daily cycles in T and RH are reflected on the canister surface, but offset due to heat load from the fuel.

- Calculate canister surface RH using ambient AH and canister surface T, using the water equation of state of Wagner and Pruß (2002)*
- Overall results—Small increases in canister temperature correlate with:
 - Lowering of canister surface RH relative to ambient RH
 - Narrowing of the RH band



* Wagner W. and Pruß A. (2002). "The IAPWS formulation 1995 for the thermodynamic properties of ordinary water substance for general and scientific use." *Journal of Physical and Chemical Reference Data* 31(2): 387-535.

Diurnal Cycles in Temperature and RH

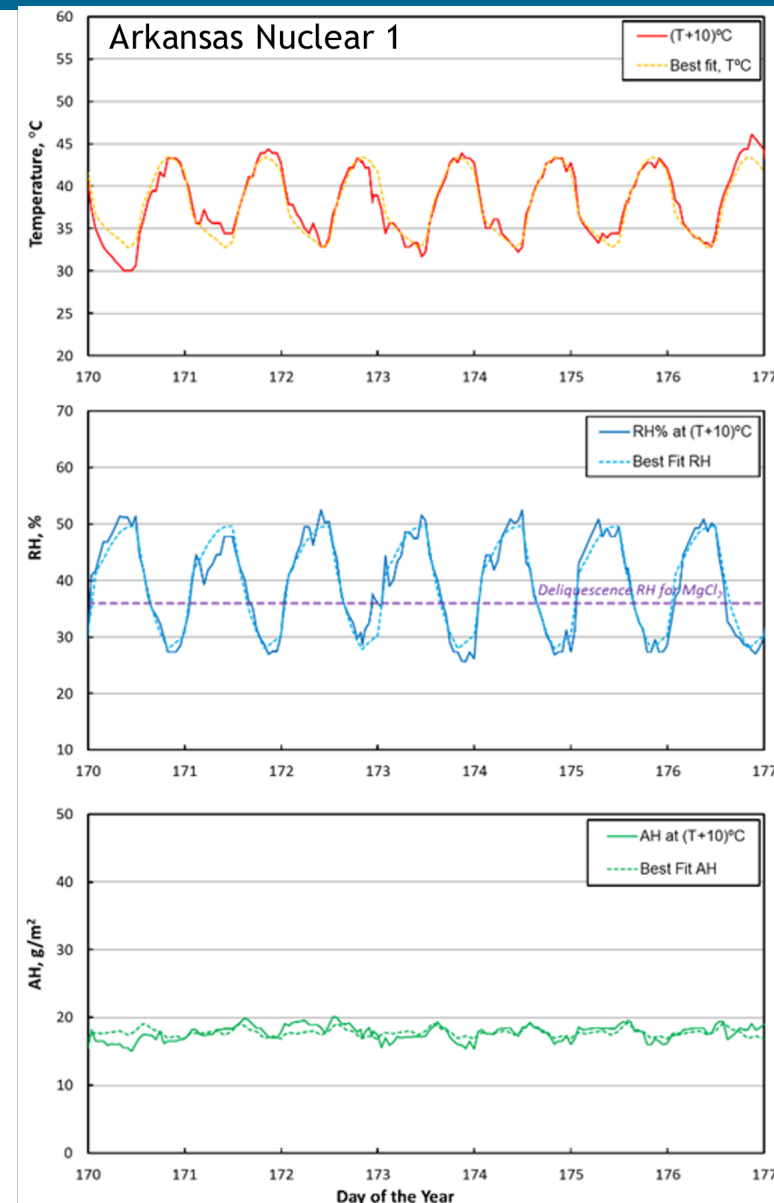
RH value of interest: 35% RH, the DRH for bischofite

- Selected AR-1 data as showing the largest diurnal variation in RH.
- Selected a ΔT of 10°C to best bound the bischofite DRH
- Derived a best-fit 12-step T/RH cycle that best fits calculated T, RH data
- Tested cycle to ensure it could be implemented: large simultaneous changes in T and RH could result in transients. No transients.

Best-fit diurnal cycle that crosses the bischofite DRH

These are relevant testing conditions, that will eventually apply to all canisters. The same calculation was carried out for the conditions of NaCl deliquescence, but they are not relevant for testing, because...

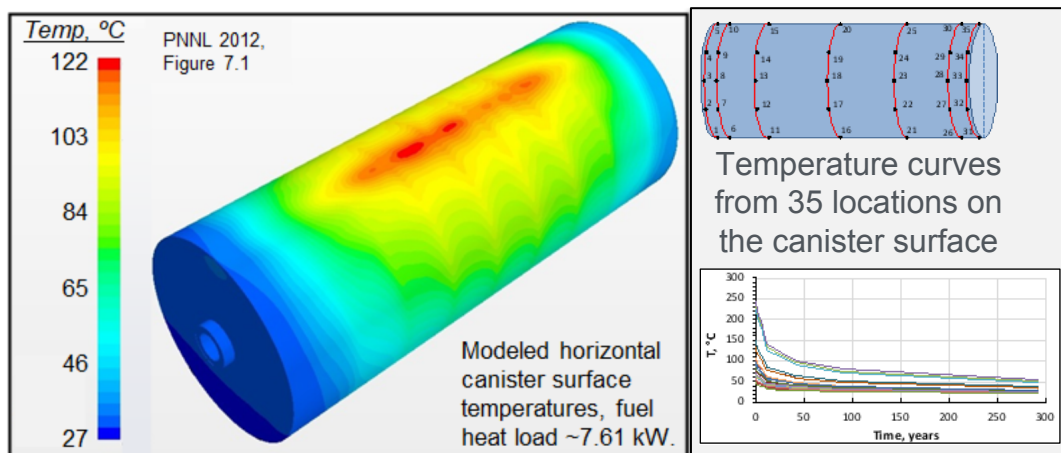
Hour	Temp. °C	RH, %
2	41.68	30.33
4	36.45	41.68
6	35.27	43.92
8	34.35	46.69
10	33.69	48.68
12	32.74	49.54
14	33.44	49.57
16	38.24	40.98
18	40.55	34.62
20	42.69	30.62
22	43.51	27.82
24	42.97	29.15



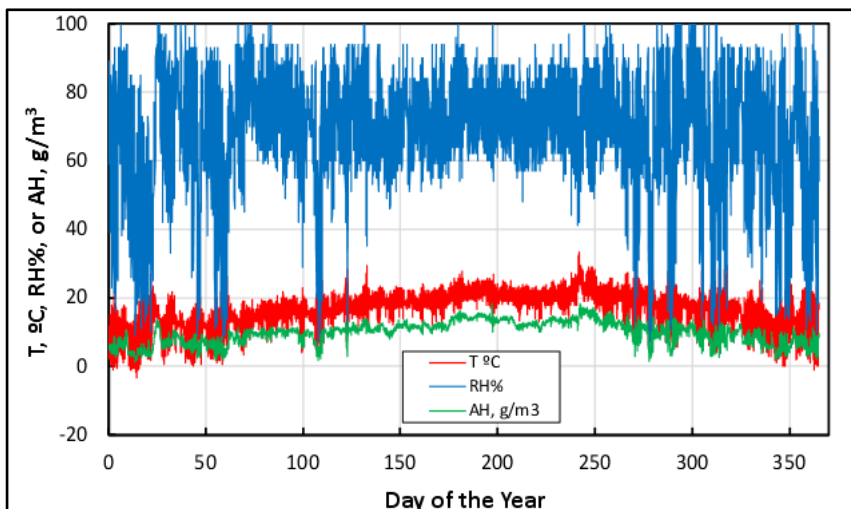
Diurnal Cycles in Temperature and RH

...the deliquescence RH for bischofite is reached in 10-20 years at some locations on the canister surface, but the DRH for NaCl is not reached for hundreds of years at any location

Canister thermal data

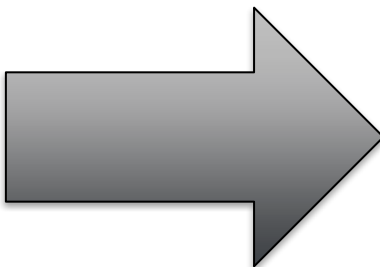


Weather data



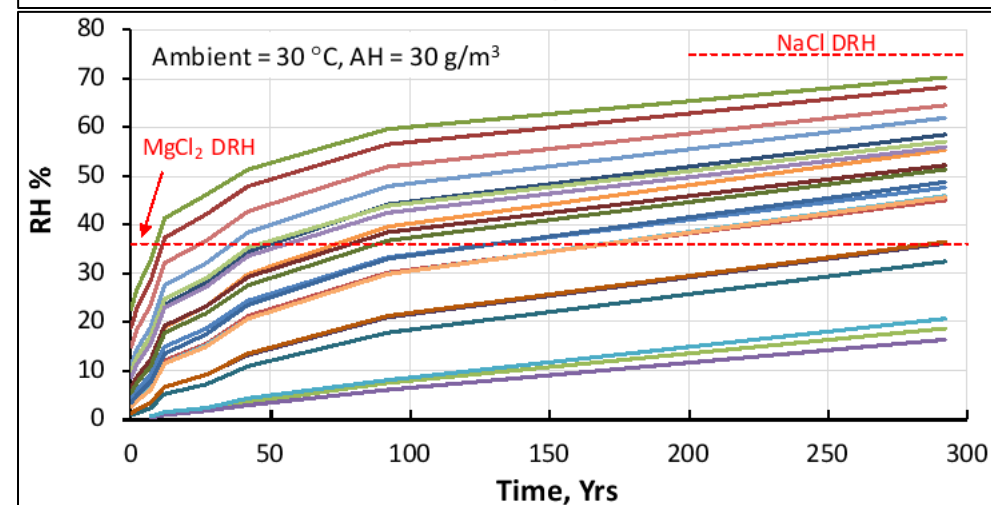
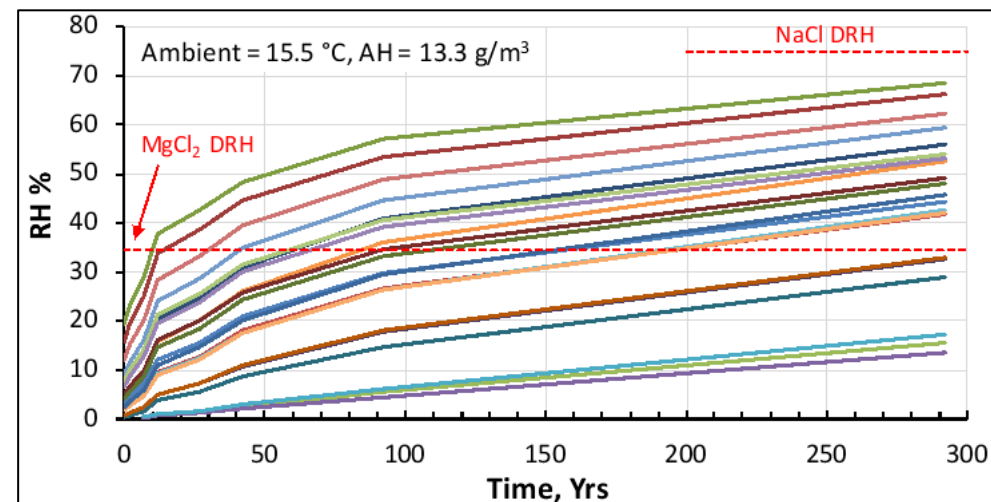
Base-case thermal model

- Ambient air T = 60°F (15.5°C)
- Max. AH = 13.3 g/m³



Base-case model +14.5°C to match observed field AH

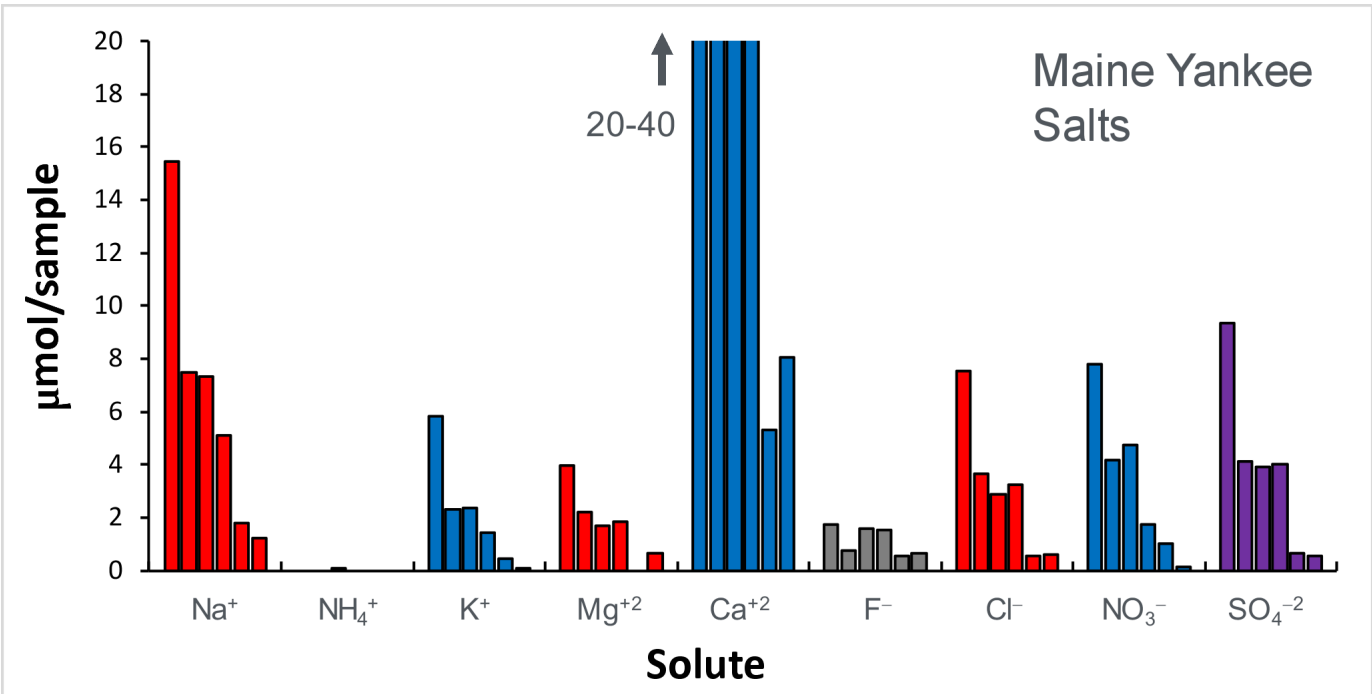
- Ambient air T = 86°F (30°C)
- Max. AH = 30 g/m³



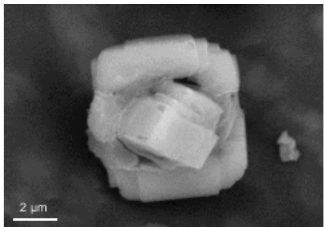
Soluble Salt Chemistry

While salts in dust collected from Diablo Canyon ISFSI appear to be dominantly sea salts, soluble salt compositions at East Coast sites differ significantly from sea-salts

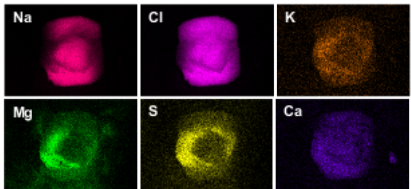
- Significant contribution from continental salts (relatively enriched in Ca, K, SO₄, NO₃, sometimes NH₄).
- Effect of sea salt particle-gas conversion reactions (reactions with SO₂, NO_x convert chlorides to nitrates, sulfates)



Sea-salt aerosols from Diablo Canyon ISFSI



Diablo Canyon salt aggregates: dominantly NaCl with interstitial MgSO₄ and trace K, Ca phases. Consistent with seawater ion compositions.



Normalized salt composition

Species		Normalized molar conc.
Species	Normalized molar conc.	
Na ⁺	1.0000	
K ⁺	0.3516	
Ca ²⁺	4.8576	
Mg ²⁺	0.2655	
Cl ⁻	0.4838	
NO ₃ ⁻	0.5223	
SO ₄ ²⁻	0.5985	
HCO ₃ ⁻	*9.3947	

* Based on charge balance

* Based on charge balance

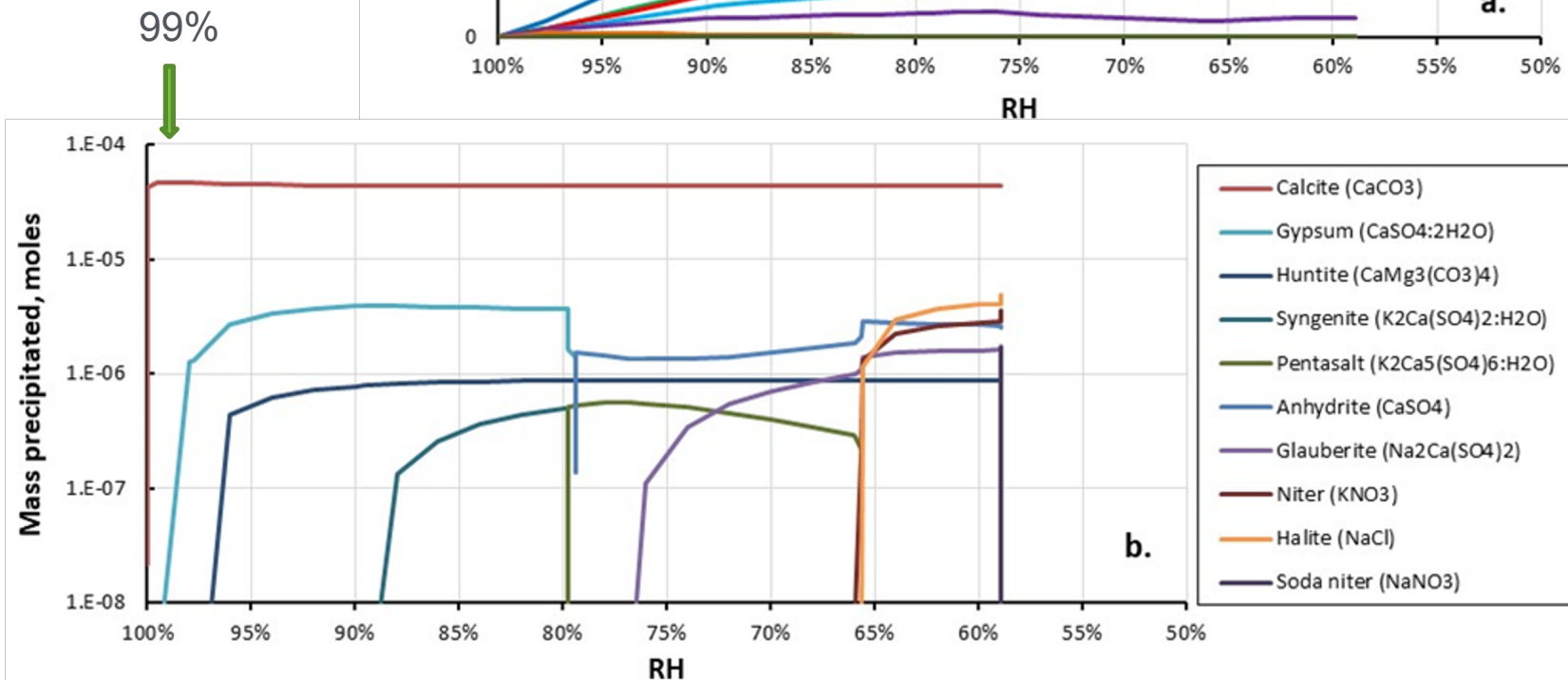
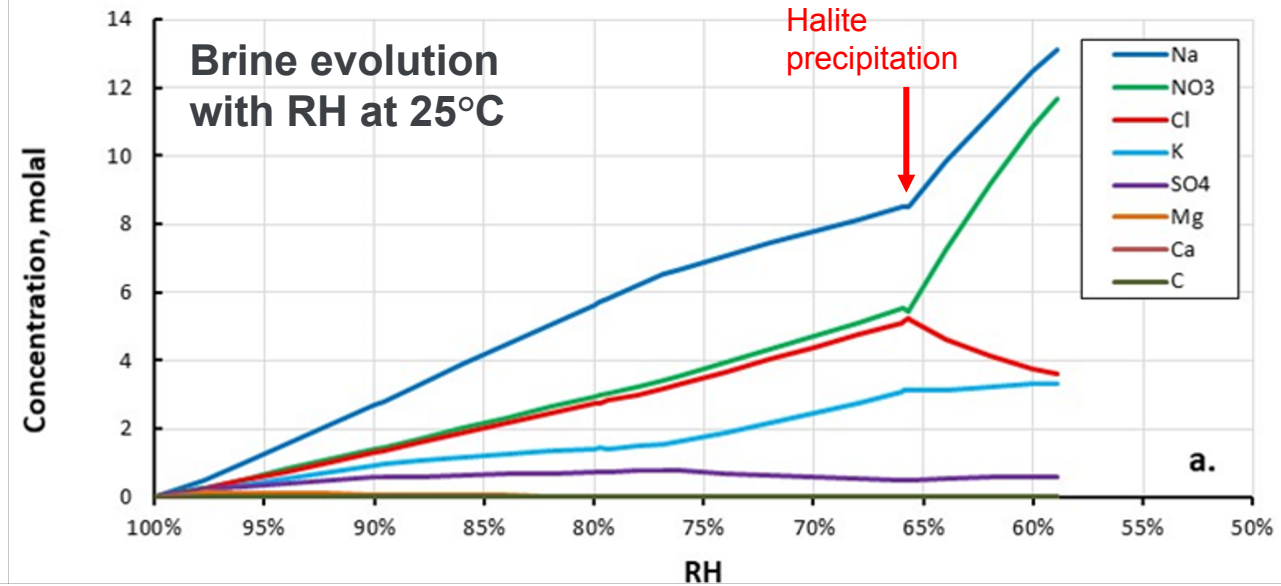
Use Maine Yankee data to produce a normalized salt composition

Soluble Salt Chemistry

Goal—identify a brine composition that can be deposited as aerosols on samples for atmospheric corrosion testing.

Method—use EQ3/6 and Pitzer database to simulate evaporation of the identified salt composition. Target composition—0.2-0.4 molal ($\approx 99\%$ RH). Brine must be stable as a liquid (*no precipitates!*)

Problem: Using normalized salt composition, salts precipitate at low degrees of evaporation (0.003 molal)



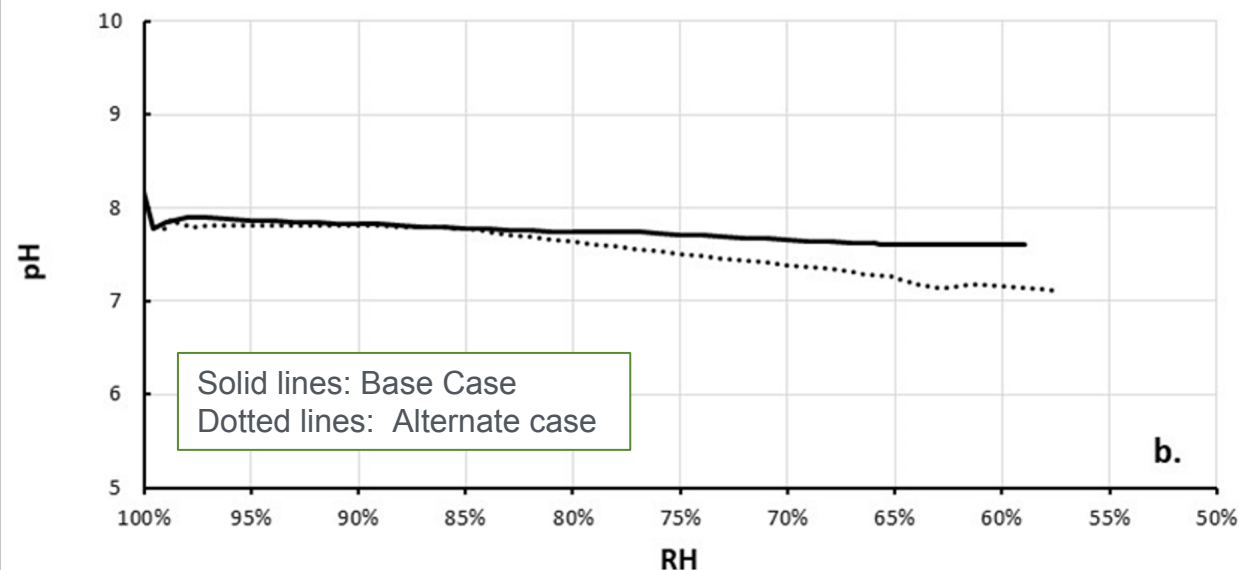
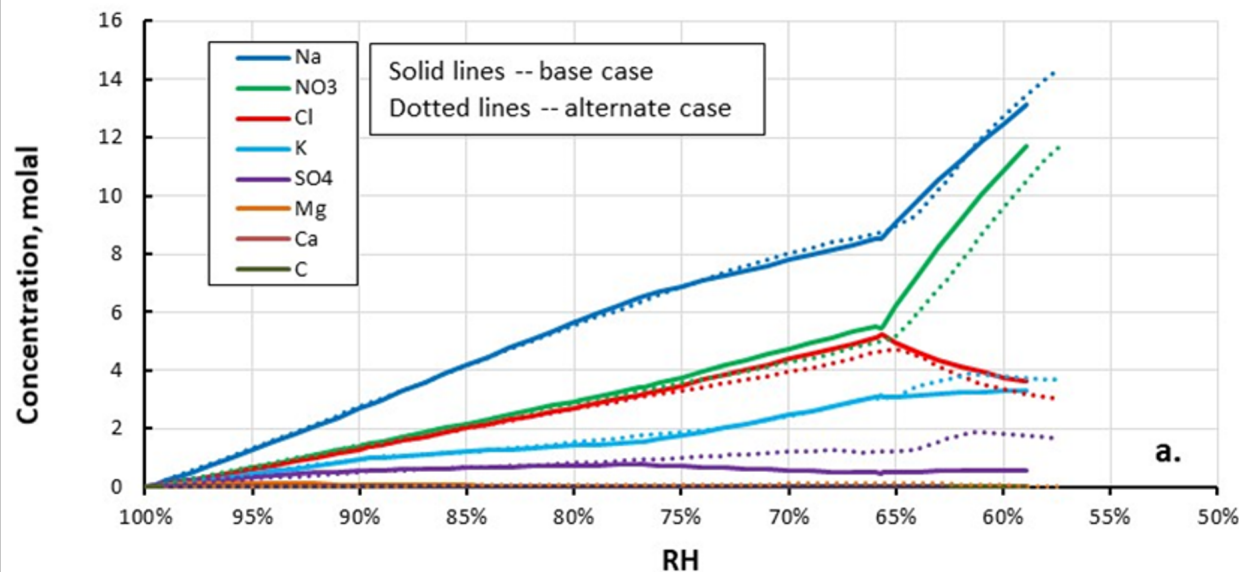
Soluble Salt Chemistry

Goal—identify a brine composition that can be deposited as aerosols on samples for atmospheric corrosion testing.

Solution—Subtract solution components to achieve necessary concentrations without precipitation, while affecting brine evolution as little as possible. *Brine composition evolves similarly to original solution; no precipitation at 99% RH (0.4 molal).*

Brine composition to use:

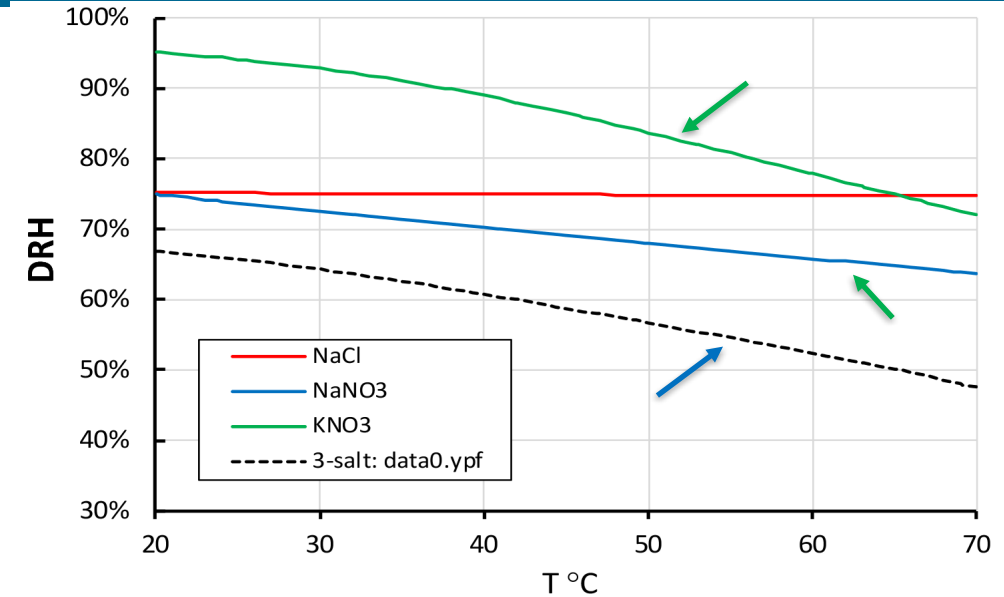
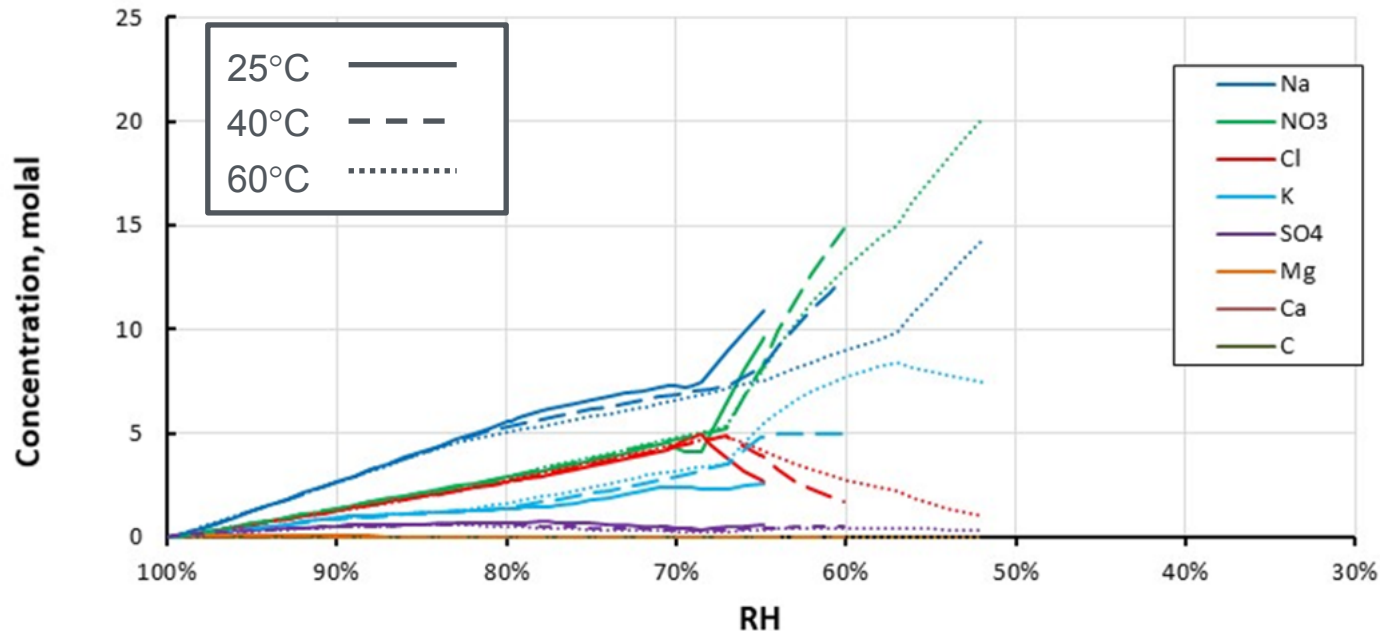
Species	Conc., molal	To mix:	
		Salt	Wt, grams
Na ⁺	2.417E-01	NaCl	5.3590
K ⁺	8.499E-02	NaNO ₃	3.5070
Ca ⁺²	9.416E-03	KNO ₃	8.5929
Mg ⁺²	3.209E-03	CaCl ₂	1.0450
Cl ⁻	1.169E-01	MgCl ₂ ·6H ₂ O	0.6524
NO ₃ ⁻	1.263E-01	Na ₂ SO ₄	7.6789
SO ₄ ⁻²	5.406E-02	NaHCO ₃	0.0543
HCO ₃ ⁻	6.467E-04	SUM	26.8896



Soluble Salt Chemistry

Deliquescence properties of the identified salt assemblage: *Necessary to determine range of relevant testing conditions*

- Solubility of nitrate salts increases significantly with temperature, so the DRH drops.
- DRH of the predicted salt assemblage decreases with increasing temperature
- Concentration of deliquescent brine increases as temperatures increase



Conclusions

- Identified a brine composition for use in atmospheric testing.
- Duplicating field conditions requires not only matching Cl/NO₃ ratios of the starting salts, but also incorporation of minor species that play a large role in buffering the brine pH.
- Presence of nitrate can greatly affect the deliquescence RH and possible range of testing conditions (T, RH).

Inert Dust Effects

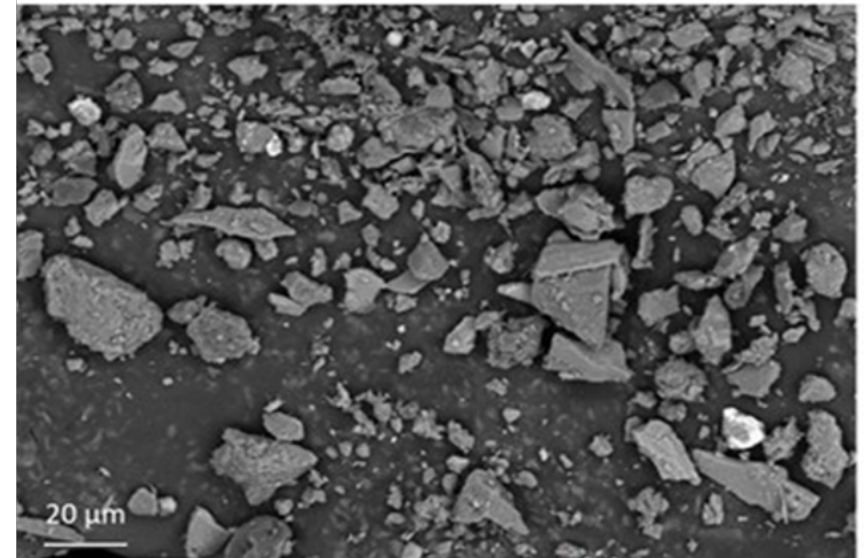
Diagenetic mineral fragments (quartz, aluminosilicates, carbonates) are the most abundant dust particles on canister surfaces; plant matter (e.g., pollen) can also be common. Salts are a minor component.

Possible effects of inert minerals:

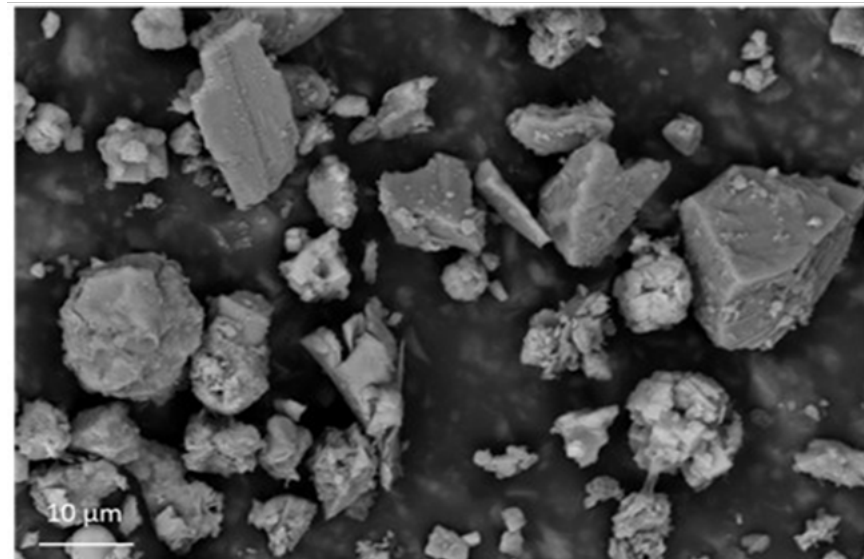
- Brine spreading via capillary processes—development of a larger cathode
- Crevice corrosion, in occluded regions under larger grains

To evaluate the potential *physical* effects of inert dust minerals, we characterized dust particle sizes, and will perform corrosion tests using sea-salts and inert mineral particles of representative sizes.

Hope Creek



Diablo Canyon



Inert Dust Effects

Procedure: Determine dust size distributions from SEM images of dust collected from in-service canisters (sampling bias towards smaller particles). Evaluated dust from four sites:

Hope Creek ISFSI (New Jersey)

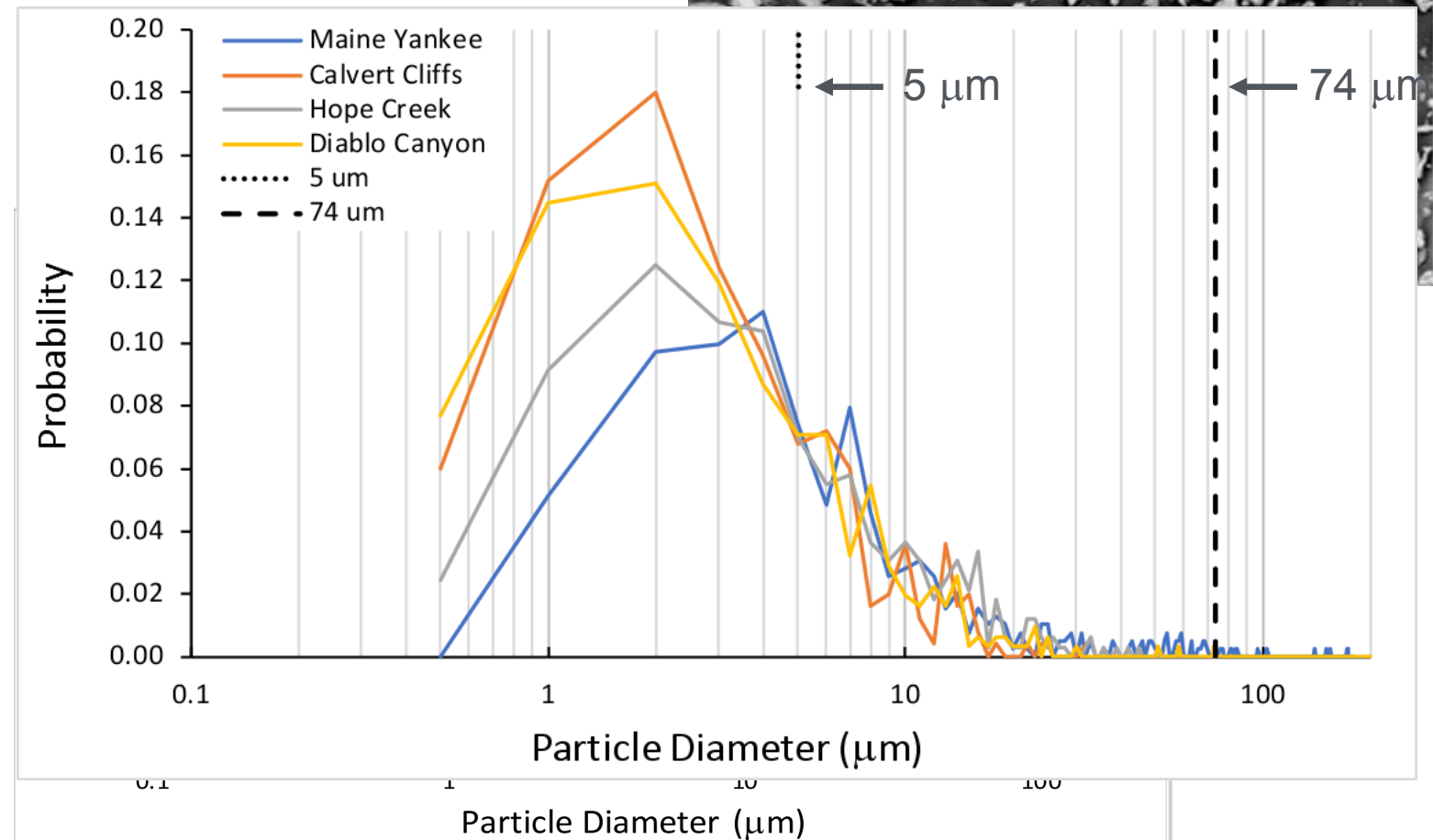
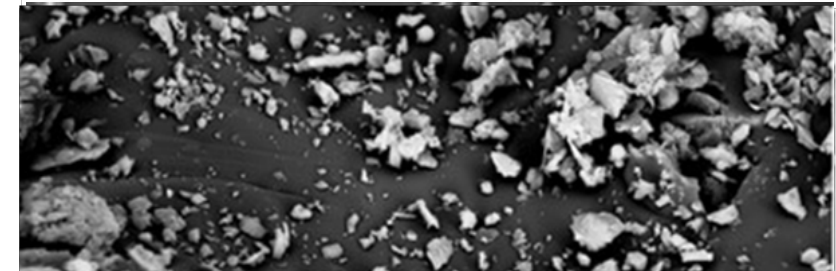
Calvert Cliffs ISFSI (Maryland)

Diablo Canyon ISFSI (California)

Maine Yankee ISFSI (Maine)

For testing purposes:

- Inert mineral – **quartz**
- Fine particles to evaluate capillary brine spreading: **5 μm Min-U-Sil quartz**
- Coarse particles to evaluate crevicing: **74 μm (200 mesh) Sil-Co-Sil quartz**
- **Mixed 5 μm /74 μm to evaluate coupled effects**



Pitting Exposures in the Defined Environments

- Current Status:
 - Cyclic exposures in-progress
 - Dust exposures under calibration
 - Mixed chemistry exposures in development

Cyclic Exposure Test Plan:

Sample	Seawater Deposition	Surface Finish	Cycle		Exposure Time (weeks)						Total Sam.
	µg/cm ²	Grit/polish	Site	0	1	2	4	26	52	78 / 104	
304H	300	120	Arkansas Nuclear 1	2	3	3	3	3	3	3	20
304H	300	1200	"	2	3	3	3	3	3	3	20
304L	300	120	"	2	3	3	3	3	3	3	20
304L	300	1200	"	2	3	3	3	3	3	3	20
316L	300	120	"	2	3	3	3	3	3	3	20
316L	300	1200	"	2	3	3	3	3	3	3	20
Total:				12	18	18	18	18	18	18	120

**In-progress, pulled exposure times to 4 weeks*

- Objective:
 - Gain pitting statistics across more relevant environments
 - Inform better the potential influences on corrosion and SCC initiation

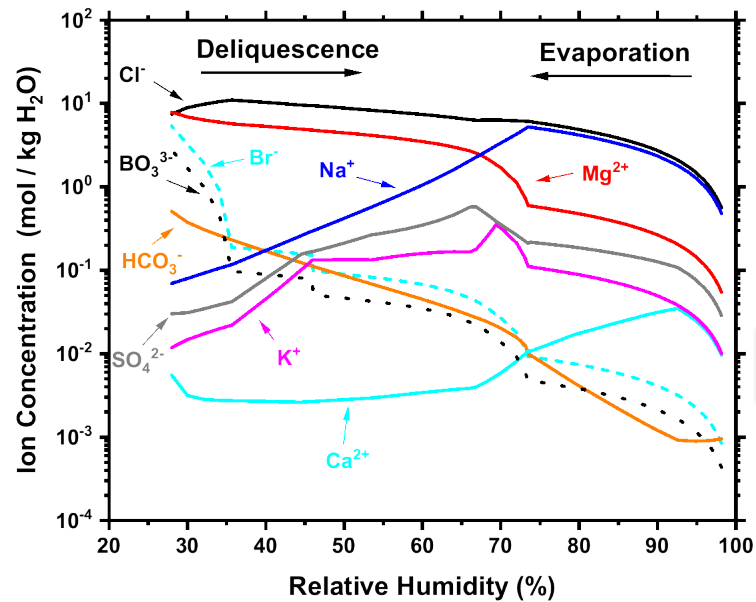
Dust Exposure Test Plan:

Coupon Size	Total	5.0 µm	74 µm	Mix	No Dust	1 month	6 month	12 month	24 month	Notes
8x8	6	2	2	1	1	0	0	1	1	* Pull no dust and mix at 24 months
4x4	18	5	5	5	3	0	2	2	2	*Pull no dust at final three sampling intervals
2x2	67	21	21	21	4	5	5	6	6	*Pull one no dust per time interval
2x1	38	11	11	11	5	3	3	3	3	*Pull one no dust per time interval and two at 24 months
2x1 (304L, 2017 exposures)	31	9	9	9	4	2	2	3	3	*Pull one no dust per time interval
Total	160	48	48	47	17	10	11	12	15	

**Dust deposition process under calibration, exposure to be started shortly*

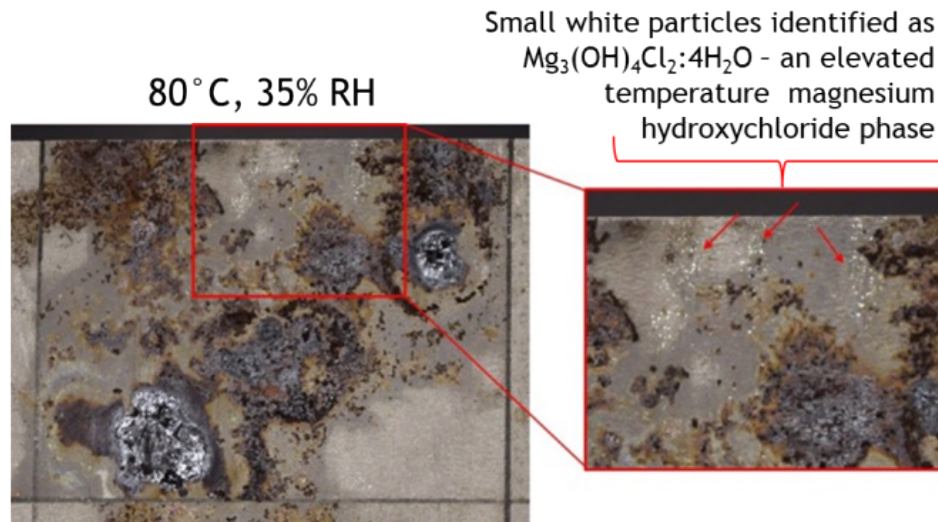
Importance of MgCl_2

What brines are likely to form on the surface?



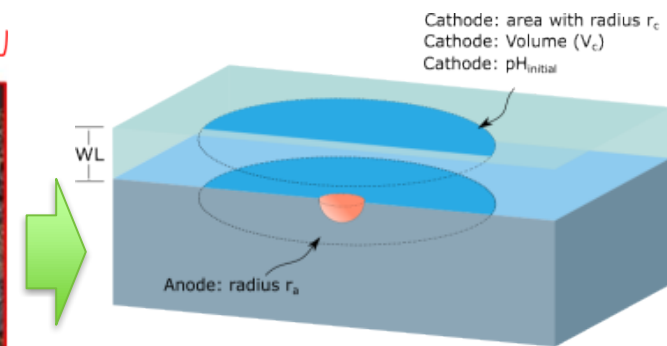
***MgCl_2 Dominated Brine
for > 300 years!***

Why is MgCl_2 Significant?



***Formation of precipitates can
lead to brine dry-out***

How do MgCl_2 brines impact corrosion?



...and SCC initiation?

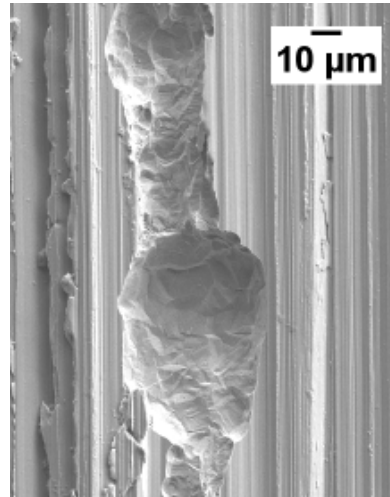
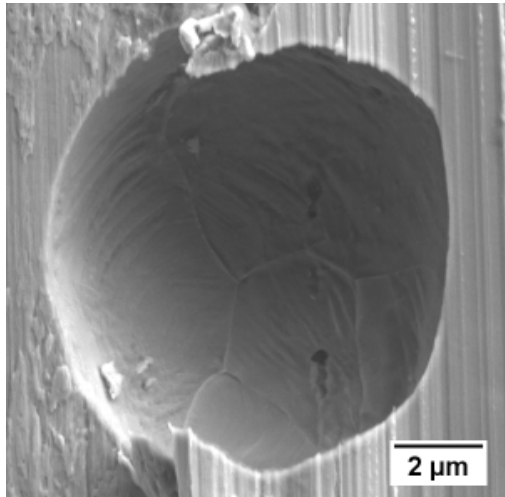
Pit Morphology

Brine composition greatly impacts resultant pit morphology...

NaCl Dominated Brines

76 %RH Seawater

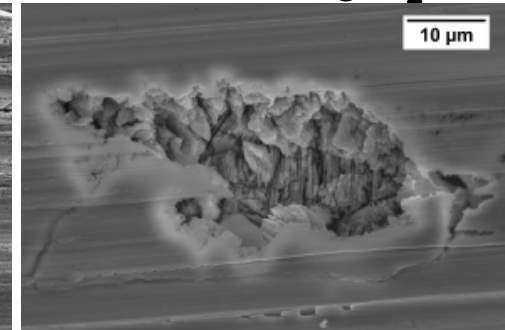
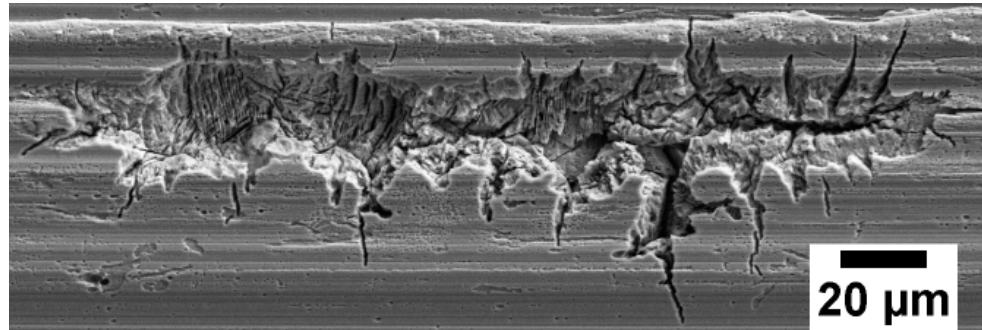
5.22 M NaCl



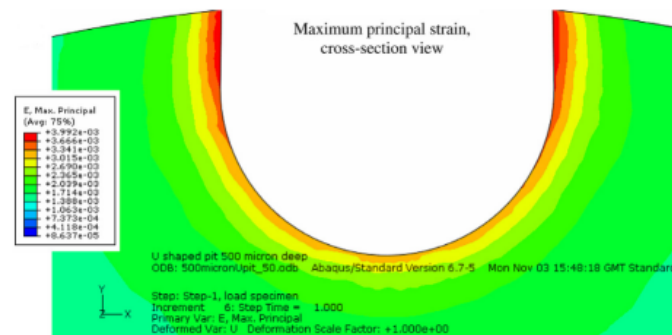
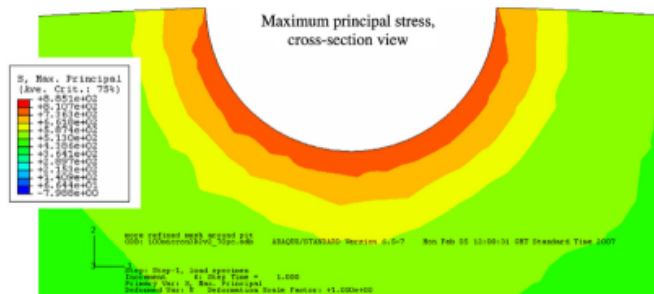
MgCl₂ Dominated Brines

40 %RH Seawater

4.47 M MgCl₂



Pits formed in MgCl₂ brines are much larger and more irregular in shape...why would this be

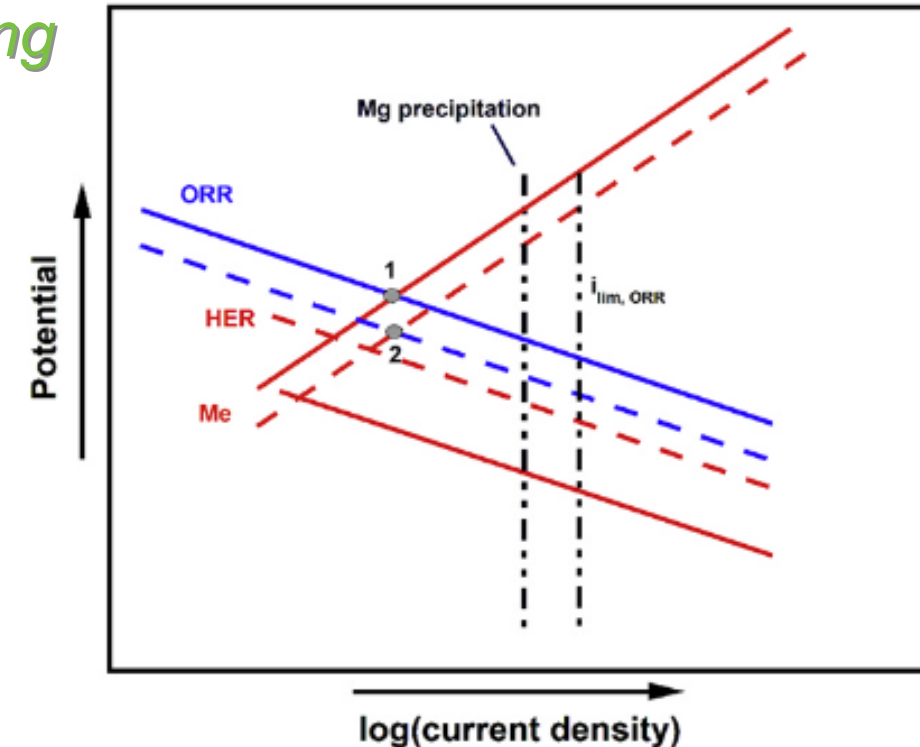
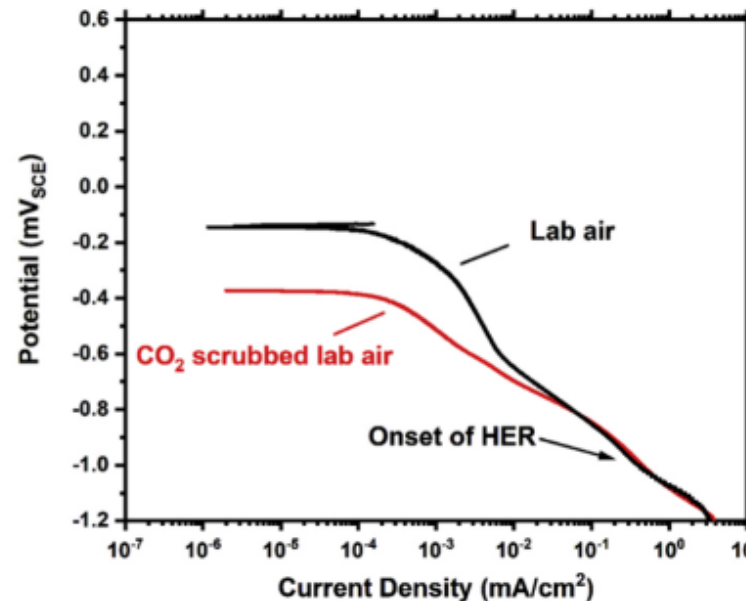
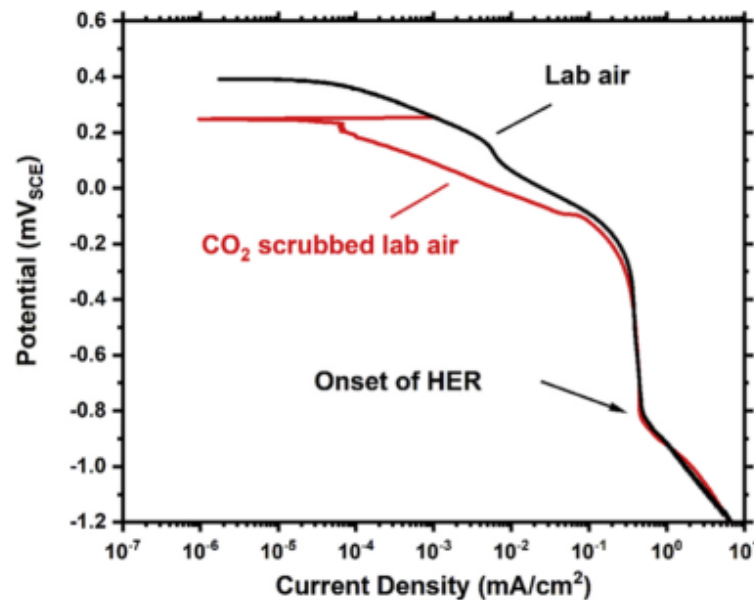


Pit geometry influences stress distribution → influences susceptibility for SCC initiation.

Cathodic Reactions

- To further understand the influence of brine composition on pit morphology we have to determine the influence on governing corrosion kinetics...
 - What is the influence of brine composition on resultant cathodic kinetics?** ...dominated by HER over ORR

Implications: H may influence near surface cracking

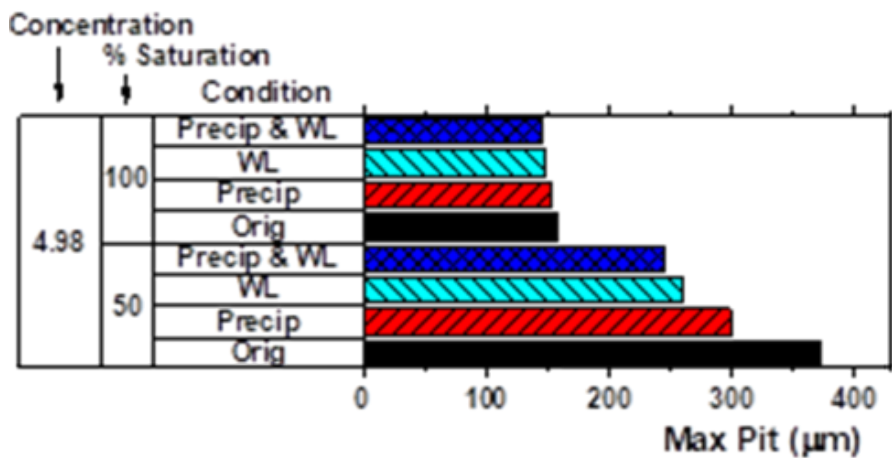


Results published in:

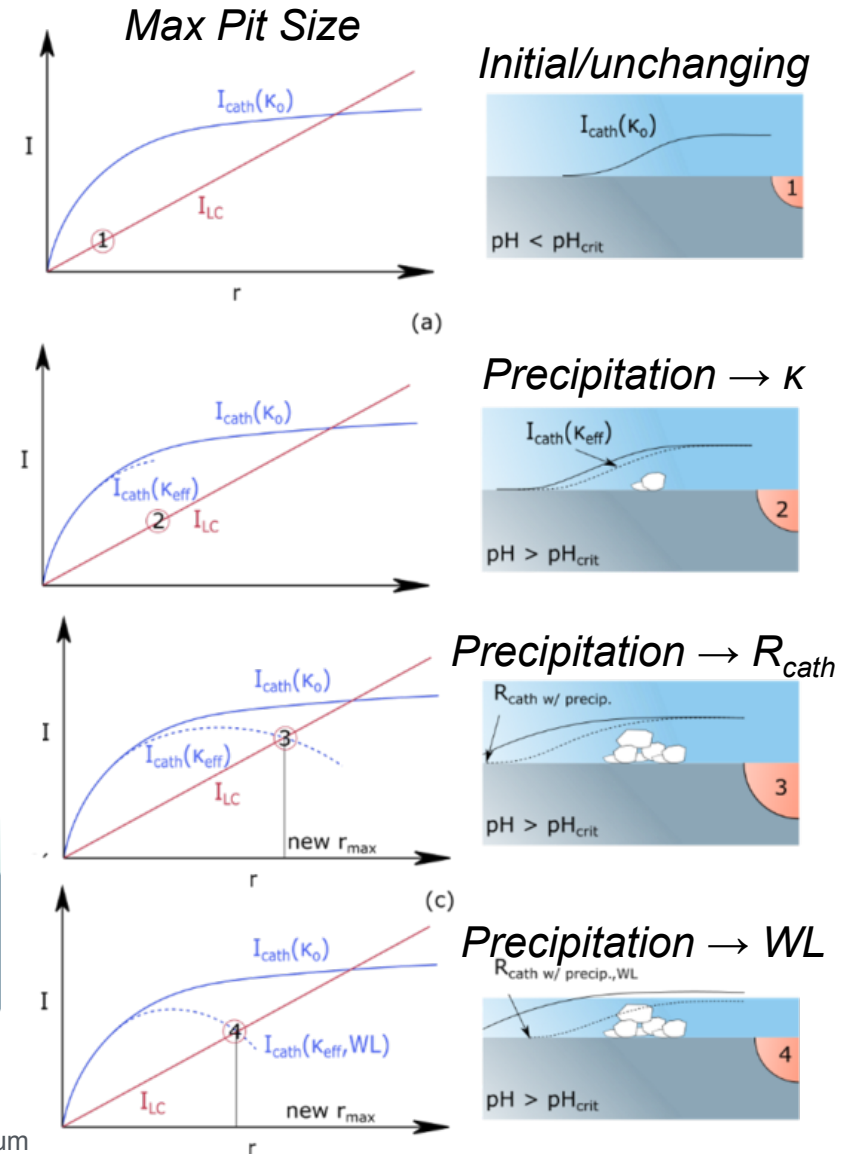
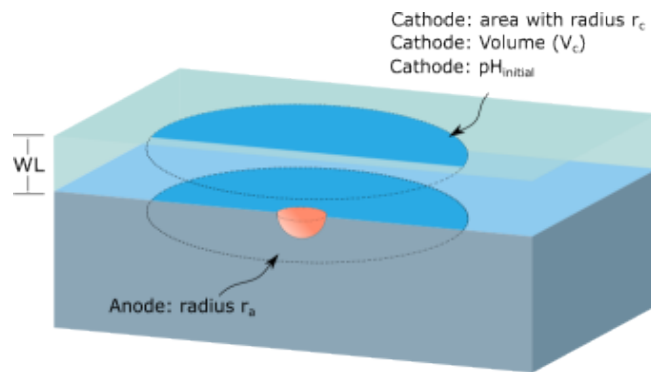
Katona, R. M., Carpenter, J. C., Knight, A. W., Bryan, C. R., Schaller, R. F., Kelly, R. G., & Schindelholz, E. J. (2020). Importance of the hydrogen evolution reaction in magnesium chloride solutions on stainless steel. *Corrosion Science*, 177, 108935.

Evolution of Cathodic Brines

- Considering cathodic precipitation in prediction calculation decreases predicted maximum pit sizes significantly



Pit Schematic



Results submitted to:

R. M. Katona, A. W. Knight, C. R. Bryan, R. F. Schaller, R. G. Kelly. Quantitative Assessment of Environmental Phenomena on Maximum Pit Size Predictions in Marine Environments. Submitted to Electrochimica Acta. 2020

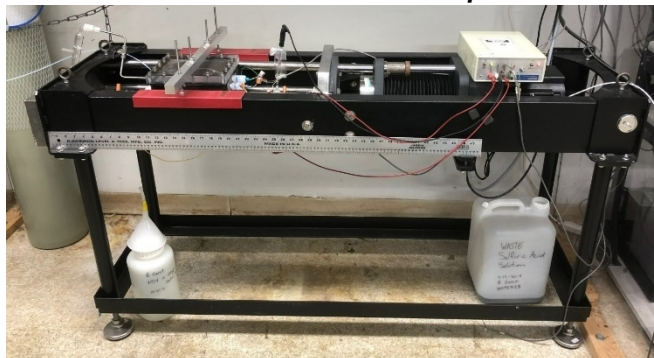
Crack Growth Rates

Vertical Setup



*Four load frames
acquired, installed,
calibrated, and
running initial tests*

Horizontal Setup

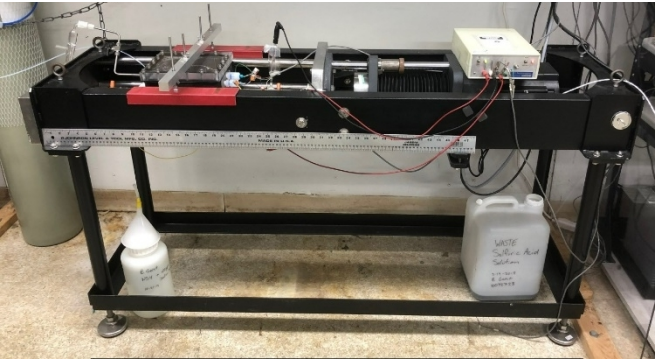


Crack Growth Rates

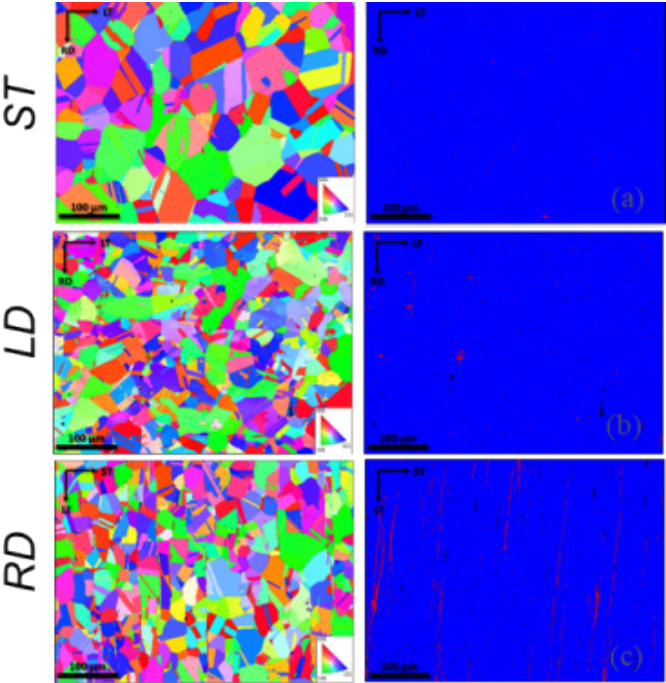
Vertical Setup



Horizontal Setup



Microstructural Characterization of 304L



304L material
characterized

Initial full immersion
environments
selected for CGR
testing:
-Temperature
-Brine Composition

Initial Full Immersion Environments for CGR Testing

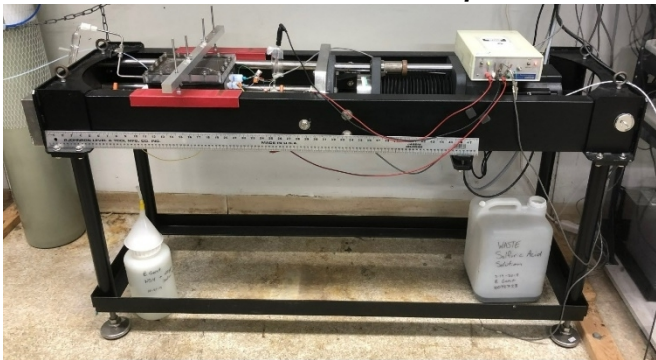
Temperature (°C)	Frequency (Hz)	Environment Type
35	10 ⁻² -10 ⁻⁹	5.3M NaCl
45	10 ⁻² -10 ⁻⁹	5.3M NaCl
55	10 ⁻² -10 ⁻⁹	5.3M NaCl
35	10 ⁻² -10 ⁻⁹	4.98 M MgCl ₂
55	10 ⁻² -10 ⁻⁵	4.98 M MgCl ₂
35	10 ⁻² -10 ⁻⁹	40% RH Seawater
35	10 ⁻² -10 ⁻⁵	75% RH Seawater

Crack Growth Rates

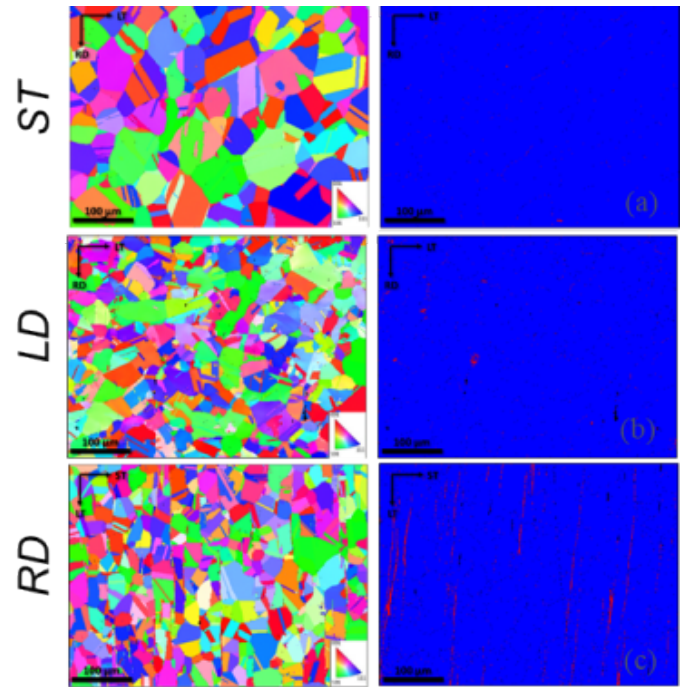
Vertical Setup



Horizontal Setup



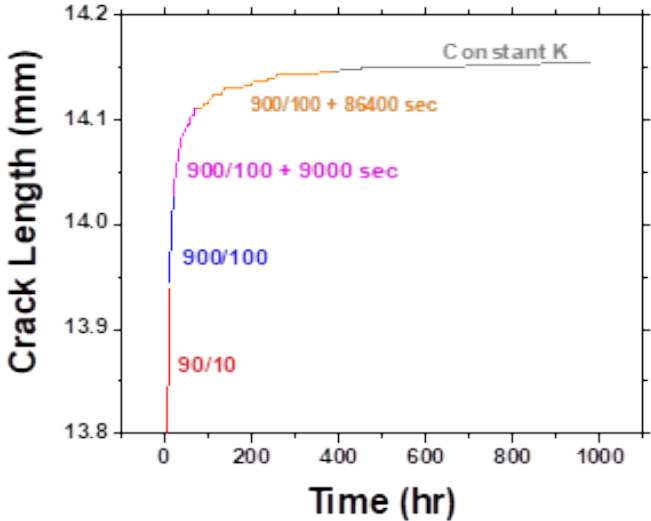
Microstructural Characterization of 304L



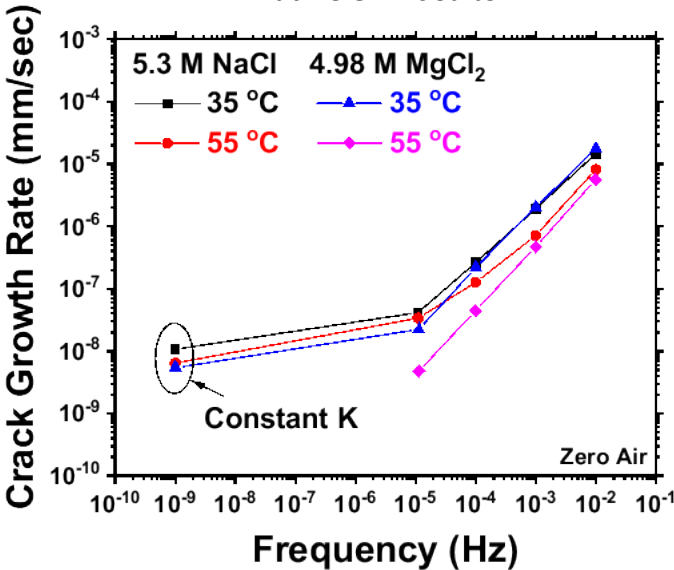
Initial Full Immersion Environments for CGR Testing

Temperature (°C)	Frequency (Hz)	Environment Type
35	10 ⁻² -10 ⁻⁹	5.3M NaCl
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Tapered approach to constant K CGR



Initial CGR results

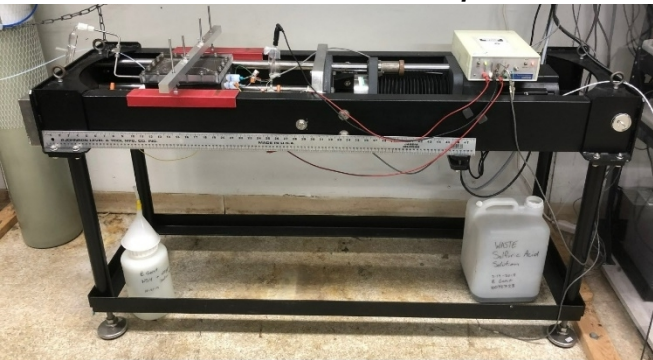


Crack Growth Rates

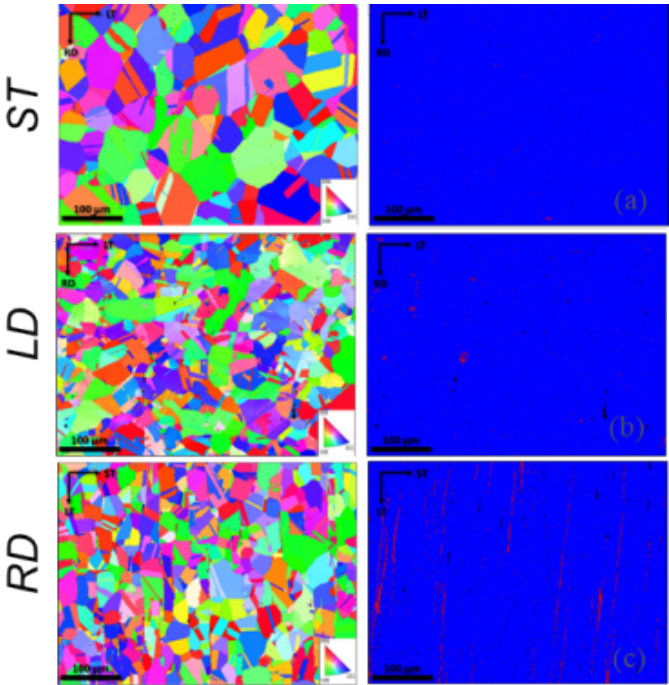
Vertical Setup



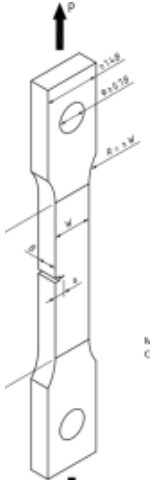
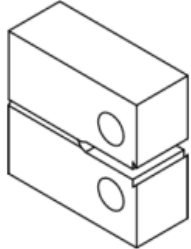
Horizontal Setup



Microstructural Characterization of 304L



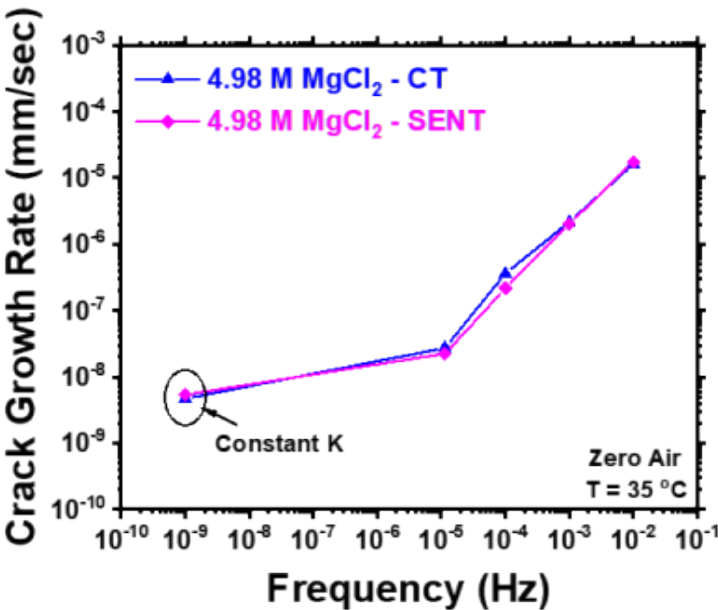
CT Sample



SENT Sample

Comparison of CT vs. SENT geometry

-SENT geometry may lend itself to atmospheric testing



Initial Full Immersion Environments for CGR Testing

Temperature (°C)	Frequency (Hz)	Environment Type
35	10 ⁻² -10 ⁻⁹	5.3M NaCl
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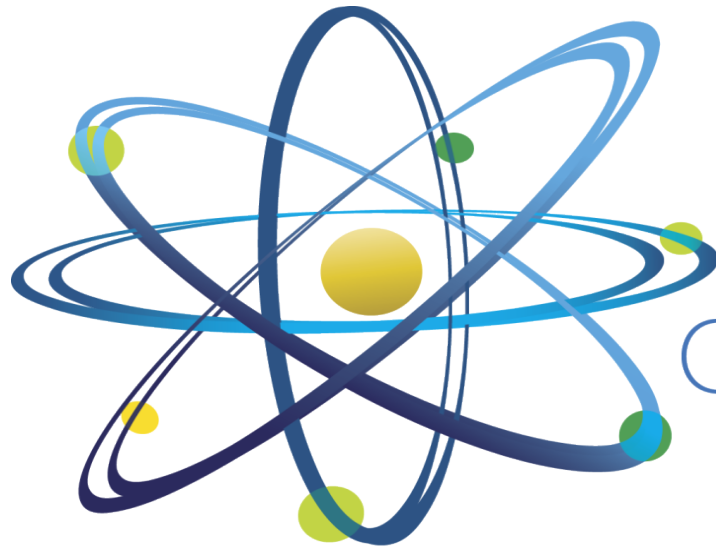
Summary Slides

- **Determination of canister-relevant environments**
 - ISFSI site sampling and thermodynamic modeling enable better prediction of potential brines on canister surfaces.
 - Applying information gained about these brines to develop enhanced corrosion testing; including both potential corrosion accelerants (cycling and dust) and inhibitors (nitrates).
 - Additionally, have shown that MgCl_2 -dominant brines will be present for long time periods (>300 years) on the canister surface
- **Corrosion testing and modeling in canister relevant environments**
 - Expanding testing to more relevant scenarios to better establish controlling factors for pitting and potential SCC initiation
 - Expanding modeling efforts to account for non-static brine/corrosion conditions to better predict pitting and SCC initiation
- **Crack growth rate**
 - Installed and started initial tests in varied brine environments to explore potential effects on CGR
 - Verified sample geometry to initiate atmospheric testing

Acknowledgements

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Questions?



Clean. **Reliable. Nuclear.**