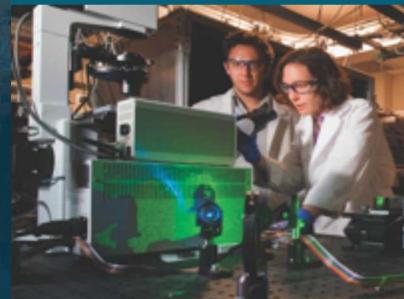


# IAEA CRP I31033 : SNL YEAR I PROGRESS



SAND2020-7174PE



*Lucas I. Albright, KC Wagner, Jesse Phillips, David L. Luxat*  
July 16, 2020

SAND-XXXXXX X

IAEA CRP I31033 "Advancing the State-of-Practice in Uncertainty and Sensitivity Methodologies for Severe Accident Analysis in Water Cooled Reactors"



Sandia National Laboratories is a multimission laboratory managed and operated by National Technology & Engineering Solutions of Sandia, LLC, a wholly owned subsidiary of Honeywell International Inc., for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-NA0003525.

# Contents

1. Year 1 Progress Overview
2. Project Objectives
3. Methodology
4. Workflow Overview
5. Model Description
6. Input Parameter Selection
7. Reference Case

# Year I Progress Overview



Task	Comment	Status
Plant Model Development	–	Complete
Input Parameter Selection	–	Complete
PDF Selection	–	Complete
Methodology	<ul style="list-style-type: none"> <li>Not a “best-estimate” uncertainty analysis</li> <li>We believe application of “best-estimate” uncertainty analysis methodologies to be misaligned with some project objectives</li> <li>We apply modified uncertainty analysis methodologies that is consistent with project objectives – explained in the following slides</li> </ul>	In progress
Reference Case	–	Complete
Summary Report	No delays expected	In progress

# Project Objectives and Uncertainty Analysis Methodology



Investigate model form uncertainty between two material interaction modelling options available in MELCOR

Explore the range of MELCOR results produced by each respective model

Inform future MELCOR model development

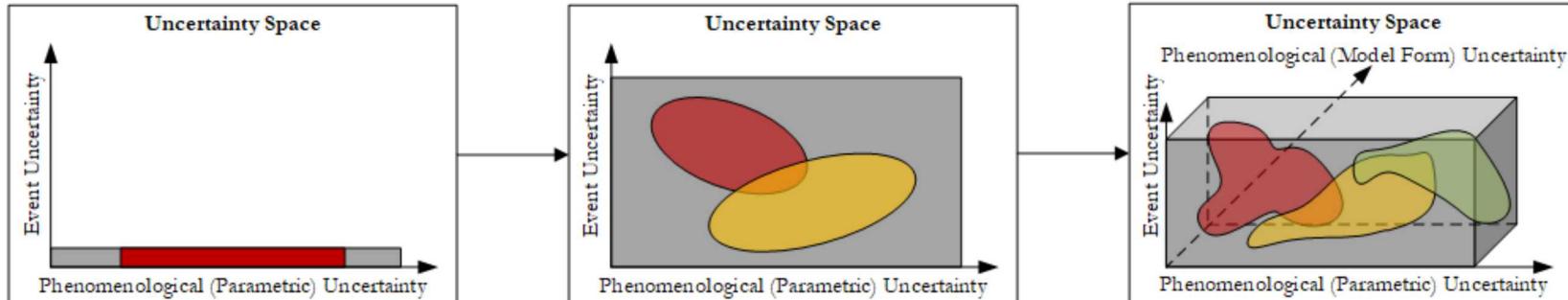
This UA is different from previous SNL studies which considered source term and consequence uncertainty (e.g., NUREG/CR-7155)

Research Objectives:

- Comparison of the overall accident progression exhibited by each model
- Comparison of the distributions of different figures of merit
- Identification of correlations and biases that each model may introduce

Expansion of the uncertainty space domain:

- Inclusion of other forms of uncertainty is a more “complete” representation of reality
- Gross bifurcations may emerge (due to model differences, modelling gaps, etc.)



# Methodology



Not a “best-estimate” uncertainty analysis – not attempting to quantify the uncertainty in a traditional sense

Identify the underlying biases of each model through an “exploratory” uncertainty analysis

- Not using “best-estimate” distributions of input parameters or attempting to establish “best-estimate” distributions of FOMs
- Uniform distributions are utilized to promote coverage of the uncertainty space and perform a “blind” comparison of models
  - Removal of a priori biases on input and result distributions to investigate model form bias

## Comparison

- Qualitative comparison of results (magnitudes, timings, and distribution/clustering characteristics)
- Quantitative comparison of results (minimums, maximums, etc.)
- Pointedly avoiding application of statistical methods that may impose misleading “artifacts” and inappropriate structure to the data

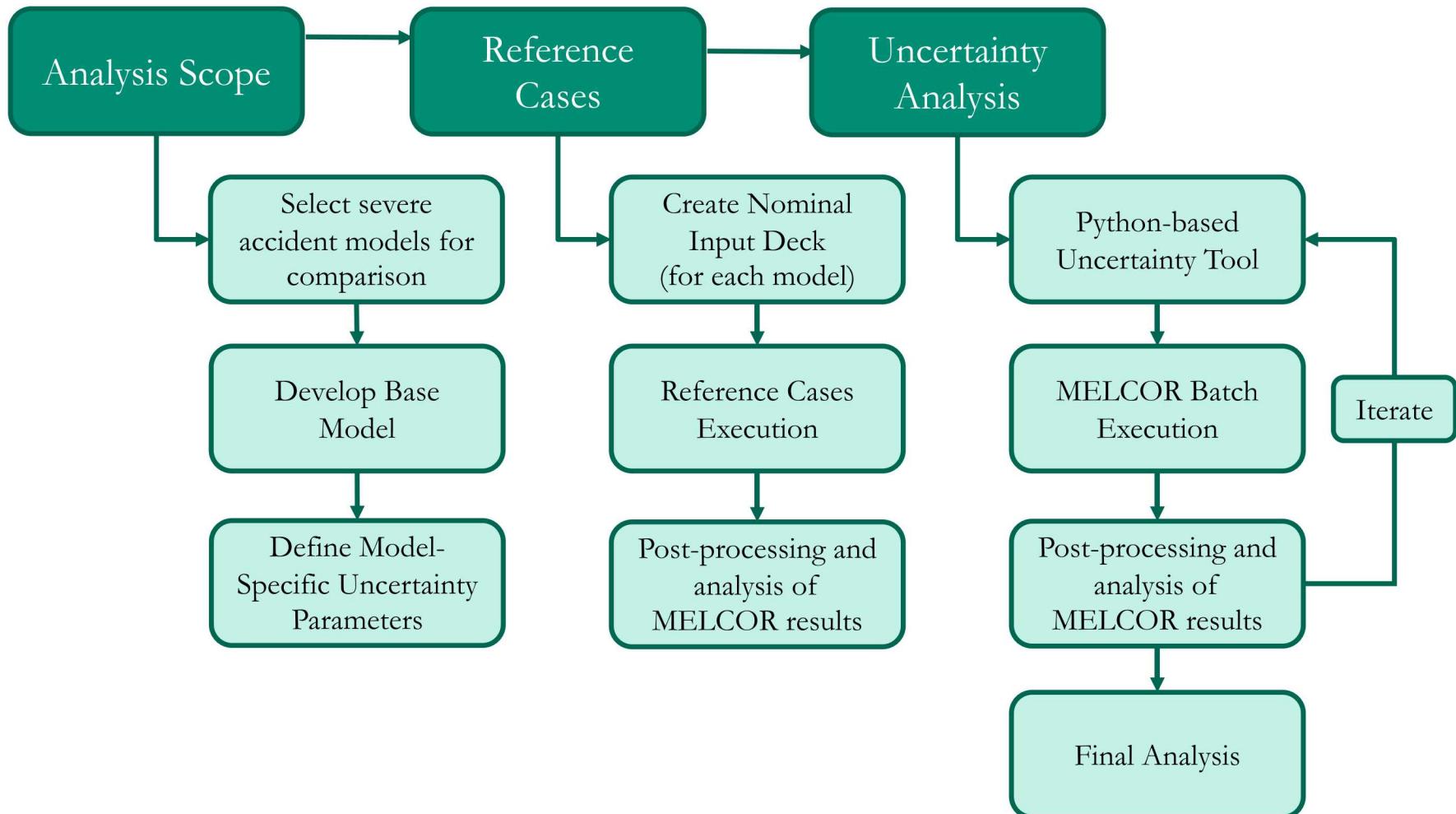
## Correlation

- Identification of unknown correlations between input parameters and FOMs or multiple FOMs.
- Comparison of known/unknown correlations between each model

## Clustering

- Identification of result clustering within each model’s distribution
- Identification of cluster differences between models (cluster “existence”, “location”, and “size”).

# Uncertainty Analysis Workflow



# 7 Model Description



## Plant Description

- 460 MW(e) BWR/3 reactor, Mk-I containment
- Core thermal hydraulic phenomena modeled in 26 control volumes (1 lower plenum, 25 core region)
- Core degradation phenomena modeled in 88 core cells (50 active core, 38 lower plenum)
- Containment phenomena modeled in 6 control volumes

## Scenario Description

- Modelling assumptions and boundary conditions

Boundary Condition	Description
<b>RPV Depressurization prior to Lower Head Failure</b>	Not permitted
<b>Lower Head Gross Creep Failure</b>	Permitted
<b>Lower Head Penetration Failure</b>	Not permitted
<b>Drywell Head Flange leakage</b>	Begins at 0.6481 MPa pressure in the drywell
<b>Main Steam Line Isolation Valve Closure</b>	At 0.0 hours
<b>Feedwater System Ceases Operation</b>	At 0.0 hours
<b>IC Train A Operation</b>	0.1-0.28 hours 0.52-0.55 hours 0.63-0.67 hours 0.77-0.8 hours
<b>IC Train B Operation</b>	0.1-0.28 hours
<b>Wetwell Venting</b>	At 23.7 hours
<b>Reactor Building Explosion</b>	At 24.8 hours

# Input Parameters



Input Record	Description	Units	Distribution	Parameter Options		Reference
				Interactive Materials Model	Eutectics Model	
<b>Material Interaction Model</b>						
<b>Material Interaction Model Activation</b>	This analysis involves a comparison of the interactive materials and eutectics models available in MELCOR	-	-	Interactive Materials Model Activate	Eutectics Model Activate	-
<b>MP_PRC: ZRO2-INT, UO2-INT</b>	Interactive materials model reduced liquefactions temperatures for ZRO2-INT and UO2-INT	K	Uniform	2230.0-2728.0	-	Informed by SOARCA (3 $\sigma$ )
<b>Candling Models</b>						
<b>COR_SC: 1131(2)</b>	Molten Material Holdup Parameters: Maximum ZrO <sub>2</sub> temperature permitted to hold up molten Zr in CL.	K	Uniform	2100-2540	2100-2540	Informed by SOARCA (min-max)
<b>COR_SC: 1141(2)</b>	Core Melt Breakthrough Candling Parameters: Maximum melt flow rate per unit width after breakthrough	kg m/s	Uniform	0.1-2.0	0.1-2.0	Informed by SOARCA (min-max)
<b>Fuel Rod Failure Models</b>						
<b>COR_ROD</b>	Rod Collapse Model	-	Discrete Uniform	Active (0), Disabled (1)	Active (0), Disabled (1)	-
<b>COR_CCT: DRZRMN</b>	Component Critical Minimum Thicknesses	m	Uniform	0.0-0.00015	0.0-0.00015	
<b>COR_SC: 1132(1)</b>	Core Component Failure Parameters: Temperature to which oxidized fuel rods can stand in the absence of unoxidized Zr in the cladding.	K	Uniform	2230.0-2728.0	2230.0-2728.0	Informed by SOARCA (3 $\sigma$ )
<b>Debris Quenching and Dryout Models</b>						
<b>COR_EDR: DHYPD, DHYPB (Active Core)</b>	Particulate debris equivalent diameter in the active core region	m	Uniform	0.005-0.015	0.005-0.015	Engineering judgement
<b>COR_EDR: DHYPD, DHYPB (Lower Plenum)</b>	Particulate debris equivalent diameter in the lower plenum	m	Uniform	0.0001-0.005	0.0001-0.005	Engineering judgement
<b>COR_LP: HDBH2O</b>	Heat transfer coefficient of falling debris	W/m <sup>2</sup> K	Uniform	100.0-4000.0	100.0-4000.0	Engineering judgement
<b>COR_LP: VFALL</b>	Velocity of falling debris	m/s	Correlated to particulate debris diameter in the lower plenum	-	-	Engineering judgement
<b>COR_SC: 1244 (3)</b>	Debris Dryout Heat Flux Correlation: Minimum Debris Porosity	-	Uniform	0.15-0.4	0.15-0.4	Engineering judgement
<b>COR_TST: IMPLZDM</b>	Lipinski zero-dimensional dryout heat flux flag	-	Discrete Uniform	Active (0), Disabled (1)	Active (0), Disabled (1)	-
<b>Numerical Uncertainty</b>						
<b>CVH_SC: 4422 (2)</b>	A random number seed that varies the t/h solution matrix to include and evaluate numerical model variance importance . A value of 0.0 indicates that MELCOR will generate a random number seed based on the system clock time.	-	Uniform	1-1e6	1-1e6	-

# Reference Case



Transient: Short term station blackout (STSBO)

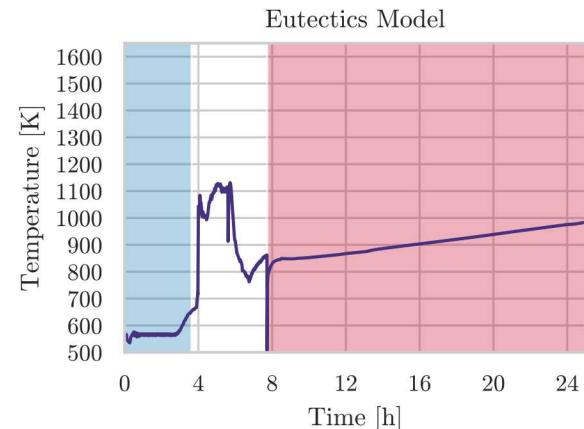
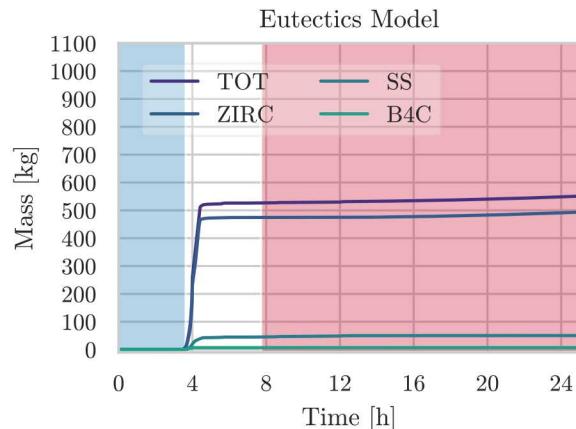
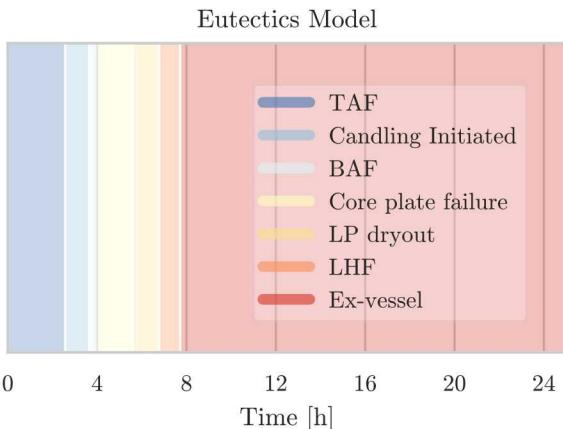
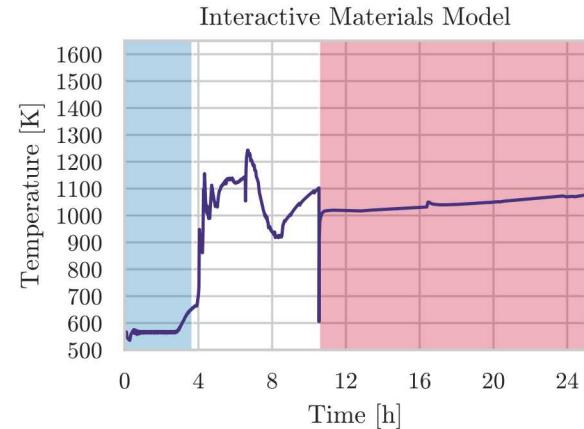
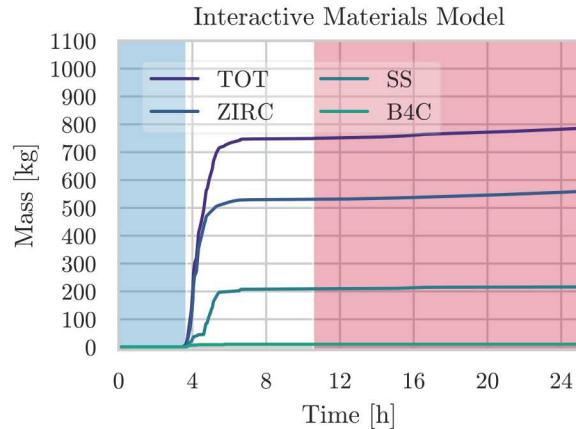
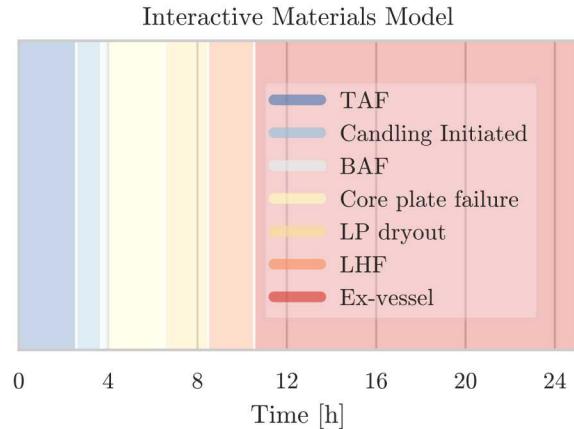
Simulation length: 25 hours

Key outputs for FOM Determination

- Overall Accident Progression
  - Key event timings
- Hydrogen Generation
- Thermal Hydraulic Response
  - Primary Coolant System Response
  - Containment Response
- Reactor Core Degradation
- RPV Lower Head Breach

Input Record	Reference Case Parameter Values	
	Interactive Materials Model	Eutectics Model
<b>Material Interaction Model</b>		
<b>Material Interaction Model Activation</b>	Interactive Materials Model	Eutectics Model
<b>MP_PRC: ZRO2-INT, UO2-INT</b>	2479.0	—
<b>Candling Models</b>		
<b>COR_SC: 1131(2)</b>	2400.0	2400.0
<b>COR_SC: 1141(2)</b>	1.0	1.0
<b>Fuel Rod Failure Models</b>		
<b>COR_ROD</b>	Active (0)	Active (0)
<b>COR_CCT: DRZRMN</b>	0.0001	0.0001
<b>COR_SC: 1132(1)</b>	2479.0	2479.0
<b>Debris Quenching and Dryout Models</b>		
<b>COR_EDR: DHYPD, DHYPB (Active Core)</b>	0.01	0.01
<b>COR_EDR: DHYPD, DHYPB (Lower Plenum)</b>	0.002	0.002
<b>COR_LP: HDBH2O</b>	4000.0	4000.0
<b>COR_LP: VFALL</b>	1.5	1.5
<b>COR_SC: 1244 (3)</b>	0.15	0.15
<b>COR_TST: IMPLZDM</b>	Active (0)	Active (0)
<b>Numerical Uncertainty</b>		
<b>CVH_SC: 4422 (2)</b>	492074	492074

# Sample Results



Accident Progression

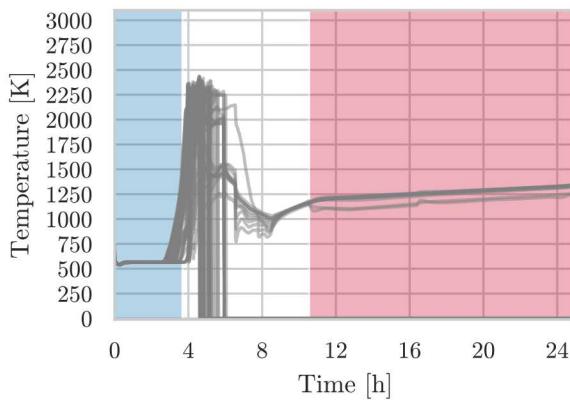
Hydrogen Generation

Steamdome Temperature

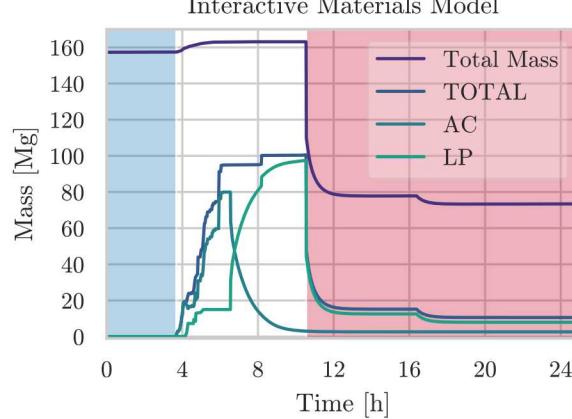
# Sample Results



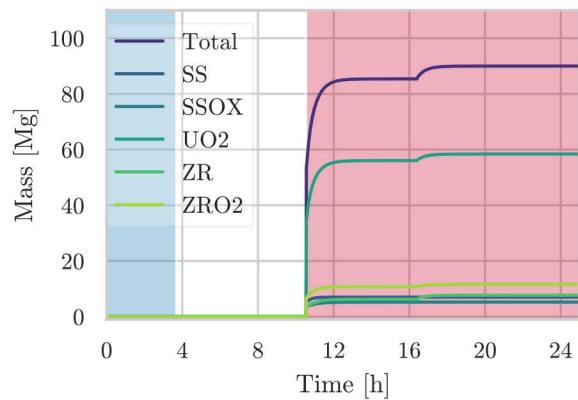
Interactive Materials Model



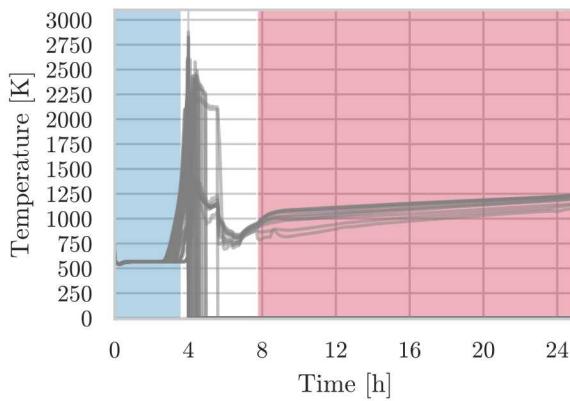
Interactive Materials Model



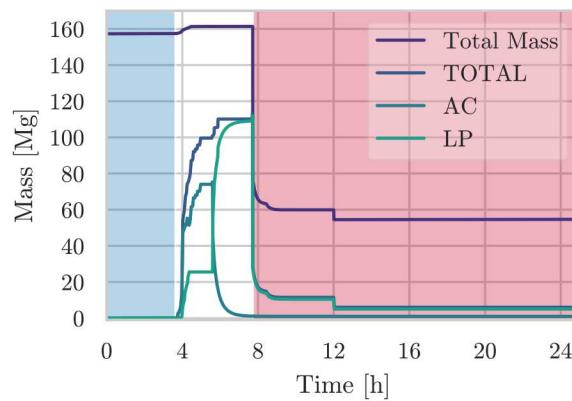
Interactive Materials Model



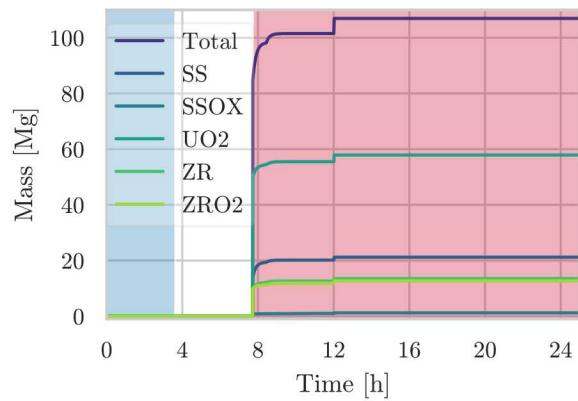
Eutectics Model



Eutectics Model



Eutectics Model



Fuel Temperature

Debris Distribution

Ejected Mass

## Acknowledgements



This work was jointly supported by the U.S. DOE-NE IUP Fellowship Program and the United States Nuclear Regulatory Commission. The views expressed in the article do not necessarily represent the views of the U.S. Department of Energy or the United States Government.

Sandia National Laboratories is a multimission laboratory managed and operated by National Technology & Engineering Solutions of Sandia, LLC, a wholly owned subsidiary of Honeywell International Inc., for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-NA0003525.



Thank you for your attention

