



SAND2018-7981C

Quantifying the Effects of Microstructure on Localization in Stainless Steel

PRESENTED BY

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Goal: Understand (predict) localization leading to failure

Processing variables

- Alloying
- Forming
- Heat treatment

Property variables

- Microstructure
- Defect distribution

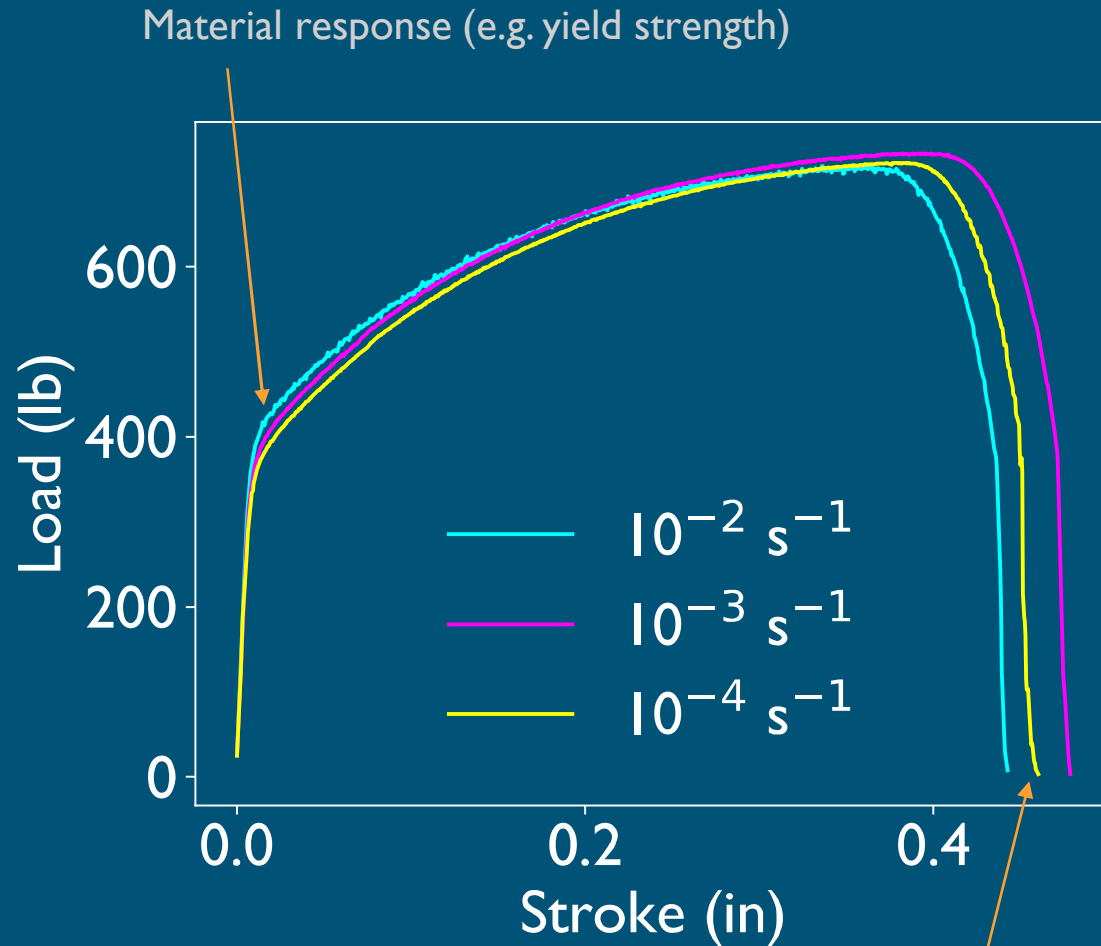
Predictor space

- Deformation rate
- Temperature
- Loading mode

Outcome space

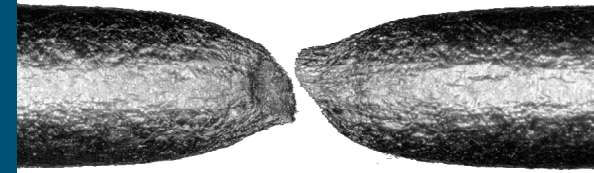
- (An)isotropy
- Strength
- Ductility



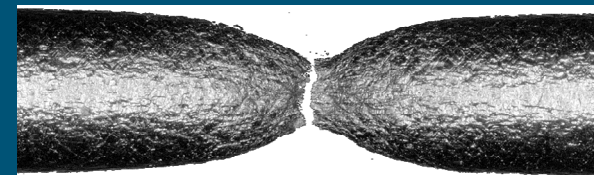


Structural response? (e.g. strain to failure)

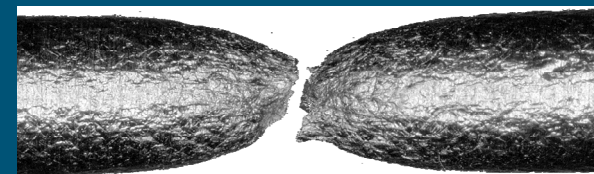
Tests at 200 °C



10^{-2} s^{-1}

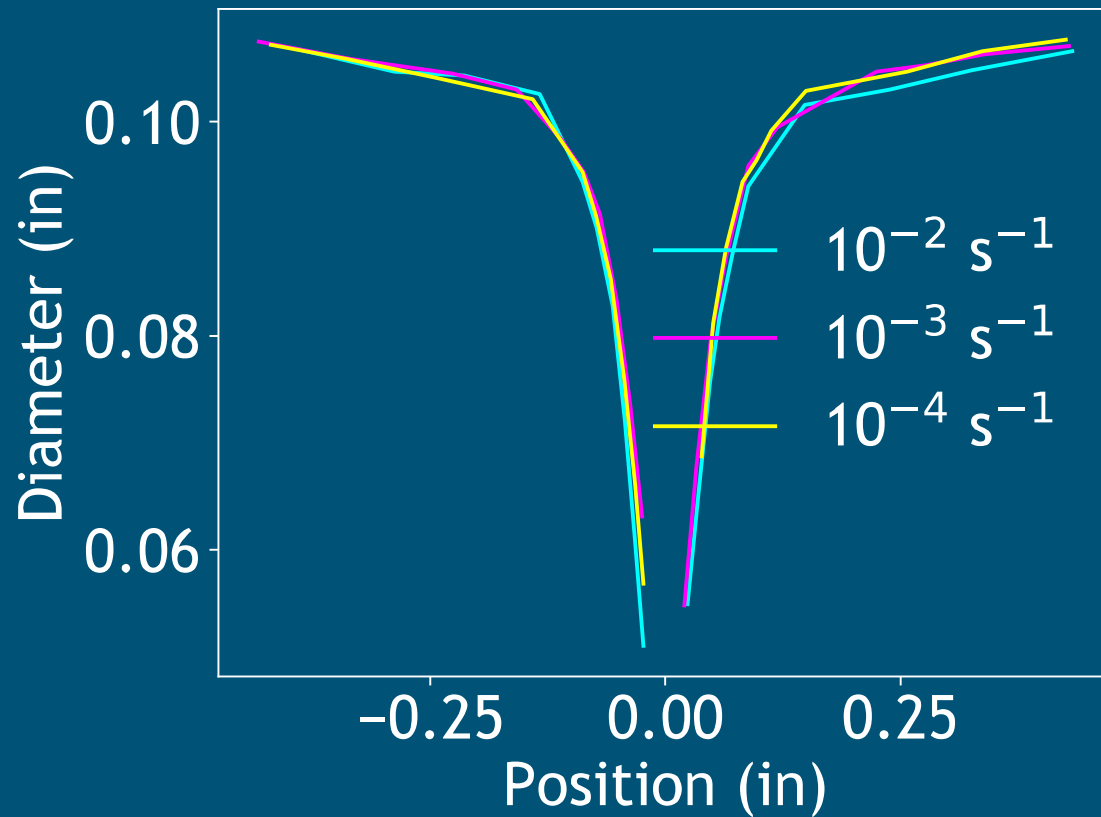


10^{-3} s^{-1}

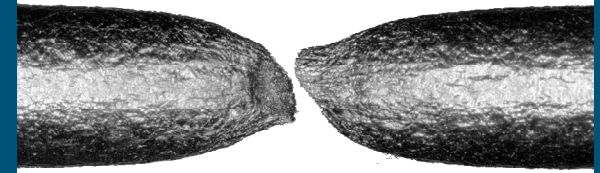


10^{-4} s^{-1}

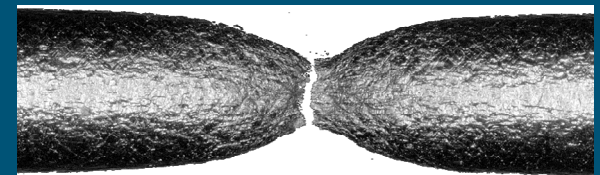
Rate sensitivity at the structural scale



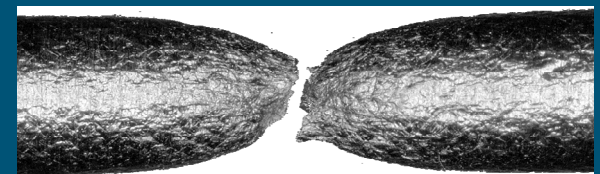
Tests at 200 °C



10^{-2} s^{-1}



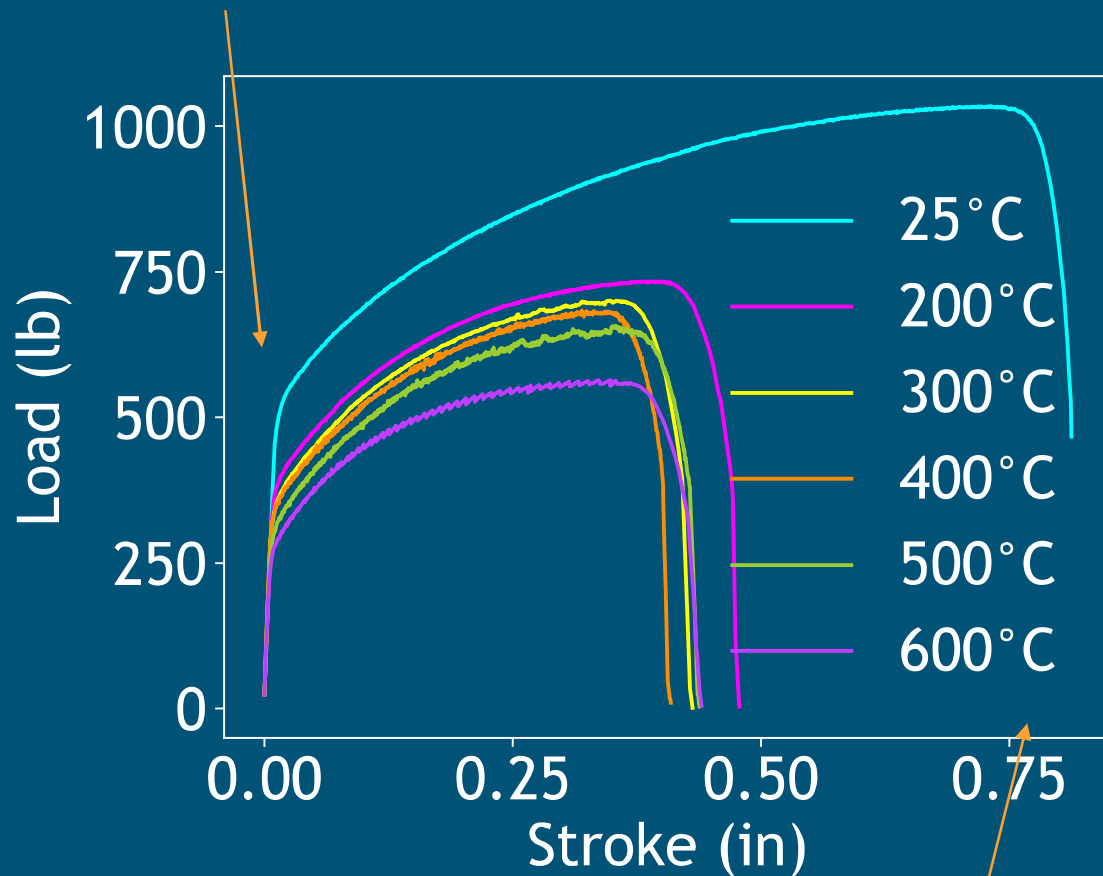
10^{-3} s^{-1}



10^{-4} s^{-1}

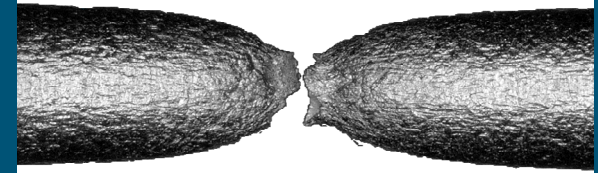
Temperature sensitivity at the (micro)structural scale

Material response (e.g. yield strength)

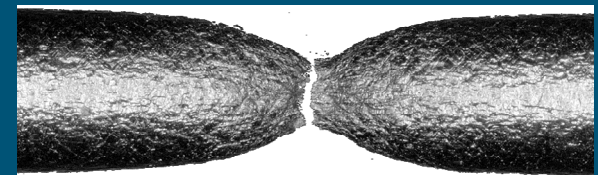


Structural response? (e.g. strain to failure)

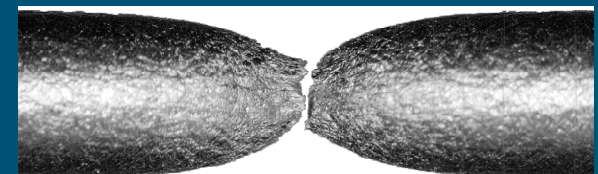
Tests at 10^{-3} s^{-1}



25 °C

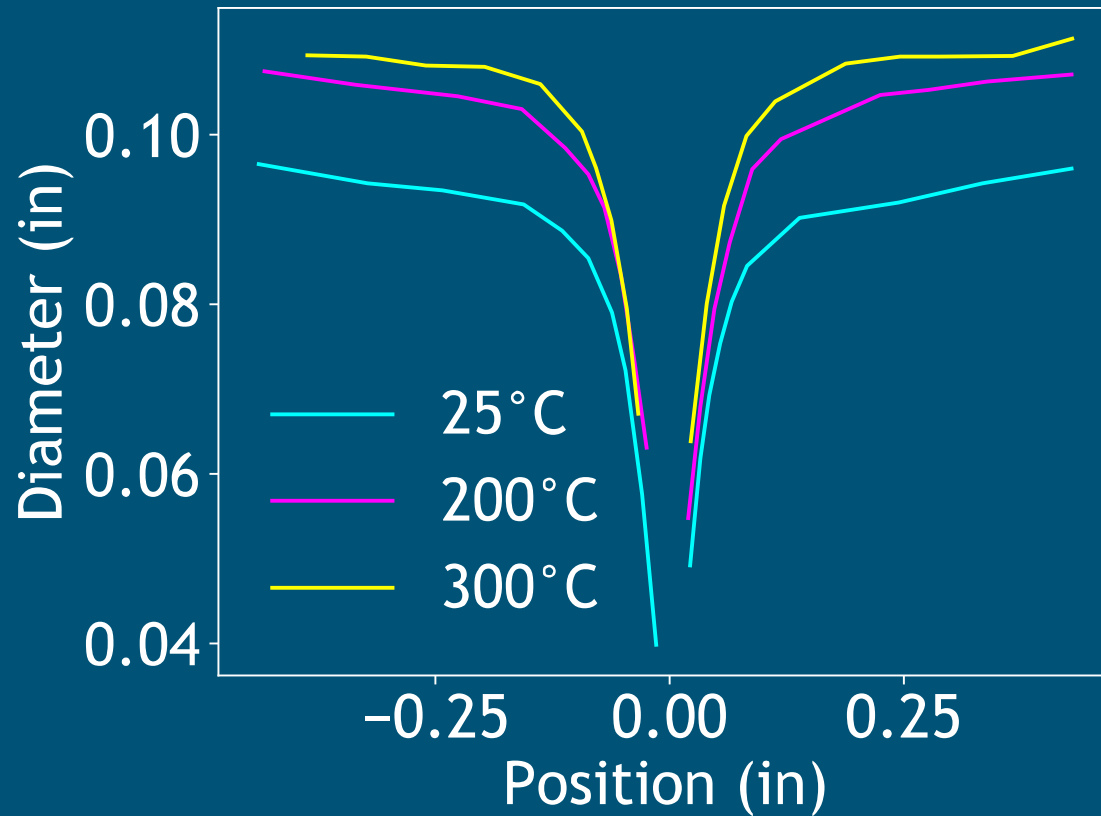


200 °C

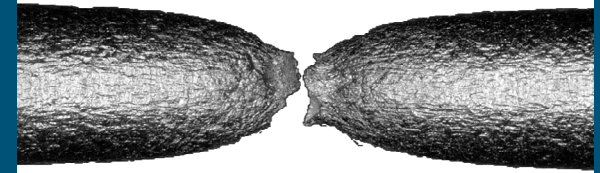


300 °C

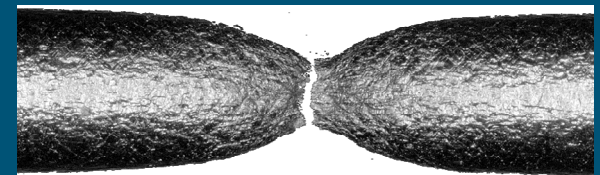
Temperature sensitivity at the structural scale



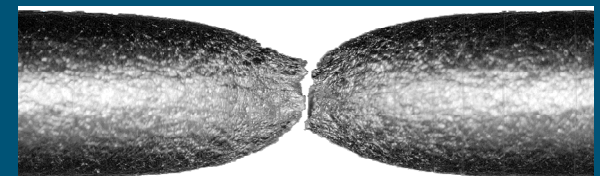
Tests at 10^{-3} s^{-1}



25 °C



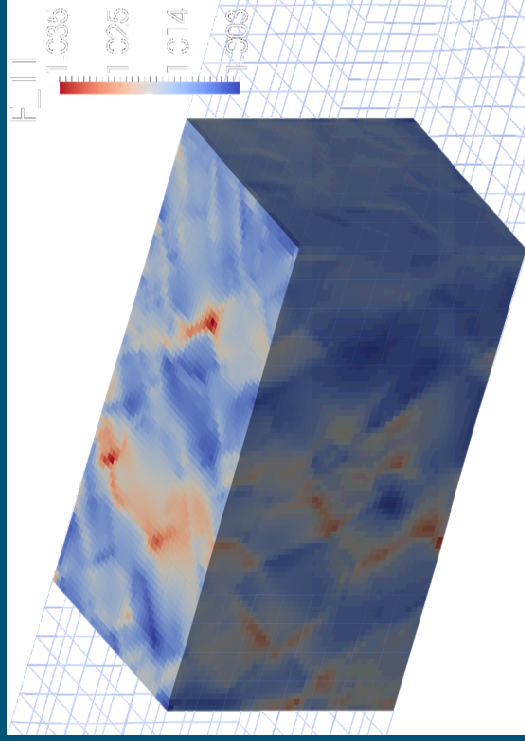
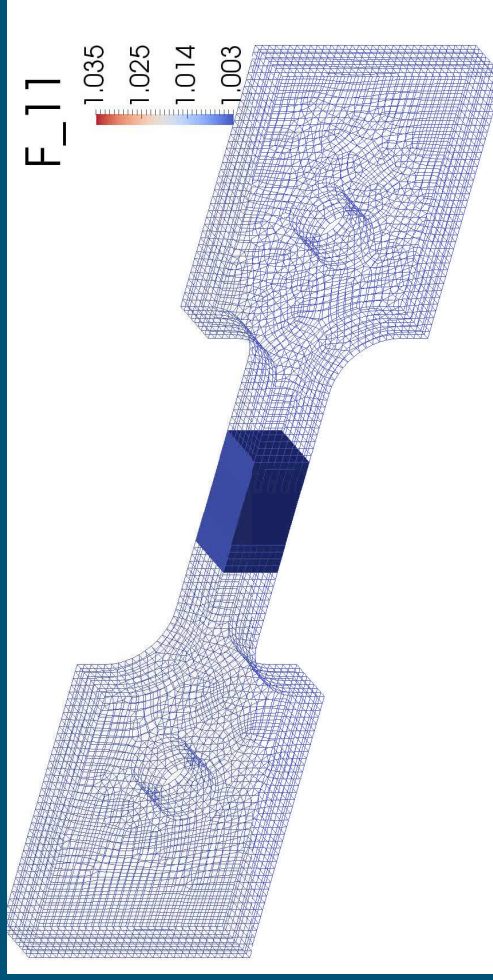
200 °C



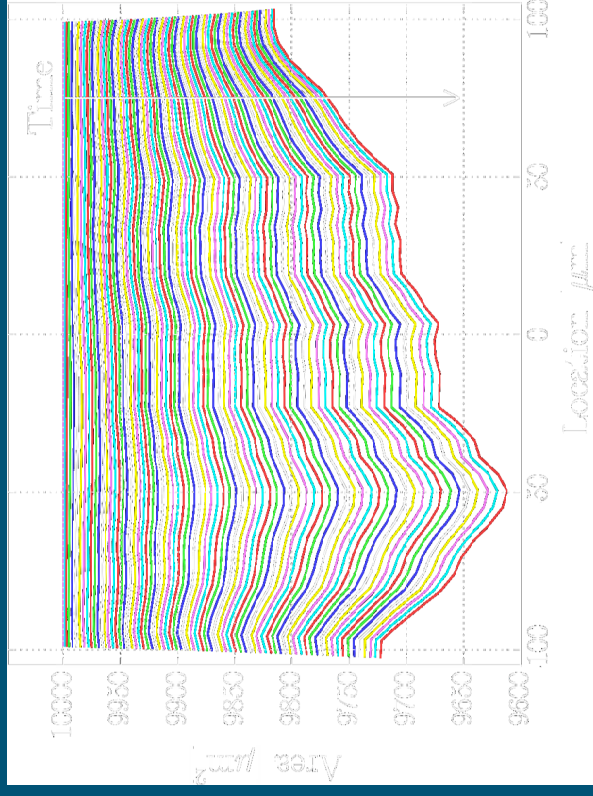
300 °C

7 Performance: Necking Localization

Heterogeneity and localization in plasticity

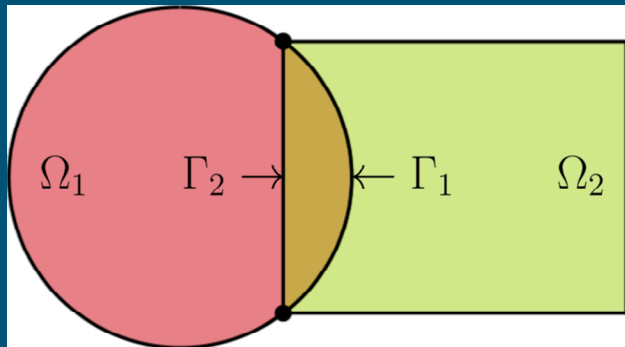


Reduction in area over time



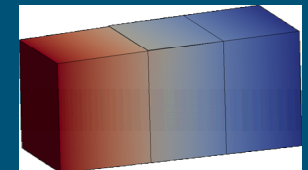
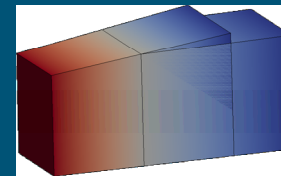
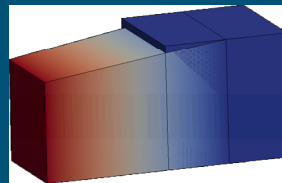
C. Alleman et. al., *Comp. Mech.*, 61(1-2), 2018.

Concurrent Coupling: Schwarz Method



Concept of solution scheme

- Solve on Ω_1 using initial guess for BCs on Γ_1 .
- Solve on Ω_2 using BCs on Γ_2 interpolated from Ω_1 .
- Solve on Ω_1 with BCs on Γ_1 interpolated from Ω_2 .

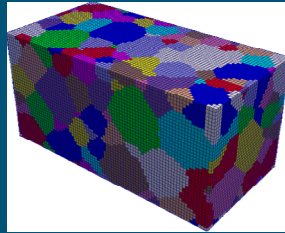


- Mathematical proof of convergence for solid mechanics problem
- Allows coupling of nonconforming domains with different element types and levels of refinement
- Information is exchanged concurrently among two or more subdomains
- Different solvers can be used for each subdomain
- Different material models can be coupled provided that they are compatible

9 Performance: Local/Global Response

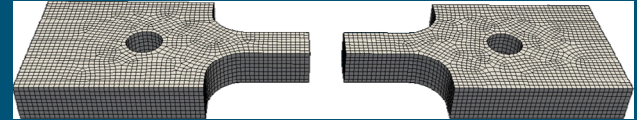
Mesoscale

voxelated microstructure derived
from Kinetic Monte Carlo evolution
(F. Abdeljawad)

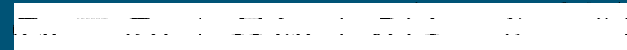


+

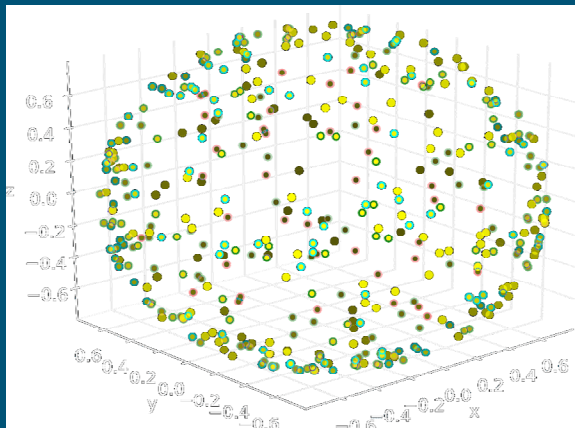
Macroscale



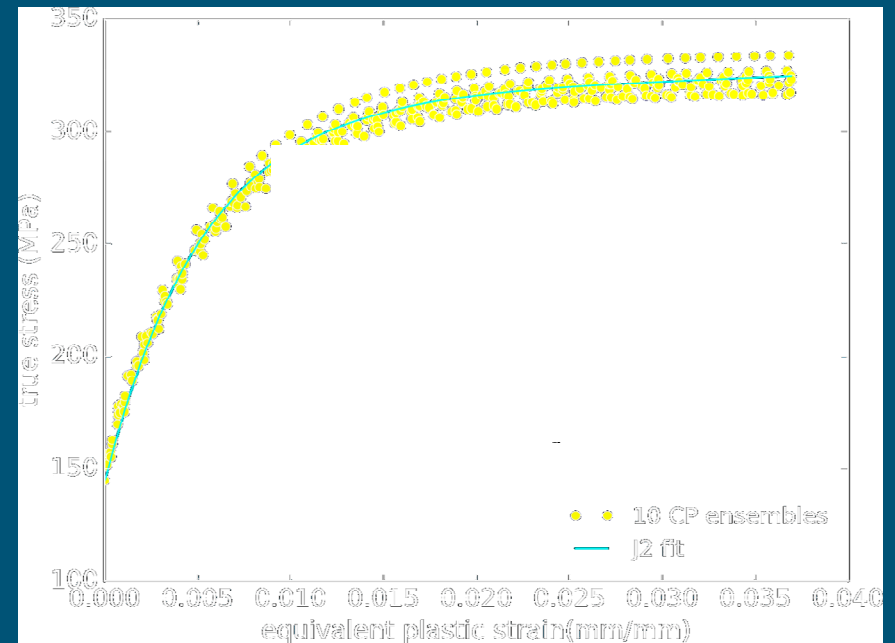
- Load microstructural ensembles in uniaxial stress
- Fit flow curves with a macroscale J_2 plasticity model

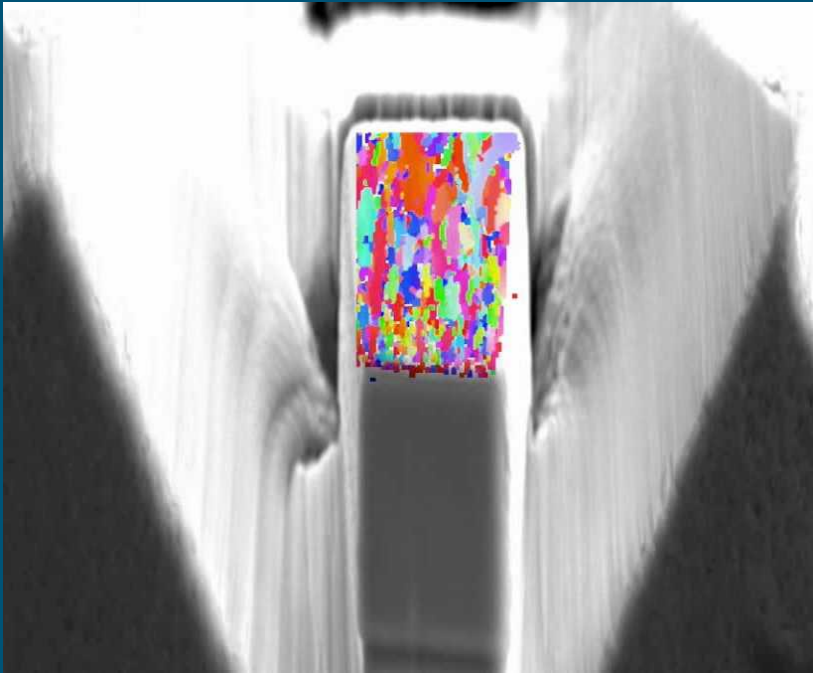


Fix microstructure, investigate ensembles



151 axial vectors
from 3 of the 10
ensembles of
random rotations

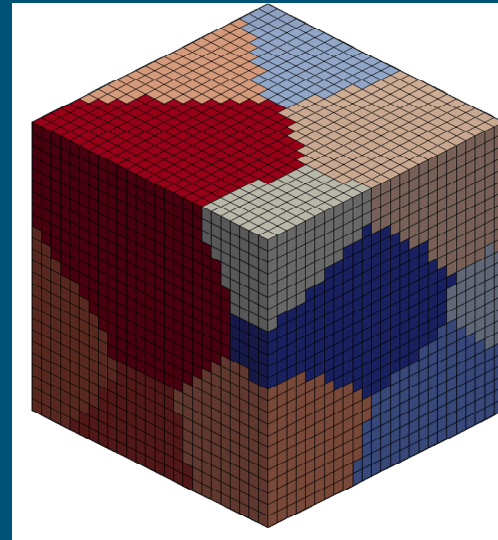




Sugar, 2017

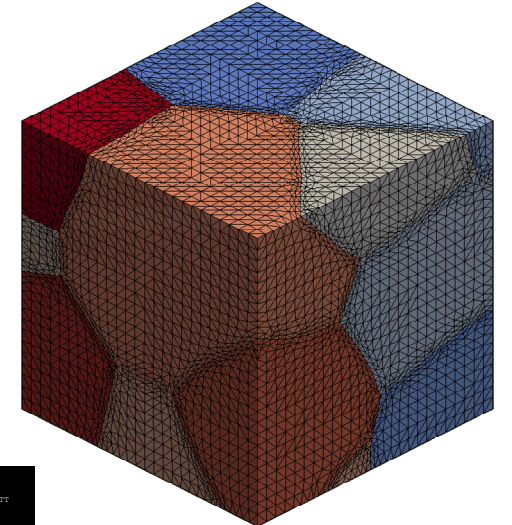
Serial sectioning characterization experiment

Demonstration on Ni sample



DREAM.3D

Compute microstructure
statistics, output voxelized
microstructure



SCULPT

Input: voxel orientations
Output: conformal mesh

```

SSSSS  CCCCC  UU  UU  LL  PPPPP  TTTTT
SS  SS  CC  CC  UU  UU  LL  PP  PP  TT
SS  SS  CC  CC  UU  UU  LL  PP  PP  TT
SSSSS  CCCCC  UU  UU  LL  PPPPP  TTTTT
SS  SS  CC  CC  UU  UU  LL  PP  PP  TT
SS  SS  CC  CC  UU  UU  LL  PP  PP  TT
SSSSS  CCCCC  UU  UU  LL  PPPPP  TTTTT

```

Kinematics

Multiplicative elastic-plastic decomposition

$$\mathbf{F}^e = \mathbf{F} \cdot (\mathbf{F}^p)^{-1}$$

Crystal elasticity

Linear elastic constitutive relation

$$\mathbf{T}^* = \mathbb{L}^c : \mathbf{E}^e$$

Elastic Lagrangian strain

$$\mathbf{E}^e = \frac{1}{2} [(\mathbf{F}^e)^T \mathbf{F}^e - \mathbf{I}]$$

Crystal Plasticity

Evolution of plastic deformation gradient

$$\dot{\mathbf{F}}^p = \mathbf{L}^{p*} \cdot \mathbf{F}^p$$

Plastic part of the velocity gradient

$$\mathbf{L}^{p*} = \sum_{\alpha} \dot{\gamma}^{\alpha} \mathbf{m}_0^{\alpha} \otimes \mathbf{n}_0^{\alpha}$$

Resolved shear stress

$$\tau^{\alpha} = [(\mathbf{F}^e)^T \cdot \mathbf{F}^e \cdot \mathbf{T}^*] : \mathbf{m}_0^{\alpha} \otimes \mathbf{n}_0^{\alpha}$$

Hardening

- Linear w/ recovery

$$\dot{g}^{\alpha} = (H - R_d g^{\alpha}) |\dot{\gamma}^{\alpha}|$$

- Saturation

$$\dot{g}^{\alpha} = \dot{g}_0 \left(\frac{g_s - g^{\alpha}}{g_s - g_0} \right) H^{\alpha\beta} |\dot{\gamma}^{\beta}|$$

- Dislocation density

$$g^{\alpha} = \sqrt{H^{\alpha\beta} \rho^{\beta}}, \dot{\rho}^{\alpha} = \left(\kappa_1 \sqrt{\Sigma \rho^{\beta}} - \kappa_2 \rho^{\alpha} \right) |\dot{\gamma}^{\alpha}|$$

Plastic flow

- Power law

$$\dot{\gamma}^{\alpha} = \dot{\gamma}_0 \left| \frac{\tau^{\alpha}}{g^{\alpha}} \right|^m \text{sign}(\tau^{\alpha})$$

- Dislocation drag

$$\dot{\gamma}^{\alpha} = D \frac{\tau^{\alpha}}{g^{\alpha}}$$

- Thermal activation

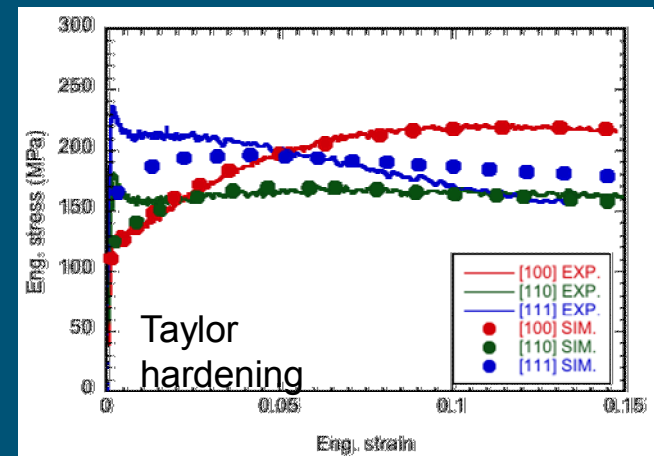
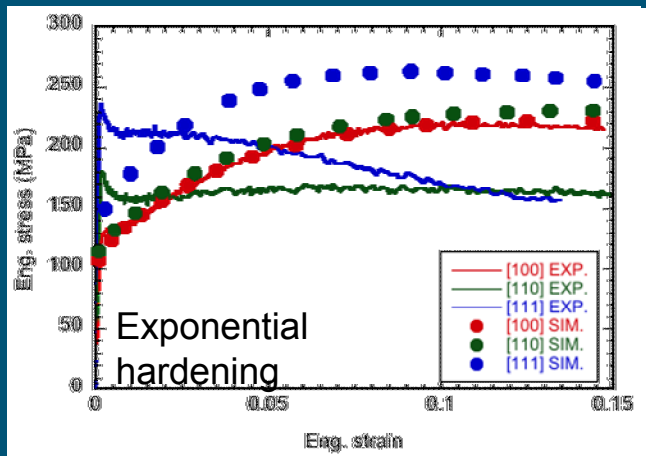
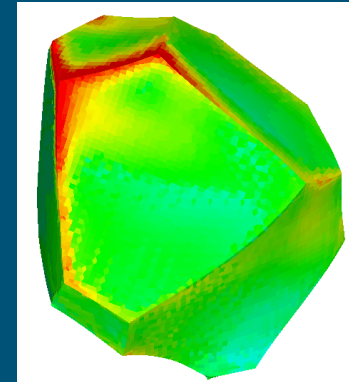
$$\dot{\gamma}^{\alpha} = \dot{\gamma}_0 \exp \left(-\frac{F_0}{k_B \theta} \left[1 - \left(\frac{\tau^{\alpha} - g^{\alpha}}{\tau_0} \right)^p \right]^q \right)$$

Linear hardening w/ recovery

$$\dot{g}^\alpha = (H - R_d g^\alpha) |\dot{\gamma}^\alpha|$$

Taylor (dislocation density) hardening

$$g^\alpha = \sqrt{H^{\alpha\beta} \rho^\beta}, \quad \dot{\rho}^\alpha = \left(\kappa_1 \sqrt{\sum \rho^\beta} - \kappa_2 \rho^\alpha \right) |\dot{\gamma}^\alpha|$$



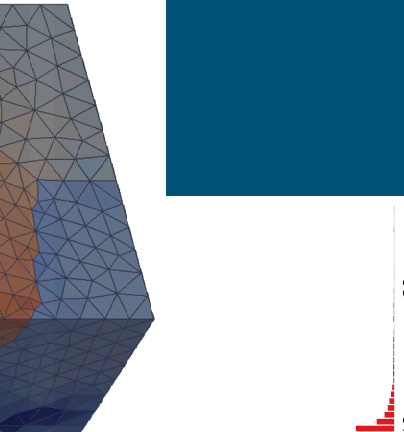
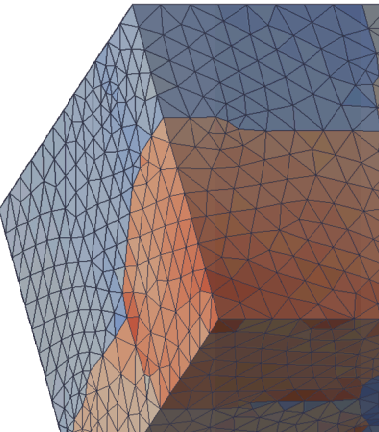
Lim, 2016

- Parameterize through [100] Ta single crystal experiments
- Predict [110] and [111] response.
- *Dislocation density based Taylor hardening model* most accurately reflects anisotropy.

11

Microstructure
statistical
a single see
underlying
morphology

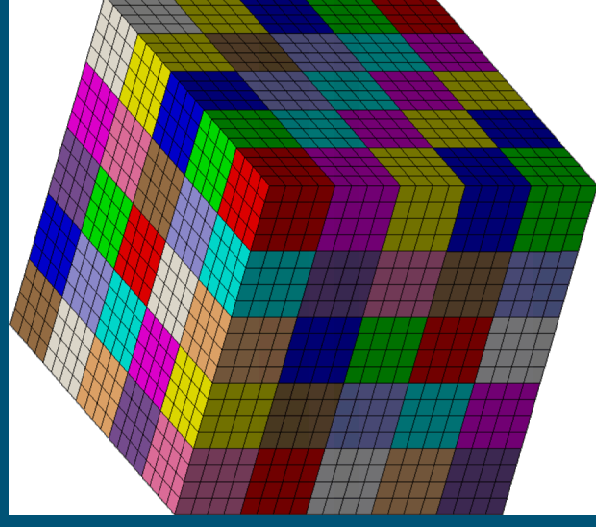
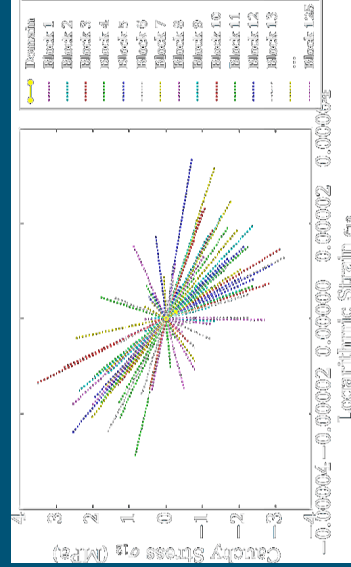
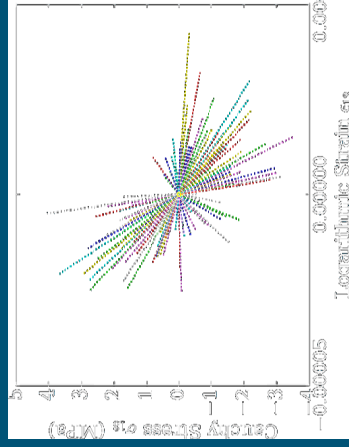
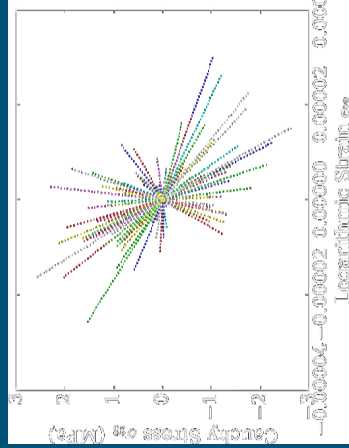
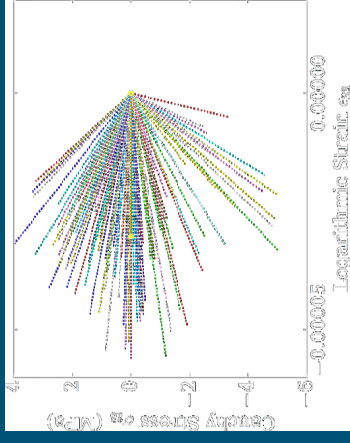
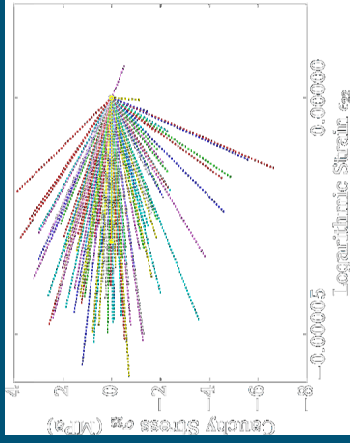
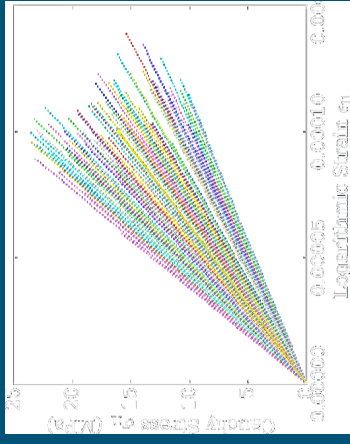
Microstructure performance equivalence: metrics for mechanical response?



Resolved Shear Stress (MPa)	Number of Elements
-20	0
-15	0
-10	0
-5	0
0	2500
5	2500
10	2500
15	0
20	0

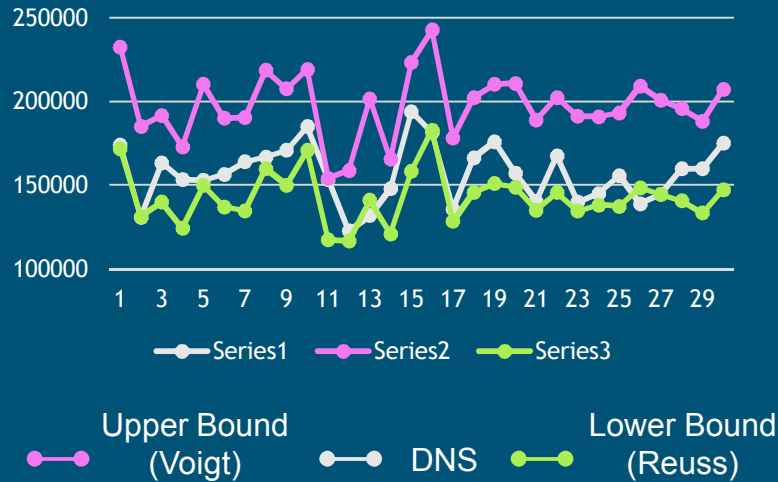


Performance: Crystal Elasticity

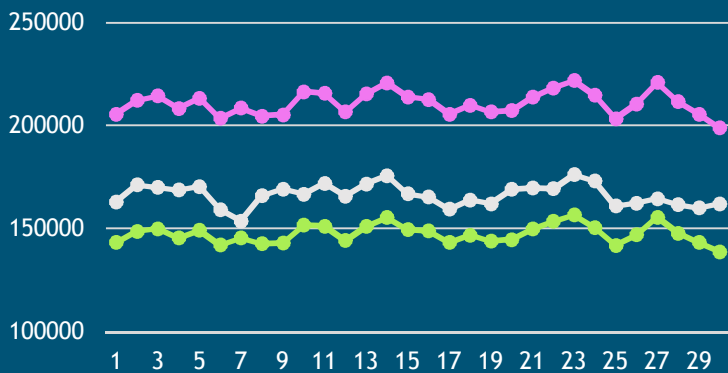


Performance: (An)isotropic Elasticity

Bounds - 8 Grains

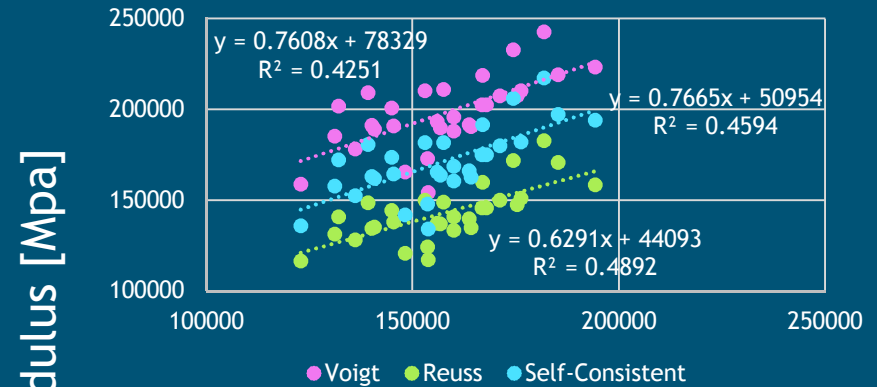


Bounds - 125 Grains

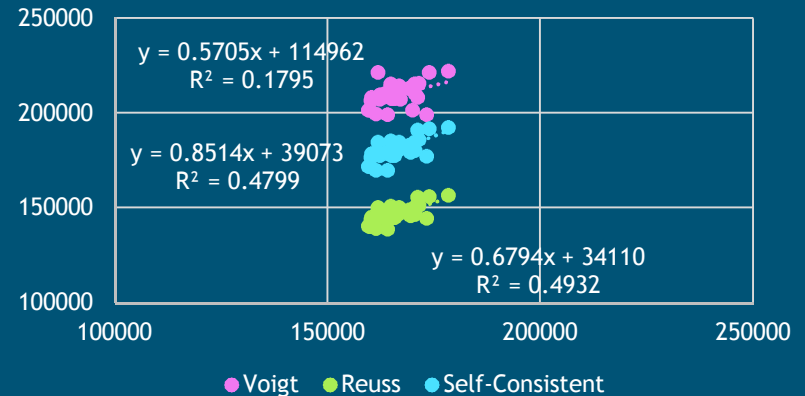


Microstructure #

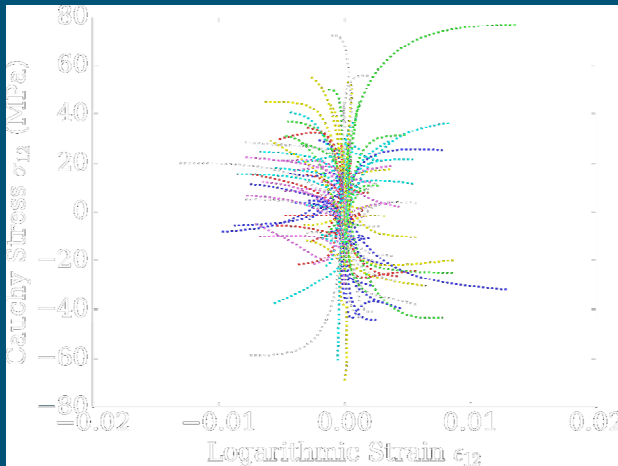
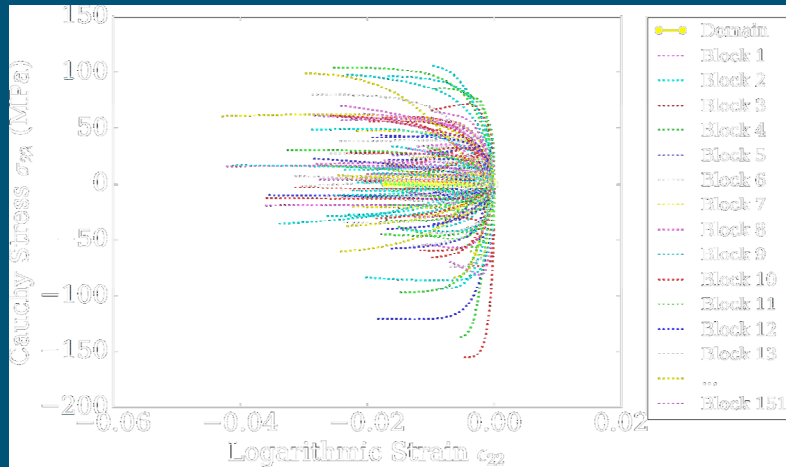
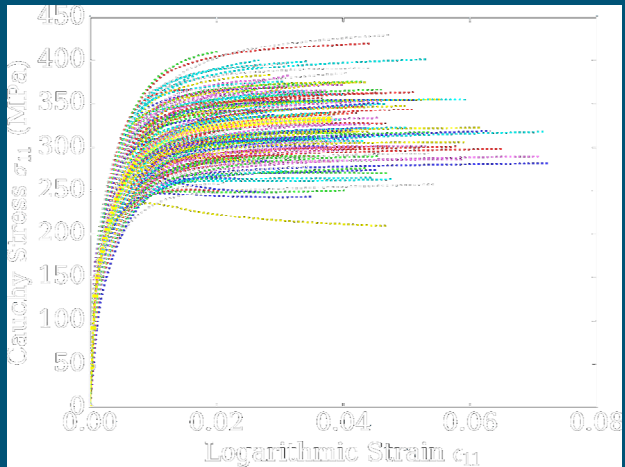
Modulus Correlation - 8 Grains



Modulus Correlation - 125 Grains

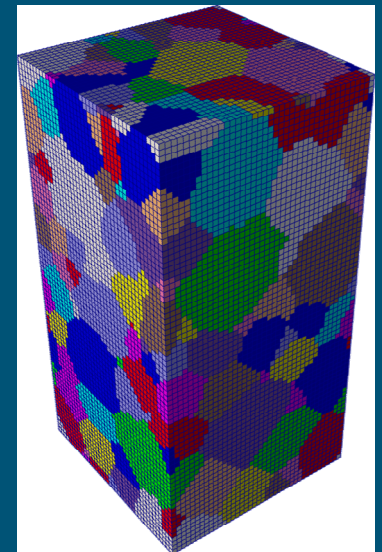


Simulated Modulus [Mpa]

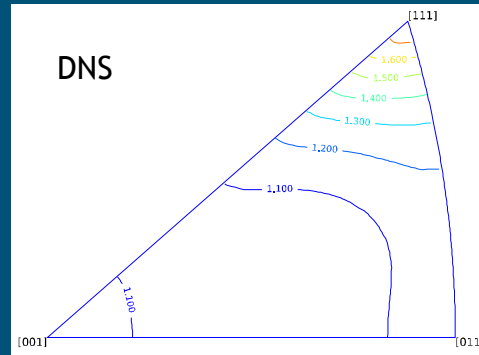
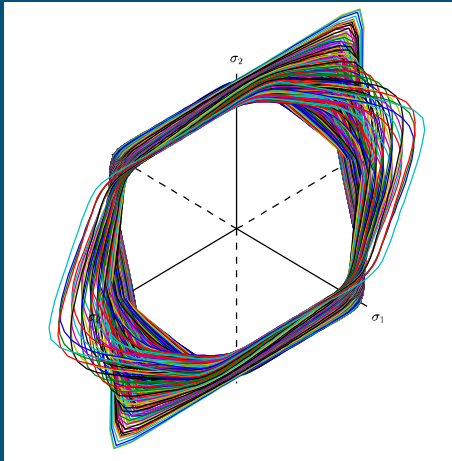


Predict performance from properties:

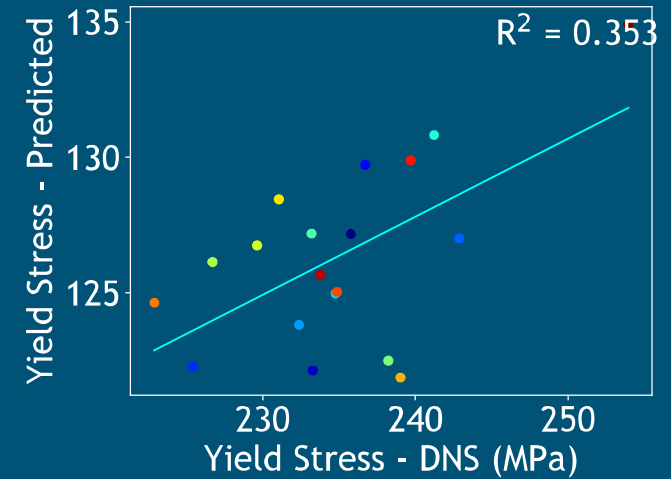
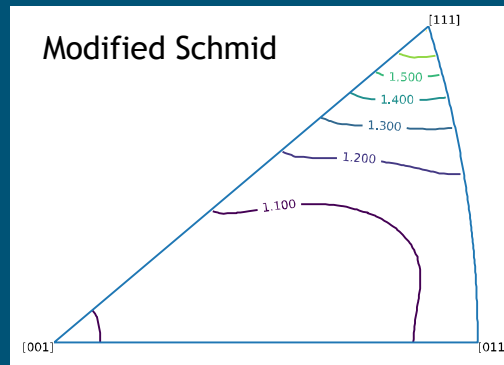
- Property Metrics
 - Beyond average grain size
 - Grain neighborhood character
- Response Metrics
 - Characterize heterogeneity
 - Locally triaxial stress state, but globally uniaxial
 - Isotropic macroscale; anisotropic mesoscale
- Mapping from property metrics to response metrics
 - Framework to upscale response

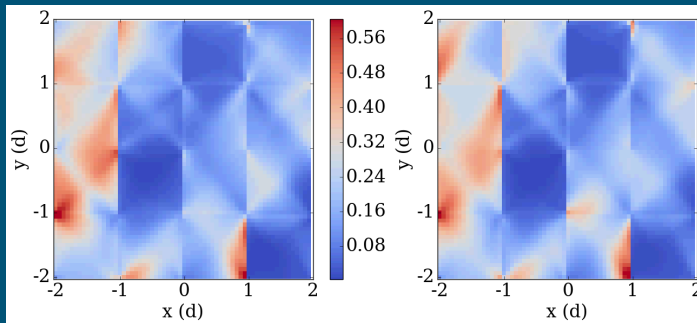
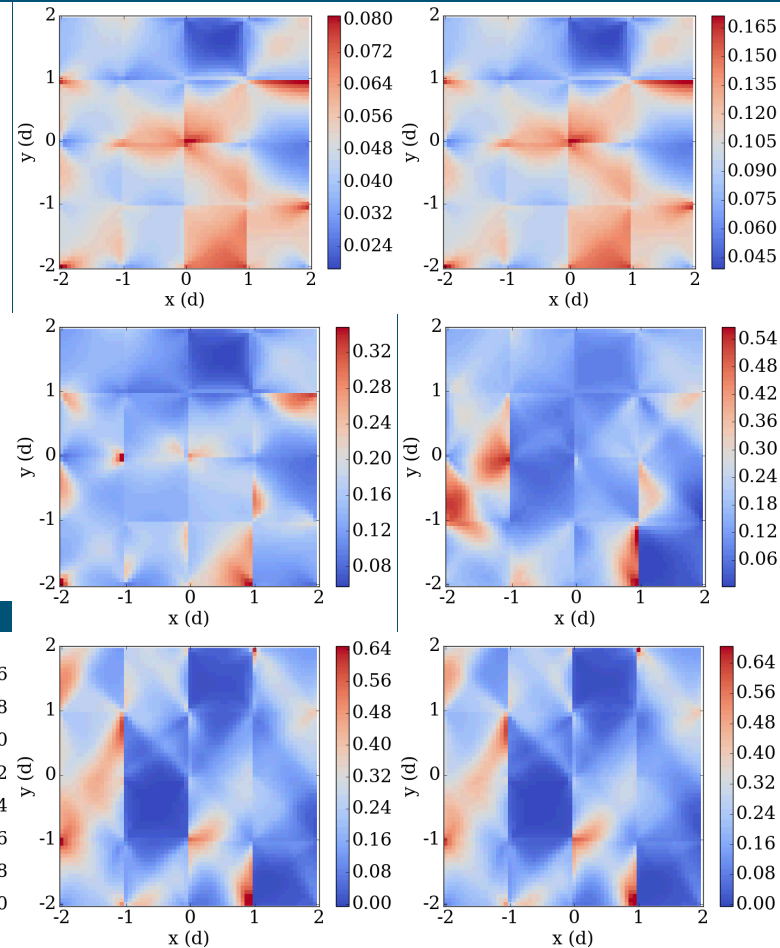
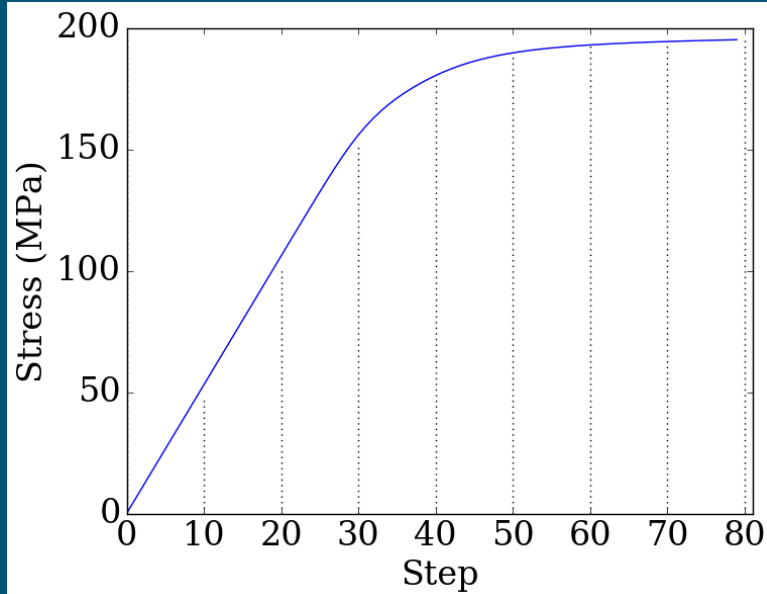


Yield loci for anisotropic single crystals oriented throughout the orientation space.

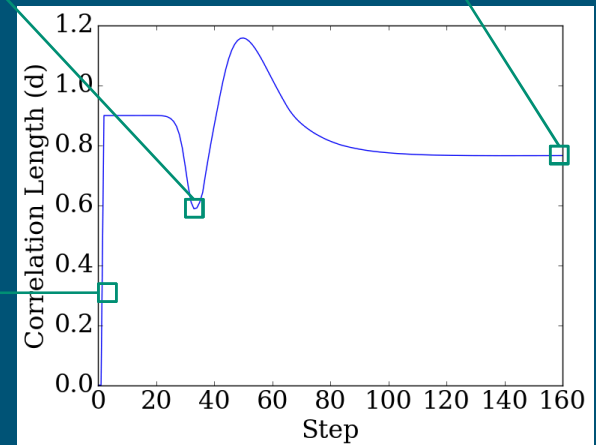
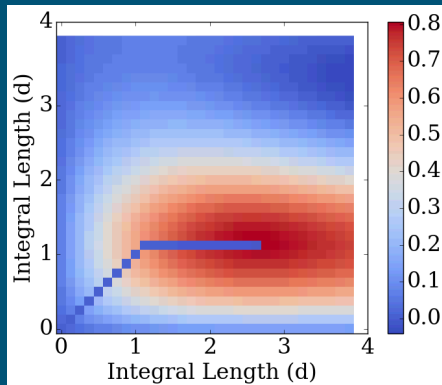
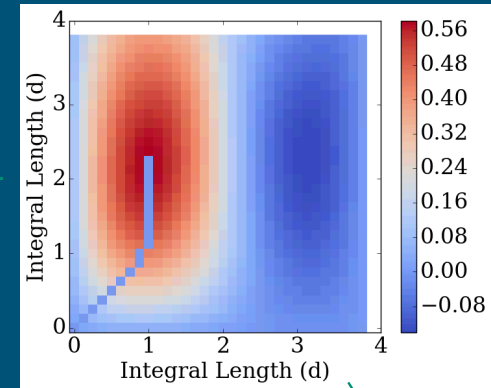
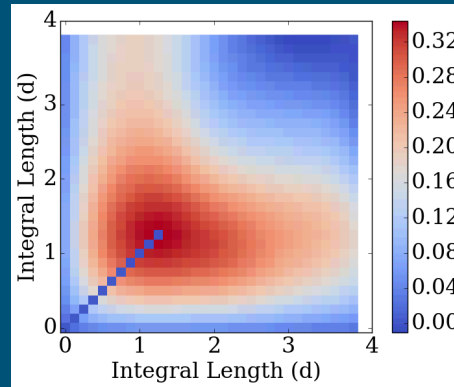
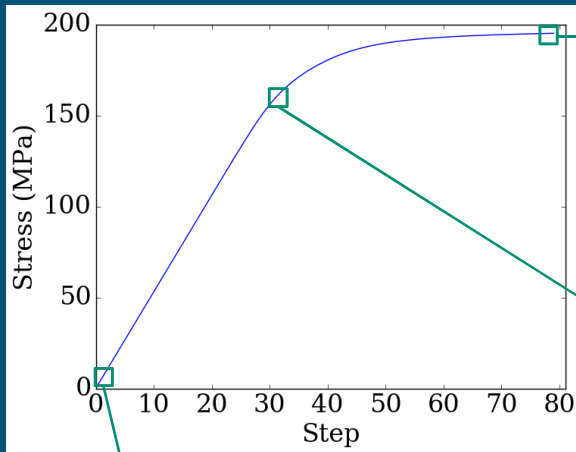


Uniaxial tensile yield strengths for anisotropic single crystals oriented throughout the orientation space.



Total Power, $\underline{\underline{\sigma}} : \underline{\underline{L}}$ 

Correlation Length: Total Power





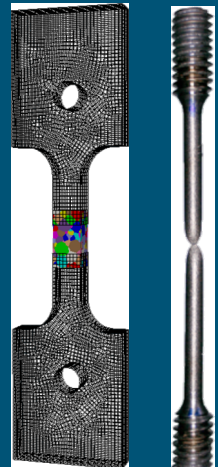
Goal: Understand (predict) localization leading to failure

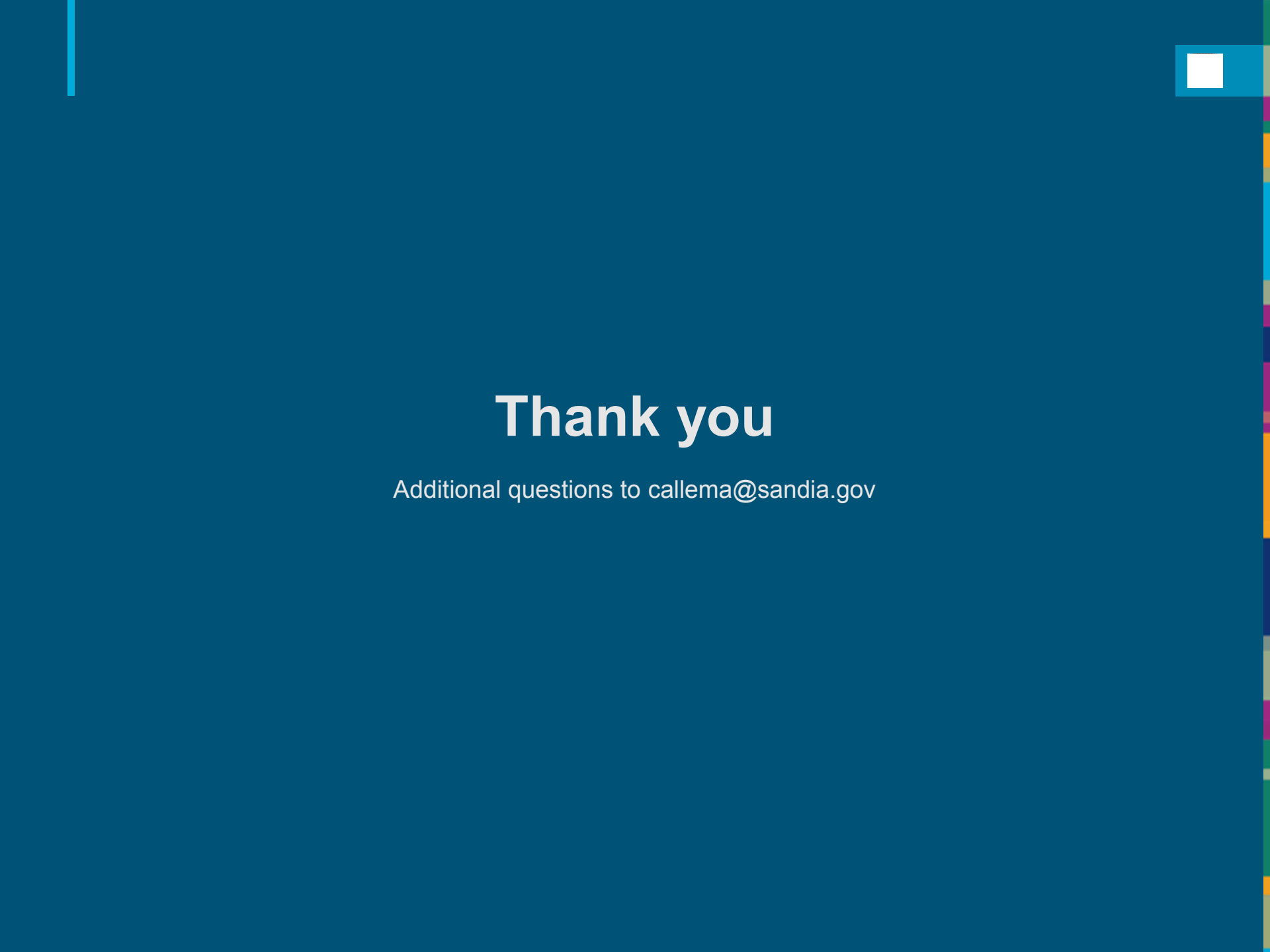
Modeling

- Structure-microstructure coupling (Schwarz)
- Investigating effects of microstructural physics

Coupling to characterization and mechanical testing

- Realistic microstructures
- Rate and temperature dependence
- Identifying/discovering mechanisms of deformation





Thank you

Additional questions to callema@sandia.gov