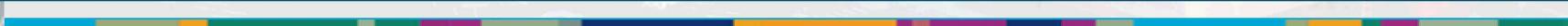


# Nonlocal Models and Peridynamics

Computational Math Seminar  
School of Mathematical and Statistical Sciences  
Clemson University  
March 25, 2020



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**Sandia National Laboratories**



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# Outline

- Local Models, Nonlocal Models, and Length Scales
- Peridynamics Overview
- Example Computations
- Material Models and Failure Models
- Discretizations and Numerical Methods
- Asymptotically Compatible Discretizations
- Nonlocal Calculus
- Condition Number Analysis

# Mathematical Models



- We use numerical solutions of mathematical models to inform high-consequence decisions.**
- When is a mathematical model any good?**
- Model Validation**
  - “Am I solving the right problem?”
  - Is the model sufficient for the application?
  - Is model quantitatively predictive?
  - Is model predictive outside of its calibration range?
- Model Verification**
  - “Am I solving the problem right?”
  - Are the equations solved correctly?
  - Can model produce known analytical solutions?
- We are trained from an early age to use (local) PDE-based models to describe physical phenomena.**
- Today, I'll discuss physical phenomena for which classical models appear inadequate, and for which another mathematical approach may be required.
- Let's start with a discussion on local and nonlocal models, length scales, and multiscale models.



“All models are wrong,  
but some are useful.”

- George Box

# Local and Nonlocal Models

- **Local models** depend upon function values and derivatives at a point

- $f_1(x) = u_{xx}(x), f_2(x) = a u_{xx}(x) + b u_{xxxx}(x)$

- **Nonlocal models** depend upon values of a function at many points

- $f_3(x) = \int_{-\delta}^{\delta} (u(x+y) - u(x)) dy$

- **Some models possess length scales. How can we identify and control them?**

- Scale invariant (self-similar):  $f_1(x) = u_{xx}(x)$

- If  $x$  is rescaled, there exists a rescaling of  $u$  that preserves equation

- A single length scale:  $f_2(x) = a u_{xx}(x) + b u_{xxxx}(x)$

- Length scale is  $\sqrt{b/a}$  (from dimensional analysis)

- Rescaling  $x$  can make first term dominant or second term dominant

- An infinite number of length scales:  $f_3(x) = \int_{-\delta}^{\delta} (u(x+y) - u(x)) dy$

- Consider a series expansion:  $f_3(x) = \frac{\delta^3}{3} u_{xx}(x) + \frac{\delta^5}{60} u_{xxxx}(x) + \frac{\delta^7}{2520} u_{xxxxxx}(x) + \dots$

At a fundamental level, multiscale modeling is about identification of length scales and control of model behavior at those length scales

# Local and Nonlocal Models

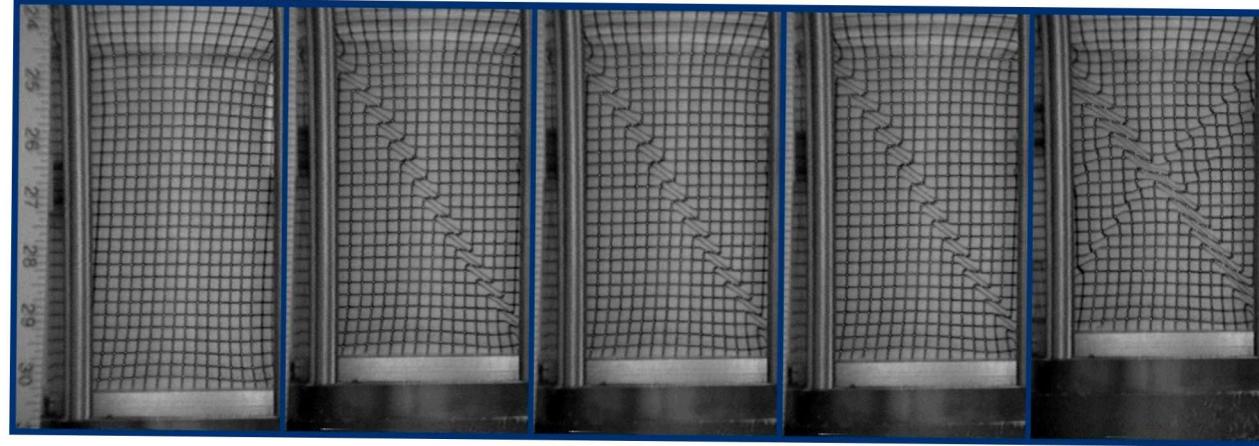
- We use PDE-based (local) models to describe most physical phenomena.
  - Solid mechanics, fluid mechanics, electricity and magnetism, etc.
- Classical PDE-based physics is descriptive of most (?) phenomena...
  - ... except when it isn't.
- Classical models may cease to be descriptive if they cannot represent length scales of all dominant physical processes they are attempting to capture.
  - This includes most *multiscale* phenomena (example: fracture, failure, etc.)
- When our PDE-based models cease to be descriptive, our typical first response is to modify them (or modify their discretization) to make them to elicit desired behavior.
- The critical issue at hand is representation and control of behavior at multiple length scales.
  - In practice, nonlocal models do this fairly naturally.
- A first-principles matching of length scales in nonlocal models to length scales in observed physical phenomena remains an open question for many applications.

# Nonlocal Models & Length Scale Effects

- Length scale effects arise in many applications



Specimen before test



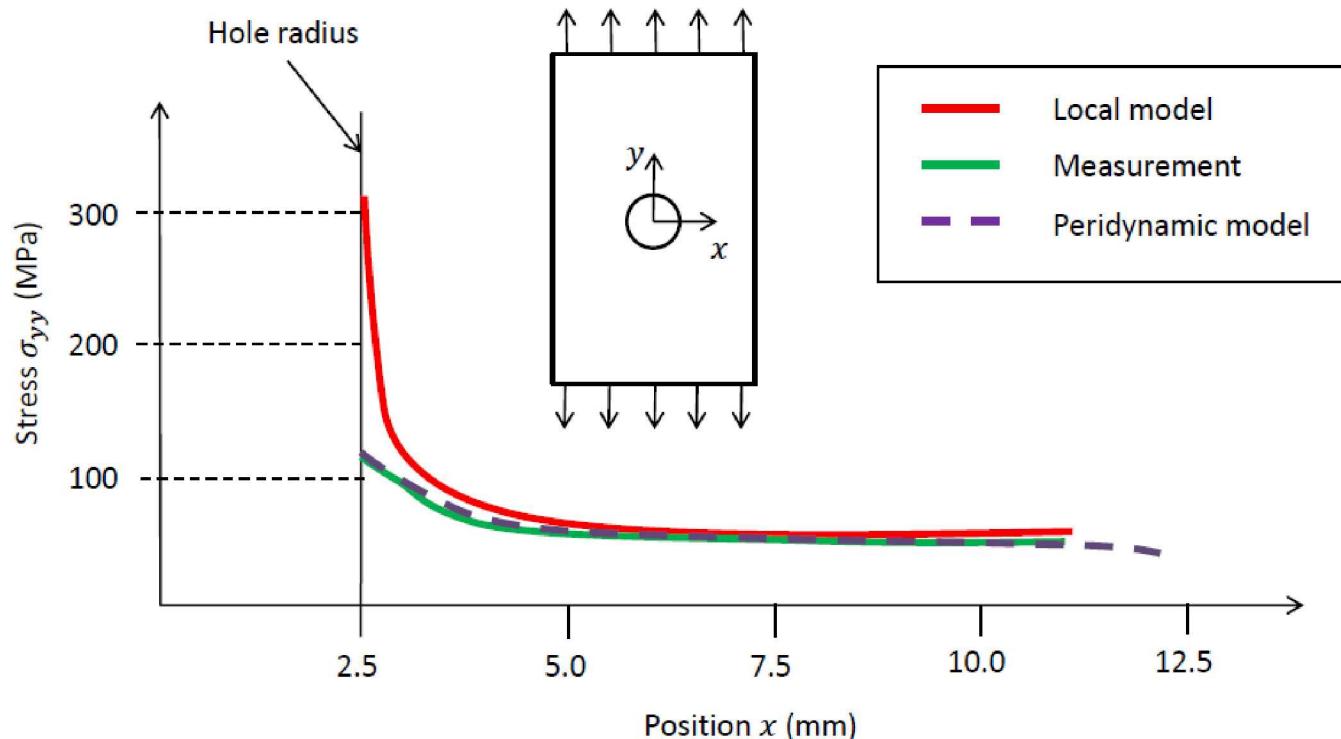
Onset of strain localization into shear band for F-75 Ottawa sand\*

- Example: Size of shear band (strain localization)

- A shear band is a narrow zone of intense shearing that develops during severe deformation of ductile materials.
- Finite element models of shear bands show **size of band decrease as mesh is refined**, meaning mesh length scale is controlling shear band size (nonphysical)!
- Higher gradient models introduced to control this behavior. Introduces additional length scales (ad-hoc).
- Nonlocal models can preserve size of shear band under mesh refinement.

# Nonlocal Models & Length Scale Effects

- Length scale effects arise in many applications



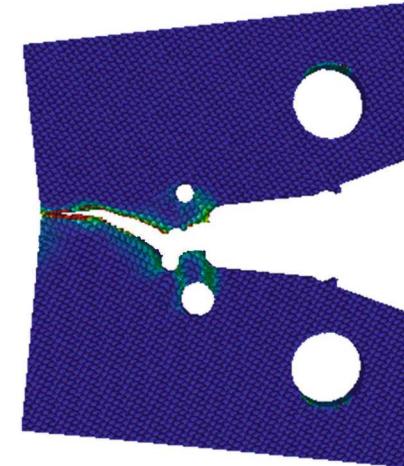
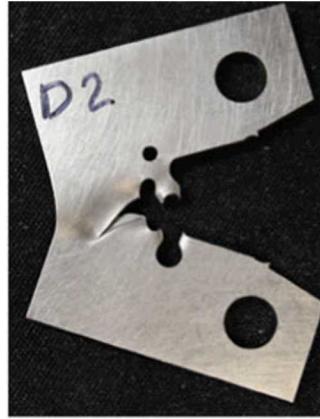
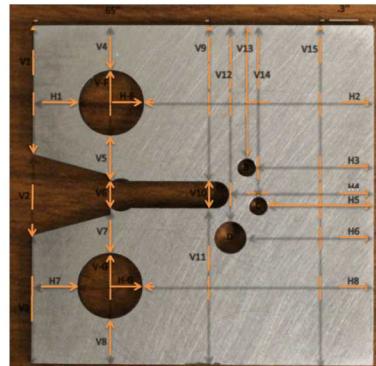
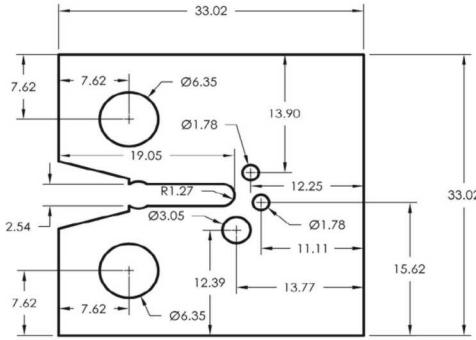
## Heterogeneous media\*

- Comparison of stress along the midplane in an open hole tension test on a fabric-reinforced composite.
- Local theory over-predicts the stress concentration, as compared with optically measured data.
- Peridynamic model has better agreement, apparently due to nonlocality.

# Nonlocal Models & Length Scale Effects



- Length scale effects arise in many applications



- Fracture and Failure\*
- Classical theory predicts infinite stress ( $1/\sqrt{r}$  singularity) at crack tip.
- Classical theory (based on PDEs) not defined on crack surfaces
- Common numerical approaches (XFEM, etc.) enrich solution space with (for example) heaviside functions to allow admission of discontinuous solutions
- Nonlocal models avoid infinities and are defined everywhere (on and off cracks).

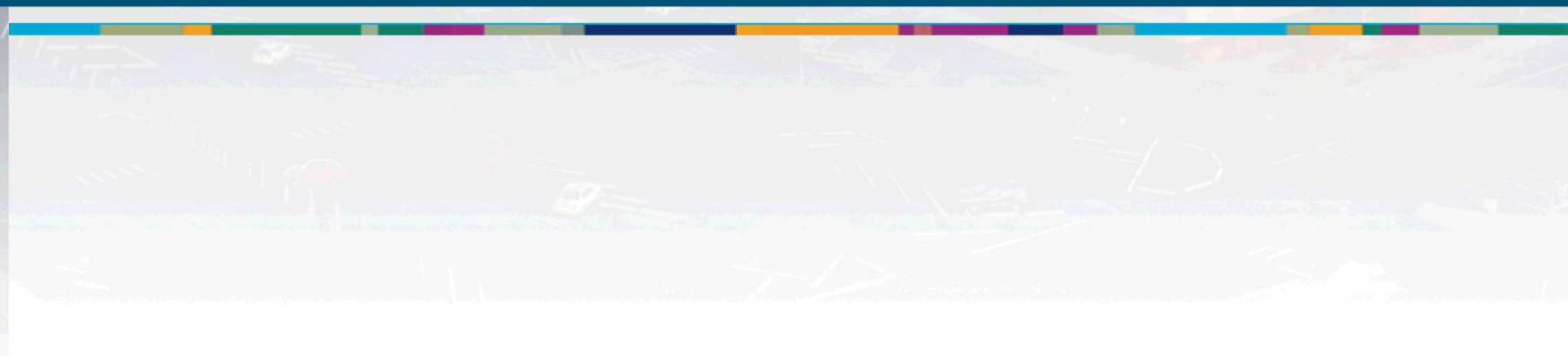
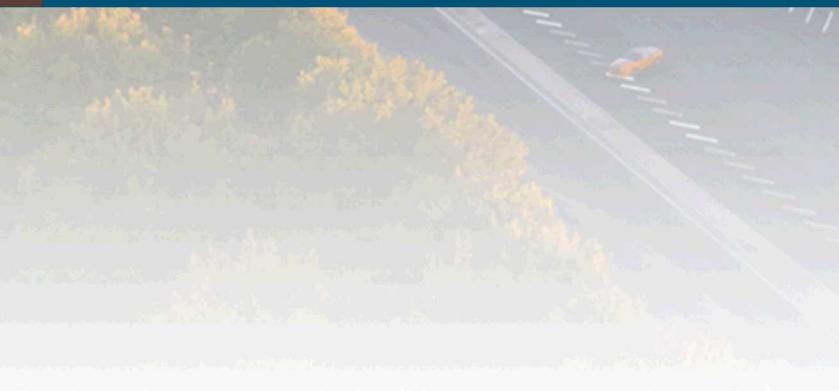
# Nonlocal Models



- Nonlocality and nonlocal models are not a new concept.
- There are a large number of nonlocal models used in computational science
  - Particle models: DPD, SPH, MPM, MD, ...
  - Nonlocal continuum models: Eringen, Bazant, Kunin, Kromer, ...
- Peridynamics, a nonlocal extension of classical continuum mechanics, has been demonstrated to be a superset of some prior nonlocal models:
  - SPH [G.C. Ganzenmüller, S. Hiermaier, M. May, 2015]
  - MD [Seleson, P, Gunzburger, Lehoucq, 2009]
  - Theories of Kunin [Kunin, 1982]
  - Theories of Rogula [Rogula, 1982]



# Peridynamics Overview



# What is Peridynamics?

- Peridynamics is a nonlocal extension of classical solid mechanics

- Peridynamic equation of motion (integral, nonlocal)

$$\rho \ddot{u}(x, t) = \int_{H_x} f(u(x') - u(x), x' - x) dV' + b(x, t)$$

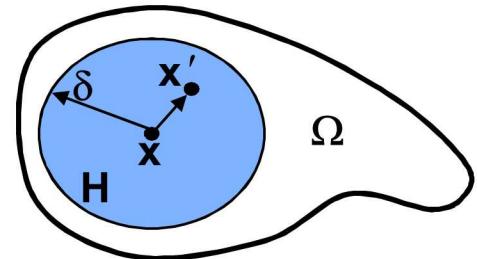
- Replace PDEs with integral equations
- Utilize same equation everywhere; nothing “special” about cracks
- No assumption of differentiable fields (admits fracture)
- No obstacle to integrating nonsmooth functions
- $f(\cdot, \cdot)$  is “force” function; contains constitutive model
- $f = 0$  for points  $x, x'$  more than  $\delta$  apart (like cutoff radius in MD!)
- Peridynamics is “continuum form of molecular dynamics”

- Impact

- Nonlocality
- Larger solution space (fracture)
- Account for material behavior at small & large length scales (multiscale material model)

- Ancestors

- Kröner, Eringen, Edelen, Kunin, Rogula, etc.



Point  $x$  interacts directly with all points  $x'$  within  $H$

“It can be said that all physical phenomena are nonlocal. Locality is a fiction invented by idealists.”

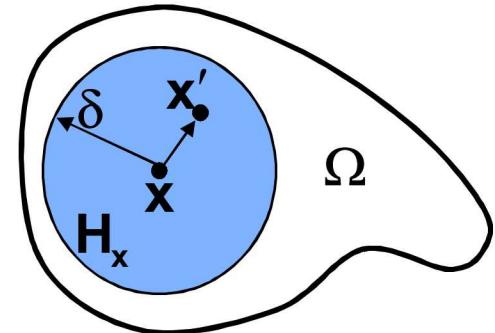


# Peridynamics: The Basics



## □ Horizon and family

- Point  $x$  interacts directly with all points with distance  $\delta$  (horizon)
- Material within distance  $\delta$  of  $x$  is denoted  $H_x$  (family of  $x$ )



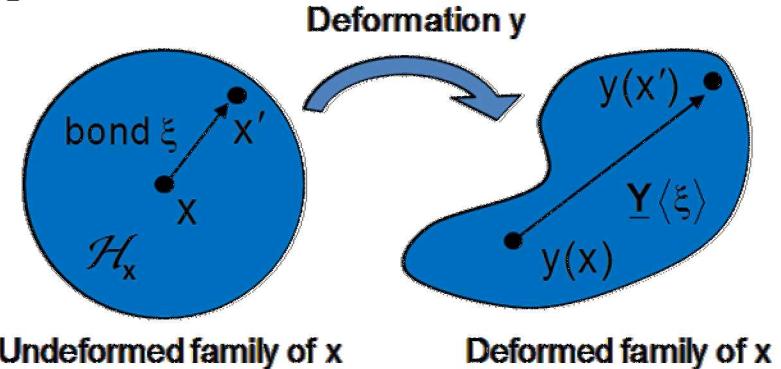
## □ Bonds and bond forces

- Vector between  $x$  and any point in its family is called a bond:  $\xi = x' - x$
- Each bond has pairwise force density vector applied at both points:  $f(x', x, t)$
- This vector is determined jointly by collective deformation of  $H_x$  and collective deformation of  $H_{x'}$
- Bond forces are antisymmetric:  $f(x', x, t) = -f(x, x', t)$
- Bond degrade and fail, admitting damage, failure, and fracture

## □ Deformation state

- Deformation state operator  $\underline{Y}$  maps each bond  $\xi$  into its deformed image

$$\underline{Y} \langle \xi \rangle = y(x') - y(x)$$



# Peridynamics: The Basics

## □ Bonds and states

- $f(x', x)$  has contributions from material models at both  $x$  and  $x'$

$$f(x', x) = \underline{T}[x, t] \langle x' - x \rangle - \underline{T}[x', t] \langle x - x' \rangle$$

- $\underline{T}[x]$  is the force state – it maps bonds onto bond force densities

- $\underline{T}[x]$  is determined by the constitutive model  $\underline{T} = \hat{T}(\underline{Y})$ , where  $\hat{T}$  maps deformation state to force state

## □ Peridynamics vs. standard equations

Relation	Peridynamic theory	Standard theory
Kinematics	$\underline{Y} \langle x' - x \rangle = y(x') - y(x)$	$\underline{F}(x) = \frac{\partial y}{\partial x}(x)$
Linear momentum balance	$\rho \ddot{u}(x) = \int_{H_x} (\underline{T}[x] \langle x' - x \rangle - \underline{T}[x'] \langle x - x' \rangle) dV_{x'} + b(x)$	$\rho \ddot{y}(x, t) = \nabla \cdot \sigma(x) + b(x)$
Constitutive model	$\underline{T} = \hat{T}(\underline{Y})$	$\sigma = \hat{\sigma}(F)$
Angular momentum balance	$\int_{H_x} \underline{Y} \langle x' - x \rangle \times \underline{T} \langle x' - x \rangle dV_{x'} = 0$	$\sigma = \sigma^T$
Elasticity	$\underline{T} = W_Y$ (Frechet derivative)	$\sigma = W_F$ (tensor gradient)
First law of thermodynamics	$\dot{\varepsilon} = \underline{T} \bullet \dot{\underline{Y}} + h + r$	$\dot{\varepsilon} = \sigma \cdot \dot{F} + h + r$

# Peridynamics: The Basics

## □ Mechanical Properties of Peridynamics

- **Conserves energy (in absence of fracture, plastic deformation, etc.)**
- **Conserves linear & angular momentum (always)**
- **Obeys the laws of thermodynamics (restrictions on constitutive models)**

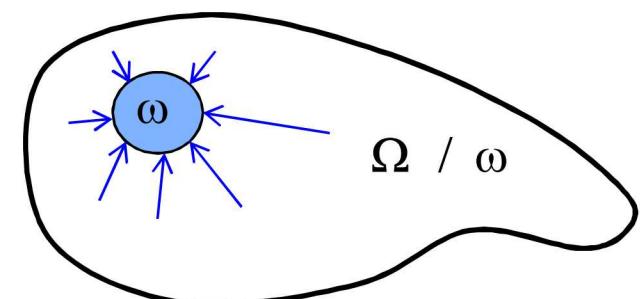
## □ Example: Conservation of Momentum

- **Rate of change of momentum of material within  $\omega$  equals force of body outside  $\omega$  acting upon  $\omega$  plus external body force upon  $\omega$ :**

$$\frac{d}{dt} \int_{\omega} \rho \dot{u}(x, t) dV_x = \int_{\omega} \int_{\Omega/\omega} (T[x, t] \langle x' - x \rangle - T[x', t] \langle x - x' \rangle) dV_{x'} dV_x + \int_{\omega} b(x, t) dV_x$$

- **No self-interaction**

$$\int_{\omega} \int_{\omega} (T[x, t] \langle x' - x \rangle - T[x', t] \langle x - x' \rangle) dV_{x'} dV_x = 0$$



# Peridynamics: The Basics

## □ Energy Balance

- $T$  is work conjugate to  $Y$ :
- This leads to energy balance (first law of thermodynamics)

$$\dot{\varepsilon} = \underline{T} \bullet \dot{\underline{Y}} + \underline{q} + \underline{r}$$

where

- $\varepsilon$  = internal energy density
- $q$  = rate of heat transport
- $r$  = energy source rate

Peridynamic equivalent  
of stress power  $\sigma \cdot \dot{F}$

## □ Thermodynamic Admissibility for Constitutive Models

- Second law of thermodynamics (Clausius-Duhem inequality):

$$\theta \dot{\eta} \geq \underline{q} + \underline{r}$$

where

- $\theta$  = absolute temperature
- $\eta$  = entropy density
- Combining with first law gives thermodynamic admissibility condition for constitutive models:

$$\underline{T} \bullet \dot{\underline{Y}} - \theta \dot{\eta} - \dot{\psi} \geq 0$$

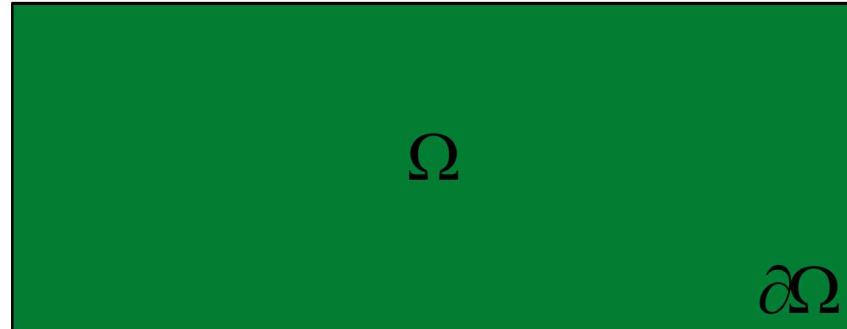
where

- $\psi = \varepsilon - \theta \eta$  is free energy density

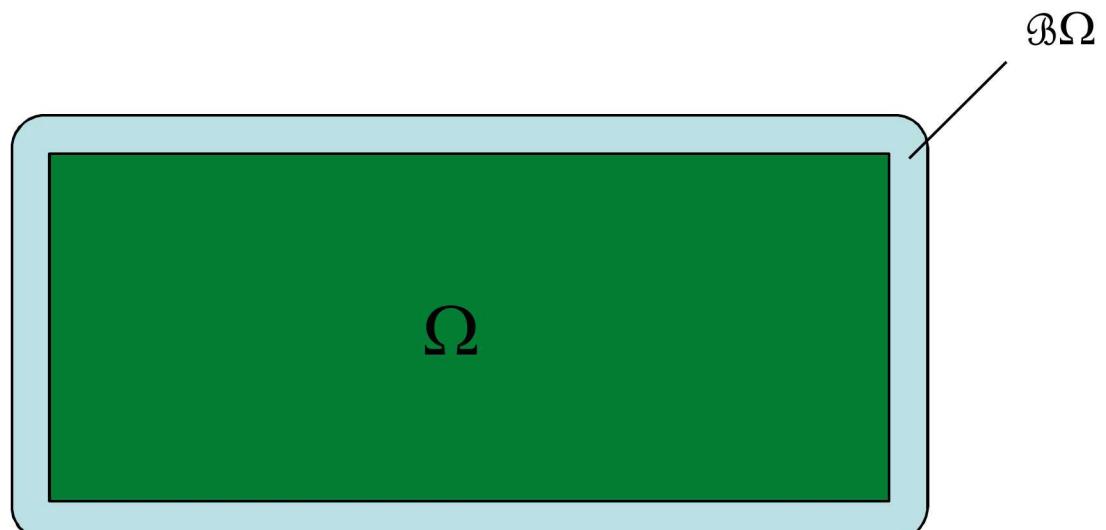
# Nonlocal Boundary Conditions



- For local models (for example, PDE-based models), we apply boundary conditions on the boundary of the domain (hence the name)

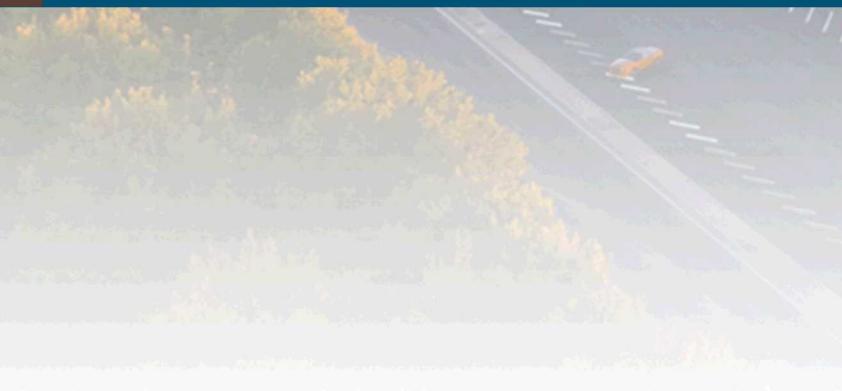


- A Peridynamic “boundary” becomes a volumetric region, sometimes called a “nonlocal boundary”, “collar”, etc.
- Boundary conditions for these models are called “nonlocal boundary conditions”, “volume constraints”, etc.





## Example Computations



# Codes

- **PDLAMMPS (Peridynamics-in-LAMMPS) (Open source, C++)**
  - Developers: Parks, Seleson, Plimpton, Silling, Lehoucq
  - Particular discretization of PD has computational structure of molecular dynamics (MD)
  - LAMMPS: Sandia's open-source massively parallel MD code ([lammps.sandia.gov](http://lammps.sandia.gov))
  - More info & user guide: [www.sandia.gov/~mlparks](http://www.sandia.gov/~mlparks)



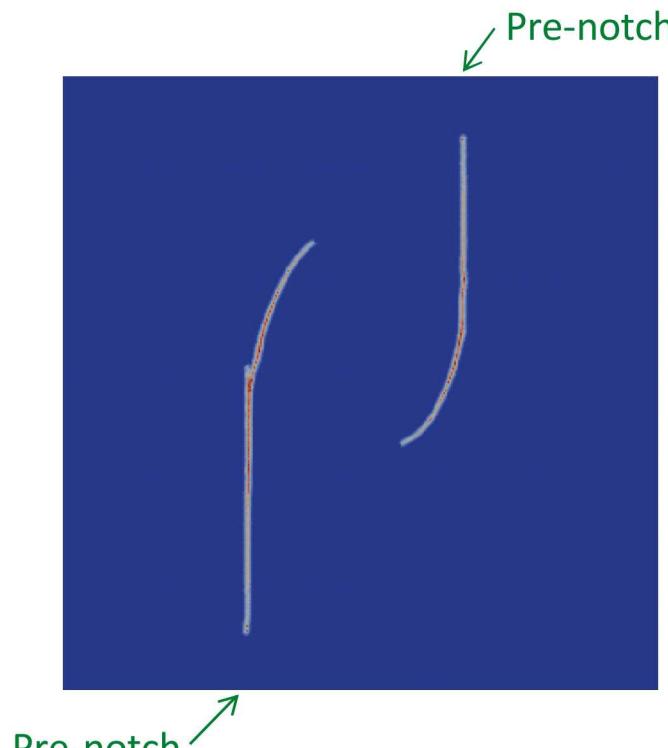
- **Peridigm (Open Source, C++)**
  - <http://peridigm.sandia.gov>; <http://github.com/peridigm/peridigm>
  - Developers: Parks, Littlewood, Mitchell, Silling
  - Intended as Sandia's primary open-source PD code
  - Built upon Sandia's Trilinos Project ([trilinos.sandia.gov](http://trilinos.sandia.gov))
  - Massively parallel
  - Explicit, implicit time integration
  - State-based linear elastic, elastic-plasticity, viscoelastic models
  - DAKOTA interface for UQ/optimization/calibration, etc. ([dakota.sandia.gov](http://dakota.sandia.gov))

# Two Interacting Cracks

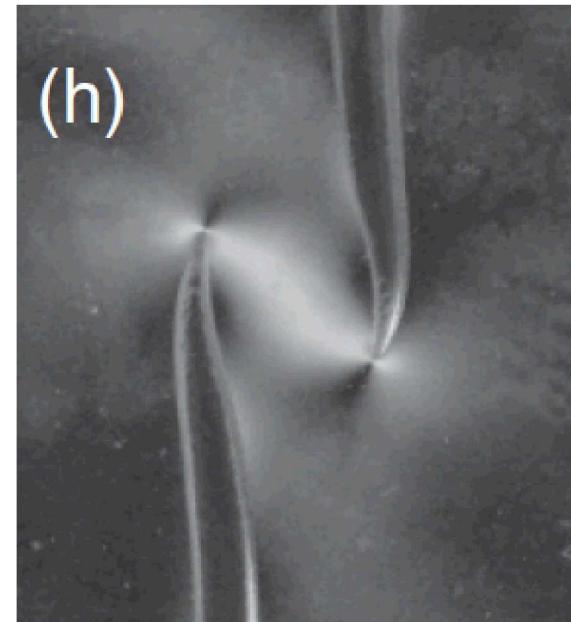


- Offset notches thin rectangular elastic plate
- Uniaxial strain applied from sides
- Approaching cracks produce “en passant” crack pattern

Simulation performed  
with PDLAMMPS



**Peridynamics**



**Physical Experiment\***

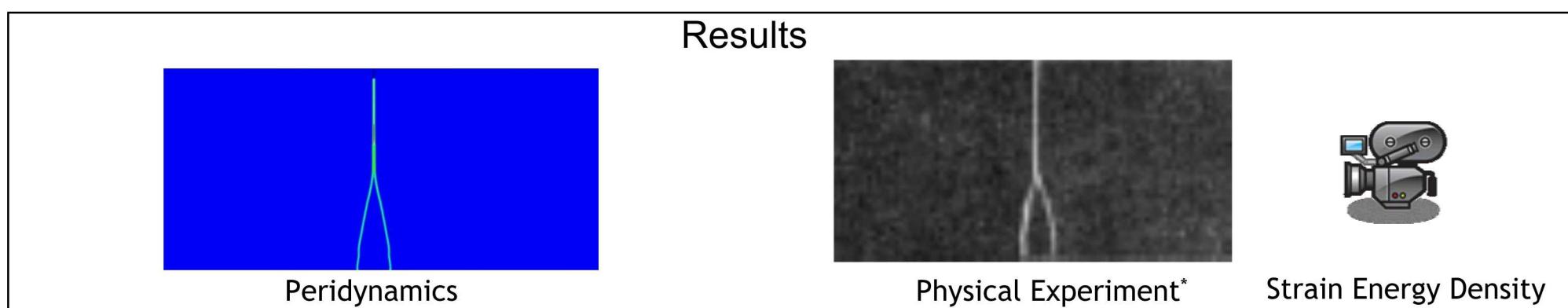
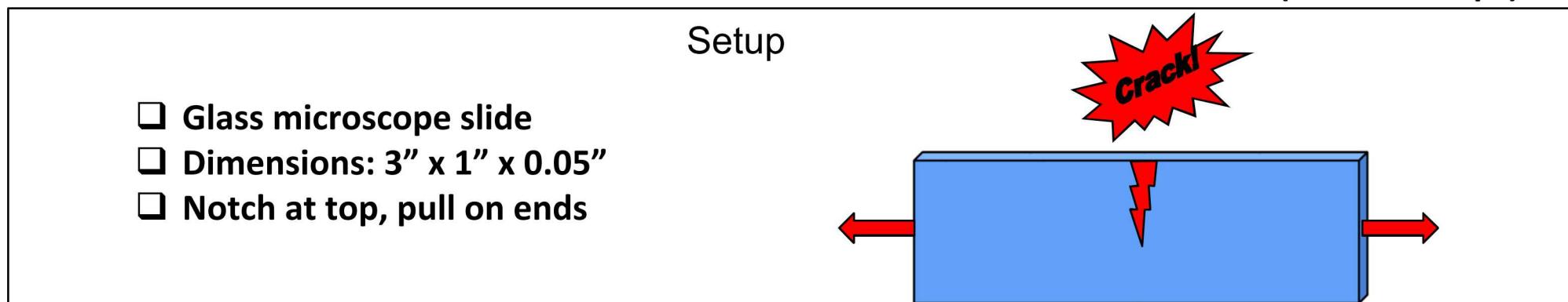
# Fracture in Glass Plate



- Dynamic brittle fracture in glass
  - Joint with Florin Bobaru, Youn-Doh Ha, & Stewart Silling

Simulation performed with PDLAMMPS

- Soda-lime glass plate (microscope slide)
  - Dimensions: 3" x 1" x 0.05"
  - Density: 2.44 g/cm<sup>3</sup>
  - Elastic Modulus: 79.0 Gpa
- Discretization (finest)
  - Mesh spacing: 35 microns
  - Approx. 82 million particles
  - Time: 50 microseconds (20k timesteps)



# Fracture in Glass Plate



## ❑ Dawn (LLNL): IBM BG/P System

- ❑ 500 teraflops; 147,456 cores

## ❑ Part of Sequoia procurement

- ❑ 20 petaflops; 1.6 million cores

## ❑ Discretization (finest)

- ❑ Mesh spacing: 35 microns
- ❑ Approx. 82 million particles
- ❑ Time: 50 microseconds (20k timesteps)
- ❑ 6 hours on 65k cores

## ❑ Largest peridynamic simulations in history

Simulation performed with PDLAMMPS



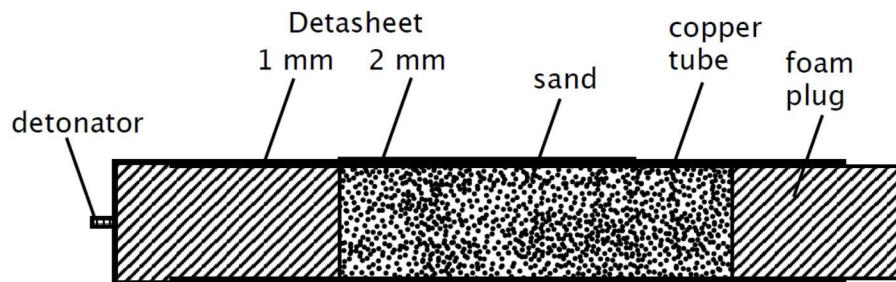
*Dawn at LLNL*

## Weak Scaling Results

# Cores	# Particles	Particles/Core	Runtime (sec)	T(P)/T(P=512)
<b>512</b>	<b>262,144</b>	<b>4096</b>	<b>14.417</b>	<b>1.000</b>
<b>4,096</b>	<b>2,097,152</b>	<b>4096</b>	<b>14.708</b>	<b>0.980</b>
<b>32,768</b>	<b>16,777,216</b>	<b>4096</b>	<b>15.275</b>	<b>0.963</b>

# Explosively Compressed Cylinder\*

- Motived by experiments of Vogler & Lappo\*
- Commonly used for consolidation of powders
- Copper cylinders filled with granular material and wrapped with Detasheet explosive
- Polyurethane foam plugs used to keep granular sample in tube.
  
- Geometry and Material Properties
  - Copper tubes 305 mm long, ID 50.8 mm, wall thickness of 1.52 mm
  - PETN based Detasheet with thicknesses of 1, 2, 4, or 6 mm were used, and a
  - Detonation traveled down length of tube, compressing both tube and sand fill



Cylinder schematic

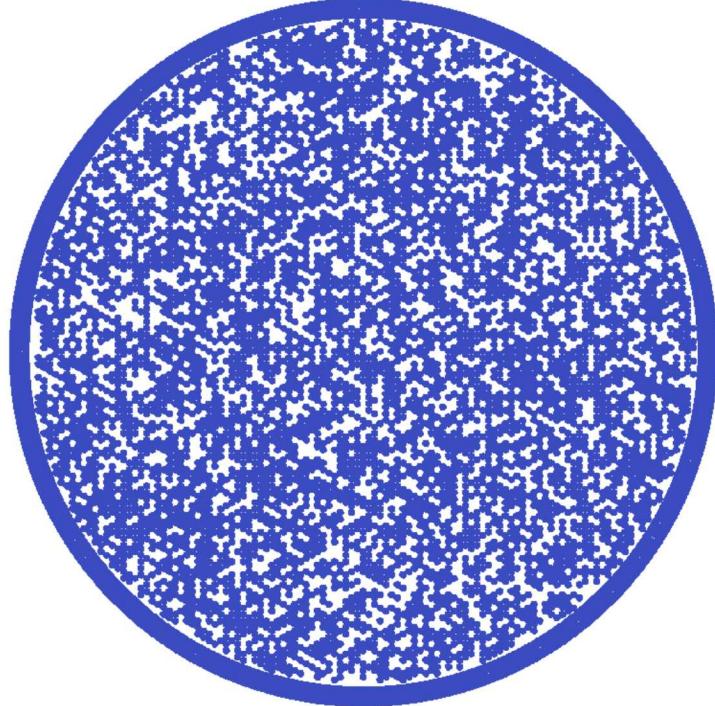


Cylinder after compression

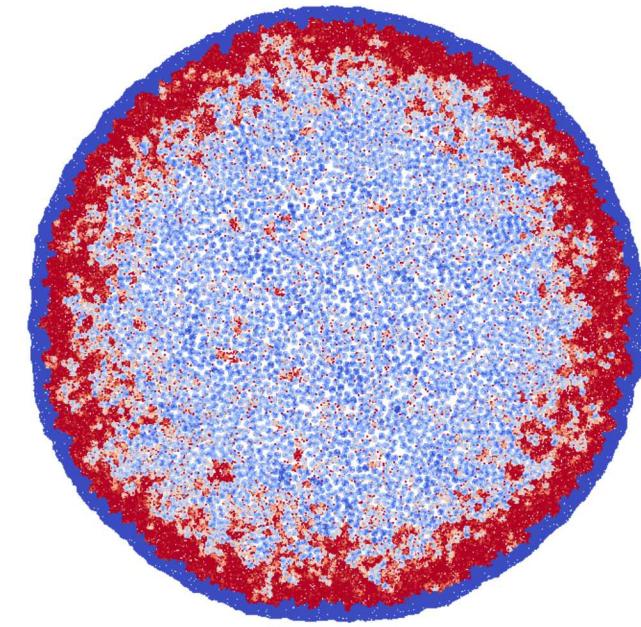
# Explosively Compressed Cylinder

- ❑ Peridigm computational results (with C. Hoffarth, D. Littlewood)
- ❑ Color indicates damage (blue = undamaged, red = damaged)

Simulation performed  
with Peridigm



Before



After

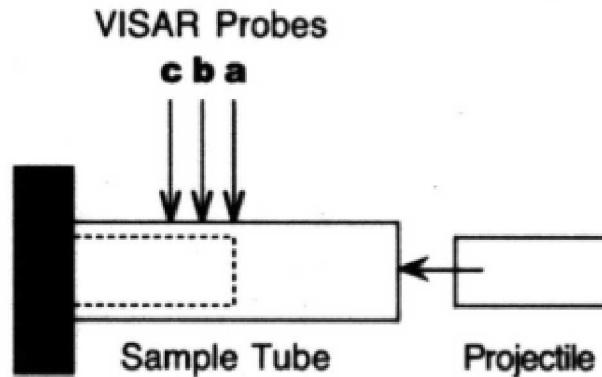
# Expanding Tube Simulation\*\*



## □ Experimental Setup

- Tube expansion via collision of Lexan projectile and plug within AerMet tube
- Accurate recording of velocity and displacement on tube surface

Simulation performed with  
Sierra/SolidMechanics



## □ Modeling Approach

- AerMet tube modeled with peridynamics, elastic-plastic material model with linear hardening
- Lexan plugs modeled with classical FEM, equation-of-state Johnson-Cook material model
- Interaction via contact algorithm

Experimental setup\*



Model discretization

Vogler, T.J., Thornhill, T.F., Reinhart, W.D., Chhabidas, L.C., Grady, D.E., Wilson, L.T., Hurricane, O.A., and Sunwoo, A. Fragmentation of materials in expanding tube experiments. *International Journal of Impact Engineering*, 29:735-746, 2003.

\*\* D. Littlewood. 2010. Simulation of dynamic fracture using peridynamics, finite element modeling, and contact. Proceedings of the ASME 2010 International Mechanical Engineering Congress and Exposition, British Columbia, Canada.

# Expanding Tube Simulation\*\*



Simulation performed with  
Sierra/SolidMechanics

## AerMet Tube

- Peridynamics
- Elastic-plastic constitutive model
- 73,676 sphere elements
- Horizon set to five times element radius

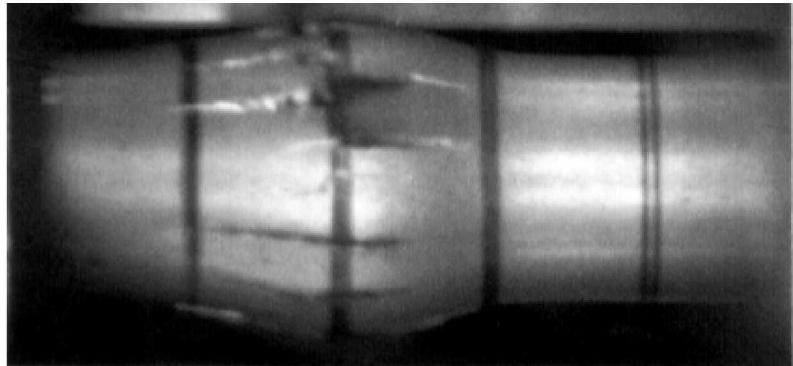
Parameter	Value
Density	7.87 g/cm <sup>3</sup>
Young's Modulus	194.4 GPa
Poisson's Ratio	0.3
Yield Stress	1.72 GPa
Hardening Modulus	1.94 GPa
Critical Stretch	0.02

## Lexan Projectile/Plug

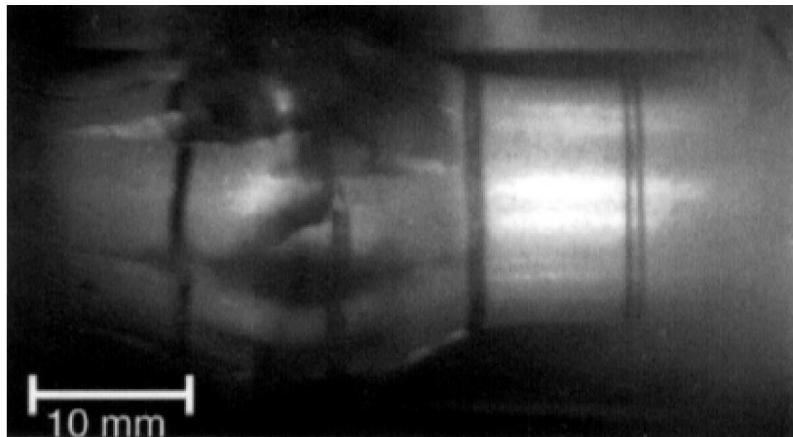
- Classical FEM
- Johnson-Cook constitutive model
- 53,214 hexahedron elements

Parameter	Value
Density	1.19 g/cm <sup>3</sup>
Young's Modulus	2.54 GPa
Poisson's Ratio	0.344
Yield Stress	75.8 MPa
Hardening Constant <i>B</i>	68.9 MPa
Rate Constant <i>C</i>	0.0
Hardening Exponent <i>N</i>	1.0
Thermal Exponent <i>M</i>	1.85
Reference Temperature	70.0 ° F
Melting Temperature	500.0 ° F

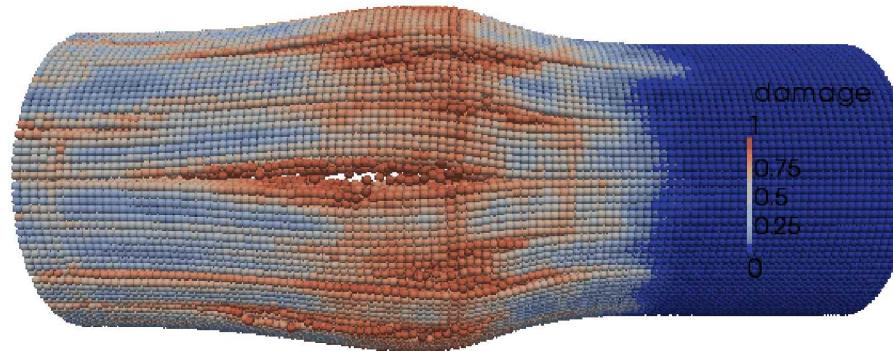
# Expanding Tube Simulation\*\*



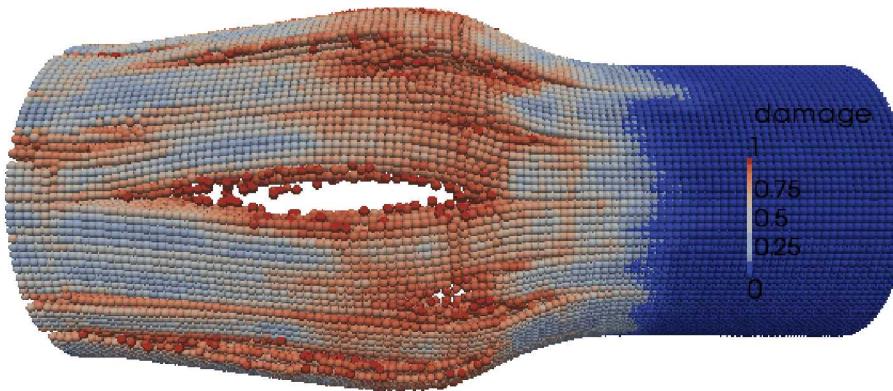
Experimental image at 15.4 microseconds\*



Experimental image at 23.4 microseconds\*



Simulation at 15.4 microseconds\*\*



Simulation at 23.4 microseconds\*\*

Simulation performed with  
Sierra/SolidMechanics

Vogler, T.J., Thornhill, T.F., Reinhart, W.D., Chhabidas, L.C., Grady, D.E., Wilson, L.T., Hurricane, O.A., and Sunwoo, A. Fragmentation of materials in expanding tube experiments. *International Journal of Impact Engineering*, 29:735-746, 2003.

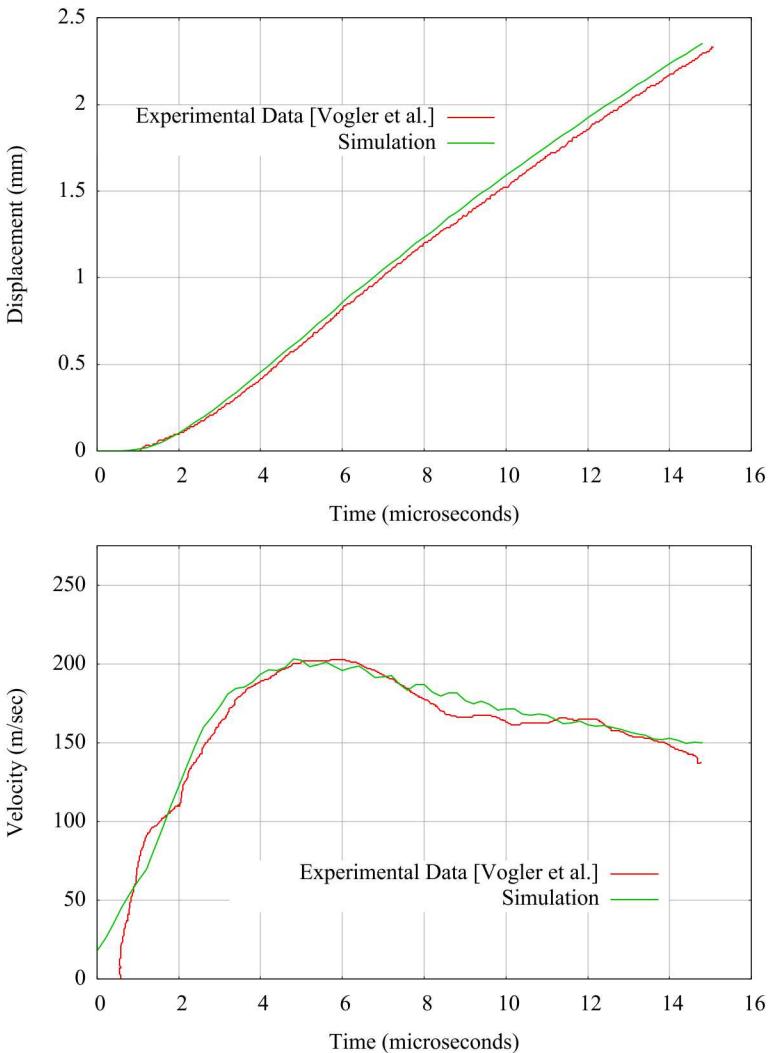
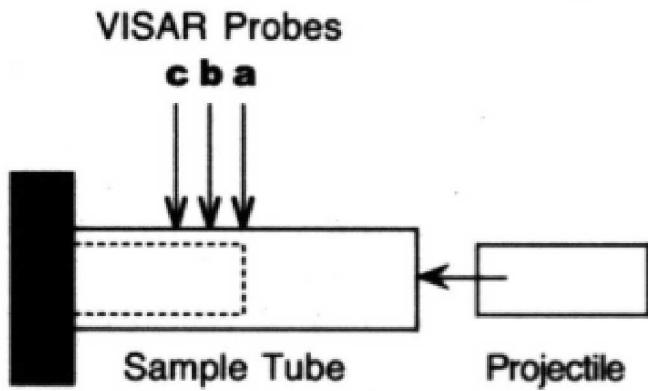
\*\* D. Littlewood. 2010. Simulation of dynamic fracture using peridynamics, finite element modeling, and contact. *Proceedings of the ASME 2010 International Mechanical Engineering Congress and Exposition*, British Columbia, Canada.

# Expanding Tube Simulation\*\*



Simulation performed with  
Sierra/SolidMechanics

Displacement and velocity  
on tube surface  
at probe position A

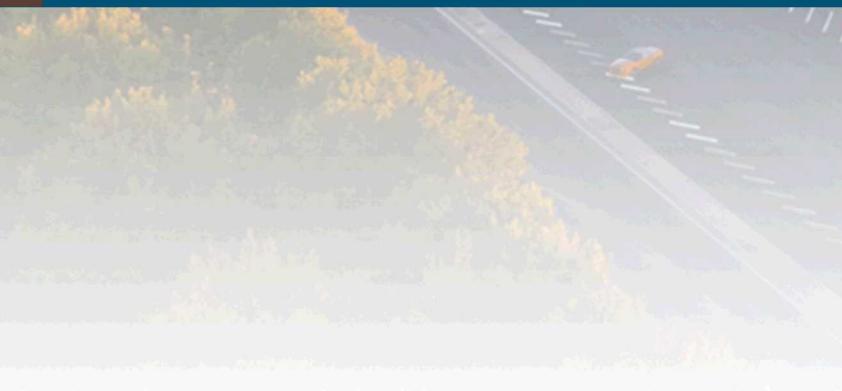


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# Material Models and Fracture Models



# Peridynamic Material Models

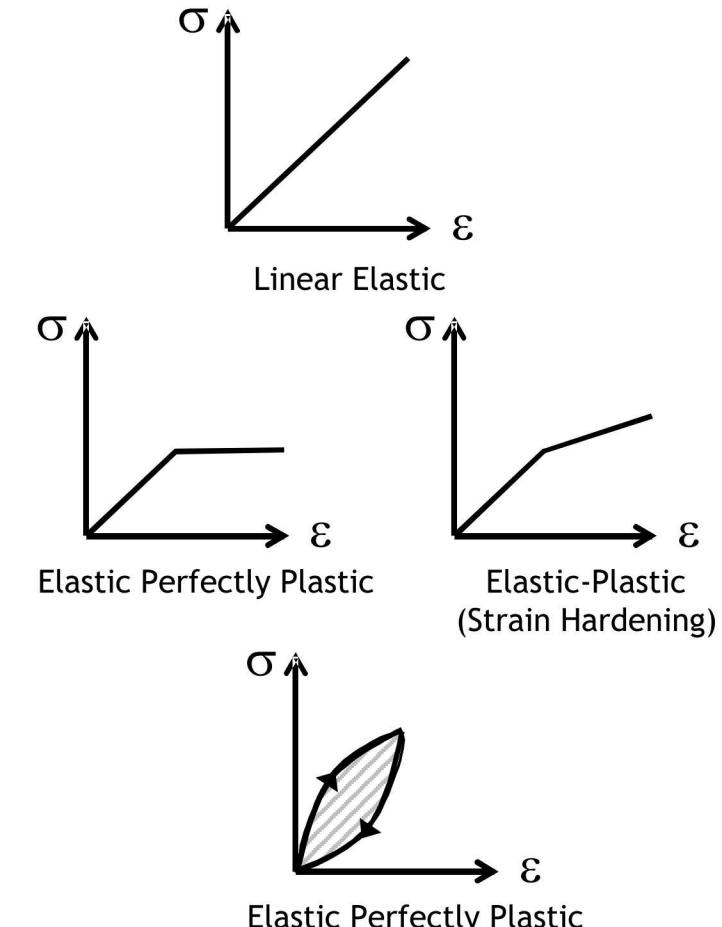


- Quick survey of some material classes
- **Linear Isotropic Elastic Materials**
  - Hooke's law
  - Returns to reference configuration when released
  - Example: spring

- **Elastic-Plastic Materials**
  - Elastic for small deformations (< 1% strain)
  - Deforms plastically for larger deformations
  - Example: spring (when stretched too far)

- **Viscoelastic Materials**
  - Exhibit viscous and elastic properties under deformation
  - Hysteresis in stress/strain curves
  - Example: skin (pinch it and let it recover)\*

- Can wrap classical material models (existing material libraries) in peridynamic “skin”
- PD codes (Peridigm, PDLAMMPS) allow users to define their own material models



# Peridynamic Material Modeling

- Linear Peridynamic Solid (LPS)\*
  - Nonlocal analog to linear isotropic elastic solid
  - $k$  is bulk modulus,  $\mu$  is shear modulus

$$\rho \ddot{\mathbf{u}}(\mathbf{x}, t) = \int_{\mathbb{H}} \left( \mathbf{T}[\mathbf{x}, t] \langle \mathbf{x}' - \mathbf{x} \rangle - \mathbf{T}[\mathbf{x}', t] \langle \mathbf{x} - \mathbf{x}' \rangle \right) dV_{\mathbf{x}'} + \mathbf{b}(\mathbf{x}, t)$$

$$\mathbf{T}[\mathbf{x}, t] \langle \mathbf{x}' - \mathbf{x} \rangle = \left( \frac{3k\theta}{m} \underline{\omega} \underline{\mathbf{x}} + \frac{15\mu}{m} \underline{\omega} \mathbf{e}^d \right) \frac{\mathbf{x}' - \mathbf{x}}{\|\mathbf{x}' - \mathbf{x}\|}$$

# Peridynamic Material Models

- Elastic-Plastic Model\*
  - Nonlocal analogue to perfect plasticity model
  - Relevant for ductile materials and ductile failure
- Rate equations and constraints
  - Additive decomposition of extension state:  $\mathbf{e}^d = \mathbf{e}^{de} + \mathbf{e}^{dp}$
  - Elastic force state relations:

$$\mathbf{T}[\mathbf{x}, t] \langle \mathbf{x}' - \mathbf{x} \rangle = \left( \frac{3k\theta}{m} \underline{\omega} \underline{\mathbf{x}} + \alpha \underline{\omega} (\mathbf{e}^d - \mathbf{e}^{dp}) \right) \frac{\mathbf{y}' - \mathbf{y}}{\|\mathbf{y}' - \mathbf{y}\|}$$

- Elastic force state domain defined by yield surface/function that depends upon deviatoric force state:
  - $f(t_d) = \psi(t^d) - \psi_0 \leq 0$ , where  $\psi(t^d) = \frac{1}{2} \| \mathbf{t}^d \|^2$
- Flow rule describing rate of plastic deformation:  $\dot{\mathbf{e}}^{dp} = \lambda \nabla^d \Psi$
- Loading/un-loading conditions (Kuhn-Tucker constraints):
  - $\lambda > 0, f(t^d) \leq 0,$
  - Consistency condition:  $\lambda \dot{f}(t^d) = 0$

# Peridynamic Material Models



## □ Viscoelastic Model\*

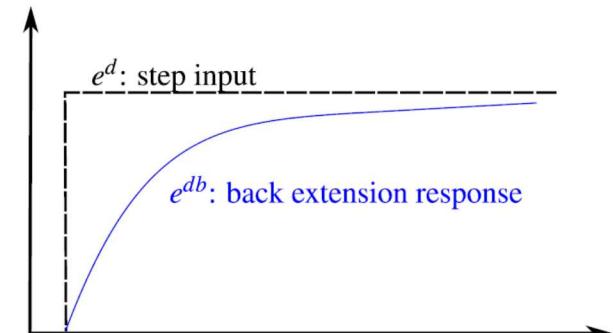
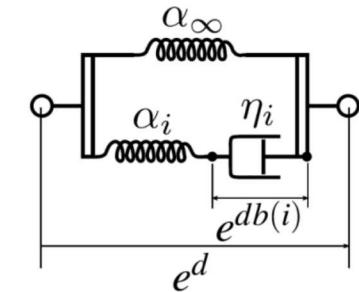
- Nonlocal analog to standard linear solid
- Applicable where rate effects important
- Adds viscous terms to deviatoric portion of extension state; bulk response remains elastic
- Logical intermediate step between fluid and solid
- viscous fluid: little or no elastic resistance to shear (fluids flow) but resists compressive volumetric deformations
- elastic solid: elastic resistance to both shear and volumetric deformations

## □ Viscoelastic Model\*

- Nonlocal analog to standard linear solid

$$\begin{aligned} \text{□ Scalar deviatoric force: } \mathbf{t}^d &= \eta_i \dot{\mathbf{e}}^{db} \\ &= \alpha_i (\mathbf{e}^d - \mathbf{e}^{db}) \end{aligned}$$

$$\text{□ Evolution equation: } \dot{\mathbf{e}}^{db} = \frac{1}{\tau^b} (\mathbf{e}^d - \mathbf{e}^{db})$$



Memory Foam

# Peridynamic Fracture Modeling

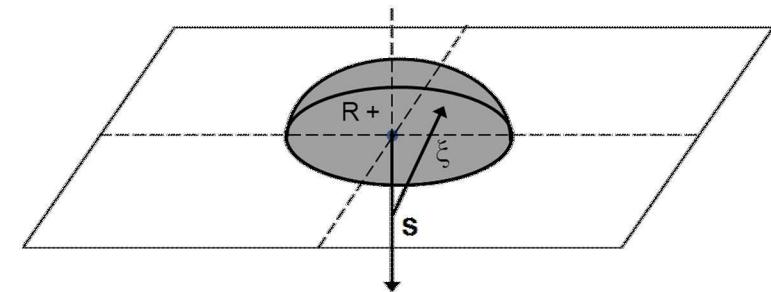
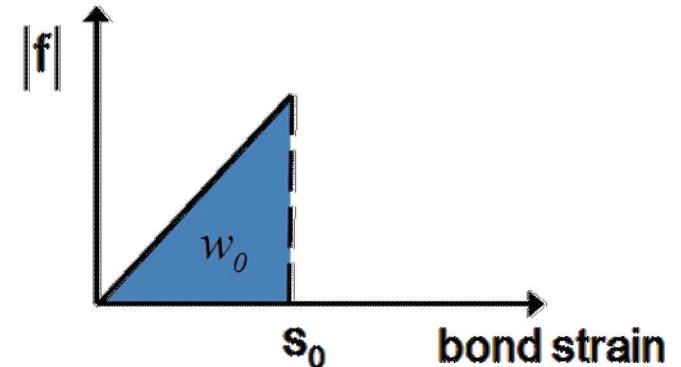


## □ Fracture

- Break bond if bond stretch  $s$  exceeds critical stretch  $s^*$
- If work to break bond  $\xi$  is  $w_0(\xi)$ , then energy release rate found by summing this work per unit crack area

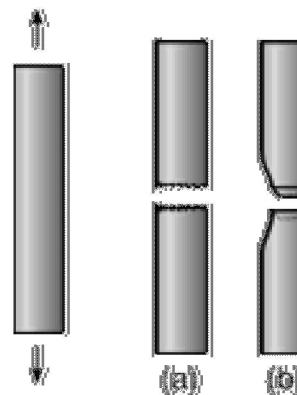
$$G = \int_0^\delta \int_{R_+} w_0(\xi) dV_\xi ds$$

- Can then get the critical strain  $s^*$  for bond breakage in terms of  $G$  (strain energy release rate), an experimentally measurable quantity



## □ Fracture

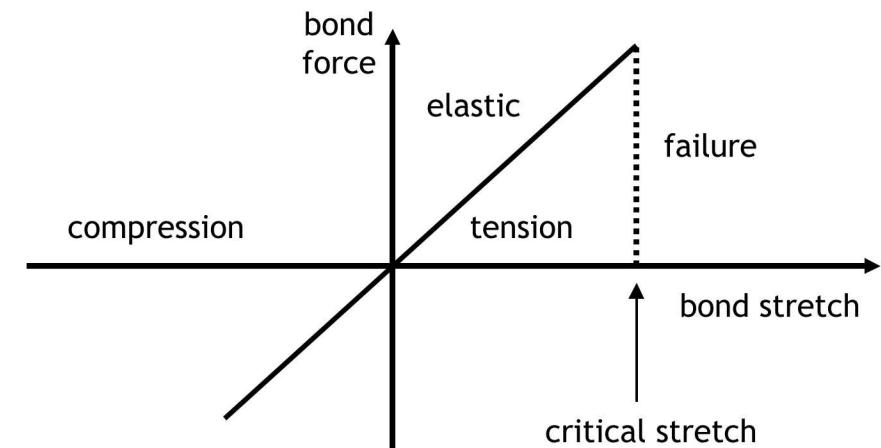
- (a) Brittle
- (b) Ductile



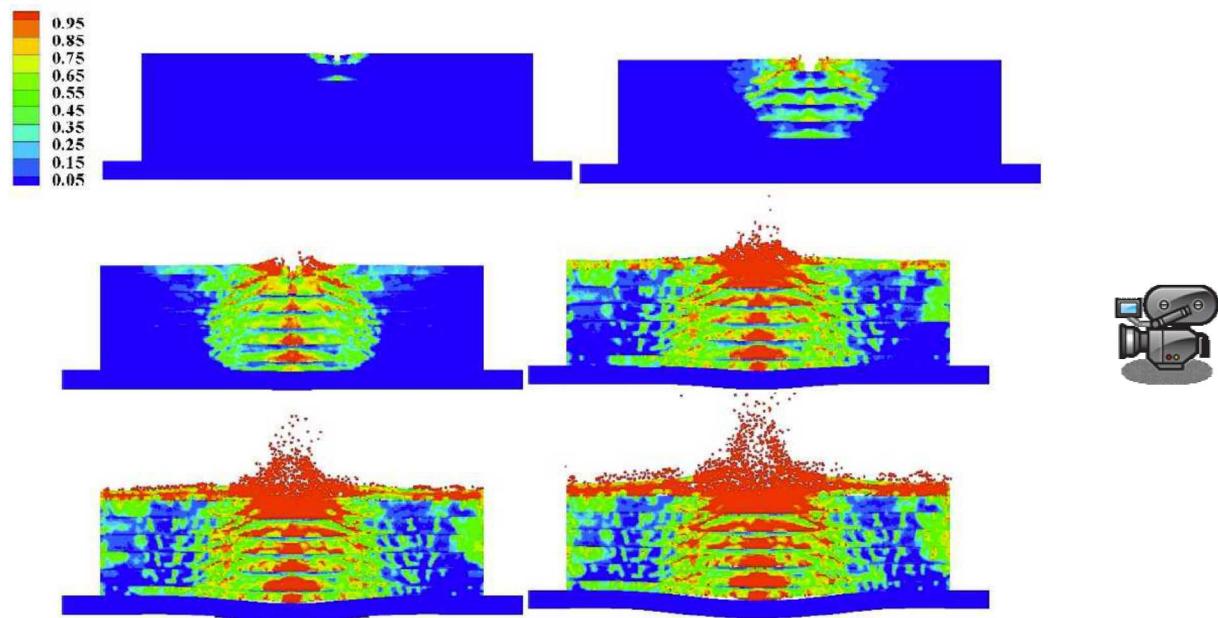
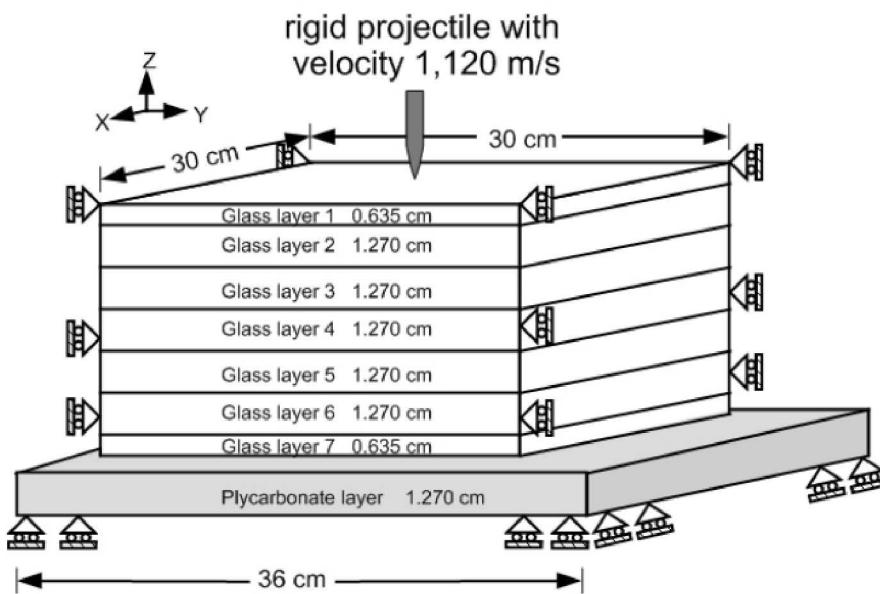
# Peridynamic Fracture Modeling (Brittle)



- **Brittle Fracture**
  - No plastic deformation takes place before failure
  - Typically involves catastrophic failure
  - Bond responds elastically until failure at critical stretch



- **Example: Impact in Layered Glass**
  - No plastic deformation takes place before failure

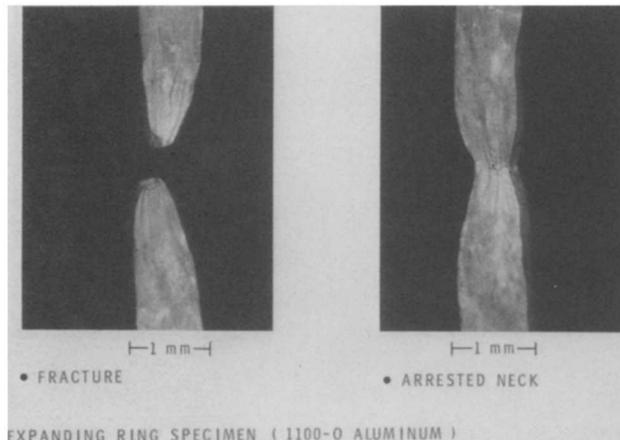
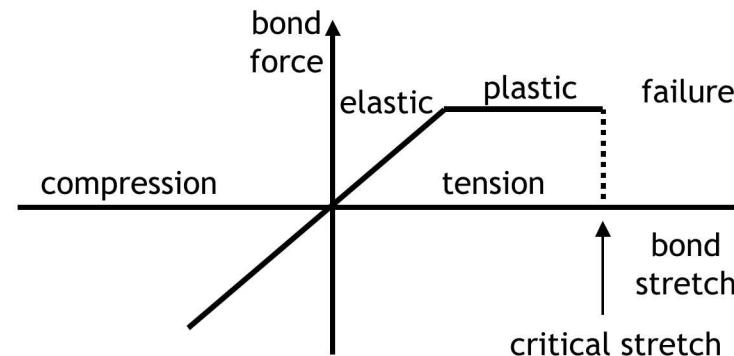


# Peridynamic Fracture Modeling (Ductile)

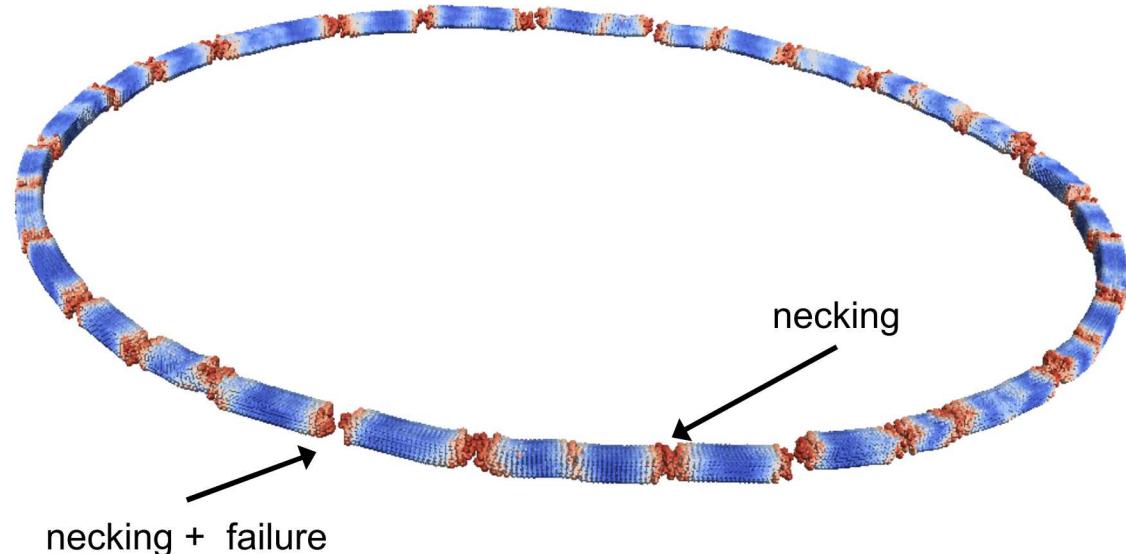


Simulation performed with Peridigm

- Ductile fracture
  - Plastic deformation before failure
  - Can typically sustain large strain before failure
  
- Example: Electromagnetically loaded ring
  - 1100-0 aluminum ring (ductile)
  - Motivated by ring fragmentation experiments of Grady & Benson\*
  - Used peridynamic elastic/plastic model\*\*

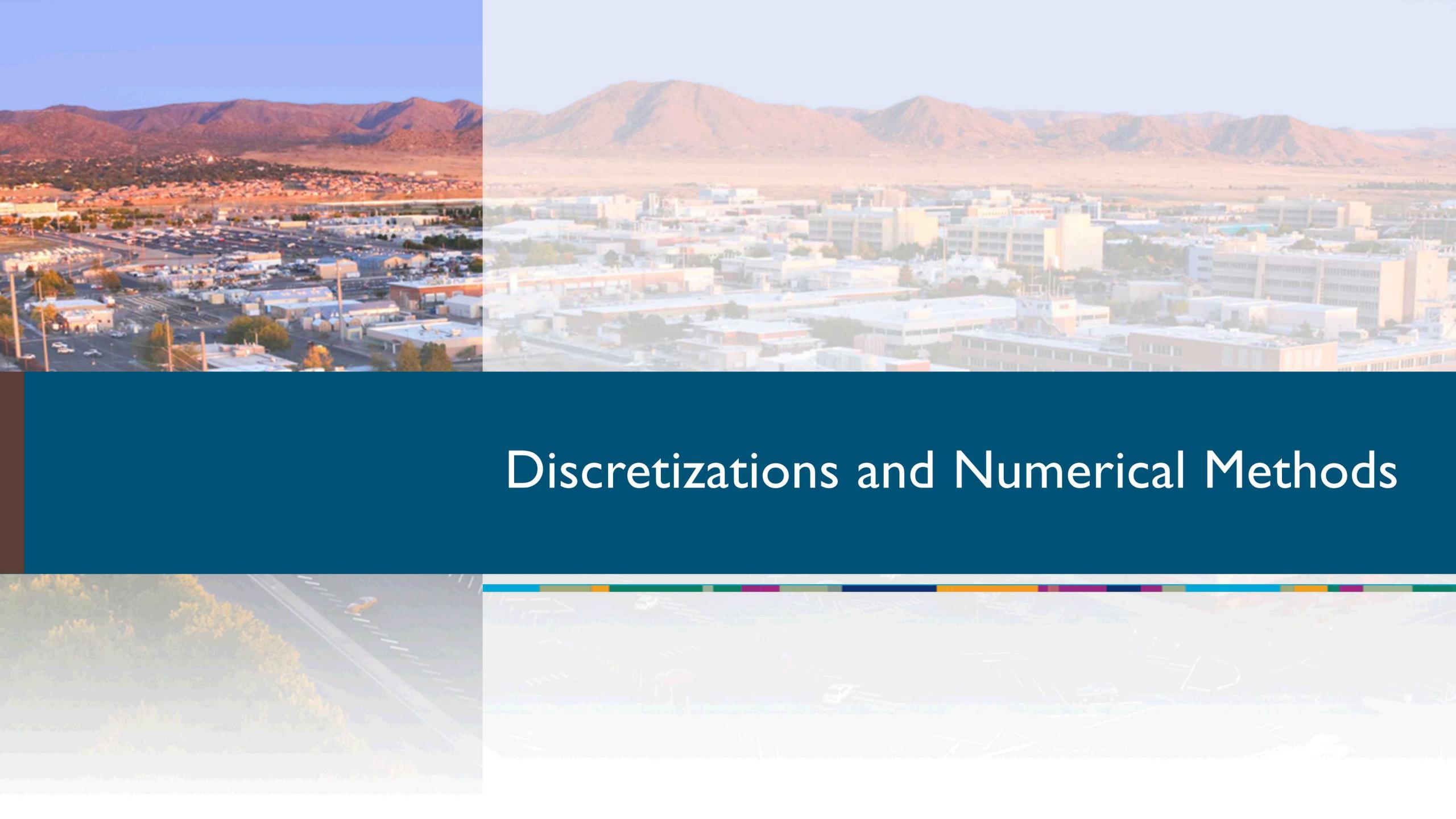


Fracture and arrested neck region from dynamic expansion of ring\*



\* D. Grady, D. Benson, Fragmentation of metal rings by electromagnetic loading, *Experimental Mechanics*, 23(4), pp. 393-400, 1983

\*\* J. Mitchell, A Nonlocal, Ordinary, State-Based Plasticity Model for Peridynamics, SAND2011-3166, 2011.



# Discretizations and Numerical Methods

# Discretizing Peridynamics

- Peridynamics is a continuum model – You choose the discretization scheme
- Temporal discretization
  - Explicit time integration (Velocity-Verlet)
  - Implicit time integration (Newmark-beta method)
- Spatial discretization (weak form)
  - Nonlocal Galerkin finite elements
  - Nonlocal discontinuous Galerkin finite elements
- Spatial discretization (strong form) 
  - Midpoint quadrature
  - Gauss quadrature\*

Primary discretization  
used in production codes.
- Solvers
  - Nonlocal domain decomposition methods
  - Nonlocal multigrid
  - Nonlinear (Newton/Krylov, nonlinear CG)
  - Linear (preconditioned Krylov subspace methods)

# Nonlocal Weak Form



## □ Prototype operator

$$\mathcal{L}\{u\}(x) = - \int_{\bar{\Omega}} C(x, x') [u(x') - u(x)] dx'$$

$$C(x, x') = C(x', x)$$

$$C(x, x') = 0 \text{ if } \|x - x'\| > \delta$$

## □ Need nonlocal weak form\* → Multiply by test function and “integrate by parts”

$$a(u, v) = - \int_{\bar{\Omega}} \int_{\bar{\Omega}} C(x, x') [u(x') - u(x)] v(x) dx' dx$$

$$= \frac{1}{2} \int_{\bar{\Omega}} \int_{\bar{\Omega}} C(x, x') [u(x') - u(x)] [v(x') - v(x)] dx' dx$$

## □ Compare with local Poisson operator

### □ Hooke's law

$$-\nabla^2 u(x) \quad \xrightarrow{\text{Diagram}} \quad \frac{1}{2} \int \nabla u \cdot \nabla v \, dx$$

# Nonlocal Quadrature



## □ Local Quadrature (Review)

- One integral required
- Compute products of *gradients* of shape functions and apply Gauss quadrature
- Gradient *drops* polynomial order (lower order quadrature scheme required)

$$a(u, v) = \frac{1}{2} \int \nabla u \cdot \nabla v \, dx$$

## □ Nonlocal Quadrature

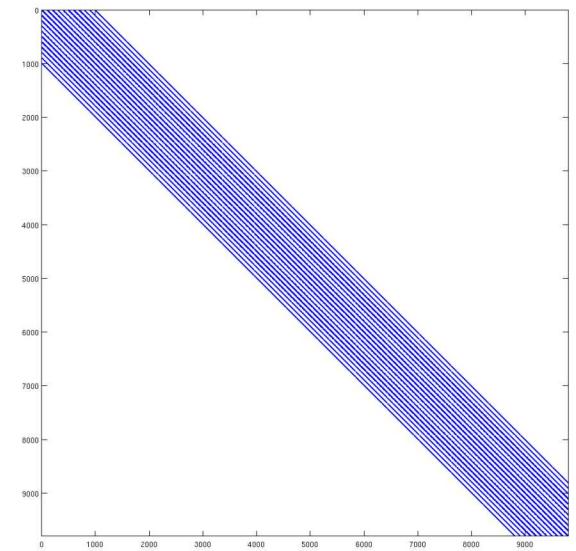
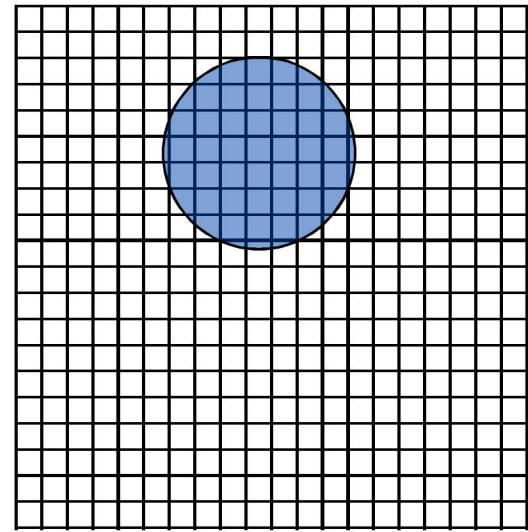
- *Two* integrals required
- Compute products of differences of shape functions and integrate
- No gradient → higher polynomial order (higher order quadrature needed)
- Nonlocality generates substantially more work over each element
- Discontinuous integrands a challenge for quadrature routines (more later...)

$$\begin{aligned} a(u, v) &= - \iint_{\bar{\Omega} \times \bar{\Omega}} C(x, x') [u(x') - u(x)] v(x) dx' dx \\ &= \frac{1}{2} \iint_{\bar{\Omega} \times \bar{\Omega}} C(x, x') [u(x') - u(x)] [v(x') - v(x)] dx' dx \end{aligned}$$

- Integration by parts is standard in local (classical) FEM.
- Unclear if there is any computational value in nonlocal setting

# Nonlocal Weak Form – 2D

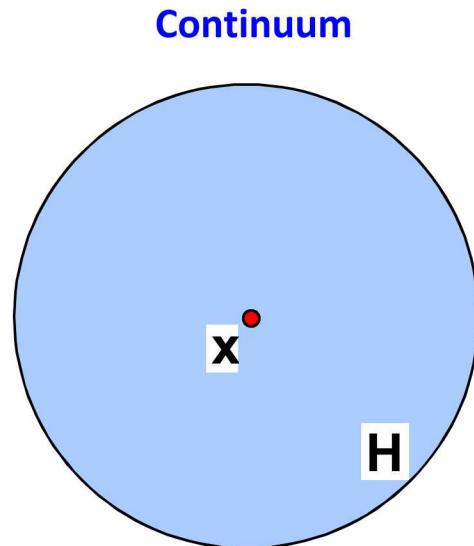
- Let  $\Omega = (0,1) \times (0,1)$ ;  $u=0$  on  $\partial\Omega$
- Weak form requires quadruple integral
  - **Expensive!**
- Matrix bandwidth controlled by  $\delta/h$ 
  - $\delta \sim |\Omega|$  gives dense matrix (intractable at large scales)
  - Classical FEM has (roughly) constant nnz per row
- Integrand discontinuous!
  - Gauss quadrature not accurate
  - Adaptive quadrature (expensive)
  - Use 1-norm, not 2-norm distance? (blue circle becomes blue square)
  - Break up integral into many separate integrals where integrand continuous over each subregion
- Exact analytic for approach for quadrature?
  - Intractable (so far)
- More practical approach: approximate blue region by simpler geometric shape and then performing quadrature



Stiffness Matrix Sparsity Pattern  
(10,000 unknowns, 3.4M nnz)

# Strong Form Discretization

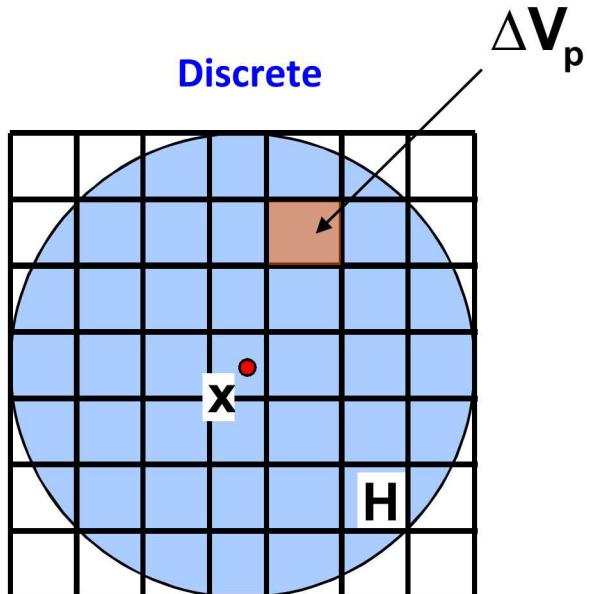
- Spatial Discretization
  - Approximate integral with sum\*
  - Midpoint quadrature
  - Piecewise constant approximation (could go higher)



$$\int_H f(u(x', t) - u(x, t), x' - x) dV'$$

# Strong Form Discretization

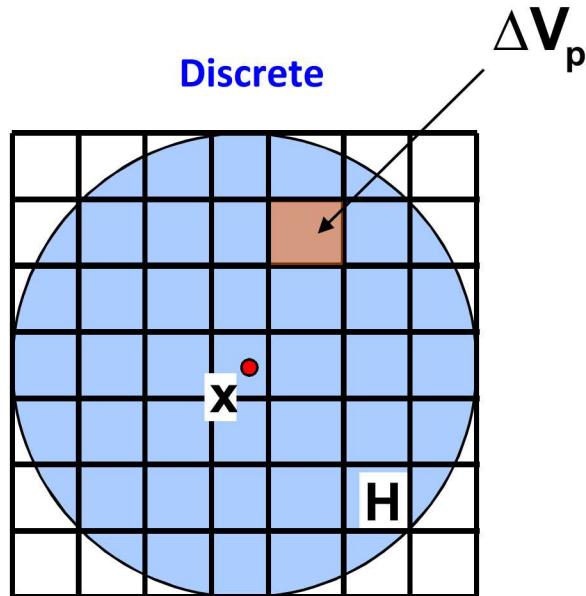
- Spatial Discretization
  - Approximate integral with sum\*
  - Midpoint quadrature
  - Piecewise constant approximation (could go higher)



$$\sum_p f(u(x_p, t) - u(x_i, t), x_p - x_i) \Delta V_p$$

# Strong Form Discretization

- Spatial Discretization
  - Approximate integral with sum\*
  - Midpoint quadrature
  - Piecewise constant approximation (could go higher)



$$\sum_p f(u(x_p, t) - u(x_i, t), x_p - x_i) \Delta V_p$$

- Temporal Discretization

- Explicit central difference in time

$$\ddot{u}(x, t) \approx \ddot{u}_i^n = \frac{u_i^{n+1} - 2u_i^n + u_i^{n-1}}{\Delta t^2}$$

- Velocity-Verlet

$$v_i^{n+1/2} = v_i^n + \left( \frac{\Delta t}{2m} \right) f_i^n$$

$$u_i^{n+1} = u_i^n + (\Delta t) v_i^{n+1/2}$$

$$v_i^{n+1} = v_i^{n+1/2} + \left( \frac{\Delta t}{2m} \right) f_i^{n+1}$$



# Asymptotically Compatible Discretizations

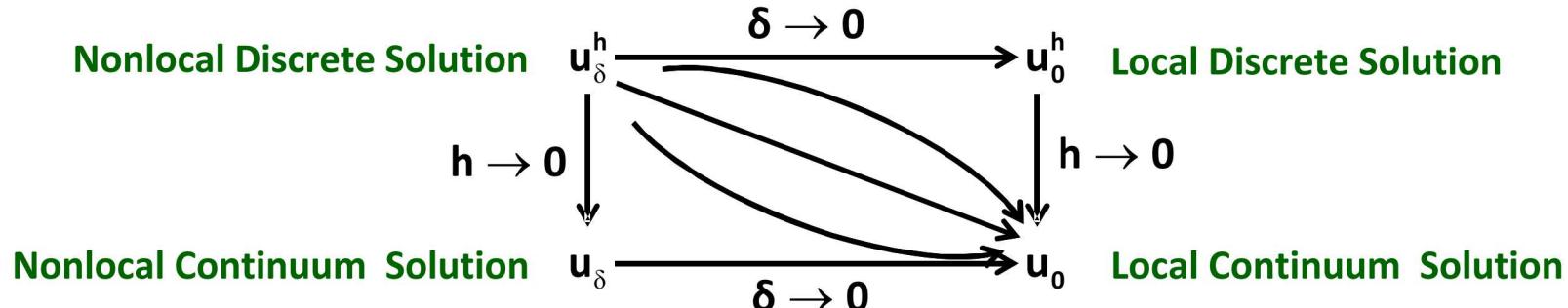


# Model Convergence ( $\delta$ Convergence)

- We are interested in nonlocal models that reduce to their local counterpart as the nonlocal parameter goes to zero.
  - i.e.,  $\lim_{\delta \rightarrow 0} \mathbf{L}_\delta \mathbf{u}_\delta = \mathbf{L}_0 \mathbf{u}_0$
- Example:
  - $\mathbf{L}_\delta \mathbf{u} = \int_{x-\delta}^{x+\delta} \mathbf{C}(x, y)(\mathbf{u}(y) - \mathbf{u}(x)) dy, \quad \mathbf{L}_0 \mathbf{u} = \frac{\partial}{\partial x} \mathbf{k}(x) \frac{\partial \mathbf{u}}{\partial x}$
- In general, this must be proven for each specific model or class of models (diffusion, elasticity, plasticity, etc.)
- A simple observation:
  - Let  $\mathbf{C}(x, y) = \frac{3}{\delta^3} \left( \frac{\mathbf{k}(x) + \mathbf{k}(y)}{2} \right)$
  - Assume we can series expand  $\mathbf{u}(y)$ ,  $\mathbf{k}(y)$  about  $x$ . Then,
 
$$\mathbf{L}_\delta \mathbf{u} = \frac{\partial}{\partial x} \mathbf{k}(x) \frac{\partial \mathbf{u}}{\partial x} + \delta^2 \left( \frac{3}{20} \frac{\partial^2 \mathbf{k}}{\partial^2 x} \frac{\partial^2 \mathbf{u}}{\partial^2 x} + \frac{1}{10} \frac{\partial \mathbf{k}}{\partial x} \frac{\partial^3 \mathbf{u}}{\partial^3 x} + \dots \right)$$
  - Leading order terms are the local model; all others vanish with  $\delta$ .
- **Nonlocal models naturally encapsulate many length scales.**

# Solution Convergence

- We also desire mesh-convergent solutions.
  - i.e.,  $\lim_{h \rightarrow 0} u_\delta^h = u_\delta$
- Thus, it should follow naturally that  $\lim_{h, \delta \rightarrow 0} u_\delta^h = u_0$ .
- It was shown by Q. Du & X. Tian\*, \*\* that this is not always the case!
  - The interplay between the length scales  $h, \delta$  is important!
- Du & Tian define a general framework for these convergence results\*\*



- Practical (non-intuitive?) result:
  - Piecewise constant discretization converges only if  $h \rightarrow 0$  faster than  $\delta \rightarrow 0$ .
  - PWC is most common PD discretization;  $\delta = \kappa h$  a common assumption!
  - PWL is asymptotically compatible (i.e., convergent for any sequence  $h, \delta \rightarrow 0$ )

\*X. Tian and Q. Du, *Analysis and Comparison of Different Approximations to Nonlocal Diffusion and Linear Peridynamic Equations*, SIAM J. Numer. Anal., v51(6), pp. 3458–3482, 2013.

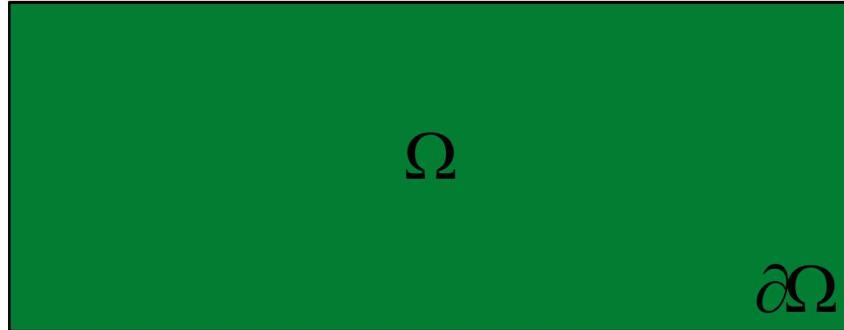
\*\* X. Tian and Q. Du, *Asymptotically Compatible Schemes and Applications to Robust Discretization of Nonlocal Models*, SIAM J. Numer. Anal., v52(4), pp. 1641–1665, 2014.

# Nonlocal Calculus

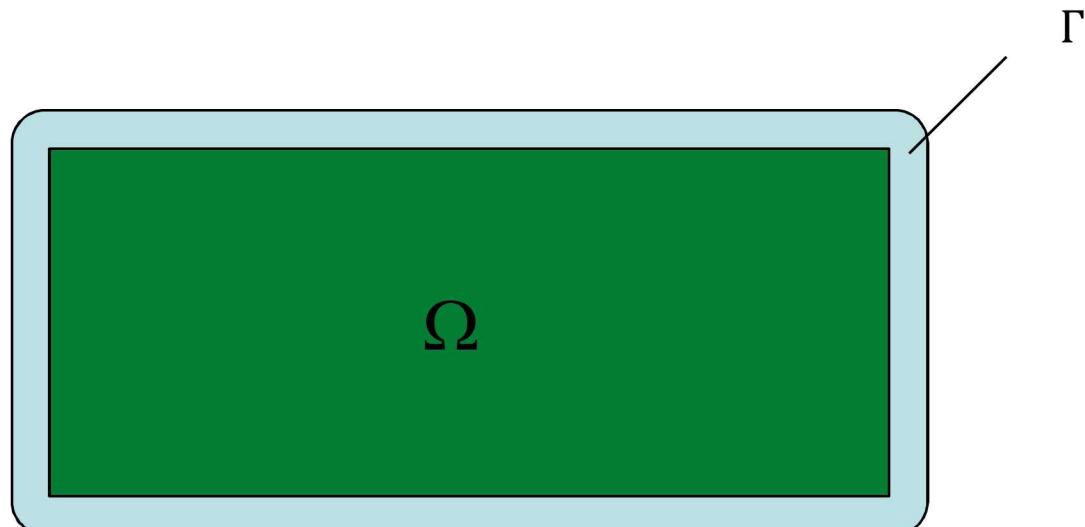
# Nonlocal Boundaries



- For local models (for example, PDE-based models), we apply boundary conditions on the boundary of the domain (hence the name)



- A Peridynamic “boundary” becomes a volumetric region, sometimes called a “nonlocal boundary”, “collar”, etc.
- Boundary conditions for these models are called “nonlocal boundary conditions”, “volume constraints”, etc.



# Nonlocal Operators\*

## □ Nonlocal Point Divergence

Given a vector two-point function  $v(x, y): \mathbb{R}^n \times \mathbb{R}^n \rightarrow \mathbb{R}^k$  and a symmetric vector-valued function  $\alpha(x, y): \mathbb{R}^n \times \mathbb{R}^n \rightarrow \mathbb{R}^k$ , the nonlocal point divergence operator is a mapping  $\hat{\lambda}_\alpha: v \mapsto \hat{\lambda}_\alpha[v]$ , where  $\hat{\lambda}_\alpha[v]: \mathbb{R}^n \rightarrow \mathbb{R}$  is given by

$$D_\alpha[v](x) = \int_{\Omega \cup \Gamma} (v(x, y) \cdot \alpha(x, y) - v(y, x) \cdot \alpha(y, x)) dy \quad \text{for } x \in \Omega.$$

## □ Nonlocal Two-Point Gradient

Given a function  $u(x): \mathbb{R}^n \rightarrow \mathbb{R}$ , the formal adjoint of  $\hat{\lambda}_\alpha$  is the nonlocal two-point gradient operator  $\square_\alpha: u \mapsto \square_\alpha[u]$ , where  $\square_\alpha[u]: \mathbb{R}^n \times \mathbb{R}^n \rightarrow \mathbb{R}^k$  is given by

$$G_\alpha[u](x, y) = (u(y) - u(x)) \alpha(x, y) \quad \text{for } (x, y) \in \mathbb{R}^n \times \mathbb{R}^n$$

## □ Nonlocal Normal

Given a vector two-point function  $v(x, y): \mathbb{R}^n \times \mathbb{R}^n \rightarrow \mathbb{R}^k$  and a symmetric vector-valued function  $\alpha(x, y): \mathbb{R}^n \times \mathbb{R}^n \rightarrow \mathbb{R}^k$ , the nonlocal normal is a mapping  $\cdot \cdot \cdot_\alpha: v \mapsto \cdot \cdot \cdot_\alpha[v]$  where  $\cdot \cdot \cdot_\alpha[v]: \mathbb{R}^n \rightarrow \mathbb{R}$  is given by

$$N_\alpha[u](x) := - \int_{\Omega \cup \Gamma} (v(x, y) \cdot \alpha(x, y) - v(y, x) \cdot \alpha(y, x)) dy \quad \text{for } x \in \Gamma$$

\* There is also a nonlocal curl; I won't talk about it today.

# Familiar Relationships



## □ Nonlocal Gauss Theorem

Given a vector two-point function  $v(x, y): \mathbb{R}^n \times \mathbb{R}^n \rightarrow \mathbb{R}^k$ , we have

$$\int_{\Omega} D_a[v](x) dx = \int_{\Gamma} N_a[v](x) dx$$

## □ Nonlocal Integration by Parts

Given a function  $u(x): \mathbb{R}^n \rightarrow \mathbb{R}$ ,  $v(x, y): \mathbb{R}^n \times \mathbb{R}^n \rightarrow \mathbb{R}^k$ , and a symmetric vector-valued function  $\alpha(x, y): \mathbb{R}^n \times \mathbb{R}^n \rightarrow \mathbb{R}^k$ , we have

$$\int_{\Omega} u(x) D_a[v](x) dx - \int_{\Omega \cup \Gamma} \int_{\Omega \cup \Gamma} G_a[u](x, y) \alpha(y) dy dx = \int_{\Gamma} u(x) N_a[v](x) dx$$

## □ Nonlocal Green's First Identity

Given the function  $u(x), v(x): \mathbb{R}^n \rightarrow \mathbb{R}$ , and a symmetric vector-valued function  $\alpha(x, y): \mathbb{R}^n \times \mathbb{R}^n \rightarrow \mathbb{R}^k$ , we have

$$\int_{\Omega} u(x) D_a[G_a[v]](x) dx - \int_{\Omega \cup \Gamma} \int_{\Omega \cup \Gamma} G_a[u](x, y) \alpha(y) G_a[v](y) dy dx = \int_{\Gamma} u(x) N_a[G_a[v]](x) dx$$

# Nonlocal Laplacian



We can compose nonlocal operators in familiar ways.

## □ Nonlocal Laplacian

Given a function  $u(x): \mathbb{R}^n \rightarrow \mathbb{R}$  and  $\mu(x, y) = \alpha(x, y) \cdot \alpha(x, y)$  where  $\alpha(x, y): \mathbb{R}^n \times \mathbb{R}^n \rightarrow \mathbb{R}^k$  is a symmetric vector-valued function, the nonlocal Laplace operator is defined as

$$L_\mu[u](x) := D_\alpha [G_\alpha[u]](x) = 2 \int_{\Omega \cup \Gamma} (u(y) - u(x)) \mu(x, y) dy \quad \text{for } x \in \Omega$$

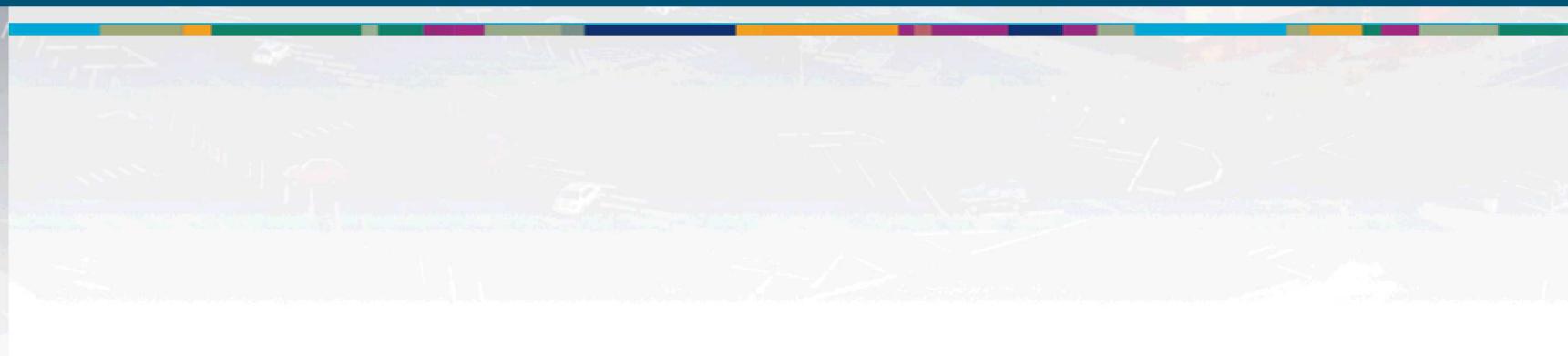
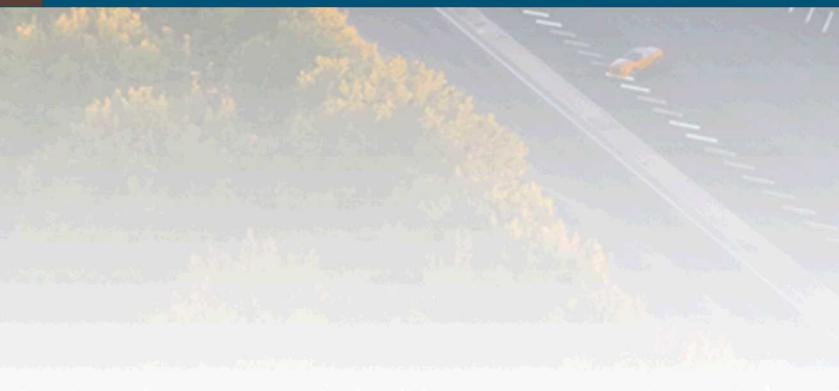
## □ Nonlocal Poisson Equation (Dirichlet Boundary Conditions)

$$L_\mu[u](x) = b(x) \quad \text{for } x \in \Omega$$

$$u(x) = g(x) \quad \text{for } x \in \Gamma$$



# Conditioning Results



# Background: Condition Number



We denote the condition number of  $A$  as  $\kappa(A) := \|A\| \|A^{-1}\|$ .

We can demonstrate its usefulness via perturbation analysis. Let  $Ax=b$  and consider the perturbed system:

- $(A + \varepsilon E)x(\varepsilon) = b + \varepsilon e$

Let  $\delta(\varepsilon) = x(\varepsilon) - x$ . Then,

- $(A + \varepsilon E)\delta(\varepsilon) = b + \varepsilon e - (b - \varepsilon E)$
- $(A + \varepsilon E)\delta(\varepsilon) = \varepsilon(e - Ex)$
- $\delta(\varepsilon) = \varepsilon(A + \varepsilon E)^{-1}(e - Ex)$

We observe that the function  $x(\varepsilon)$  is differentiable at  $\varepsilon=0$ :

- $x'(0) = \lim_{\varepsilon \rightarrow 0} \frac{x(0+\varepsilon) - x(0)}{\varepsilon} = A^{-1}(e - Ex)$

Perturbing the pair  $(A, b)$  by the small amount  $(\varepsilon E, \varepsilon e)$  will cause the solution to change by  $\varepsilon x'(0)$ . Thus,

- $\|x(\varepsilon) - x\| = \varepsilon \|A^{-1}(e - Ex)\|$
- $\|x(\varepsilon) - x\| \leq \varepsilon \|A^{-1}\| (\|e\| + \|E\| \|x\|) + O(\varepsilon^2)$

Further simplification and use of the relationship  $\|b\| \leq \|A\| \|x\|$  gives the relative variation in the solution to the relative sizes of the perturbation

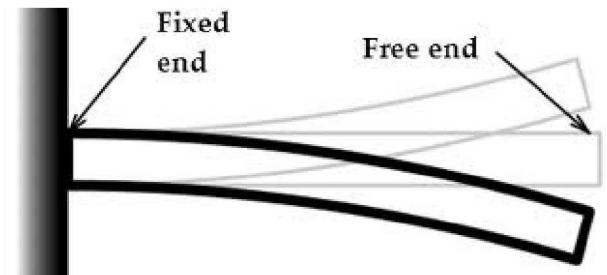
- $\frac{\|x(\varepsilon) - x\|}{\|x\|} \leq \varepsilon \|A^{-1}\| \|A\| \left( \frac{\|e\|}{\|b\|} + \frac{\|E\|}{\|A\|} \right) + O(\varepsilon^2)$

# Background: Condition Number



What does this mean physically?

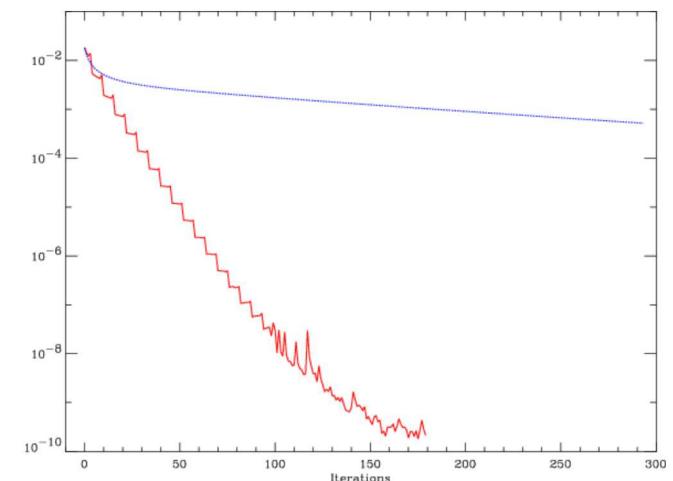
- For Ill-conditioned systems, small perturbation in input can result in a large change in solution



Cantilevered beam

What does this mean for linear solvers?

- Condition number dictates accuracy
  - Using relationships  $Ax=b$ ,  $e=A^{-1}r$ , can show that  $\frac{\|e\|}{\|x\|} \leq \|A\| \|A^{-1}\| \frac{\|r\|}{\|b\|}$
  - Small relative residual does not imply small relative error!
- Condition number dictates convergence rate
  - Convergence rate of conjugate gradients:  $\|e^{(k)}\|_A \leq 2 \left( \frac{\sqrt{\kappa(A)} - 1}{\sqrt{\kappa(A)} + 1} \right)^k \|e^{(0)}\|_A$

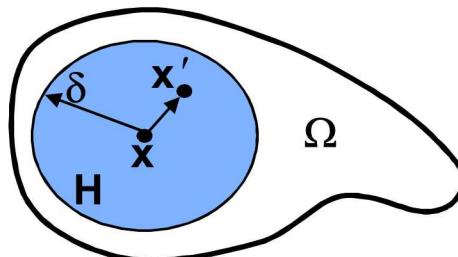


Convergence curves for optimal Krylov methods

# Conditioning of Peridynamic Operators



- Why is conditioning important?
  - Condition number dictate convergence rates of linear solvers
  - Condition numbers dictate the accuracy of computed solution
  - Rule of thumb:  
**If  $\kappa(A) = 10^{16-d}$ , then computed solution has d digits of accuracy (double precision)**  
If  $\kappa(A) = 10^{16}$ , expect zero digits of accuracy!
- Old saying: ***"You get the answer you deserve..."***



Point x interacts directly with all points  $x'$  within  $H$

- New component in nonlocal modeling is peridynamic horizon  $\delta$ 
  - How does  $\delta$  affect the conditioning?
  - Develop preconditioners/solvers optimized for nonlocal models at extreme scales
- To explore the effects of conditioning, let's consider a FEM discretization of peridynamics

# Spectral Equivalence

- For simplicity, assume

$$C(x, x') = \chi_\delta(x - x') \equiv \begin{cases} 1 & \text{if } \|x - x'\| \leq \delta \\ 0 & \text{otherwise} \end{cases}$$

“Canonical”  
Kernel Function

- Main Theorem\*

$$\lambda_1(\bar{\bar{\Omega}})\delta^{d+2} \leq \frac{a(u, u)}{\|u\|_{L_2(\bar{\bar{\Omega}})}} \leq \lambda_2(\bar{\bar{\Omega}})\delta^d \quad u \in L_{2,0}(\bar{\bar{\Omega}})$$

- Let  $K$  be a finite element discretization of  $a(u, u)$ . Then, in  $h \ll \delta$  limit,

$$\kappa(K) \sim \mathcal{O}(\delta^{-2})$$

- Dominant length scale in nonlocal model set by  $\delta$ .
  - Contrast with local model, where length scaled introduced by  $h$
  - **Mesh-independent condition number bound!**

# Conditioning Results – 1D

□ Let  $\Omega = (0,1)$ ,  $\mathcal{E}\Omega = [-\delta,0] \cup [1,\delta]$ .

□  $u=0$  on  $\mathcal{E}\Omega$

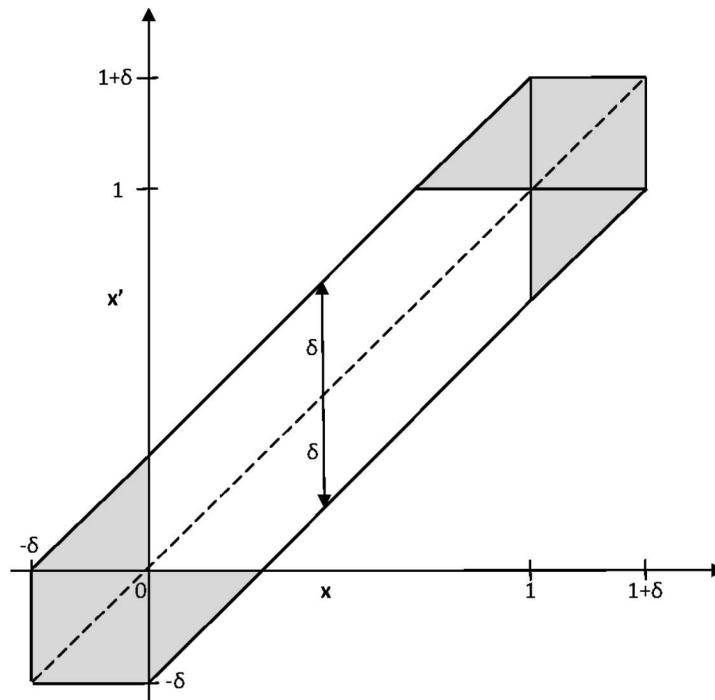
□ Let  $C(x,x') = \begin{cases} 1 & \text{if } \|x - x'\| \leq \delta \\ 0 & \text{otherwise} \end{cases}$

□ Weak form becomes

$$a(u,v) = - \int_0^{x-\delta} \int_{x-\delta}^{x+\delta} [u(x') - u(x)] v(x) dx' dx$$

□ Numerical Study

- PW constant and PW linear SFs
- Hold  $\delta$  fixed, vary  $h$
- Hold  $h$  fixed, vary  $\delta$



Integration Domain in  $(x,x')$   
(grey = outside  $\Omega$ )

# Conditioning Results – 1D

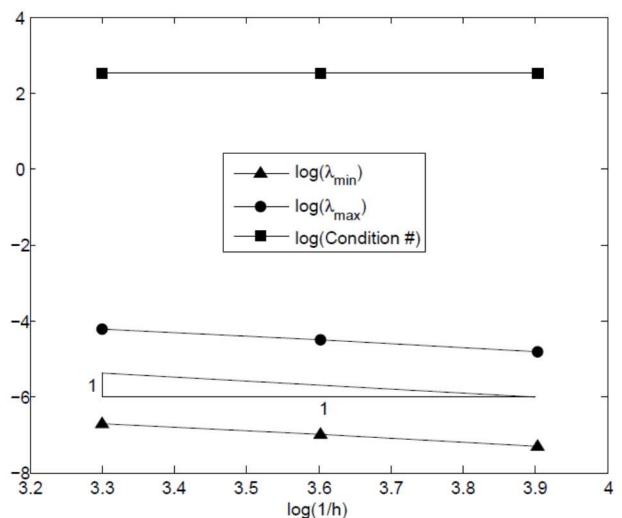
□ Observations:  $\kappa(K) \sim O(\delta^{-2})$ , only weak  $h$ -dependence

(a) Constant  $\delta$ , vary  $h$ .

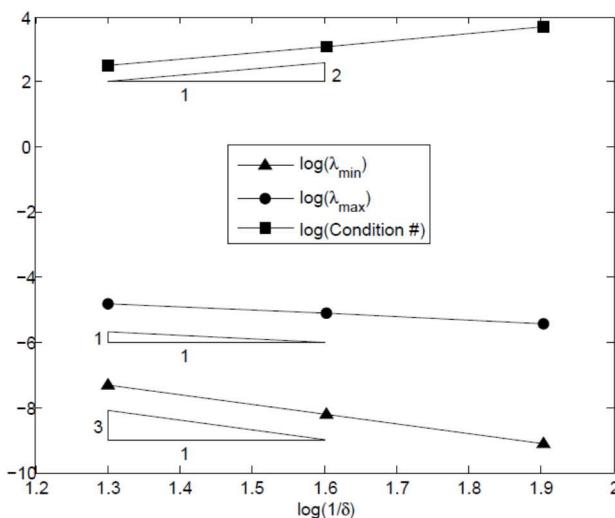
$1/h$	$1/\delta$	Piecewise Constant Shape Functions			Piecewise Linear Shape Functions		
		$\lambda_{\min}$	$\lambda_{\max}$	Condition #	$\lambda_{\min}$	$\lambda_{\max}$	Condition #
2000	20	1.94E-07	6.07E-05	3.13E+02	1.94E-07	6.07E-05	3.13E+02
4000	20	9.69E-08	3.04E-05	3.13E+02	9.69E-08	3.04E-05	3.14E+02
8000	20	4.84E-08	1.52E-05	3.14E+02	4.84E-08	1.52E-05	3.14E+02

(b) Constant  $h$ , vary  $\delta$ .

$1/h$	$1/\delta$	Piecewise Constant Shape Functions			Piecewise Linear Shape Functions		
		$\lambda_{\min}$	$\lambda_{\max}$	Condition #	$\lambda_{\min}$	$\lambda_{\max}$	Condition #
8000	20	4.84E-08	1.52E-05	3.15E+02	4.84E-08	1.52E-05	3.14E+02
8000	40	6.24E-09	7.61E-06	1.22E+03	6.24E-09	7.60E-06	1.22E+03
8000	80	7.92E-10	3.80E-06	4.80E+03	7.91E-10	3.80E-06	4.80E+03



(a) Constant  $\delta$ , vary  $h$ .



(b) Constant  $h$ , vary  $\delta$ .

# Conditioning Results – 2D

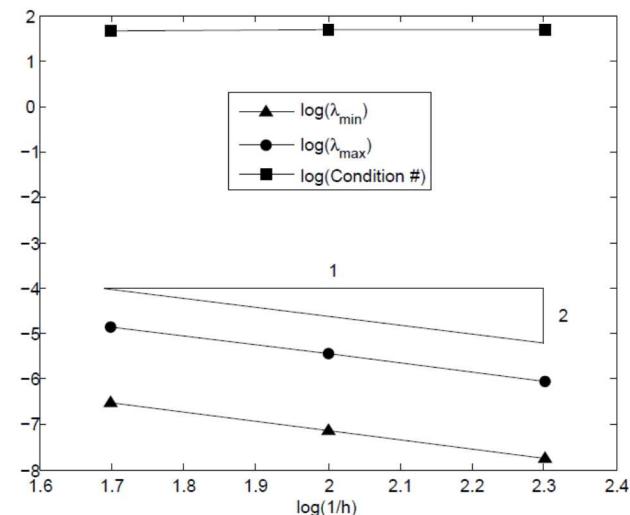
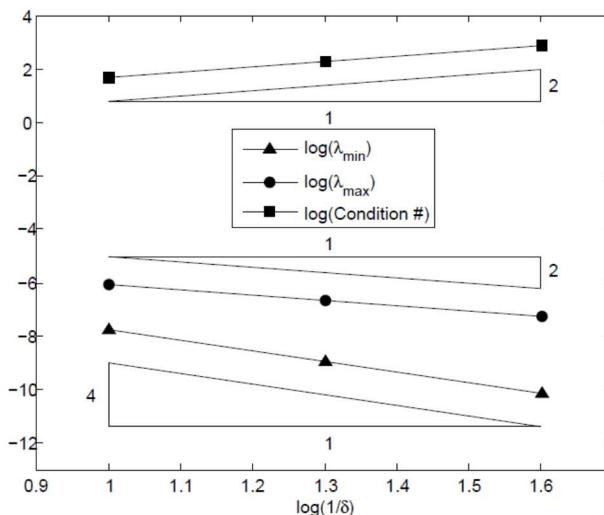
- Do exact quadrature (no quadrature error)
- Observations:  $\kappa(K) \sim O(\delta^{-2})$ , weak  $h$ -dependence

(a) Constant  $\delta$ , vary  $h$ .

$1/h$	$1/\delta$	$\lambda_{\min}$	$\lambda_{\max}$	Condition #
50	10	2.95E-07	1.40E-05	4.77E+01
100	10	7.11E-08	3.54E-06	4.97E+01
200	10	1.75E-08	8.86E-07	5.05E+01

(b) Constant  $h$ , vary  $\delta$ .

$1/h$	$1/\delta$	$\lambda_{\min}$	$\lambda_{\max}$	Condition #
200	10	1.75E-08	8.86E-07	5.05E+01
200	20	1.17E-09	2.22E-07	1.90E+02
200	40	7.63E-11	5.50E-08	7.21E+02

(a) Constant  $\delta$ , vary  $h$ .(b) Constant  $h$ , vary  $\delta$ .

# More General Results



- Consider a more general kernel ...

$$a(u, u) = \frac{1-s}{\delta^{2-2s}} \int_{\overline{\Omega} \setminus H_x} \int \frac{(u(y) - u(x))^2}{|y-x|^{d+2s}} dy dx, \quad u \in H^s(\overline{\Omega}), \quad s \in (0,1)$$

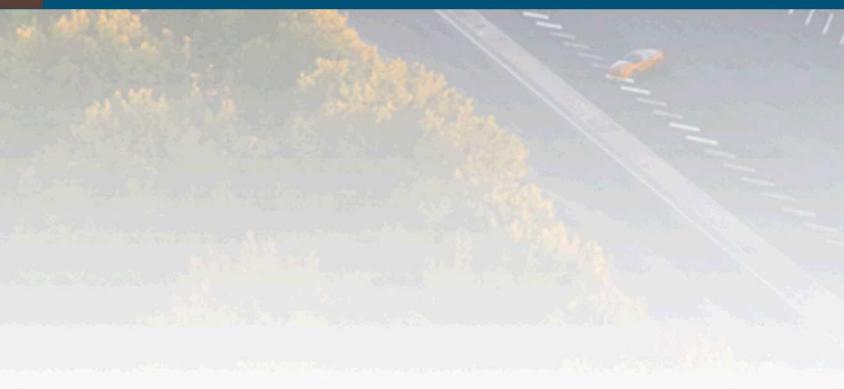
- Can capture  $h$ -,  $\delta$  -, and  $s$ -quantification of conditioning (Aksoylu & Unlu, 2015, Zhou & Du, 2010)

$$\kappa(A) \leq c \min \left\{ h^{-2s} \delta^{-(2-2s)}, h^{-2} \right\}$$

- Note interplay of  $\delta, h$



# Summary



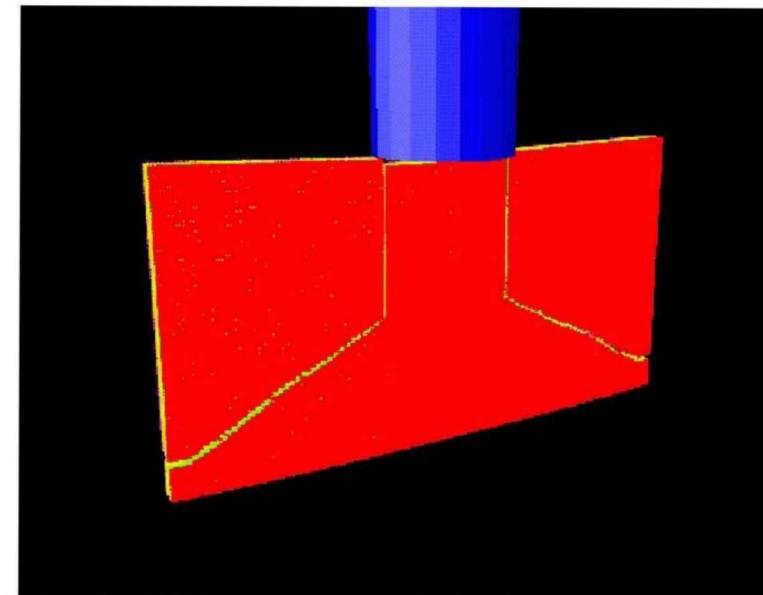
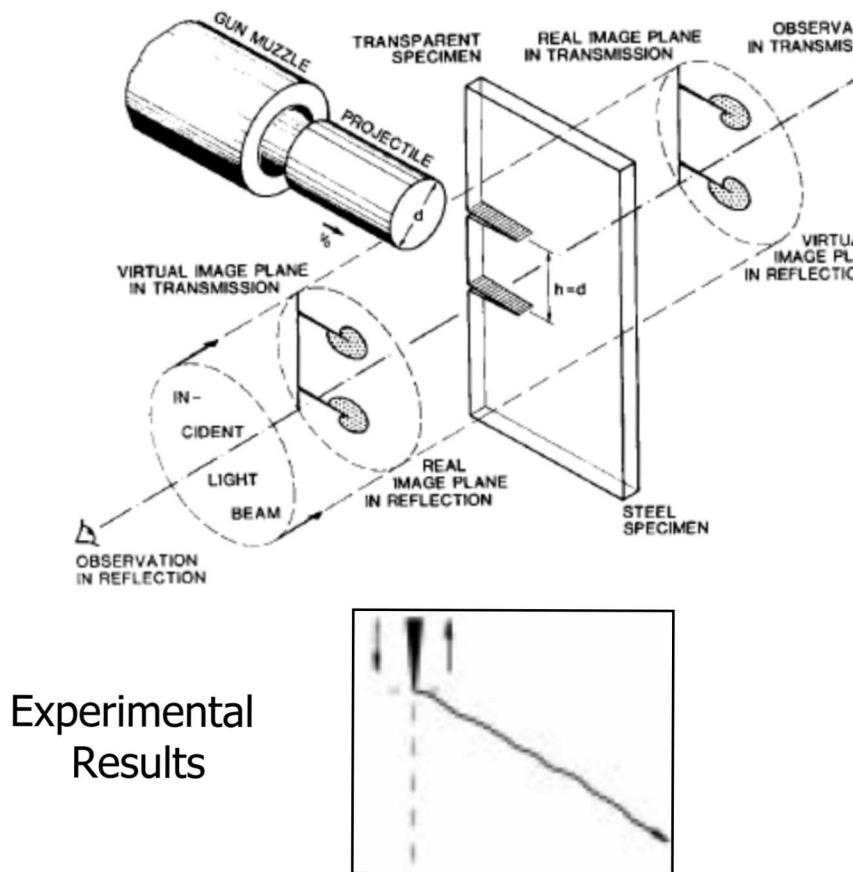
# Summary: Survey of Computational Peridynamics

- Local Models, Nonlocal Models, and Length Scales
- Peridynamics overview
- Example computations
- Material models and fracture models
  - Linear isotropic elastic
  - Elastic-plastic
  - Viscoelastic
  - Brittle and ductile failure
- Discretizations and numerical methods
  - Weak form discretization
  - Strong form discretization
- Asymptotically Compatible Discretizations
- Nonlocal Calculus
- Condition Number Analysis

# Kalthoff-Winkler Experiment

- Dynamic fracture in steel (Kalthoff & Winkler, 1988)
- Mode-II loading at notch tips results in mode-I cracks at  $70^\circ$  angle
- Peridynamic model reproduces the crack angle observed experimentally\*

Simulation performed  
with EMU

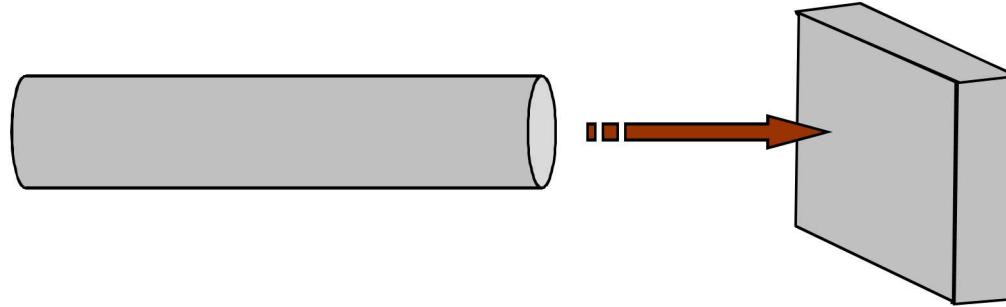


# Taylor Bar Test



## □ Taylor impact test of 6061-T6 aluminum\*

Simulation performed  
with EMU



Experiment



Peridynamic Model\*

# Failure in Fiber-Reinforced Composites

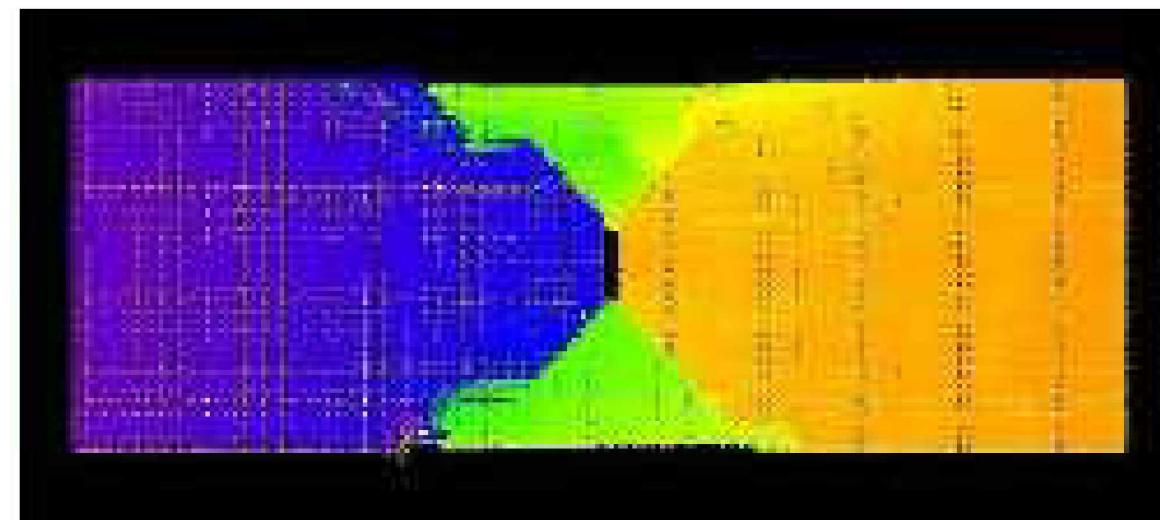


- Splitting and fracture mode changes in fiber-reinforced composites\*
- Fiber orientation between plies strongly influences crack growth

Simulation performed  
with EMU



Typical crack growth in notched laminate  
(photo courtesy Boeing)



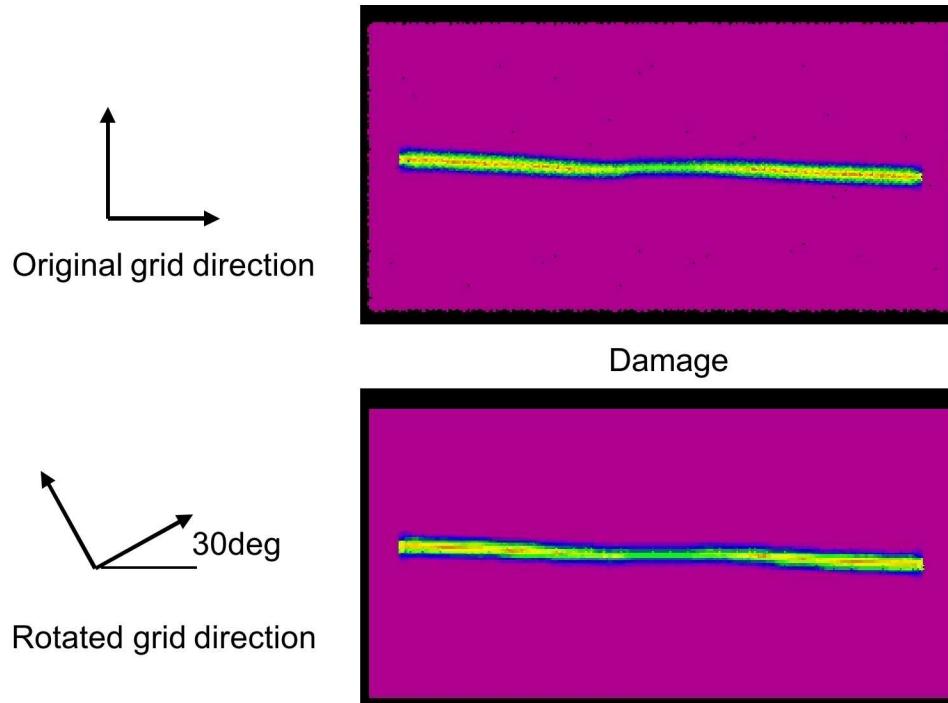
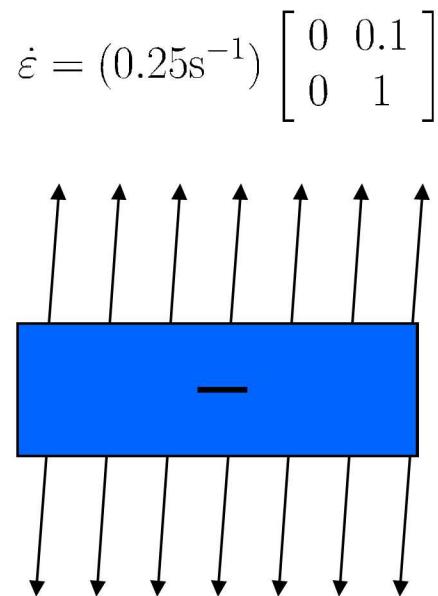
Peridynamic Model

# Mesh-Independent Crack Growth



- Discrete peridynamic model exhibits mesh-independent crack growth
- Plate with a pre-existing defect is subjected to prescribed boundary velocities
- Crack growth direction depends continuously on loading direction

Simulation performed with EMU



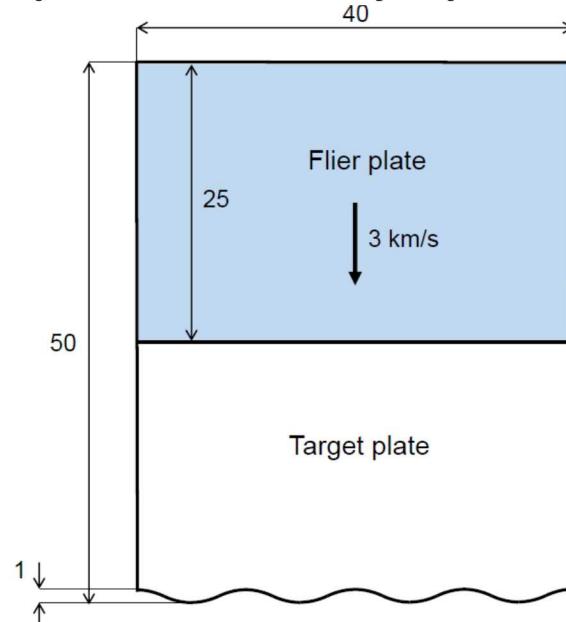
- Nonlocal network of bonds in many directions allows cracks to grow in any direction.

# Shockwave Ejecta

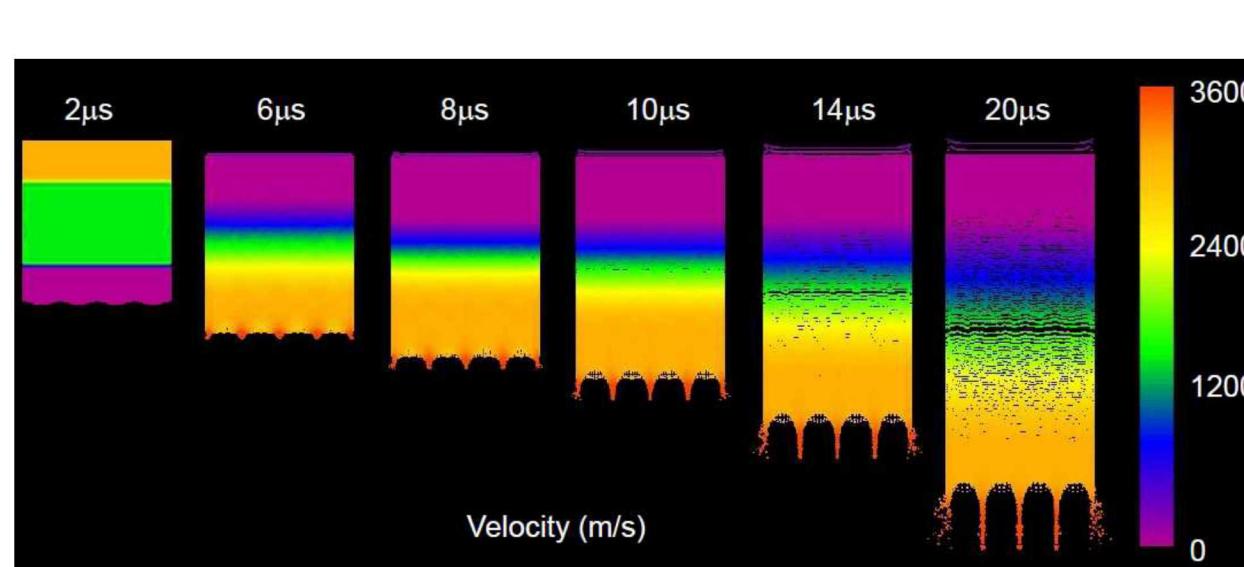


- Motivated by experiments by Ogorodnikov et al.\*
- Utilize Peridynamic Eulerian model with Mie-Grüneisen EOS
- Impact aluminum flyer plate on aluminum target plate at 3 km/s, pressure 30 Gpa

Simulation performed with EMU



Initial geometry.  
Dimensions in mm.



Peridynamic simulation results.  
Six different simulation times are shown.

- Computed shock velocity is 7.140 km/s; Expected value is 7.230 km/s.
- Computed jet tip velocity is 4.0 km/s; Experimentally measured value is 3.7 km/s.



# Maximum Interaction Distance



- Recall the linear peridynamic solid (LPS) model

$$\rho \ddot{\mathbf{u}}(\mathbf{x}, t) = \int_{\mathcal{H}} \left( \mathbf{T}[\mathbf{x}, t] \langle \mathbf{x}' - \mathbf{x} \rangle - \mathbf{T}[\mathbf{x}', t] \langle \mathbf{x} - \mathbf{x}' \rangle \right) dV_{\mathbf{x}'} + \mathbf{b}(\mathbf{x}, t)$$

$$\mathbf{T}[\mathbf{x}, t] \langle \mathbf{x}' - \mathbf{x} \rangle = \left( \frac{3k\theta}{m} \underline{\omega}_{\mathbf{x}} + \frac{15\mu}{m} \underline{\omega}_{\mathbf{e}^d} \right) \frac{\mathbf{x}' - \mathbf{x}}{\|\mathbf{x}' - \mathbf{x}\|}$$

$$\square \text{ The dilatation is defined as } \theta = \frac{3}{m} \int_{\mathcal{H}} \underline{\omega}_{\mathbf{x}} \mathbf{e} dV$$

- Movement at  $\mathbf{x}''$  influences dilatation at  $\mathbf{x}'$ .
- Dilatation at  $\mathbf{x}'$  influences force state at  $\mathbf{x}$ .
- In the state-based theory, the effective interaction distance is  $2\delta$ !
  - Affects communication patterns
  - Affects stiffness matrix bandwidth ( $\sim 2\delta/h$ , not  $\delta/h$ )

