

# Substitution of Co with Ni in Co/Al<sub>2</sub>O<sub>3</sub> catalysts for Fischer-Tropsch synthesis

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**Abstract:** The effect of cobalt substitution with nickel was investigated for the Fischer-Tropsch synthesis reaction. Catalysts having different Ni/Co ratios were prepared by aqueous incipient wetness co-impregnation, characterized and tested using a continuously stirrer tank reactor (CSTR) for more than 200 h. The addition of nickel did not significantly modify the morphological properties measured. XRD, STEM and TPR-XANES results showed intimate contact between nickel and cobalt, strongly suggesting the formation of a Co-Ni solid oxide solution in each case. Moreover, TPR-XANES indicated that nickel addition improves the cobalt reducibility. This may be due to H<sub>2</sub> dissociation and spillover, but more likely due to a chemical effect of intimate contact between Co and Ni resulting in Co-Ni alloying after activation. FTS testing revealed a lower initial activity when nickel was added. However, CO conversion was observed to continuously increase with time on-stream until a steady-state value (34-37% depending on Ni/Co ratio) was achieved, which was very close to the value observed for undoped Co/Al<sub>2</sub>O<sub>3</sub>. This trend suggests nickel can stabilize cobalt nanoparticles even if at a lower weight % of Co. Currently, the cobalt price is 2.13 times the price of nickel. Thus, comparing the activity/\$, the catalyst with a Ni/Co ratio of 25/75 has better performance than the unpromoted catalyst. Finally, nickel promoted catalysts exhibited slightly higher initial selectivity to light hydrocarbons initially, but this difference typically diminished with time on-stream; once leveling off in conversion was achieved, the C<sub>5+</sub> selectivities were similar (~80%) for Ni/Co ratios up to 10/90, and only slightly lower (~77%) at Ni/Co of 25/75.

**Keywords:** Fischer-Tropsch synthesis, bimetallic catalyst, cobalt-nickel alloys, TPR-XANES/EXAFS

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## 1. Introduction

Fischer-Tropsch synthesis (FTS) is a catalytic reaction which converts syngas, a mixture of CO and H<sub>2</sub> derived from natural gas, coal, and/or biomass, to high quality fuels. The active metals for FTS are iron, cobalt, nickel and ruthenium. Among these metals, ruthenium is the most active. However, its application for large-scale FTS plants is impractical because of low abundance and very high cost [1]. In contrast, nickel is cheaper, but high selectivities to short-chained hydrocarbons, especially methane, are obtained because of its high hydrogenation capability [2]. Thus, cobalt and iron are the only relevant catalysts which are currently used commercially. Cobalt is especially advantageous for converting methane derived syngas because of its high activity and selectivity to linear long-chained hydrocarbons, low deactivation rate and finally low activity for water-gas shift

(WGS) [3, 4]. However, cobalt is more expensive than iron. Indeed, the cobalt price range in the last five years has been in the range of 22-100 \$/kg [5].

The activity of cobalt catalysts depends on the number of exposed  $\text{Co}^0$ , the active sites, on the catalyst surface [6]. Systems with relatively high dispersions are needed in order to maximize the surface availability of  $\text{Co}^0$ . For this reason, cobalt is typically supported on high surface area carriers with strong interactions (e.g.,  $\text{Al}_2\text{O}_3$ ,  $\text{TiO}_2$ ). However, thermodynamic studies suggest cobalt nanoparticles lower than 4 nm might be re-oxidized by water under FTS reaction conditions [7, 8]. Thus, the optimal particle sizes are in the range of 6-10 nm [9]. Even if the particle size, as well as the interaction with the support, are optimized, the majority of the cobalt is locked within the particle instead of being exposed to the surface. Therefore, the incorporation of a second metal, less expensive and with similar electronic properties of cobalt, could be a possible route to decrease the total preparation cost of the catalyst. DFT screening was used by Van Helden et al. [10] to identify the alloys which have similar adsorption and electronic properties to cobalt catalyst.  $\text{NiCo}_3$ ,  $\text{AlNi}_3$  and  $\text{SiFe}_3$  are suitable cheaper candidates. However,  $\text{SiFe}_3$  and  $\text{AlNi}_3$  are quite difficult to produce at the nanoscale level. In contrast, Co-Ni alloys can be easily prepared at different Ni/Co ratios. Ni-Mn bimetallic systems were also investigated during  $\text{CO}_x$  hydrogenation. The authors reported the formation of  $\text{NiMnO}_3$  when Ni/Mm ratio is higher than 1 and higher activity for CO hydrogenation [11].

Cobalt and nickel have different electronic configurations. Cobalt is a  $d^7$  metal which dissociates CO and stabilizes the vinylic intermediate. This intermediate species is stable in an  $sp^3$  configuration which favors the chain growth to linear hydrocarbons during FTS [2]. In contrast, nickel ( $d^8$  metal) has a greater electronic back-donation capability. Thus, vinylic intermediates cannot be sufficiently stabilized, thus favoring the production of light saturated hydrocarbons, especially methane. Therefore, it is of fundamental importance to investigate alloys with different Ni/Co ratios in order to determine the optimal nickel loading for (1) the stability of the vinylic intermediate, (2) catalyst stability with time on-stream, and (3) high selectivity to longer chained hydrocarbons.

Co-Ni alloys for FTS were investigated by different authors [10, 12-22]. Ishihara et al. studied Co-Ni alloys supported on  $\text{MnO-ZrO}_2$  [13] and  $\text{SiO}_2$  [12, 14]. The authors found that the electronic interactions between nickel and cobalt create new adsorption sites, which strengthens the adsorption of hydrogen and enhances the catalytic activity. Further research has suggested that nickel facilitates reduction of cobalt, shifting it to lower temperature, as well as increasing the cobalt dispersion [16, 18]. Moreover, Rytter et al. [18] observed that cobalt catalyst with nickel loadings up to 5 wt% have an improved stability because of the suppression of coking through nickel decoration of the cobalt surface. Recently, López-Tinoco et al. [20] characterized well-controlled nanoparticles consisting of Co-Ni alloys and compared them with a conventional heterogenous catalyst. TPR-XANES/EXAFS showed that cobalt and nickel have an oxidation state which can be tuned from +2 to 80% metallic. However, well-controlled nanoparticles can currently be prepared in only small amounts, and as such, cannot be easily used for commercial FTS applications. The authors prepared a conventional nickel-cobalt catalyst and found similar activity to  $\text{Co/Al}_2\text{O}_3$  at steady-state conditions. However, additional investigations are needed in order to speculate the role of nickel in these bimetallic systems.

In the present work, catalysts with different Ni/Co ratios were prepared and characterized by BET, XRD, ICP, TPR-XANES, and STEM. The activity and the catalytic stability have been evaluated by testing the catalyst in a CSTR reactor for more than 200 h.

## 2. Results

### 2.1 Catalyst characterization

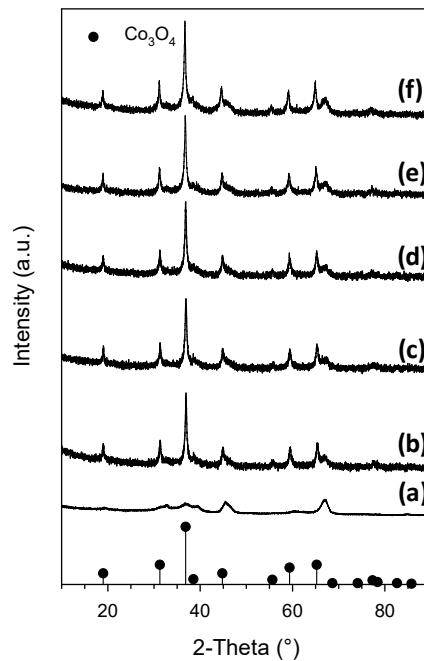
BET surface areas for the prepared catalysts are shown in Table 1. The surface area, pore volume and pore diameter are similar among all the samples suggesting the substitution of cobalt with nickel does not affect the morphological properties. Table 1 also shows the ICP results. The cobalt loading

is slightly higher (~30%) than the theoretical value (25%), whereas all Ni/Co ratios are consistent with the nominal values.

XRD patterns for  $\text{Al}_2\text{O}_3$  and the oxide catalysts are plotted in Figure 1. All the catalysts show the characteristic reflection peaks associated with  $\text{Co}_3\text{O}_4$  (i.e.  $2\Theta = 36.8^\circ$ ). No diffraction peaks correlated to nickel compounds are detected for the nickel promoted catalyst. This suggests nickel is well dispersed, as well as the formation of a Co-Ni solid oxide solution.

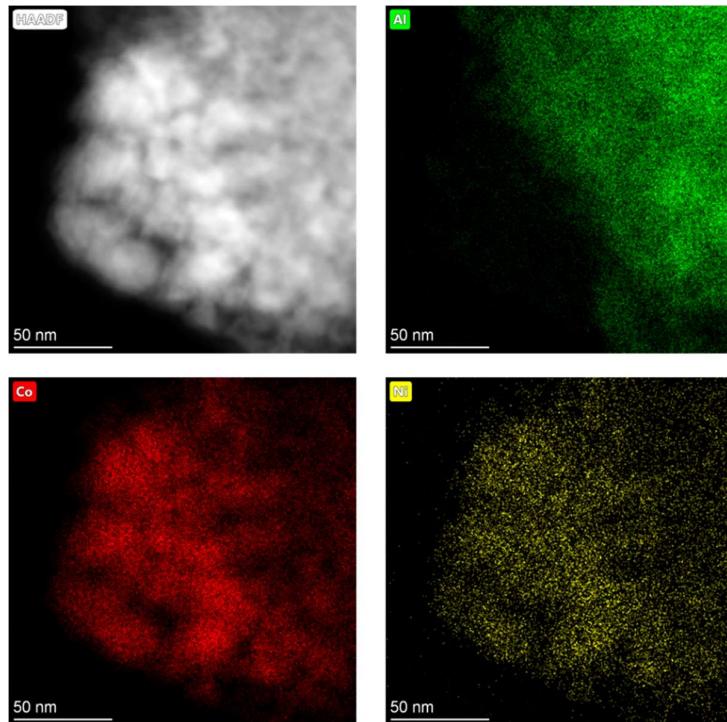
**Table 1:** BET, BJH and ICP results for the prepared catalysts.

Sample ID	$A_s$ (BET) [ $\text{m}^2/\text{g}$ ]	$V_p$ (BJH Des) [ $\text{cm}^3/\text{g}$ ]	$D_p$ (BJH Des) [ $\text{\AA}$ ]	%Co	%Ni
25%Co	95.5	0.243	93	30.21	-
25%M – 5%Ni-95%Co	92.9	0.226	91	30.49	1.43
25%M – 10%Ni-90%Co	96.5	0.227	94	31.58	2.97
25%M – 25%Ni-75%Co	96.0	0.236	89	24.86	7.7
25%M – 50%Ni-50%Co	91.6	0.237	87	17.4	16.2

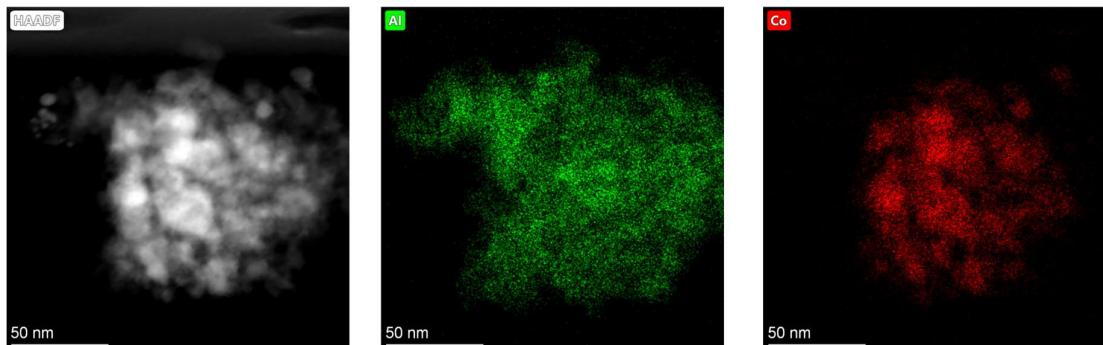


**Figure 1:** XRD for (a) 25%Co/ $\text{Al}_2\text{O}_3$ , (b) 25%M (M = 5%Ni-95%Co)/ $\text{Al}_2\text{O}_3$ , (c) 25%M (M = 10%Ni-90%Co)/ $\text{Al}_2\text{O}_3$ , (d) 25%M (M = 25%Ni-75%Co)/ $\text{Al}_2\text{O}_3$ , and (e) 25%M (M = 50%Ni-50%Co)/ $\text{Al}_2\text{O}_3$ .

Figure 2 shows TEM and STEM of reduced 25%M (10%Ni-90%Co)/ $\text{Al}_2\text{O}_3$ . The particle sizes are distributed between 18 and 23 nm, whereas the presence of nickel and cobalt was confirmed by EDS analysis. These two metals are uniformly distributed confirming the formation of a Ni-Co solid oxide solution as pointed it out from XRD. The Co/Ni weight ratio is close to 10, similar to the theoretical value. The particle sizes for the 25%Co/ $\text{Al}_2\text{O}_3$  are between 15 and 20 nm (Figure 3). EDS analysis shows areas richer in cobalt (until 55 wt. %), and others poorer in cobalt (10 wt. %); however, the average cobalt loading is close to 28 wt.% over an extended area.



**Figure 2:** HAADF-STEM image of sample 25%M (10%Ni-90%Co). Elemental mapping legend: (Yellow) Nickel, (Red) Cobalt, and (Green) Aluminum.



**Figure 3:** HAADF-STEM image of sample 25%Co. Elemental mapping legend: (Green) Aluminum, and (Red) Cobalt.

Hydrogen chemisorption with pulse reoxidation results are presented in Table 2. The degree of reduction results are similar with those of the TPR-XANES/EXAFS data as it will be shown in the next sections. With increasing Ni/Co ratio, the mixed metal oxides exhibit more facile reduction. There also appears to be a slight increase in average metal diameter with increases in Ni/Co ratio as well. If the traditional approach, designated method #1, of assuming complete oxidation of reduced metals to their respective oxides is used, then the increase is only slight (i.e., from 11.2 to 15.2 nm). However, if method #2 is used, the difference is wider (i.e., from 7.0 to 13.5 nm). Method #2 assumes that, during reduction, all  $\text{Co}_3\text{O}_4$  reduces to  $\text{CoO}$ , while only a portion of  $\text{CoO}$  reduces to  $\text{Co}^0$  (and a fraction of  $\text{NiO}$  reduces to  $\text{Ni}^0$ ). Thus, during the reoxidation with  $\text{O}_2$  pulse, the  $\text{Ni}^0$  and  $\text{Co}^0$  oxidize to  $\text{NiO}$  and  $\text{CoO}$ , and all  $\text{CoO}$  (including  $\text{CoO}$  obtained from  $\text{Co}^0$  oxidation as well as the  $\text{CoO}$  previously resulting from merely partial reduction of  $\text{Co}_3\text{O}_4$ ) oxidizes to  $\text{Co}_3\text{O}_4$ .

**Table 2:** H<sub>2</sub> chemisorption and pulse O<sub>2</sub> titration.

μmol H <sub>2</sub> desorbed/g <sub>cat</sub>	Uncorr. % Disp.	Uncorr. Diam. (nm)	O <sub>2</sub> uptake (μmol/g <sub>cat</sub> )	* % Red.	** % Red.	* % Disp.	** % Disp.	* Corr. Diam. (nm)	** Corr. Diam. (nm)
<b>25%Co/Al<sub>2</sub>O<sub>3</sub></b>									
91.3	4.3	24	1324	46.8	29.1	9.2	14.8	11.2	7.0
<b>25%M(95%Co-5%Ni)/Al<sub>2</sub>O<sub>3</sub></b>									
104.0	4.9	21.1	1317	47.3	30.4	10.4	16.1	10.0	6.4
<b>25%M(90%Co-10%Ni)/Al<sub>2</sub>O<sub>3</sub></b>									
92.5	4.4	24	1495	54.6	40.5	8.0	10.8	12.9	9.6
<b>25%M(75%Co-25%Ni)/Al<sub>2</sub>O<sub>3</sub></b>									
94.6	4.5	23.2	1563	59.9	48.7	7.5	9.2	13.9	11.3
<b>25%M(50%Co-50%Ni)/Al<sub>2</sub>O<sub>3</sub></b>									
94.7	4.5	23.1	1594	65.7	58.5	6.8	7.6	15.2	13.5

\* method #1 assuming Ni<sup>0</sup> oxidizes to NiO and Co<sup>0</sup> oxidizes to Co<sub>3</sub>O<sub>4</sub>.

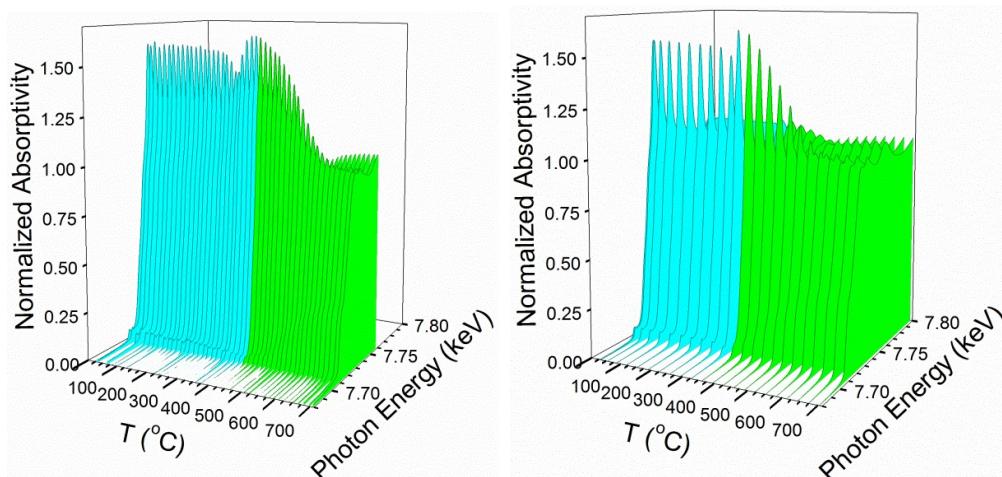
\*\* method #2 assuming all Co<sub>3</sub>O<sub>4</sub> reduced to CoO and some NiO and CoO reduced to Ni<sup>0</sup> and Co<sup>0</sup>. During oxidation, then, the Ni<sup>0</sup> and Co<sup>0</sup> oxidize to NiO and CoO, and all CoO oxidizes to Co<sub>3</sub>O<sub>4</sub>.

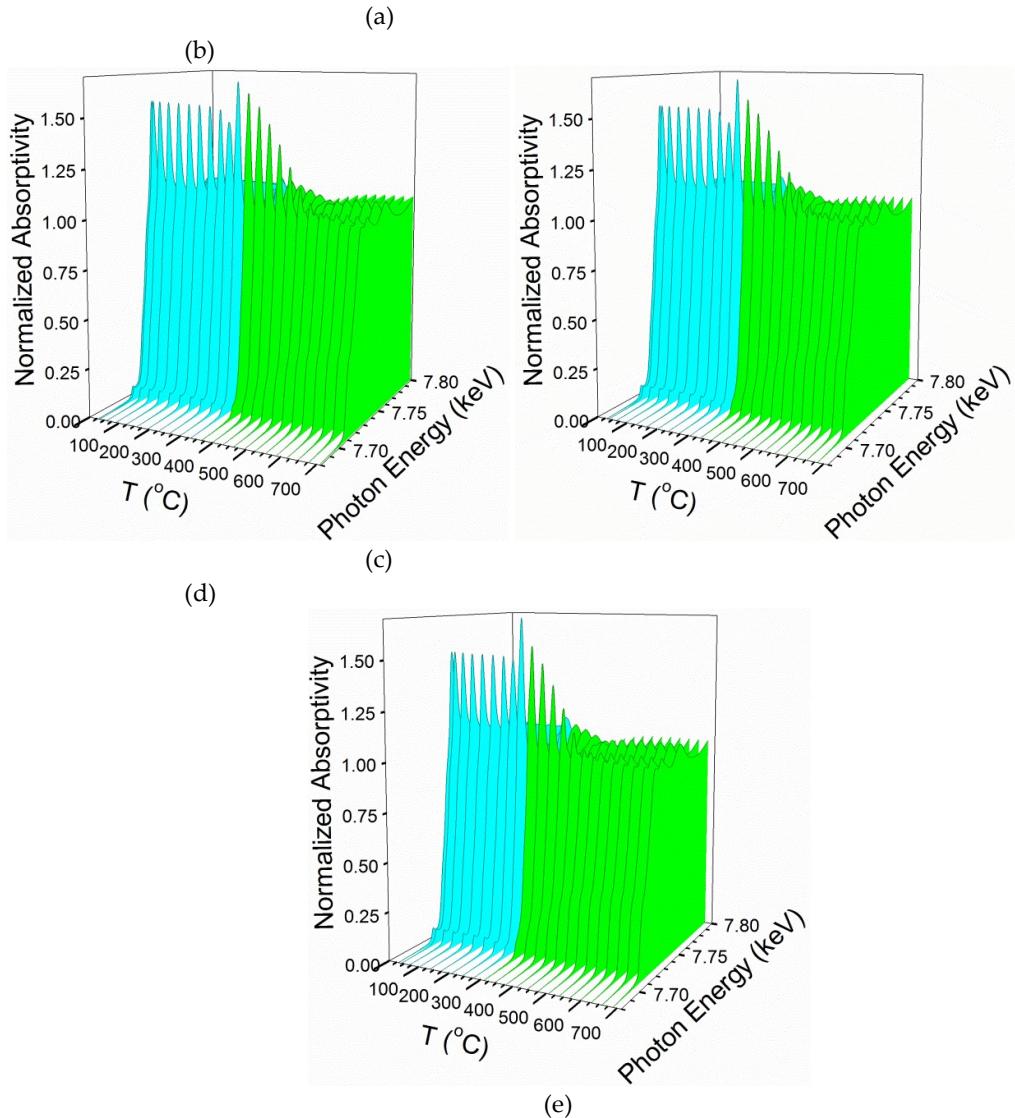
## 2.2 Cobalt reducibility

### H<sub>2</sub> TPR-XANES

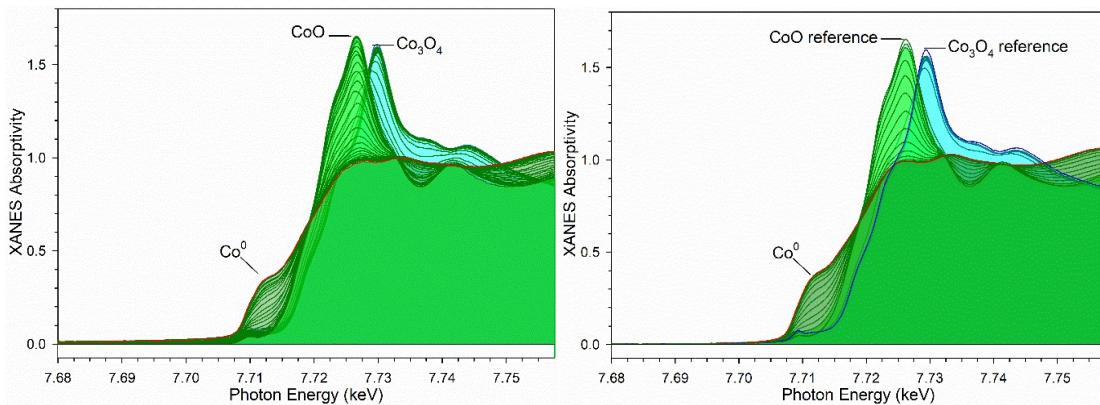
Figures 4 and 5 display H<sub>2</sub> TPR-XANES spectra for the prepared samples at the Co K-edge as a function of increasing Ni/Co ratio using two different perspectives. The perspective of Figure 4 is versus temperature, whereas the perspective of Figure 5 is that of photon energy. XANES snapshots at the point of 100% Co<sub>3</sub>O<sub>4</sub>, 100% CoO, and the final spectrum at the point of maximum reduction to Co<sup>0</sup> are shown in Figure 6. Cobalt oxides reduce to metallic compounds in two steps: (I) Co<sub>3</sub>O<sub>4</sub> + H<sub>2</sub> = 3CoO + H<sub>2</sub>O and (II) 3CoO + 3H<sub>2</sub> = 3Co<sup>0</sup> + 3H<sub>2</sub>O. Figure 6 shows that with increasing Ni/Co ratio, the reduction of cobalt oxides systematically moves to lower temperature.

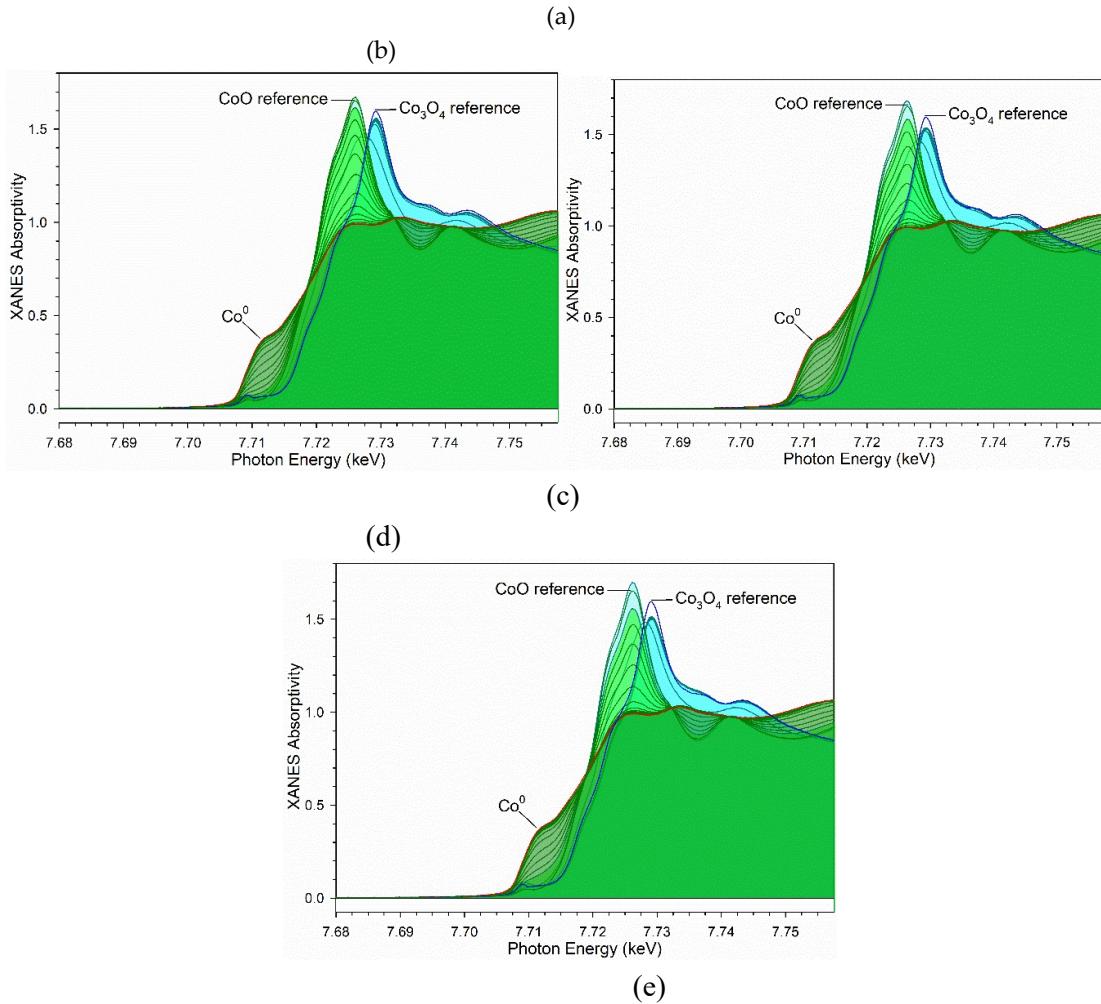
For all of the catalysts, the initial spectrum at 25°C resembles that of Co<sub>3</sub>O<sub>4</sub>. The point of 50%Co<sub>3</sub>O<sub>4</sub>/50%CoO was reached at 339 °C (Ni/Co = 0/100), 308 °C (Ni/Co = 5/95), 294 °C (Ni/Co = 10/90), 273 °C (Ni/Co = 25/75), and 249 °C (Ni/Co = 50/50). Thus, up to a Δ 90°C decrease in reduction temperature was achieved. The point of 100%CoO was obtained at 400 °C (Ni/Co = 0/100), 330 °C (Ni/Co = 5/95), 330 °C (Ni/Co = 10/90), 305 °C (Ni/Co = 25/75), and 278 °C (Ni/Co = 50/50). Thus, up to a Δ 122°C decrease in reduction temperature was obtained in converting Co<sub>3</sub>O<sub>4</sub> to CoO.



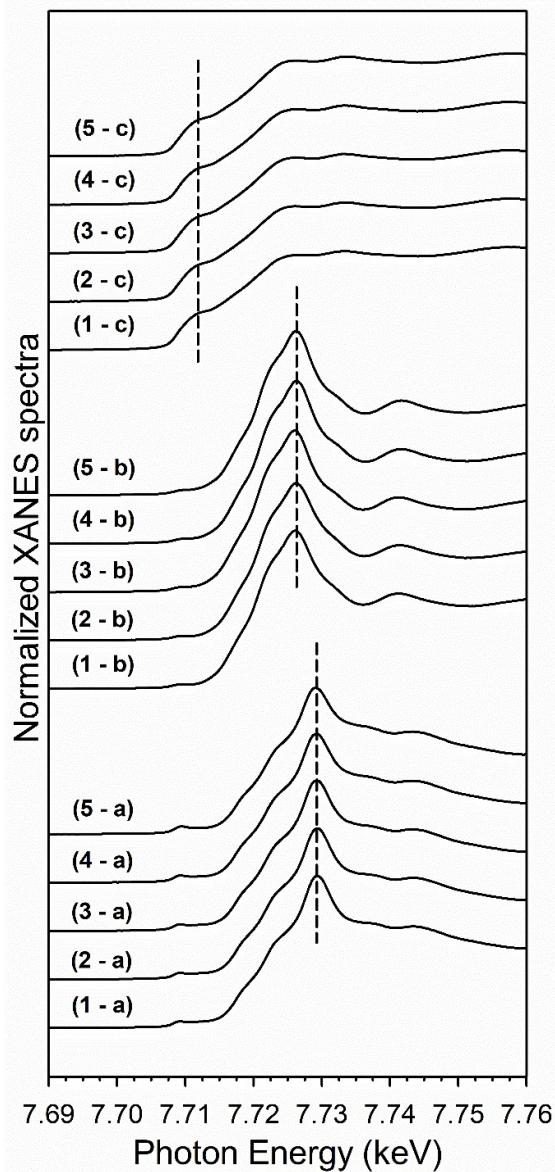


**Figure 4:** H<sub>2</sub>-TPR-XANES spectra at the Co K-edge of (a) 25%Co/Al<sub>2</sub>O<sub>3</sub>, (b) 25%M (M = 5%Ni-95%Co)/Al<sub>2</sub>O<sub>3</sub>, (c) 25%M (M = 10%Ni-90%Co)/Al<sub>2</sub>O<sub>3</sub>, (d) 25%M (M = 25%Ni-75%Co)/Al<sub>2</sub>O<sub>3</sub>, and (e) 25%M (M = 50%Ni-50%Co)/Al<sub>2</sub>O<sub>3</sub>.

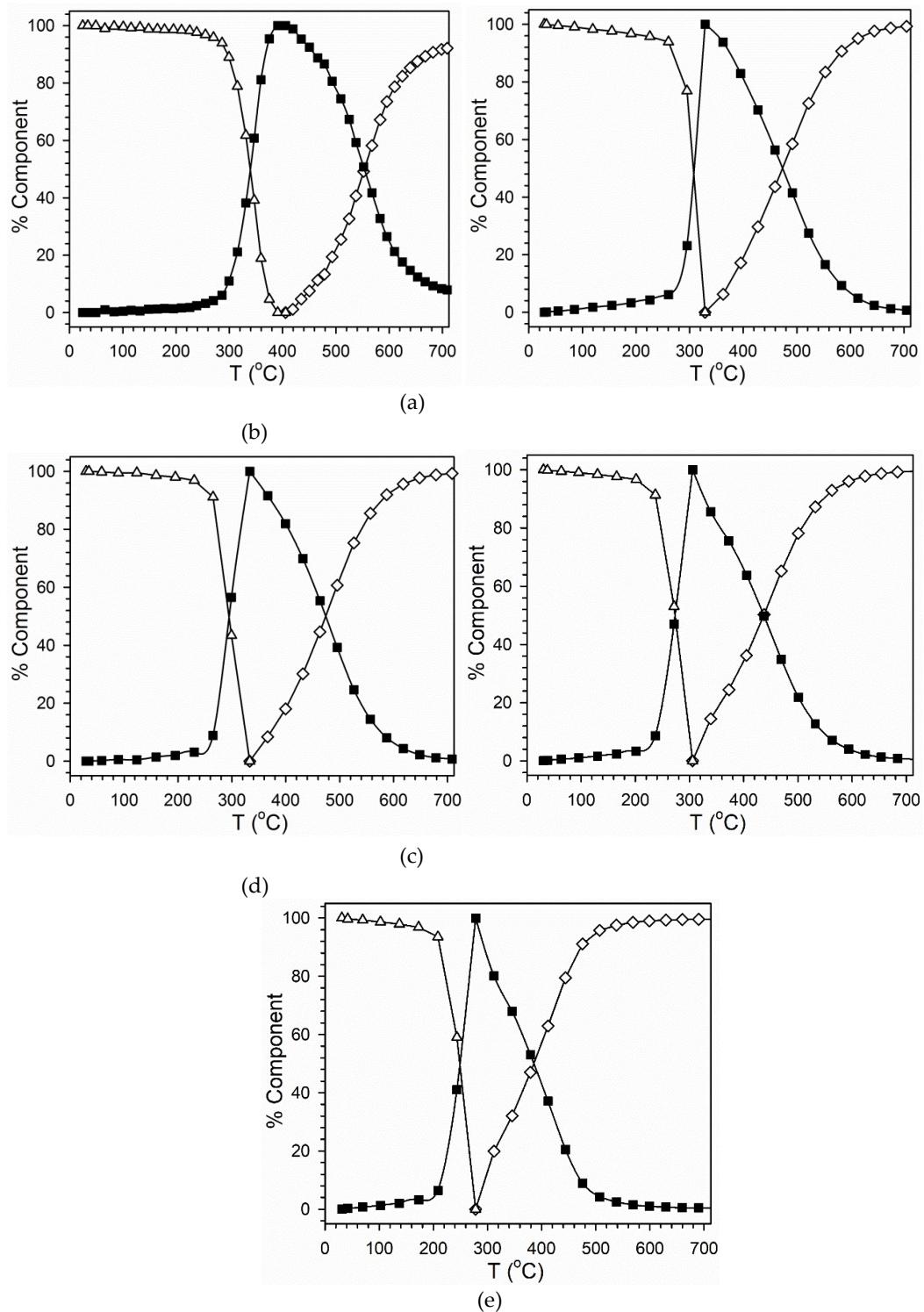




**Figure 5:**  $\text{H}_2$ -TPR-XANES spectra (XY view) at the Co K-edge of (a) 25%Co/Al<sub>2</sub>O<sub>3</sub>, (b) 25%M (M = 5%Ni-95%Co)/Al<sub>2</sub>O<sub>3</sub>, (c) 25%M (M = 10%Ni-90%Co)/Al<sub>2</sub>O<sub>3</sub>, (d) 25%M (M = 25%Ni-75%Co)/Al<sub>2</sub>O<sub>3</sub>, and (e) 25%M (M = 50%Ni-50%Co)/Al<sub>2</sub>O<sub>3</sub>.



**Figure 6:** Co K-edge XANES spectra of (a) initial point consisting of primarily  $\text{Co}_3\text{O}_4$ , (b) point of maximum  $\text{CoO}$  content, and (c) final spectrum consisting of primarily  $\text{Co}^0$  for (1) 25% $\text{Co}/\text{Al}_2\text{O}_3$ , (2) 25% $\text{M}$  ( $\text{M} = 5\%\text{Ni}-95\%\text{Co}$ )/ $\text{Al}_2\text{O}_3$ , (3) 25% $\text{M}$  ( $\text{M} = 10\%\text{Ni}-90\%\text{Co}$ )/ $\text{Al}_2\text{O}_3$ , (4) 25% $\text{M}$  ( $\text{M} = 25\%\text{Ni}-75\%\text{Co}$ )/ $\text{Al}_2\text{O}_3$ , (5) 25% $\text{M}$  ( $\text{M} = 50\%\text{Ni}-50\%\text{Co}$ )/ $\text{Al}_2\text{O}_3$ .



**Figure 7:** LC fittings of H<sub>2</sub>-TPR-XANES spectra at the Co K-edge of (a) 25%Co/Al<sub>2</sub>O<sub>3</sub>, (b) 25%M (M = 5%Ni-95%Co)/Al<sub>2</sub>O<sub>3</sub>, (c) 25%M (M = 10%Ni-90%Co)/Al<sub>2</sub>O<sub>3</sub>, (d) 25%M (M = 25%Ni-75%Co)/Al<sub>2</sub>O<sub>3</sub>, and (e) 25%M (M = 50%Ni-50%Co)/Al<sub>2</sub>O<sub>3</sub>.

The point of 50%CoO/50%Co<sup>0</sup> was attained at 553 °C (Ni/Co = 0/100), 473 °C (Ni/Co = 5/95), 473 °C (Ni/Co = 10/90), 437 °C (Ni/Co = 25/75), and 386 °C (Ni/Co = 50/50). Thus, up to a Δ 167°C decrease in reduction temperature was achieved by doping Co with Ni. It is evident that, unlike the Group 10 metal Pt, where substantial shifts in the reduction of Co oxides were observed with minute amounts of Pt, significantly higher quantities of Ni are required to achieve the same level of reduction. For example, just 0.5%Pt was able to facilitate a decrease of 194°C for the Co<sub>3</sub>O<sub>4</sub> to CoO transition, and a decrease of 120°C from CoO to Co<sup>0</sup> [23], which is < 1/40<sup>th</sup> of the atomic amount. In comparison with the TPR profile of CoO during reduction of undoped 25%Co/Al<sub>2</sub>O<sub>3</sub>, this is likely in part due to the strong interactions between Ni oxides and alumina support.

## H<sub>2</sub> TPR-EXAFS

TPR-EXAFS spectra at the Co K-edge are shown in Figures 8 and 9, including a plot that highlights the temperature (Figure 8), and a plot that emphasizes differences as a function of distance from the absorber (Figure 9). The initial cyan spectrum of each TPR-EXAFS profile represents Co<sub>3</sub>O<sub>4</sub>. It can be differentiated from CoO (i.e., the first green spectrum) by the fact that the Co-O peak is significantly more intense, while the Co-Co coordination peak is broadened due to the presence of additional oxygen atoms (Figure 9). Following the transition to CoO, the CoO slowly converts to Co<sup>0</sup>, resulting in a final well-resolved peak for Co-Co metal coordination. In a manner similar to Pt and Ru promoters, Ni facilitates both steps of reduction – however, as mentioned previously, on an atomically equivalent basis, Ni is far less effective than either Pt or Ru [23]. It differs from Re, which only catalyzes the second step, CoO reduction to Co<sup>0</sup>. Unlike Pt and Ru oxides, which reduce at low temperatures, Re oxide was observed to reduce at a similar range as Co<sub>3</sub>O<sub>4</sub> reduction to CoO (e.g. 300 – 350°C), and it was supposed that a reduced form was necessary in order to facilitate CoO reduction through a H<sub>2</sub> dissociation and spillover mechanism [23]. Thus, if a hydrogen dissociation and spillover mechanism operated for the case of Ni, one would expect that NiO should reduce to Ni<sup>0</sup> prior to the reduction of Co oxides. Based on the Ni X-ray absorption spectroscopy results, this does not seem to be the case.

### 2.3 Nickel reducibility

## H<sub>2</sub> TPR-XANES

TPR-XANES spectra in Figure 11 and 12 at the Ni K-edge reveal that, initially, Ni oxide is associated with Co<sub>3</sub>O<sub>4</sub> (see spectra in cyan color) and this Ni oxide subsequently undergoes a change in electronic structure to a form of Ni oxide associated with CoO (initial green spectrum). This change is best observed by examining the head-on spectra of Figure 13, as well as the XANES snapshots shown in Figure 14. Let us refer to this transition as step one. Step two is further reduction of Ni<sup>2+</sup> to Ni<sup>0</sup> (dark green spectra in Figure 12).

Figure 14 provides quantitative information regarding the Ni species present along the TPR trajectory. In step one, the point of 50%Ni<sup>2+</sup>-Co<sub>3</sub>O<sub>4</sub> / 50%Ni<sup>2+</sup>-CoO was reached at 333 °C (Ni/Co = 5/95), 286 °C (Ni/Co = 10/90), 261 °C (Ni/Co = 25/75), and 234 °C (Ni/Co = 50/50). Thus, up to a Δ 99°C decrease in reduction temperature was achieved (compared to a Δ of 60°C for the cobalt system over the same range of loading), and the temperatures match well with those of the Co<sub>3</sub>O<sub>4</sub> to CoO transitions described earlier at the 50% point of conversion, especially at higher Ni/Co ratios. The point of 100%Ni<sup>2+</sup>-CoO was obtained at 362 °C (Ni/Co = 5/95), 332 °C (Ni/Co = 10/90), 305 °C (Ni/Co = 25/75), and 278 °C (Ni/Co = 50/50). Thus, up to a Δ 84°C decrease in reduction temperature was obtained in converting 100%Ni<sup>2+</sup>-Co<sub>3</sub>O<sub>4</sub> to 100%Ni<sup>2+</sup>-CoO (compared to a Δ of 52°C for the cobalt system over the same range of loading). Once again, the temperatures match quite well with those of the Co<sub>3</sub>O<sub>4</sub> to CoO transitions described earlier for Co K-edge data, and match nearly perfectly at Ni/Co loadings of 10%, 25%, and 50%.

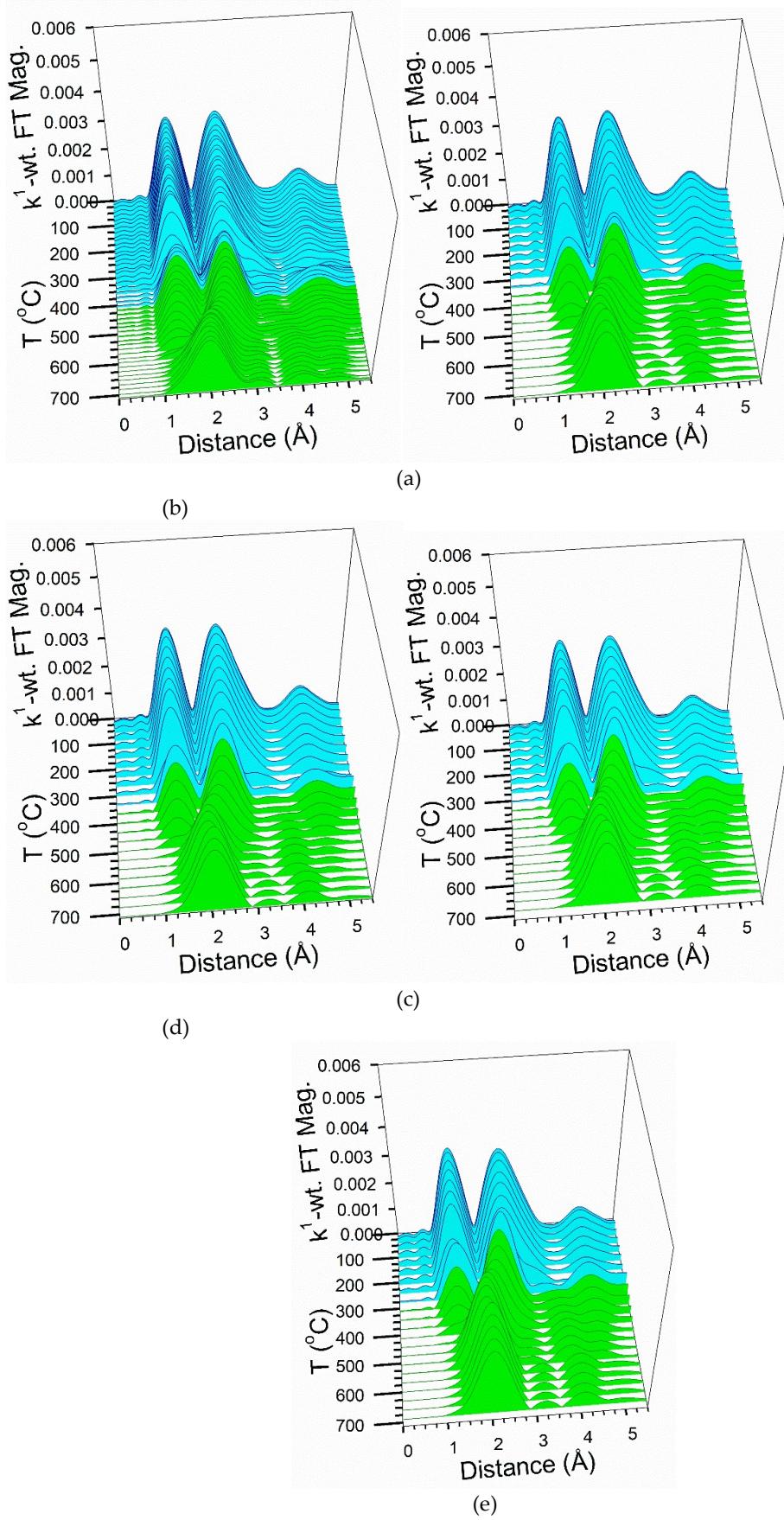
Continuing, the point of 50%Ni<sup>2+</sup>-CoO/50%Ni<sup>0</sup> was achieved at 503 °C (Ni/Co = 5/95), 482 °C (Ni/Co = 10/90), 458 °C (Ni/Co = 25/75), and 412 °C (Ni/Co = 50/50). Thus, up to a Δ 91°C decrease in reduction temperature was achieved by doping Co with Ni (compared to a Δ of 87°C for the cobalt system over the same range of loading).

The similarities in temperature ranges between Co<sub>3</sub>O<sub>4</sub> to CoO and the Ni<sup>2+</sup>-Co<sub>3</sub>O<sub>4</sub> to Ni<sup>2+</sup>-CoO transitions, as well those between CoO to Co<sup>0</sup> and Ni<sup>2+</sup>-CoO to Ni<sup>0</sup>-Co<sup>0</sup> transitions, suggest that the effect may not be simply a H<sub>2</sub> dissociation and spillover mechanism, but rather a chemical effect due to intimate contact between Ni and Co in both oxide (e.g., solid solution) and metallic (e.g., alloy) phases, throughout the TPR trajectory.

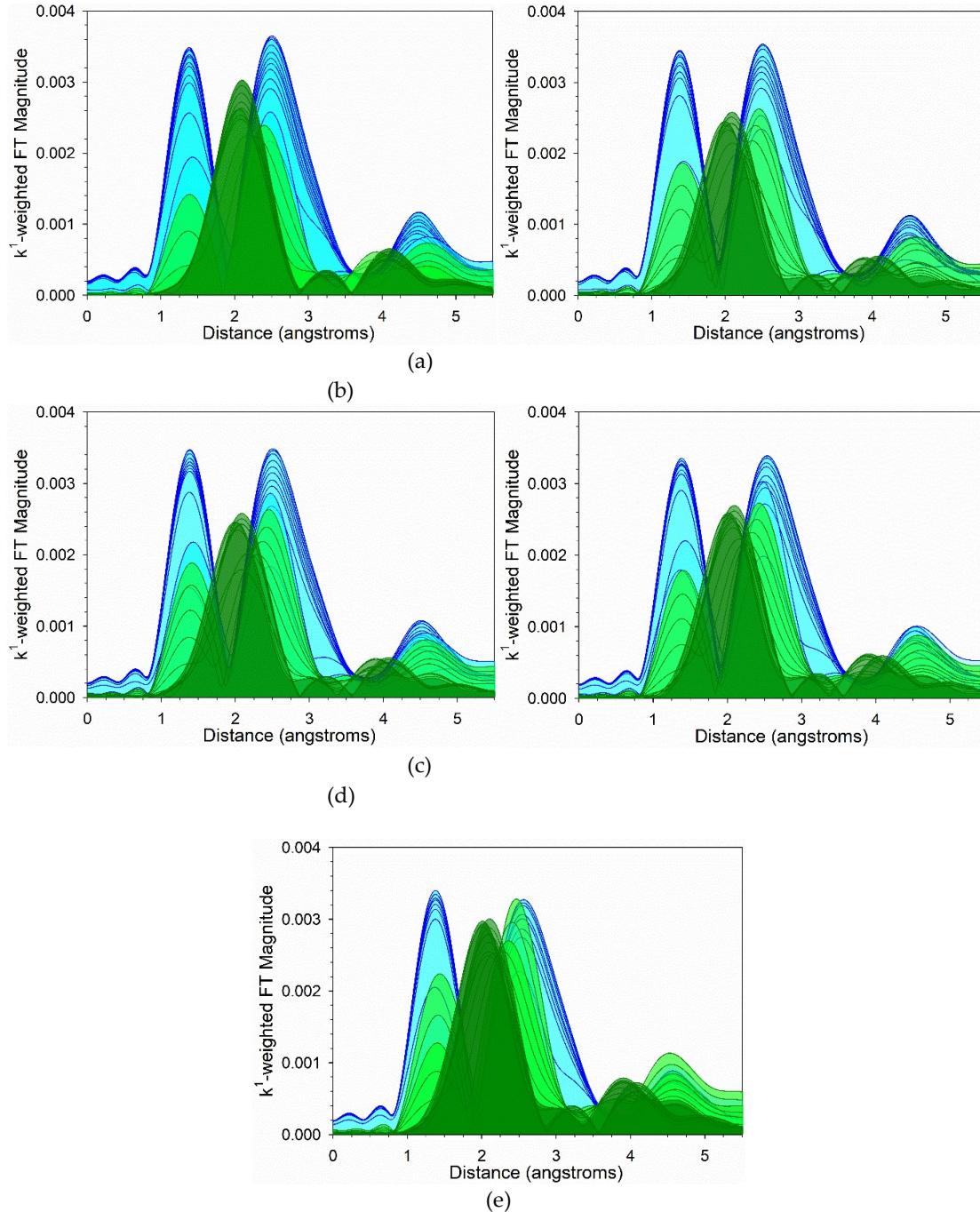
### H<sub>2</sub> TPR-EXAFS

Comparing the TPR-EXAFS spectra of Figure 15 with Figure 8, Figure 16 with Figure 9, and Figure 17 with Figure 10, it is remarkable how closely the behavior of Ni resembles that of Co. The initial cyan spectra of Figures 15 and 16 reveal that the first Ni-O peak is more intense than that of the green Ni-O peak, suggesting greater coordination to oxygen, while the second peak for Ni-Ni coordination in the initial cyan spectra is more broadened as compared to the initial green spectra, consistent with greater oxygen content forcing Ni atoms apart. Figure 17 highlights the differences between the local atomic structure of different species along the TPR profile (e.g., Co<sub>3</sub>O<sub>4</sub> associated with Ni<sup>2+</sup>; CoO associated with Ni<sup>2+</sup>; and Co<sup>0</sup> associated with Ni<sup>0</sup>).

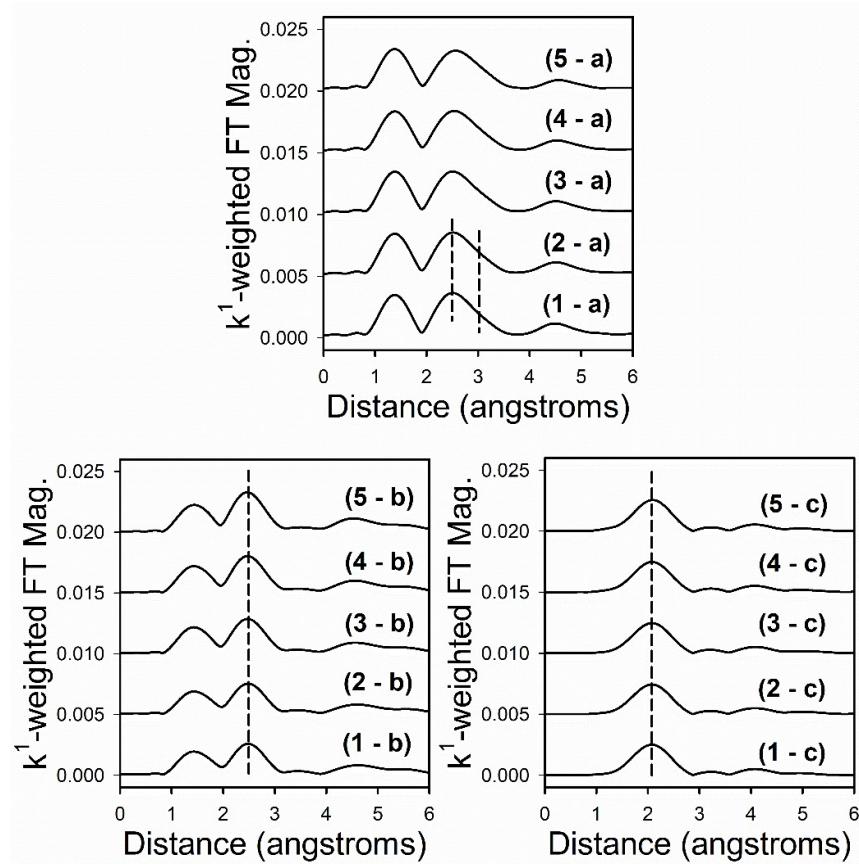
Figure 18 and 19, as well as Table 3, show EXAFS fittings for the Co K-edge and Ni K-edge data following TPR-EXAFS and cooling to ambient temperature. A simple model was developed previously [20] and applied here, where metal coordination to Ni (whether the core atom was Co or Ni) was given as a fraction, X, of metal-cobalt coordination. Using this approach, excellent fittings with low r-factors were obtained Co-Ni alloy formation is consistent with EXAFS fitting, but it cannot be considered a prove since Co and Ni are too closely related in size.



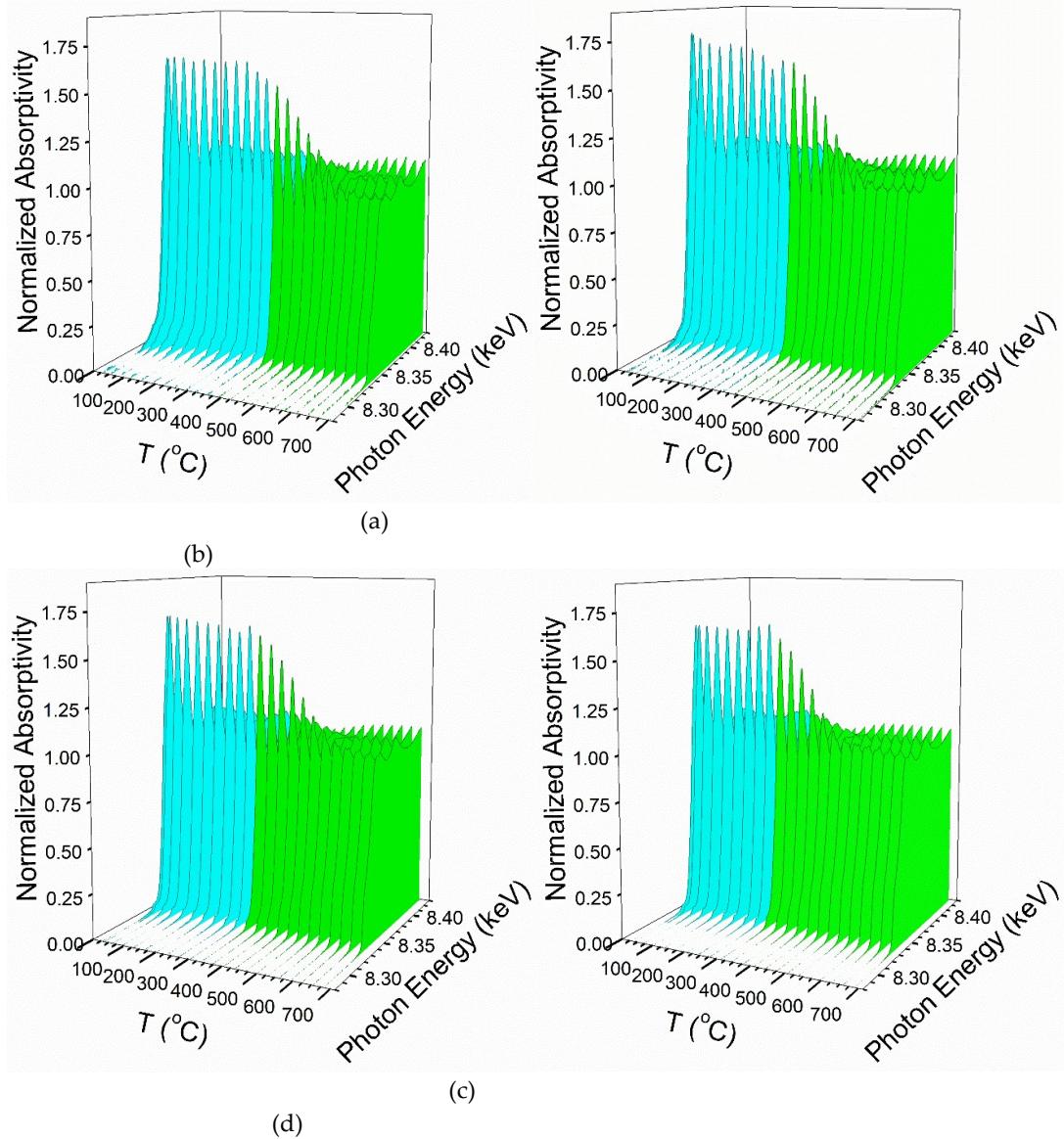
**Figure 8:** H<sub>2</sub>-TPR-EXAFS spectra at the Co K-edge of (a) 25%Co/Al<sub>2</sub>O<sub>3</sub>, (b) 25%M (M = 5%Ni-95%Co)/Al<sub>2</sub>O<sub>3</sub>, (c) 25%M (M = 10%Ni-90%Co)/Al<sub>2</sub>O<sub>3</sub>, (d) 25%M (M = 25%Ni-75%Co)/Al<sub>2</sub>O<sub>3</sub>, and (e) 25%M (M = 50%Ni-50%Co)/Al<sub>2</sub>O<sub>3</sub>. (Cyan) is reduction of Co<sub>3</sub>O<sub>4</sub> to CoO, and (Green) CoO to Co<sup>0</sup>.



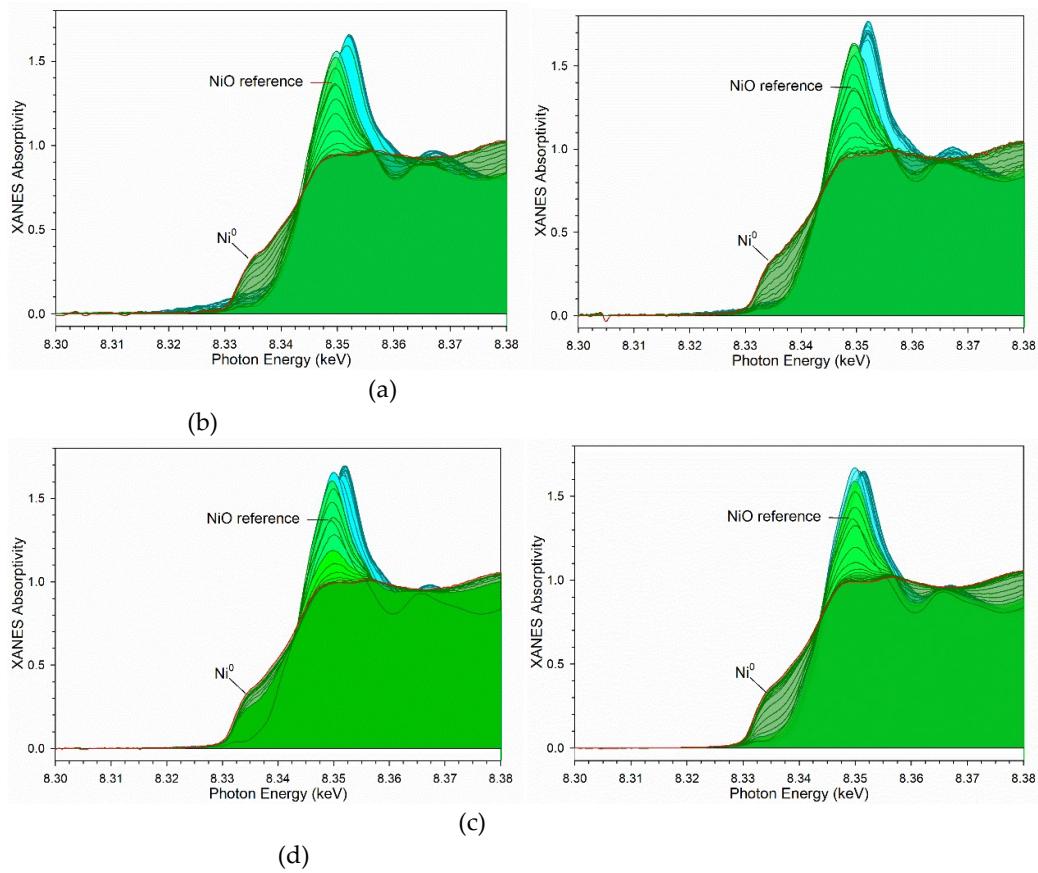
**Figure 9:** H<sub>2</sub>-TPR-EXAFS spectra (XY view) at the Co K-edge of (a) 25%Co/Al<sub>2</sub>O<sub>3</sub>, (b) 25%M (M = 5%Ni-95%Co)/Al<sub>2</sub>O<sub>3</sub>, (c) 25%M (M = 10%Ni-90%Co)/Al<sub>2</sub>O<sub>3</sub>, (d) 25%M (M = 25%Ni-75%Co)/Al<sub>2</sub>O<sub>3</sub>, and (e) 25%M (M = 50%Ni-50%Co)/Al<sub>2</sub>O<sub>3</sub>. (Cyan) is reduction of Co<sub>3</sub>O<sub>4</sub> to CoO, and (Green) CoO to Co<sup>0</sup>.



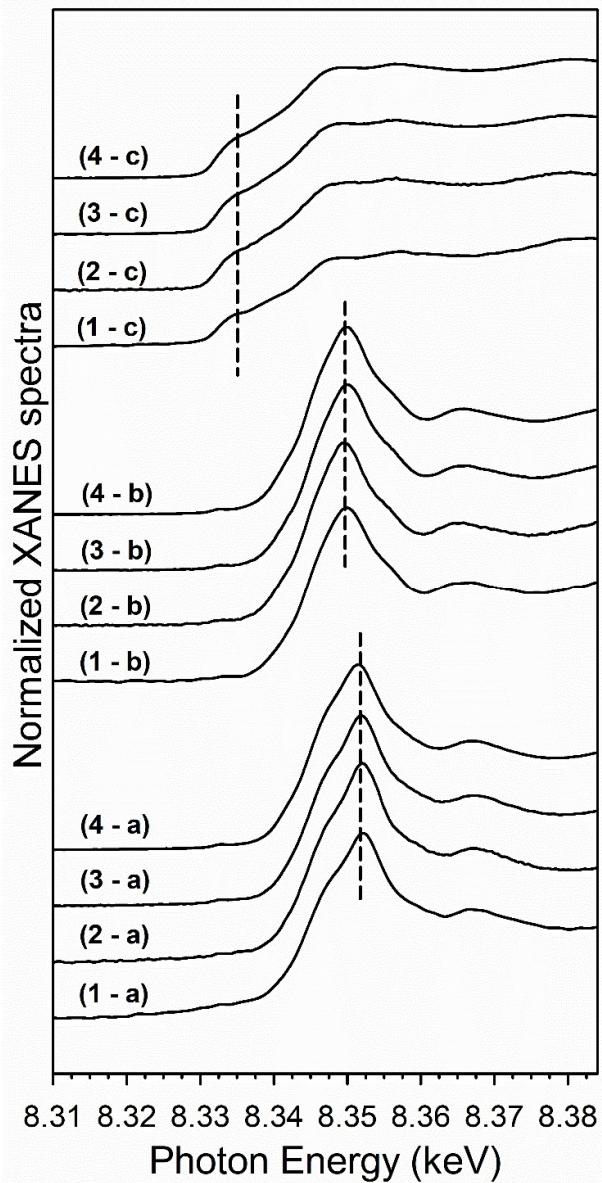
**Figure 10:** Co K-edge EXAFS spectra of (a) initial point consisting of primarily  $\text{Co}_3\text{O}_4$ , (b) point of maximum CoO content, and (c) final spectrum consisting of primarily  $\text{Co}^0$  for (1) 25%Co/ $\text{Al}_2\text{O}_3$ , (2) 25%M (M = 2.5%Ni-97.5%Co)/ $\text{Al}_2\text{O}_3$ , (3) 25%M (M = 5%Ni-95%Co)/ $\text{Al}_2\text{O}_3$ , (4) 25%M (M = 10%Ni-90%Co)/ $\text{Al}_2\text{O}_3$ , (5) 25%M (M = 25%Ni-75%Co)/ $\text{Al}_2\text{O}_3$ , (6) 25%M (M = 50%Ni-50%Co)/ $\text{Al}_2\text{O}_3$ .



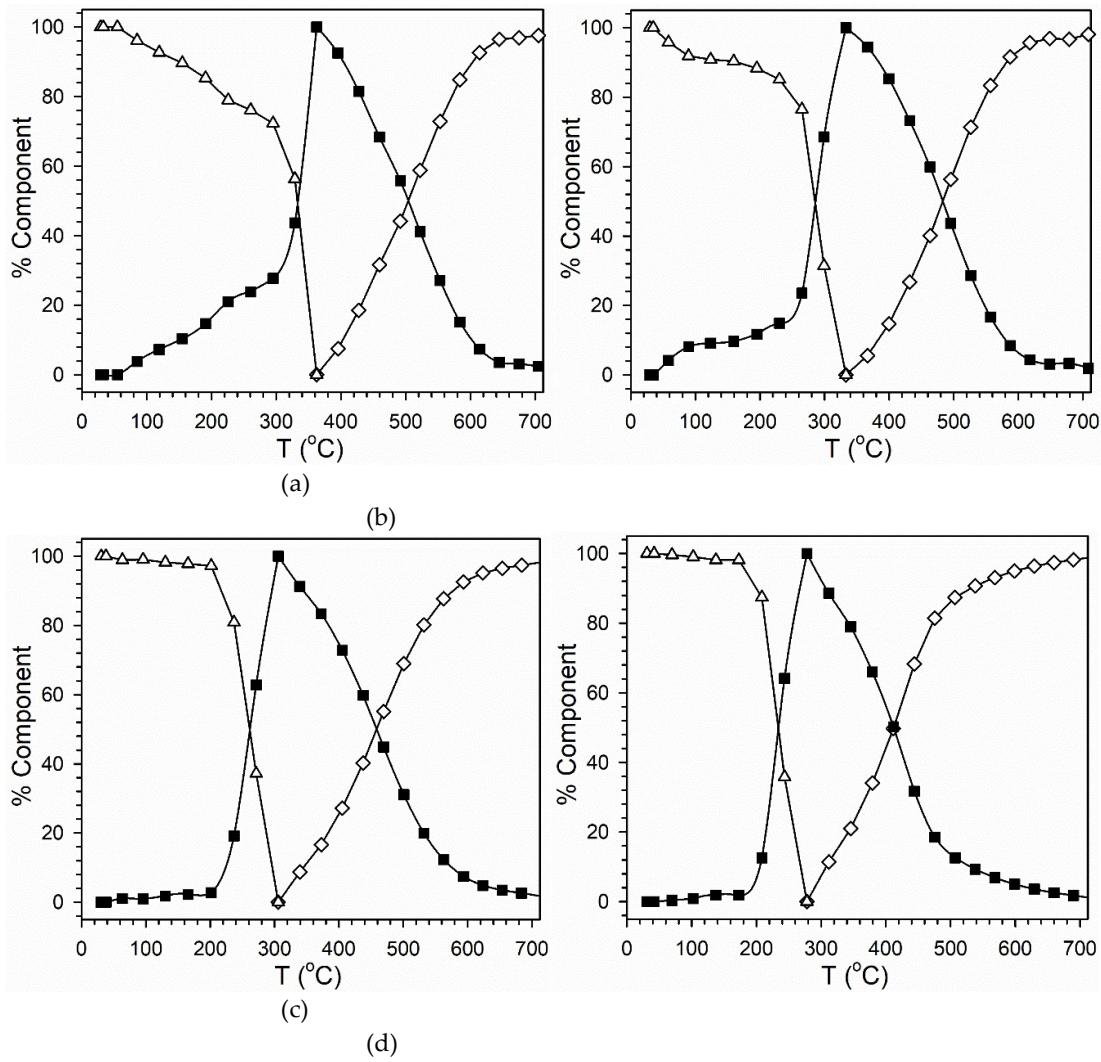
**Figure 11:** H<sub>2</sub>-TPR-XANES spectra at the Ni K-edge of (a) 25%M (M = 5%Ni-95%Co)/Al<sub>2</sub>O<sub>3</sub>, (b) 25%M (M = 10%Ni-90%Co)/Al<sub>2</sub>O<sub>3</sub>, (c) 25%M (M = 25%Ni-75%Co)/Al<sub>2</sub>O<sub>3</sub>, and (d) 25%M (M = 50%Ni-50%Co)/Al<sub>2</sub>O<sub>3</sub>. (Cyan) is Ni<sup>2+</sup> (e.g., NiO) associated with cobalt oxides during reduction of Co<sub>3</sub>O<sub>4</sub> to CoO. (Green) is reduction of Ni<sup>2+</sup> to Ni<sup>0</sup> when NiO reduction is associated with CoO reduction to Co<sup>0</sup>.



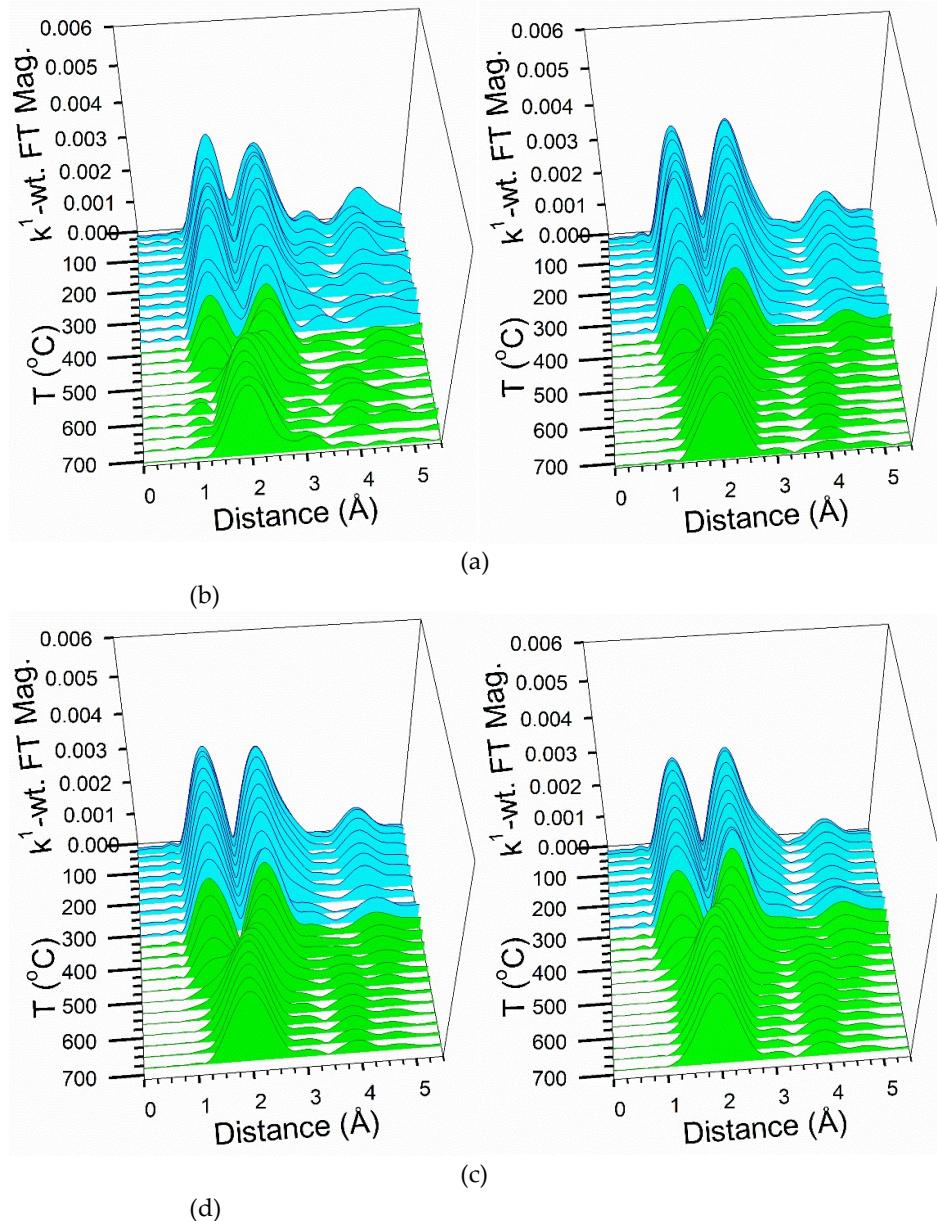
**Figure 12:**  $\text{H}_2$ -TPR-XANES spectra at the Ni K-edge of (a) 25% M ( $\text{M} = 5\% \text{Ni}-95\% \text{Co}/\text{Al}_2\text{O}_3$ , (b) 25% M ( $\text{M} = 10\% \text{Ni}-90\% \text{Co}/\text{Al}_2\text{O}_3$ , (c) 25% M ( $\text{M} = 25\% \text{Ni}-75\% \text{Co}/\text{Al}_2\text{O}_3$ , and (d) 25% M ( $\text{M} = 50\% \text{Ni}-50\% \text{Co}/\text{Al}_2\text{O}_3$ . (Cyan) is  $\text{Ni}^{2+}$  (e.g.,  $\text{NiO}$ ) associated with cobalt oxides during reduction of  $\text{Co}_3\text{O}_4$  to  $\text{CoO}$ . (Green) is reduction of  $\text{Ni}^{2+}$  to  $\text{Ni}^0$  when  $\text{NiO}$  reduction is associated with  $\text{CoO}$  reduction to  $\text{Co}^0$ .



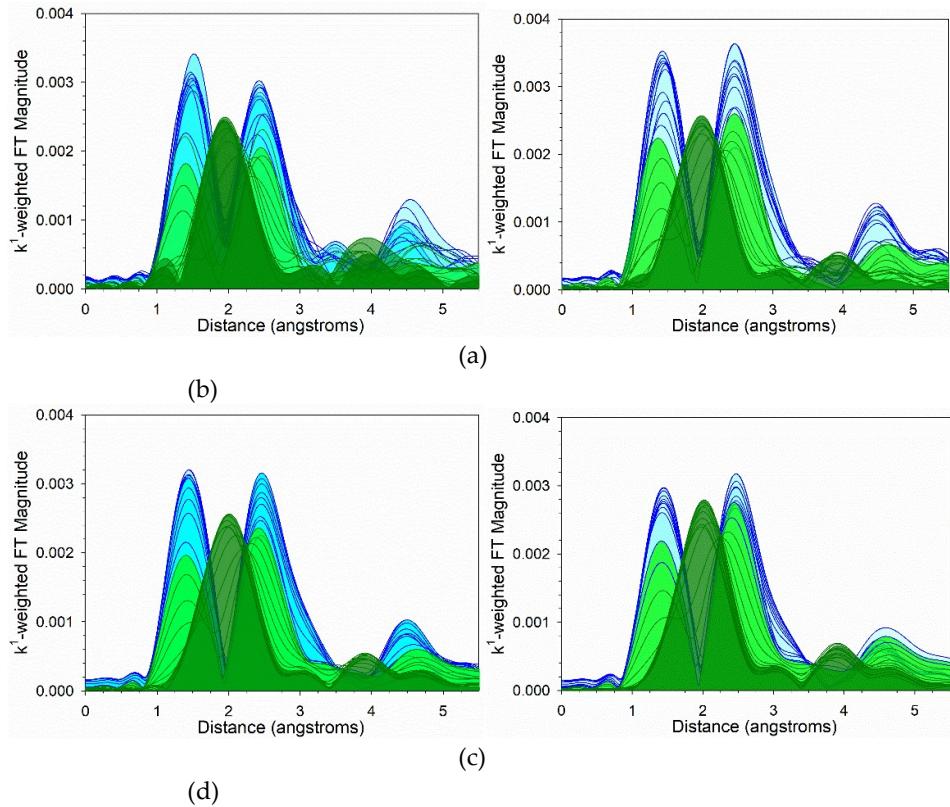
**Figure 13:** Ni K-edge XANES spectra of (a) initial point consisting of primarily NiO associated with  $\text{Co}_3\text{O}_4$ , (b) point consisting of primarily NiO associated with CoO, and (c) final spectrum consisting of primarily  $\text{Ni}^0$  for (2) 25%M ( $M = 2.5\% \text{Ni}-97.5\% \text{Co}/\text{Al}_2\text{O}_3$ , (3) 25%M ( $M = 5\% \text{Ni}-95\% \text{Co}/\text{Al}_2\text{O}_3$ , (4) 25%M ( $M = 10\% \text{Ni}-90\% \text{Co}/\text{Al}_2\text{O}_3$ , (5) 25%M ( $M = 25\% \text{Ni}-75\% \text{Co}/\text{Al}_2\text{O}_3$ , (6) 25%M ( $M = 50\% \text{Ni}-50\% \text{Co}/\text{Al}_2\text{O}_3$ .



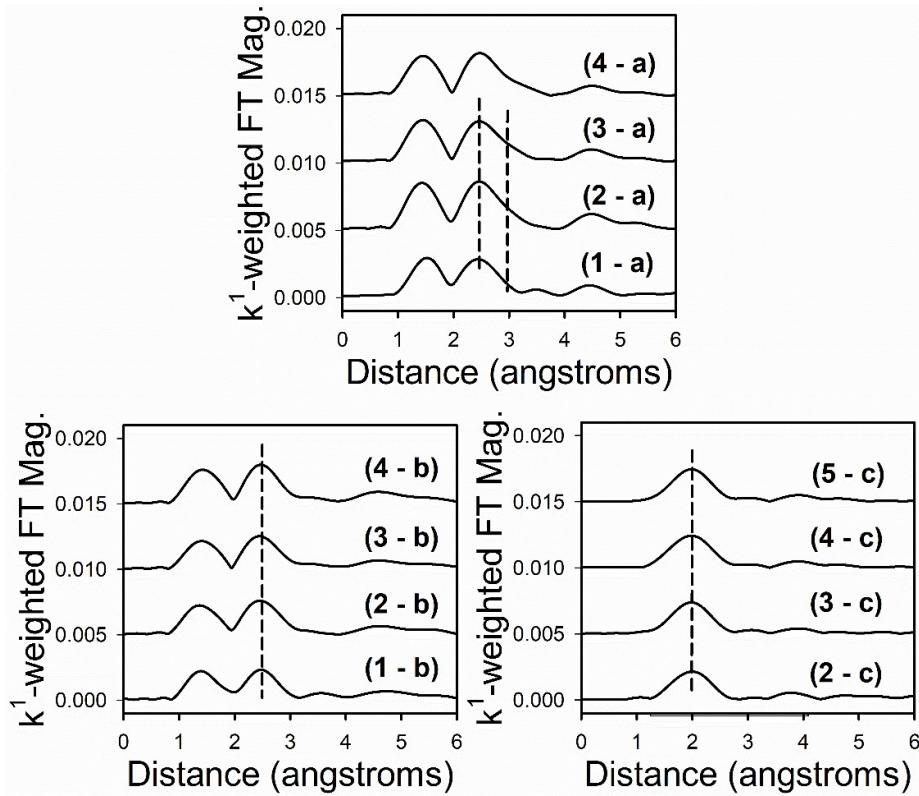
**Figure 14:** LC fittings of  $\text{H}_2$ -TPR-XANES spectra at the Ni K-edge of (a) 25%M (M = 5%Ni-95%Co)/ $\text{Al}_2\text{O}_3$ , (b) 25%M (M = 10%Ni-90%Co)/ $\text{Al}_2\text{O}_3$ , (c) 25%M (M = 25%Ni-75%Co)/ $\text{Al}_2\text{O}_3$ , and (d) 25%M (M = 50%Ni-50%Co)/ $\text{Al}_2\text{O}_3$ . Legend:  $\triangle$   $\text{Co}_3\text{O}_4$  associated with  $\text{Ni}^{2+}$ ,  $\blacksquare$   $\text{CoO}$  associated with  $\text{Ni}^{2+}$ , and  $\diamond$   $\text{Ni}^0$  associated with  $\text{Co}^0$ .



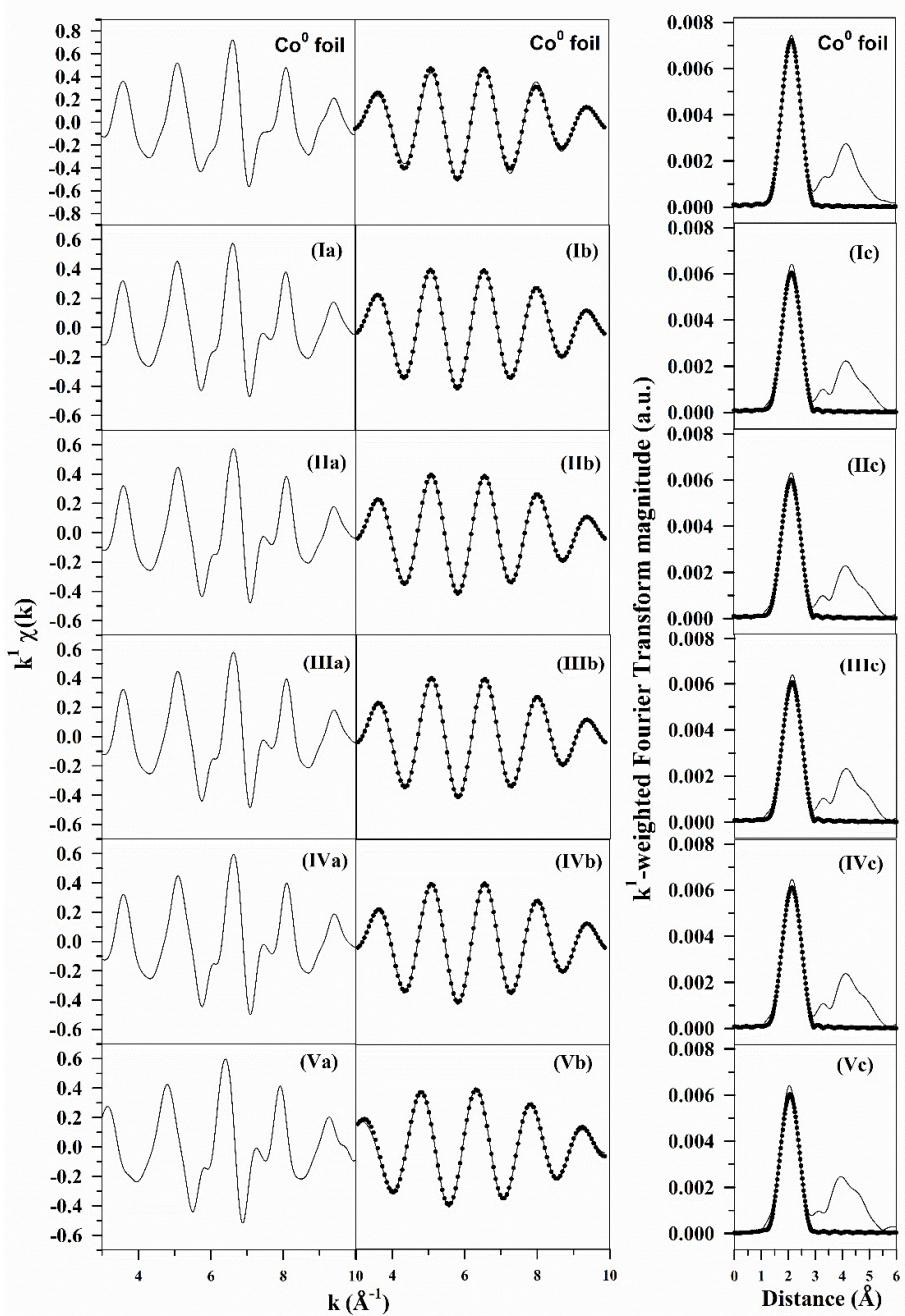
**Figure 15:** H<sub>2</sub>-TPR-EXAFS spectra at the Ni K-edge of (a) 25%M (M = 5%Ni-95%Co)/ $\text{Al}_2\text{O}_3$ , (b) 25%M (M = 10%Ni-90%Co)/ $\text{Al}_2\text{O}_3$ , (c) 25%M (M = 25%Ni-75%Co)/ $\text{Al}_2\text{O}_3$ , and (d) 25%M (M = 50%Ni-50%Co)/ $\text{Al}_2\text{O}_3$ . (Cyan) is  $\text{Ni}^{2+}$  (e.g.,  $\text{NiO}$ ) associated with cobalt oxides during reduction of  $\text{Co}_3\text{O}_4$  to  $\text{CoO}$ . (Green) is reduction of  $\text{Ni}^{2+}$  to  $\text{Ni}^{10}$  when  $\text{NiO}$  reduction is associated with  $\text{CoO}$  reduction to  $\text{Co}^0$ .



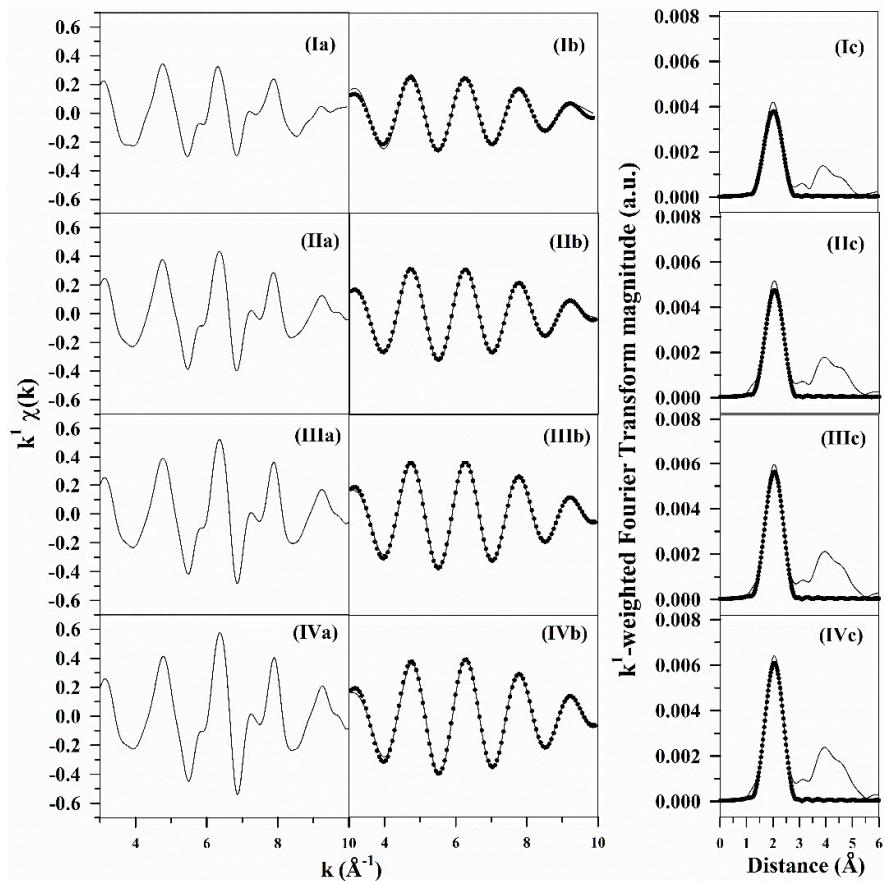
**Figure 16:** H<sub>2</sub>-TPR-EXAFS spectra at the Ni K-edge of (a) 25%M (M = 5%Ni-95%Co)/Al<sub>2</sub>O<sub>3</sub>, (b) 25%M (M = 10%Ni-90%Co)/Al<sub>2</sub>O<sub>3</sub>, (c) 25%M (M = 25%Ni-75%Co)/Al<sub>2</sub>O<sub>3</sub>, and (d) 25%M (M = 50%Ni-50%Co)/Al<sub>2</sub>O<sub>3</sub>. (Cyan) is Ni<sup>2+</sup> (e.g., NiO) associated with cobalt oxides during reduction of Co<sub>3</sub>O<sub>4</sub> to CoO. (Green) is reduction of Ni<sup>2+</sup> to Ni<sup>0</sup> when NiO reduction is associated with CoO reduction to Co<sup>0</sup>.



**Figure 17:** Ni K-edge EXAFS spectra of (a) initial point consisting of primarily NiO associated with  $\text{Co}_3\text{O}_4$ , (b) point consisting of primarily NiO associated with CoO, and (c) final spectrum consisting of primarily  $\text{Ni}^0$  for (2) 25%M (M = 2.5%Ni-97.5%Co)/ $\text{Al}_2\text{O}_3$ , (3) 25%M (M = 5%Ni-95%Co)/ $\text{Al}_2\text{O}_3$ , (4) 25%M (M = 10%Ni-90%Co)/ $\text{Al}_2\text{O}_3$ , (5) 25%M (M = 25%Ni-75%Co)/ $\text{Al}_2\text{O}_3$ , (6) 25%M (M = 50%Ni-50%Co)/ $\text{Al}_2\text{O}_3$ .



**Figure 18:** EXAFS fittings for Co K-edge data, including (a) raw  $k^1$ -weighted  $\chi(k)$  data, (b) (solid line) filtered  $k^1$ -weighted  $\chi(k)$  data and (filled circles) results of the fittings, and (c) (solid line) raw  $k^1$ -weighted Fourier transform magnitude and (d) (solid line) filtered  $k^1$ -weighted Fourier transform magnitude and (filled circles) results of the fittings for  $\text{Co}^0$  foil, (I) 25%Co/Al<sub>2</sub>O<sub>3</sub>, (II) 25%M (M = 5%Ni-95%Co)/Al<sub>2</sub>O<sub>3</sub>, (III) 25%M (M = 10%Ni-90%Co)/Al<sub>2</sub>O<sub>3</sub>, (IV) 25%M (M = 25%Ni-75%Co)/Al<sub>2</sub>O<sub>3</sub>, (V) 25%M (M = 50%Ni-50%Co)/Al<sub>2</sub>O<sub>3</sub>.



**Figure 19:** EXAFS fittings for Ni K-edge data, including (a) raw  $k^1$ -weighted  $\chi(k)$  data, (b) (solid line) filtered  $k^1$ -weighted  $\chi(k)$  data and (filled circles) results of the fittings, and (c) (solid line) raw  $k^1$ -weighted Fourier transform magnitude and (d) (solid line) filtered  $k^1$ -weighted Fourier transform magnitude and (filled circles) results of the fittings for (I) 25% $M$  ( $M = 5\% \text{Ni}-95\% \text{Co}$ )/ $\text{Al}_2\text{O}_3$ , (II) 25% $M$  ( $M = 10\% \text{Ni}-90\% \text{Co}$ )/ $\text{Al}_2\text{O}_3$ , (III) 25% $M$  ( $M = 25\% \text{Ni}-75\% \text{Co}$ )/ $\text{Al}_2\text{O}_3$ , (IV) 25% $M$  ( $M = 50\% \text{Ni}-50\% \text{Co}$ )/ $\text{Al}_2\text{O}_3$ .

1

2 **Table 3:** Results of EXAFS fitting\* for data acquired near the Co and Ni K edges for catalysts following TPR-EXAFS after cooling. The fitting  
 3 ranges were  $\Delta k = 3 - 10 \text{ \AA}^{-1}$  and  $\Delta R = 1.2 - 2.8 \text{ \AA}$ . \* $S_0^2$  set to 0.90. Mixing parameter fixed to nominal value.

4

Sample Description	N Co-Co metal	R Co-Co ( $\text{\AA}$ ) metal	N Co-Ni metal	R Co-Ni ( $\text{\AA}$ ) metal	N Ni-Ni metal	R Ni-Ni ( $\text{\AA}$ ) metal	N Ni-Co metal	R Ni-Co ( $\text{\AA}$ ) Metal	$\epsilon_0$ (eV)	$\sigma^2$ ( $\text{\AA}^2$ )	r-factor
100Co	9.9	2.489 (0.003)	-	-	-	-	-	-	6.37 (0.45)	0.00731 (0.00043)	0.0010
5Ni:95Co	9.9 (0.78)	2.489 (0.0053)	0.50 (0.04)	2.481 (0.0053)	0.32 (0.03)	2.472 (0.0053)	6.3 (0.59)	2.481 (0.0053)	6.32 (0.813)	0.00787 (0.00076)	0.014
10Ni:90Co	9.4 (0.48)	2.492 (0.0034)	0.94 (0.05)	2.483 (0.0034)	0.75 (0.04)	2.475 (0.0034)	7.5 (0.41)	2.483 (0.0034)	6.56 (0.527)	0.00777 (0.00048)	0.0035
25Ni:75Co	8.0 (0.31)	2.491 (0.0026)	2.0 (0.08)	2.482 (0.0026)	1.9 (0.08)	2.474 (0.0026)	7.4 (0.32)	2.482 (0.0026)	6.71 (0.401)	0.00719 (0.00036)	0.0023
50Ni:50Co	6.5 (0.36)	2.491 (0.0035)	3.3 (0.18)	2.483 (0.0035)	3.2 (0.18)	2.475 (0.0035)	6.4 (0.36)	2.483 (0.0035)	-4.39 (0.613)	0.00659 (0.00049)	0.0034

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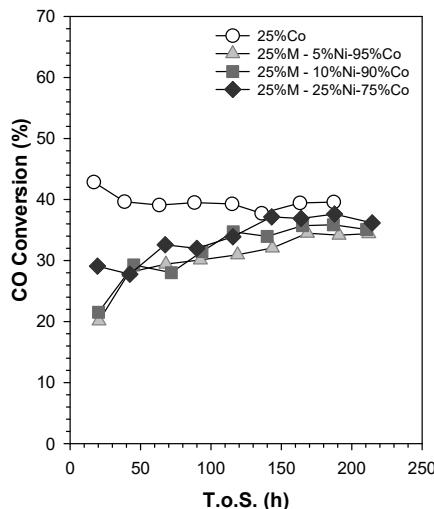
## 8    2.4 Catalytic activity

9

10    CO conversion in the first 200 h is shown in Figure 20. The CO conversion for the unpromoted  
 11 catalyst has an initial value of 42.5%, then it slightly decreases in the first few hours until a steady-  
 12 state value of 39.5% was reached. This trend is typical for cobalt-based catalysts. In contrast, CO  
 13 conversion progressively increases for all nickel promoted catalysts. 5%Ni-95%Co and 10%Ni-90%  
 14 exhibit similar CO conversion trends as the initial value is close to 20% and it continuously increases  
 15 reaching 34%, whereas 25%Ni-75Co has a higher initial CO conversion (29%) and it reaches a steady-  
 16 state value of 36%.

17    The evolution of selectivities ( $\text{CH}_4$ ,  $\text{CO}_2$ ,  $\text{C}_2\text{-C}_4$  and  $\text{C}_{5+}$ ) with T.o.S. is shown in Figure 21.  $\text{CH}_4$   
 18 selectivity and  $\text{C}_{5+}$  selectivities are stable at 7.6% and 80.7%, respectively, for the unpromoted catalyst.  
 19 The addition of nickel increases initial  $\text{CH}_4$  selectivity, whereas it decreases initial  $\text{C}_{5+}$  selectivity.  
 20 Fortunately,  $\text{CH}_4$  selectivity for the nickel promoted catalyst slowly decreased with T.o.S. For  
 21 example, the initial  $\text{CH}_4$  selectivity for 25%M-25%Ni-75%Co is 13.4%, but it reaches 9.5% after 200 h.  
 22 So, the difference as compared to  $\text{Co}/\text{Al}_2\text{O}_3$  decreases from 5.8% (absolute) to just 1.9%.

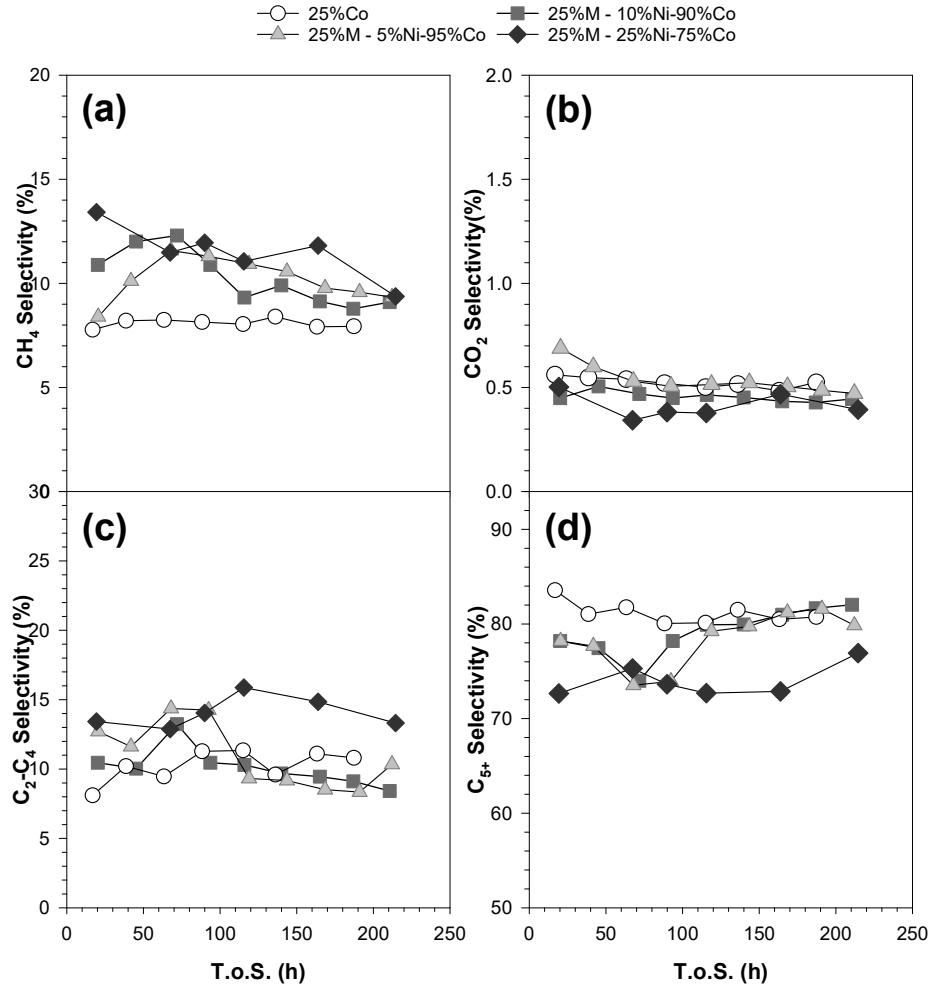
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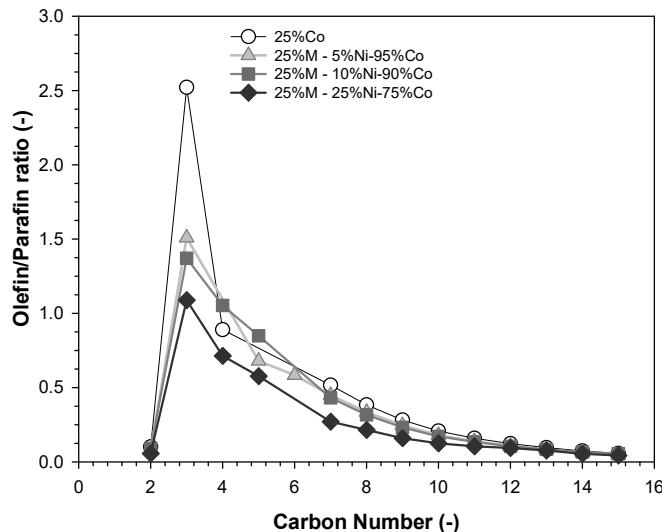


24

25    **Figure 20:** Evolution with T.o.S. of CO conversion for the prepared catalyst (process conditions:  $T =$   
 26    220,  $\text{Hz}/\text{CO} = 2$  mol/mol,  $P = 20.6$  bar,  $S.V. = 3.4$  slph per  $\text{g}_{\text{cat}}$ )

27

28  
2930 **Figure 21:** Evolution with T.o.S. of (a) CH<sub>4</sub> (b) CO<sub>2</sub> (c) C<sub>2</sub>-C<sub>4</sub> and (d) C<sub>5+</sub> selectivity for the prepared  
31 catalyst (process conditions: P= 20.6 bar, H<sub>2</sub>/CO = 2 mol/mol, T = 220°C, S.V. = 3.4 slph per g<sub>cat</sub>).32 The olefin/parafin ratio for unpromoted and nickel promoted catalysts decreases with increasing  
33 carbon number starting with ethylene species and moving upward (Figure 22). This trend is typically  
34 observed for cobalt based catalysts. However, even if the trend with the carbon number is similar  
35 among the different catalysts, the olefin content decreases by increasing the nickel content. Indeed,  
36 the olefin/parafin ratio for C<sub>3</sub> species is 2.5 for 25%Co, while it is only 1 for the 25%M- 75%Co-25%Ni.  
37 At higher carbon number the difference among the different Ni/Co loadings is not so pronounced  
38 because of the tendency of olefins to readsorb on active sites [24]. The high hydrogenation capability  
39 of nickel promoted samples is also observed by a slight decrease in chain growth probability. Indeed  
40  $\alpha_{C5-C16}$  slightly decreases from 0.85 for 25%Co to 0.83 for 25%M-25%Ni-75%Co.



41

42 **Figure 22:** Olefin/Parafin ratio at T.o.S. ~150 h (process conditions:  $P = 20.6$  bar,  $H_2/CO = 2$  mol/mol,  $T$   
43 =  $220^\circ C$ , S.V. = 3.4 slph per  $g_{cat}$ ).

44

### 45 3. Discussion

46 The promotion of nickel on cobalt-based catalyst does not significantly influence the  
47 morphological properties, as all the samples have similar surface area ( $\sim 92$   $m^2/g$ ), pore volume and  
48 pore diameter. The effect of nickel on the structural properties was investigated by XRD and STEM.  
49 XRD patterns for all the calcined catalysts showed the typical peaks associated with  $Co_3O_4$ , while no  
50 diffraction peaks associated with  $NiO$  or  $Ni^0$  were observed suggesting that a mixed metal oxide was  
51 formed. Intimate contact between cobalt and nickel was also confirmed by elemental mapping during  
52 STEM analysis, as well as by comparing TPR-XANES profiles at nickel and cobalt K-edges. Initially,  
53 nickel is associated with  $Co_3O_4$ , and then it undergoes a change in the electronic structure to a form  
54 of nickel associated with  $CoO$ . Further evidence for solid solution formation is that the  $Ni^{2+}$  associated  
55 with  $Co_3O_4$  (Ni K-edge results) and the  $Co_3O_4$  reduce over a similar temperature range, such that the  
56 temperatures at 50% conversion match very well, especially at higher Ni/Co ratios.

57 TPR-XANES and hydrogen chemisorption/ $O_2$  titration show that nickel has a beneficial effect on  
58 cobalt reducibility. The reduction of cobalt oxide is shifted to lower temperature with increasing  
59 Ni/Co ratio, and the percentage of metal reduction is increased. Voss et al. [19] have observed an  
60 improvement in the reducibility when nickel was added as the first reduction step shifts significantly  
61 to lower temperature with increasing the nickel loading. The authors proposed a hydrogen spillover  
62 from the nickel sites to cobalt oxide sites. However, the previous observed similarities in  
63 temperatures ranges between  $Co_3O_4$  to  $CoO$  and  $Ni^{2+}-Co_3O_4$  to  $Ni^{2+}-CoO$  as well as the second  
64 reduction step to the metallic phase during TPR-XANES, suggests that maybe not only  $H_2$  spillover  
65 is involved, but rather that a chemical effect exists in leading to the formation of Co-Ni alloy.

66 Cobalt-based catalysts are usually characterized by deactivation in the first few days. The  
67 possible mechanisms for this deactivation are: re-oxidation of small metallic cobalt cluster to inactive  
68  $CoO_x$ , sintering, some carbon deposition or solid-state reaction between cobalt and support [4, 25,  
69 26]. Thermodynamic calculations clearly show that when the cobalt crystallites have a diameter  
70 lower than 4.4 nm, they may be re-oxidized in the steam/hydrogen environments of FTS [7, 8]. This  
71 initial decline and leveling off period for CO conversion typical of cobalt-based catalysts was not  
72 observed for the nickel promoted systems. Rytter et al. [18] have also observed an activation period  
73 in the first 40 h. They proposed a catalyst reconstruction in the first stage of operation where nickel  
74 and cobalt partially segregate, thereby exposing the cobalt clusters to FTS reaction. However,

75 additional investigations are needed to speculate the events occurring during this induction time.  
 76 Interestingly, the performances of nickel promoted catalysts are stable, despite having lower cobalt  
 77 loading than 25%Co/Al<sub>2</sub>O<sub>3</sub>. This suggests that nickel can stabilize cobalt metal nanoparticles. Rytter  
 78 et al. [18] further proposed that the higher stability for Co-Ni alloys could be due to the suppression  
 79 of the carbon deposition and by suppressing re-oxidation phenomena via H<sub>2</sub> spillover.

80 Addition of nickel has changed the product distribution. In particular, the initial methane  
 81 selectivity increases by increasing the nickel loading, whereas the initial C<sub>5+</sub> selectivity decreases.  
 82 Higher CH<sub>4</sub> selectivities were also observed in previous works, where different Ni/Co ratios were  
 83 studied [10, 16, 18]. Interestingly, the selectivities of Co/Ni catalysts improve with time on-stream to  
 84 nearly match those of pure Co catalysts. Furthermore, the olefin content decreases as well as the  
 85 chain growth probability by increasing the Ni/Co ratio. These results are not surprising because of  
 86 the high hydrogenation capability of nickel. Furthermore, Ishihara et al. [12] studying Co-Ni alloys  
 87 supported on SiO<sub>2</sub> found that cobalt electronically interacts with nickel in the outer shell orbitals by  
 88 creating adsorption sites having a new electron density. These new sites have the highest H  
 89 adsorption strengths. Thus, hydrogen competes more effectively in the adsorption sites in co-  
 90 adsorption of CO and H<sub>2</sub> for Co-Ni alloy relative to pure cobalt based catalyst.

91 Finally, it is interesting to compare the activity/\$ (Table 4) as nickel and cobalt have different  
 92 market prices. The price of cobalt is reported to be 2.13 times the price of nickel. Thus, the partial  
 93 substitution of cobalt with nickel would be an advantage in terms of total catalyst cost. At steady state  
 94 conditions the activity/\$ for the 25%M-25%Ni-75%Co is best among the nickel promoted and  
 95 unpromoted catalyst; also, at that point, the selectivities nearly match those of the pure Co based  
 96 catalysts.

97

98 **Table 4:** Activity/\$ at steady-state condition for the tested catalyst.

Sample ID	Activity/\$
25%Co	39.5
25%M – 5%Ni-95%Co	35.4
25%M – 10%Ni-90%Co	36.8
25%M – 25%Ni-75%Co	41.9

99

## 100 4. Materials and Methods

### 101 4.1 Catalyst preparation

102 The conventional slurry impregnation method was used to prepare the catalyst containing 25%  
 103 metal by weight, with the following Ni/Co atomic ratios: 0/100, 5/95, 10/90, 25/75 and 50/50. The  
 104 support was Catalox 150  $\gamma$ -alumina with a surface area of 150 m<sup>2</sup>/g. Nickel nitrate and cobalt nitrate  
 105 (Alfa Aesar) served as the precursors to load the nickel and cobalt together (i.e., in a single solution)  
 106 onto the  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> support. In this method, the ratio of the weight of alumina to the volume of solution  
 107 used was 1:1 as reported in a Sasol patent [1], such that loading solution prepared was  
 108 approximately 2.5 times the pore volume.. The total metal loading was added by two impregnation  
 109 steps with 12.5 % of metal by weight for each step. Between each step, the catalyst was dried at 60 °C  
 110 under vacuum in a rotary evaporator, then the temperature was slowly increased until 100 °C. After  
 111 the second impregnation, the catalyst was dried and then calcined in flowing air for 4 h at 350 °C.

### 112 4.2 Characterization

113 A Micromeritics 3-Flex system (Norcross, GA, USA) using N<sub>2</sub> (UHP N<sub>2</sub>, Airgas, Lexington, KY)  
 114 for physisorption was used to measure BET surface area and porosity properties. Before testing, the  
 115 samples were pre-treated at 160 °C and 50 mTorr for at least 12 h. The BJH method was employed to  
 116 calculate the average pore volume and pore diameter.

117 XRD spectra were collected with a Philips X'Pert diffractometer with monochromatic Cu K $\alpha$   
 118 radiation ( $\lambda=1.54\text{\AA}$ ). The conditions employed included a scan rate of 0.01° per step, 2 $\theta$  range of 10-  
 119 90, and a scan time of 4 s per step.

120 Prior to STEM characterization, the samples were pre-treated in hydrogen (American Welding  
 121 & Gas, Lexington, KY, USA) at 350°C for 18 h, cooled down to room temperature and then passivated  
 122 with a mixture of 1%O<sub>2</sub> in nitrogen (American Welding & Gas, Lexington, KY, USA). STEM analysis  
 123 was performed with an FEI Talos F200X instrument (Thermo Scientific, Waltham, MA, U.S.A.)  
 124 equipped with BF, DF2, DF4 and HAADF detectors. The imaging was collected with a field emission  
 125 gun using an accelerating voltage of 200 kV and a high speed Ceta 16M camera, while Velox  
 126 software(Thermo Scientific, Waltham, MA, U.S.A.) was used for data processing. The samples were  
 127 dispersed in ethanol (Alfa Aesar, Haverhill, MA, U.S.A.), sonicated, and then drop onto a carbon-  
 128 coated copper grid and dried in air.

129 Hydrogen chemisorption and the following pulse re-oxidation was carried out using an  
 130 Altamira AMI-300 unit (Altamira Instruments, Pittsburgh, PA, USA). The sample was reduced at  
 131 350°C (ramping rate at 2°C/min) for 10 h in 10 cm<sup>3</sup>/min of UHP H<sub>2</sub> (Airgas, San Antonio, TX, USA)  
 132 blended with 20 cm<sup>3</sup>/min of UHP argon (Airgas, San Antonio, TX, USA). Then, the temperature was  
 133 cooled to 100°C, and UHP argon (30 cm<sup>3</sup>/min) was flowed through the catalytic bed to avoid the  
 134 adsorption of weakly bound hydrogen. Next, the temperature was increased to 350°C at 10°C/min in  
 135 flowing argon to desorb the chemisorbed hydrogen. The hydrogen peak obtained during the  
 136 temperature programmed desorption was integrated and the moles of hydrogen evolved was  
 137 determined by comparing to calibration pulses. Pulses of UHP O<sub>2</sub> (Airgas, San Antonio, TX, USA)  
 138 were then passed through the reactor to re-oxidize the catalyst until saturation was achieved. The  
 139 percentage of reduction was estimated with two different methods. In the first approach, nickel and  
 140 cobalt metal were assumed to oxidize to NiO and Co<sub>3</sub>O<sub>4</sub>, respectively. However, in a second  
 141 approach, we assumed all Co<sub>3</sub>O<sub>4</sub> converted at least to CoO during the reduction, and that a fraction  
 142 of NiO and CoO converted to Ni<sup>0</sup> and Co<sup>0</sup>. Thus, during re-oxidation step, the Ni<sup>0</sup> and Co<sup>0</sup> is first  
 143 oxidized to NiO and CoO. Then, all CoO oxidizes to Co<sub>3</sub>O<sub>4</sub>. These two approaches set minimum and  
 144 maximum limits for the cobalt cluster size when the uncorrected dispersion is modified by  
 145 considering the percentage of reduction by the metal, as follows:

146

147 % Dispersion (Uncorrected) = (# metal atoms on the surface)/(# metal atoms in the sample)

148 % Disp. (Corrected) = (# metal atoms on the surface)/[(# metal atoms in the sample)(% reduction)]

149

#### 150 4.3 H<sub>2</sub>-TPR XANES-EXAFS

151

152 In-situ H<sub>2</sub>-TPR XAFS experiments were carried out at the Materials Research Collaborative  
 153 Access Team (MR-CAT) beamline at the Advanced Photon Source, Argonne National Laboratory. A  
 154 cryogenically cooled Si (1 1 1) monochromator selected the incident energy and a rhodium-coated  
 155 mirror rejected higher order harmonics of the fundamental beam energy. The experiment setup was  
 156 analogous to that outlined by Jacoby [27]. The in-situ TPR of 6 catalysts were performed in stainless-  
 157 steel multi-sample holder (3.0 mm i.d. channels) Approximately 6 mg of each catalyst was loaded as  
 158 a self-supporting wafer in each channel. The catalyst was diluted with alumina in a weight ratio of  
 159 approximately 1:1. The holder was located in the center of a quartz tube, equipped with Kapton  
 160 windows, thermocouple and gas ports and. The amount of catalyst loaded was optimized for the  
 161 Co and Ni K edges, considering the absorption by aluminum of the Al<sub>2</sub>O<sub>3</sub>. The quartz tube was  
 162 positioned in a clamshell furnace mounted on the positioning table. Each sample cell was placed  
 163 relative to the beam and the position of the table was adjusted to an accuracy of 20 μm (for repeated  
 164 scans). Once the catalyst positions were fine-tuned, the reactor was purged with He ( 100 ml/min)  
 165 for more than 5 min and then the reactant gas (a mixture H<sub>2</sub>/He, 3.5%) was flowed through the  
 166 samples (100 ml/min). The temperature was increased to 700°C (ramp of ~1.0 °C/min) and then held  
 167 for 4 h. The Ni and Co K-edge spectra were collected in transmission mode. The Co metallic foil  
 168 spectrum was also recorded simultaneously for energy calibration. X-ray absorption spectra for each  
 169 catalyst were collected from 7500 to 9000 eV.

170

171 The WinXAS program was used to analyze the spectra collected during H<sub>2</sub>-TPR  
 EXAFS/XANES experiments [28]. Additional details of the EXAFS and XANES analyses for Co K-

172 edge data are reported in our previous work [29]. Ni K-edge data were processed in a similar manner  
 173 (i.e., same  $\Delta k$  and  $\Delta R$  in fittings). For qualitative comparisons of EXAFS and XANES results, the  
 174 references used for  $\text{Co}^0$ ,  $\text{CoO}$ , and  $\text{Co}_3\text{O}_4$  were the final spectrum, the point of maximum  $\text{CoO}$   
 175 content, and the initial spectrum of the TPR trajectory of undopped cobalt catalyst (25% $\text{Co}/\text{Al}_2\text{O}_3$ ).  
 176 For  $\text{Ni}^0$  and  $\text{NiO}$ , the references were  $\text{NiO}$  (Alfa Aesar, Puratronic, 99.998%, Tewksbury, MA, USA)  
 177 and a  $\text{Ni}^0$  foil.

178 For XANES analyses, linear combination fittings were carried out considering as reference  
 179 compounds for Co K-edge data the initial spectrum (a mixture of  $\text{Co}^{3+}$  and  $\text{Co}^{2+}$  similar to  $\text{Co}_3\text{O}_4$ ), the  
 180 point of maximum  $\text{CoO}$  content, and the final spectrum after  $\text{H}_2$  TPR (representing  $\text{Co}^0$ ). At the Ni  
 181 K-edge, the reference compounds were the first spectrum ( $\text{Co}_3\text{O}_4$  associated with  $\text{Ni}^{2+}$ ), the spectrum  
 182 with highest  $\text{CoO}$  content associated with  $\text{Ni}^{2+}$ , and the final spectrum after  $\text{H}_2$  TPR (representing  
 183  $\sim 100\%$   $\text{Ni}^0$ ). The data reduction and fitting for EXAFS were performed using the catalysts in their  
 184 final state following TPR and cooling in flowing  $\text{H}_2$  using the WinXAS [28], Atoms [30], FEFFIT [31],  
 185 and FEFF [31] programs. The  $k$ -range chosen for the fittings was 3-10  $\text{\AA}^{-1}$ . Fitting was confined to the  
 186 first metallic coordination shell by applying a Hanning window in the Fourier transform magnitude  
 187 spectra, and carrying out the back-transform to isolate that shell.

188  
 189 *4.4 Reaction testing*  
 190

191 Activity tests were performed in a 1 L continuously stirred tank reactor (CSTR) (PPI,  
 192 Warminster, PA, USA). Additional information on the lab scale rig can be found elsewhere [32]. In a  
 193 typical test, 9.6 g of catalyst ( $63 < dp < 125 \mu\text{m}$ ) was loaded into a fixed bed reactor. The catalyst was  
 194 reduced at 350°C for 20 h, feeding 30 Ni/h  $\text{H}_2/\text{He}$  mixture (1:3 v/v, American Welding & Gas,  
 195 Lexington, KY, USA) at atmospheric pressure. The reduced catalyst was transferred by pneumatic  
 196 transfer under the protection of inert gas to a CSTR containing 310 g of melted Polywax 3000 (Baker  
 197 Petrolite, Houston, TX, USA). In situ reduction for the transferred catalyst was performed at  
 198 atmospheric pressure and 230°C overnight feeding 30 Ni/h pure  $\text{H}_2$  (American Welding & Gas,  
 199 Lexington, KY, USA). In this work, the catalytic testing was carried out at the following process  
 200 conditions;  $P = 20.2$  bar,  $T = 220^\circ\text{C}$ , a stirring speed of 750 rpm and  $\text{H}_2/\text{CO} = 2$  mol/mol. The  
 201 unconverted reactants and the products leaving the CSTR were sent to a warm trap, in which the  
 202 temperature was set at 100 °C, and then to a cold trap maintained at 0 °C. The uncondensed stream  
 203 was reduced to atmospheric pressure, while the flowrate and the composition were measured by a  
 204 wet test meter and by an online 3000A micro-GC (Agilent, Santa Clara, CA, USA), respectively. The  
 205 micro-GC is equipped with four different columns (Plot U, Molecular Sieve, OV-1 and, Alumina )  
 206 and TCD. The reaction products were collected in three traps maintained at different temperatures:  
 207 a hot trap (200 °C), a warm trap (100 °C), and a cold trap (0 °C). The products were separated into  
 208 different fractions (wax, oil, and aqueous) for quantification. The oil ( $\text{C}_4\text{-C}_{20}$ ) fraction was analyzed  
 209 with a 7890 GC (Agilent, Santa Clara, CA, USA) equipped with DB-5 (60 m x 0.32 mm x 0.25 $\mu\text{m}$ ,  
 210 Agilent J&W) column and FID, while waxes ( $\text{C}_{21}\text{-C}_{60}$ ) were analyzed with an HP 6890 GC equipped  
 211 with ZB-1HT column (30 m x 0.25 mm x 0.10  $\mu\text{m}$ , Zebron) and FID.

212 **5. Conclusions**

213 Bimetallic catalysts with different Ni/Co ratios were prepared by standard aqueous incipient  
 214 impregnation.  $\text{N}_2$  adsorption/desorption results show that the addition of nickel has no effect on the  
 215 morphological properties as similar surface area, pore volume and pore diameter are obtained  
 216 independently from the Ni/Co ratio. XRD patterns of the samples have the peaks associated with  
 217  $\text{Co}_3\text{O}_4$ , whereas no diffraction peaks associated with Ni were observed. Thus, this suggests a Co-Ni  
 218 solid oxide solution might be formed. STEM and TPR-XANES show the nickel and cobalt are in  
 219 intimate contact, strongly suggesting the formation of a Co-Ni alloy. Moreover, TPR-XANES results  
 220 indicate that nickel promotion improves the cobalt reducibility by systematically shifting the  
 221 reduction profiles to lower temperatures. The similarities in temperature ranges between  $\text{Co}_3\text{O}_4$  to  
 222  $\text{CoO}$  and  $\text{Ni}^{2+}\text{-Co}_3\text{O}_4$  to  $\text{Ni}^{2+}\text{-CoO}$ , as well as the second reduction step to the metallic phase during

223 TPR-XANES, suggests that not only H<sub>2</sub> spillover is involved, but that a chemical effect is likely. This  
 224 is due to intimate contact in the solid solution that leads to the formation of the Co-Ni alloy.

225 The catalyst performance during FTS, in terms of conversion, selectivity and stability, were  
 226 evaluated using a CSTR. Nickel promoted catalysts have lower initial CO conversion, which  
 227 progressively increases with T.o.S. until a steady-state value is achieved. This CO conversion trend is  
 228 inverted as compared to the typical induction period observed for Co/Al<sub>2</sub>O<sub>3</sub>, where the activity  
 229 progressively declines and levels off because of deactivation phenomena. The stability of the Co-Ni  
 230 alloy may be due to the stabilization of metallic cobalt nanoparticles by nickel addition, resulting in  
 231 robust nanoparticles even at lower cobalt content compared to commercial Co loadings. CH<sub>4</sub>  
 232 selectivity increases by increasing nickel loading because of the higher hydrogenation capability of  
 233 the Co-Ni alloy. However, the difference in CH<sub>4</sub> selectivity between the Ni-promoted and  
 234 unpromoted catalyst (in terms of the absolute value) decreases with T.o.S., which is beneficial; in fact,  
 235 after stabilization, the C5+ selectivities were quite similar between catalysts prepared with Co-Ni  
 236 versus Co alone. Finally, the steady-state activity/\$ for Ni/Co ratio of 25/75 is slightly higher than  
 237 25%Co/Al<sub>2</sub>O<sub>3</sub>.

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