



Chemical Aging of Rubber: Constitutive Modeling Using Molecular Dynamics

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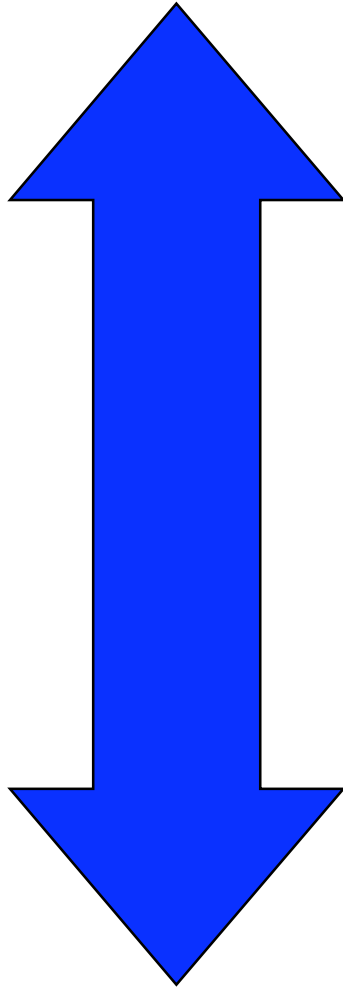


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Collaborators

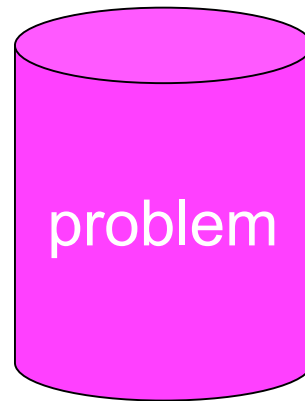
FE calculations



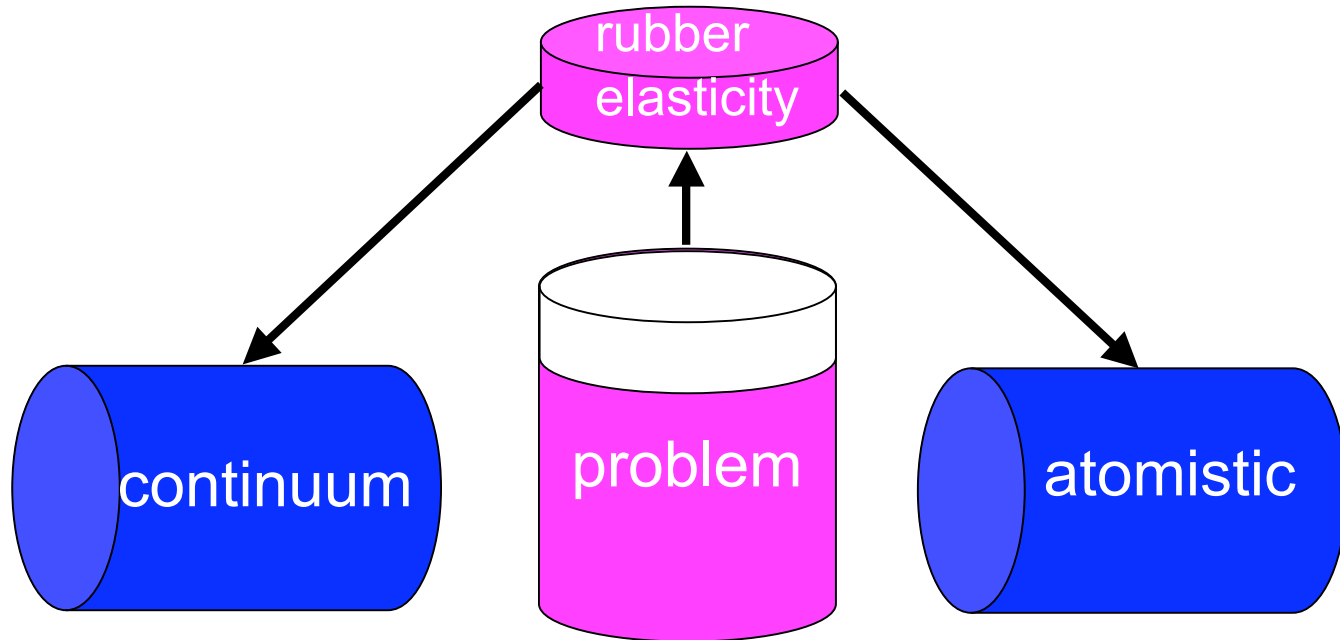
- David Lo
(1523, Materials Mechanics)
- Joanne Budzien
(1814, Computational Materials Science and Engineering)
- John Curro
(1815, Ceramic Processing and Inorganic Materials)
- Dana Rottach
(UNM, Department of Chemical and Nuclear Engineering)
- Gary Grest
(1114, Surface and Interface Sciences)
- Aidan Thompson
(1435, Multiscale Computational Materials Methods)

MD simulations

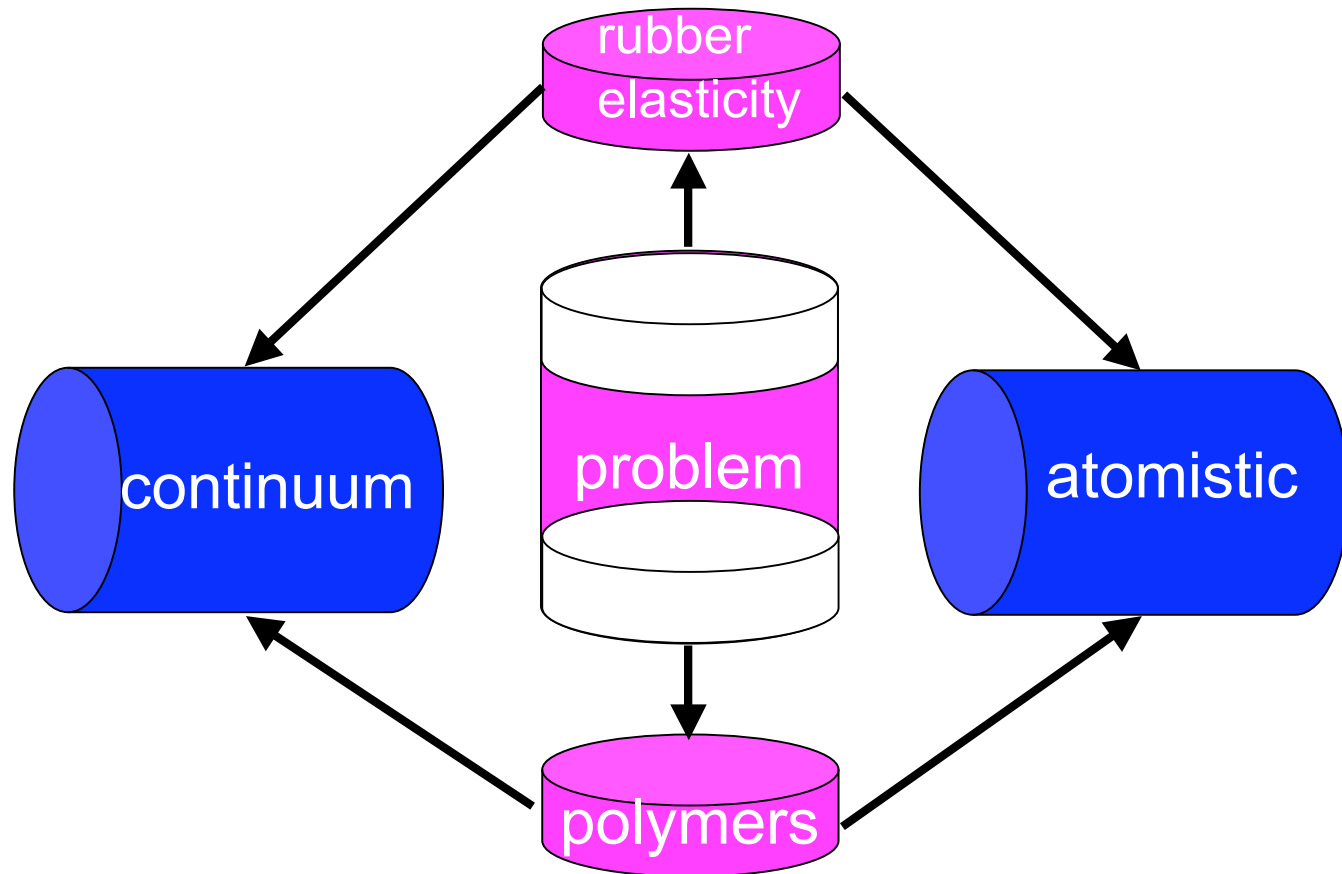
Map



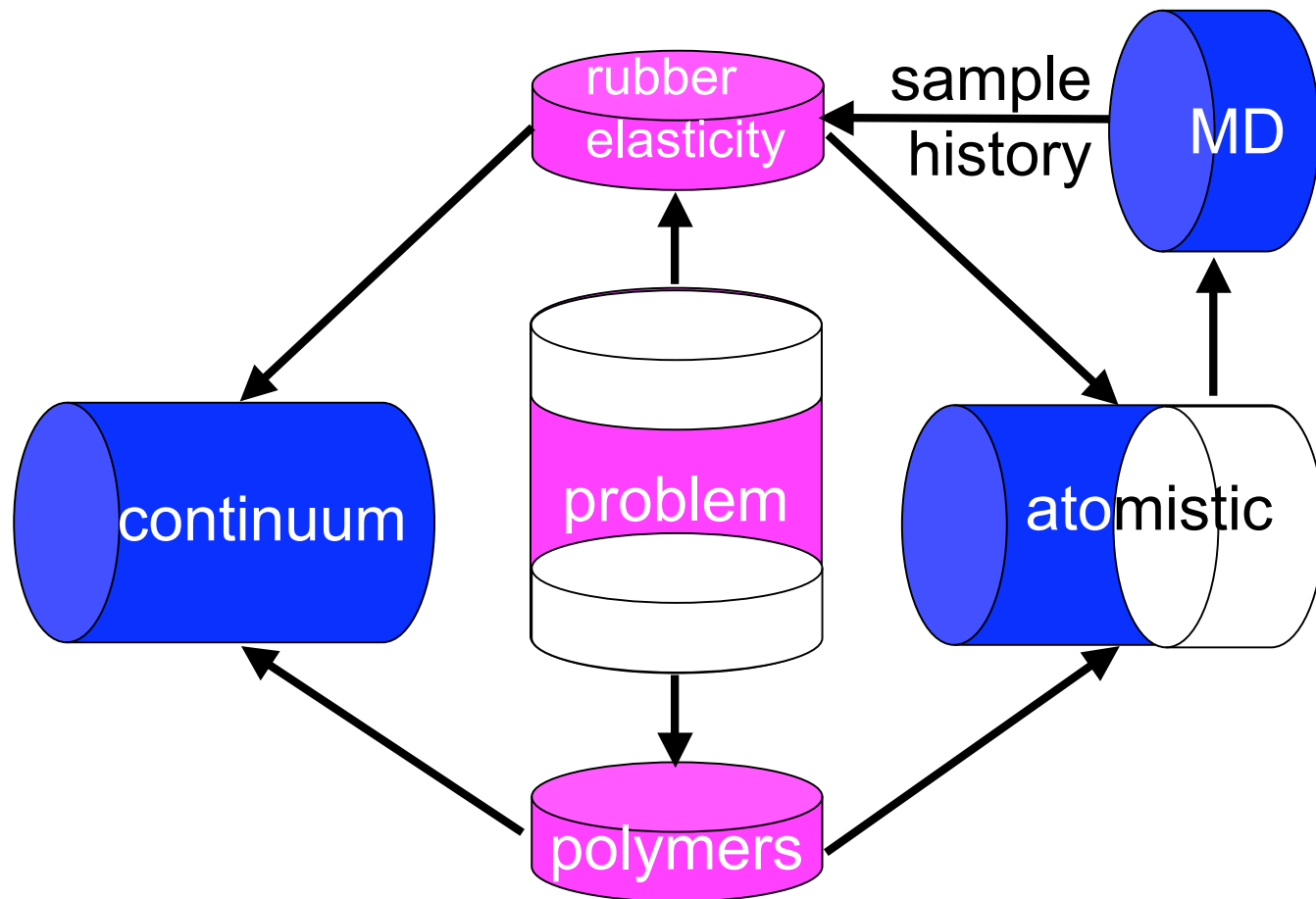
Map



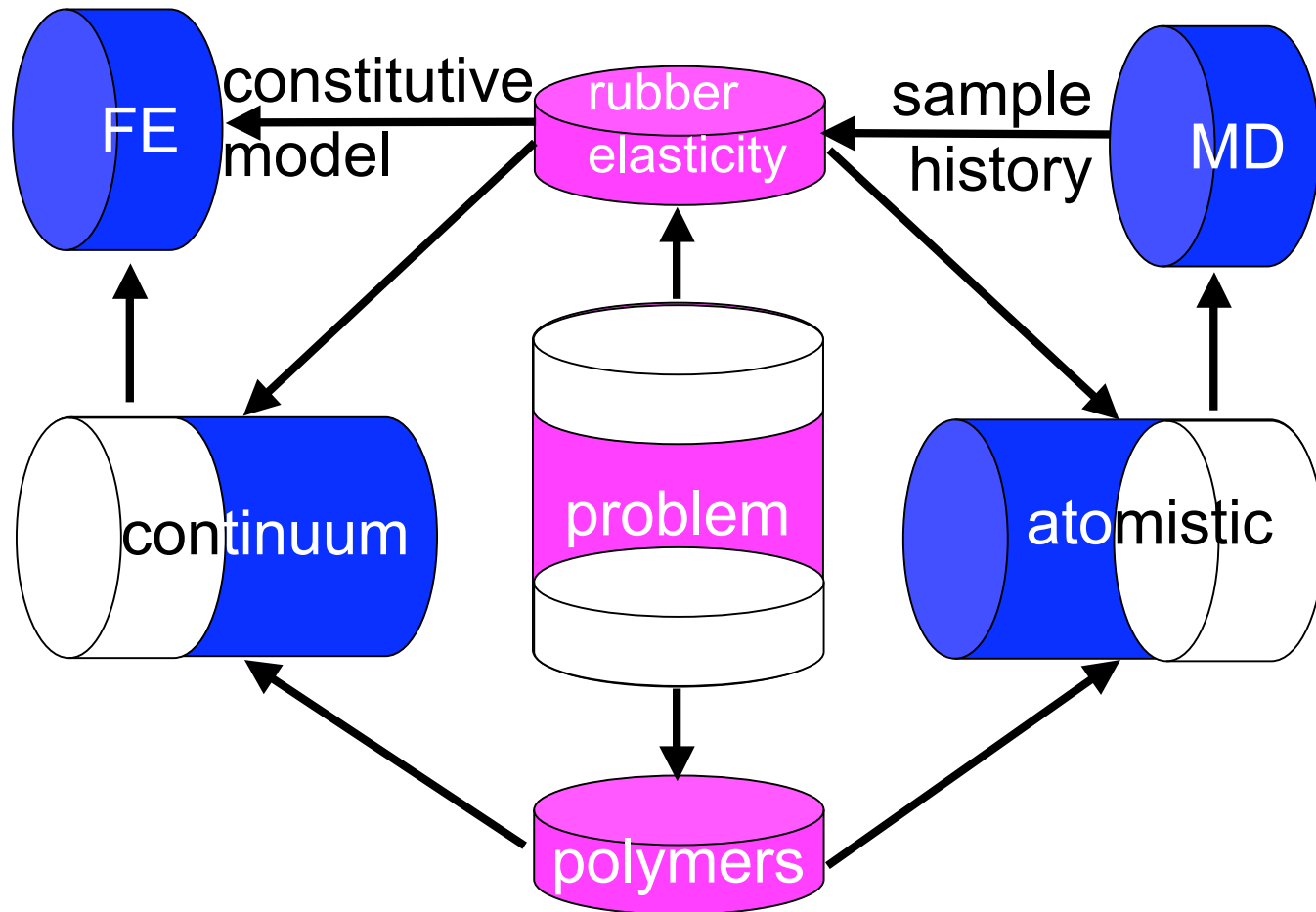
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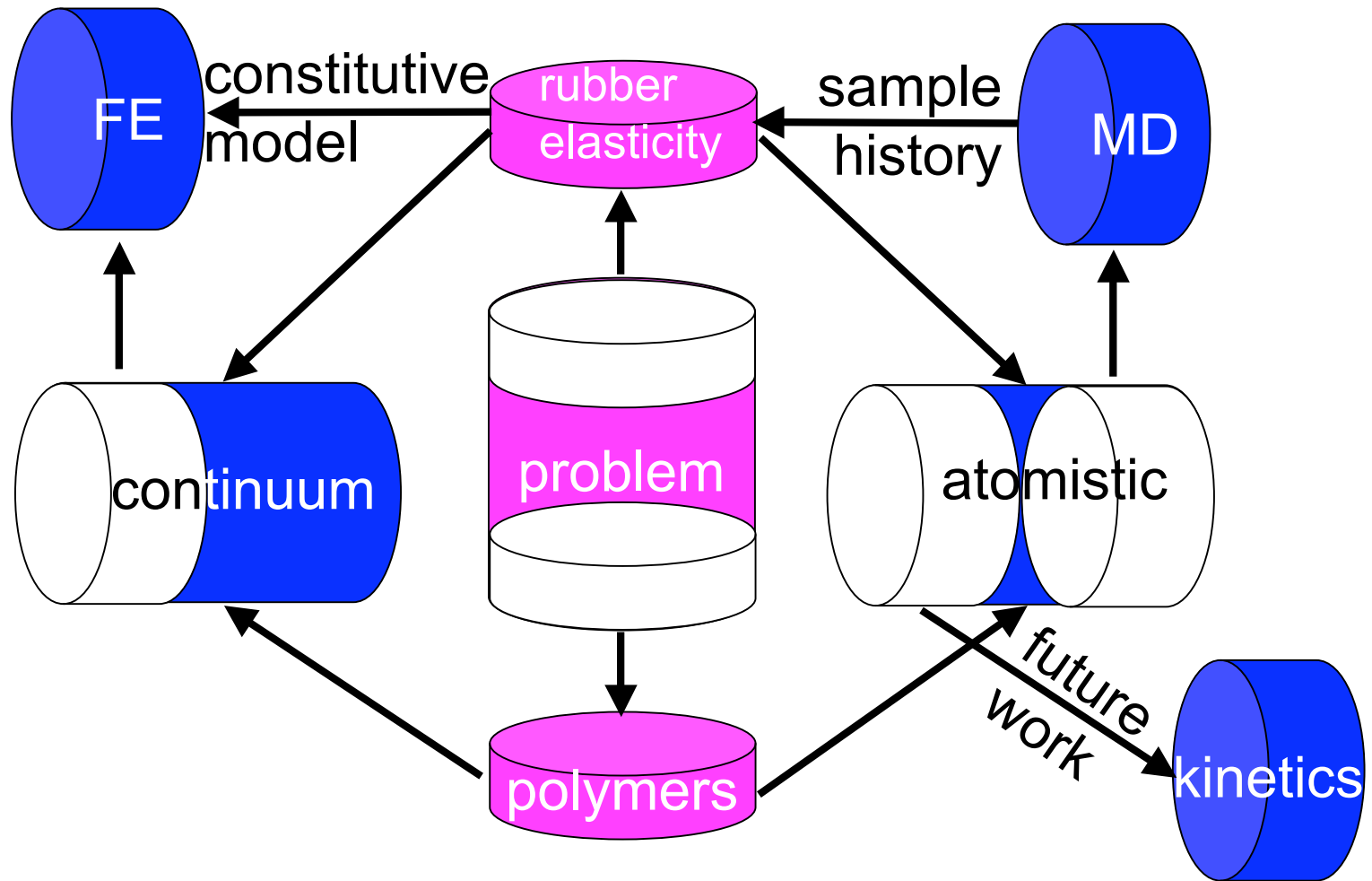
Map



Map



Map



Motivation

rubber

+

compression

time

permanent set

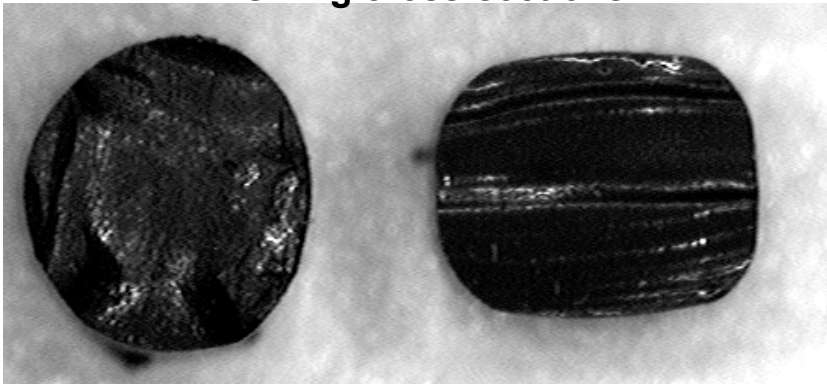
loss of sealing force

o-ring fails

best case:
damaged electronics

worst case:
Challenger blows up

O-ring cross-sections

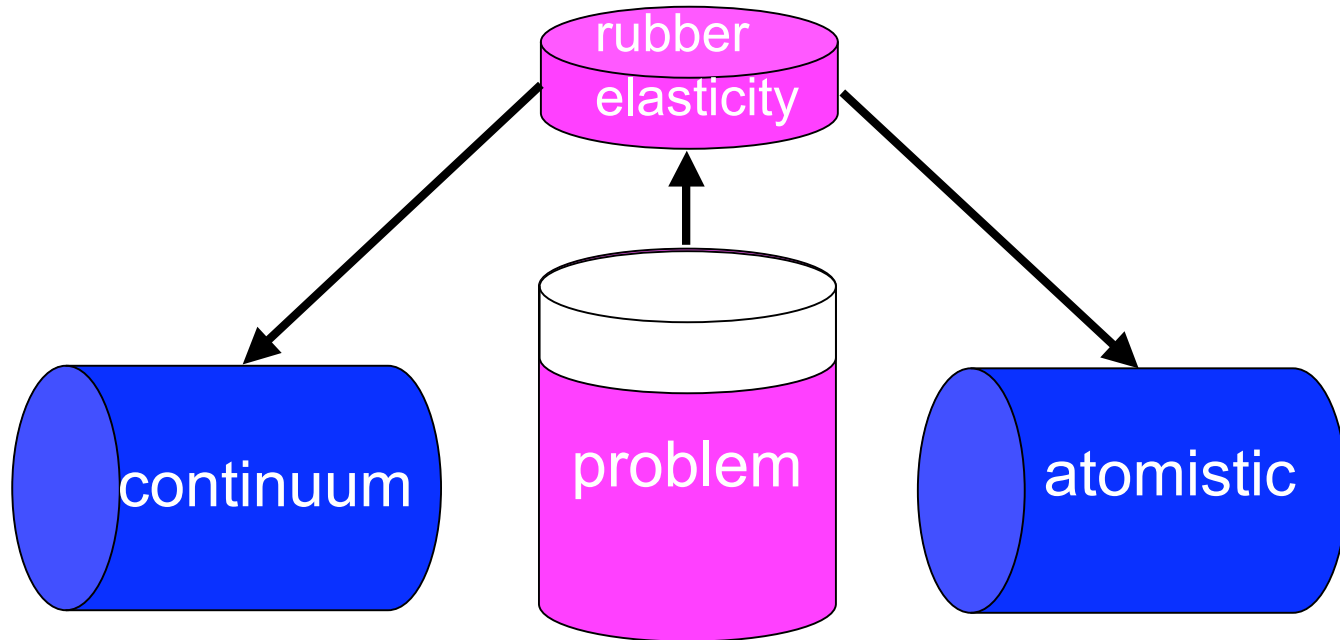


unaged

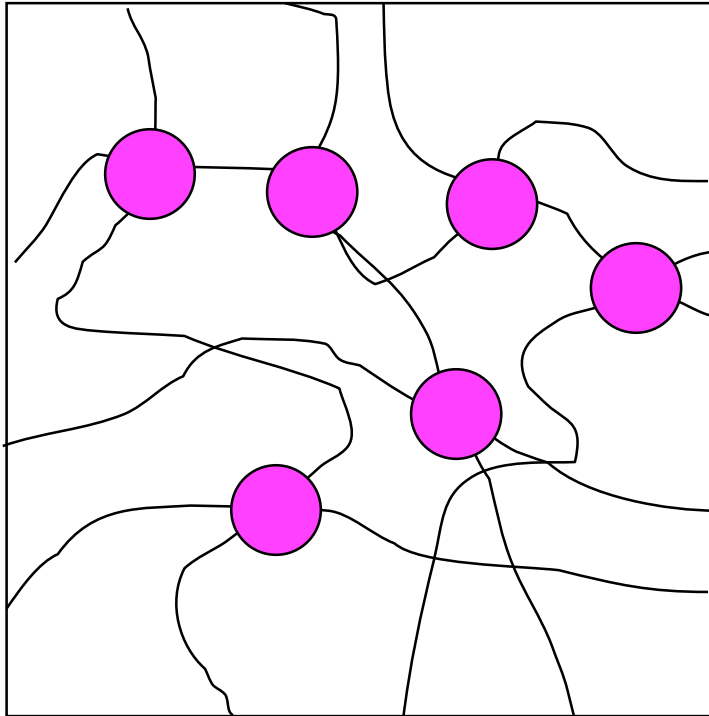
aged 15 years

KT Gillen

Map

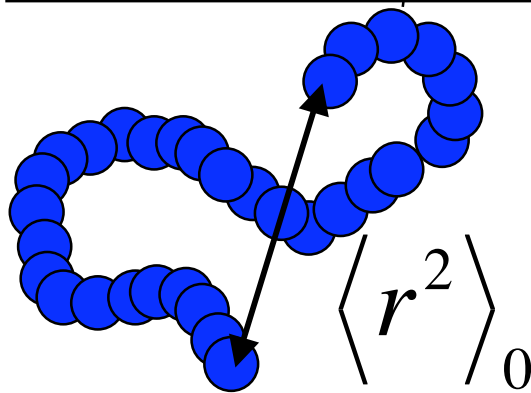


Rubber Elasticity (Atomistic)

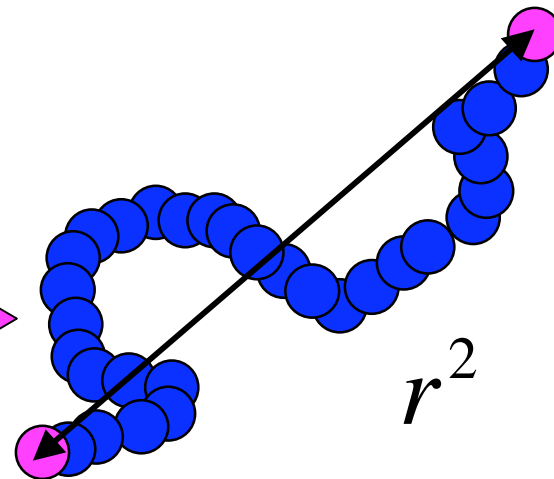


Networks carry stress

$$\frac{F^{el}}{k_B T} = \frac{3}{2} \sum_{chains} \left[\frac{r_t^2}{\langle r_t^2 \rangle_0} - 1 \right]$$



crosslinking



Changes in the average chain dimensions affect the stress

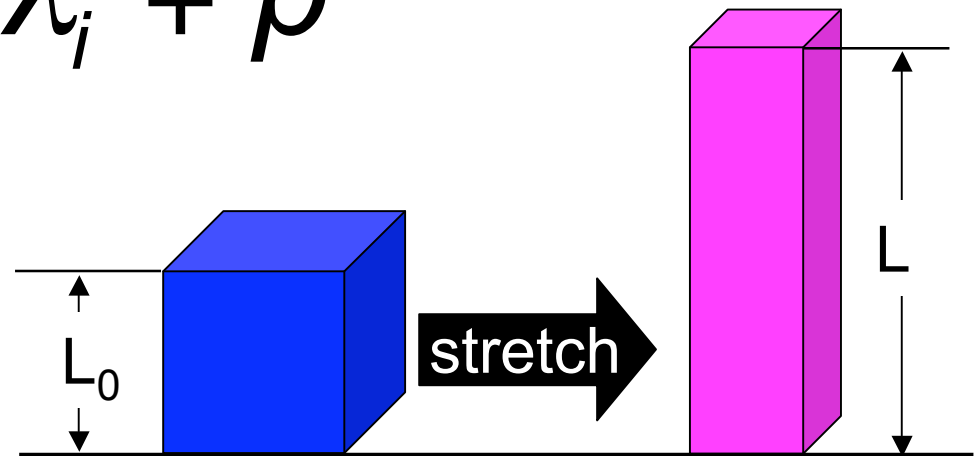
Rubber Elasticity (Continuum)

G = material-specific modulus

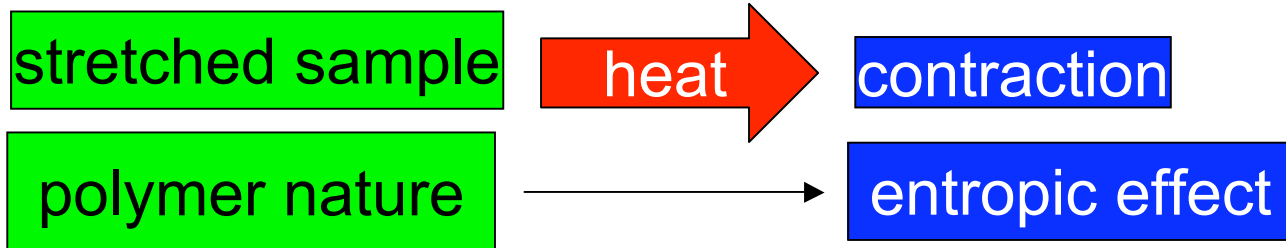
p ~ hydrostatic pressure

$$\sigma_i = G\lambda_i^2 + p$$

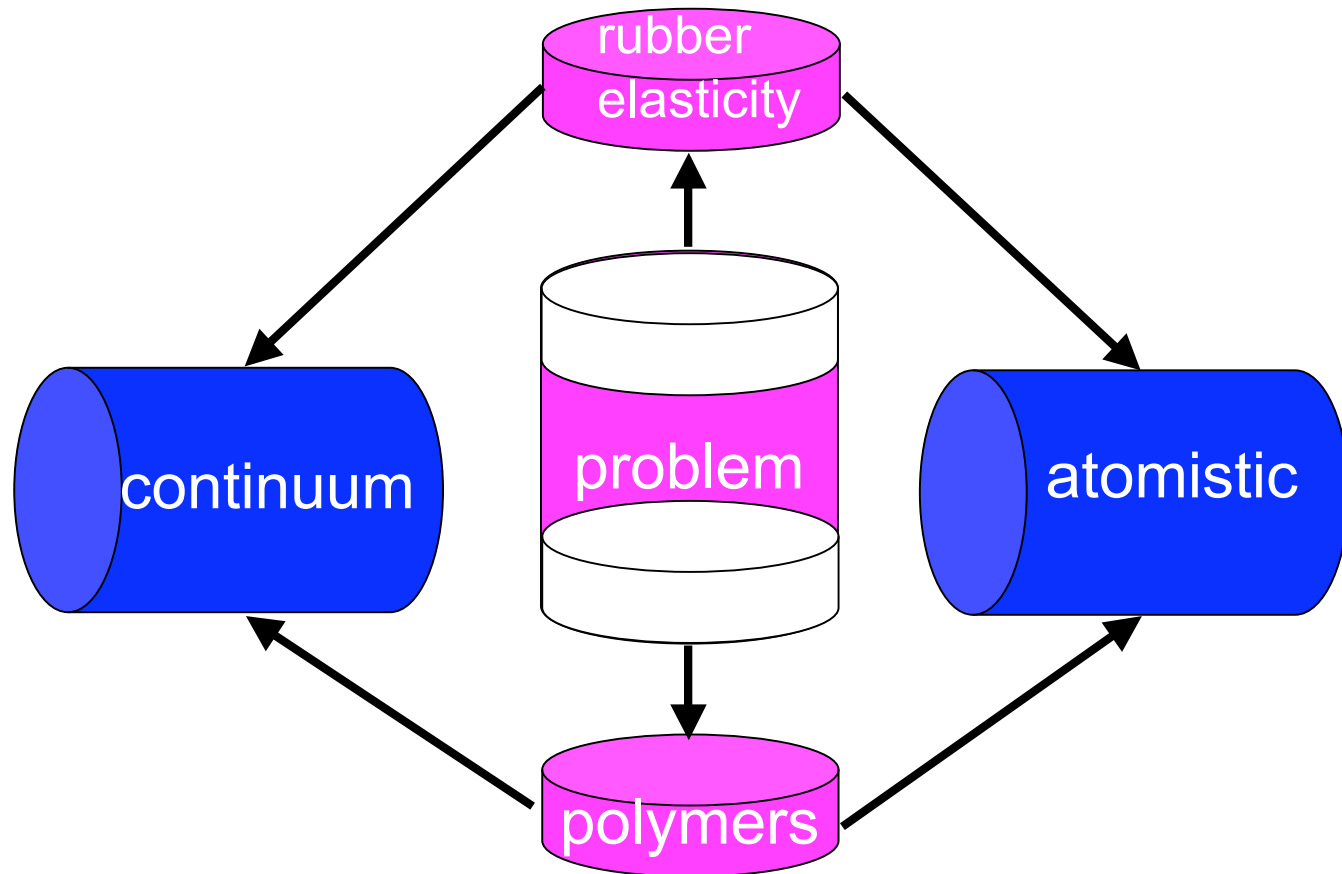
$$\lambda_i = \frac{L_i}{L_{0i}}$$



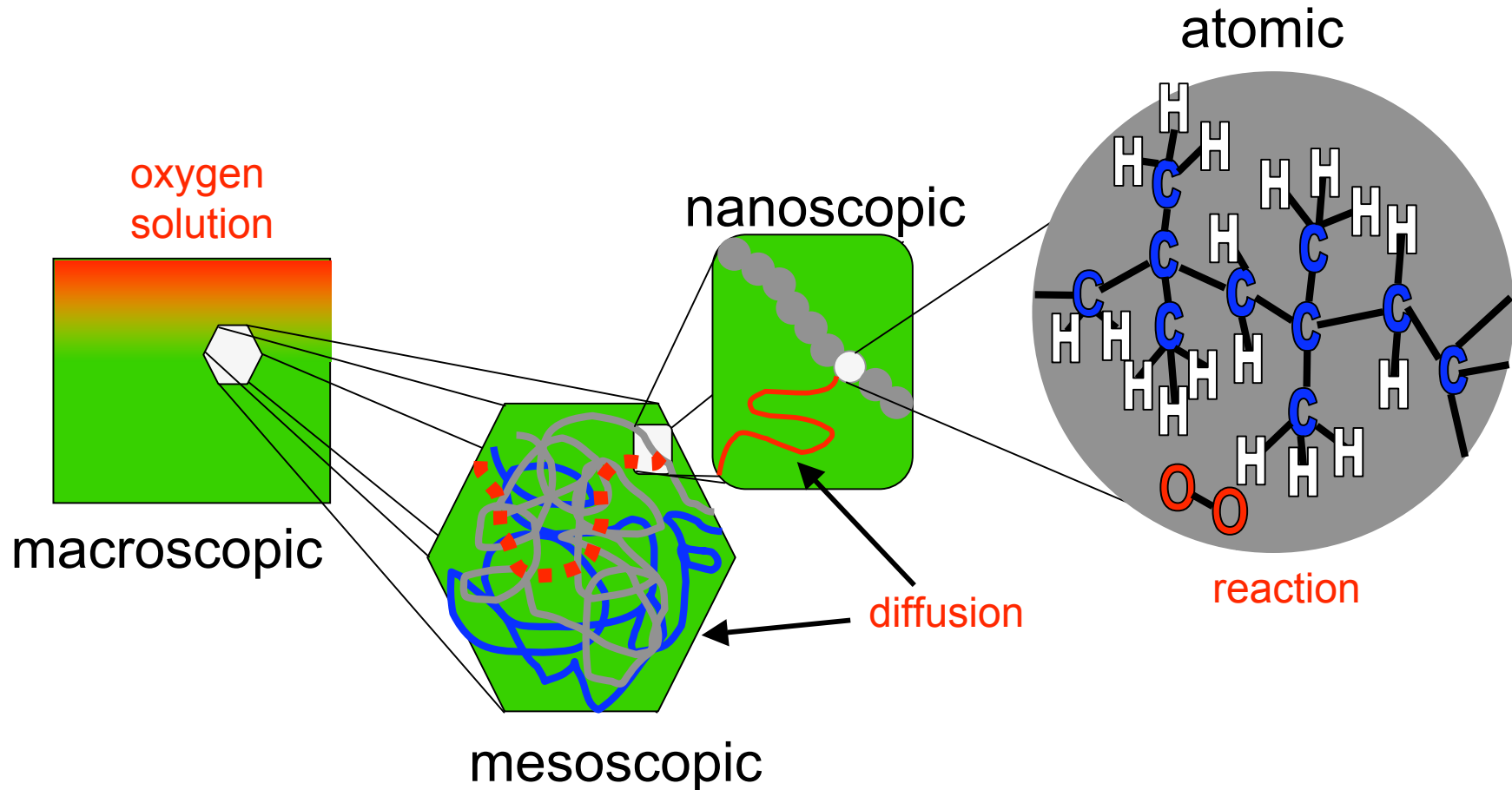
Changes in sample dimensions affect the stress



Map



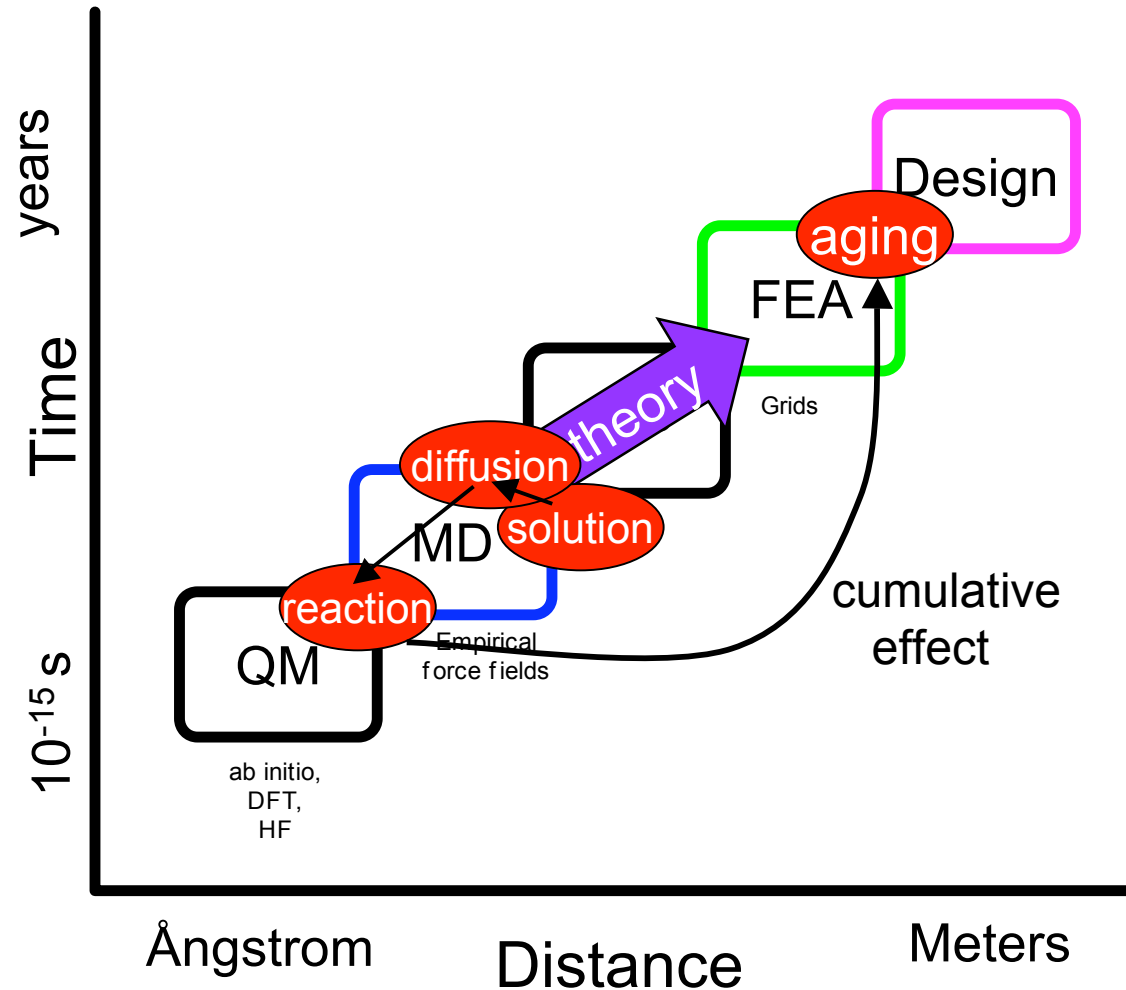
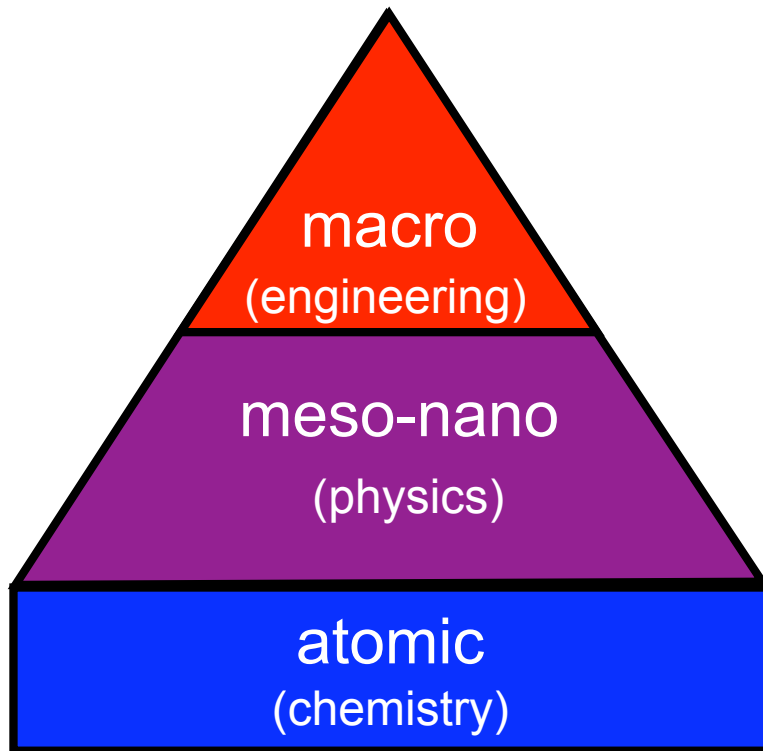
Goal: Predict Material Properties for Engineering Applications



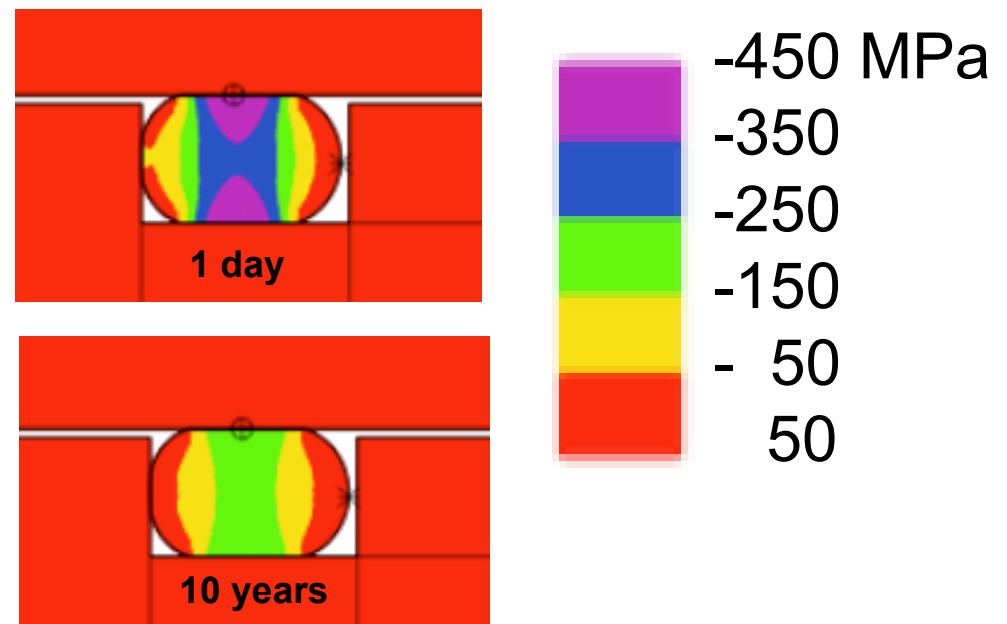
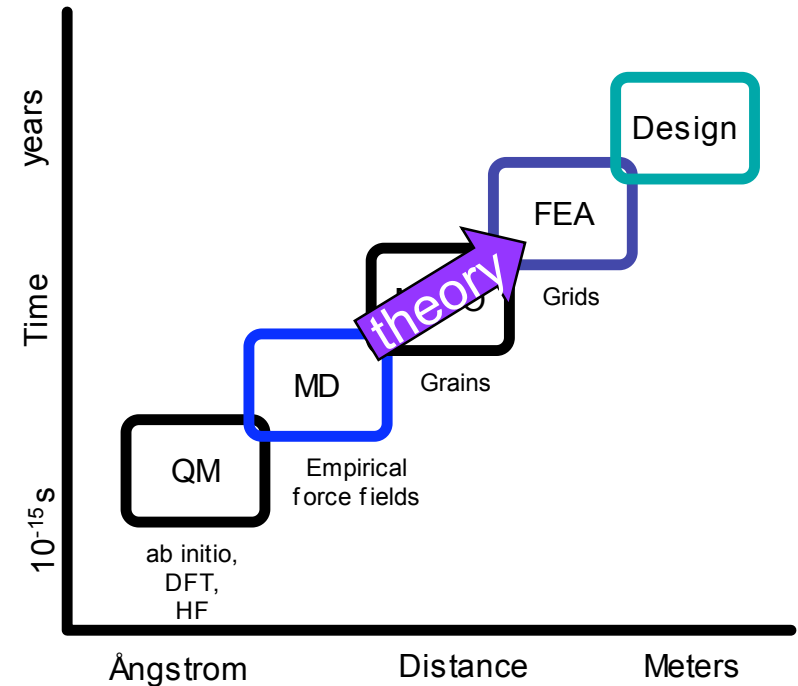
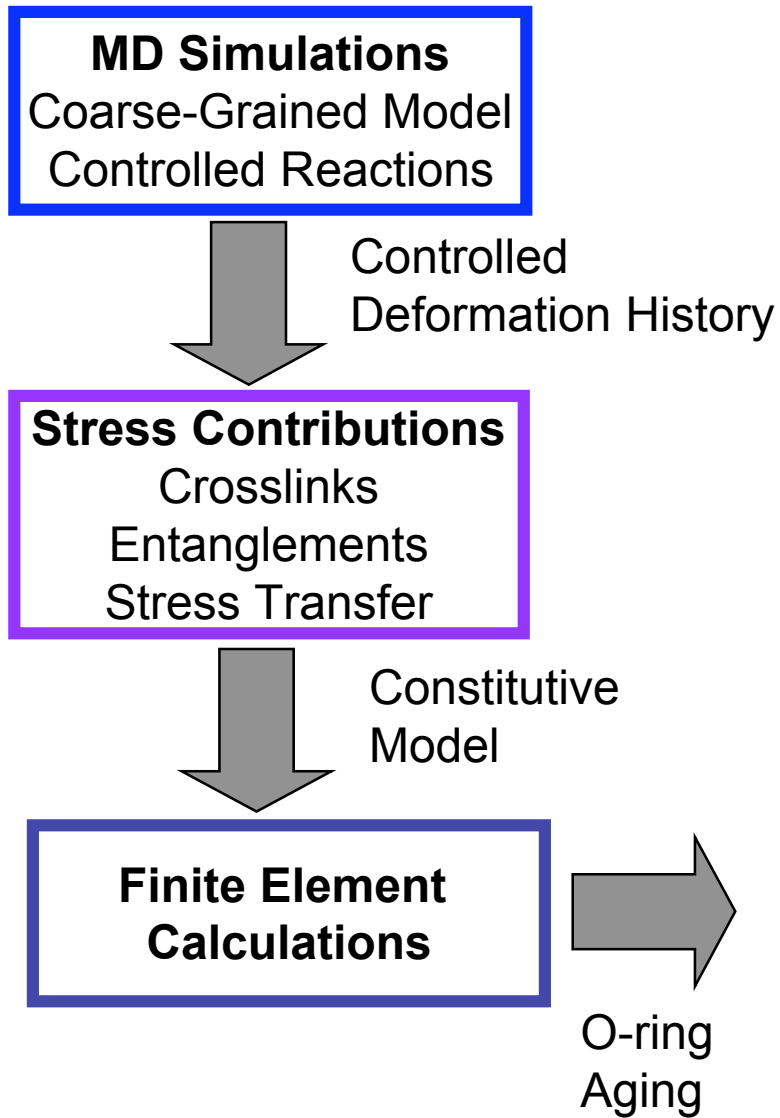
Good predictions at the macroscopic level require knowledge of chemistry and physics at smaller levels!

Problem: Processes of Interest Span Multiple Scales

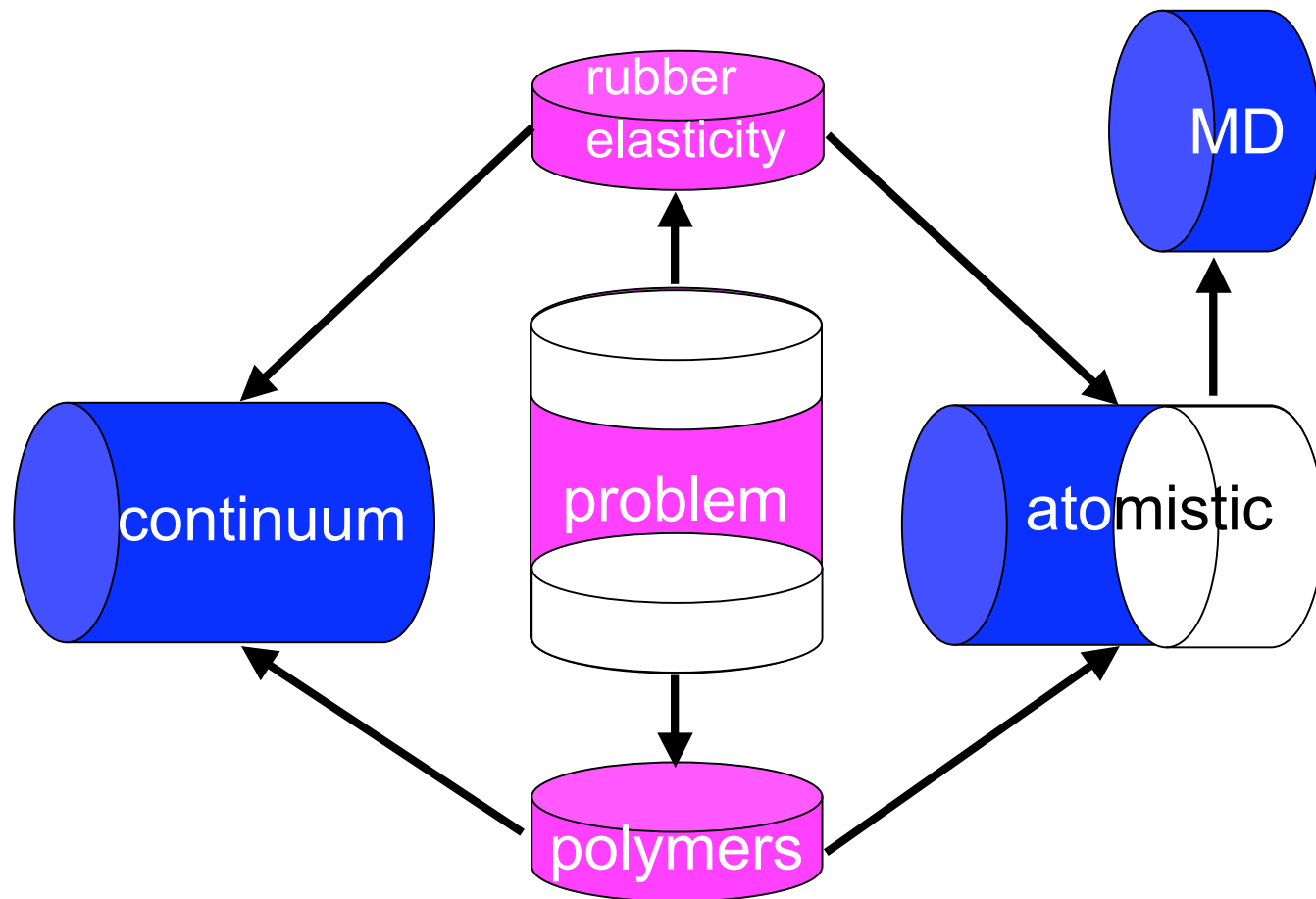
Hierarchical Approach



Strategy



Map



Coarse-grained polymers

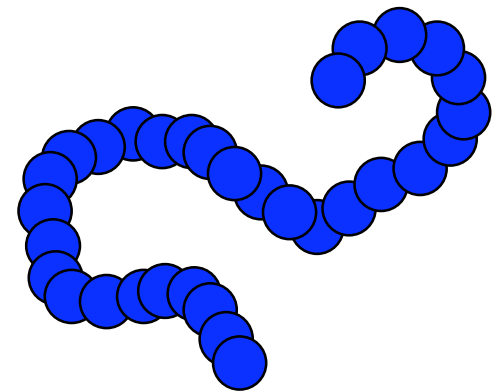
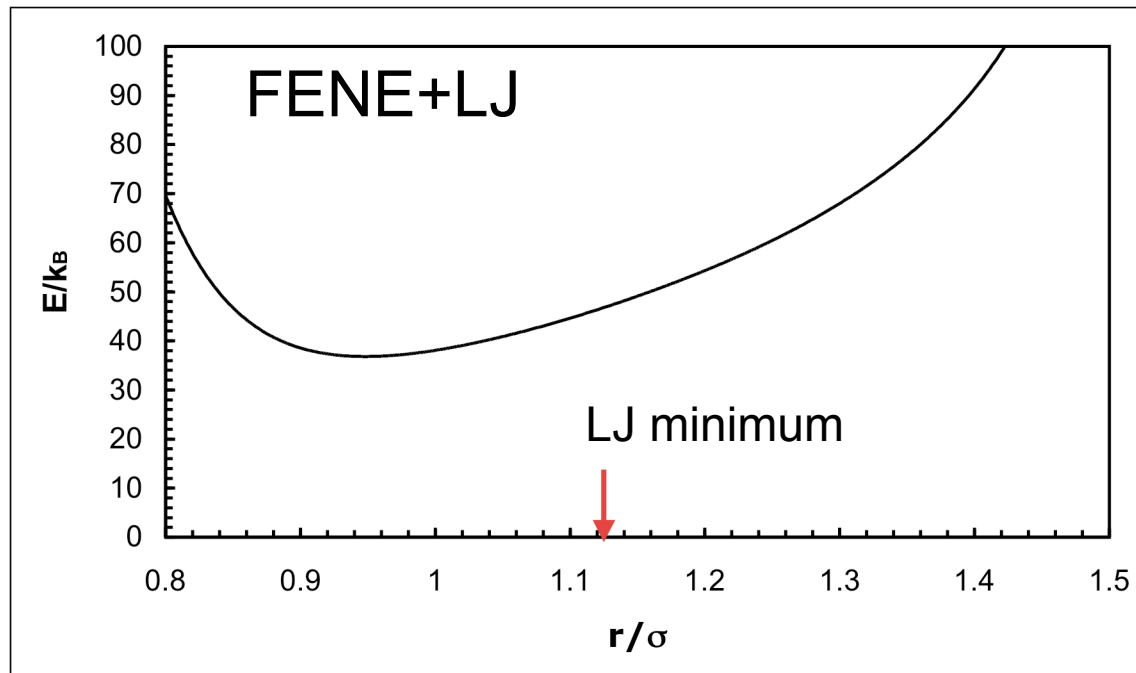
Essential Physics
bonded
excluded volume

$$U_{LJ} = 4\epsilon \left[\left(\frac{\sigma}{r} \right)^{12} - \left(\frac{\sigma}{r} \right)^6 \right] + \epsilon \quad r \leq 2^{1/6} \sigma$$

$$U_{LJ} = 0 \quad r > 2^{1/6} \sigma$$

$$U_{FENE} = -\frac{HR_0^2}{2} \ln \left[1 - \frac{r}{R_0} \right] \quad r < R_0$$

$$U_{FENE} = \infty \quad r \geq R_0$$



MD System Specifics

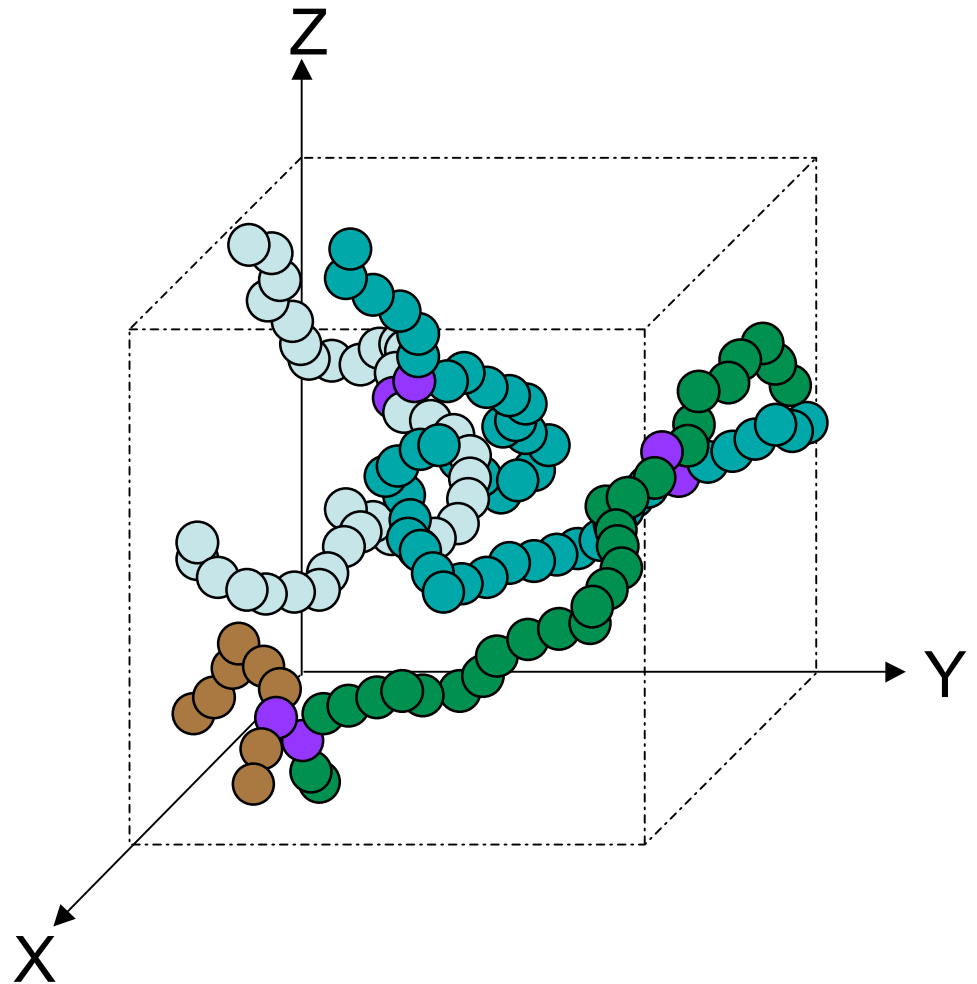
500 chains, 500 sites each, 20 reactive sites/chain

$\rho=0.85$ sites/volume

$T^*=1.0$

1. Equilibrate
2. React
3. Equilibrate
4. Deform
5. Equilibrate
6. React
7. Equilibrate

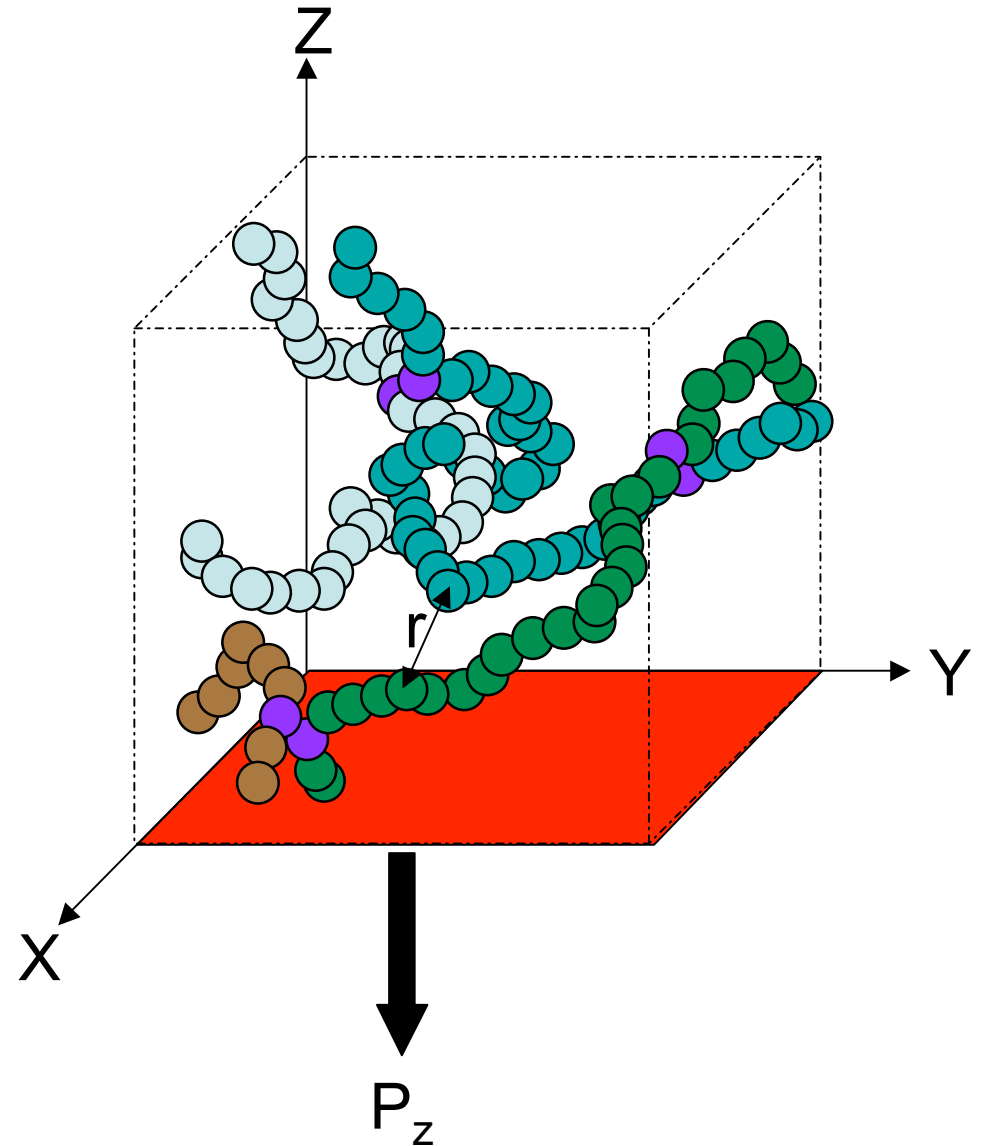
LAMMPS



Stress from MD

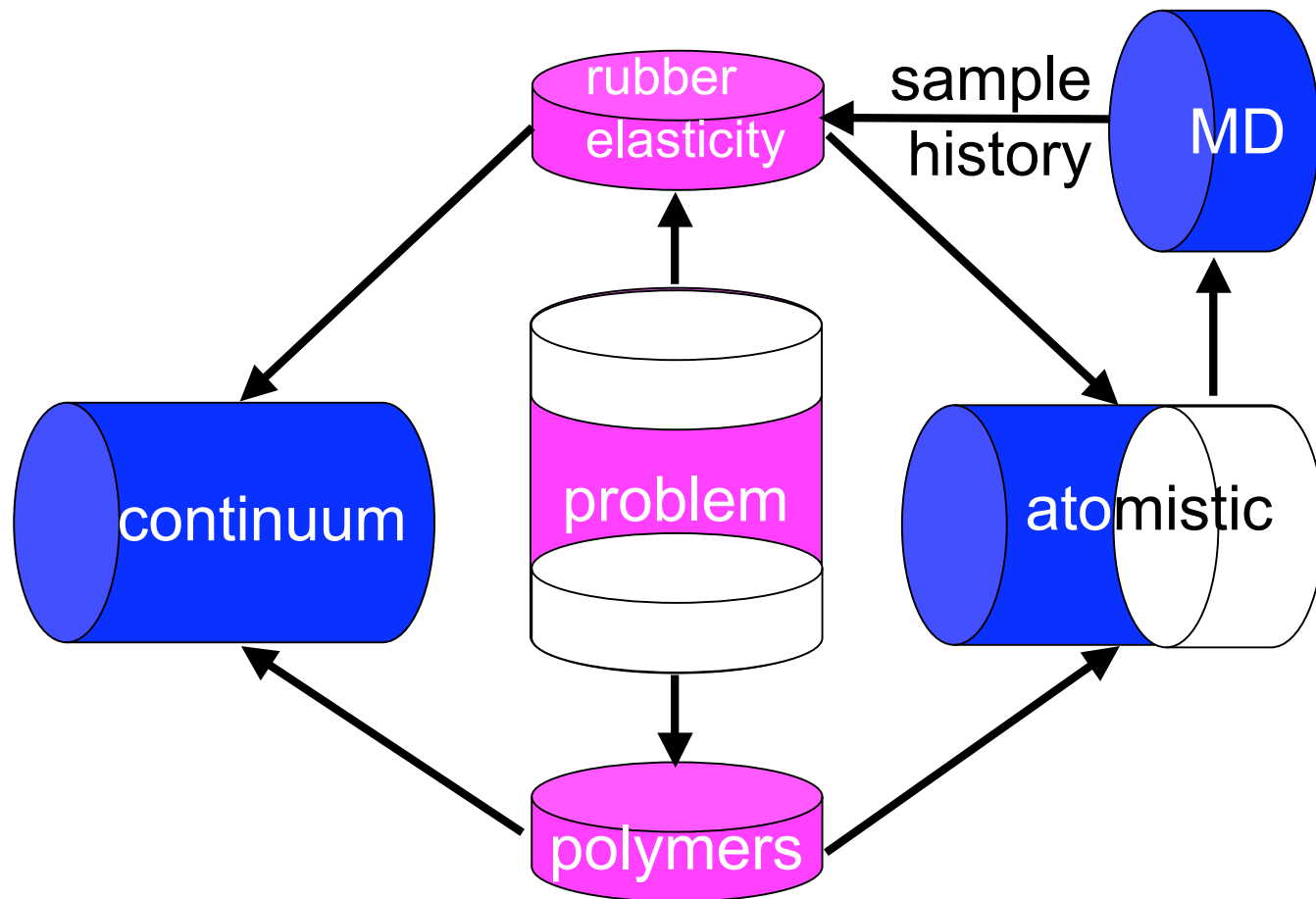
$$P = \left\langle \rho k_B T + \frac{1}{3V} \sum_i \sum_{j>i} r_{ij} \cdot f_{ij} \right\rangle$$

$$\sigma_{zz}^{dev} = P_z - \frac{1}{3} Tr \underline{\underline{P}}$$

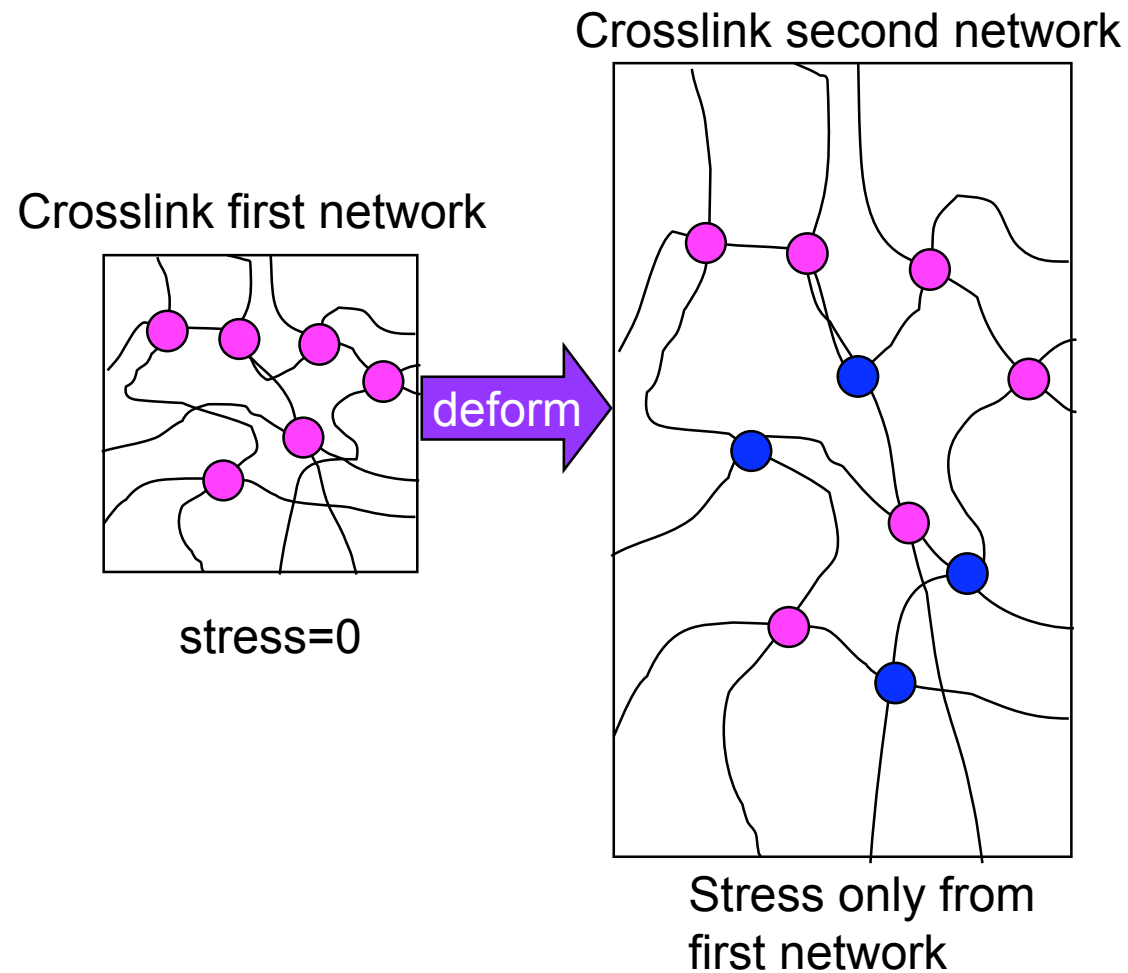


Calculate stress components from pressure components

Map



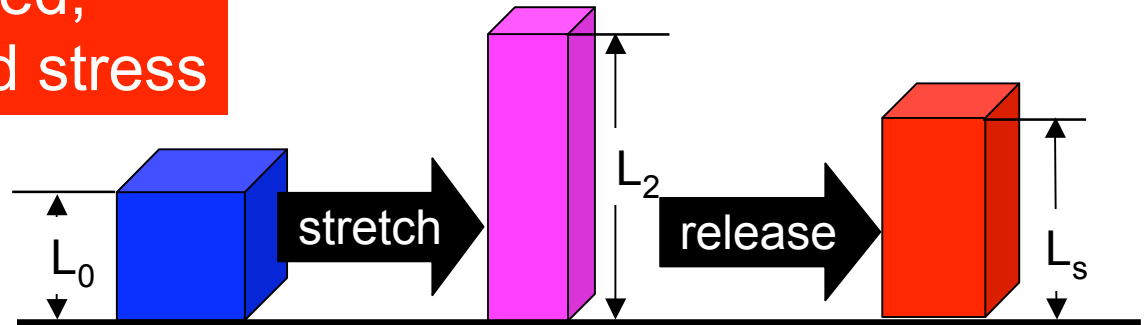
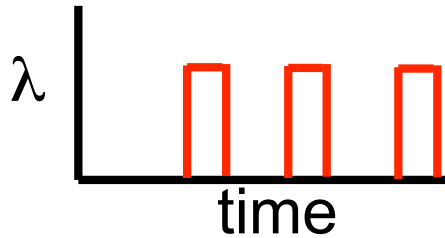
Independent Network Hypothesis



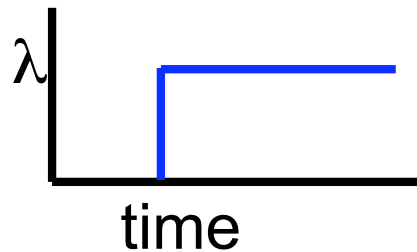
Reaction and strain histories are coupled

Experimental Data for INH

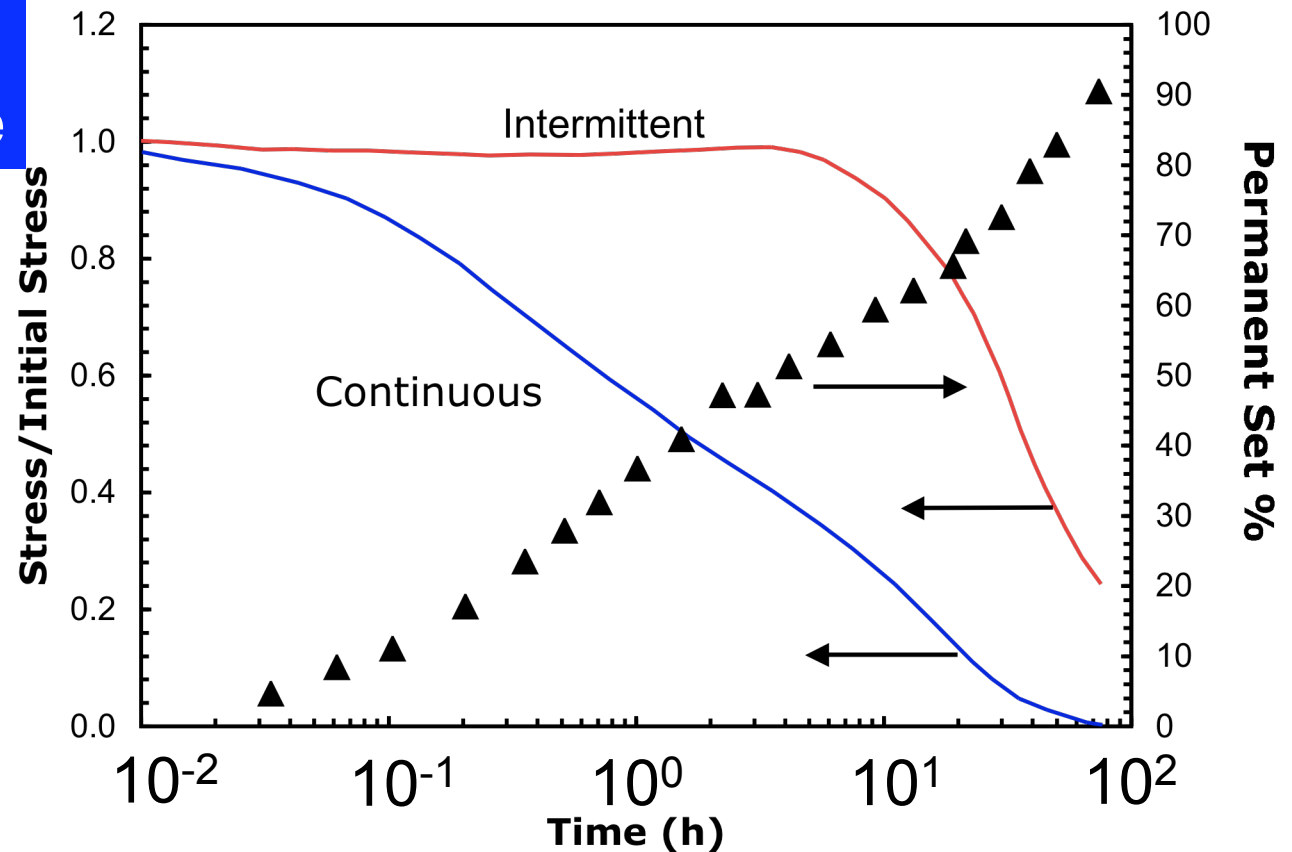
Intermittent: hold unstrained, periodic check of strained stress



Continuous: hold in strained state



Butyl Rubber
130°C, $\lambda=1.5$

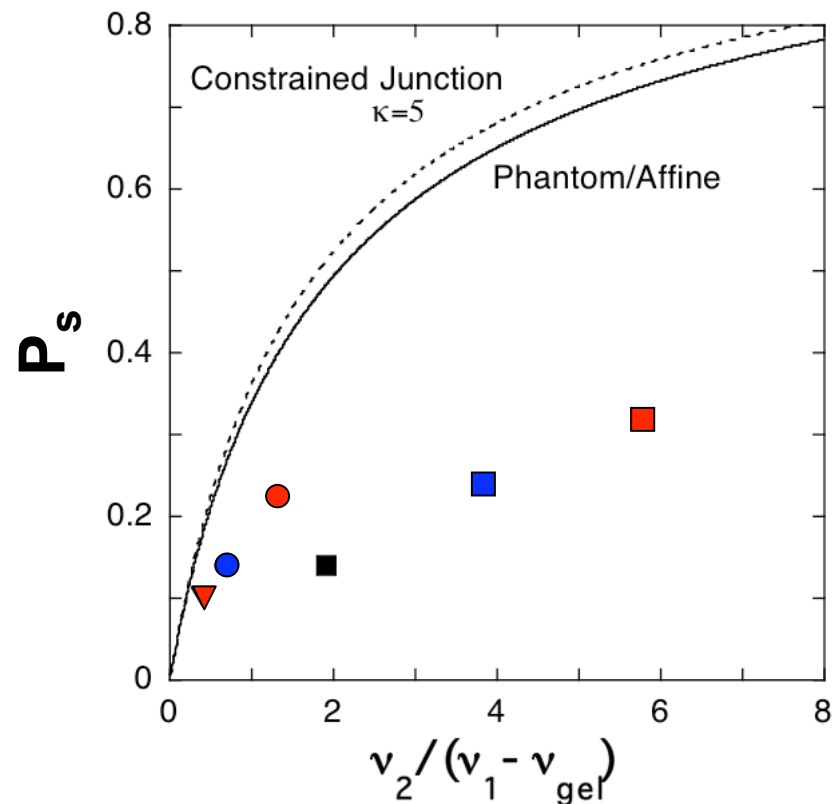
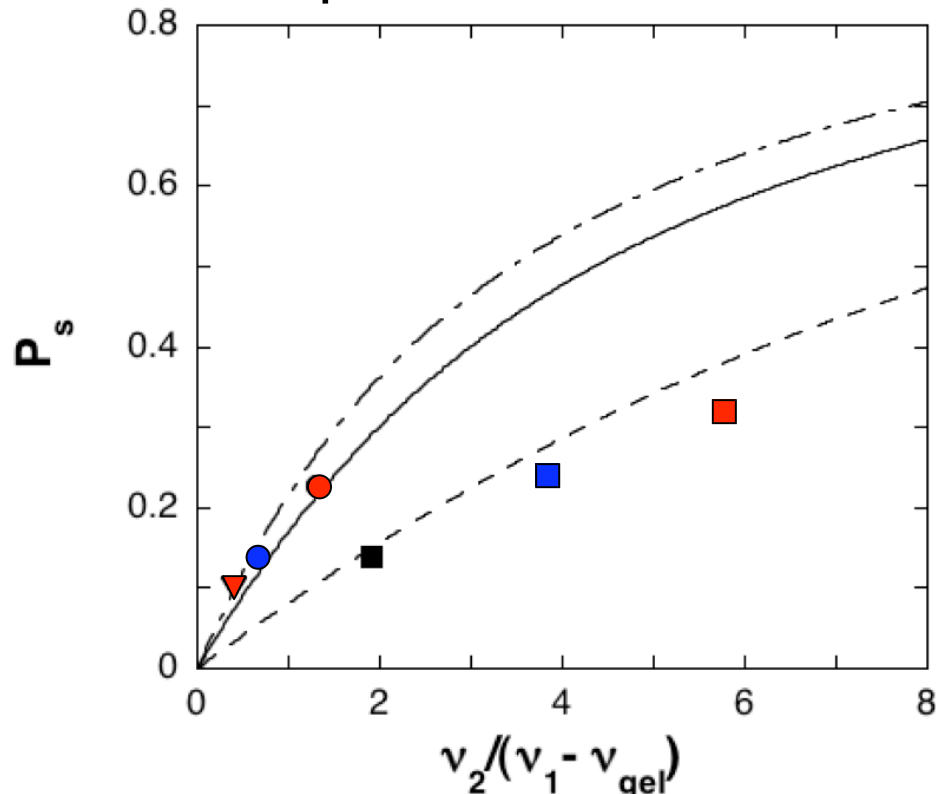
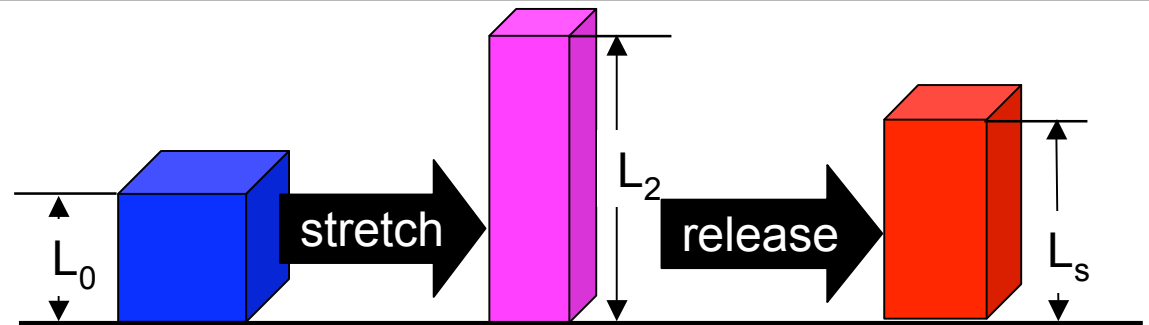


Permanent Set from MD

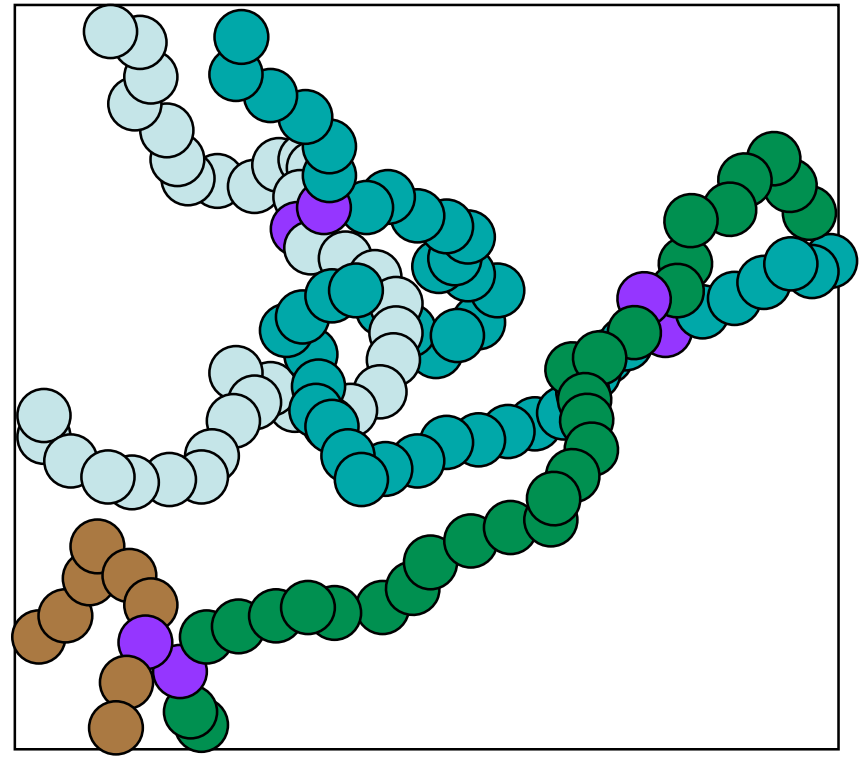
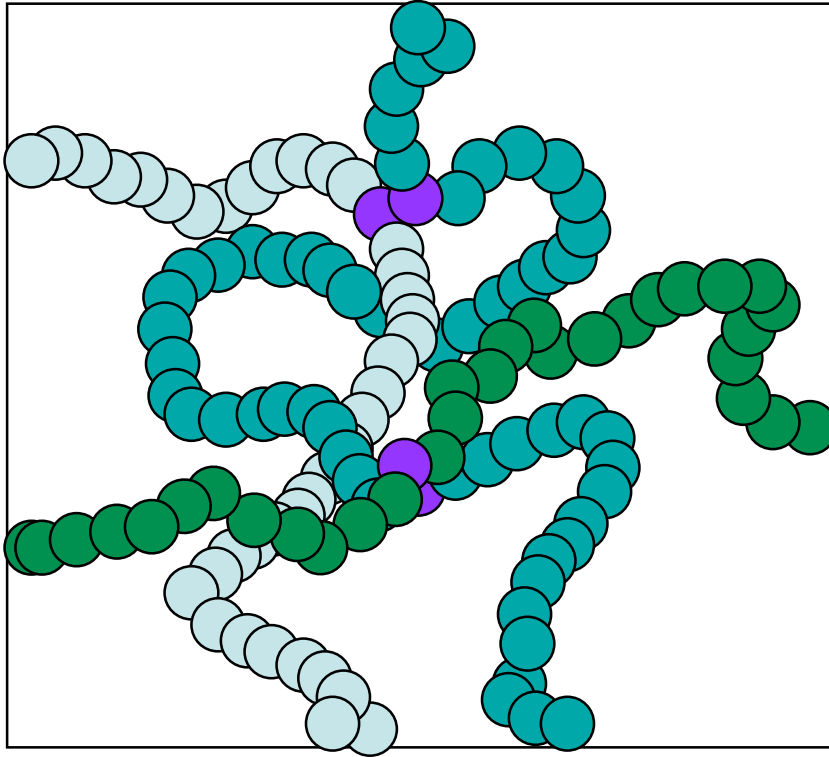
Uniaxial extension

$$P_s = \frac{\lambda_s - \lambda_0}{\lambda_2 - \lambda_0}$$

Slip-tube model

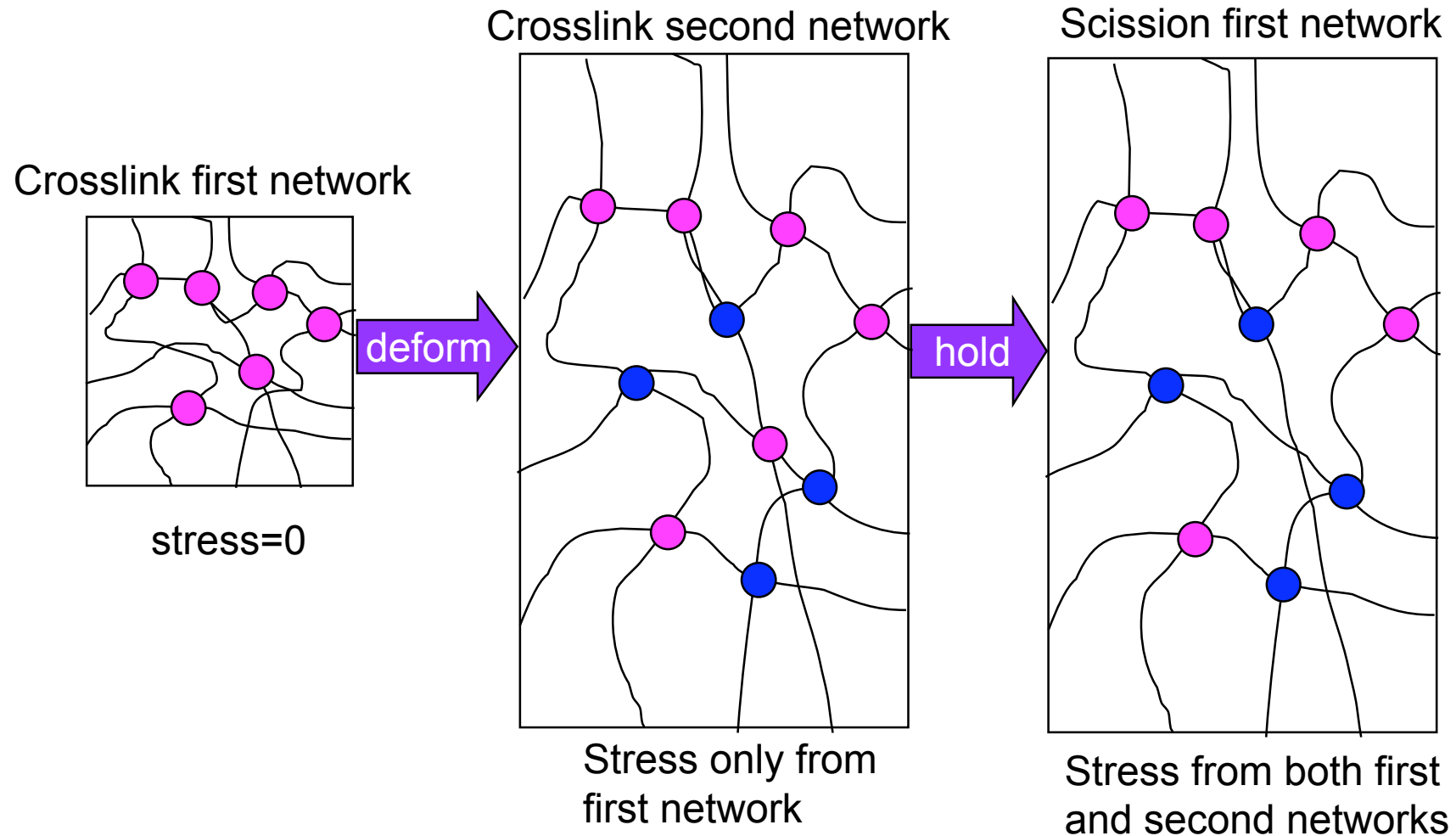


Entanglements



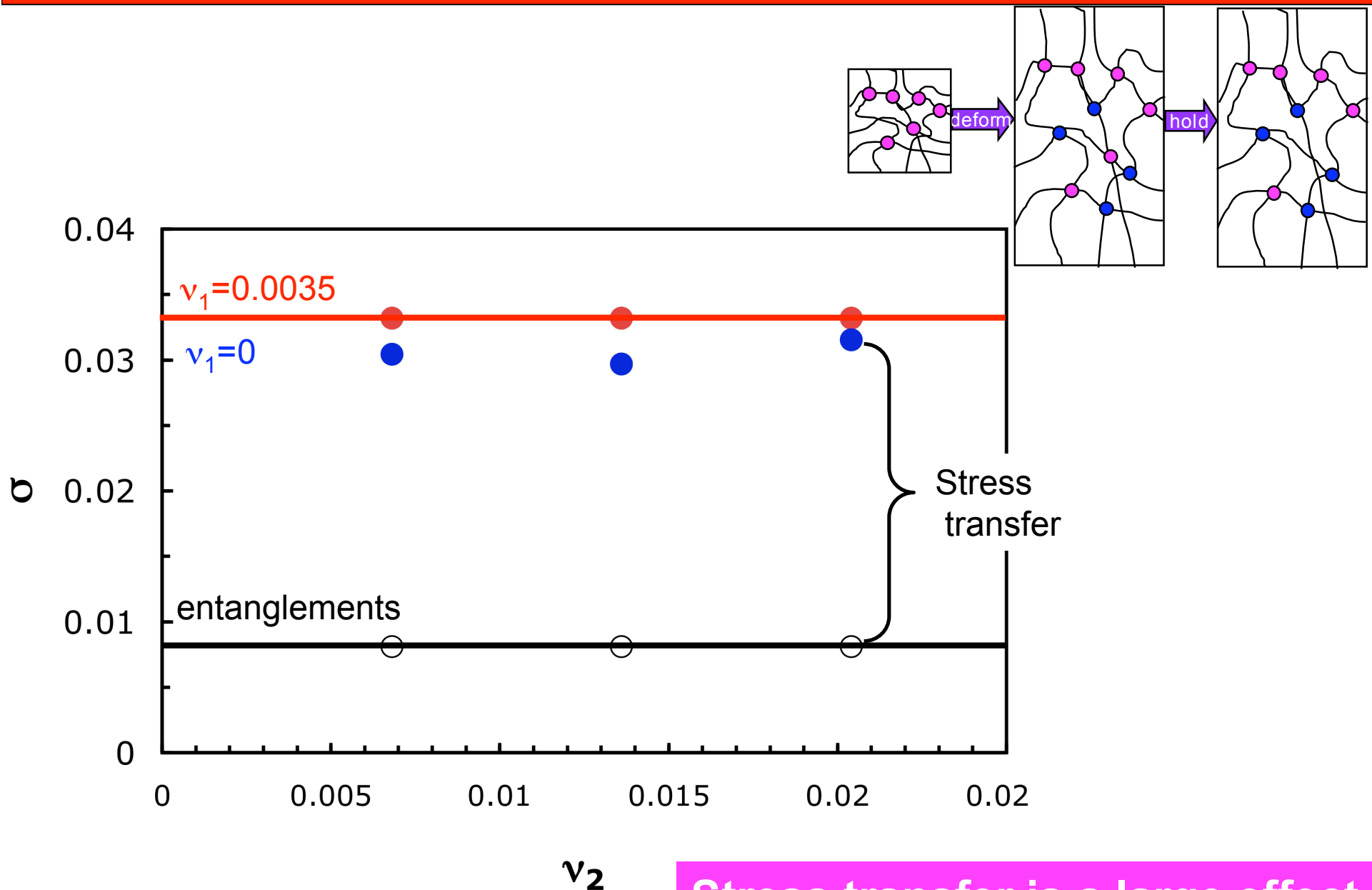
Trapped entanglements also contribute to stress

Independent Network Hypothesis (Revisited)



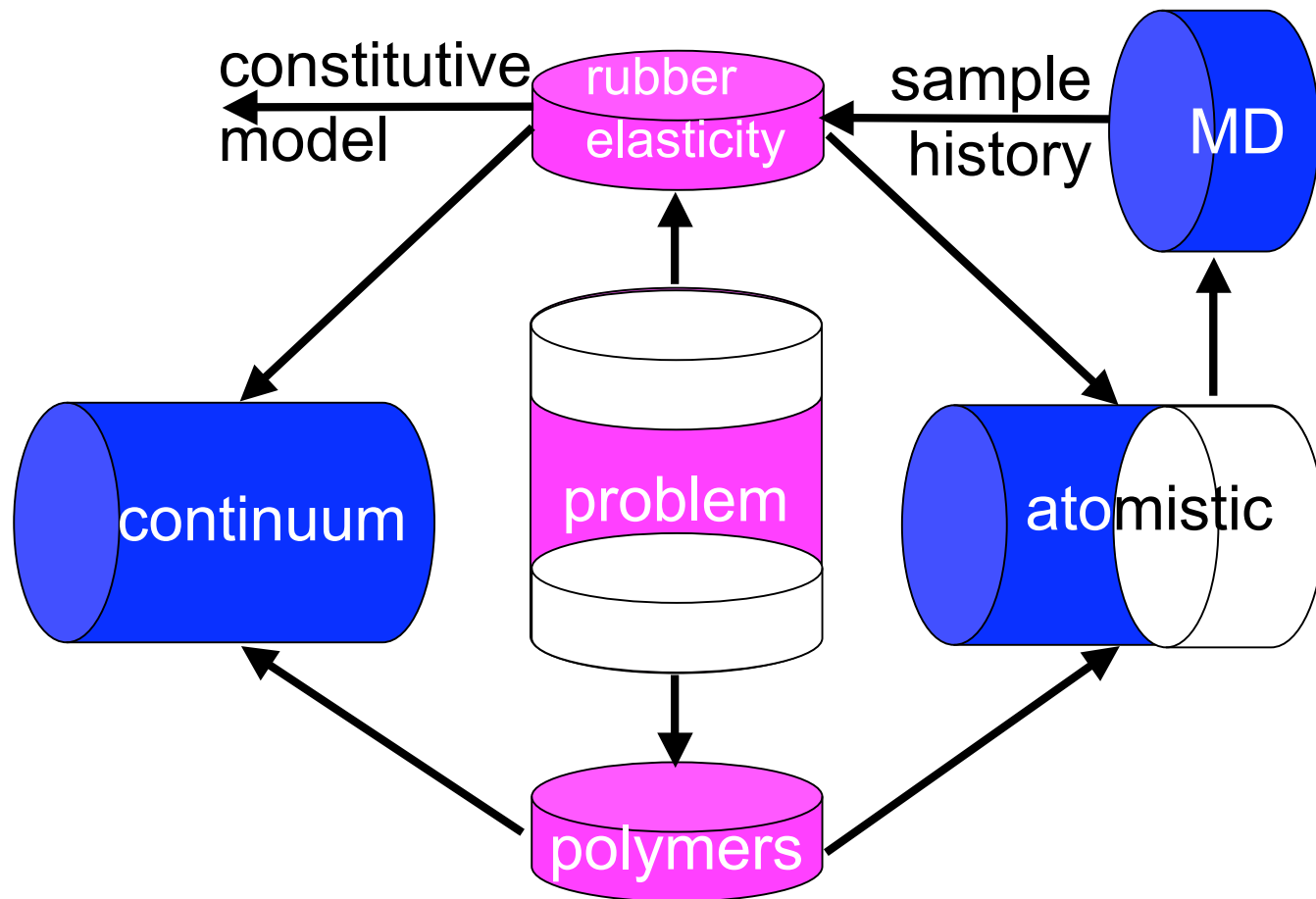
Sample retains memory of crosslinking and strain history

MD Simulation with Scission

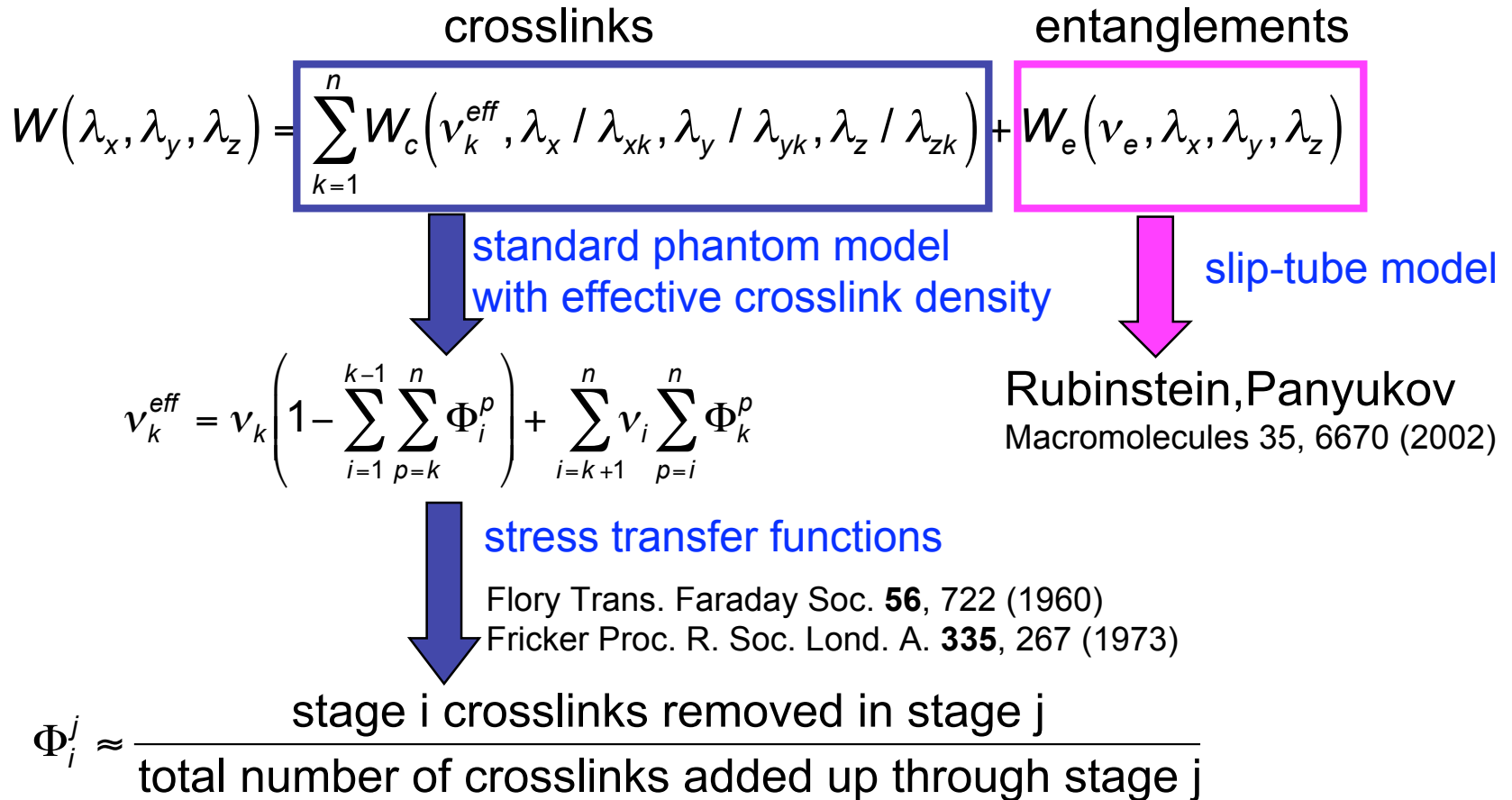


Stress transfer is a large effect

Map



General Constitutive Model



Use independent network hypothesis to formulate strain energy.
Use common form of principal stretches.

Entanglement Network

Sample most likely between 30% and 300% of original dimensions

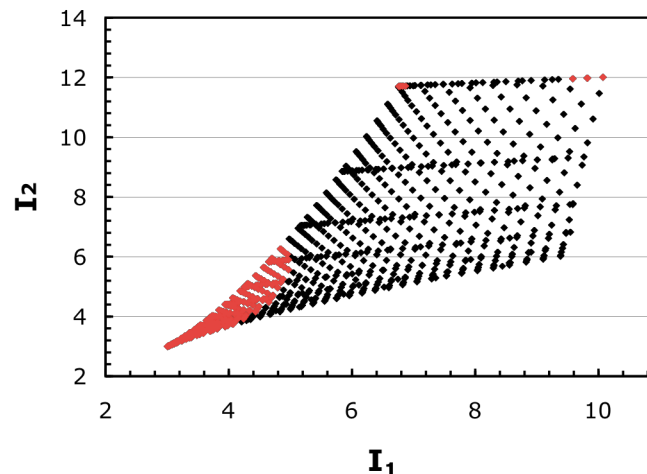
Slip-tube model
computationally demanding
for arbitrary strain

$$W = \frac{A}{2} \sum_{\alpha} \left(\frac{\lambda_{\alpha}}{\sqrt{g_{\alpha}}} + \frac{\sqrt{g_{\alpha}}}{\lambda_{\alpha}} \right) - \frac{A}{3} \sum_{\alpha} \ln \left(\frac{N g_{\alpha}}{L} \right)$$

Rubinstein, Panyukov
Macromolecules 35, 6670 (2002)

fit strain energy
for expected deformations

$$0.3 \leq \{\lambda_1, \lambda_2, \lambda_3\} \leq 3$$



Use invariant fit in FE
to calculate stress

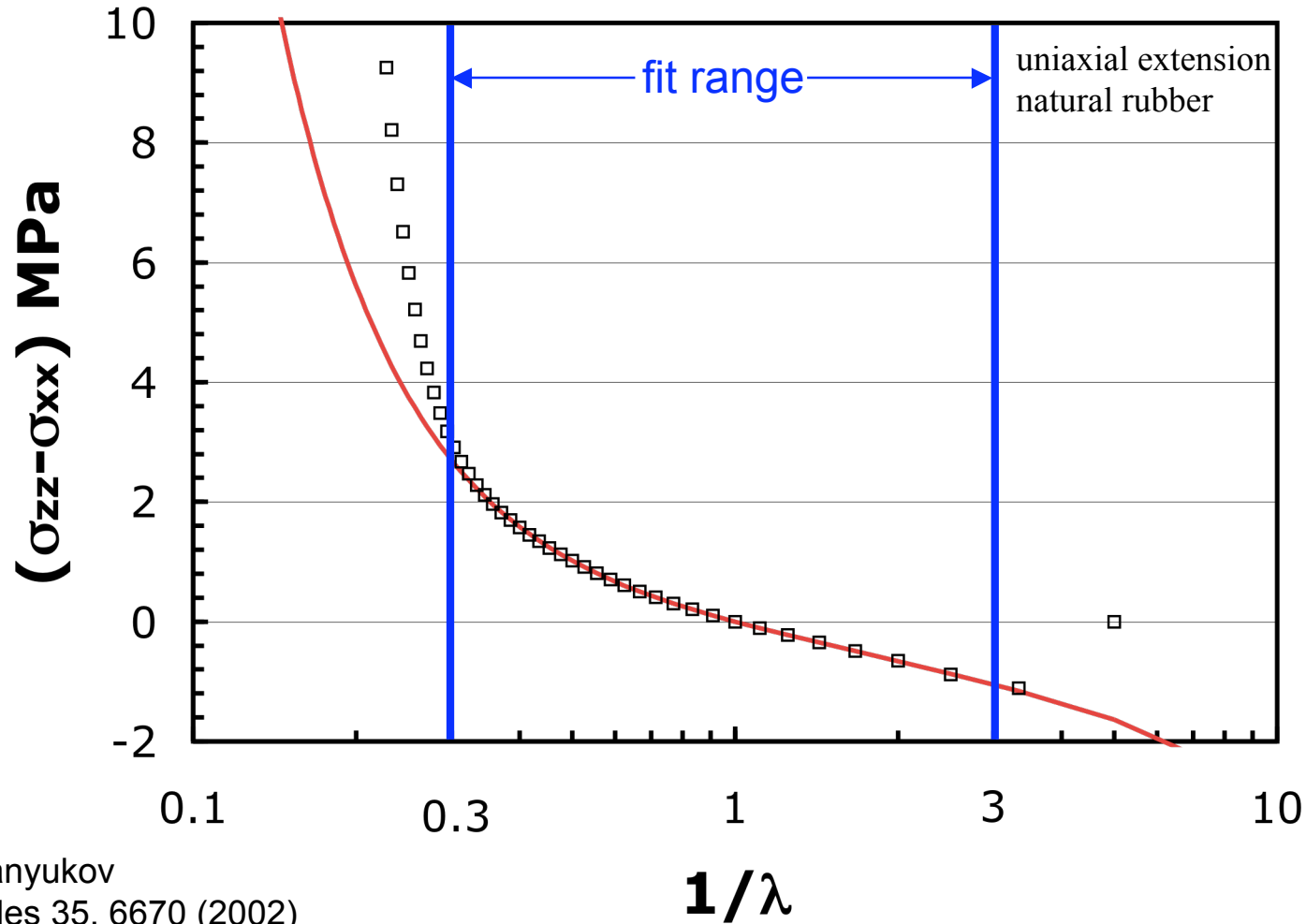
$$W = \sum_{i=1}^3 \sum_{k=1}^3 c_{ik} (I_1 - 3)^i (I_2 - 3)^k$$

$$I_1 = \lambda_1^2 + \lambda_2^2 + \lambda_3^2$$

$$I_2 = \lambda_1^2 \lambda_2^2 + \lambda_2^2 \lambda_3^2 + \lambda_3^2 \lambda_1^2$$

MD shows that only first stage networks trap entanglements

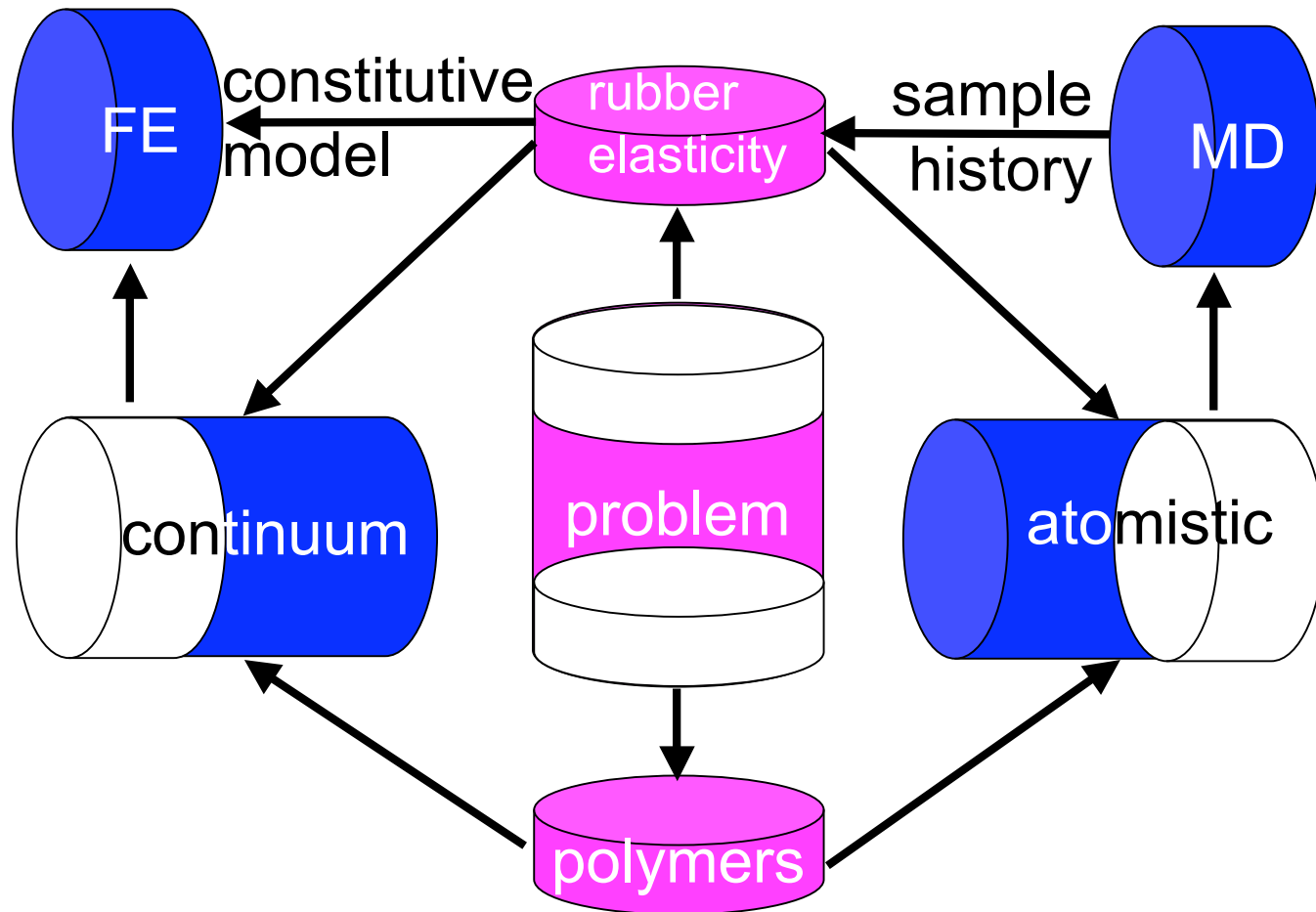
Comparing W to Experiment



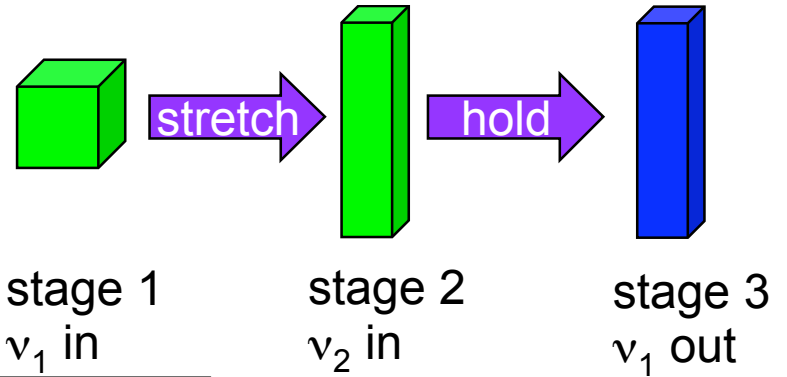
Rubinstein, Panyukov
Macromolecules 35, 6670 (2002)

Strain energies were fit to $0.3 \leq \{\lambda_1, \lambda_2, \lambda_3\} \leq 3$ (arbitrary deformation)
Good agreement found between prediction and experiment

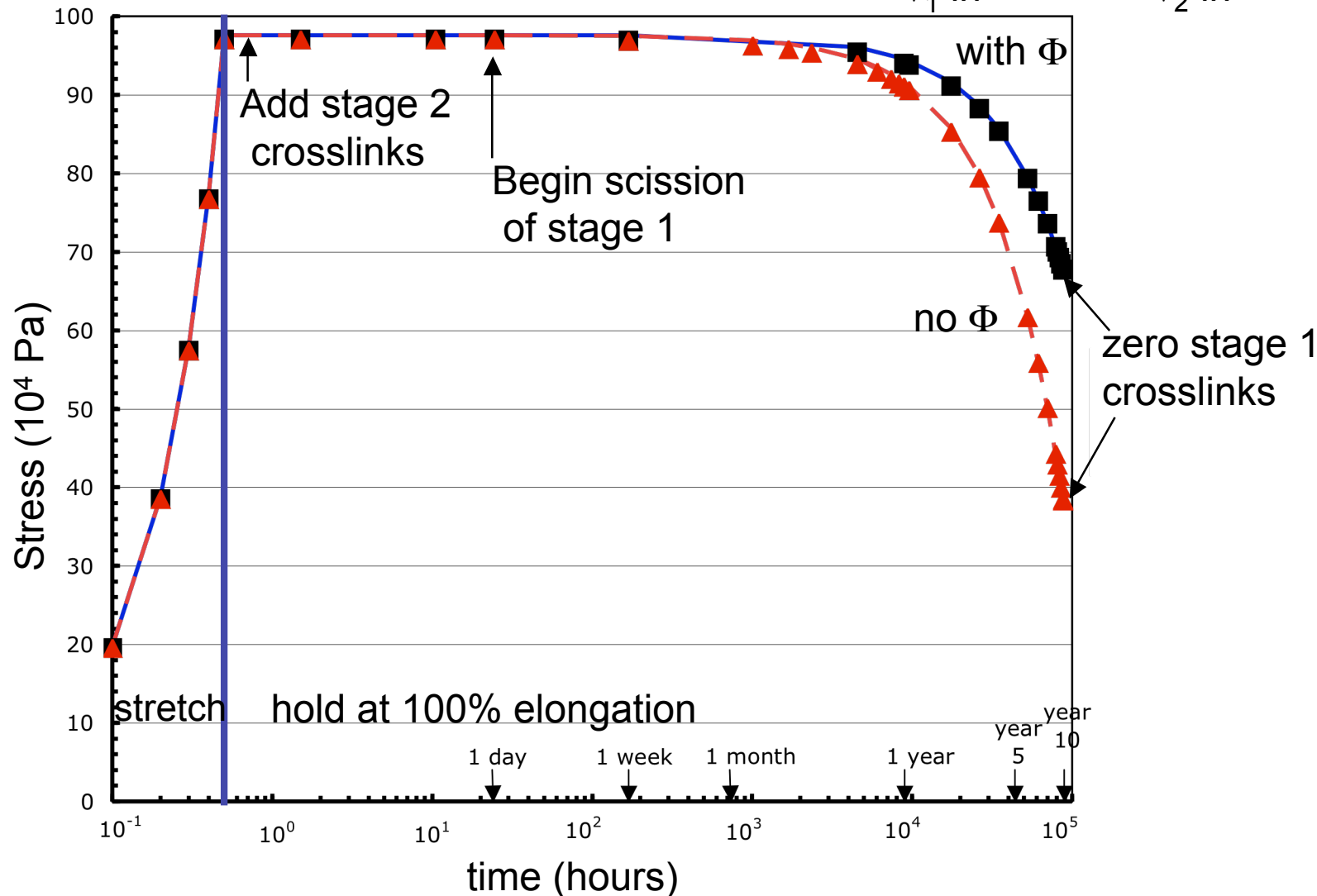
Map



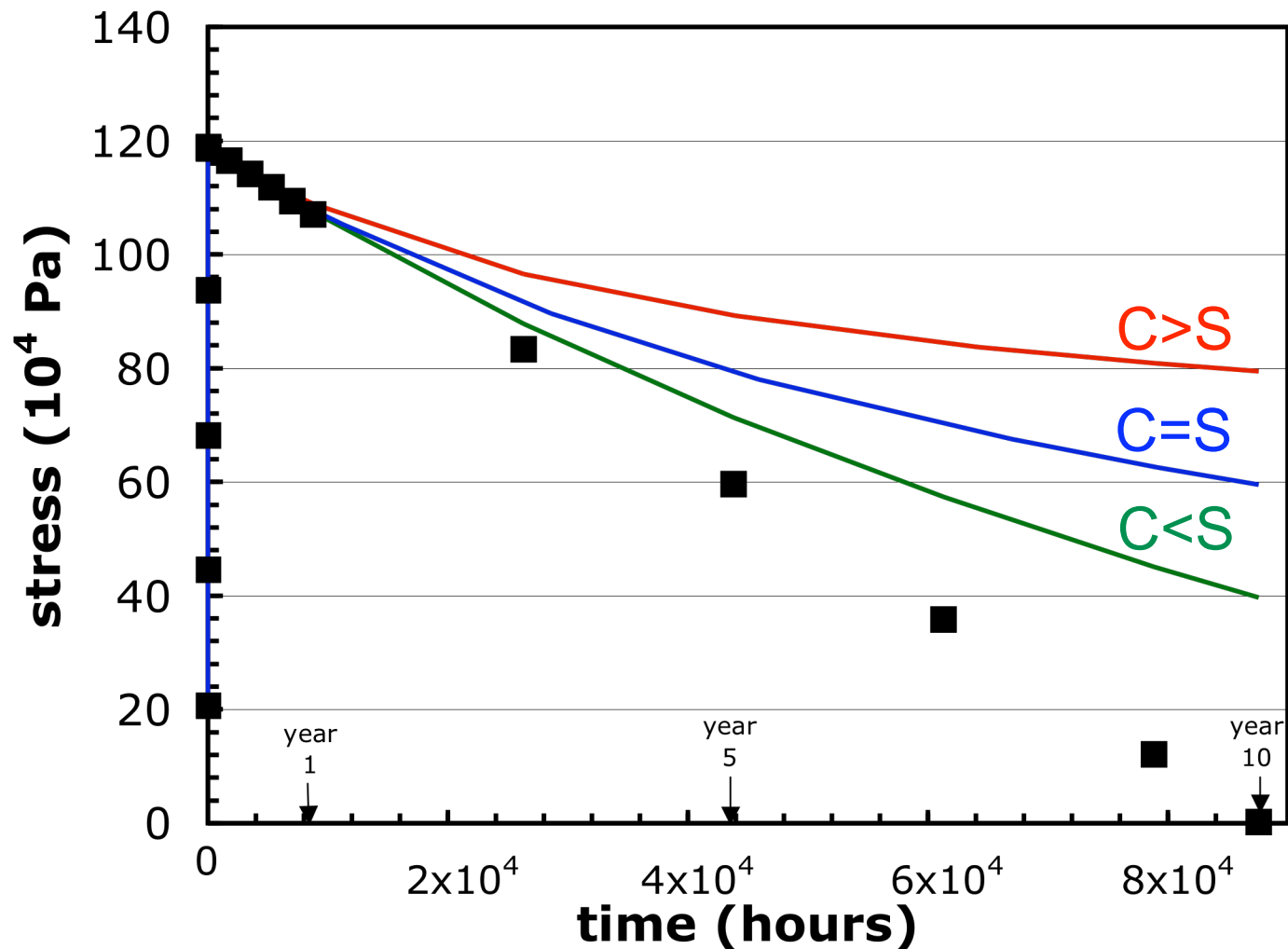
Finite Element



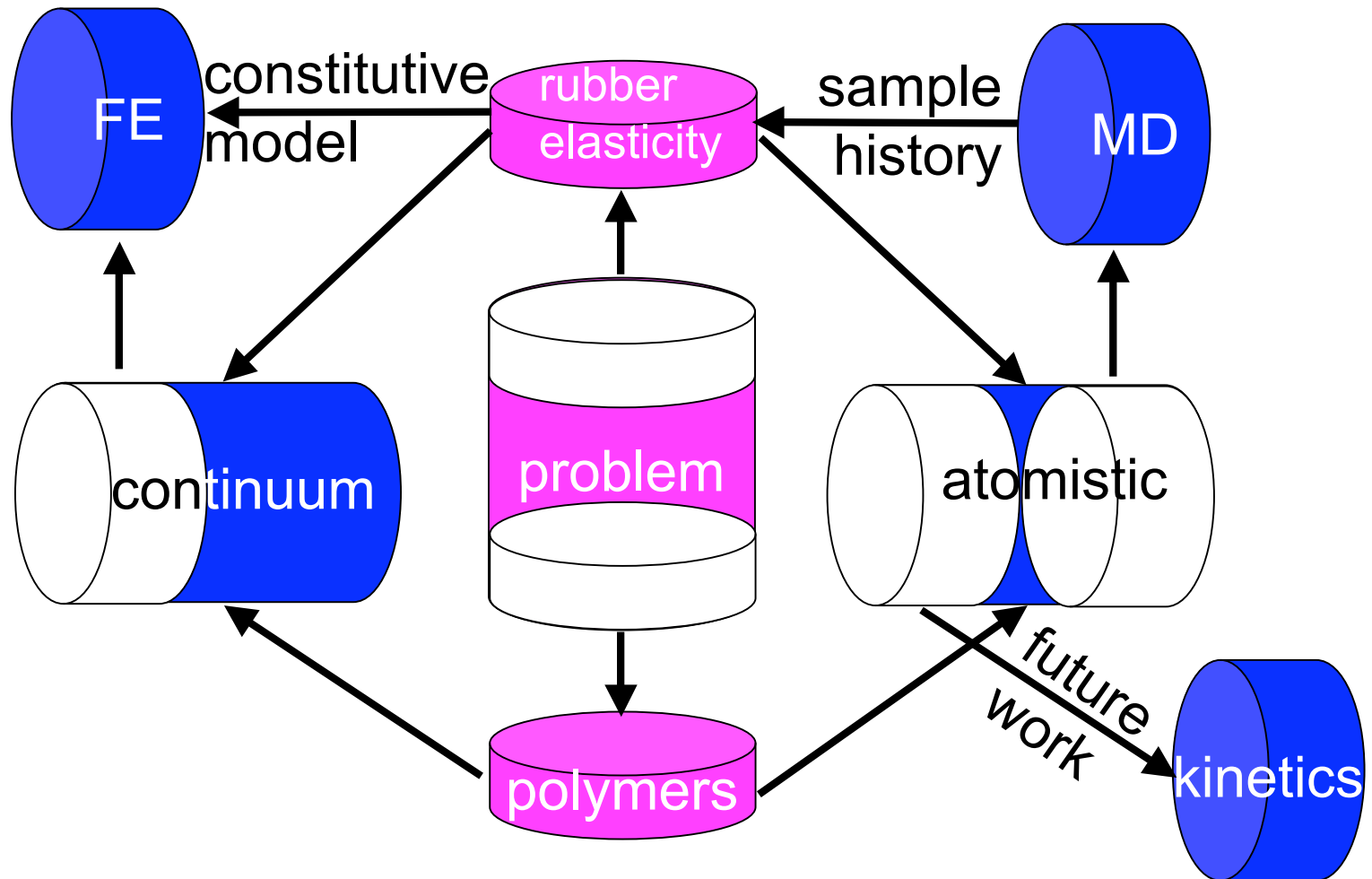
Final stress 80% higher using Φ



Simultaneous Crosslinking and Scission

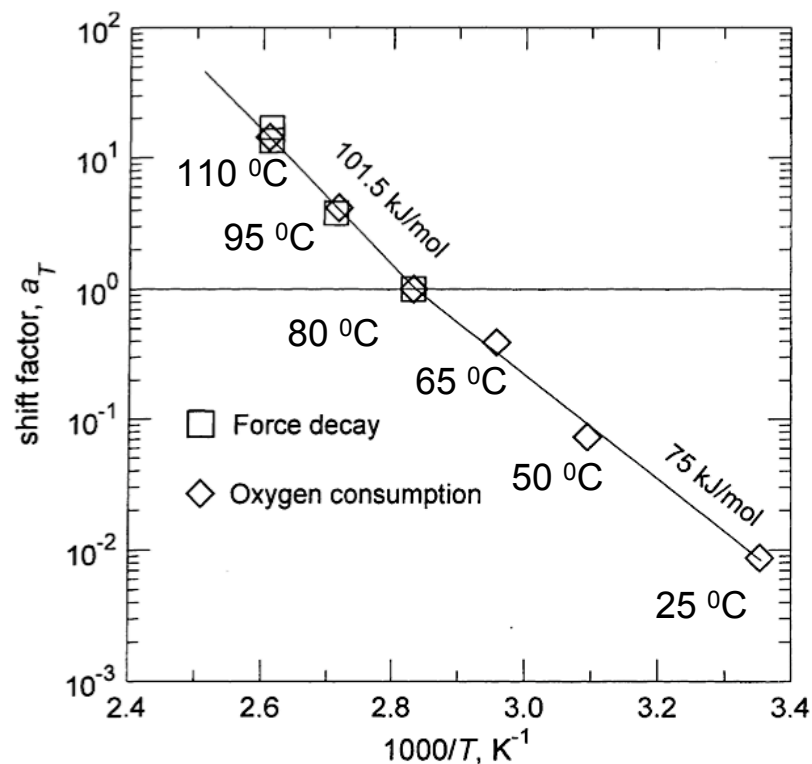


Relative rates of scission and crosslinking make a large difference in the resulting stress

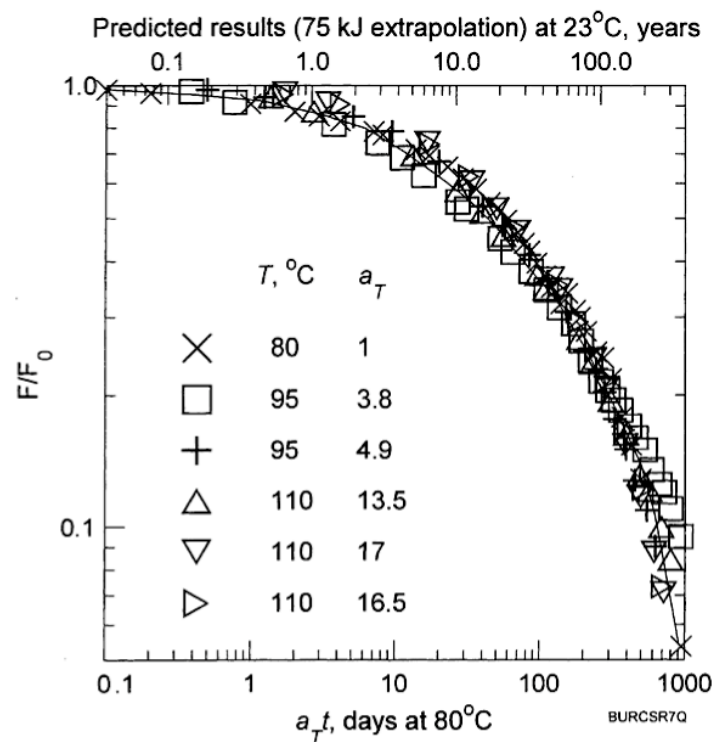


Experimental Kinetics

Butyl o-rings with accelerated aging

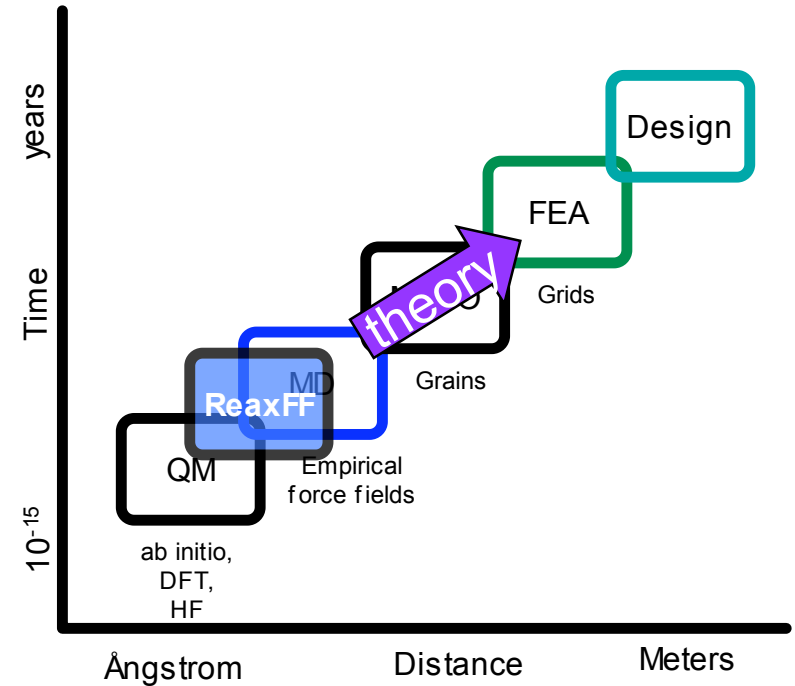
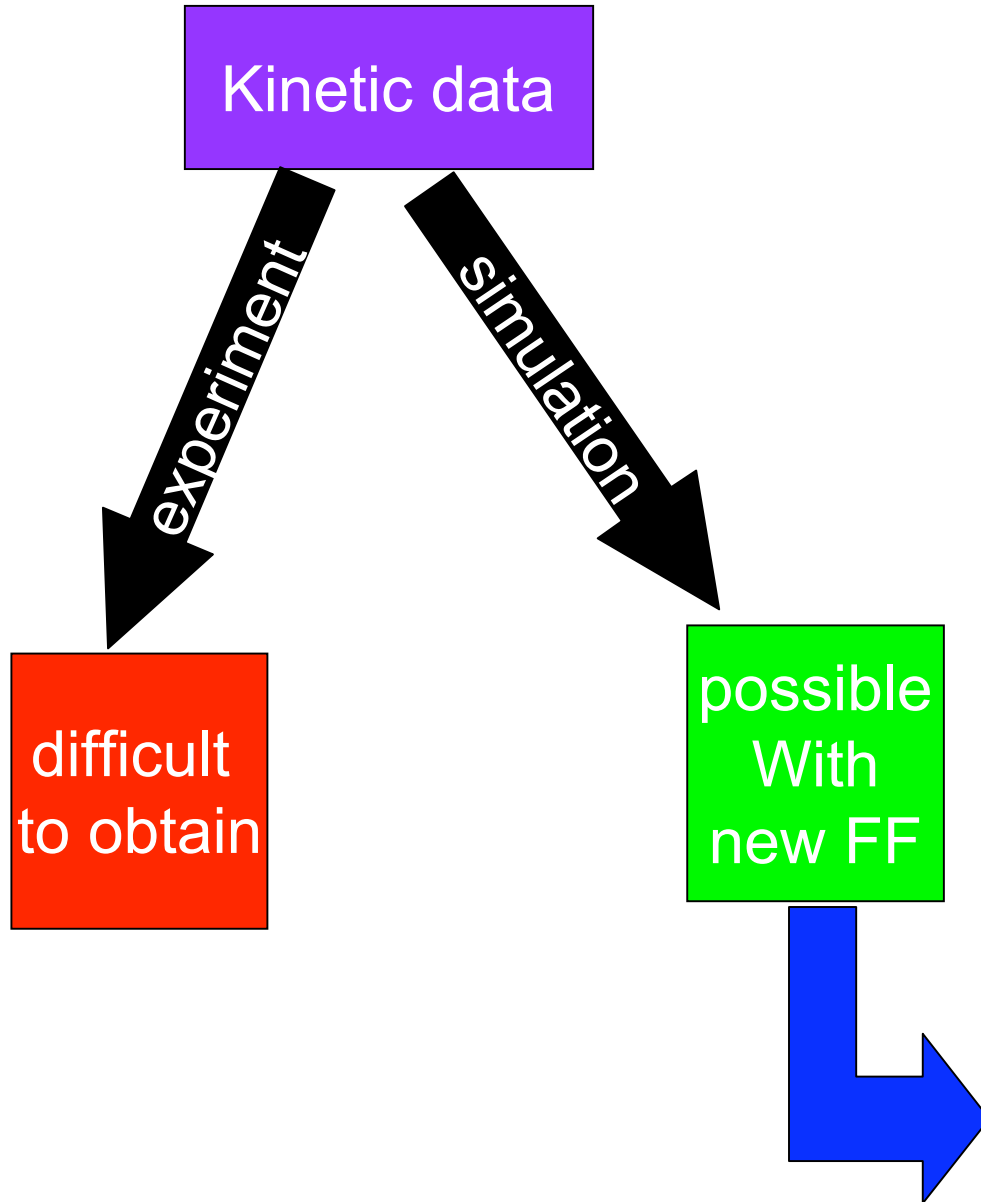


Gillen et al. Polym. Degrad. Stab. 82, 25 (2003)



Arrhenius relation changes slope at moderate temperature

Future Work



Summary

