



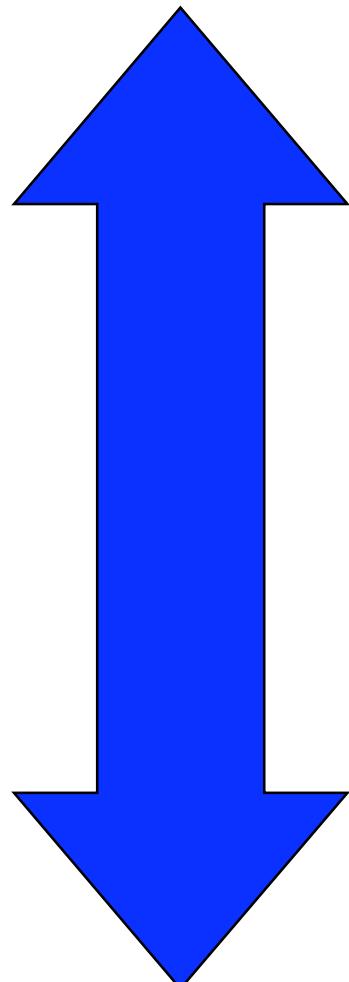
# Chemical Aging of Rubber: Constitutive Modeling Using Molecular Dynamics

Joanne Budzien

1814, Computational Materials Science and Engineering  
Sandia National Laboratories

# Collaborators

## FE calculations

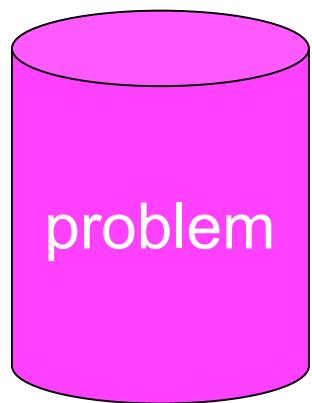


- David Lo  
(1523, Materials Mechanics)
- Joanne Budzien  
(1814, Computational Materials Science and Engineering)
- John Curro  
(1815, Ceramic Processing and Inorganic Materials)
- Dana Rottach  
(UNM, Department of Chemical and Nuclear Engineering)
- Gary Grest  
(1114, Surface and Interface Sciences)
- Aidan Thompson  
(1435, Multiscale Computational Materials Methods)

## MD simulations

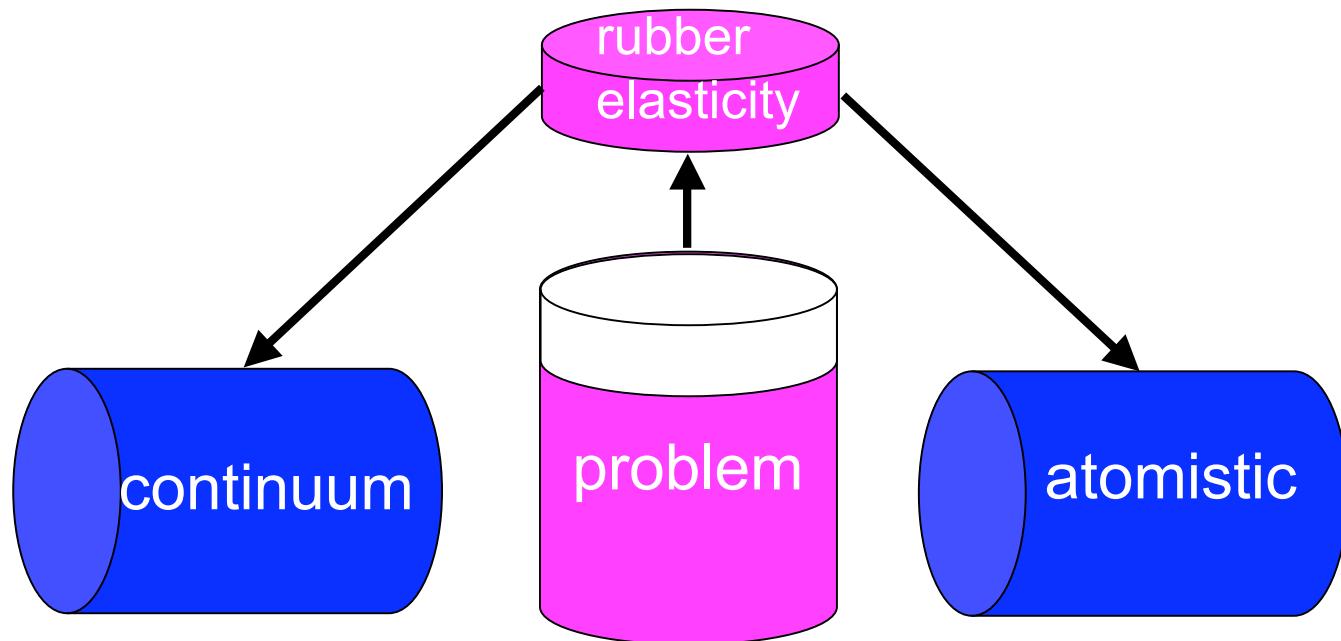
# Map

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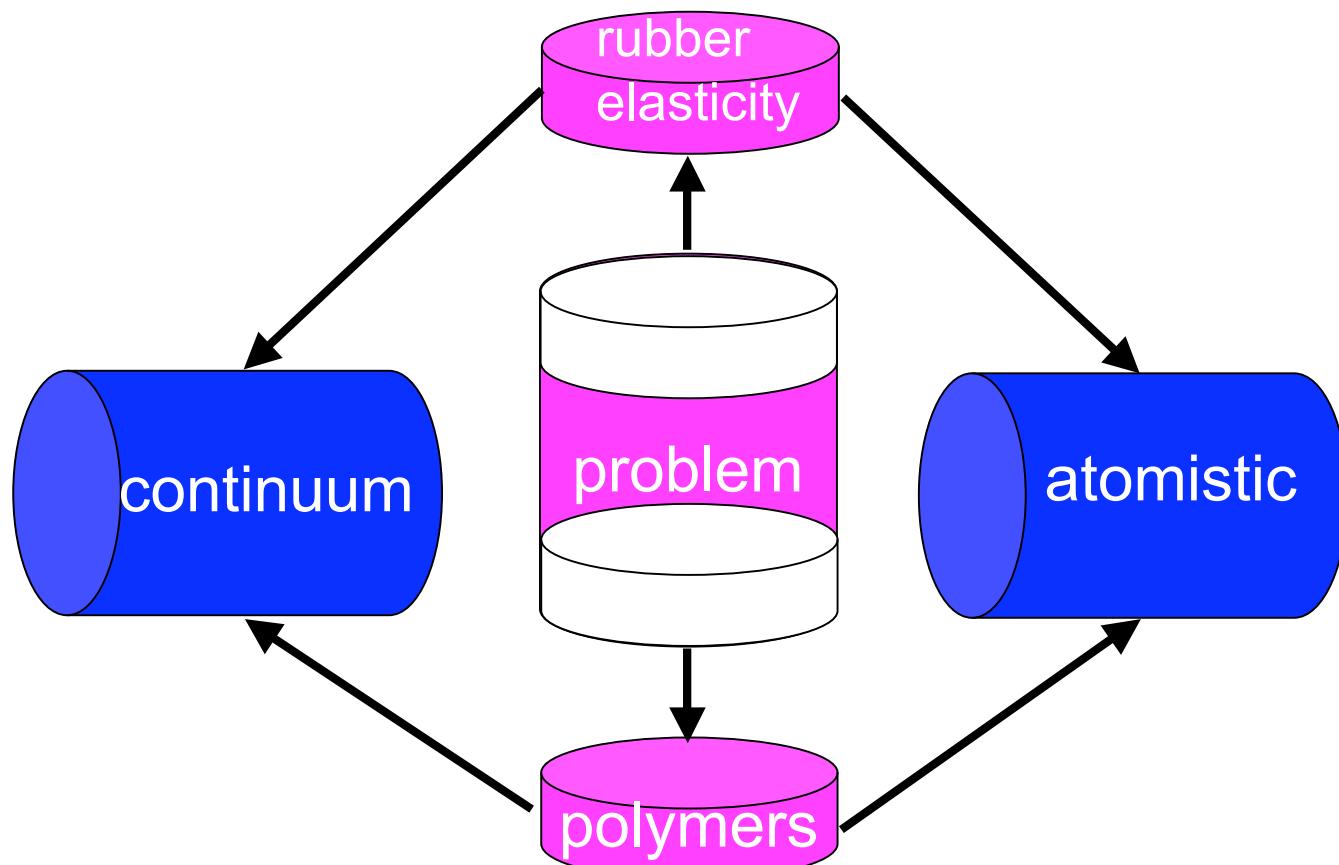
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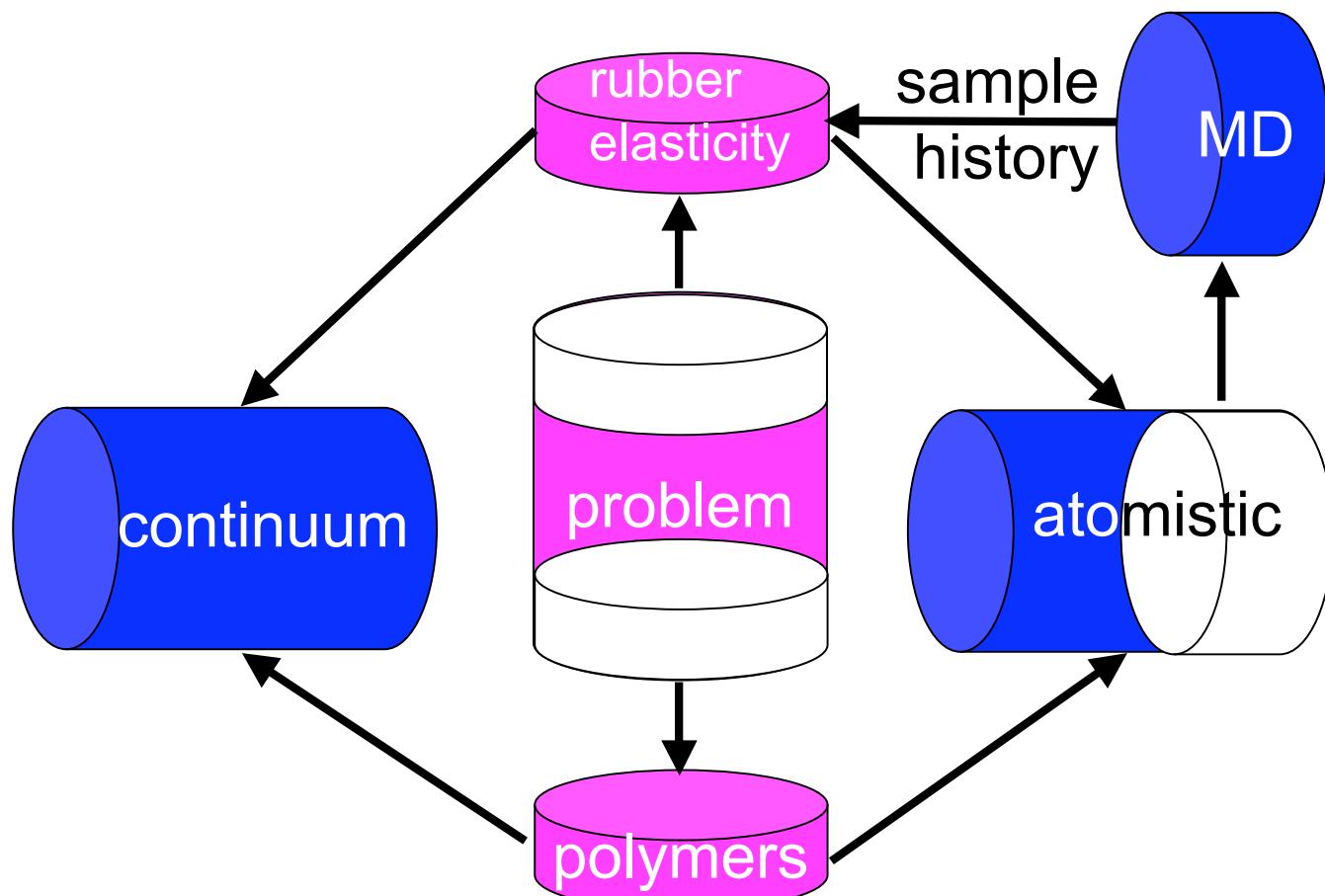
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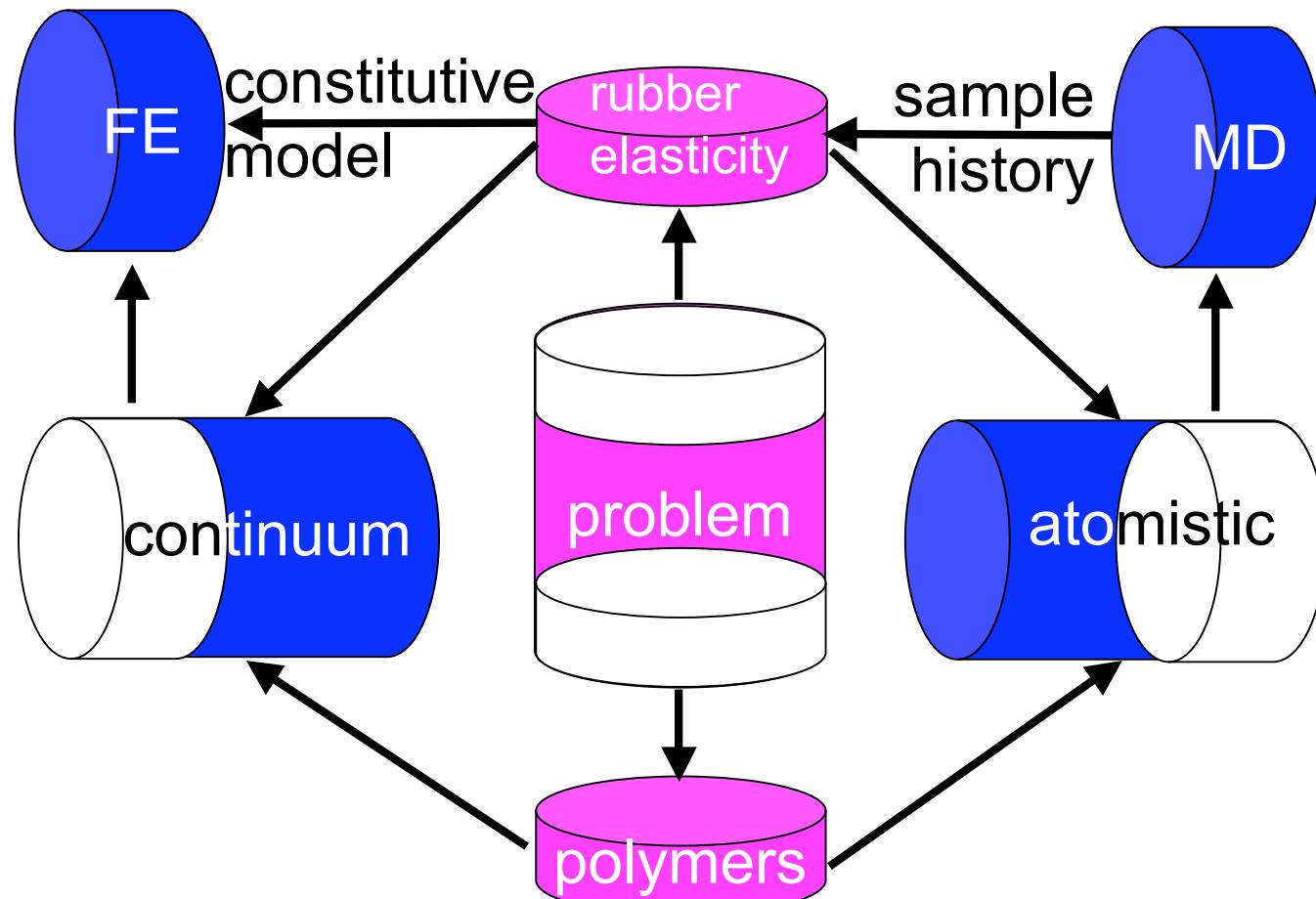
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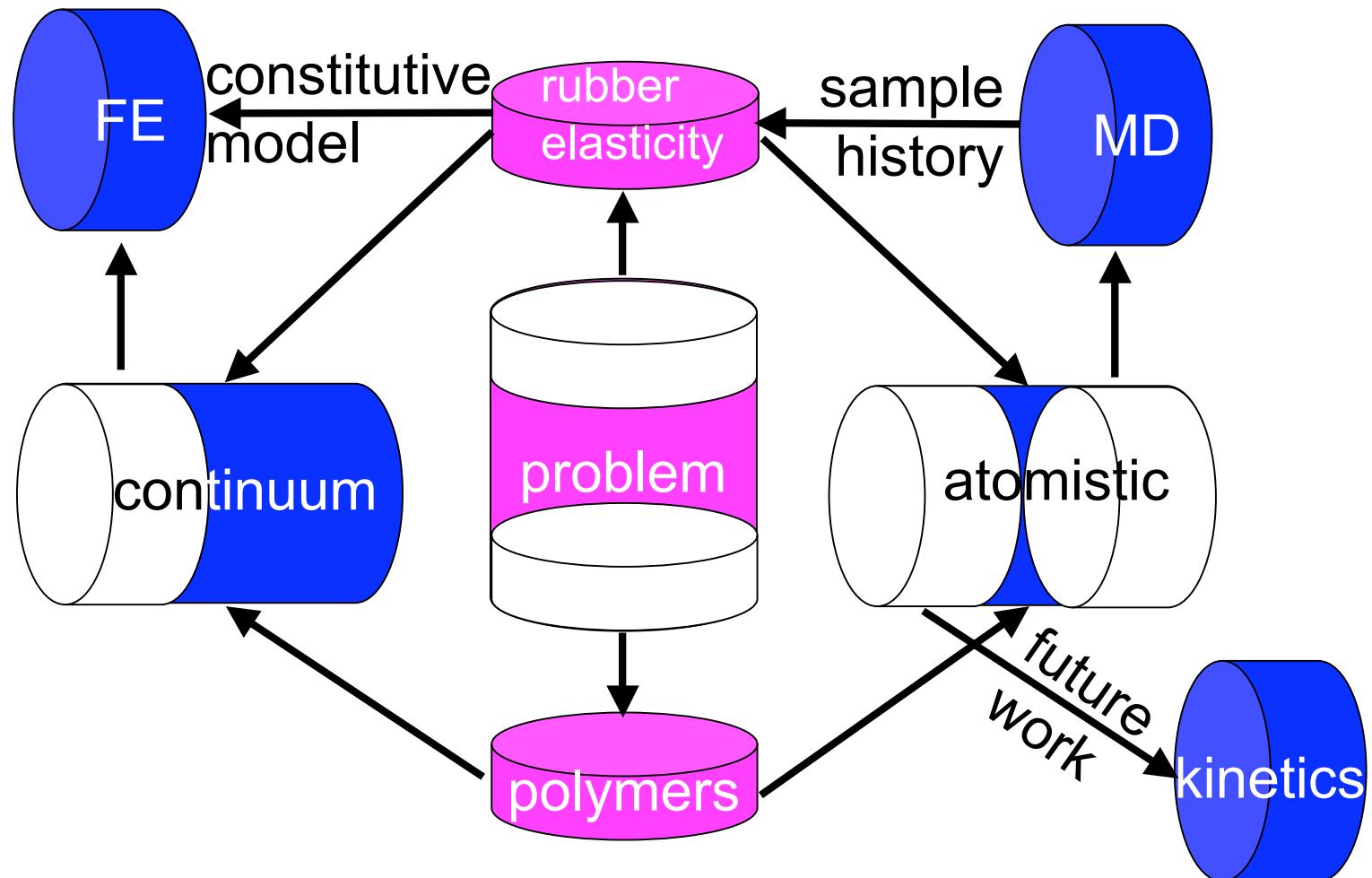
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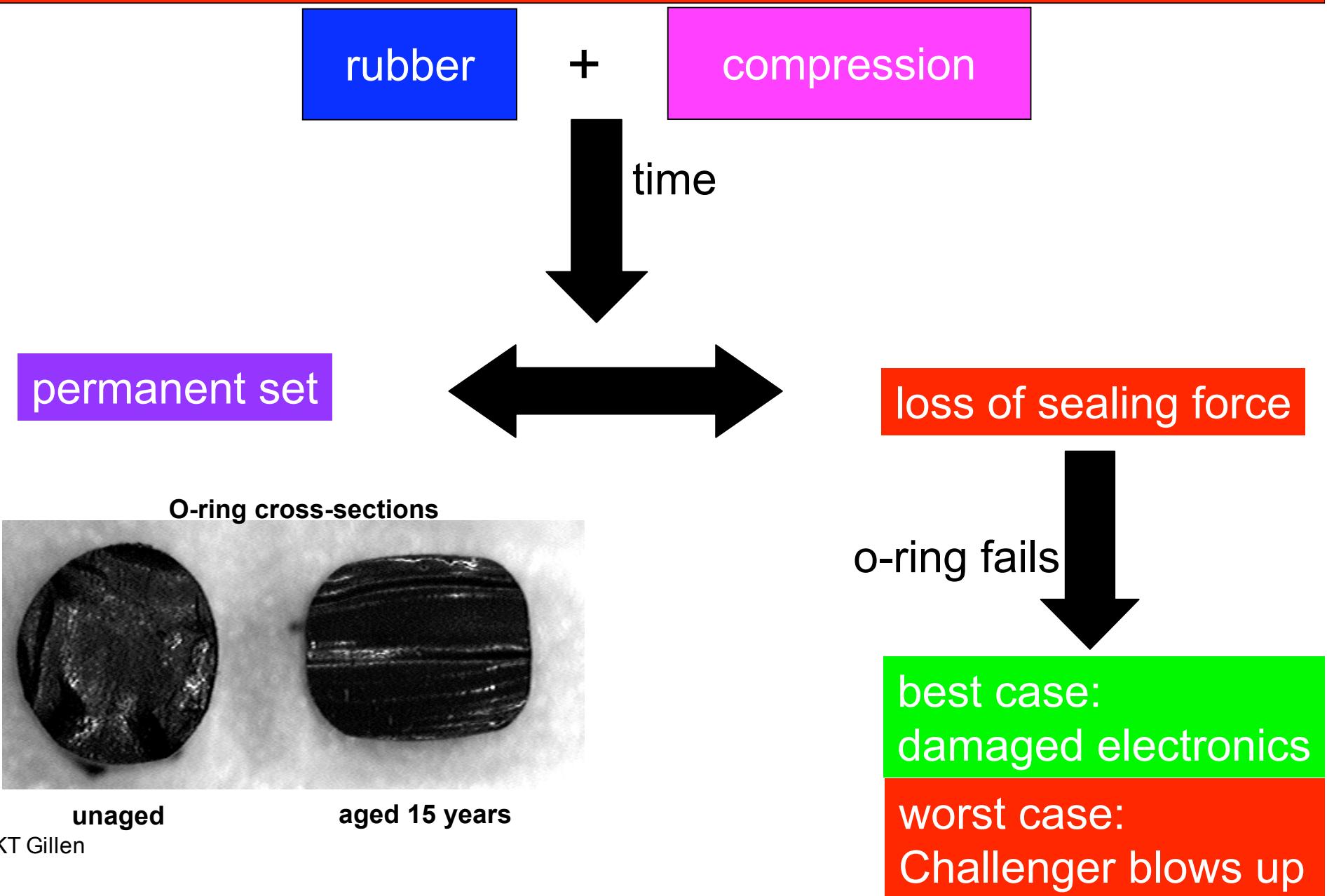


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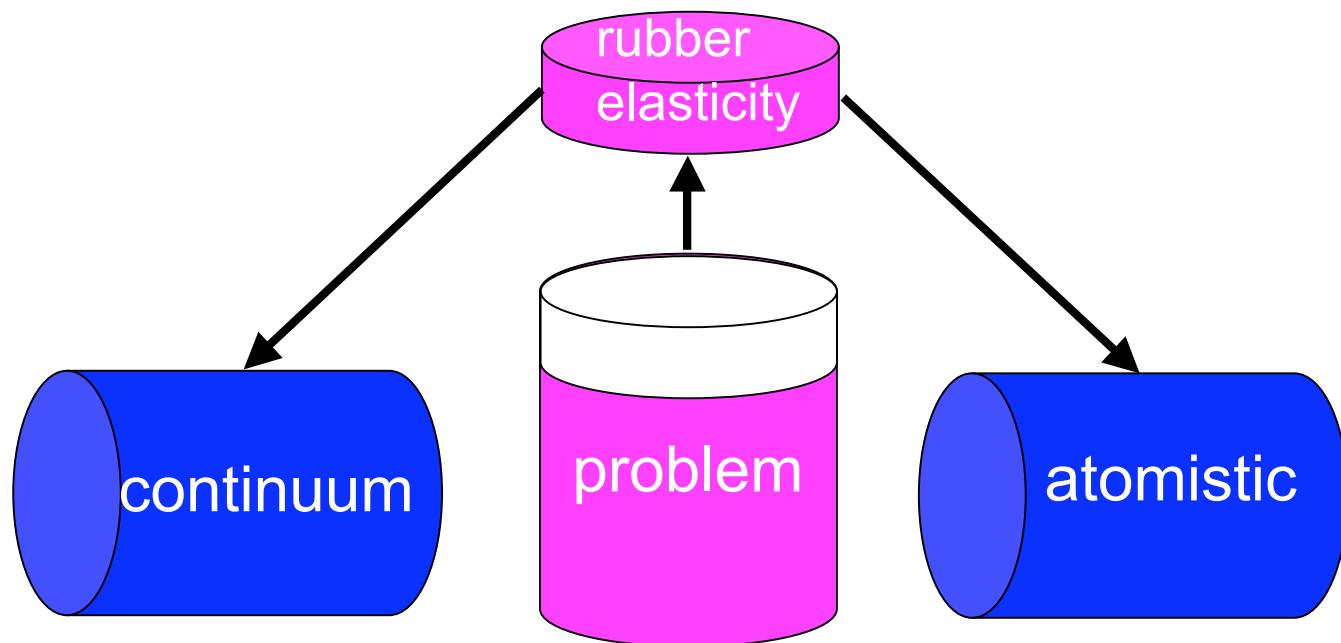


# Motivation

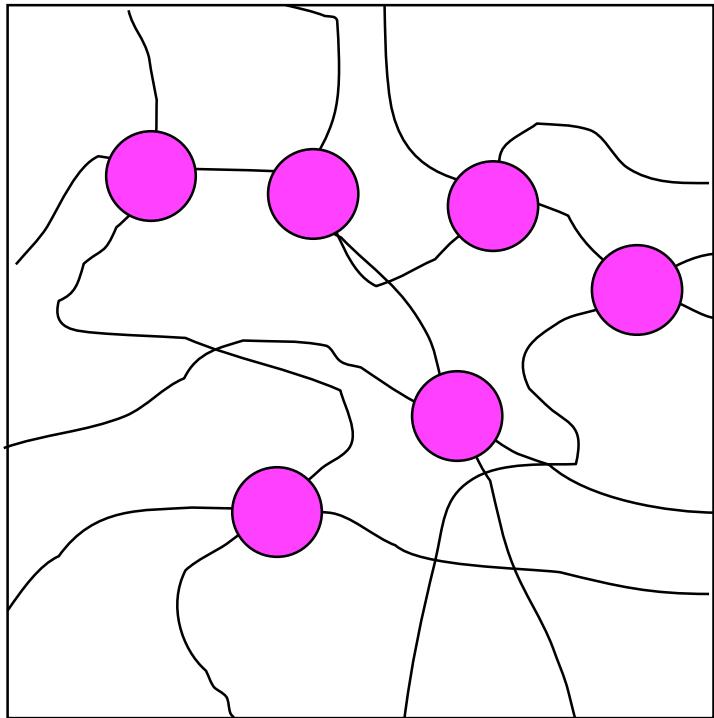


# Map

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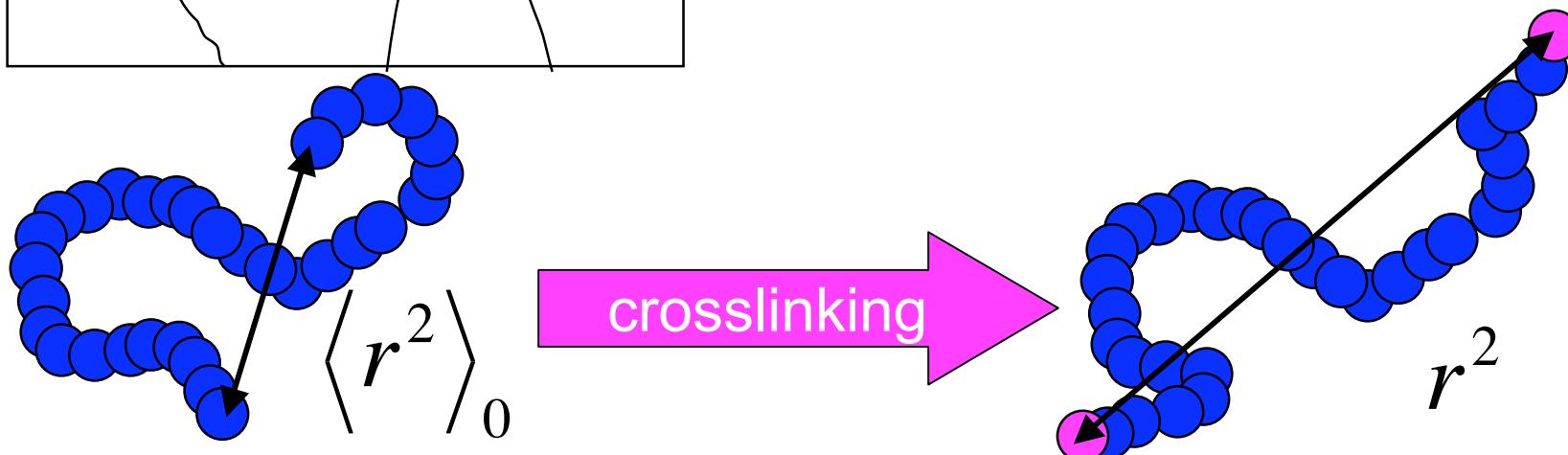


# Rubber Elasticity (Atomistic)



Networks carry stress

$$\frac{F^{el}}{k_B T} = \frac{3}{2} \sum_{chains} \left[ \frac{r_t^2}{\langle r_t^2 \rangle_0} - 1 \right]$$



Changes in the average chain dimensions affect the stress

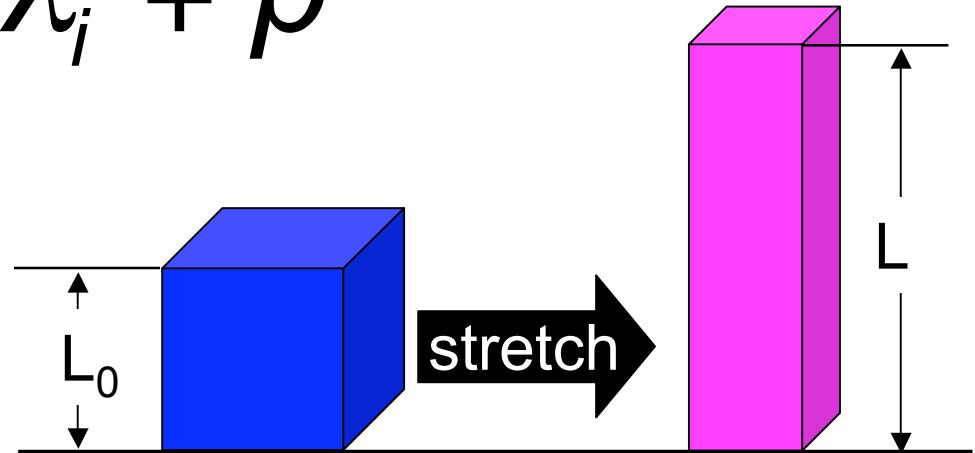
# Rubber Elasticity (Continuum)

$G$ = material-specific modulus

$p$ ~hydrostatic pressure

$$\sigma_i = G\lambda_i^2 + p$$

$$\lambda_i = \frac{L_i}{L_{0i}}$$



Changes in sample dimensions affect the stress

stretched sample

heat

contraction

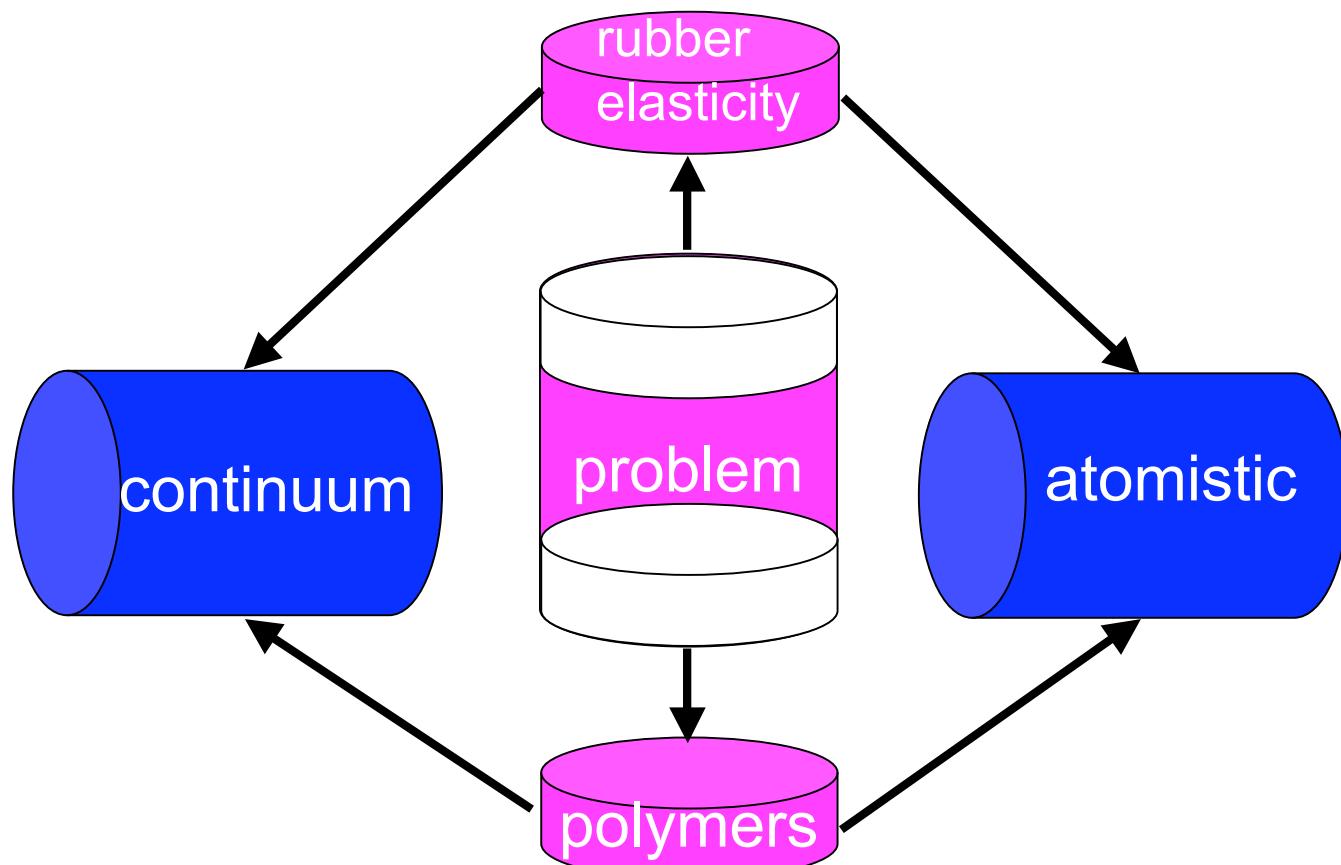
polymer nature

→

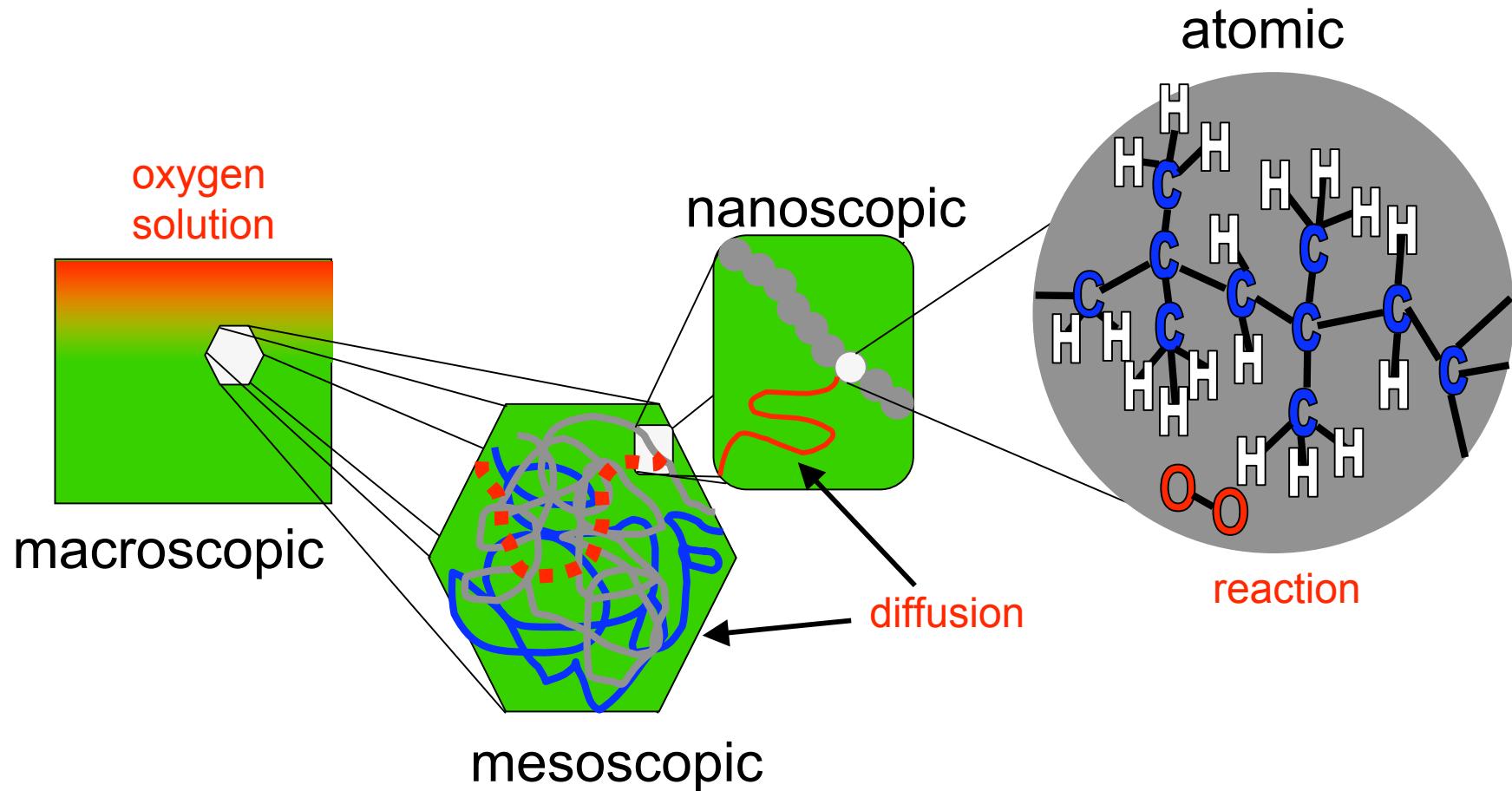
entropic effect

# Map

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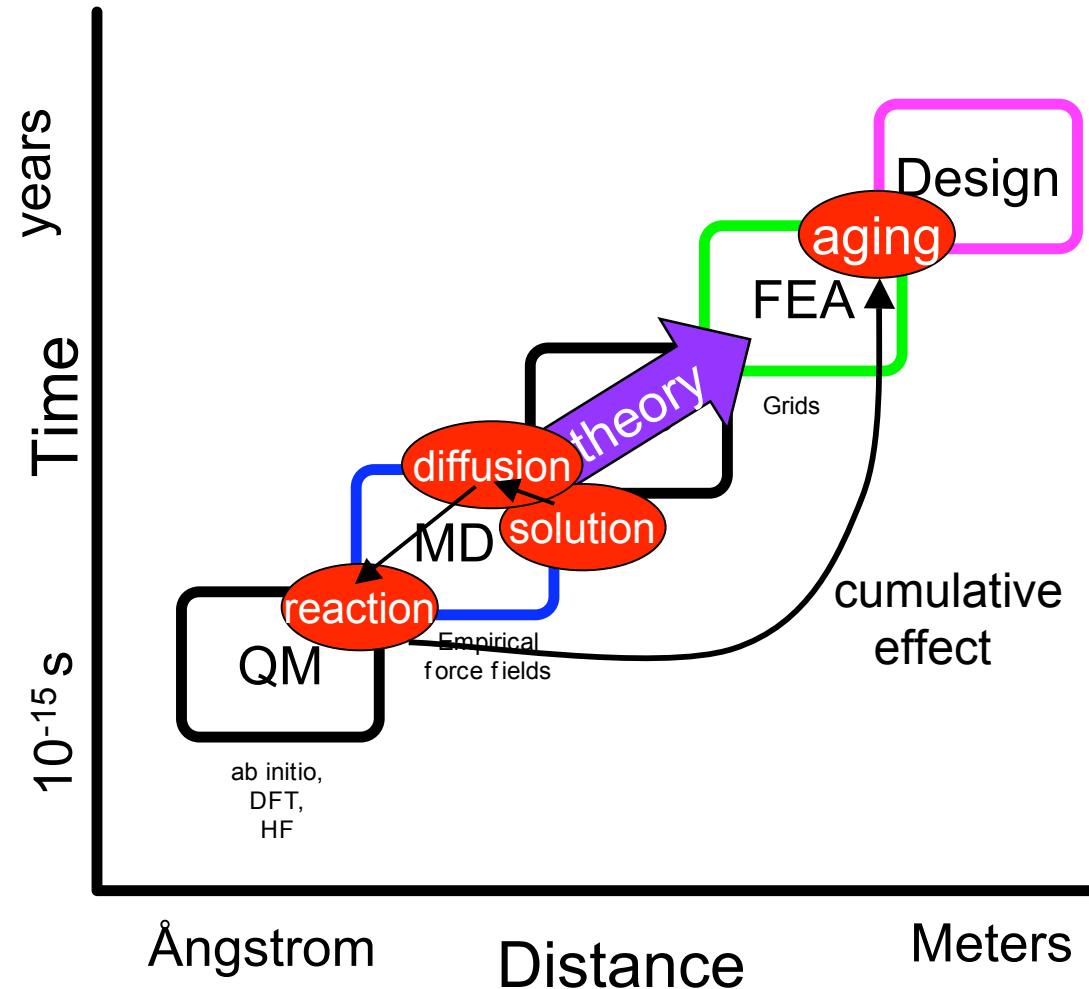
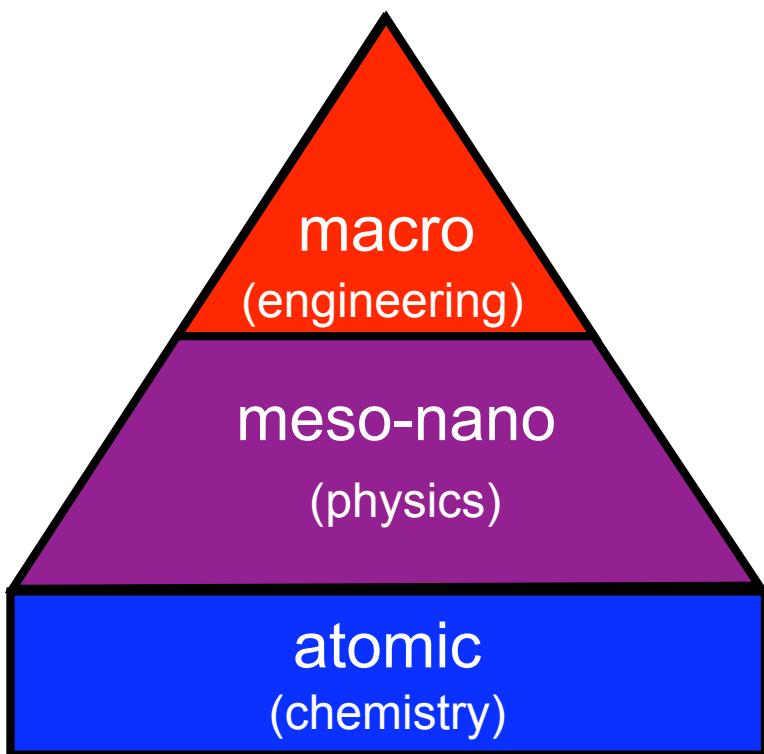
# Goal: Predict Material Properties for Engineering Applications



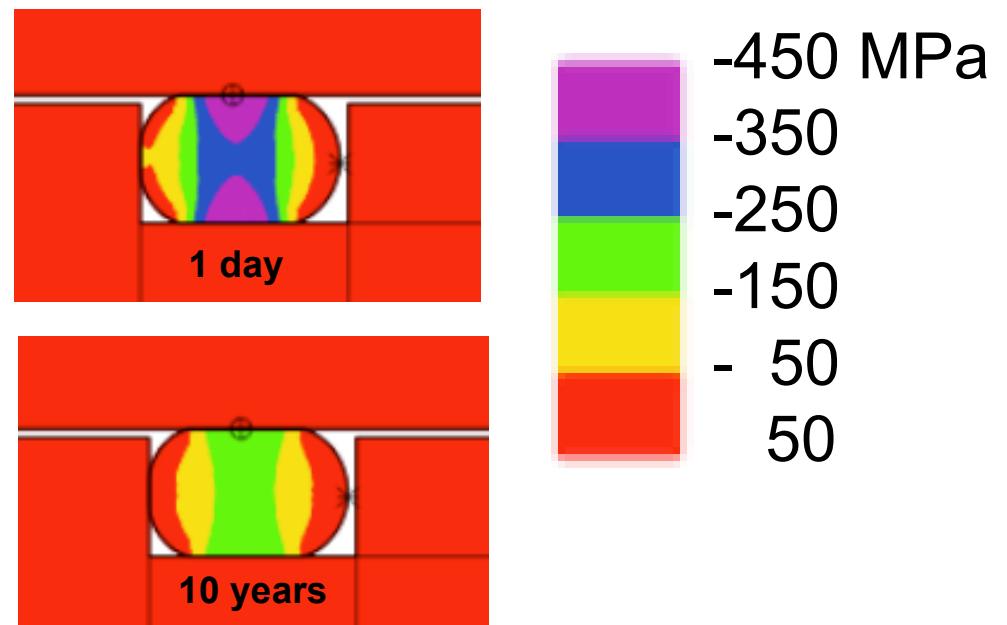
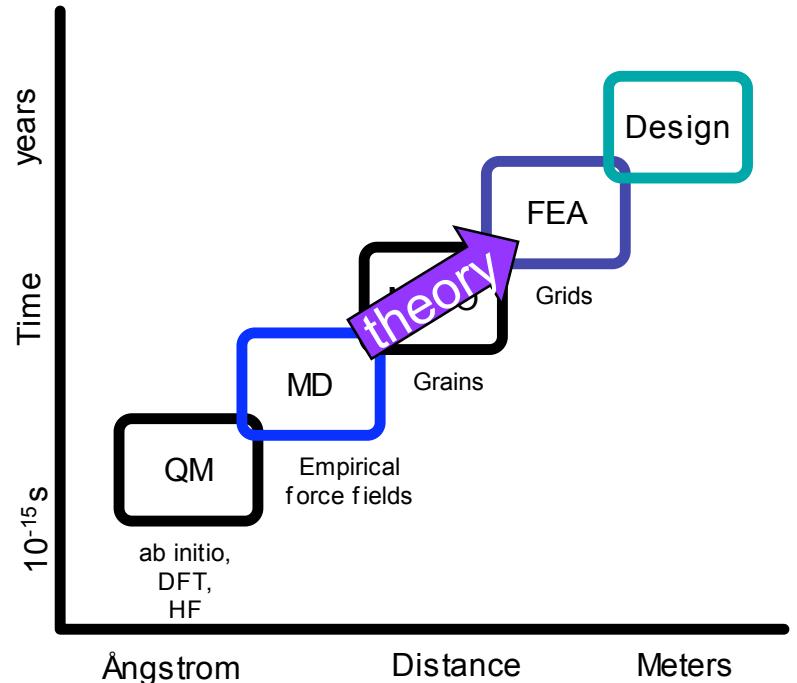
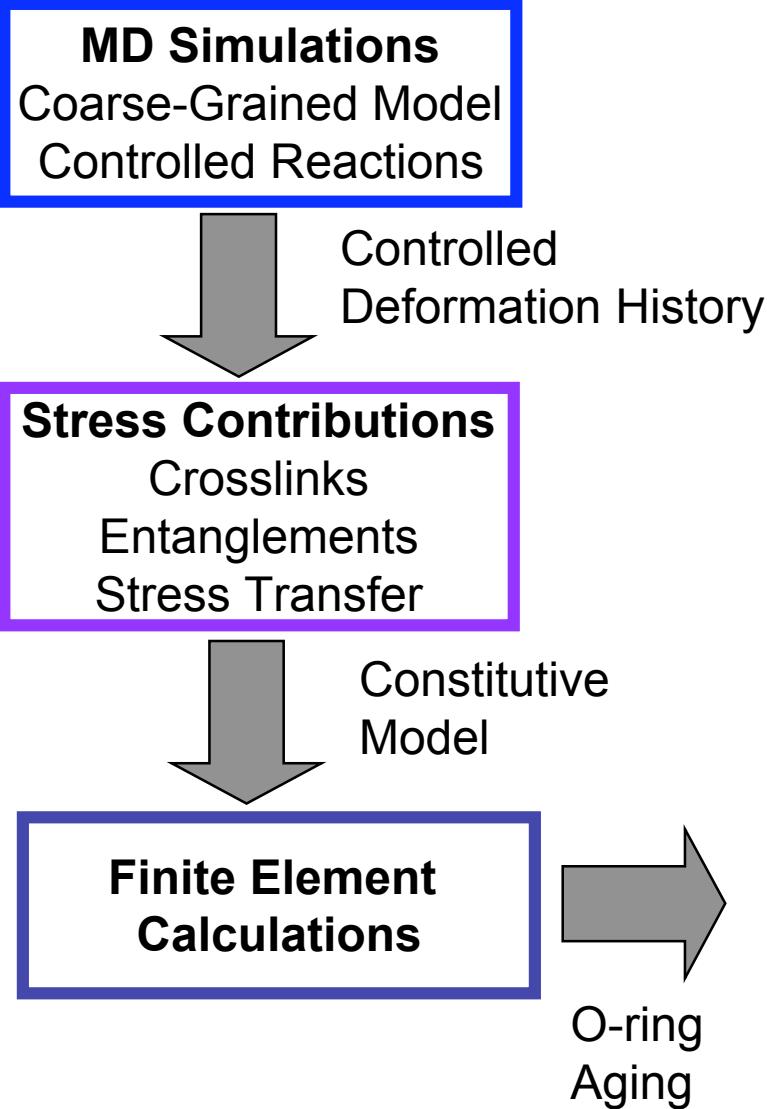
Good predictions at the macroscopic level require knowledge of chemistry and physics at smaller levels!

# Problem: Processes of Interest Span Multiple Scales

## Hierarchical Approach

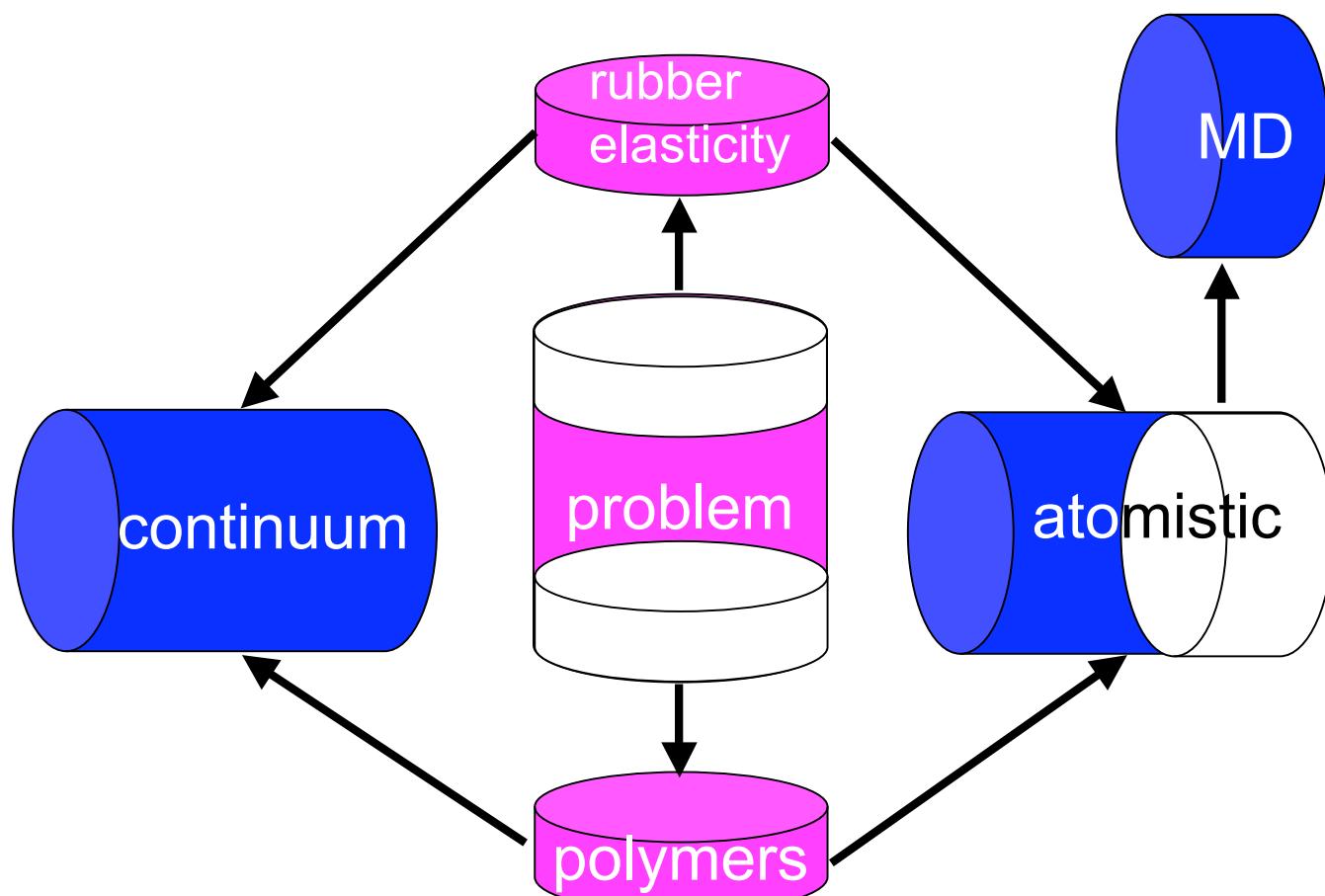


# Strategy



# Map

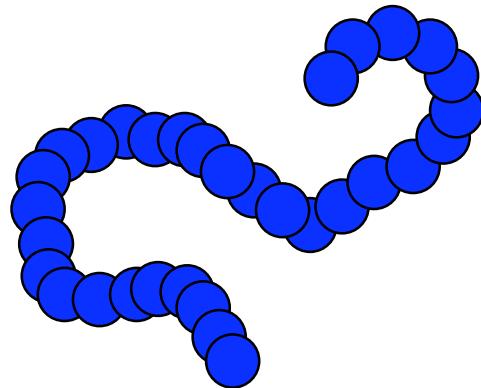
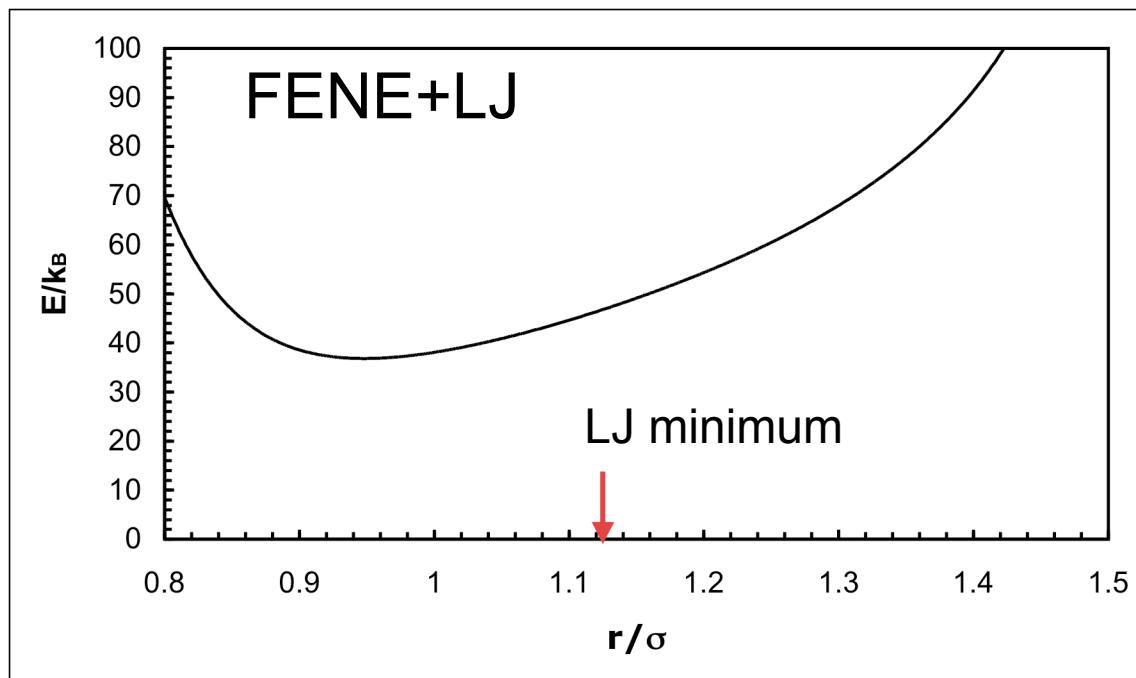
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# Coarse-grained polymers

Essential Physics  
bonded  
excluded volume

$$U_{LJ} = 4\epsilon \left[ \left( \frac{\sigma}{r} \right)^{12} - \left( \frac{\sigma}{r} \right)^6 \right] + \epsilon \quad r \leq 2^{1/6} \sigma$$
$$U_{LJ} = 0 \quad r > 2^{1/6} \sigma$$
$$U_{FENE} = -\frac{HR_0^2}{2} \ln \left[ 1 - \frac{r}{R_0} \right] \quad r < R_0$$
$$U_{FENE} = \infty \quad r \geq R_0$$



# MD System Specifics

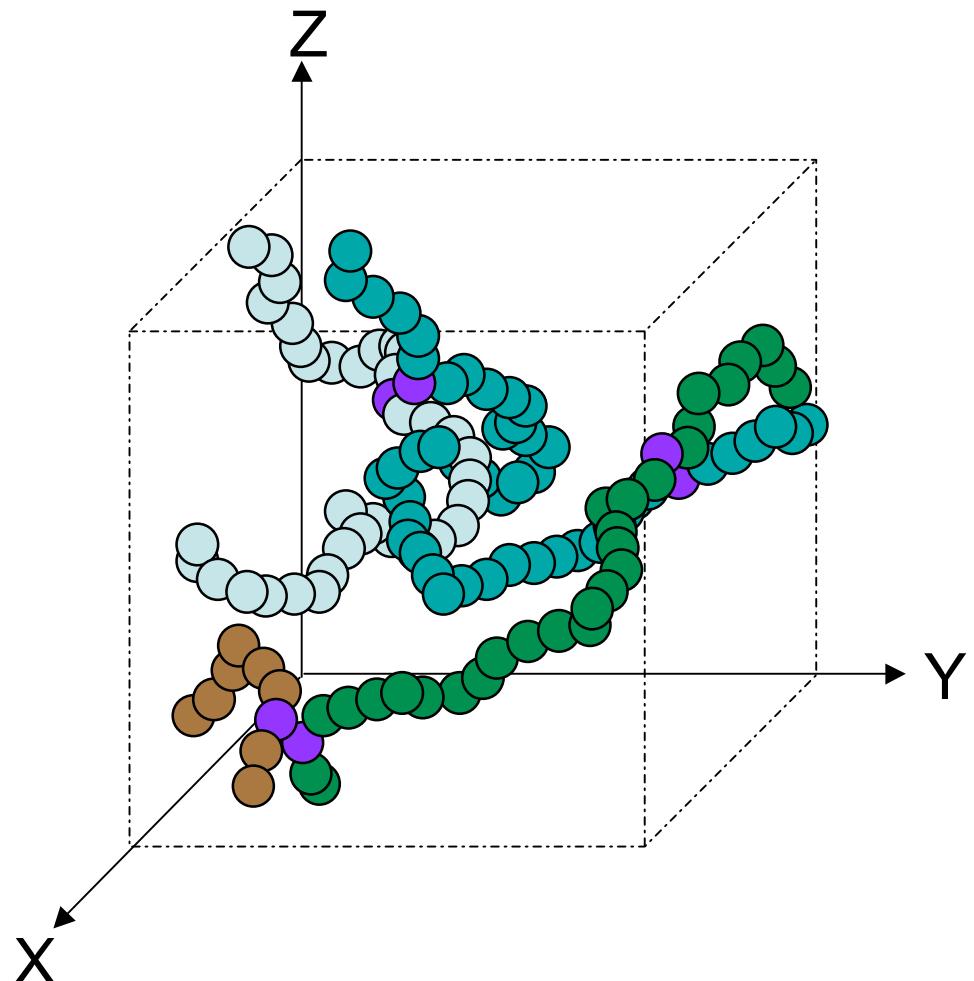
500 chains, 500 sites each, 20 reactive sites/chain

$\rho=0.85$  sites/volume

$T^*=1.0$

1. Equilibrate
2. React
3. Equilibrate
4. Deform
5. Equilibrate
6. React
7. Equilibrate

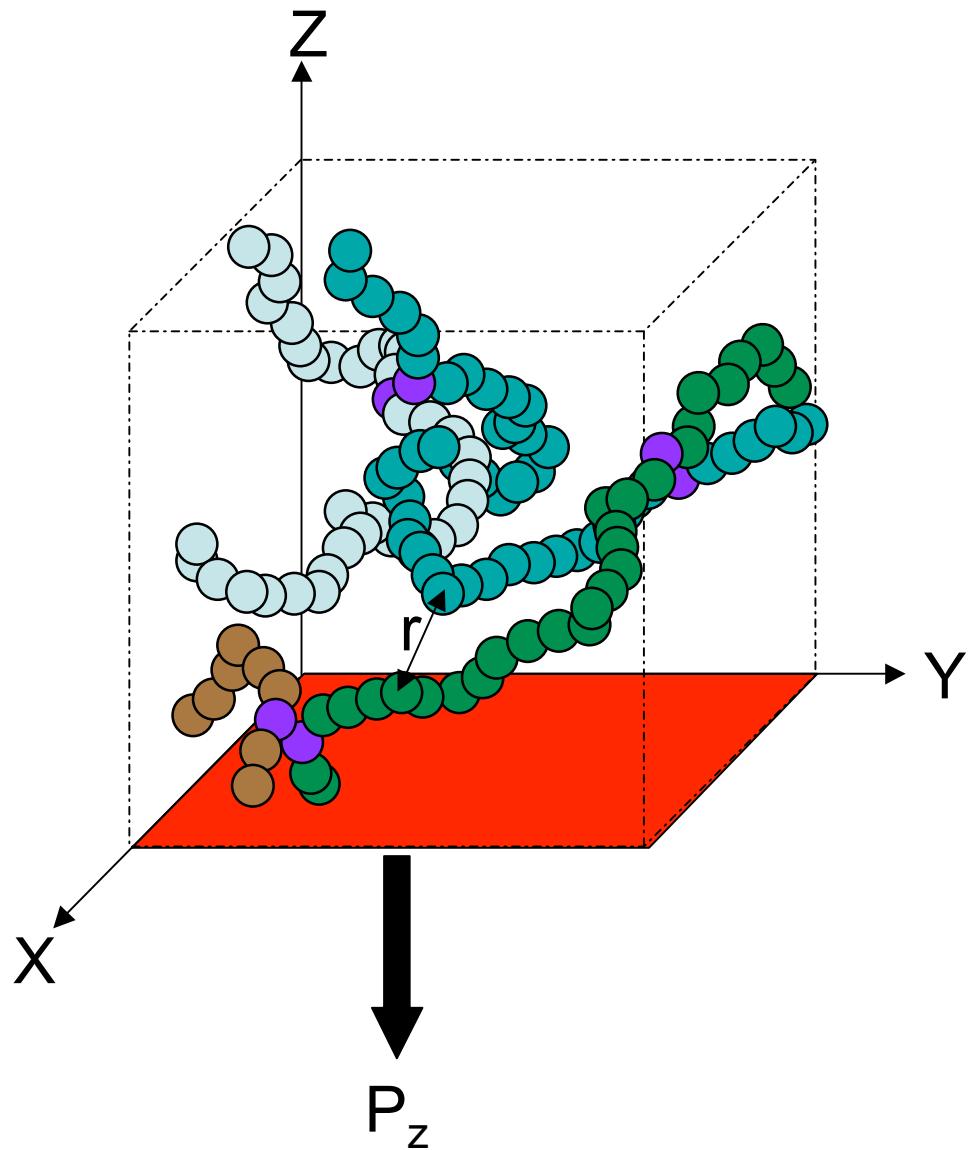
LAMMPS



# Stress from MD

$$P = \left\langle \rho k_B T + \frac{1}{3V} \sum_i \sum_{j>i} \mathbf{r}_{ij} \cdot \mathbf{f}_{ij} \right\rangle$$

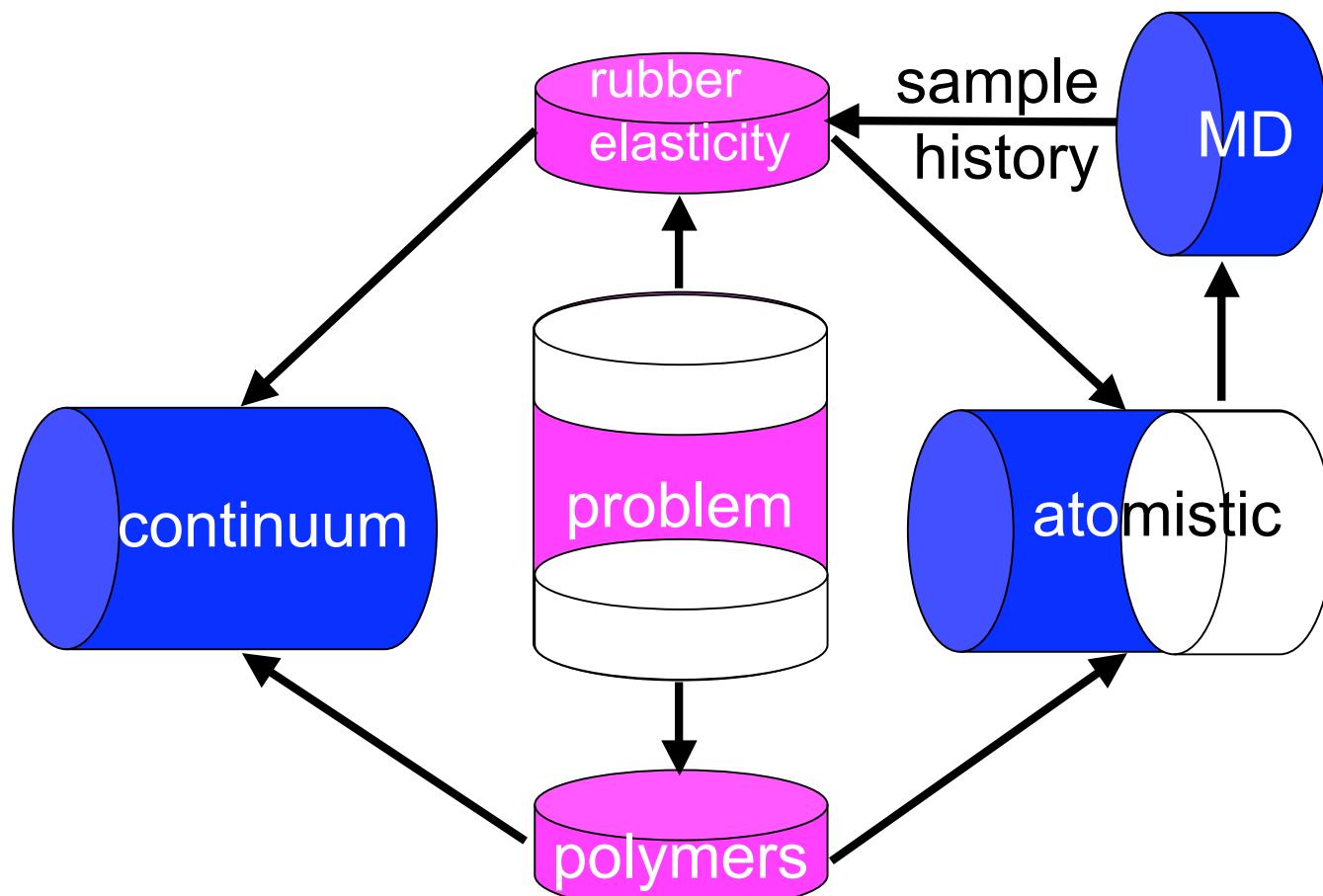
$$\sigma_{zz}^{dev} = P_z - \frac{1}{3} \text{Tr} \underline{\underline{P}}$$



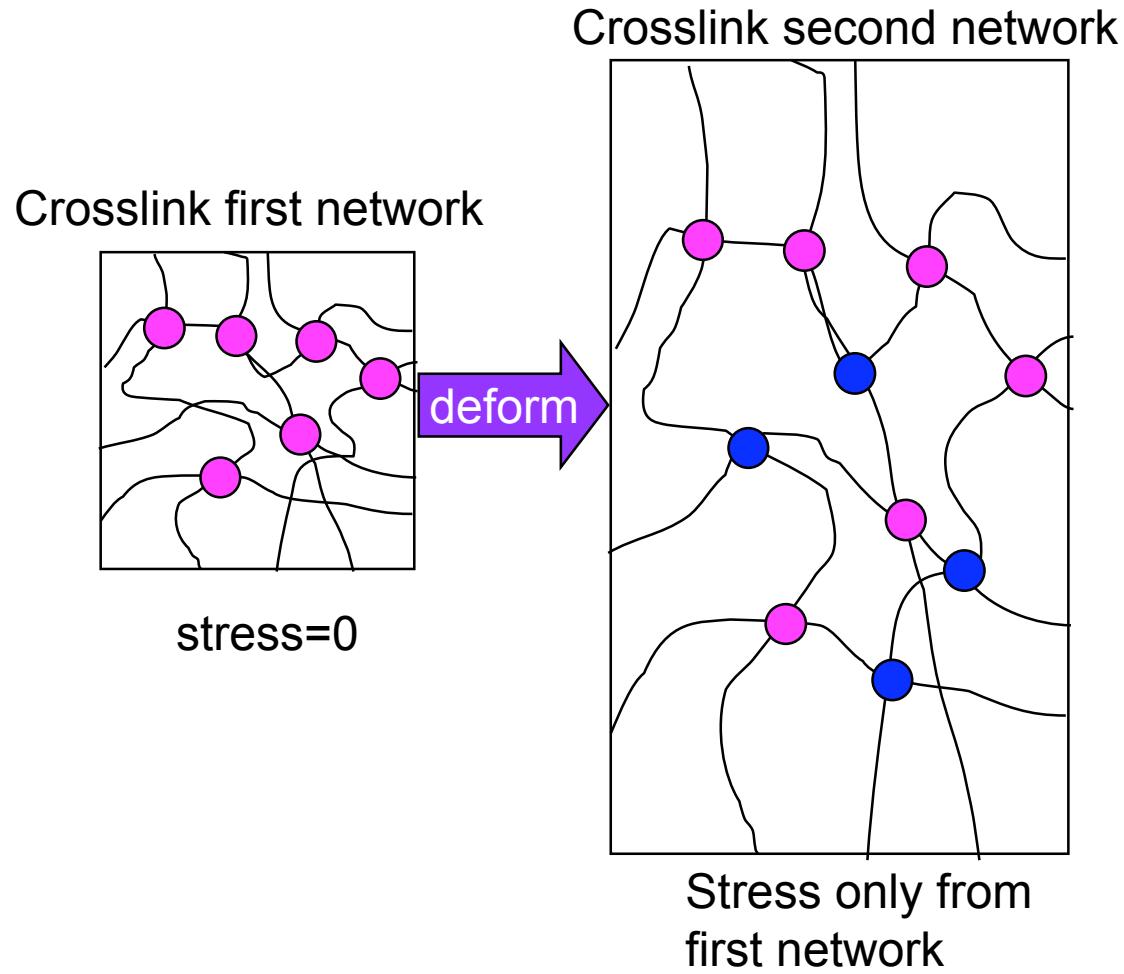
Calculate stress components from pressure components

# Map

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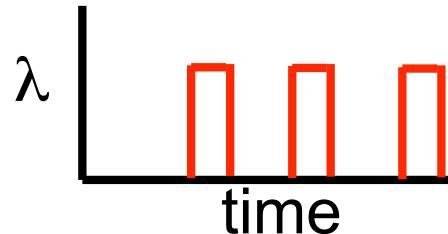
# Independent Network Hypothesis



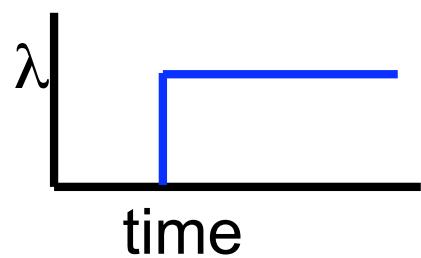
Reaction and strain histories are coupled

# Experimental Data for INH

Intermittent: hold unstrained,  
periodic check of strained stress

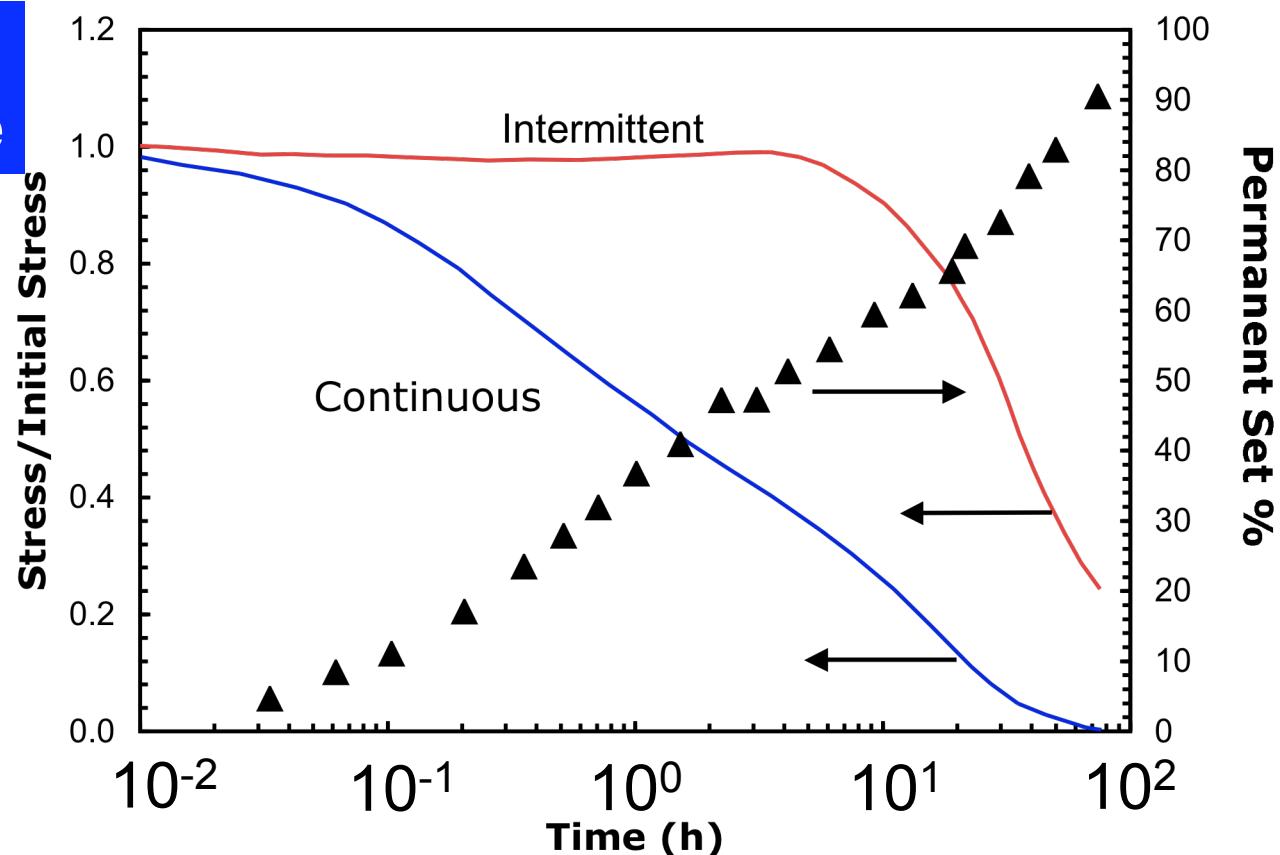
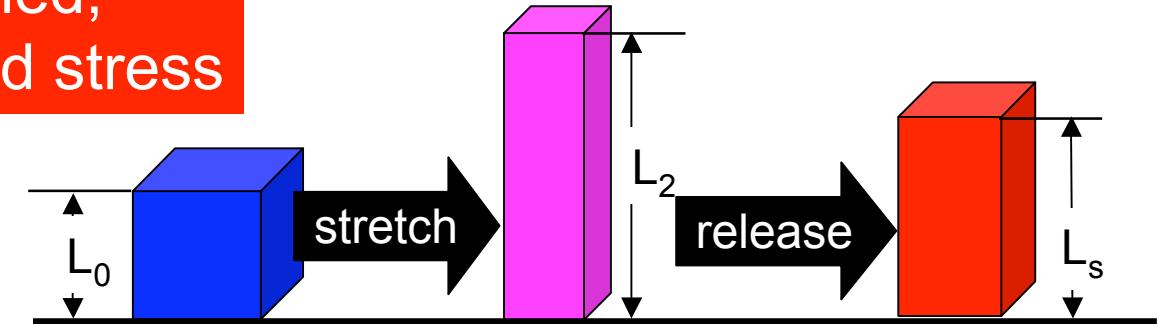


Continuous:  
hold in strained state



Butyl Rubber  
 $130^{\circ}\text{C}$ ,  $\lambda=1.5$

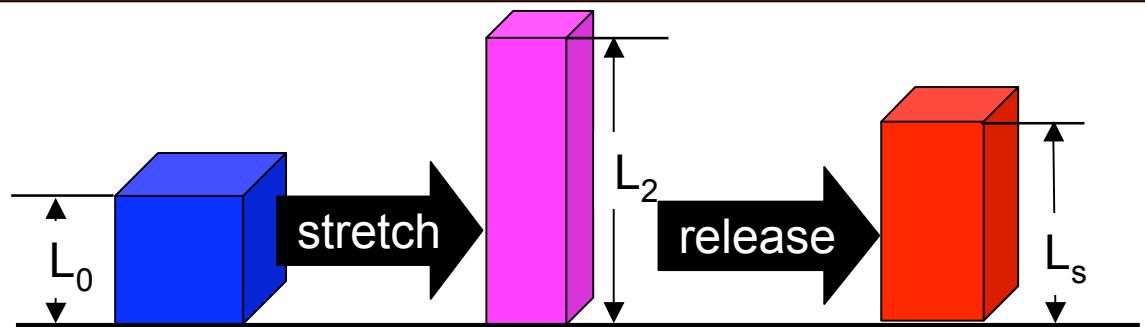
Andrews, Tobolsky, Hanson  
J. Appl. Phys. 17, 352 (1946)



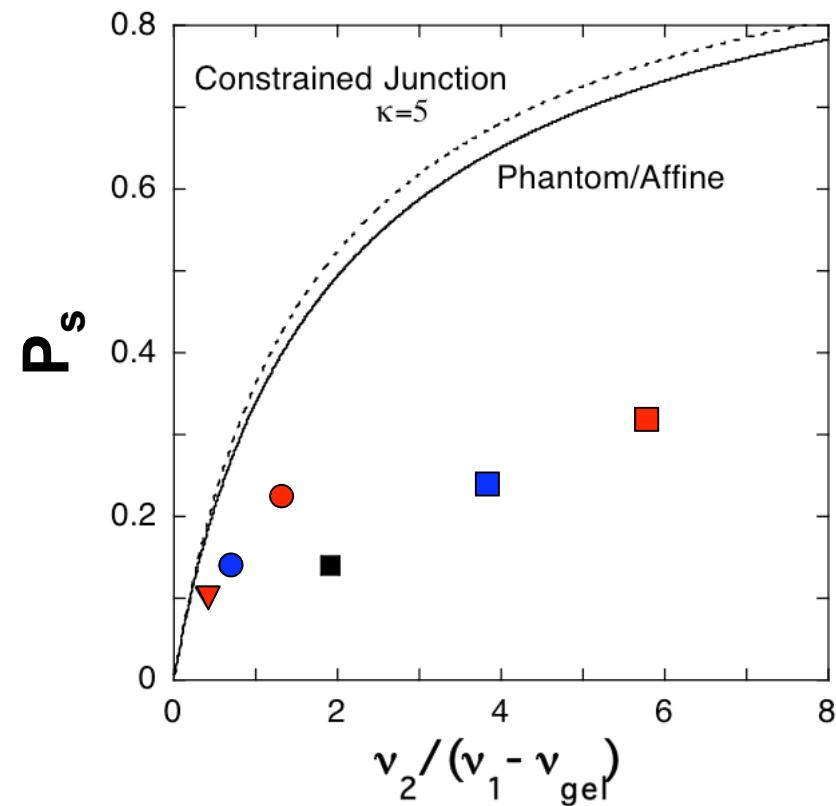
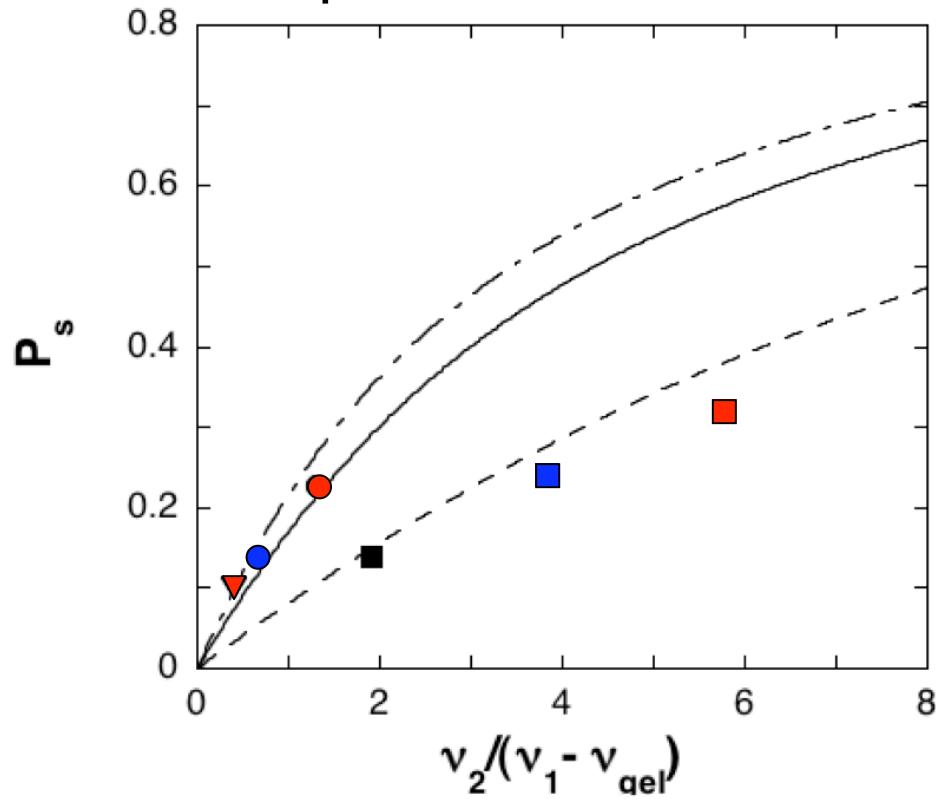
# Permanent Set from MD

## Uniaxial extension

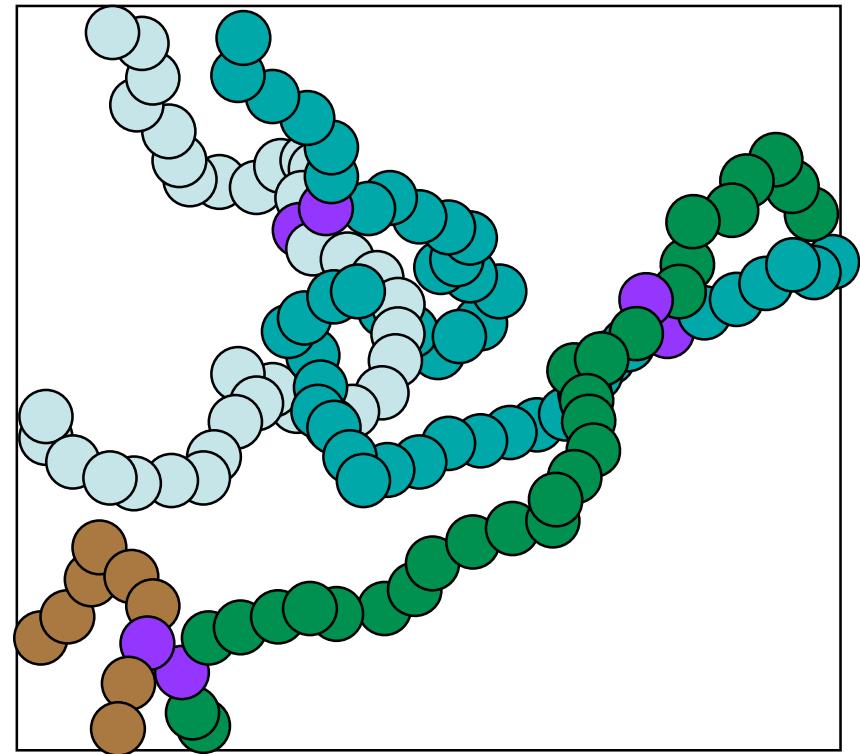
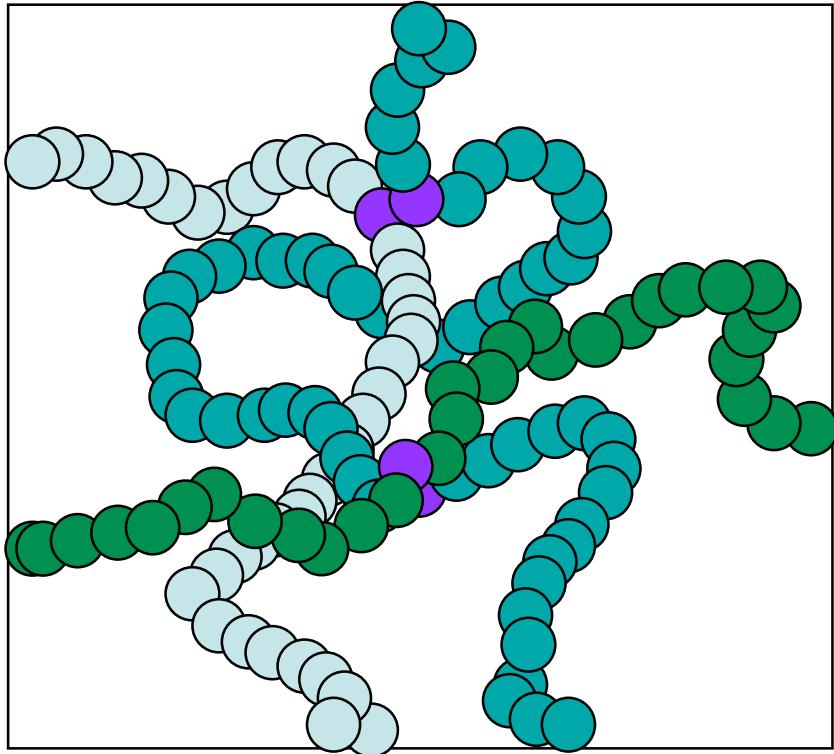
$$P_s = \frac{\lambda_s - \lambda_0}{\lambda_2 - \lambda_0}$$



## Slip-tube model

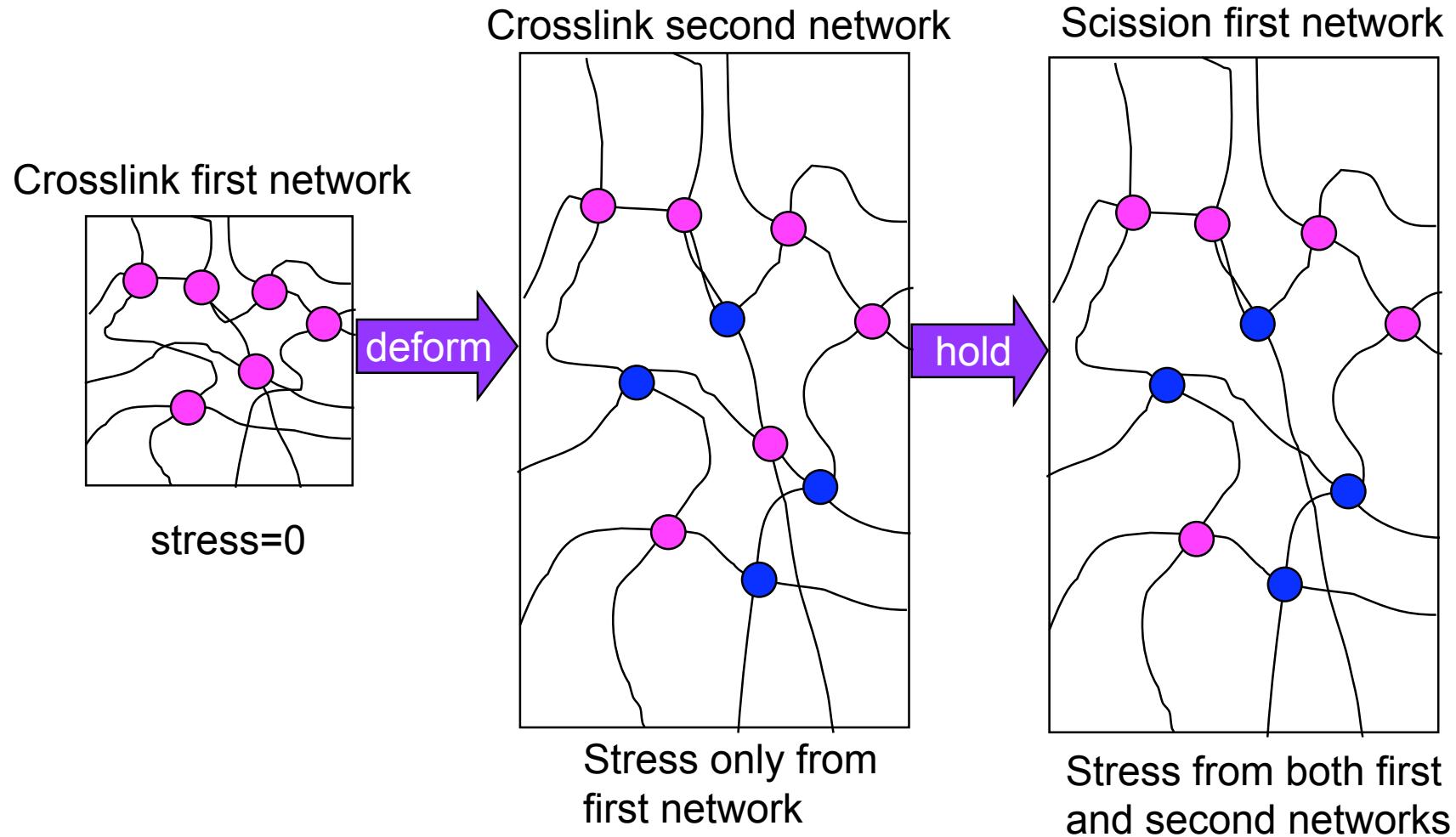


# Entanglements



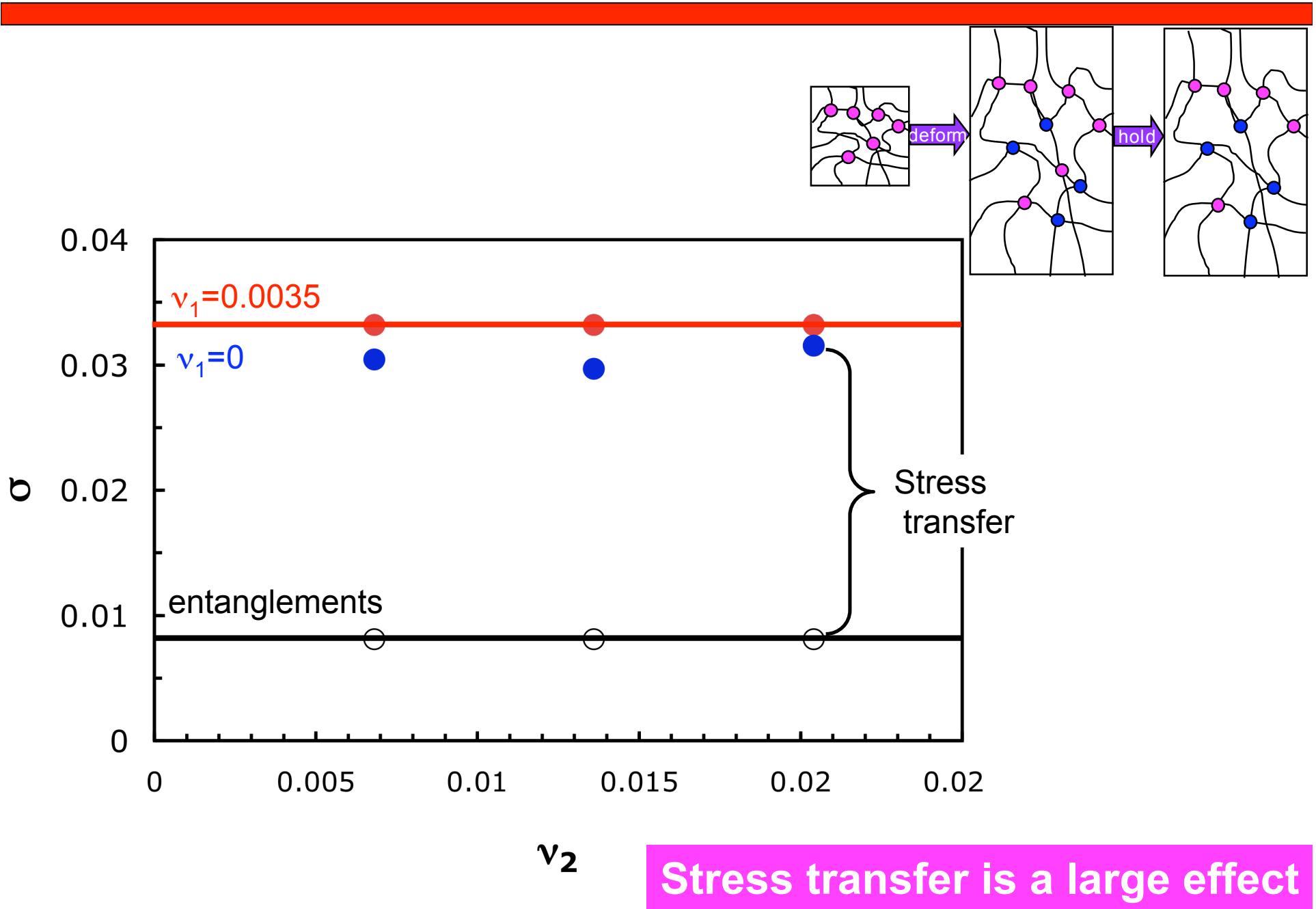
Trapped entanglements also contribute to stress

# Independent Network Hypothesis (Revisited)



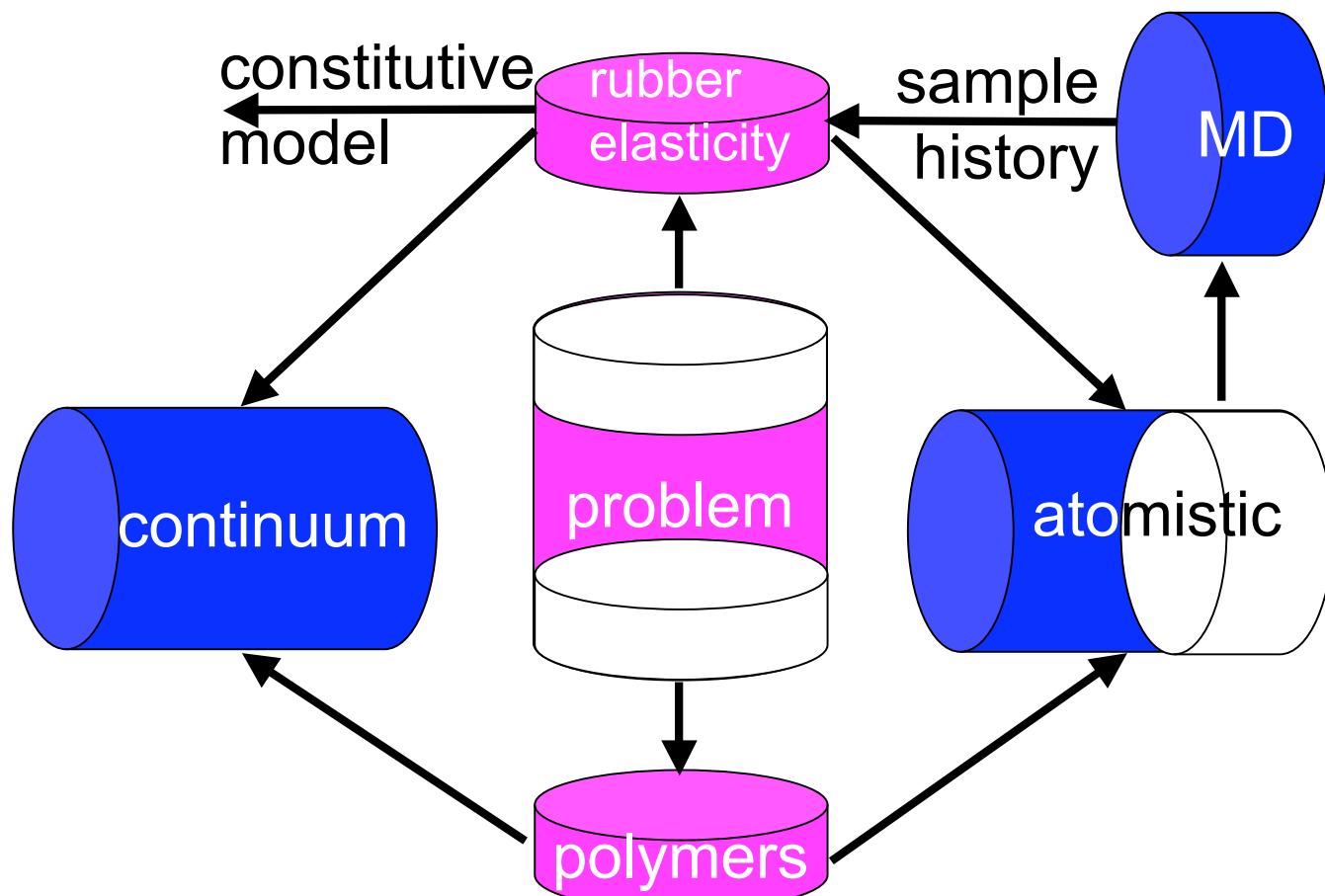
Sample retains memory of crosslinking and strain history

# MD Simulation with Scission

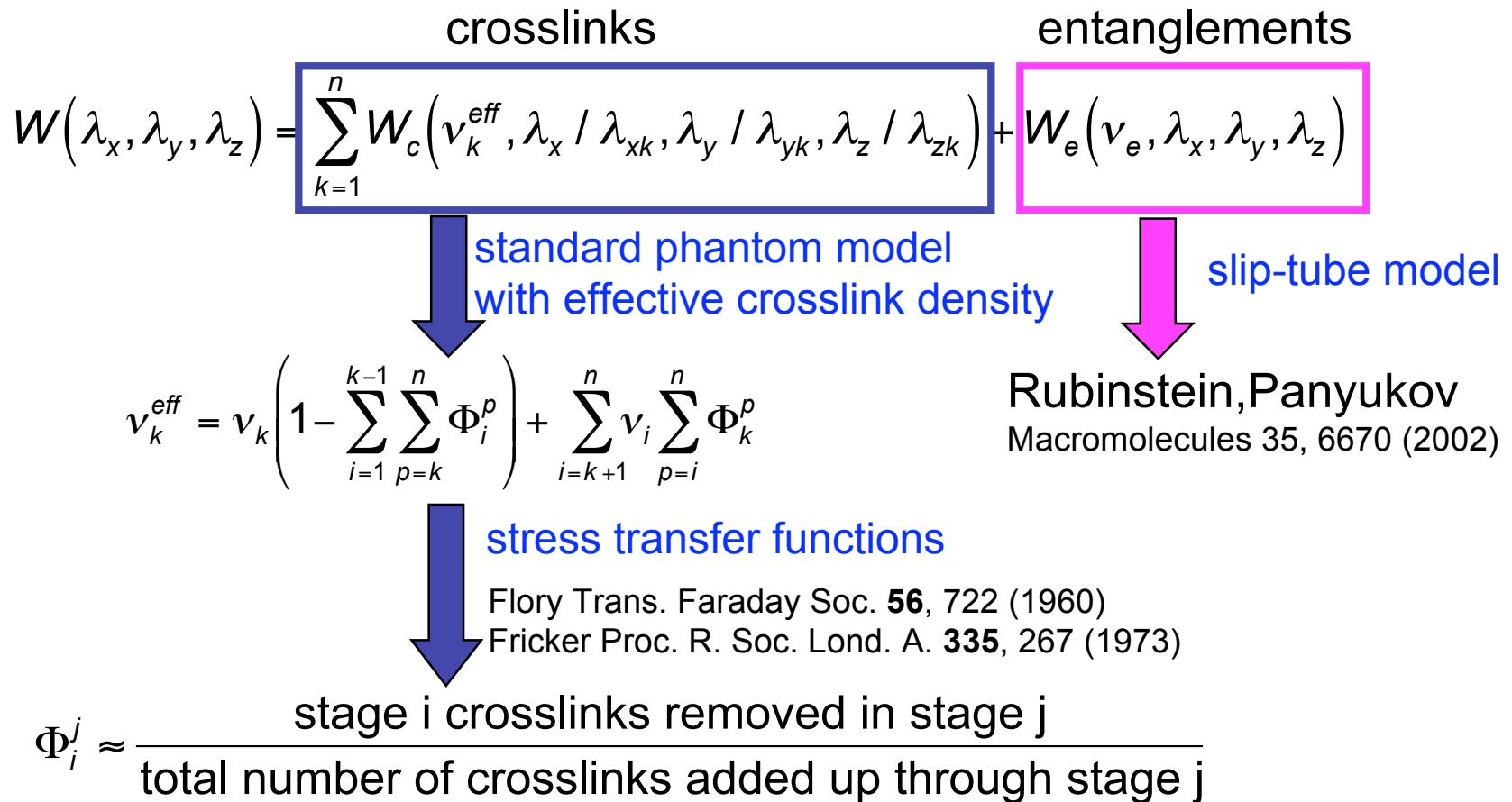


# Map

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# General Constitutive Model



Use independent network hypothesis to formulate strain energy.  
Use common form of principal stretches.

# Entanglement Network

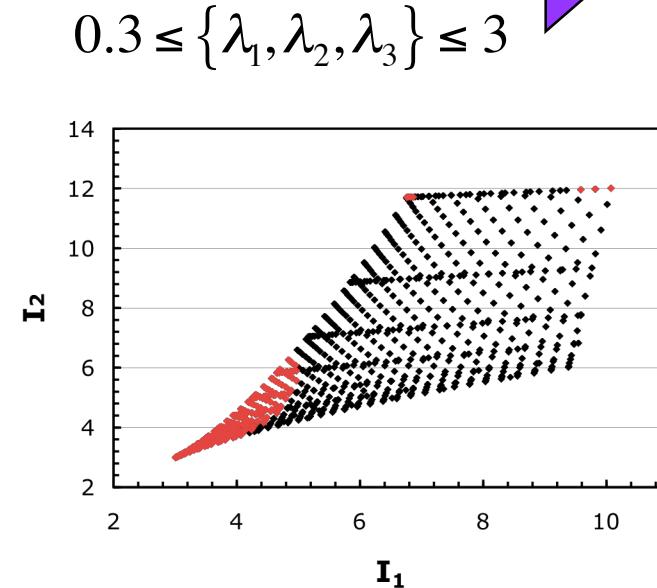
Sample most likely between 30% and 300% of original dimensions

Slip-tube model  
computationally demanding  
for arbitrary strain

$$W = \frac{A}{2} \sum_{\alpha} \left( \frac{\lambda_{\alpha}}{\sqrt{g_{\alpha}}} + \frac{\sqrt{g_{\alpha}}}{\lambda_{\alpha}} \right) - \frac{A}{3} \sum_{\alpha} \ln \left( \frac{Ng_{\alpha}}{L} \right)$$

Rubinstein, Panyukov  
Macromolecules 35, 6670 (2002)

fit strain energy  
for expected deformations



Use invariant fit in FE  
to calculate stress

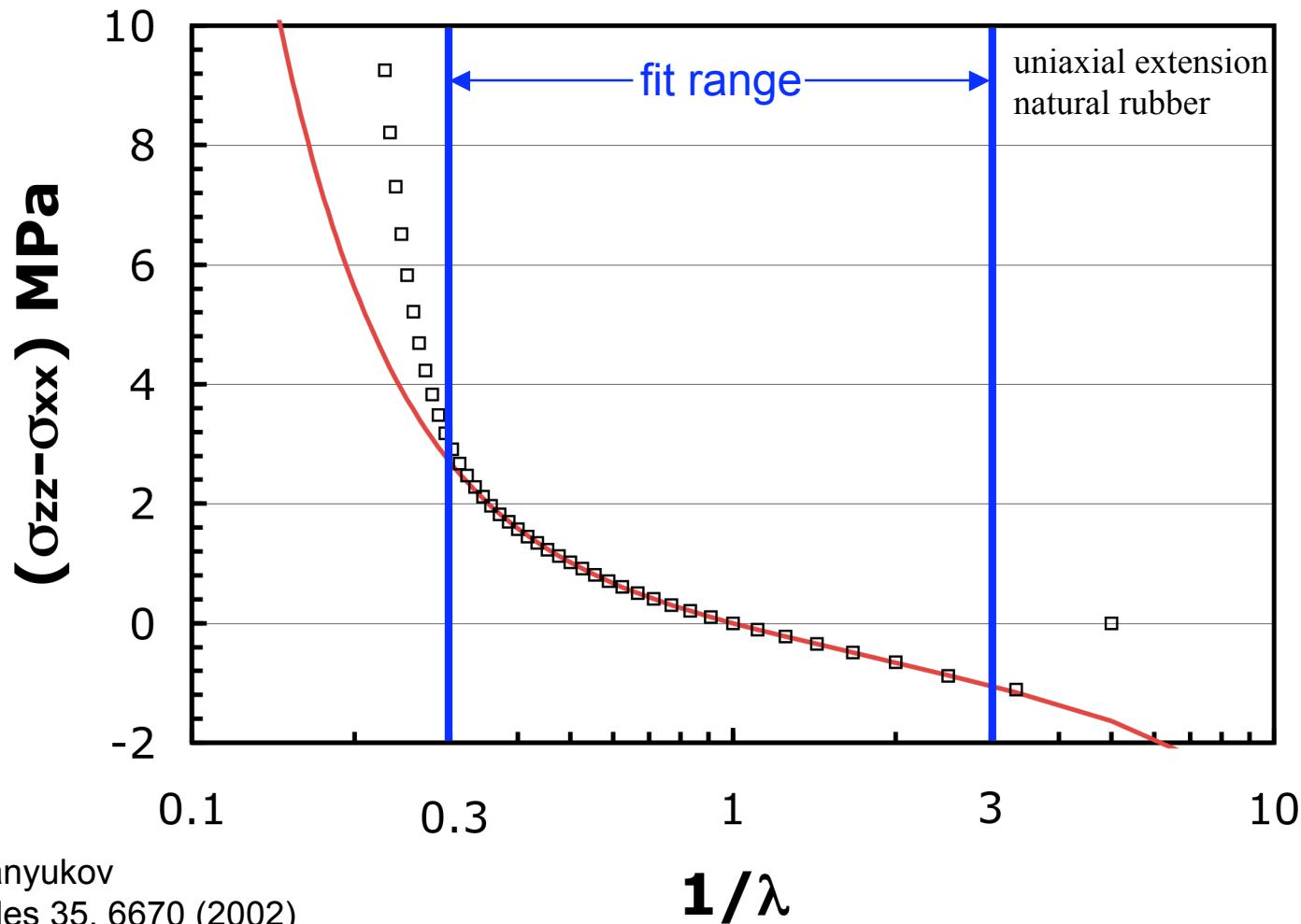
$$W = \sum_{i=1}^3 \sum_{k=1}^3 c_{ik} (I_1 - 3)^i (I_2 - 3)^k$$

$$I_1 = \lambda_1^2 + \lambda_2^2 + \lambda_3^2$$

$$I_2 = \lambda_1^2 \lambda_2^2 + \lambda_2^2 \lambda_3^2 + \lambda_3^2 \lambda_1^2$$

MD shows that only first stage networks trap entanglements

# Comparing W to Experiment

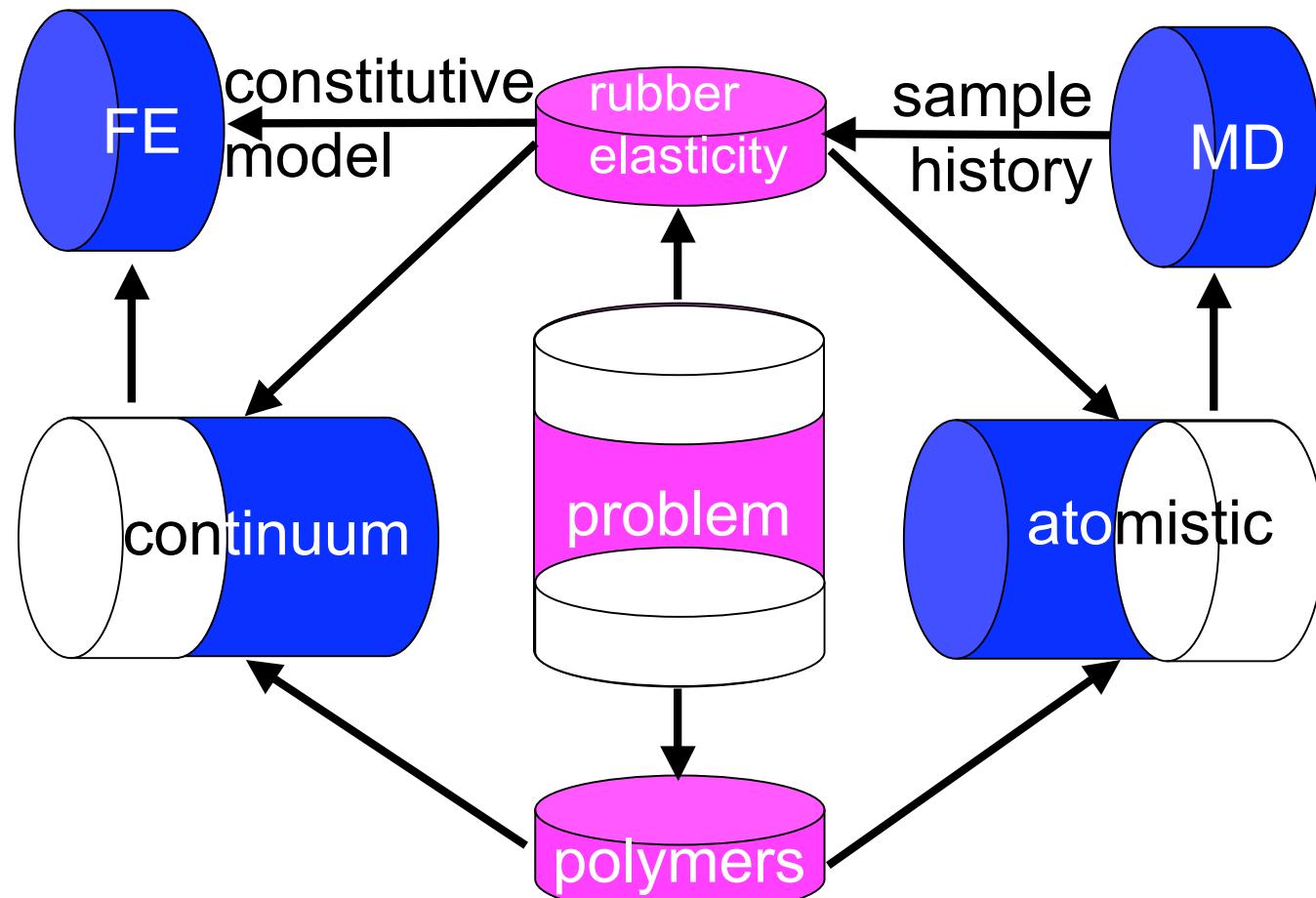


Rubinstein,Panyukov  
Macromolecules 35, 6670 (2002)

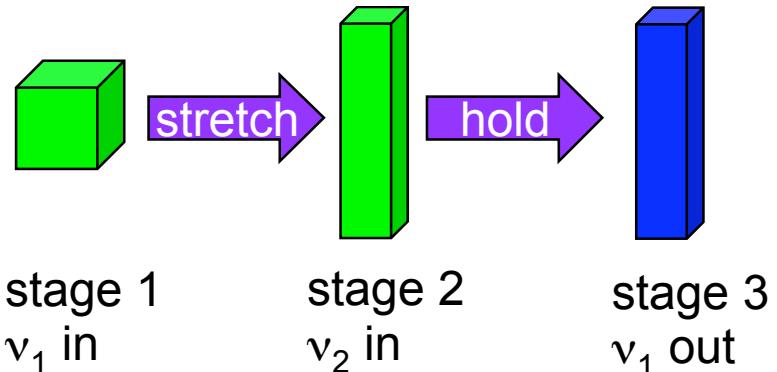
**Strain energies were fit to  $0.3 \leq \{\lambda_1, \lambda_2, \lambda_3\} \leq 3$  (arbitrary deformation)**  
**Good agreement found between prediction and experiment**

# Map

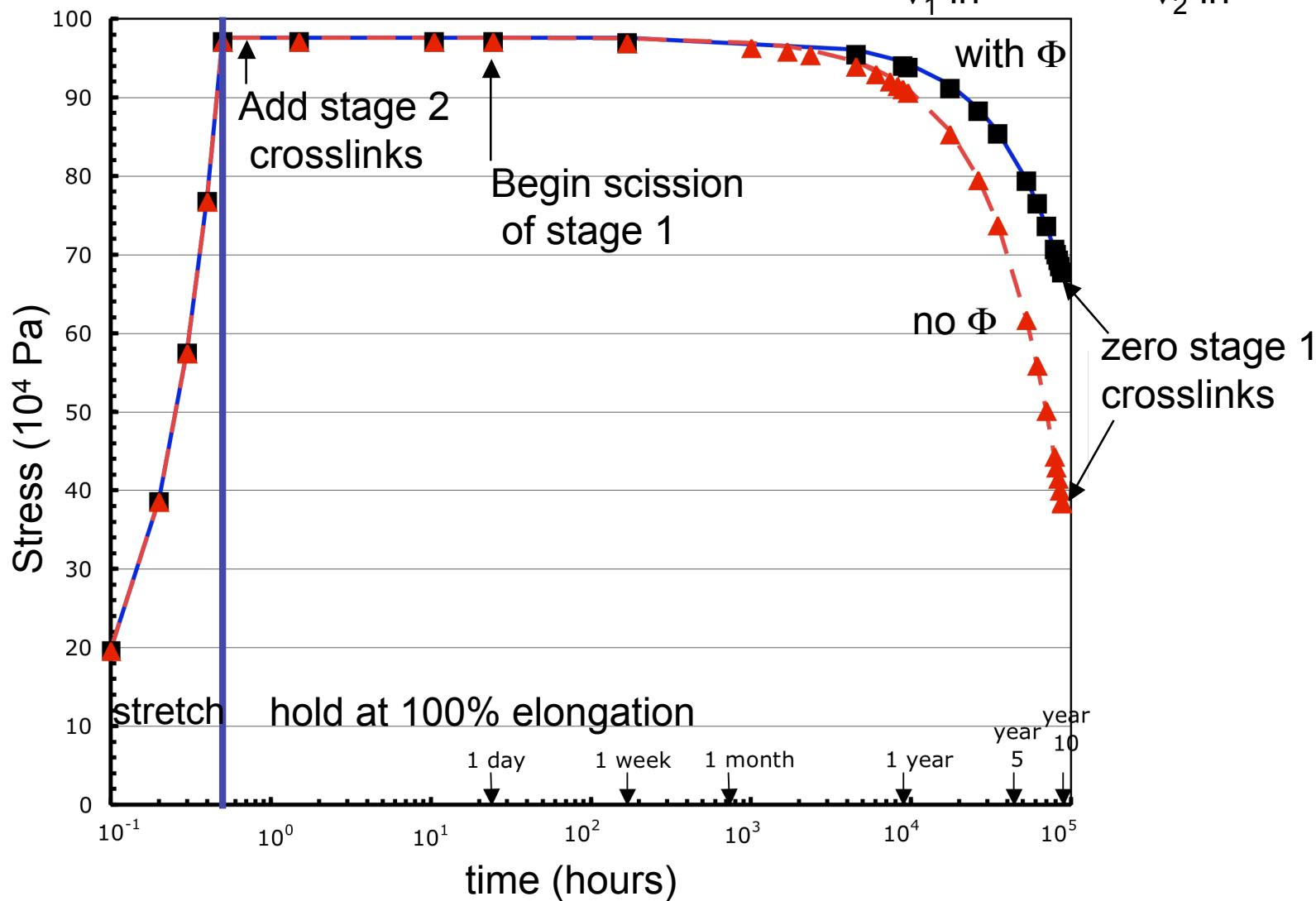
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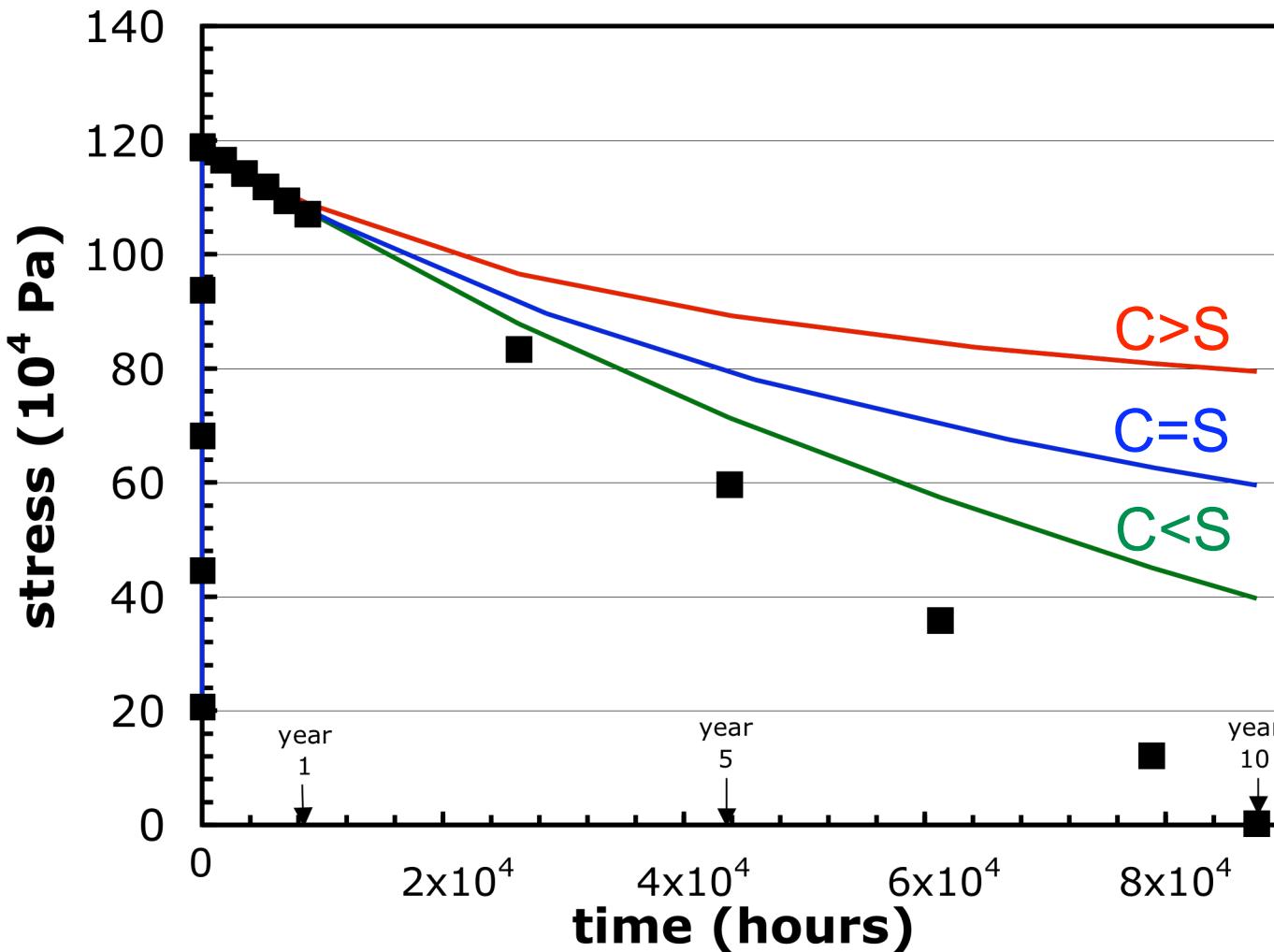
# Finite Element



Final stress 80% higher using  $\Phi$



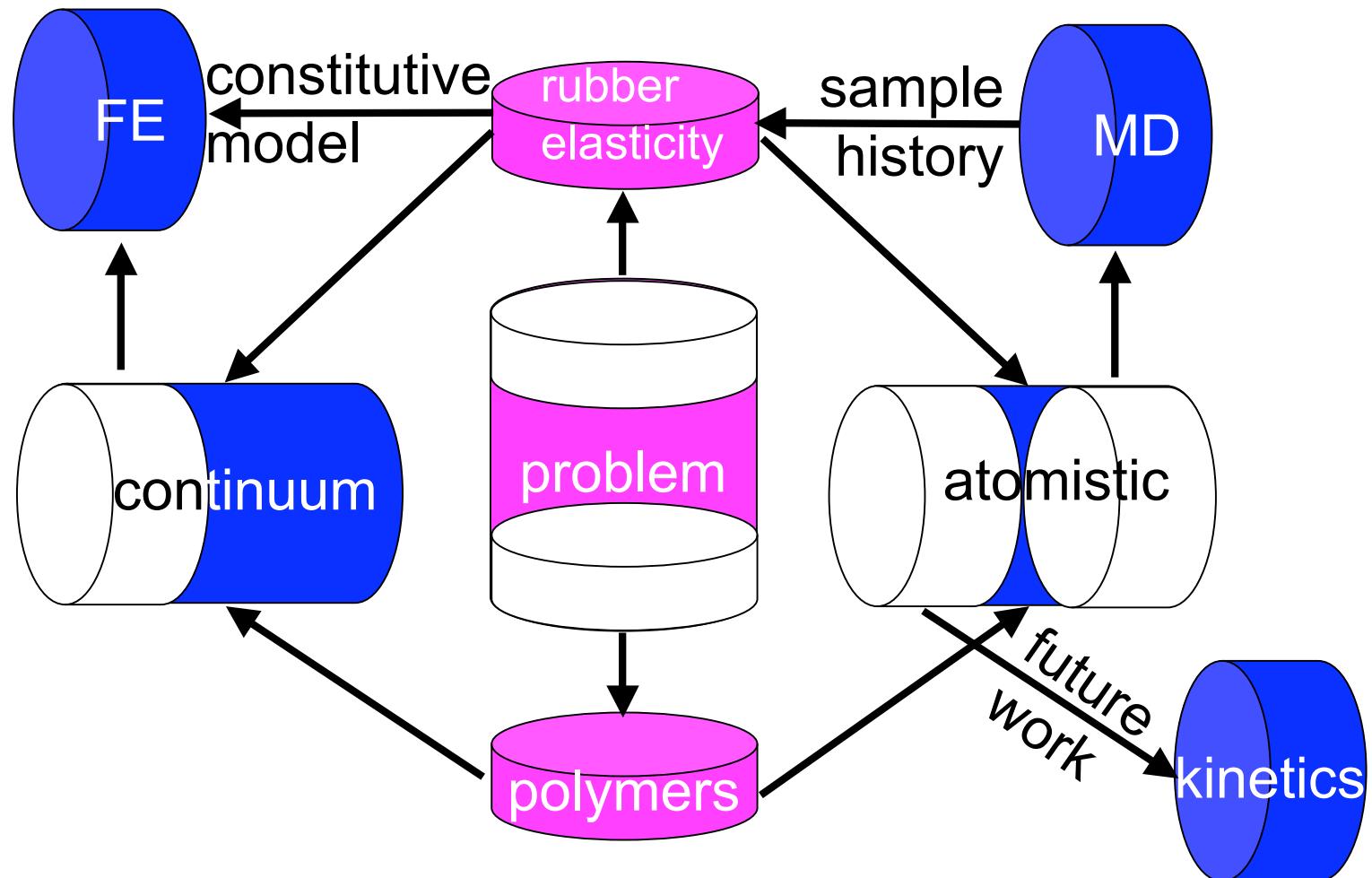
# Simultaneous Crosslinking and Scission



Relative rates of scission and crosslinking make a large difference in the resulting stress

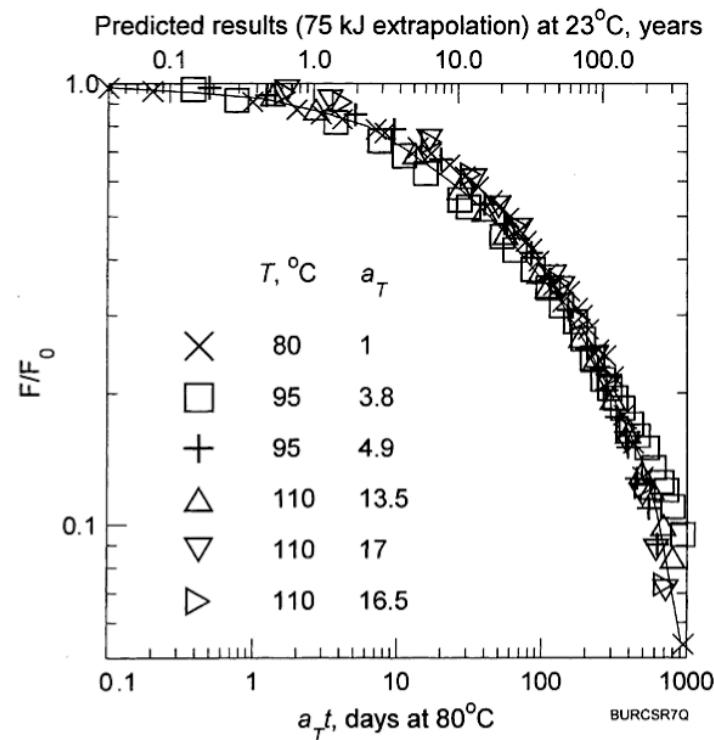
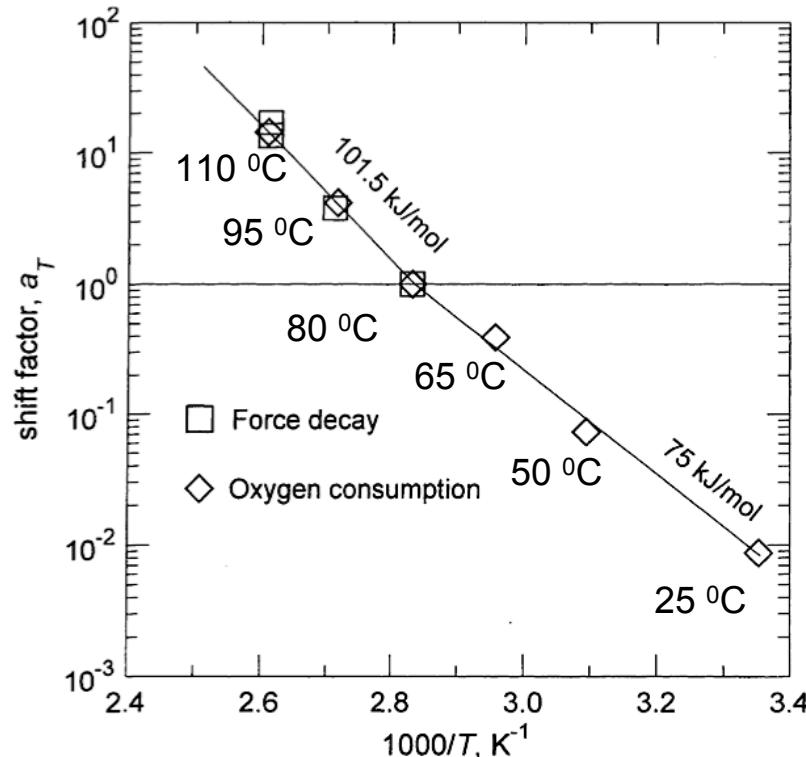
# Map

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# Experimental Kinetics

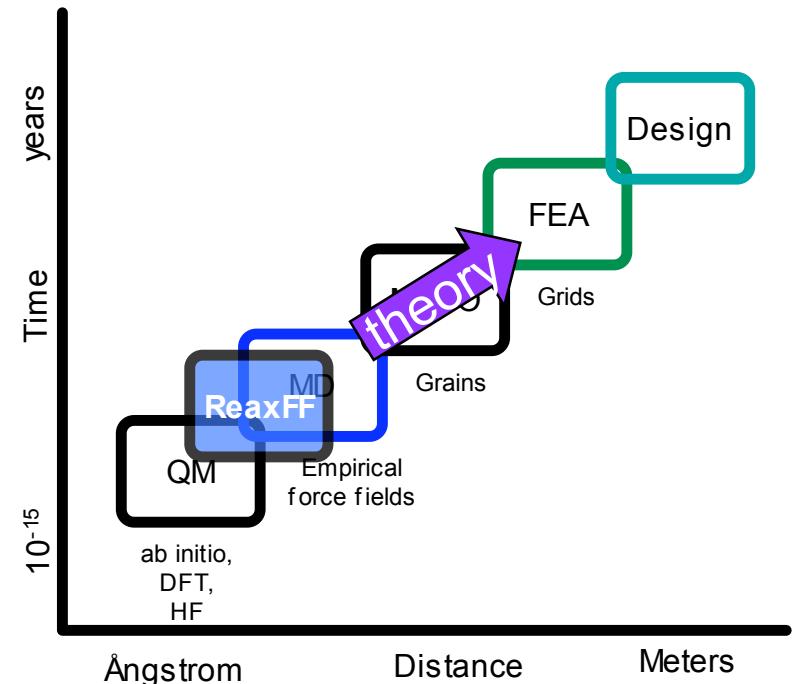
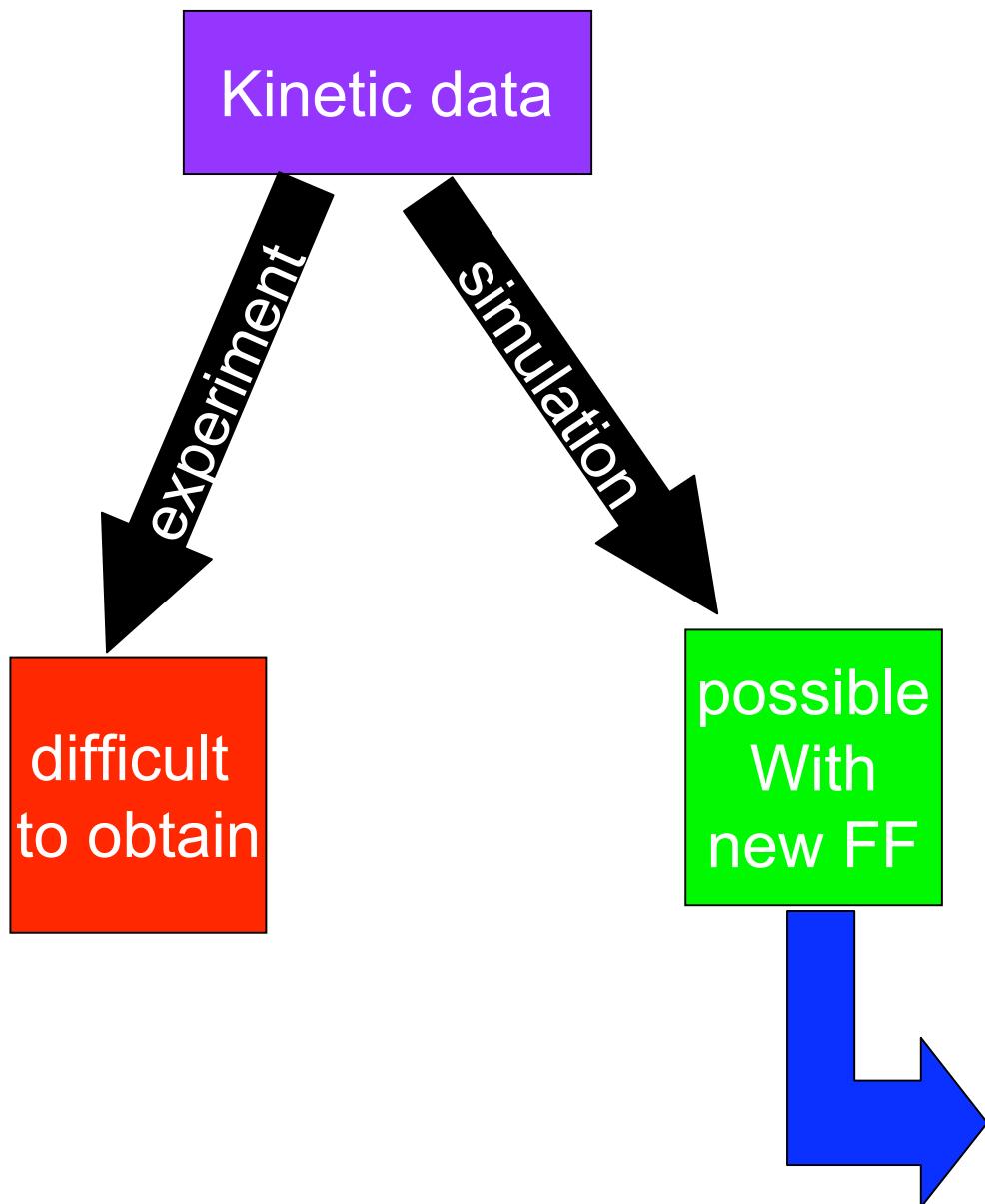
## Butyl o-rings with accelerated aging



Gillen et al. Polym. Degrad. Stab. 82, 25 (2003)

Arrhenius relation changes slope at moderate temperature

# Future Work



# Summary

