



Use of the DICE pulser for High-Pressure Strength Measurements

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Acknowledgements

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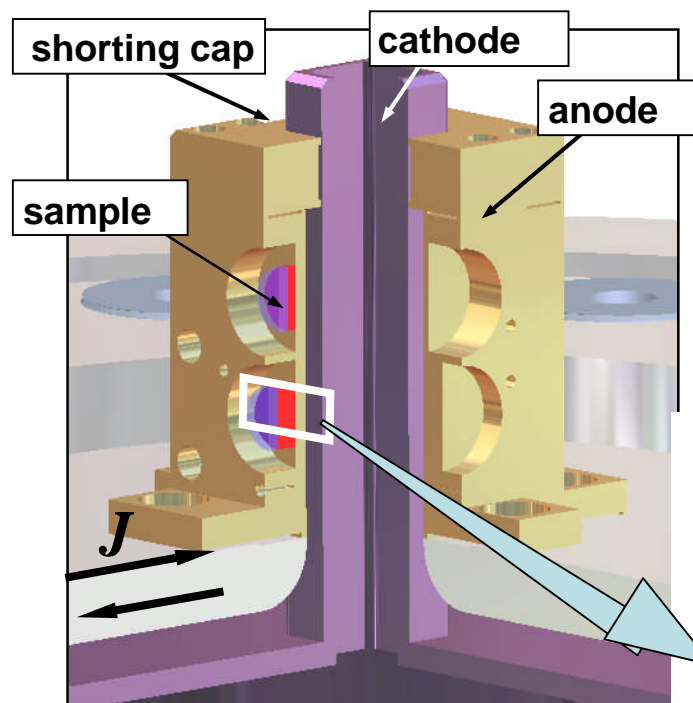
Goals

- ◆ **Develop technique on the DICE pulser for accurate measurement of compressive strength in aluminum under ramp loading**
 - **Extend previous work developed for ICE on Z**
 - **Apply to several metals and optical materials**
- ◆ **Approach**
 - **Demonstrate accurate quasi-isentropic loading data**
 - **Extend to unloading measurements for compressive strength data**

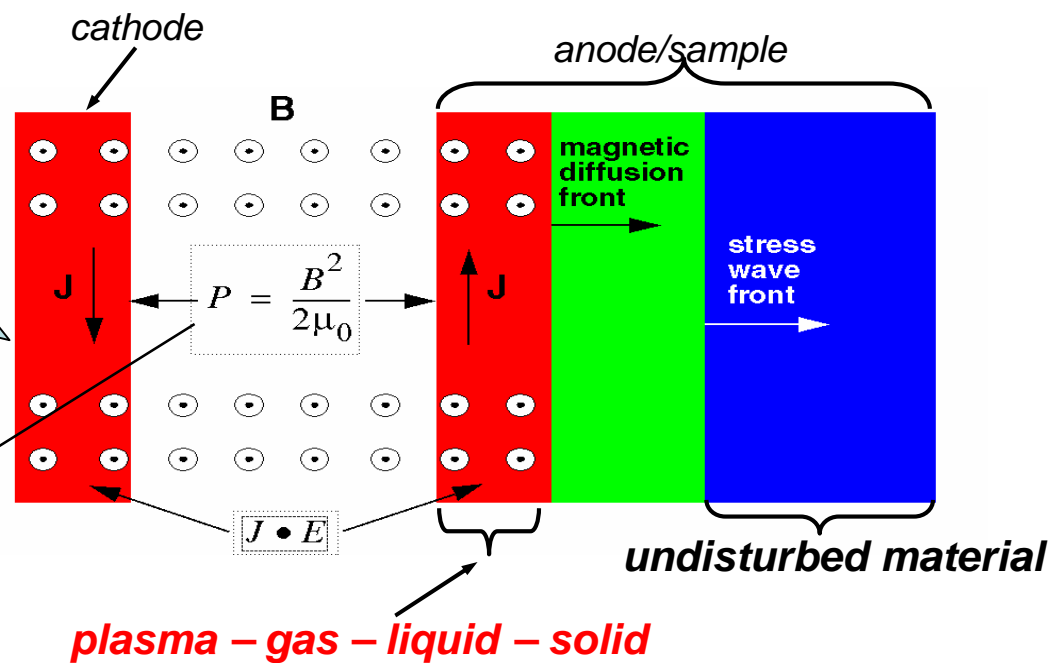
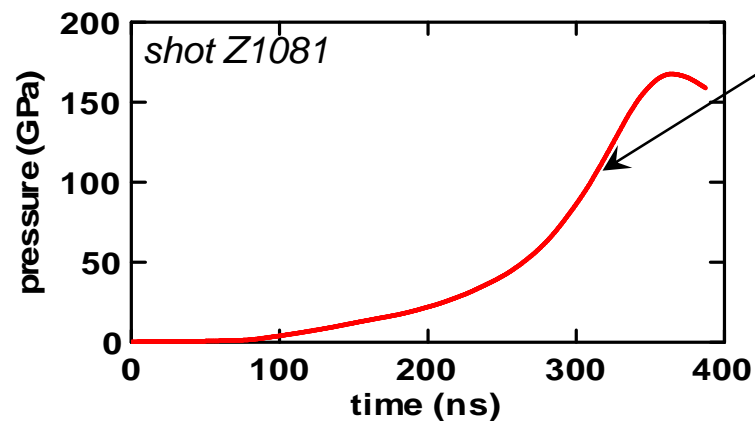
Outline

- ◆ Background
- ◆ Loading technique
- ◆ Results
- ◆ Work in progress

Magnetic drive developed on Z for producing smooth ramp waves to high pressure

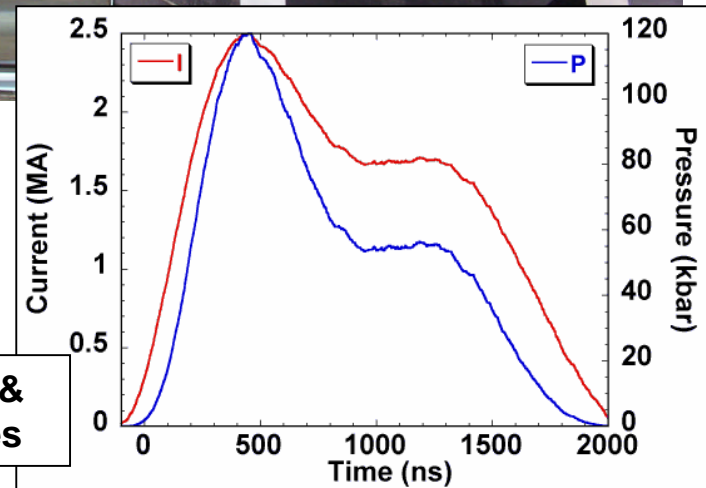
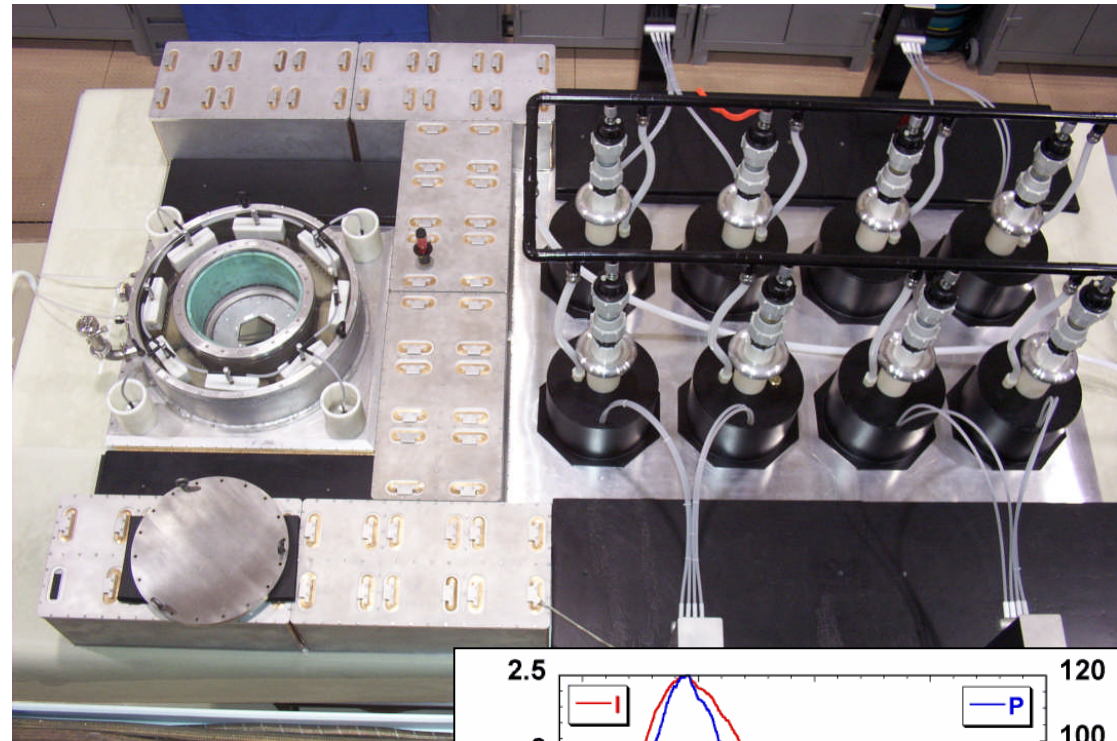


- Electric current induces magnetic field
- $J \times B$ magnetic force transferred to electrode



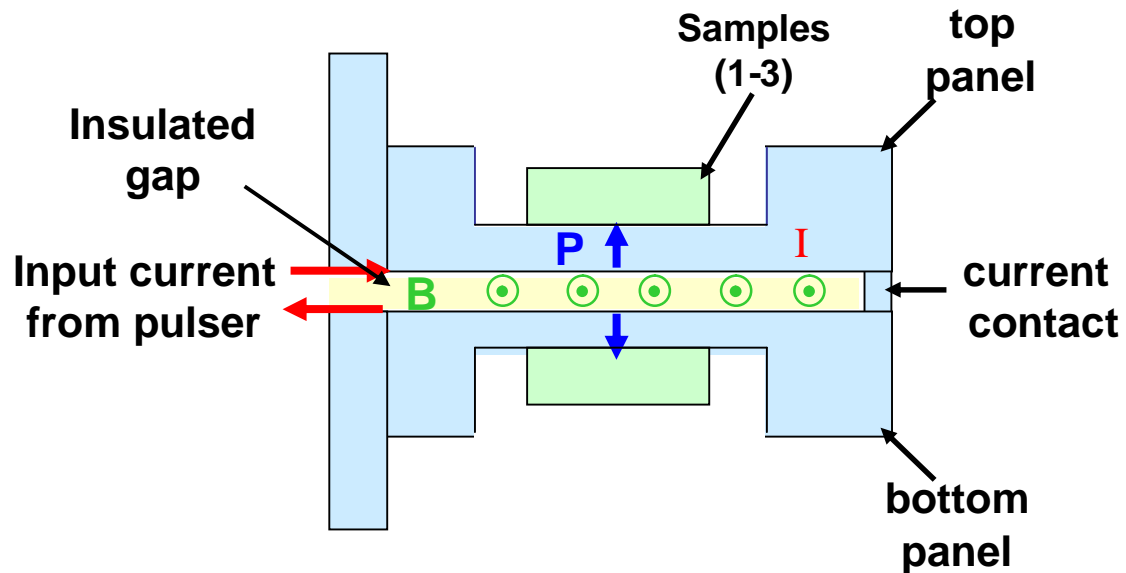
The DICE pulser produces smaller currents over longer times

- ◆ Peak current, 3.5 MA;
400 - 500 ns risetime;
peak pressure ~ 200 kbar
- ◆ High-current pulser
(~2 shots per day)
- ◆ Energy storage, eight 4- μ F capacitors, 80 kV max
- ◆ Large sample dimensions,
~ 2-3 x 12-18 mm dia.



Typical **current** &
pressure profiles

Typical sample test configuration



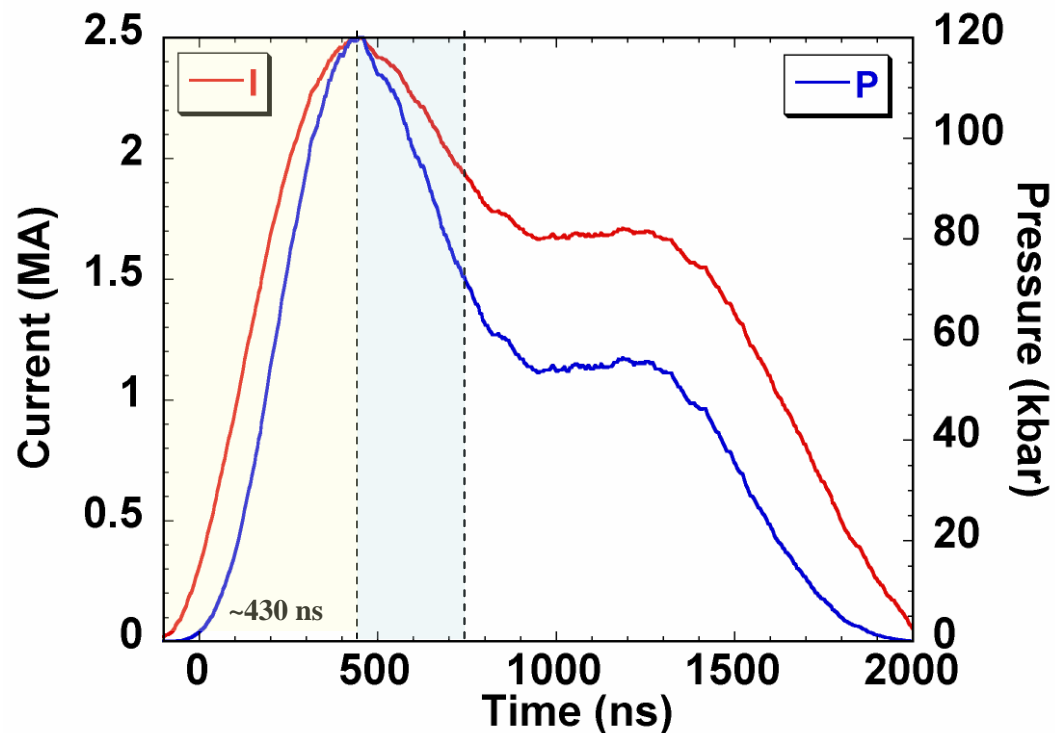
$$P_{mag} = k_P \frac{B^2}{2\mu_0} = k_P \frac{\mu_0}{2} \left(\frac{I}{w} \right)^2$$

k_p – geometry-dependent scale factor



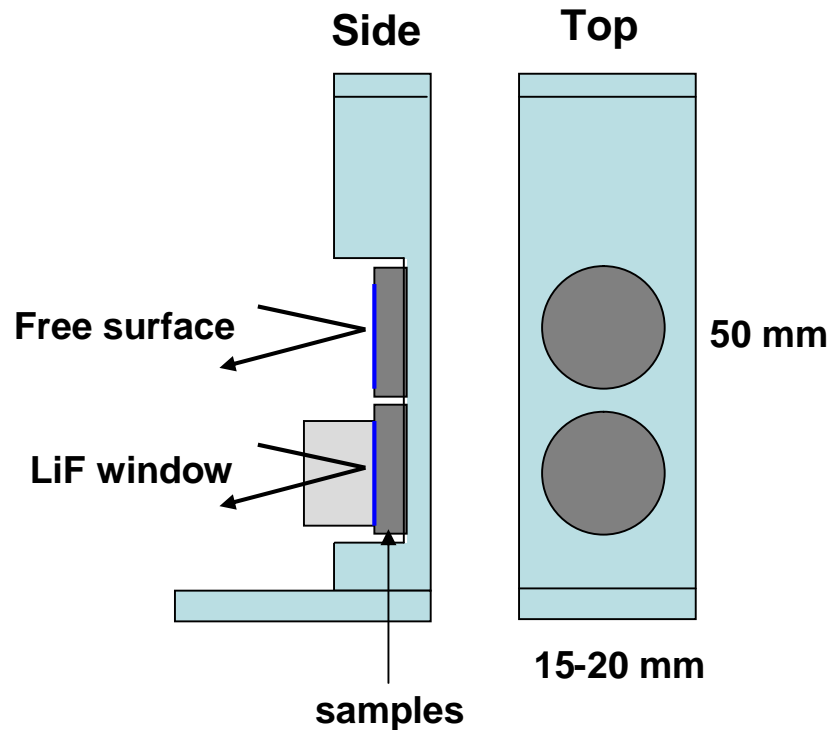
Long pulses on DICE constrain experimental configurations

Design Issues



- ◆ Bottom-top wave interactions
- ◆ Wave/diffusion front interactions
- ◆ 2-D side rarefactions
- ◆ Non-constant peak pressure
- ◆ Drive pressure uniformity
- ◆ Interface bonds

A drive configuration is being used that satisfies these requirements on AI experiments

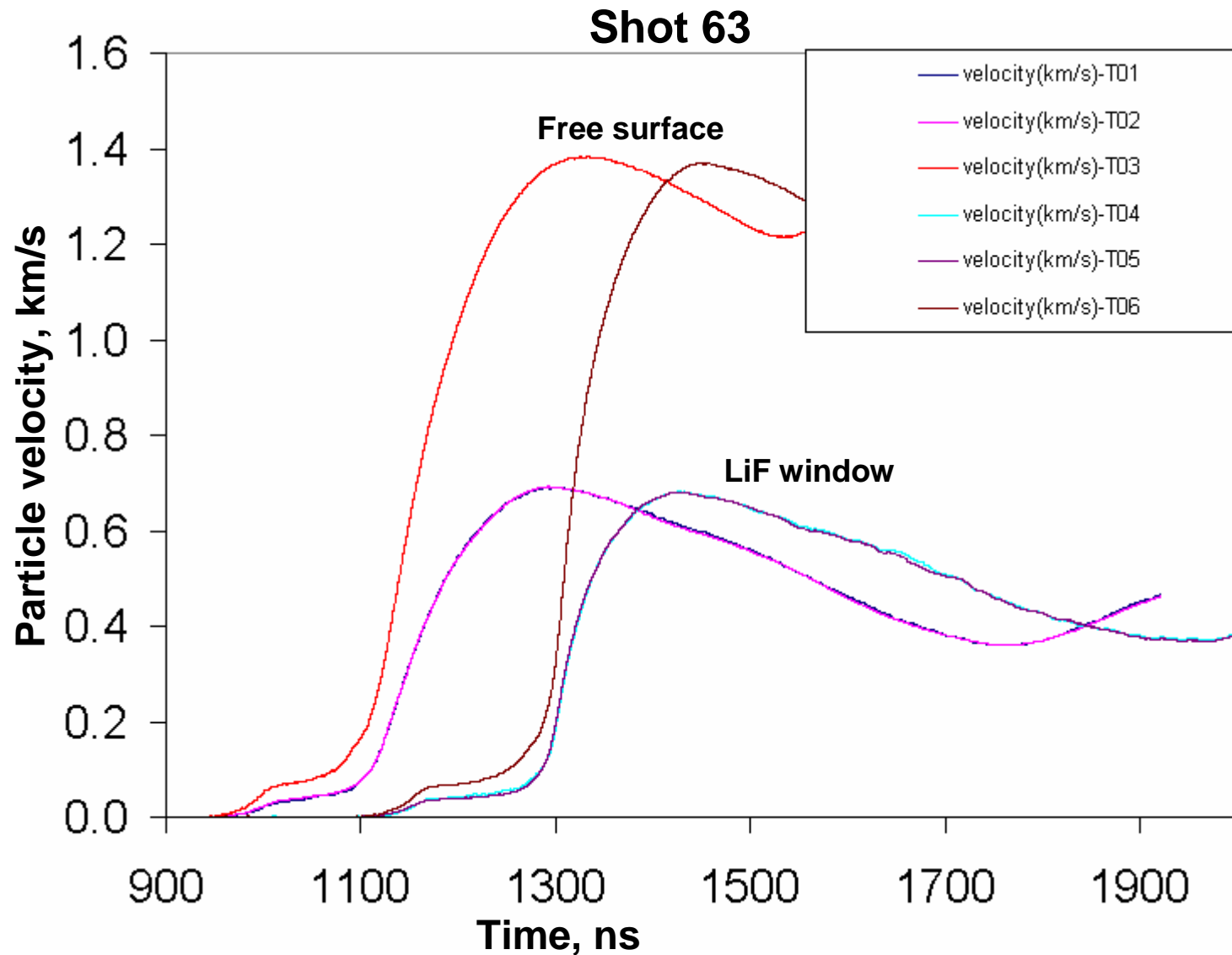


- ◆ Panels, 2 x 15 – 20 x 50 mm
- ◆ Panel thickness, 2 mm
- ◆ $\sigma_{\text{peak}} \sim 60\text{-}100$ kbar
- ◆ Drive uniformity $\sim 2\%$ central portion
- ◆ 200-300 ns of unloading
- ◆ Free surface + windows
- ◆ Analysis of opposing pairs

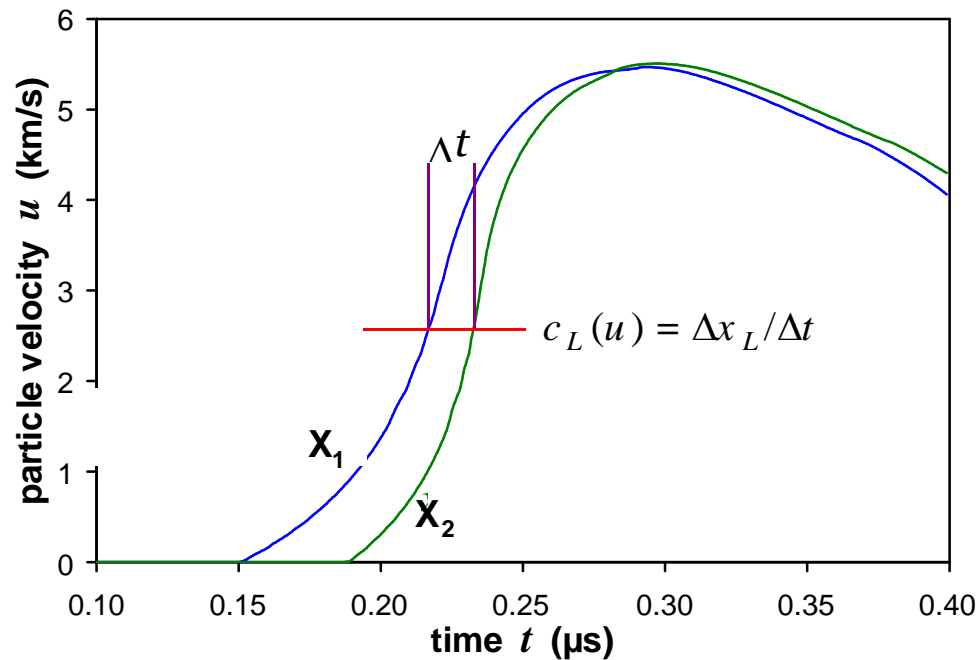
Approach is to first evaluate EOS accuracy, then obtain strength data

- ◆ **Demonstrate ability to reproduce EOS data on 6061-T6**
- ◆ **Compare to previous Z work, Sesame EOS**
- ◆ **Determine compressive strength from loading/unloading data**
- ◆ **Compare to ICE studies (GDI, Z, Omega)**
- ◆ **Improve method in future experiments**
 - Evaluation of systematic errors
 - Better drive uniformity
 - Improved sample preparation methods
 - Higher peak pressures

Recent results from free surface and window experiments on 6061-T6 aluminum

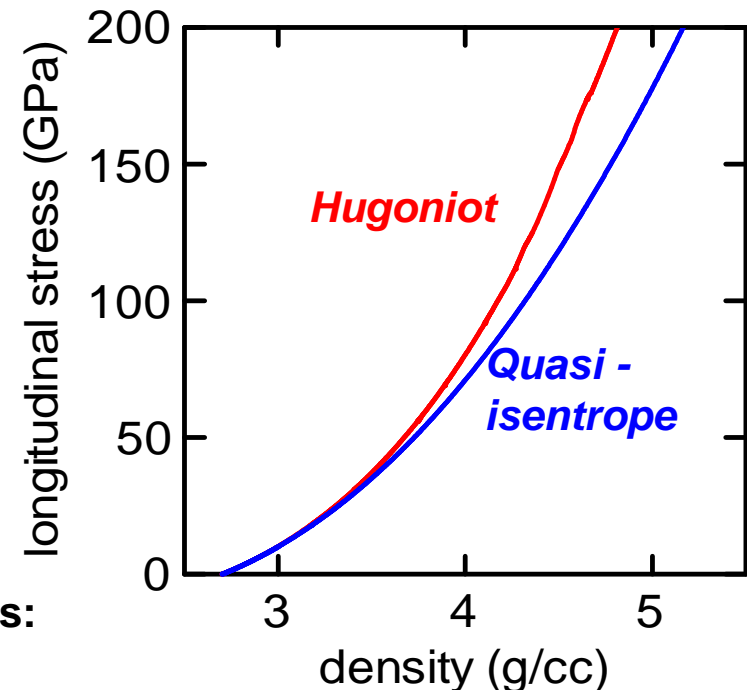


In situ wave profiles can be analyzed to provide continuous σ – ε along the loading path



$$d\sigma_x = \rho_0 c_L du$$

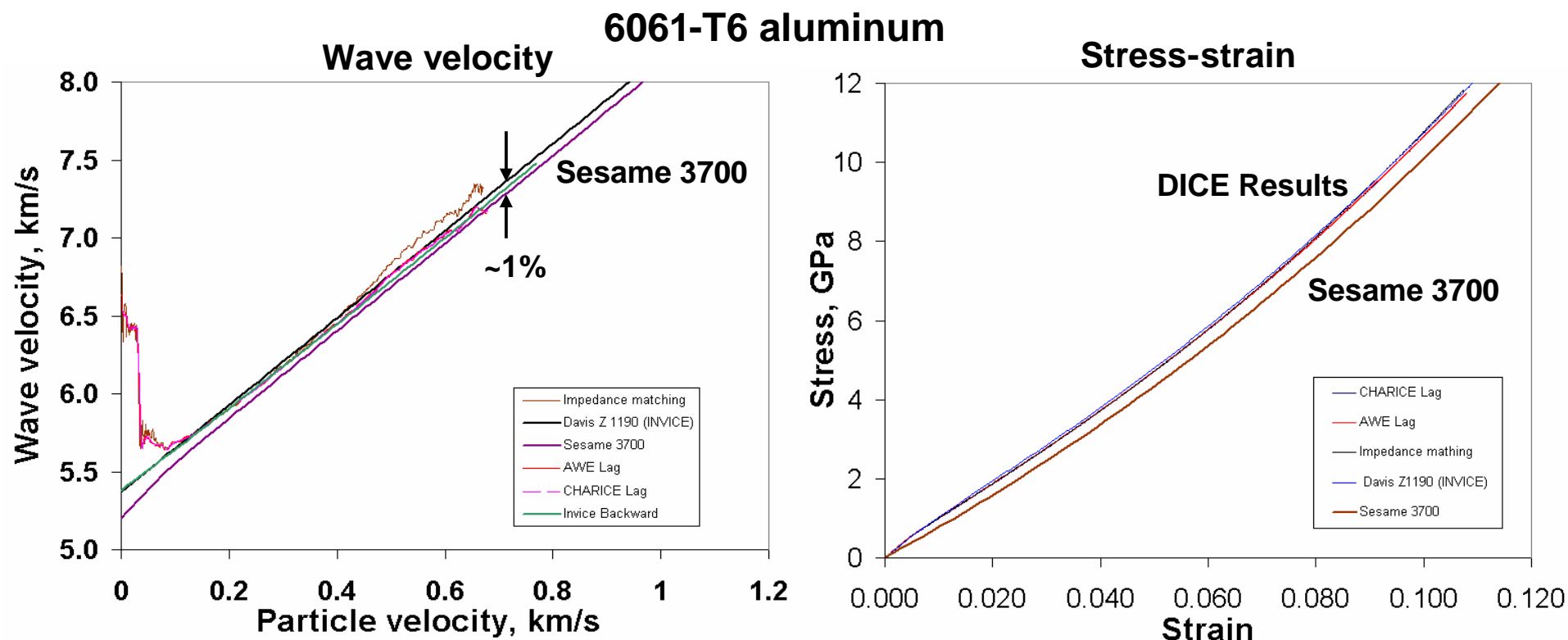
$$\frac{d\rho}{\rho^2} = \frac{du}{\rho_0 c_L}$$



Several methods used to analyze ramp wave results:

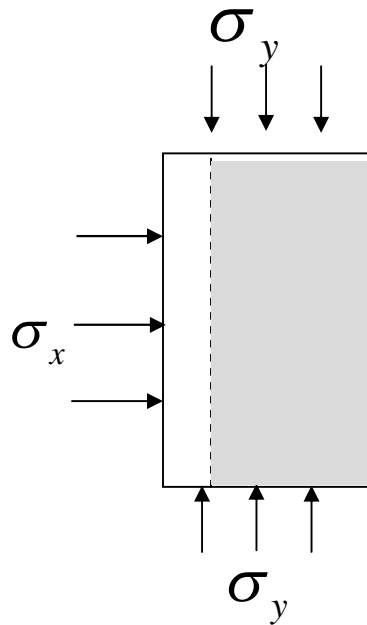
- Impedance matching
- Lagrangian wave analysis
- Backward analysis methods (INVICE)

Measured results and comparison to other data



- Agreement with other ICE data to within experimental errors
- Major contribution to the difference Sesame 3700 is material strength
- Other factors: viscous effects, systematic errors and EOS errors

A goal is to estimate shear stresses produced for uniaxial strain ramp loading



Uniaxial strain compression

Strain

$$\varepsilon_{ij} = \varepsilon_{ij}^e + \varepsilon_{ij}^p$$

$$\varepsilon_{ii} = 0 \text{ (plastic dilatation)}$$

Stress

$$P = \left(\frac{\sigma_x + 2\sigma_y}{3} \right)$$

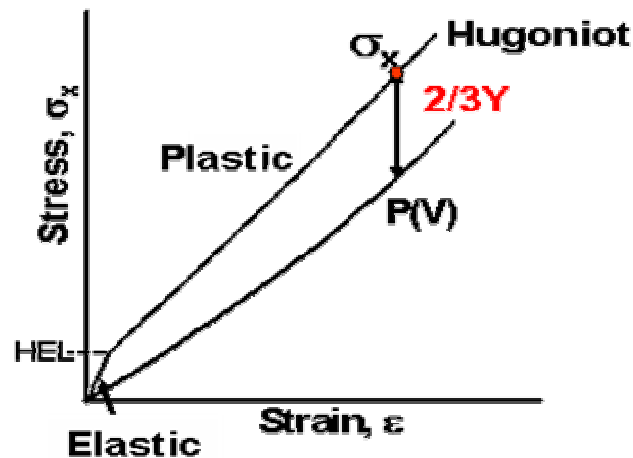
$$\tau_c = \frac{1}{2}(\sigma_x - \sigma_y)$$

$$\sigma_x = P + \frac{4}{3}\tau_c$$

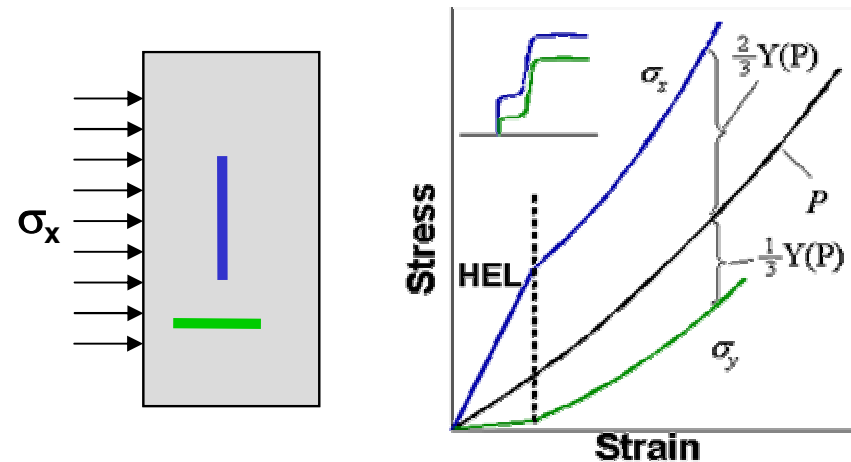
$$\sigma_x = P + \frac{2}{3}Y$$

Several techniques have been developed to study strength properties

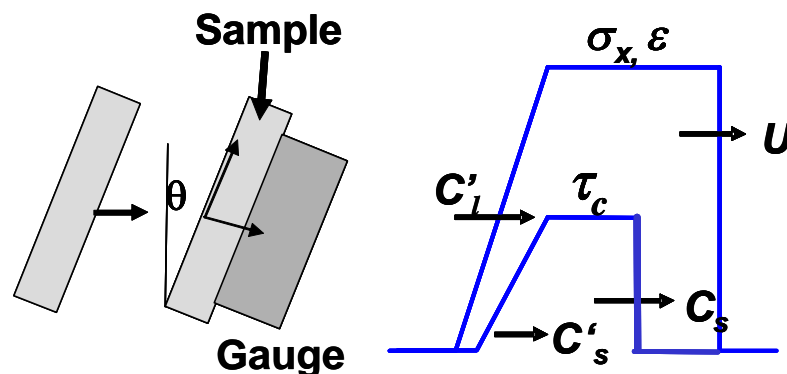
Stress Difference



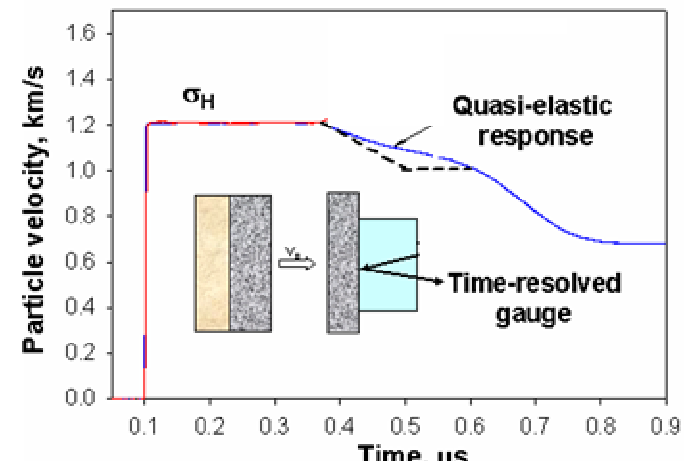
Longitudinal-lateral gauges

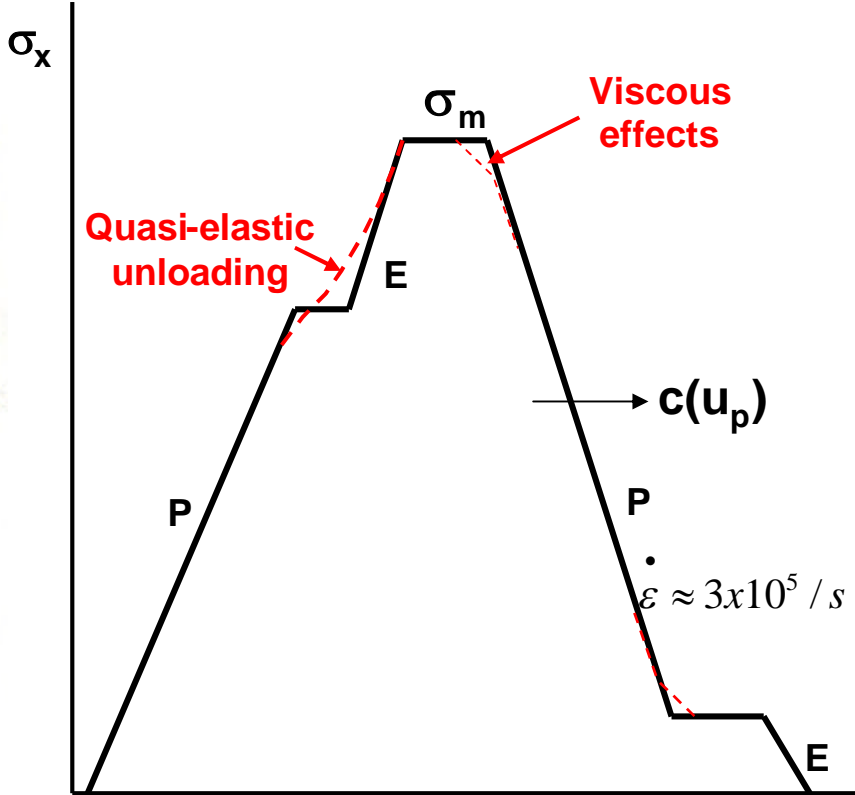


Oblique Impact



Wave Profile





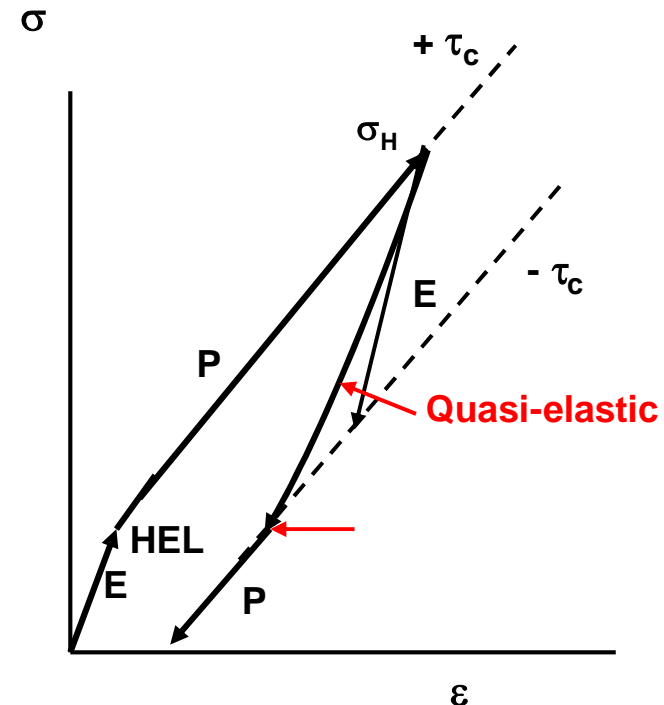
G.R. Fowles, J. Appl. Phys., 1961

Approach

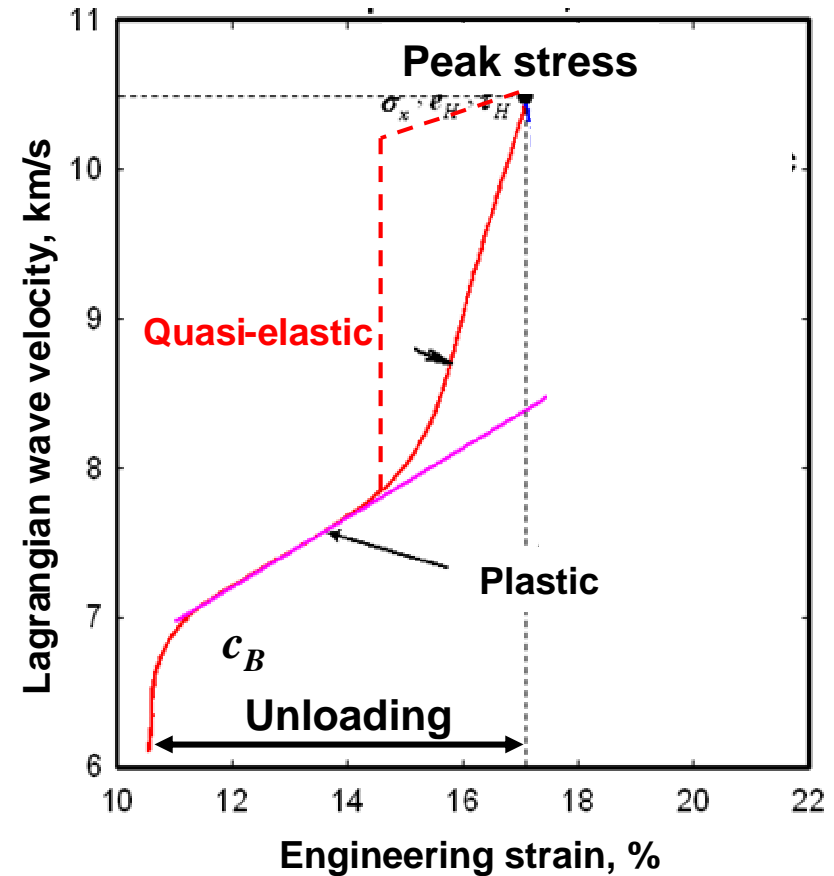
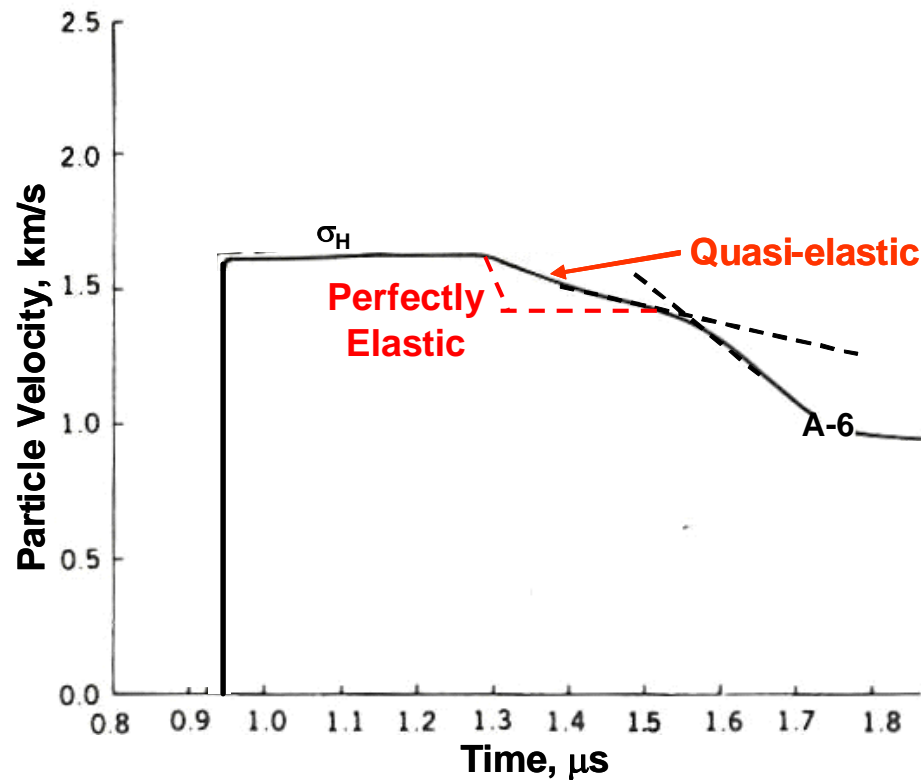
- ◆ Develop a configuration for producing uniaxial strain loading and unloading on DICE
- ◆ Investigate wave profile techniques for probing strength properties of Al for ramp loading (extension of Z work)
- ◆ Compare analysis results using different methods
 - Lagrangian wave analysis
 - Characteristics code approaches (Rothman, Ekert, Davis)
 - Backward analysis
- ◆ Investigate effects of window properties
 - E-P effects for unloading
 - Results from different windows (sapphire, LiF, ..)

Assumptions used to analyze unloading data

- Response is rate-independent
- A yield surface exists after loading and can be measured as a transition from quasi-elastic to plastic response
- The yield function depends on some measure of plastic strain or pressure
- Plastic response can be approximated by wave velocities after Q-E transition



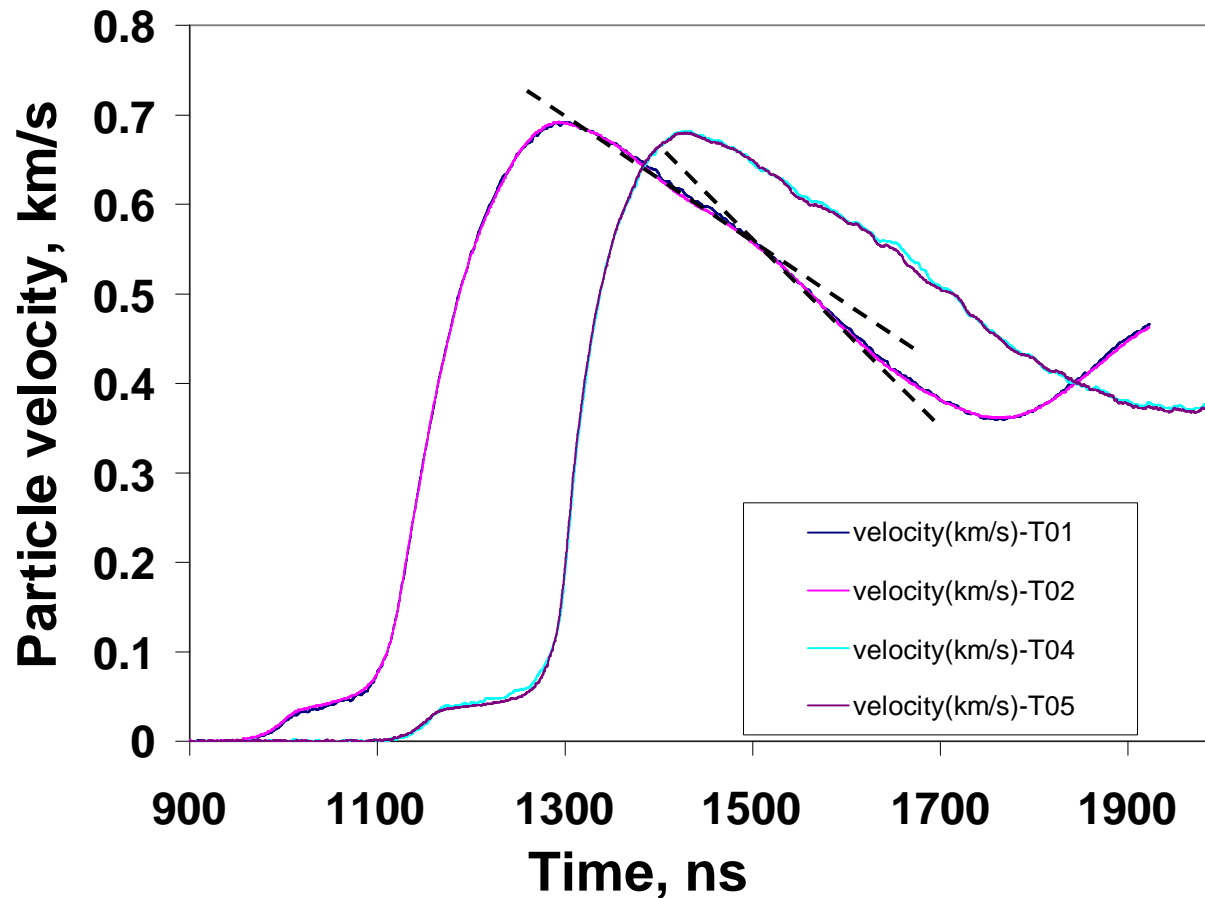
Determination of strength from shock loading/unloading profiles



$$\Delta\sigma = \frac{3}{4}\rho_0 \int_{e_1}^{e_f} (c_L^2 - c_B^2) de$$

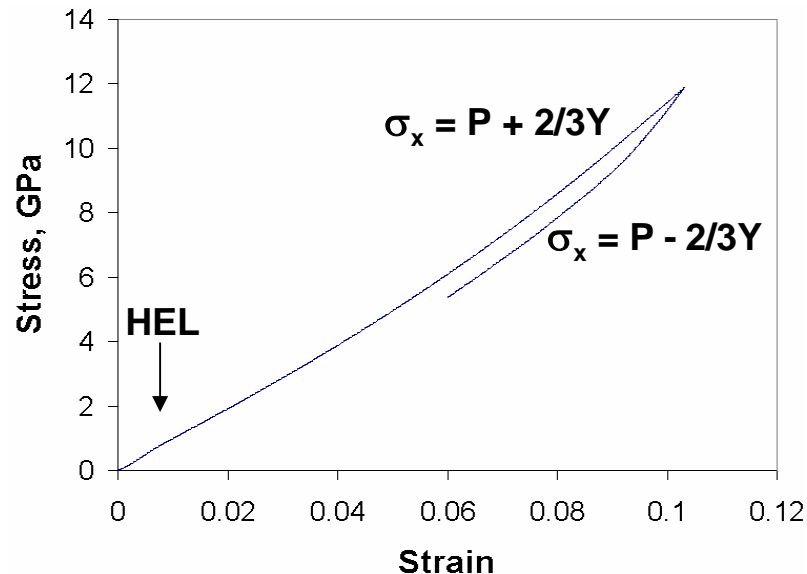
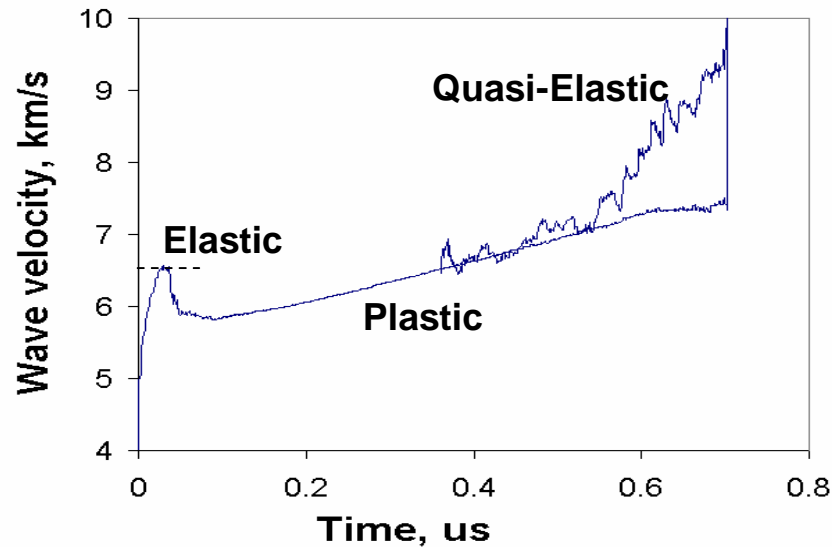
= Y if Hugoniot state is on the yield surface

Unloading wave profiles used to estimate strength - redo



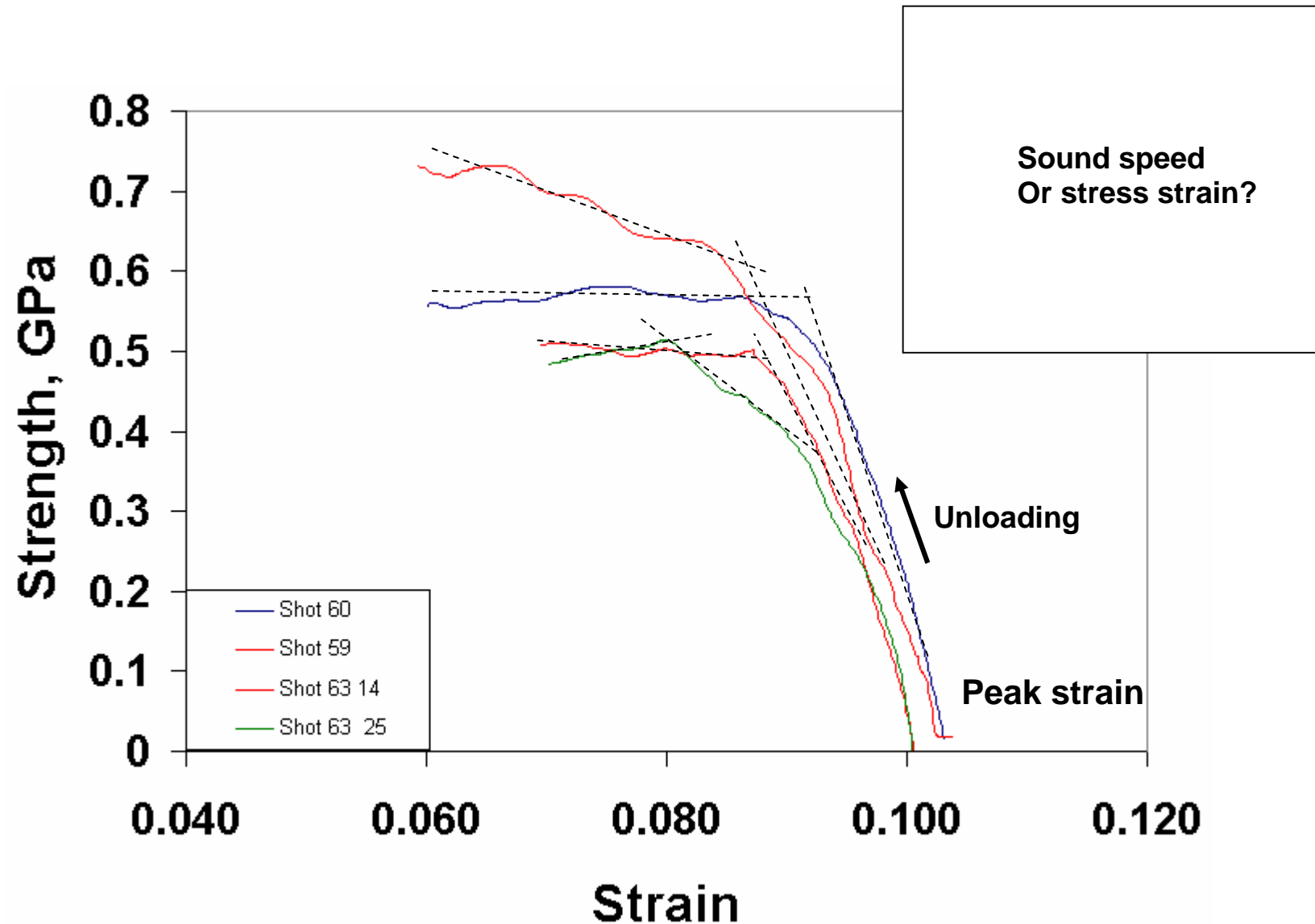
- ◆ Good VISAR reproducibility
- ◆ Quasi-elastic transition detected
- ◆ ~1.5% attenuation
- ◆ Noisy second unloading signal

Lagrangian analysis of loading and unloading in ramp experiments



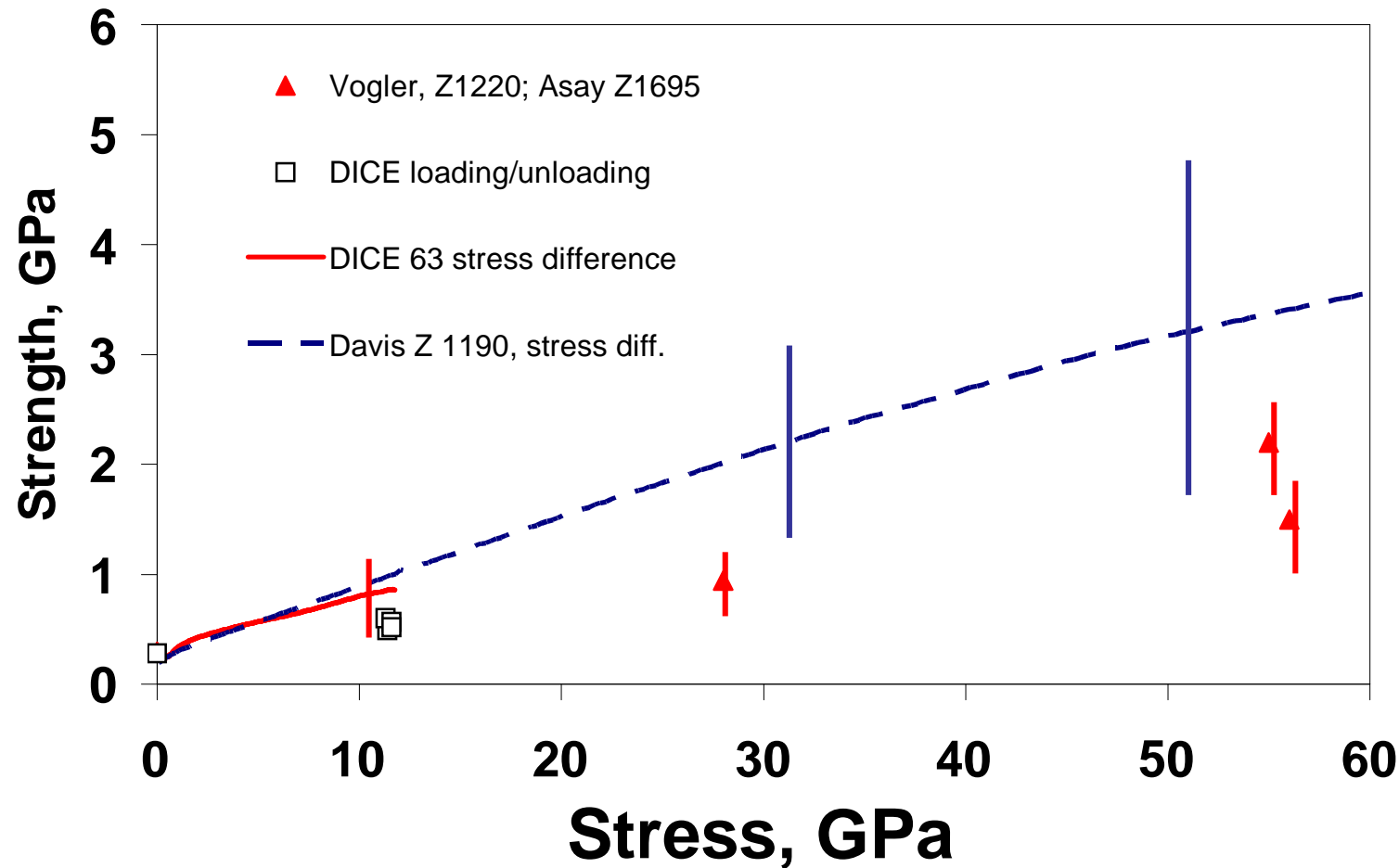
- ◆ Unloading data noisier than for shock experiments
- ◆ Measurement of loading wave velocity determines bulk response
- ◆ Softening observed near peak stress in several experiments

Strength determination

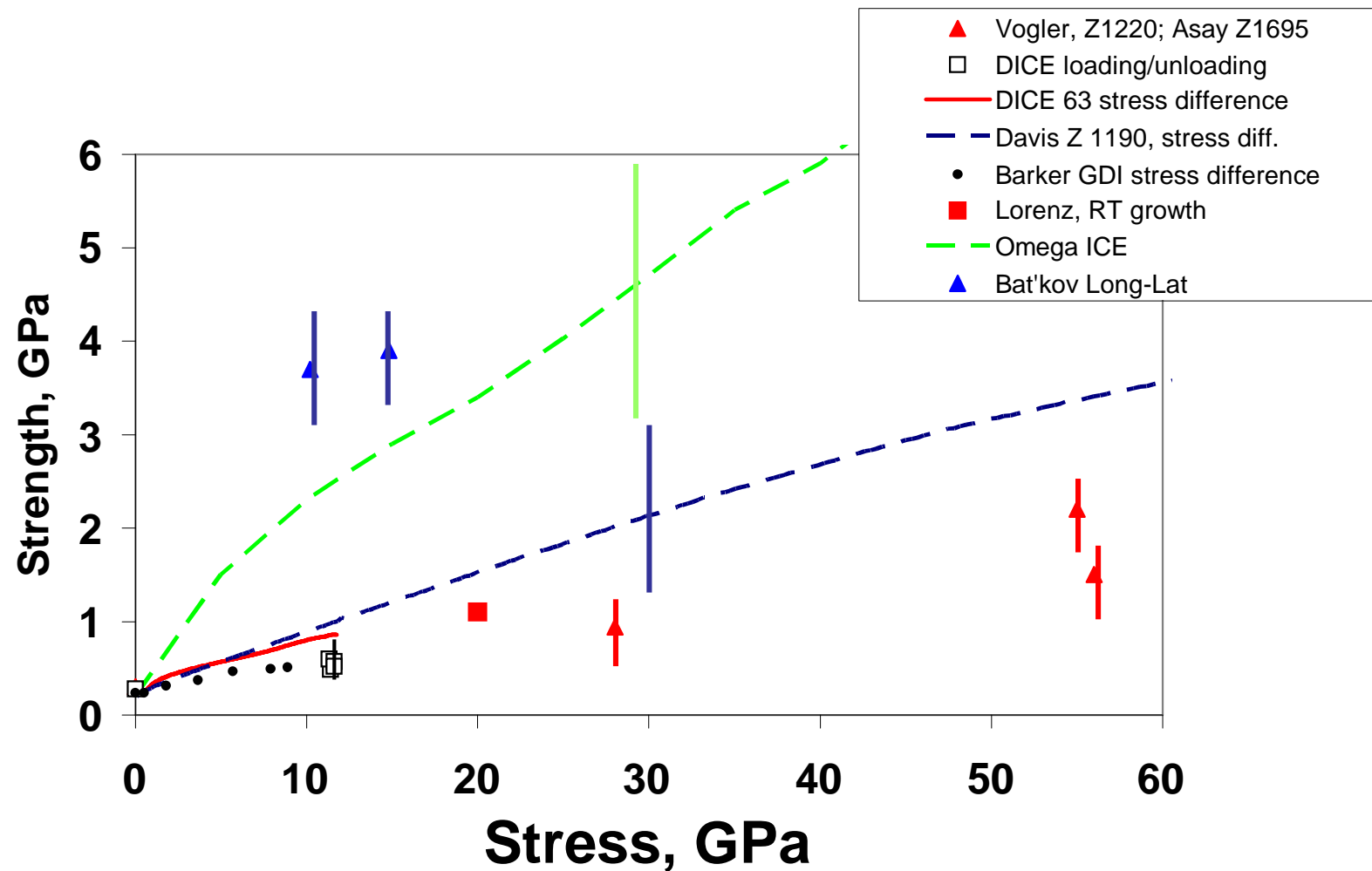


Comparison of strength data estimated from stress difference to isentrope and unloading profiles

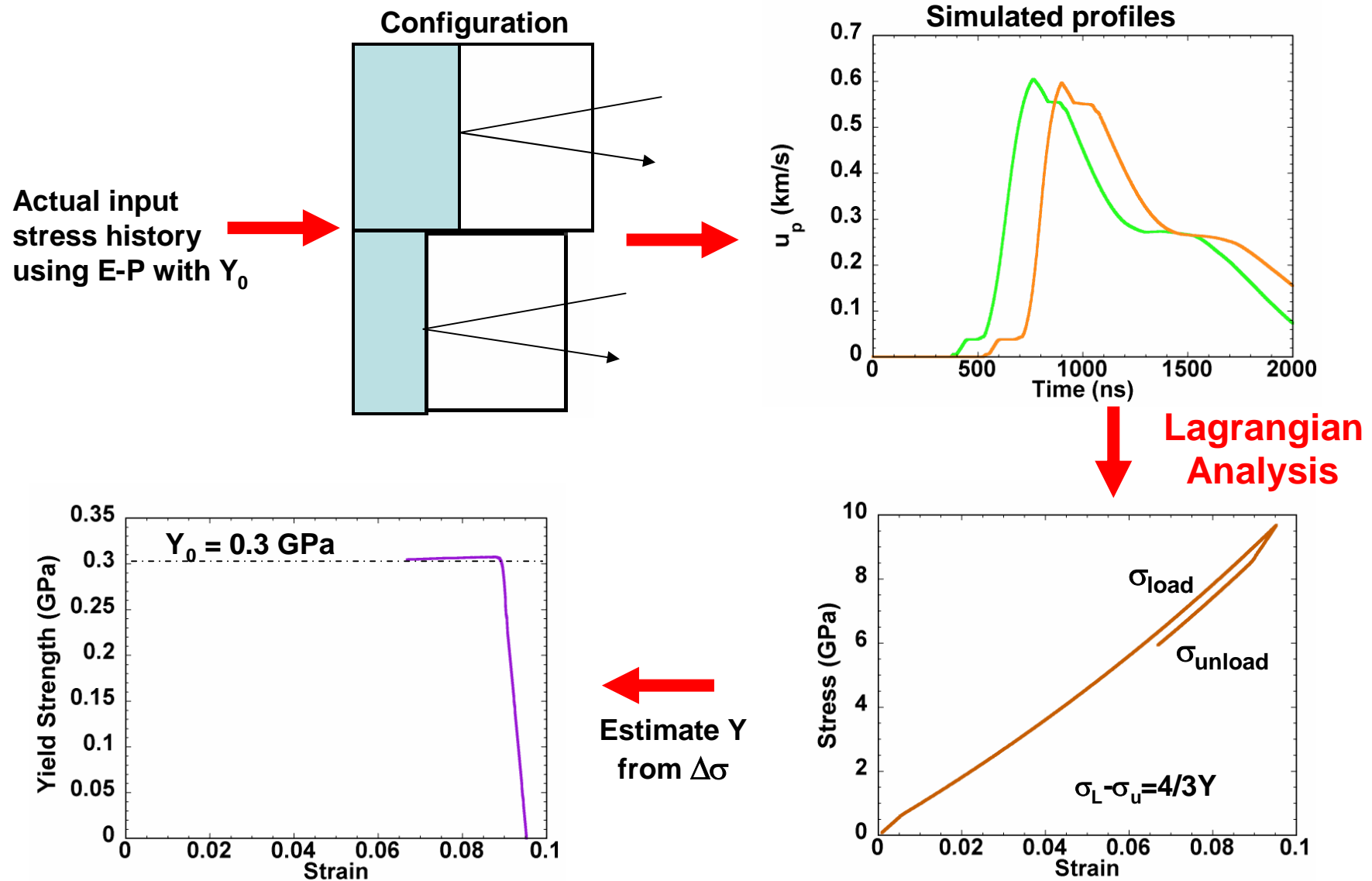
Strength of 6061-T6 for ramp loading



DICE results are consistent with other strength data for quasi-isentropic loading



1-D numerical simulations profiles are being used to simulate profiles for Lagrangian analysis



Summary

- ◆ **Loading conditions on DICE are sufficient to obtain loading and unloading and estimates of compressive strength**
- ◆ **Compressive stress-strain curves obtained on aluminum are consistent with other data**
- ◆ **Estimates of strength are consistent with several other methods, but inconsistent with strength determined from difference to the isentrope**
- ◆ **Strength measurements are difficult – coordinated effort with different techniques is necessary to develop consistent models**

Next steps

- ◆ **Improvements in experimental configuration**
 - Sample preparation techniques (diamond machining, glue bonds)
 - Better pressure drive uniformity
 - Shorter current risetimes
 - Smoother current unloading

- ◆ **Better understanding of unloading response**
 - Wave attenuation effects
 - Effect of LiF properties
 - Analysis methods for unfolding perturbed unloading profiles

- ◆ **Studies of strength in several materials**
 - Effects of initial microstructure in aluminum
 - LiF, sapphire (T. Ao)
 - High impedance materials (vanadium, tantalum, tungsten)