



Brazing Optimization of Mechanically-Applied Active Braze Filler Metal Paste

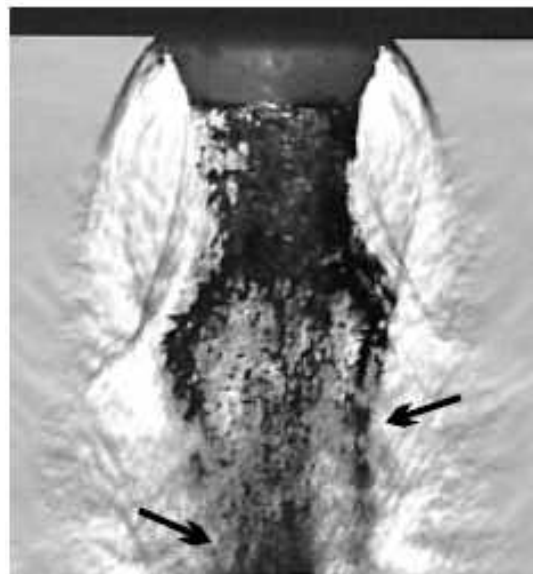
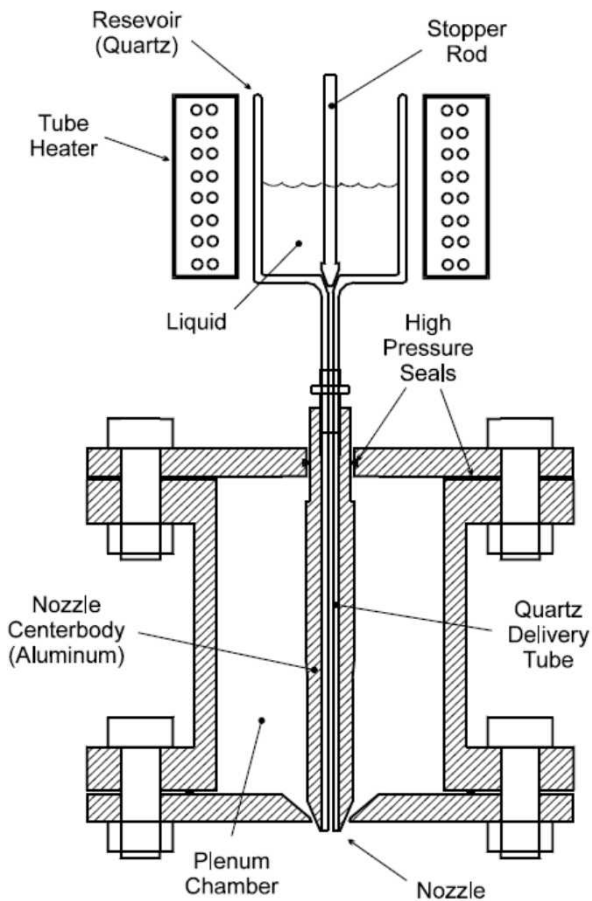
C.A. Walker, G.L. Neugebauer, D.F. Susan, V.C. Hodges,
Sandia National Laboratories, Albuquerque, NM 87185

LÖT 2007

8th International Conference

Brazing, High Temperature Brazing and Diffusion Bonding
June 19 - 21, 2007 Aachen, Germany

Metal Atomization^{1,2}



Powder is produced by the violent disruption of a stream of molten metal with a coaxial, co-directional supersonic gas flow.

1. *HIGH-SPEED IMAGING OF LIQUID METAL ATOMIZATION BY TWO DIFFERENT CLOSE-COUPLED NOZZLES*

S. Mates and G. Settles, The Pennsylvania State University

2. *THE PRODUCTION OF METAL POWDERS BY ATOMIZATION*

John Keith Beddow, The University of Iowa

Braze Paste Shipment & Packaging





Braze Paste Analysis

July 28, 2006




Sample : 97AG-1C-2ZR
Lot No. : MM46001

Department : 211
Date Received : July 18, 2006

Lab ID No. : G127

COMPOSITION:

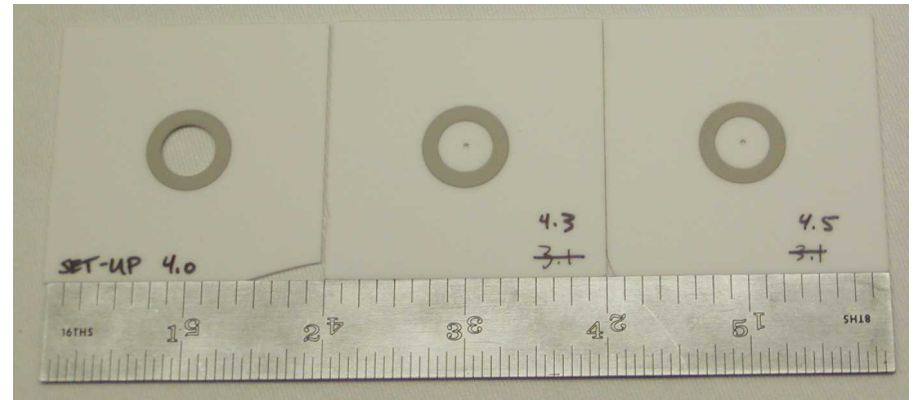
AG: *	CD: <.0001	PB: <.002	ZN: <.0001
B : .0002	CO: .0006	CR: .0007	CU: 0.99
IN: .008	FE: .002	SI: .001	SN: .005
TI: .0002	ZR: 2.31	Y : .003	P : <.001
C : 0.0090	N : 0.0000	O : 0.0000	T.Imp.=0.0229



Material passed thru a -325 mesh, resulting in 44 microns [.0017] max particle size.

Initial Screen-printing Results

- Paste printed in desired pattern with thicknesses of .0040 to .0045
- *Carrier material identified as Propylene Glycol*
- Adhered paste capable of assembly handling operations
- *Binder identified as a polymer (ex. EVA, PVA)*





Paste Printing

Equipment used

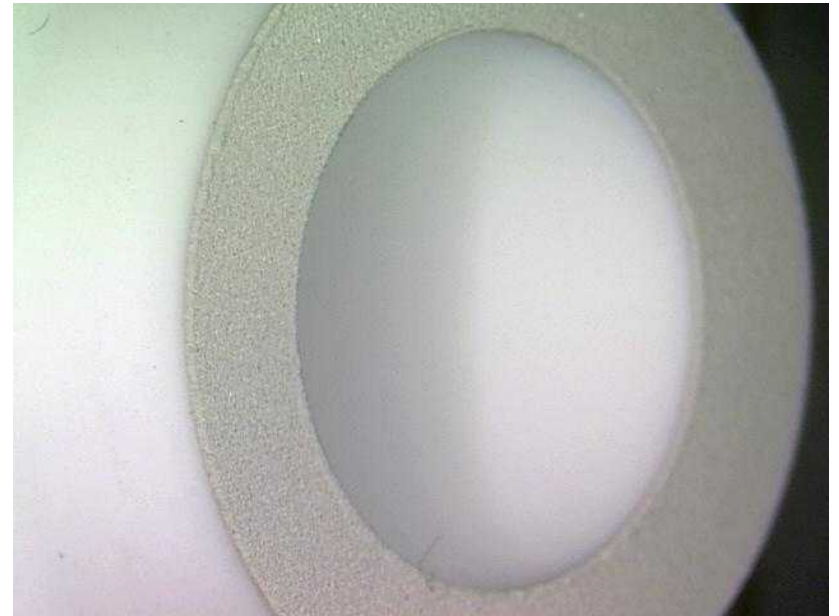
- AMI Screen Printer – adjustable print pressure
- Laser Profilometer
- Masks were made from 325 mesh material.

Details

- 40% reduction in thickness during 1 hour drying.
- Paste used as delivered, no thinning or treatment
- Extra material collected for re-use



Tensile Buttons



Standard and Half Tensile Button Samples

ASTM F-19 Tensile Buttons were fabricated to measure the leak rate and brazement tensile strength.

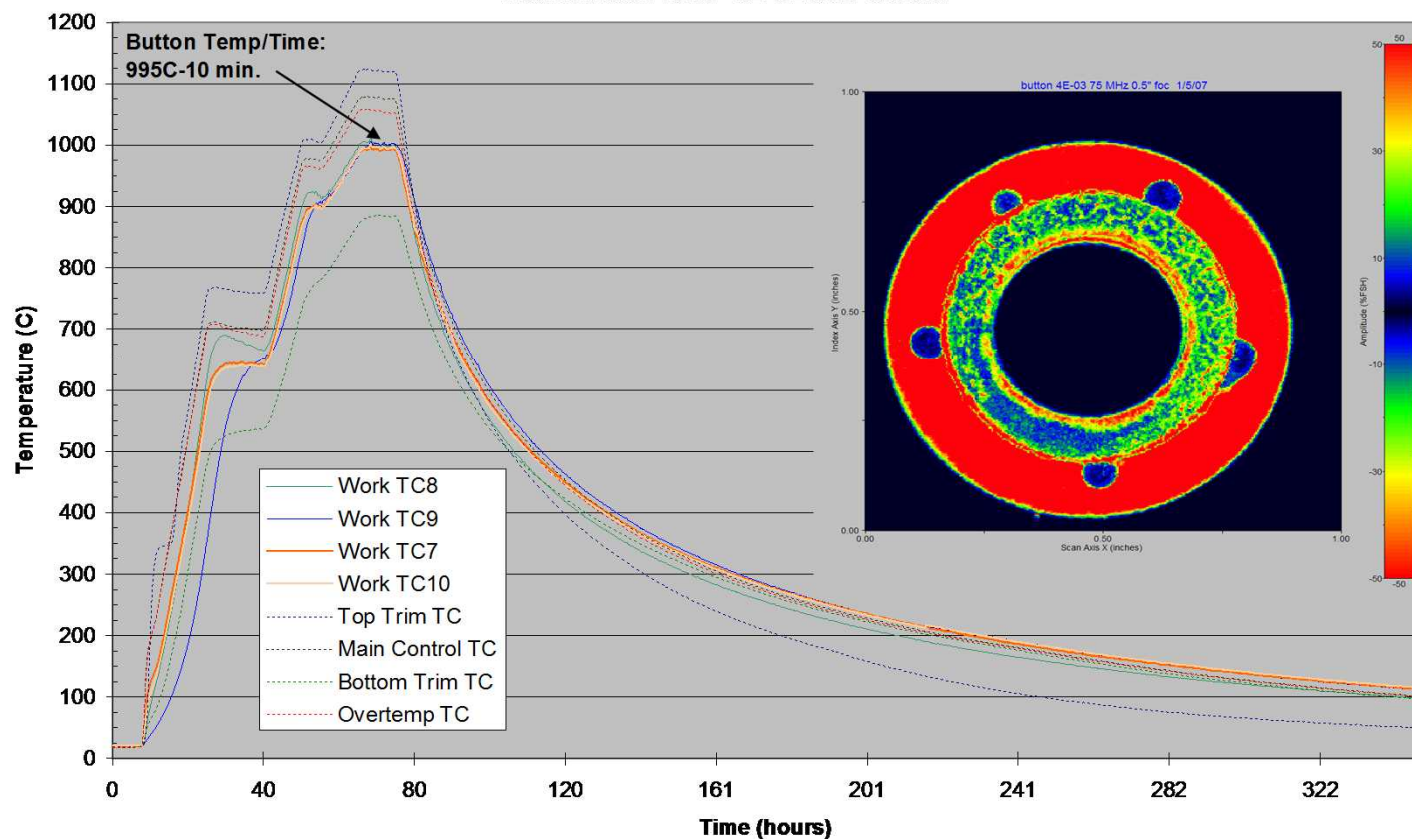


Half Tensile Button assemblies were used for ultrasonic inspection test samples.



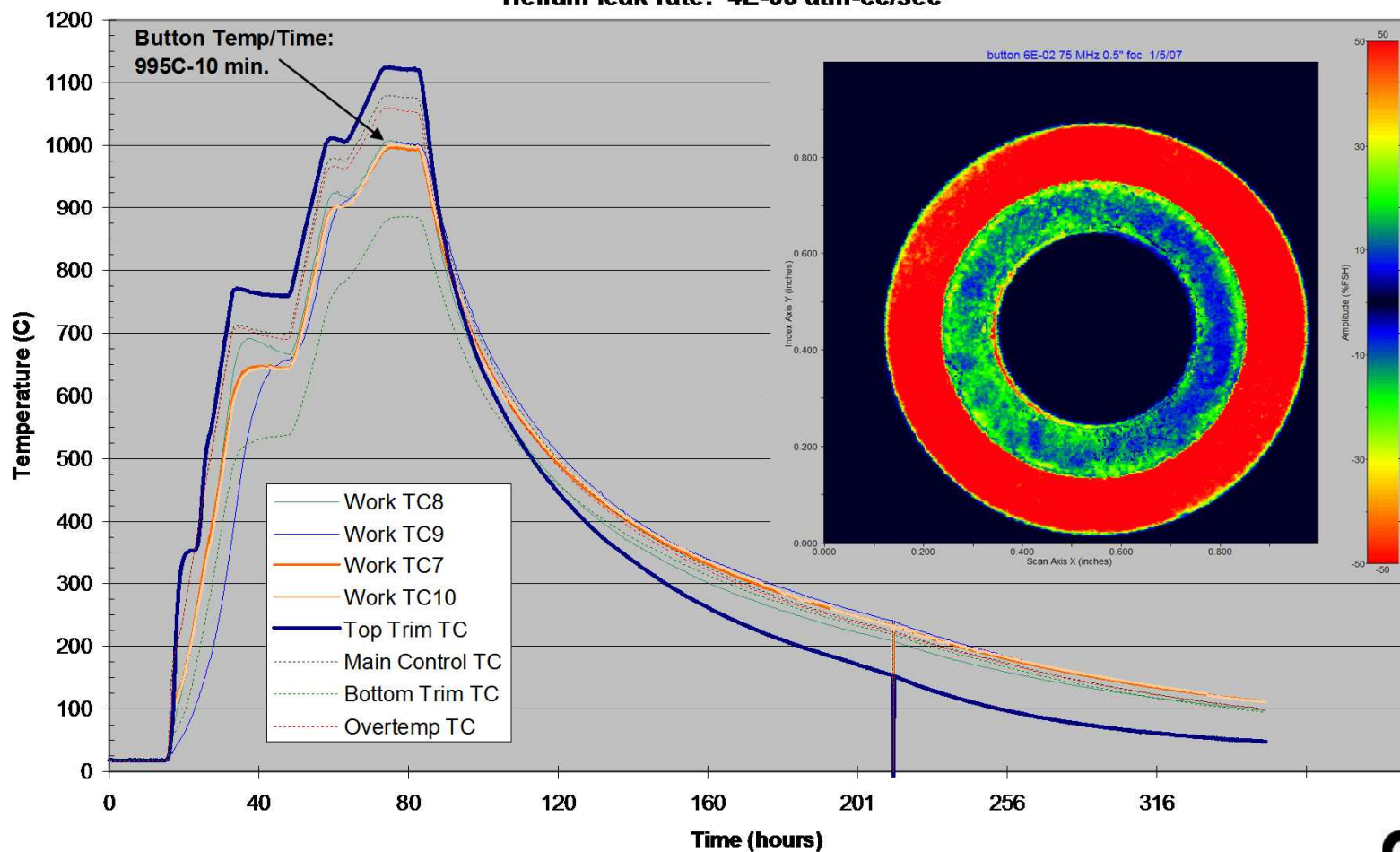
Trial 2

Temperature vs. Dew Point
Run 12182006F201
AgCuZr Paste ~0.005" thick, 3x weight
Helium leak rate: 6E-02 atm-cc/sec

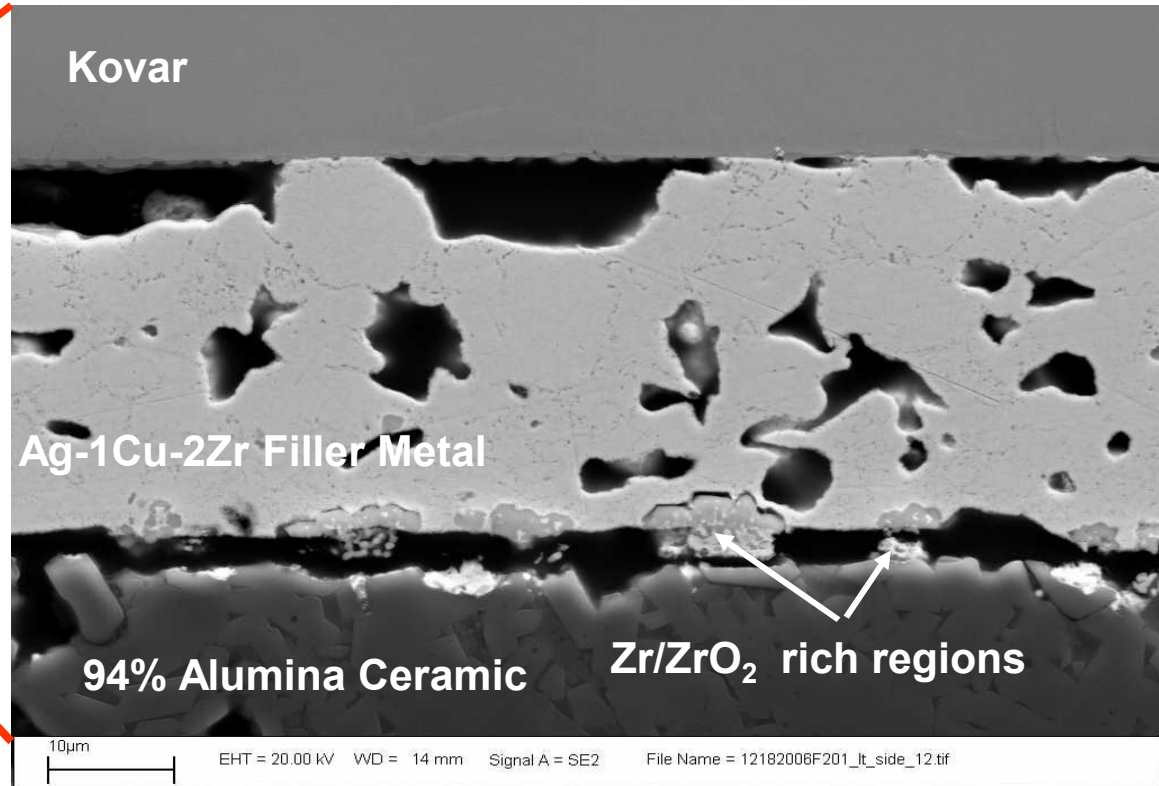
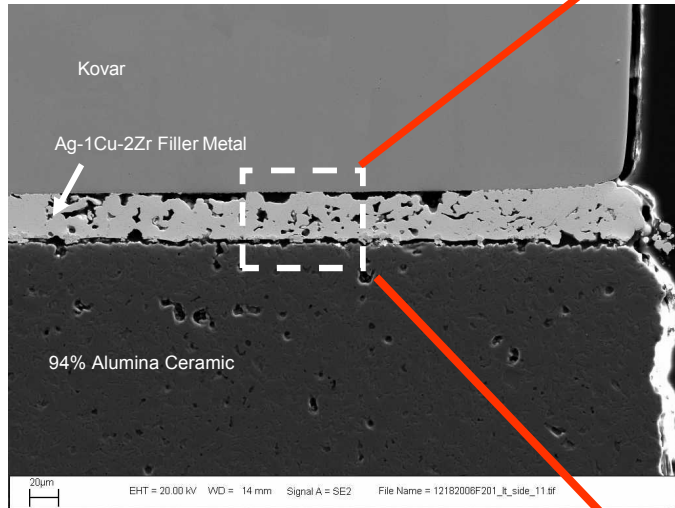


Trial 3

Temperature vs. Dew Point
Run 12192006F201
AgCuZr Paste ~0.005" thick, 1x weight
Helium leak rate: 4E-03 atm-cc/sec



Joint Porosity

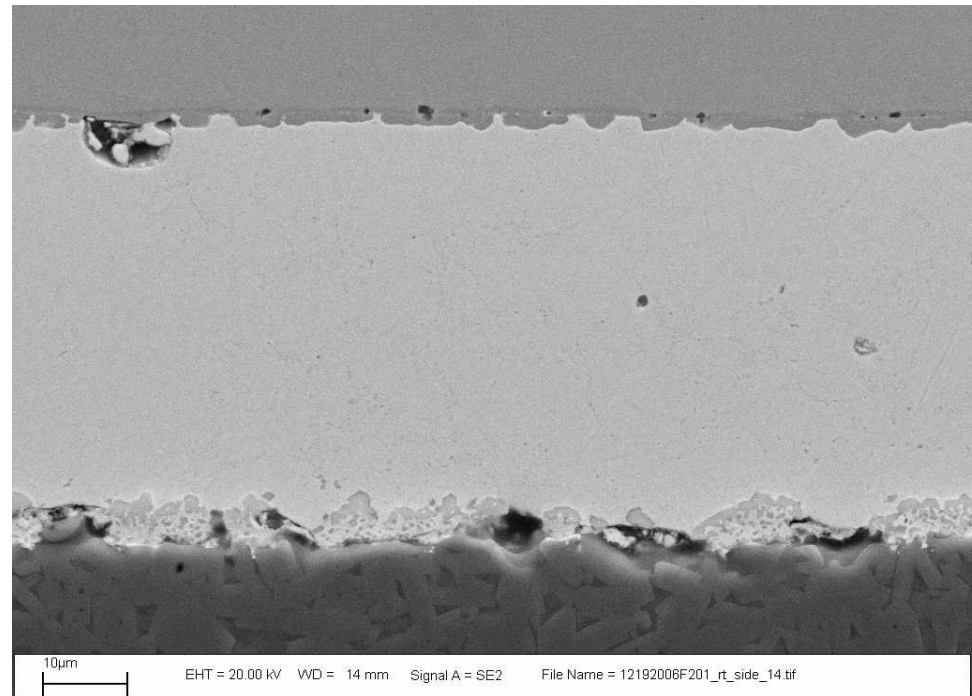
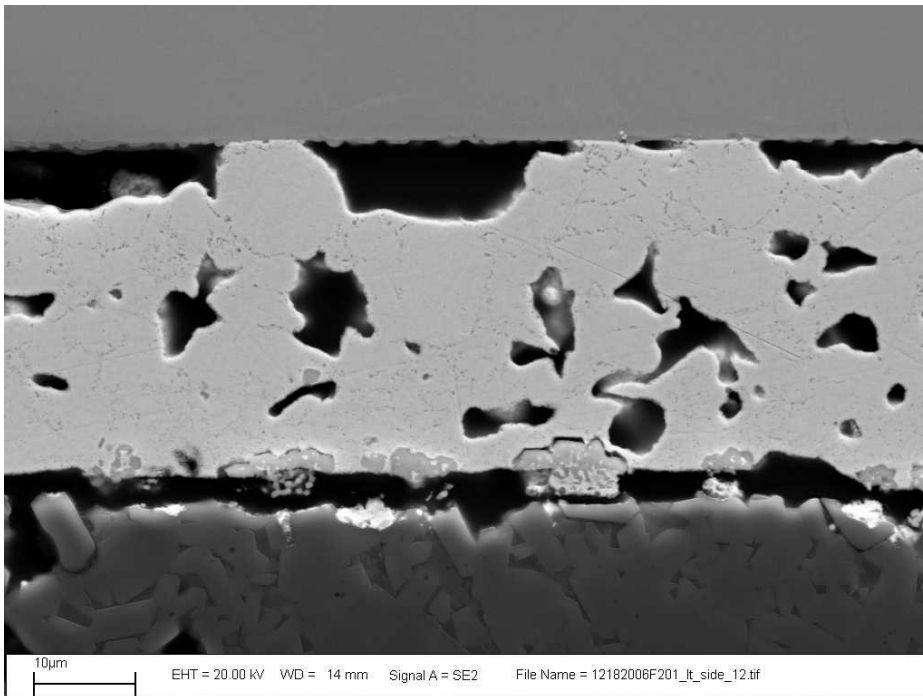


Joint Porosity

Identical Runs?

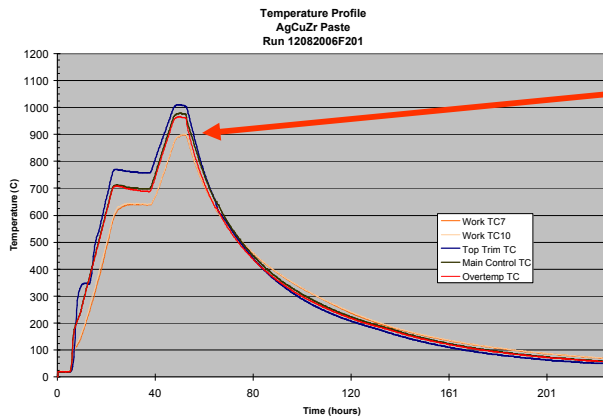
Dec 18 Run

Dec 19 Run



Joint Porosity

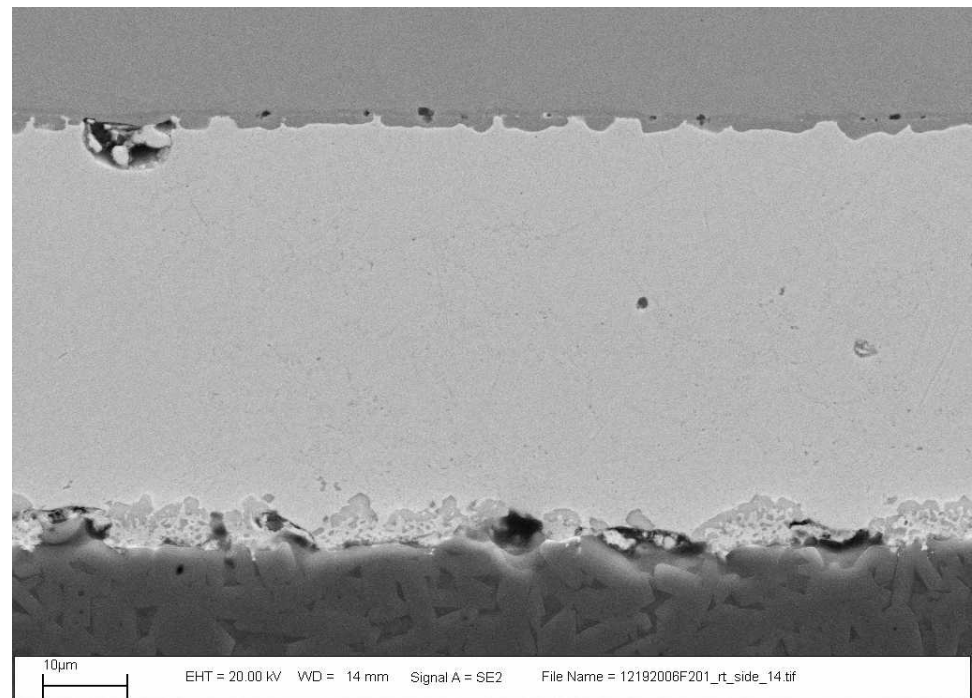
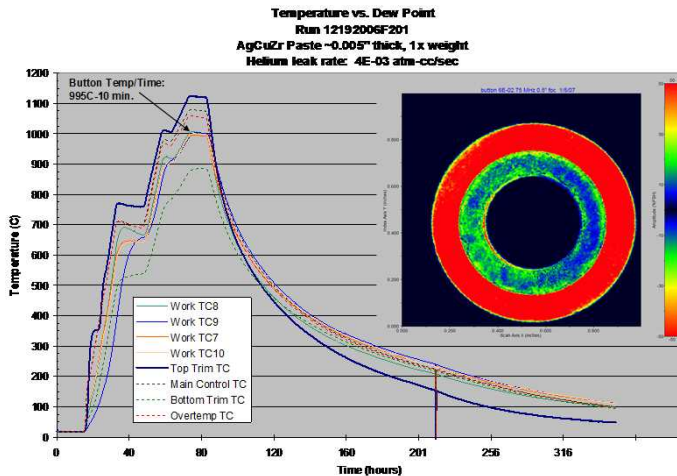
Sample run on Dec 19 received 2 thermal cycles.



Failed to reach brazing temperature.

Sample was run Dec XX and again on Dec 19.

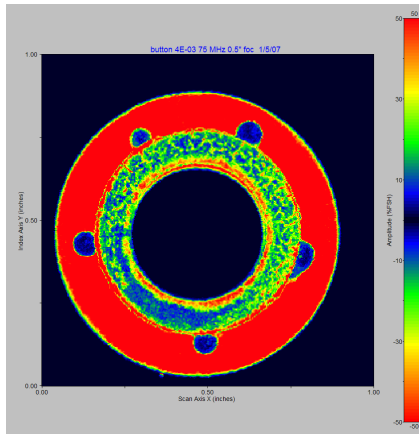
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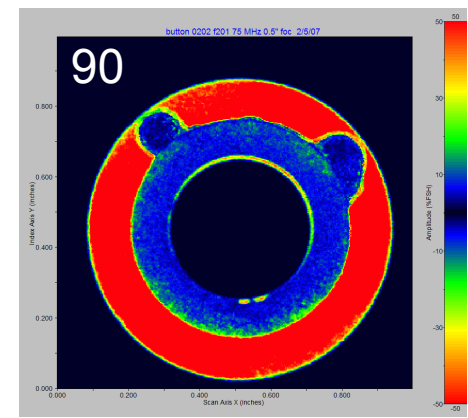
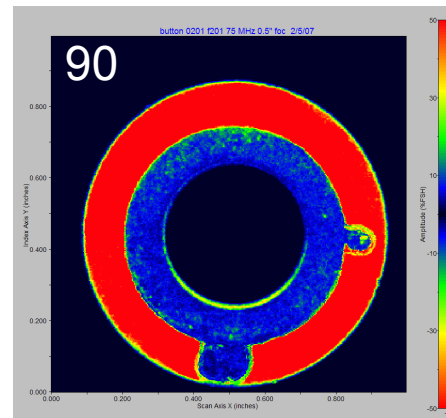
Joint Porosity Solved



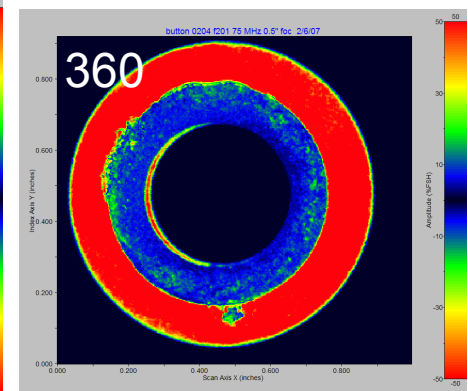
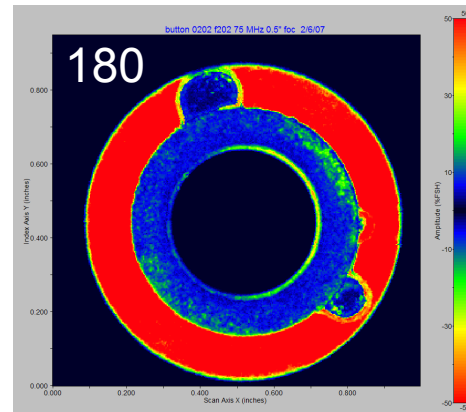
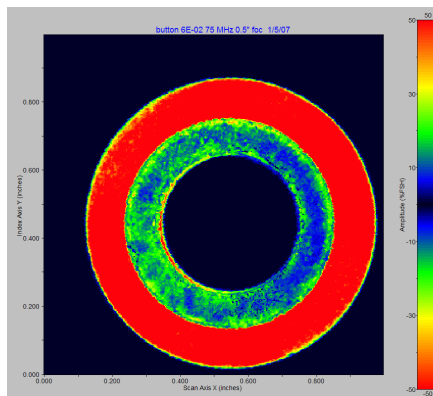
He leak rate: $6E-02$ atm-cc/sec



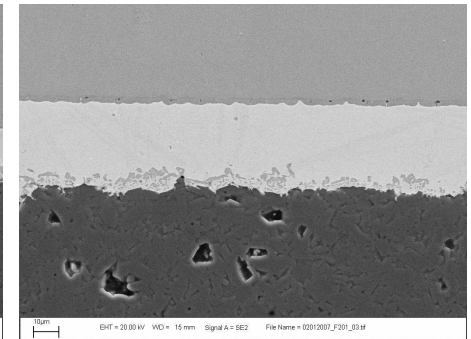
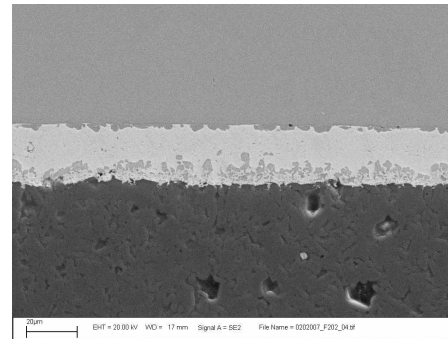
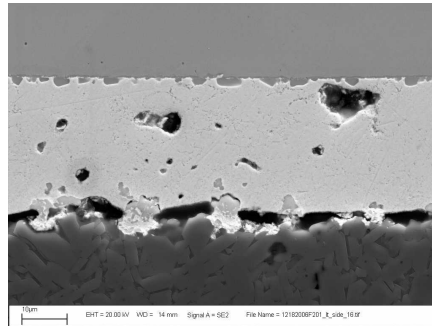
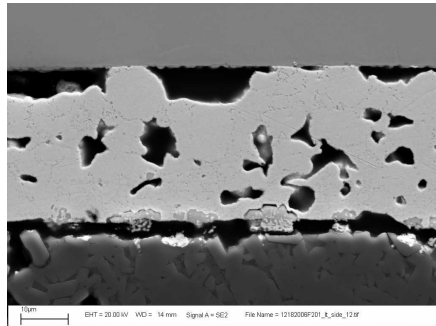
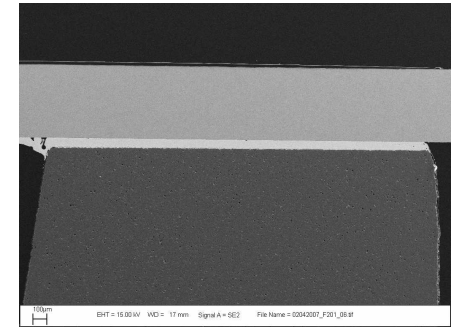
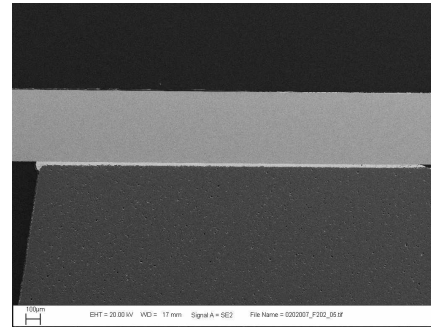
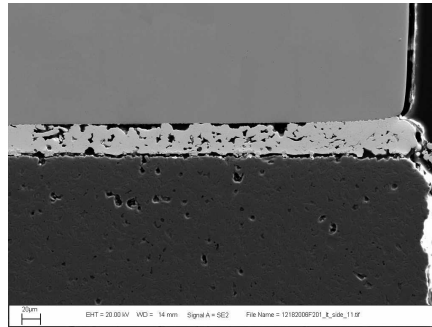
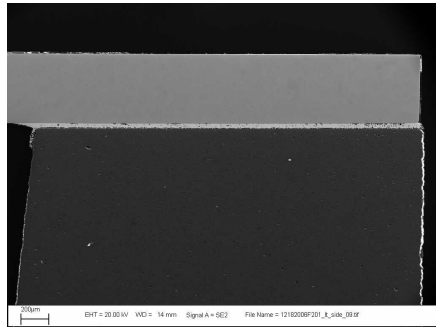
Helium Leak Rates $< 5E-09$ atm-cc/sec



He leak rate: $4E-03$ atm-cc/sec



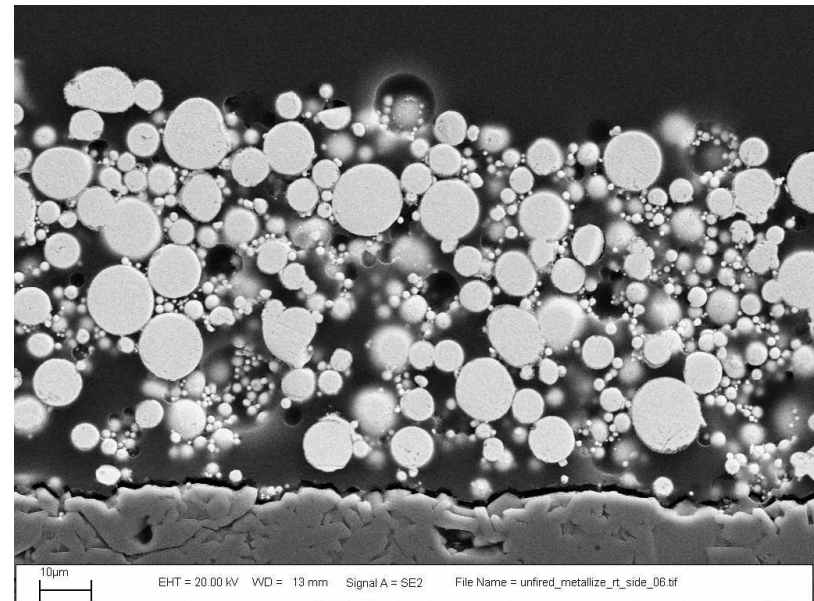
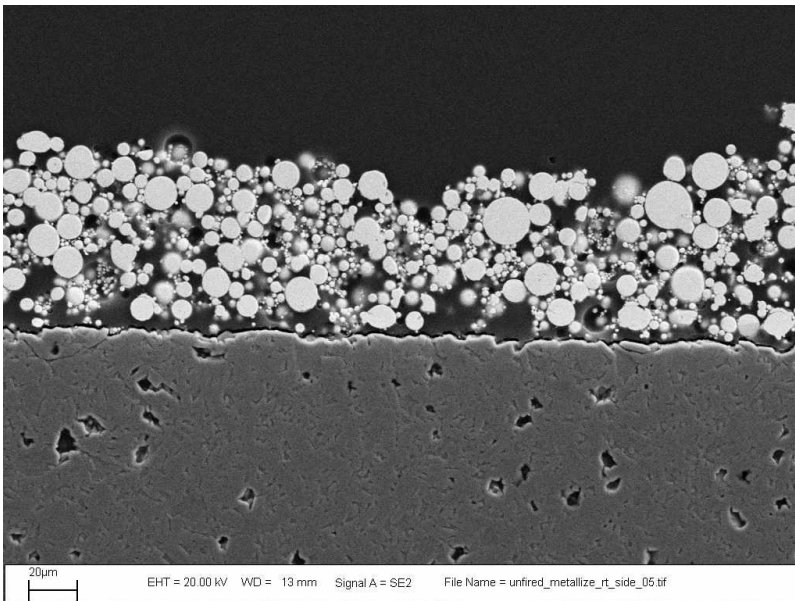
Joint Porosity Solved (continued)



January 2007

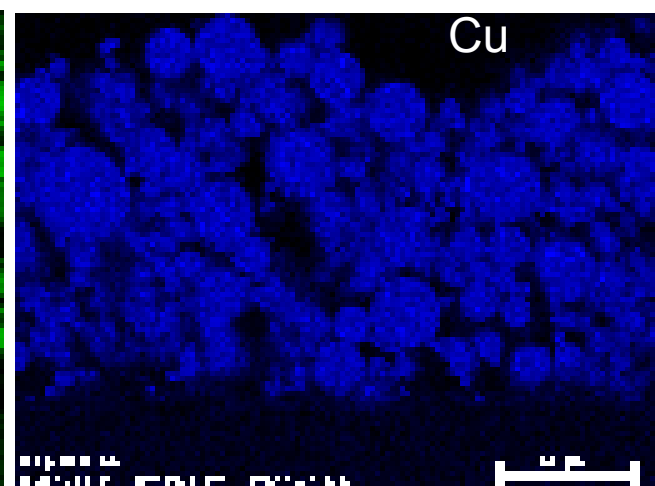
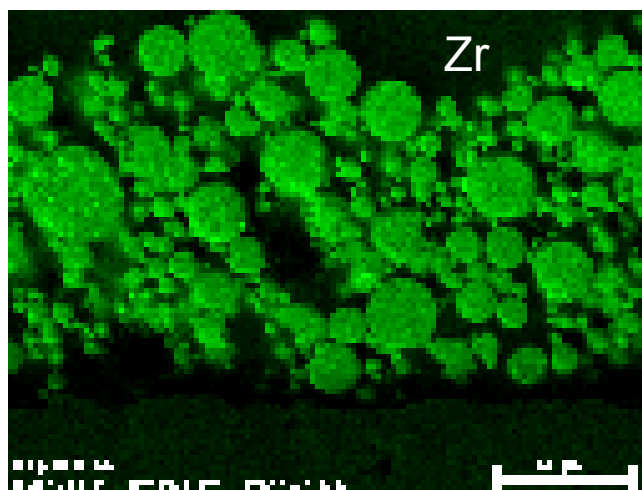
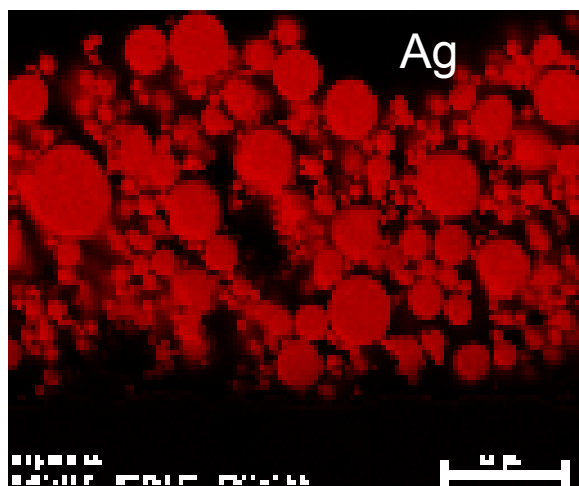
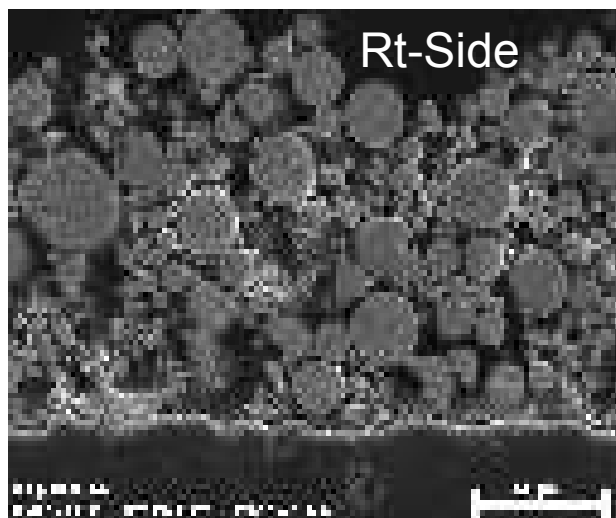
March 2007

As-Printed and Air-dried Sections Analyzed

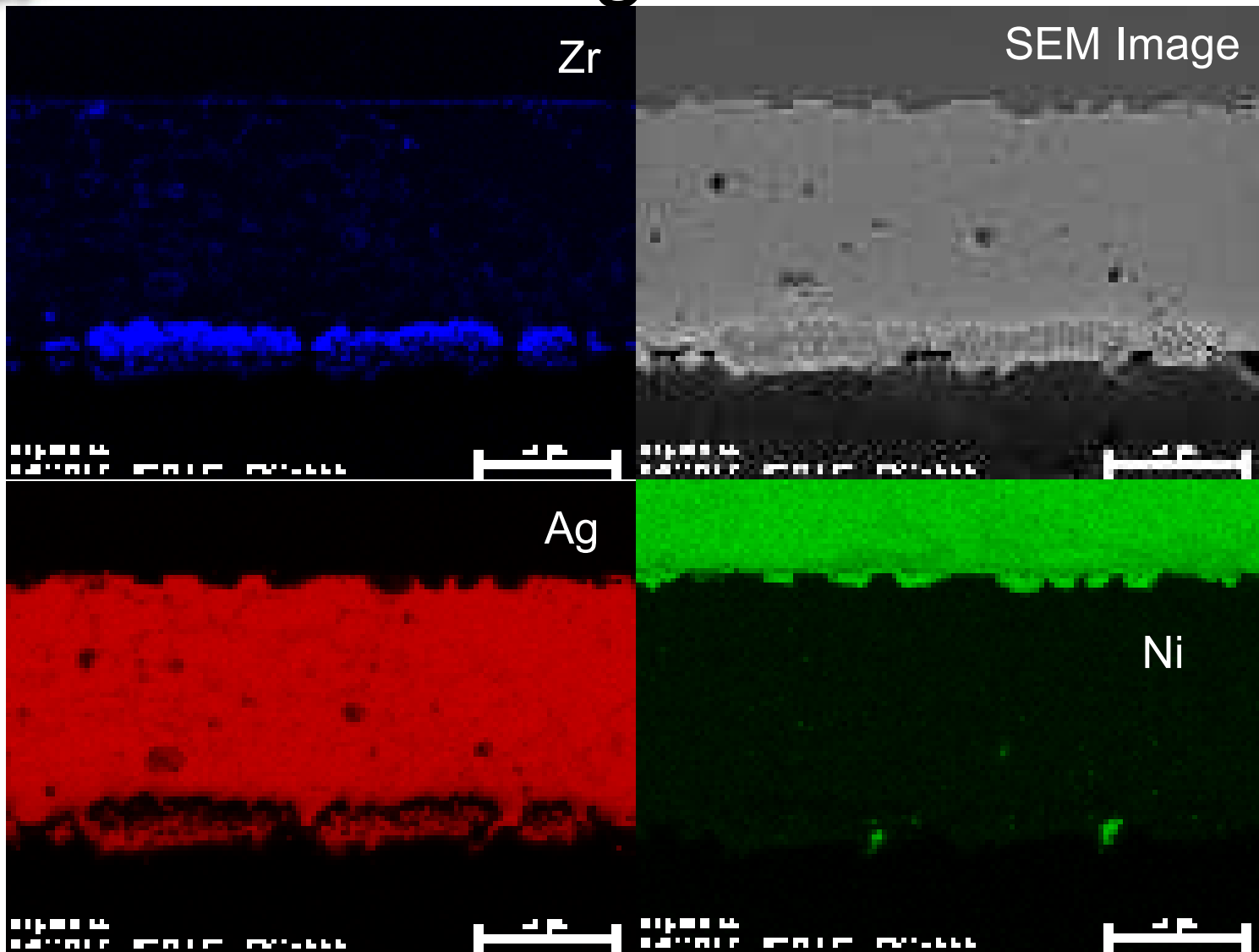


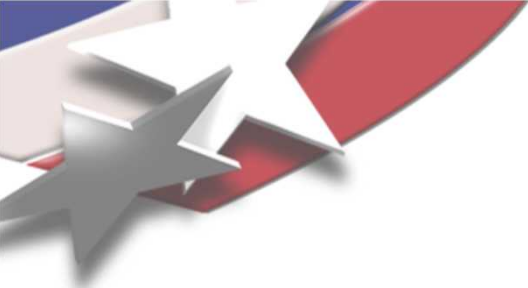
Metallography preformed by Alice Kilgo.
SEM & EDS work performed by Bonnie McKenzie

EDS Images of Air-dried paste



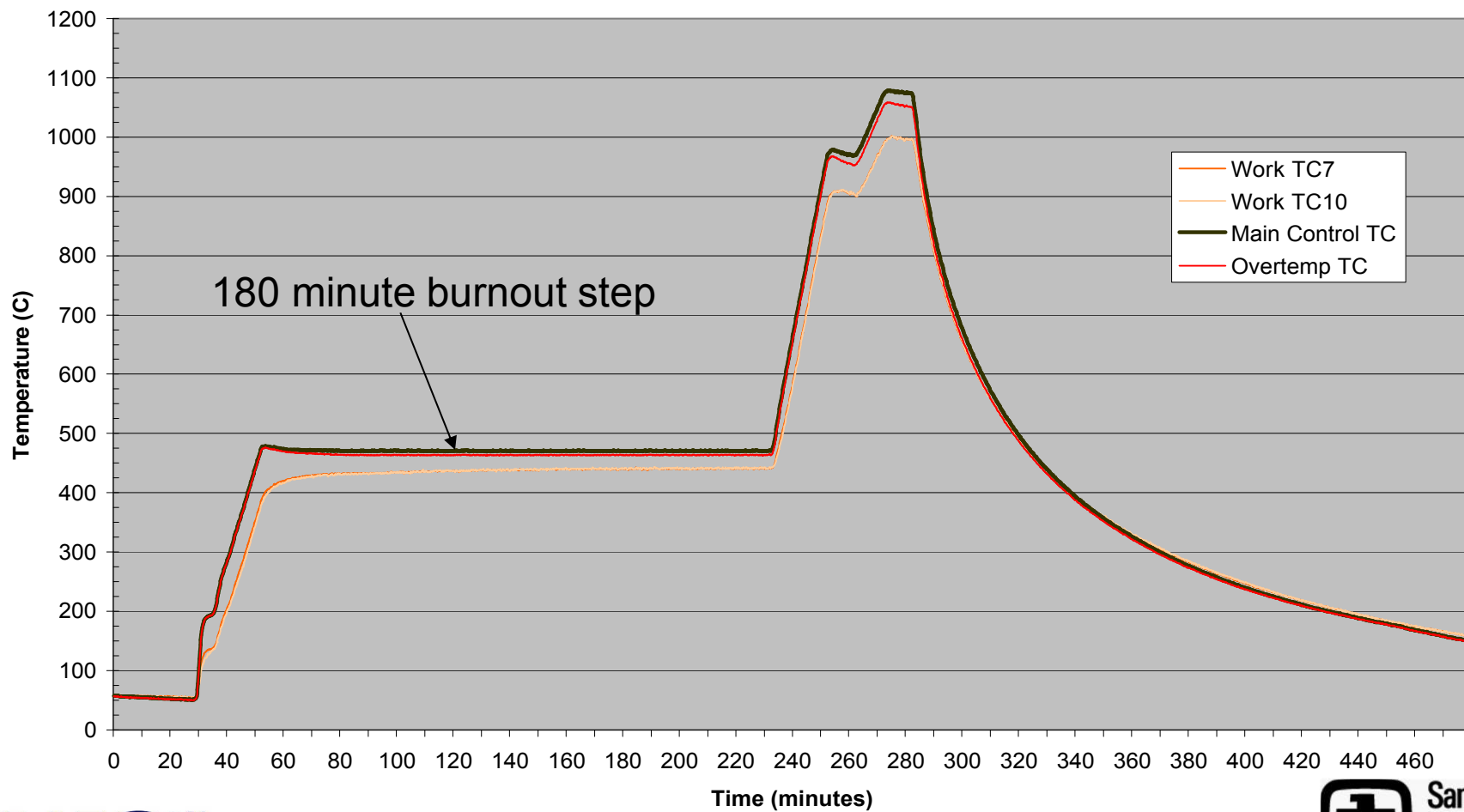
EDS Images of Brazed Joint



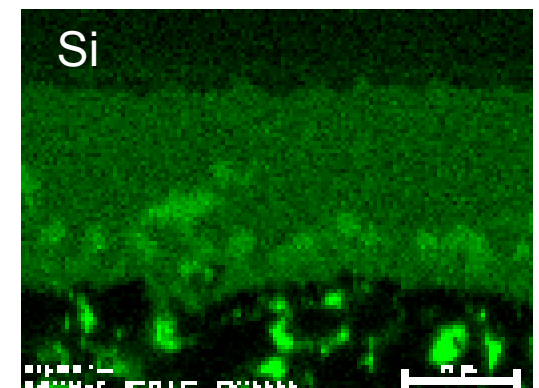
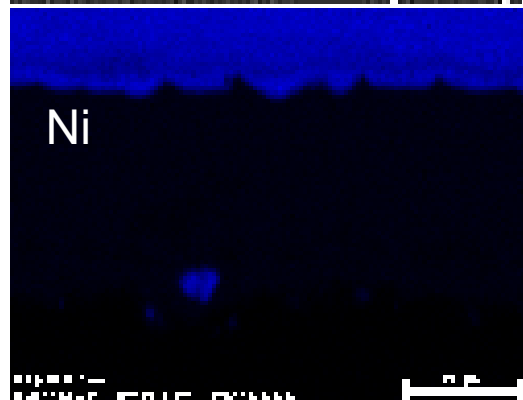
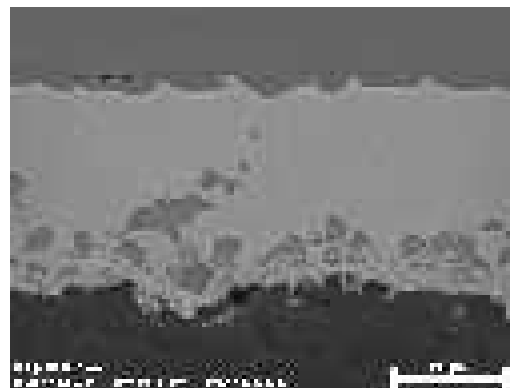
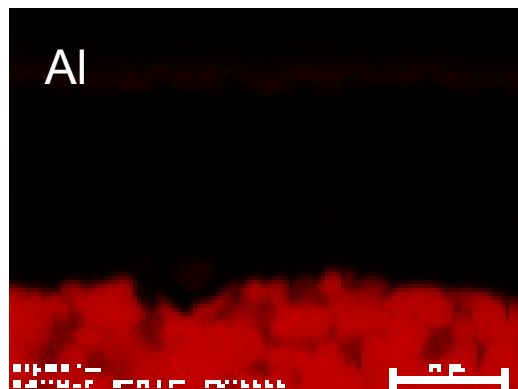
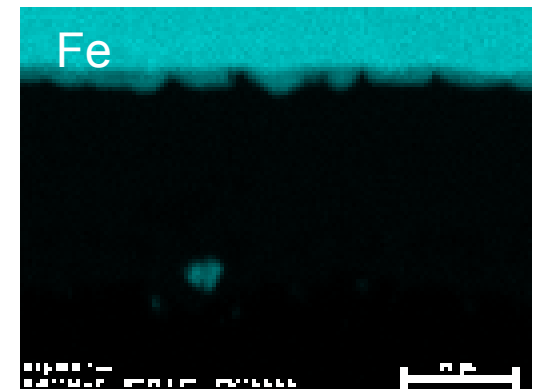
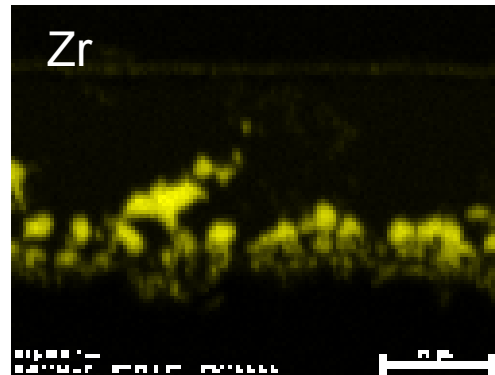
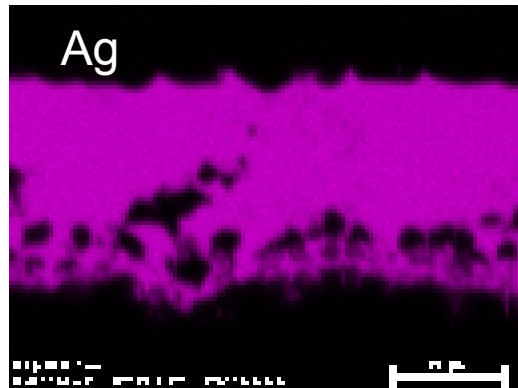


Trial 5

Temperature vs. Time
Run 02022007F202
Ag-1Cu-2Zr Paste

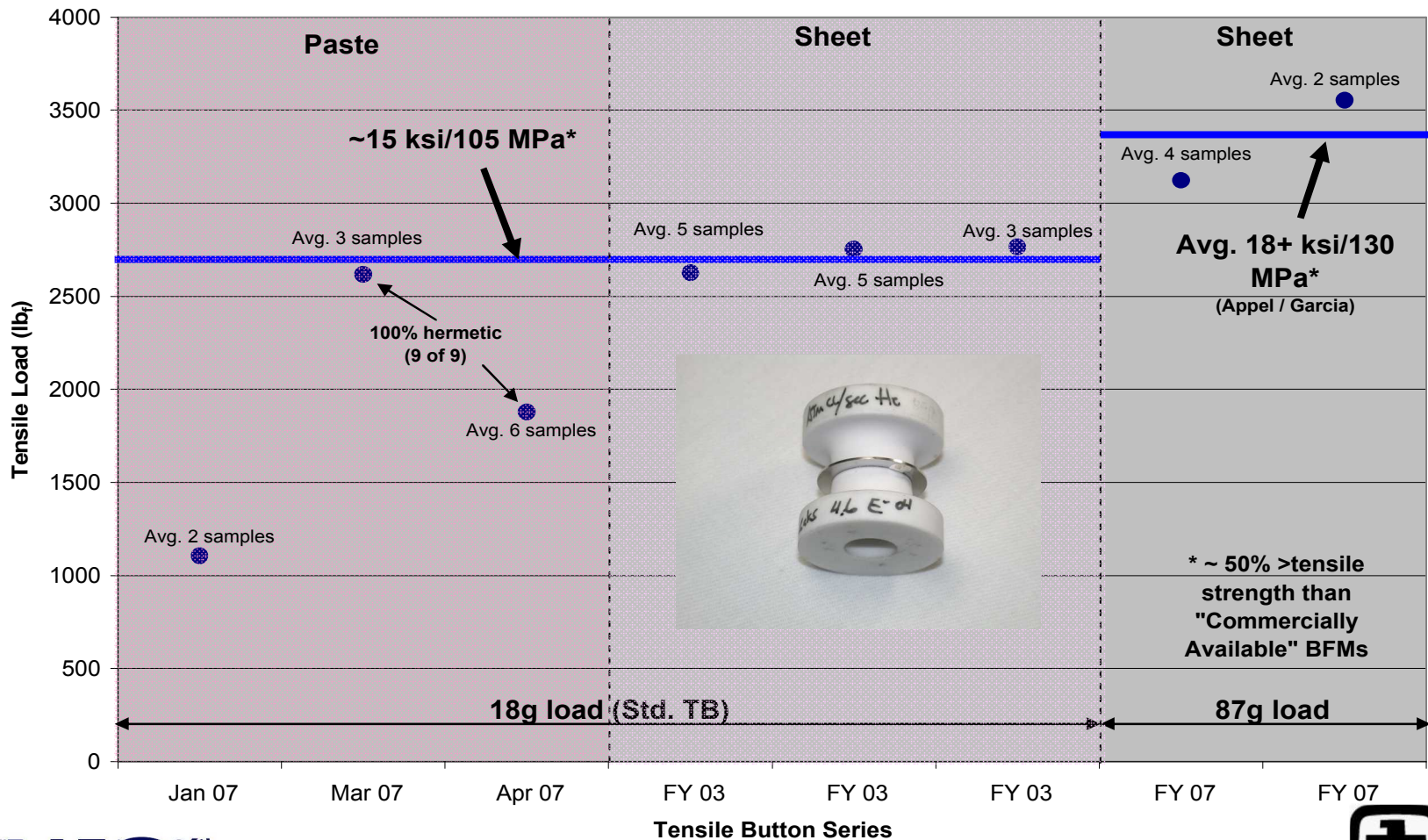


Trial 5 EDS Images



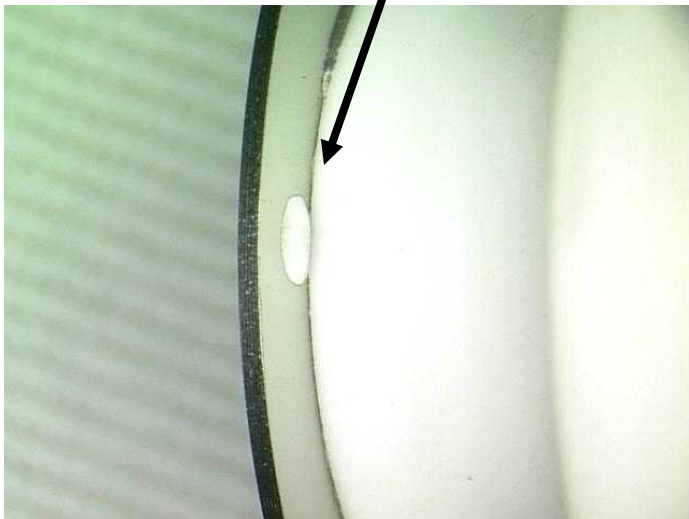
Tensile Strength Comparison Paste vs. Sheet

Ag-1Cu-2Zr
Tensile Button Strength



Braze Runout Unresolved

This condition, common with conventional braze washers could be mitigated by controlling volume (thickness) and applying surface treatment options





Current & Future Work

- 1) Eliminate the braze filler metal runout anomalies.
 - We will adjust parameters in an effort to remedy.
 - Exploration of printing the material on the Kovar™ surface to insure over-size filler metal zone.
- 2) Investigate direct application techniques on non-planar surfaces and/or more complex geometries in order to broaden the usefulness of active filler metal braze pastes.



Conclusions/Summary

- Successfully demonstrated an active braze filler metal paste screen-printing process.
- Verified that air-dried brazing paste adheres suitably to be used with standard handling procedures.
- Fabricated hermetic, porosity-free metal/ceramic brazed assemblies.
- Demonstrated similar brazed joint tensile strengths for metal foil and paste active filler metals.
- Discovered the necessity of including a low temperature extended time binder burnout step in the thermal cycle.
- The ability to rapidly change the footprint of the brazing material using inexpensive screens rather than new punches or tooling adds to the appeal of this process.
- To fully appreciate the usefulness of active filler metal braze pastes, further work in direct application techniques on non-planar surfaces and/or more complex geometries is needed.



Acknowledgements

The authors would like to thank Steven Younghouse, who performed the ultrasonic test analysis; Alice Kilgo, who performed the metallographic sample preparation; Bonnie McKenzie, for the SEM micrographs and EDS images; Tom Crenshaw, who performed the mechanical testing; and Jessica Weems for performing the supplier interfacing tasks.