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# Dynamic Behavior of Fine Sand

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Dennis Grady (ARA), John Borg (Marquette)

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March 21, 2008**



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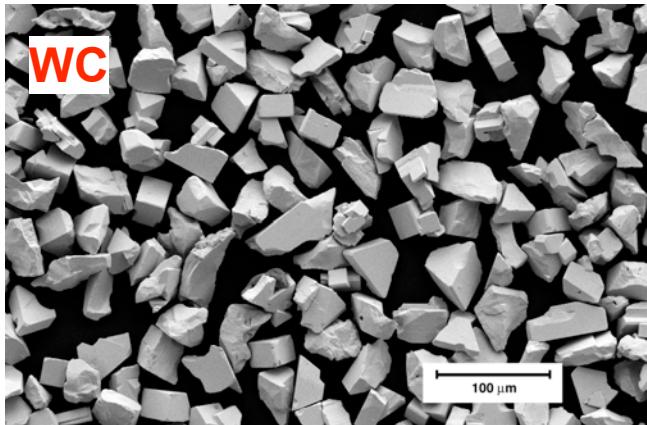




# Background

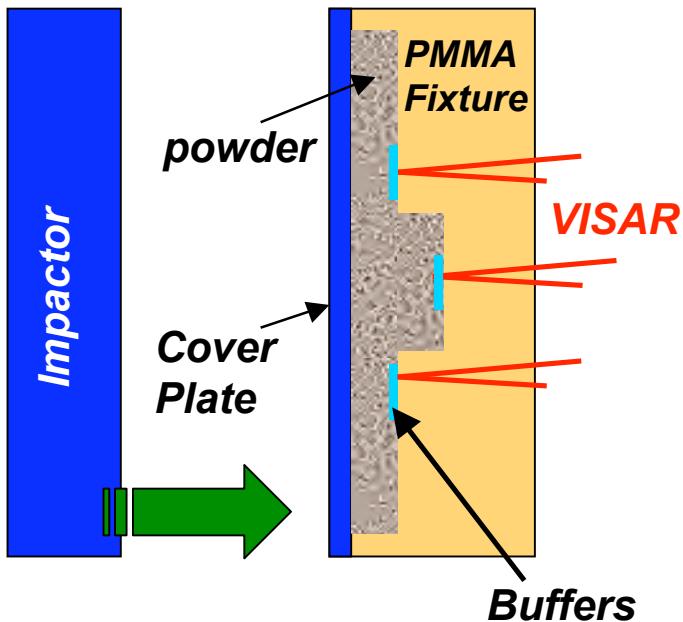
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- investigate dynamic compaction behavior of sand leveraging DOE program on granular ceramics
- develop insight into physics of dynamic behavior of these materials and the parameters that influence it
- explore a variety of techniques (quasi-static experiments, mesoscale simulations, etc.) to predict dynamic results
- determine suitability of current models within Sandia codes for simulating dynamic behavior of powders





# Planar Impact Experiments on Granular Materials



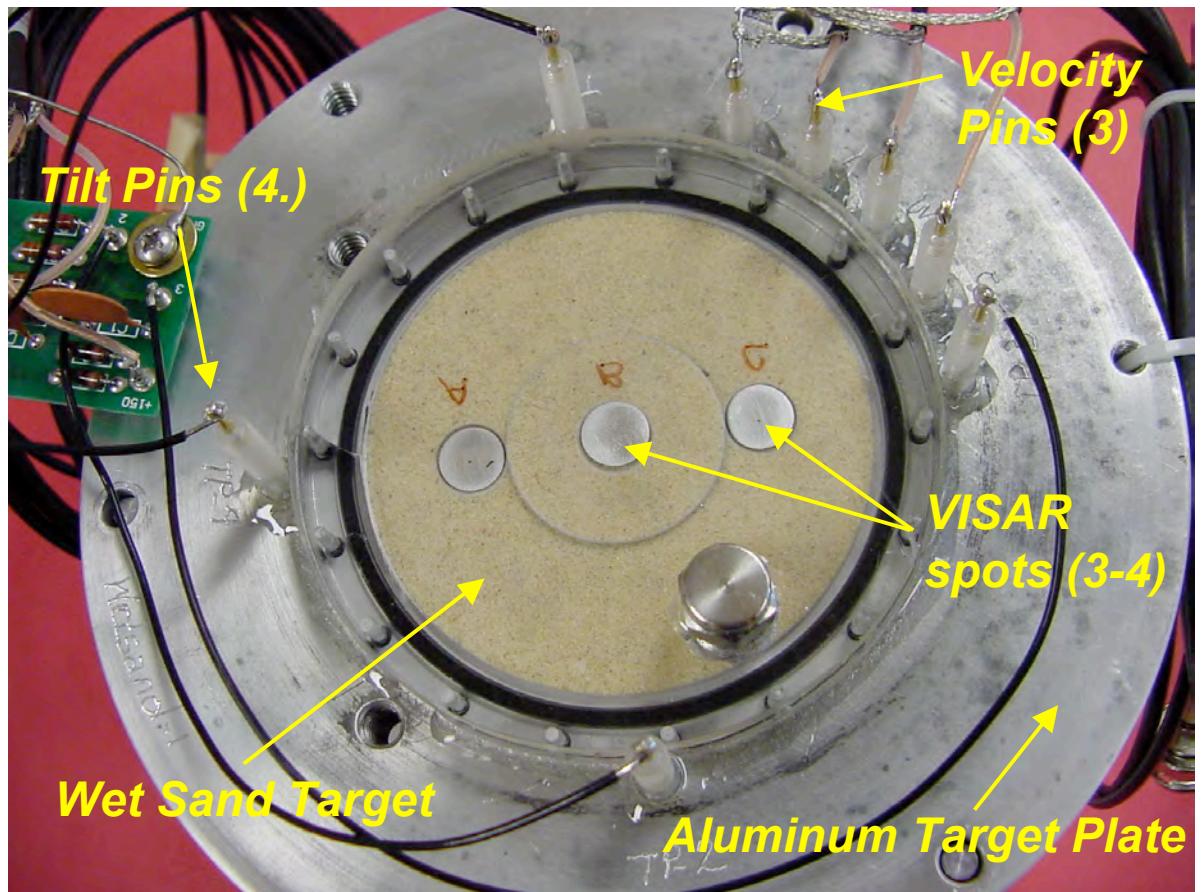
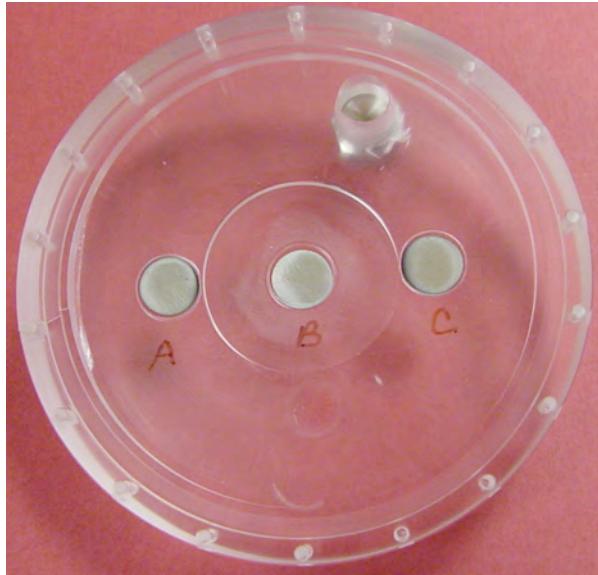
**multiple sample thicknesses on the same experiment for accurate shock velocity and uniform powder density; VISAR allows check for uniformity and steadiness**

Vogler, T.J., Lee, M.Y., Grady, D.E., 2007. "Static and dynamic compaction of ceramic powders." *International Journal of Solids and Structures* **44**, 636-658.

Brown, J.L., Thornhill, T.F., Reinhart, W.D., Chhabildas, L.C., Vogler, T.J., 2007. "Shock response of dry sand." in Shock Compression of Condensed Matter – 2007, American Institute of Physics, 1363-1366.



# Wet Sand Targets



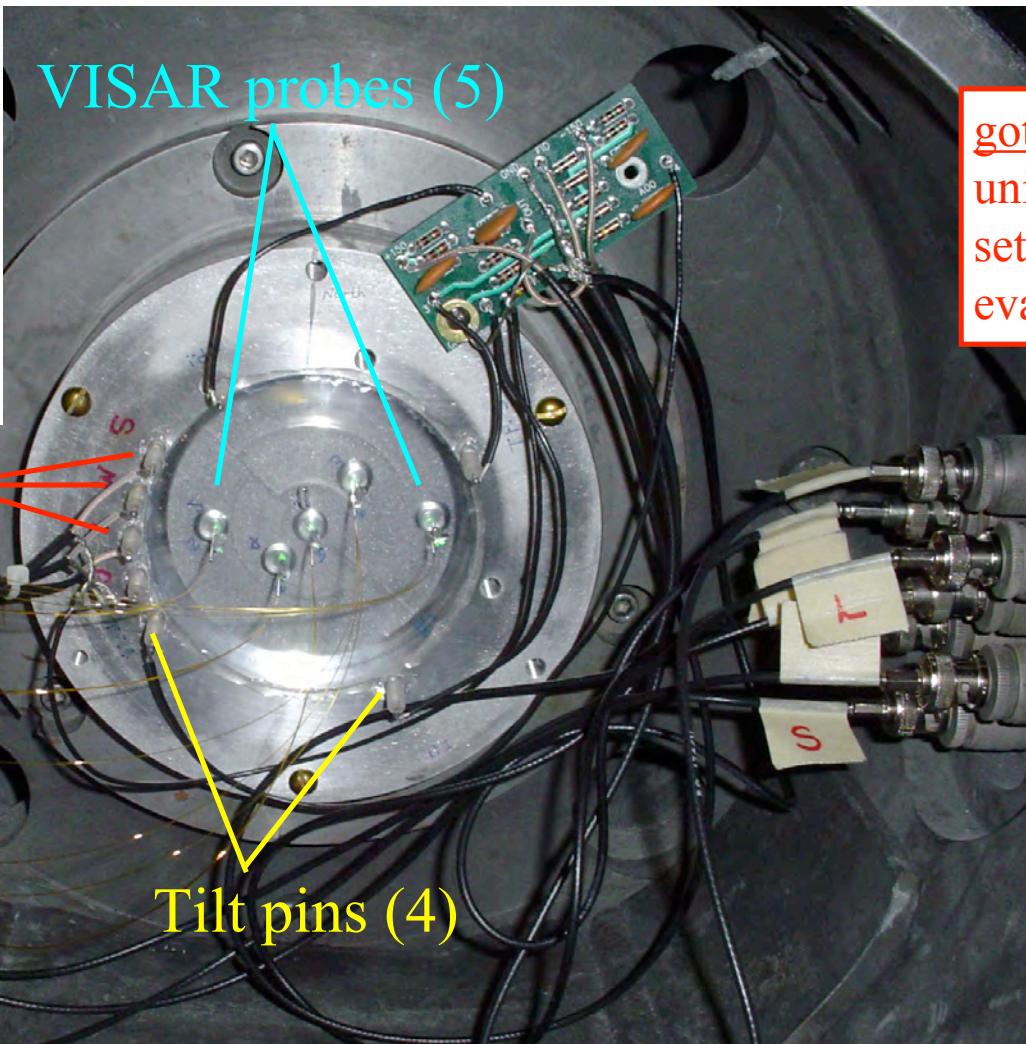


# Target Mounted in Gas Gun

**Single Stage Gun 100mm**



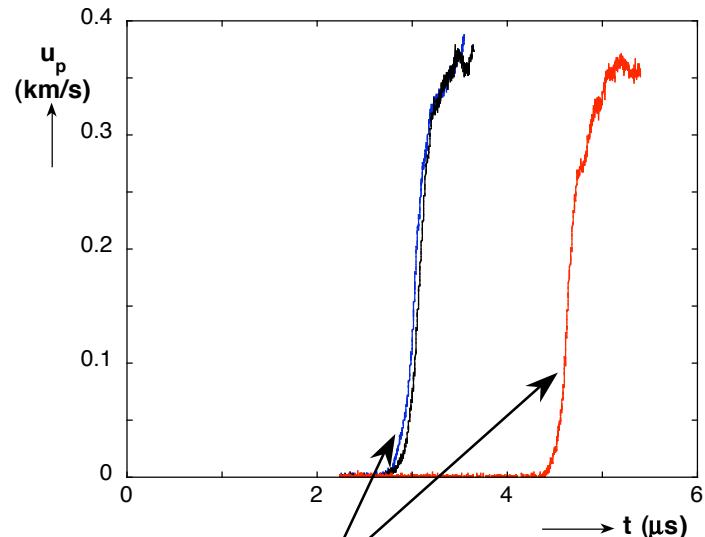
$\sim 1 \text{ km/s}$   
 $\sim 30 \text{ GPa}$



gotcha's:  
uniformity  
settling  
evacuation

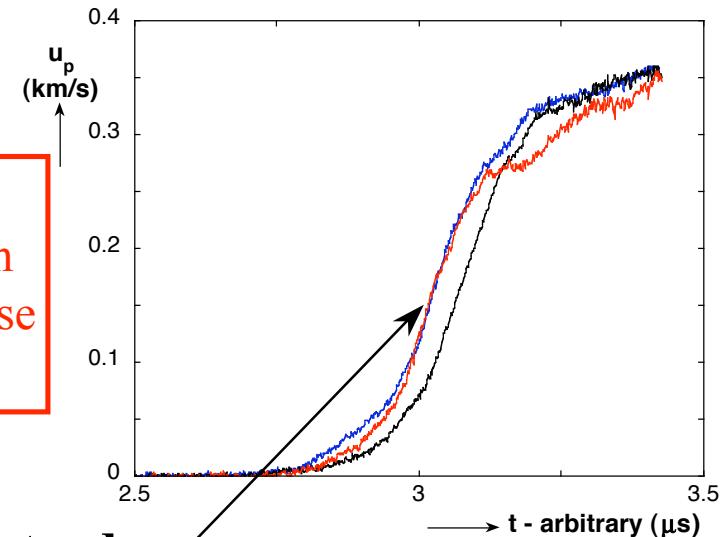


# Measured Steady Waves



**shock velocity calculated based  
on powder thicknesses and  
arrival times**

**gotcha's:**  
attenuation  
edge release  
steadiness

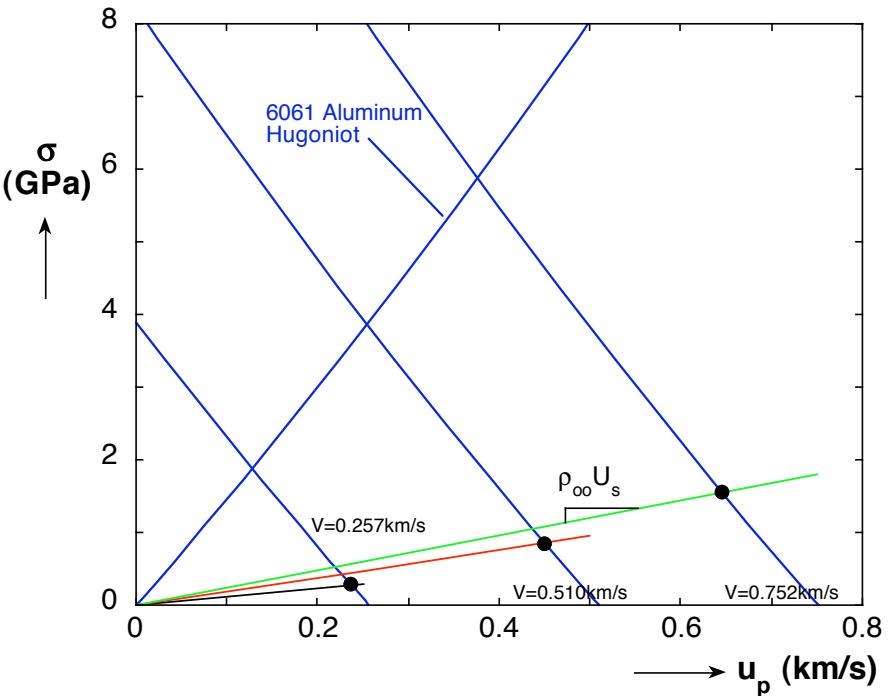
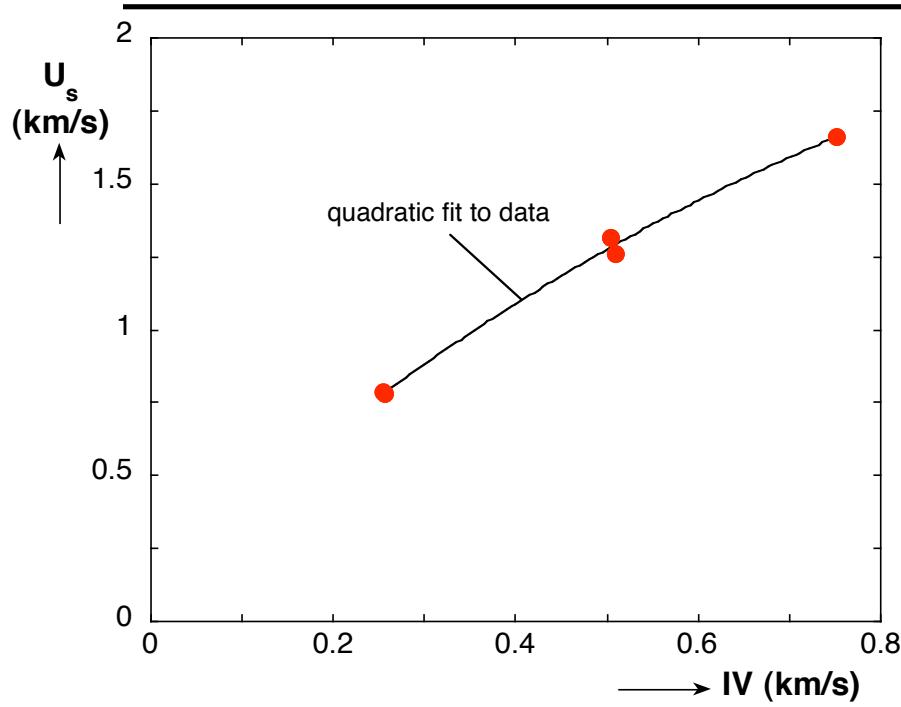


**steady,  
structured  
waves**

- since waves are steady, Rankine-Hugoniot jump conditions can be used even though waves have finite rise times



# Shock Velocities and Hugoniot States



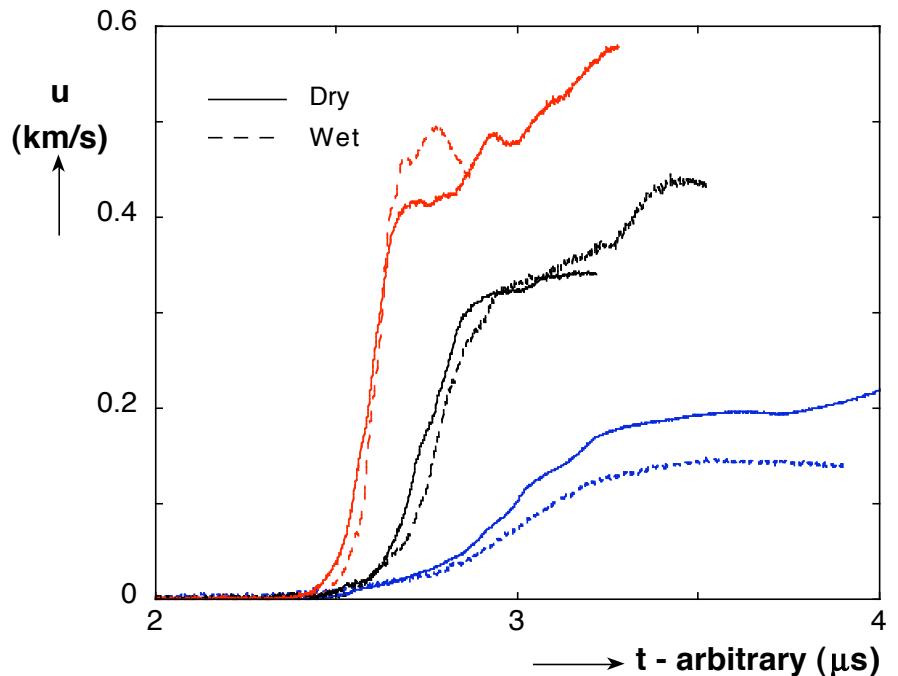
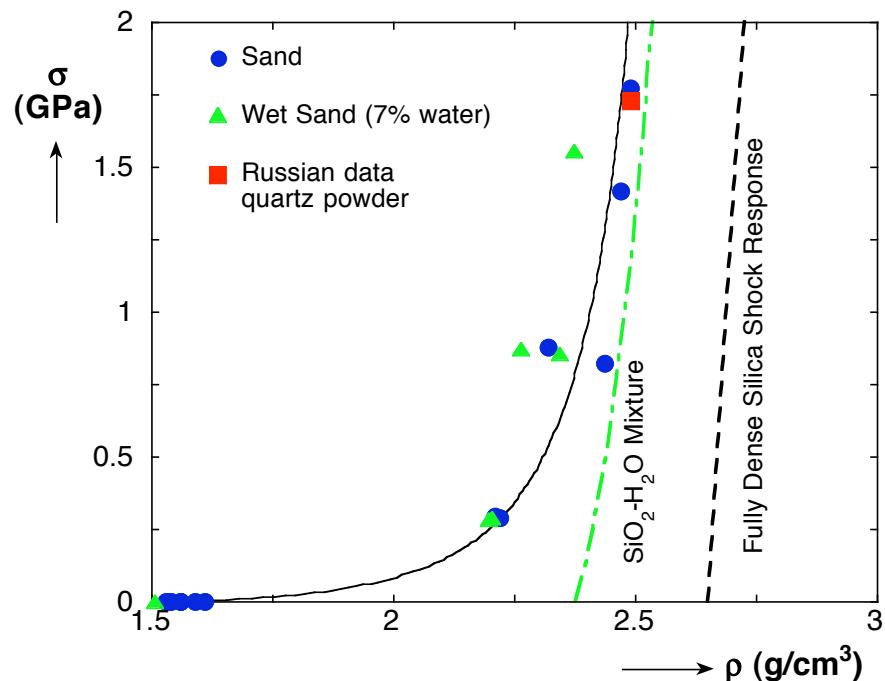
- impedance matching to aluminum impactor used to determine Hugoniot stress and particle velocity ( $\sigma = \rho_o U_s u_p$ )
- density then calculated from  $\rho = \rho_o U_s / (U_s - u_p)$



# Experimental Results

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shock data for wet and dry sand



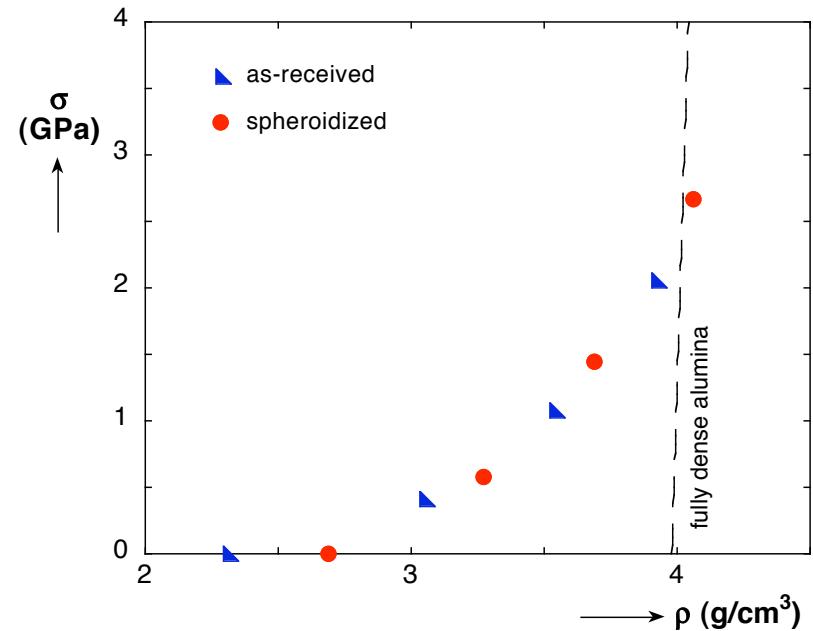
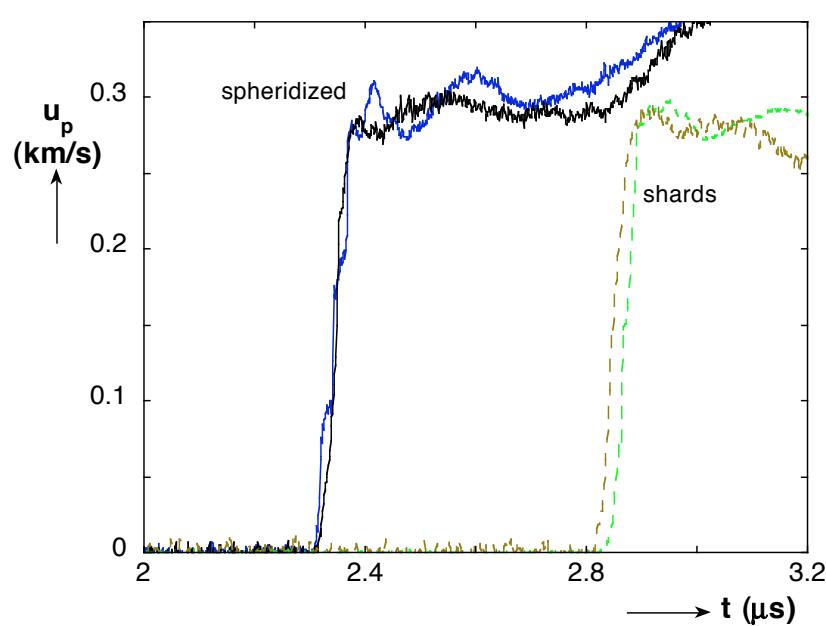
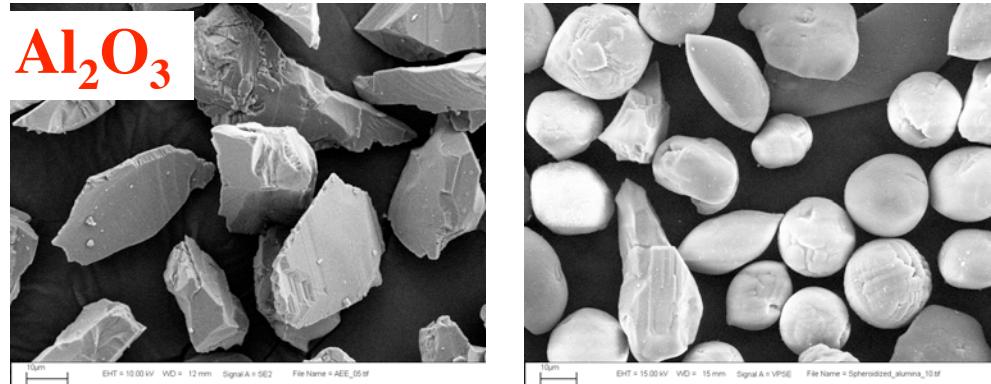
small differences in wave profiles  
between wet and dry sand

**14% moisture will be shot soon**



# Effect of Particle Morphology

plasma processing  
used to create  
spheres, changing  
particle morphology

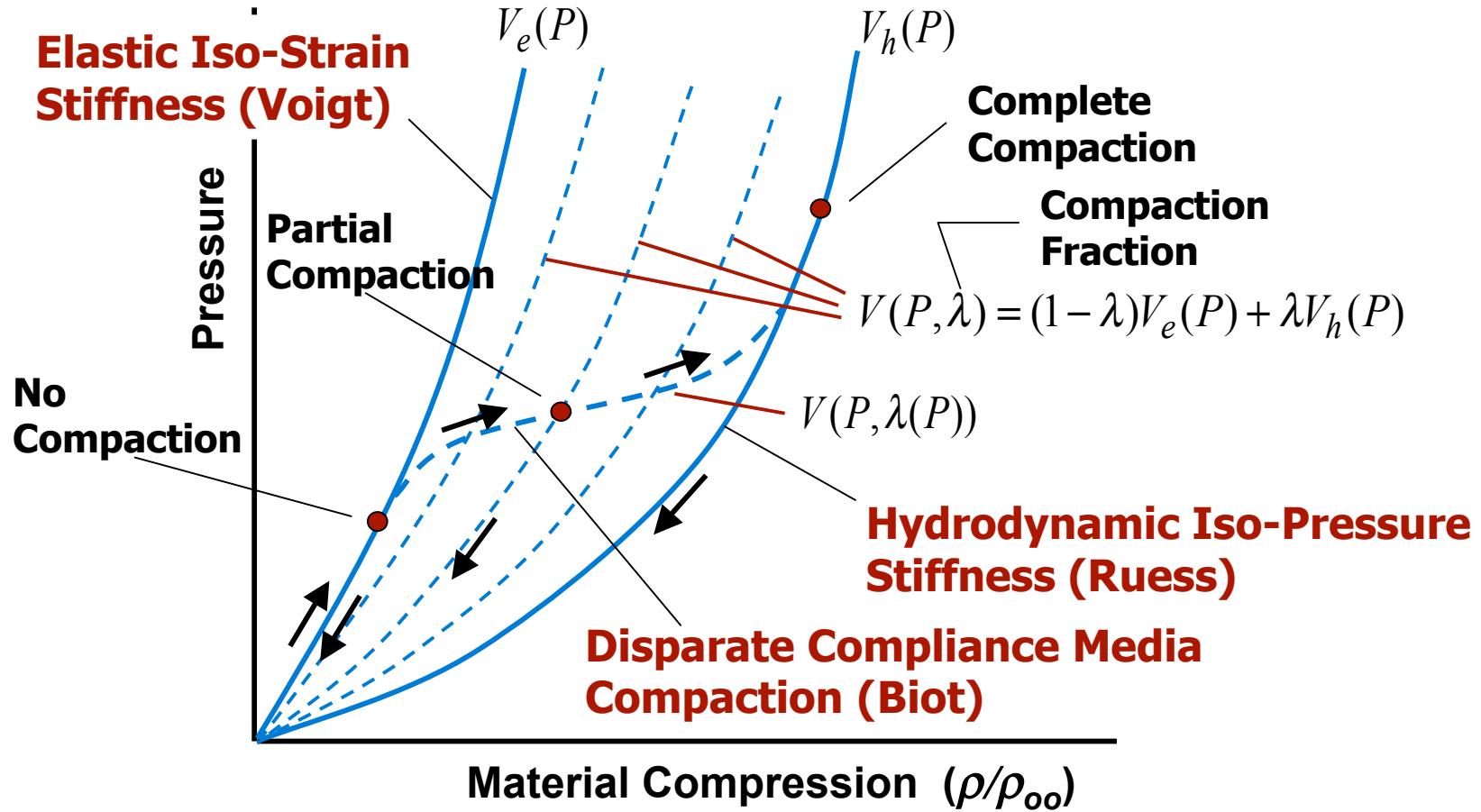


*results are insensitive to particle morphology and grain size distribution*



# Continuum P- $\lambda$ Model

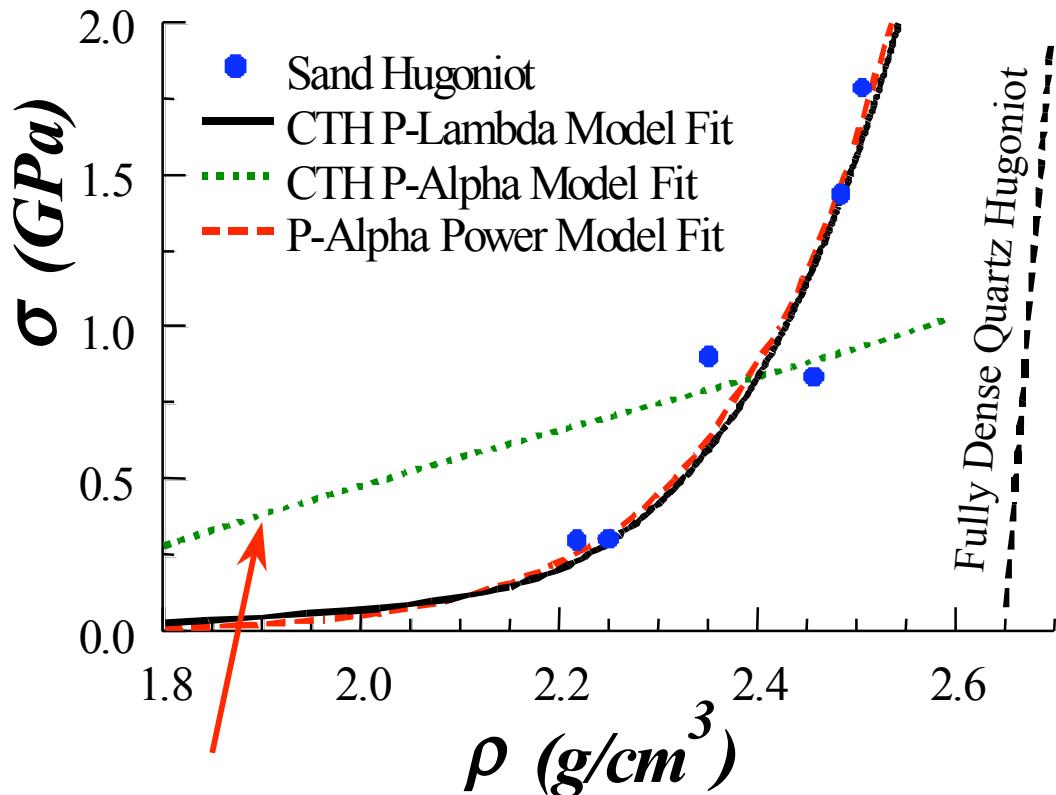
more flexible variation on P- $\alpha$  developed by Grady *et al.*; allows multiple materials but maintains simplicity of P- $\alpha$  model



Grady, D.E., 2007. "Shock wave compression of ceramics with microstructures." *International Journal of Plasticity* (in press).



# Continuum Model (P- $\alpha$ and P- $\lambda$ ) Calibration for Sand



current P- $\alpha$  form  
in CTH incorrect

## P- $\lambda$ model

$$\alpha = \rho_m / \rho$$

CTH form

$$\alpha(p) = 1 + (\alpha_0 - 1) \left( \frac{p_s - p}{p_s - p_e} \right)^n$$

alternate form

$$p(\alpha) = p_s \alpha^{-n}$$

## P- $\lambda$ model

$$v_m(p) = \lambda v_R(p) + (1 - \lambda) v_V(p)$$

$$\lambda = 1 - e^{-\left( \frac{p}{p_c} \right)^n}$$

**modification of P- $\alpha$  to correct functional form underway**



# Mesoscale Modeling of Granular Materials



- follow approach of Benson et al. for 2-D simulations
- particles idealized as circles (rods) for initial work
- constant velocity boundary condition applied
- run in CTH (explicit Eulerian finite difference code)
- Mie-Gruneisen EOS, elastic-perfectly plastic strength for powder

Borg, J.P., Vogler, T.J., (2008). "Mesoscale calculations of the dynamic behavior of a granular ceramic." *International Journal of Solids and Structures* **45**, 1676-1976.

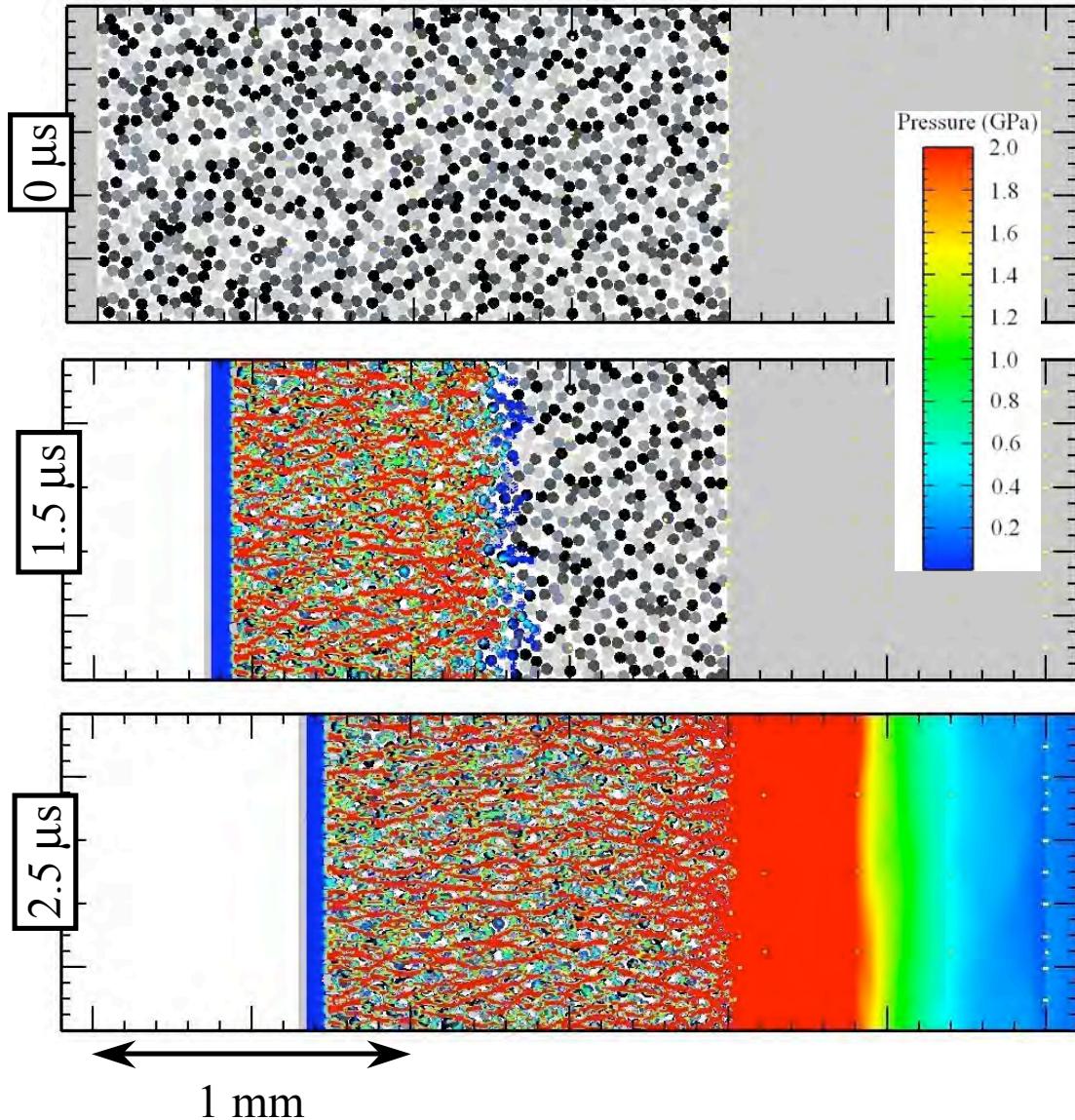
Borg, J.P., and Vogler, T.J. (2008). "Mesoscale simulations of a dart penetrating sand," *Int. J. Impact Eng.* (in press).

Borg, J.P., and Vogler, T.J. (2007). "Mesoscale calculations of shock loaded granular ceramics," in Shock Compression of Condensed Matter – 2007, American Institute of Physics, 227-230.

*get at underlying physics of granular materials*



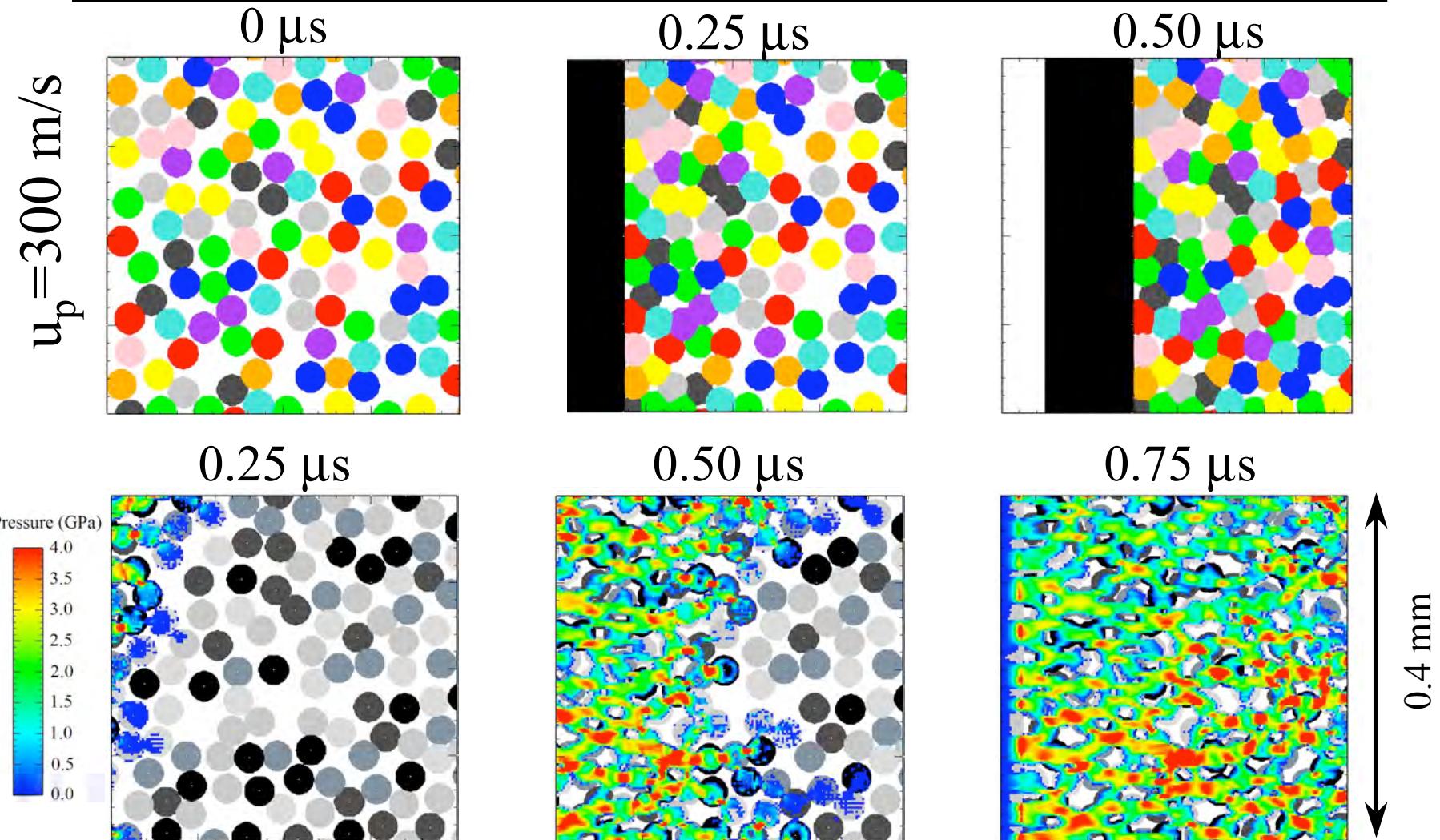
# Computational Dynamic Compaction



- **driver plate velocity**  
 $u_p = 300 \text{ m/s}$
- **shock thickness on the order of  $\sim 2\text{-}5$  particles**
- **strong force chains observed**
- **wave smooths in buffer**



# Close-Up of Compaction Process



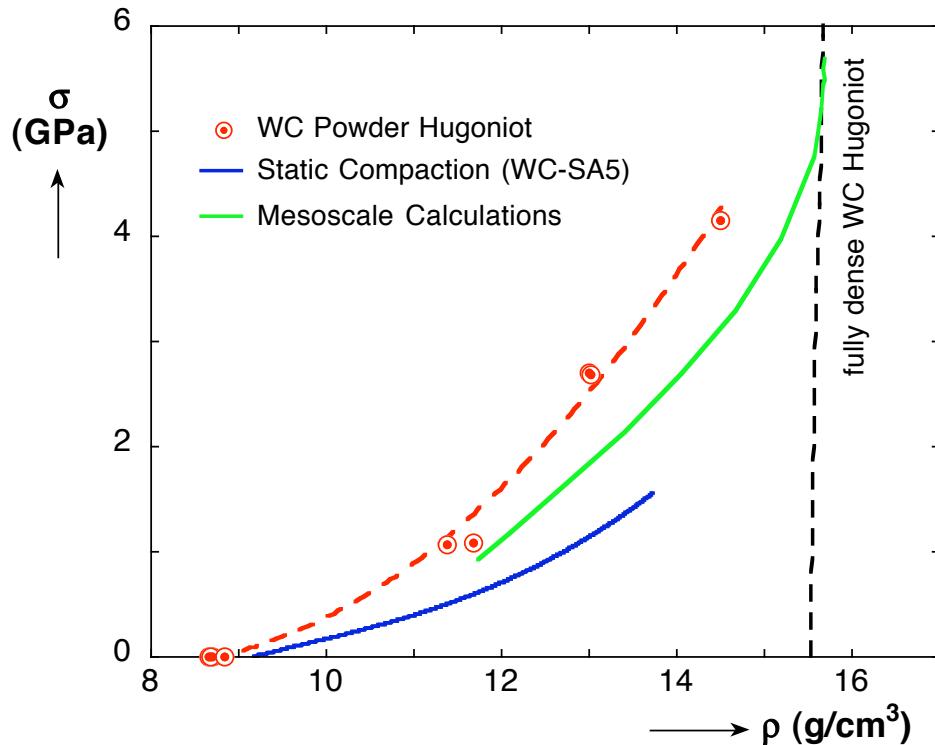
no jetting or vortices so deformation is “*quasi-static*”  
(Benson et al., 1997)



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# Calculated Hugoniot from Literature Parameters



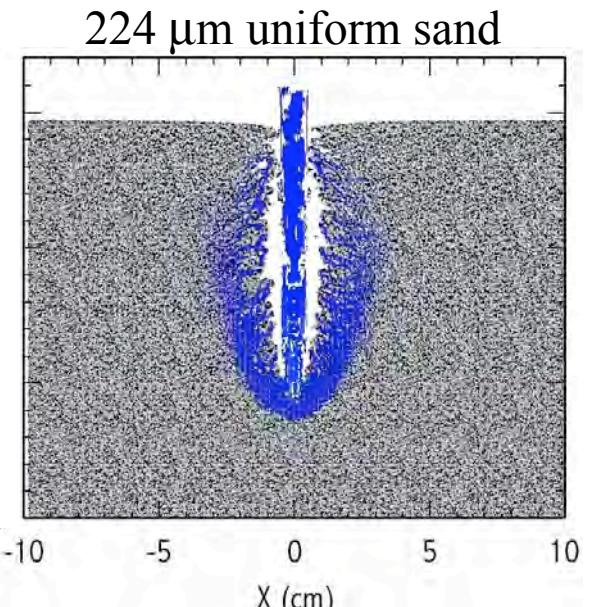
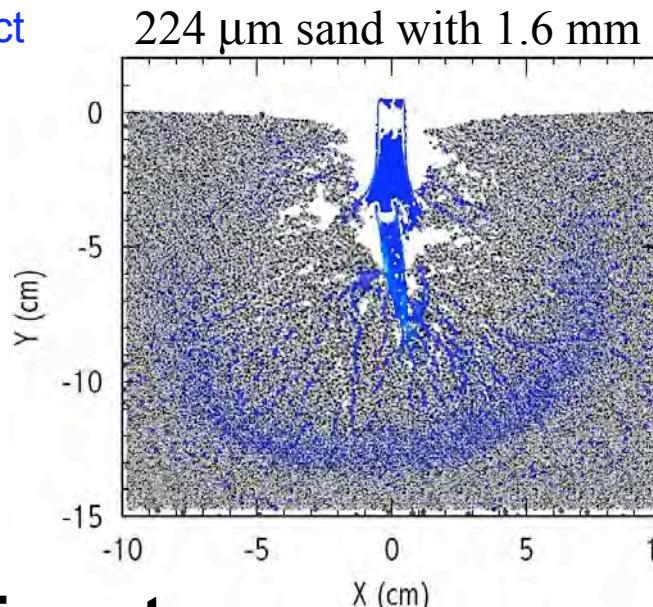
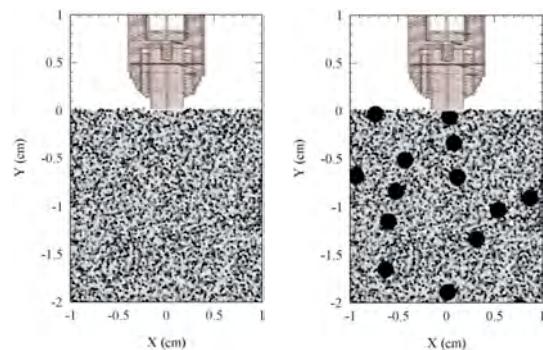
$$\sigma = \rho_o U_s u_p$$
$$\rho = \rho_o \frac{U_s}{U_s - u_p}$$

- simulations provide reasonable estimate for Hugoniot
- shortcomings of model:
  - missing physics of granular contact and fracture
  - wrong connectivity in 2-D
  - spherical particles unrealistic
  - inaccurate strength for small particles

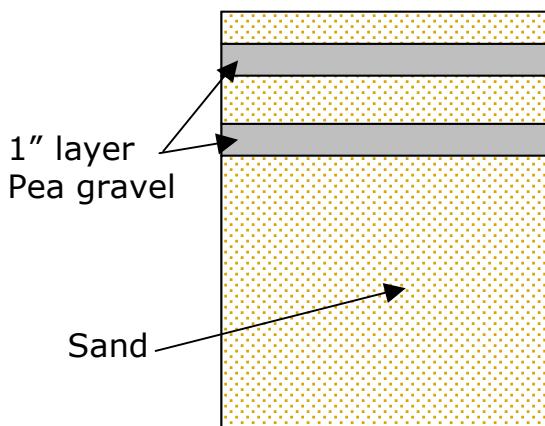
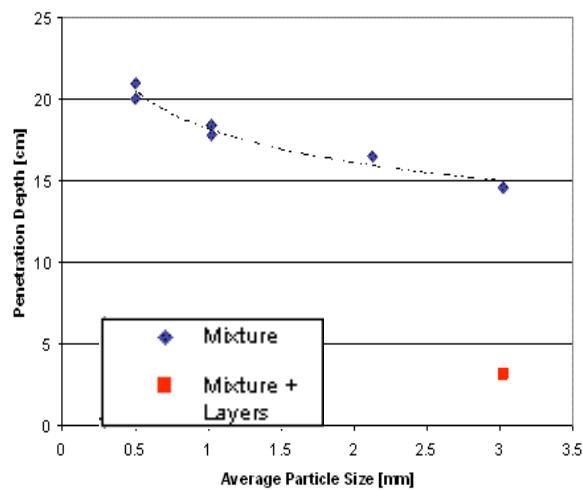


# “System Level” Work providing insight into nonuniform targets

Borg and Vogler, Int. J. Impact  
Engineering (in press)



## small-scale experiments

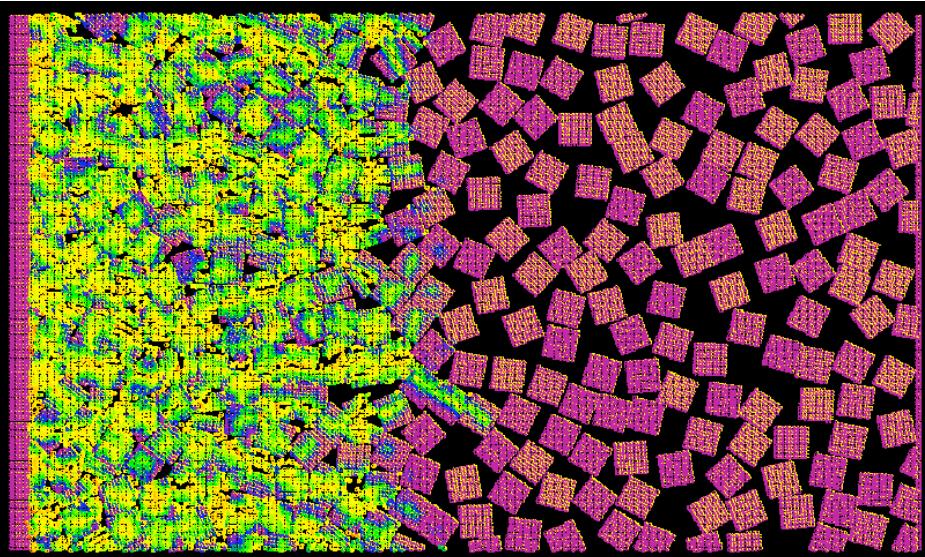
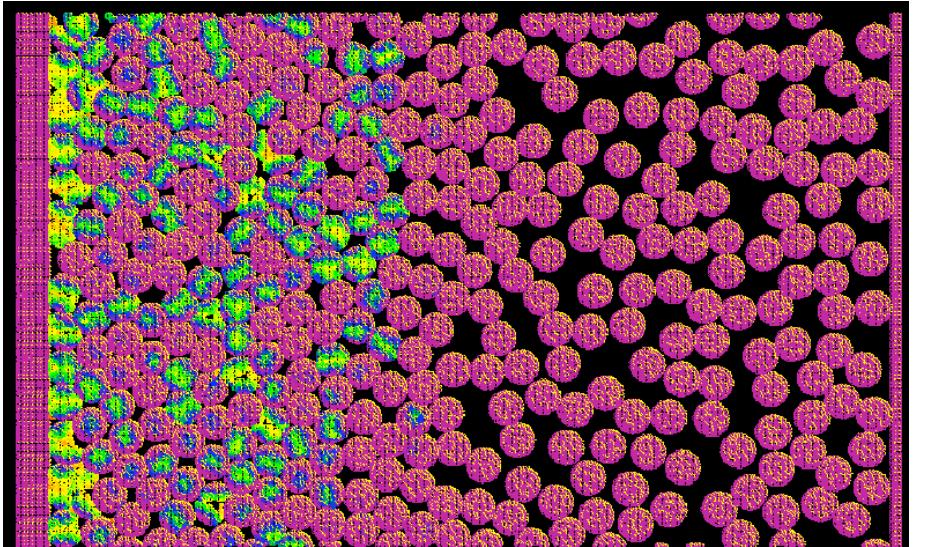


mesoscale simulations  
in progress to  
understand deflection  
mechanism



# Initial Mesoscale Calculations with Peridynamics

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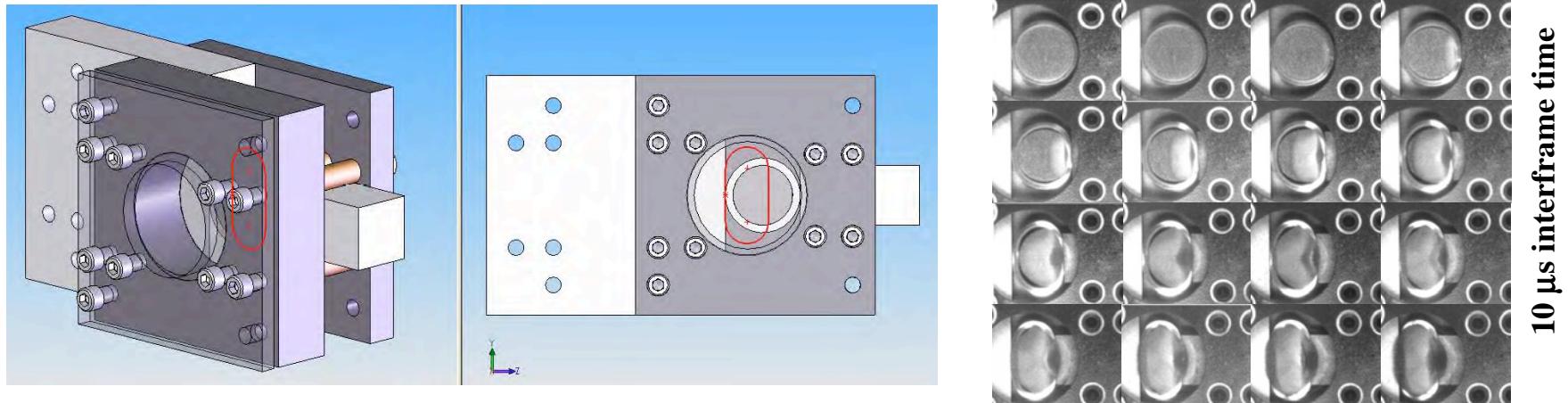


- non-local method based on reformulation of governing equations in integral form (Silling, 2000)
- includes fracture and contact missing from CTH
- behavior somewhat different than for CTH
- response insensitive to particle shape despite large differences in particle fracture

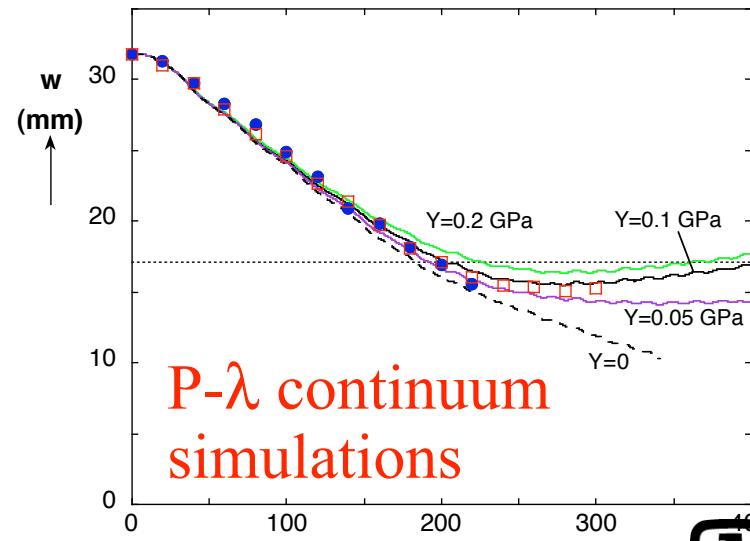
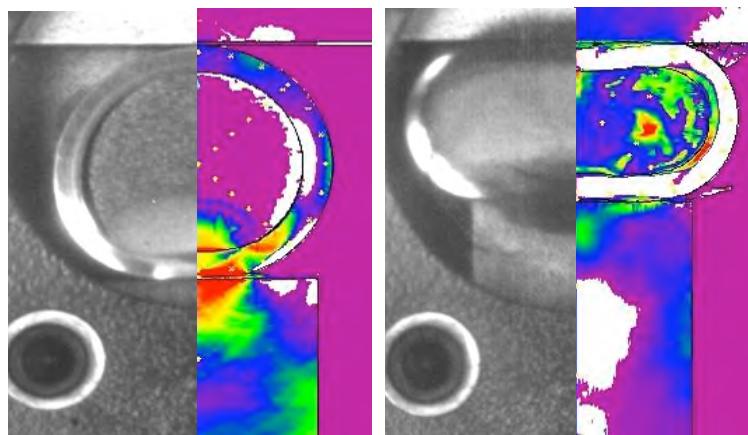


# Dynamic Validation Experiments: necessary to build confidence in models

Ring compaction experiments provide data for non-planar deformation



## 2-D CTH continuum calculation



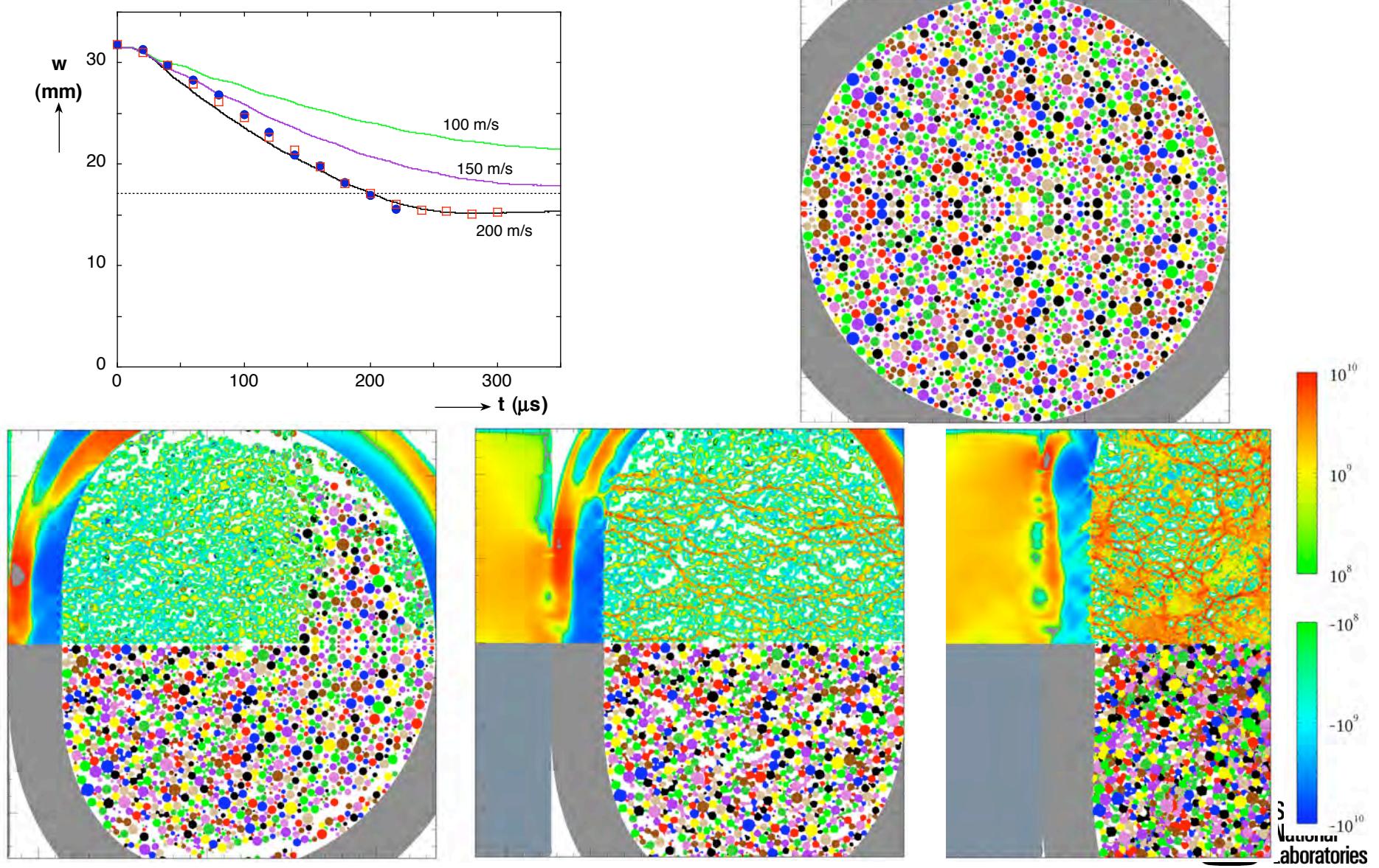
P- $\lambda$  continuum  
simulations



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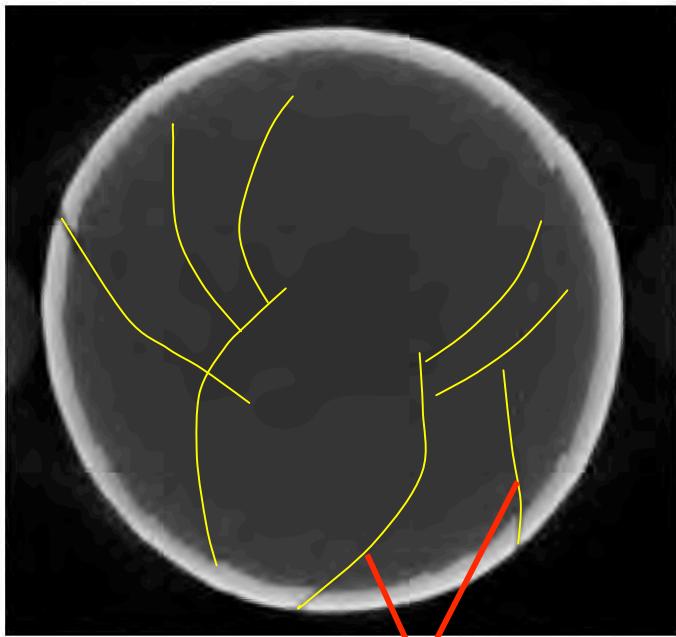


# Mesoscale Simulations of Rings





# Validation Experiments: Explosively Loaded Cylinder



compaction  
bands



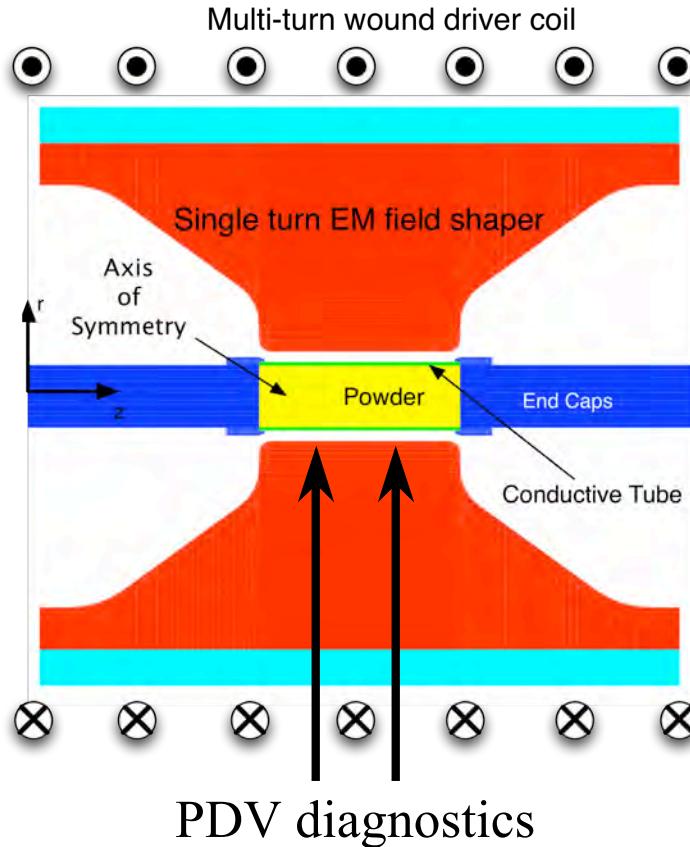
- explosively compacted cylinders to allow comparison with simulations and analytic solutions
- more difficult than expected; also late time effects
- tomographic analysis of compaction difficult and reveals localizations





# Magnetically Driven Cylindrical Compaction

in collaboration with G. Daehn (Ohio State Univ.) and G. Fenton (ARA)



will provide high-quality dynamic measurements  
in a simple (but non-planar) configuration



# Summary and Future Work

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- constructed capsule for wet sand experiments; completed planar impact tests on 7% wet sand; tests on 14% underway
- provided calibration of P- $\alpha$  and P- $\lambda$  models for dry sand (modification to P- $\alpha$  underway)
- particle morphology appears relatively unimportant
- particle fracture does not appear to be important
- layered or nonuniform targets may have significant effects

## Future Work

- planar impact tests for clayey sand
- validation experiments (additional ring crush and magnetically-driven compaction); continuum and mesoscale modeling
- additional study of morphology effects
- extend mesoscale simulations to 3-D