



# Dynamic Behavior of Granular Ceramics

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Tracy Vogler

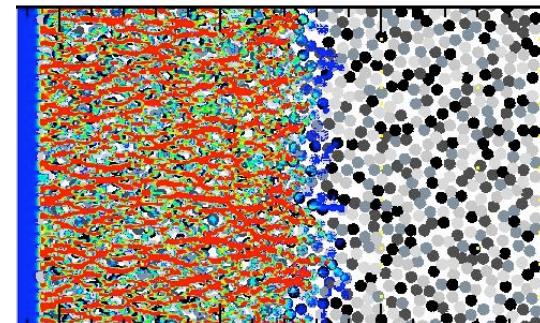
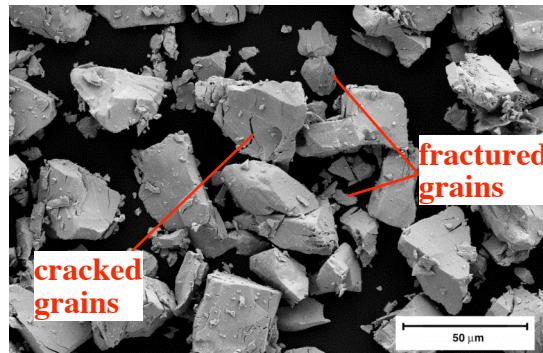
**Solid Dynamics and Energetic Materials Dept.  
Sandia National Laboratories**

## Project Team:

**J.P. Borg, D. Sandoval, K. Lappo, T.F. Thornhill, J. Brown,  
C.S. Alexander, W.D. Reinhart, D.E. Grady, L.C. Chhabildas**

## AFOSR Workshop on Particulate Mechanics in Extreme Environments

Eglin AFB  
January 29-31, 2008



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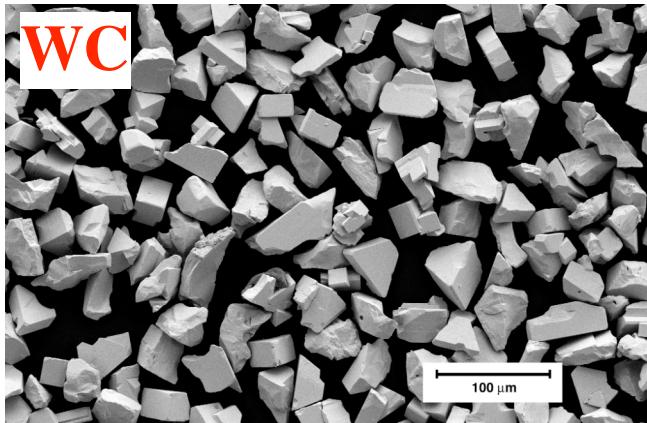


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# Investigation of Dynamic Behavior of Granular Ceramics

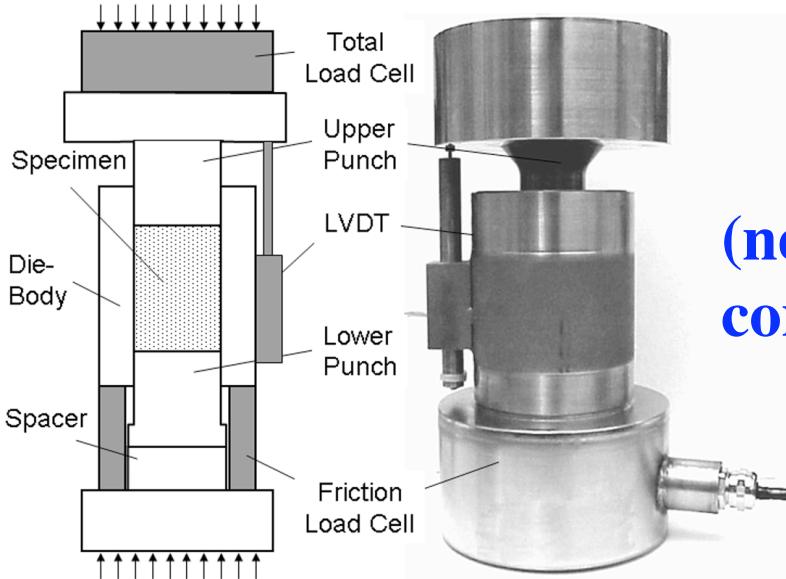
- investigate dynamic compaction behavior of ceramic powders (WC, sand,  $\text{Al}_2\text{O}_3$ , etc.)
- develop insight into physics of dynamic behavior of these materials and the parameters that influence it
- explore a variety of techniques (quasi-static experiments, mesoscale simulations, etc.) to predict dynamic results
- determine suitability of current models within Sandia codes for simulating dynamic behavior of powders





# Static Die Compaction Experiments

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(nearly) uniaxial strain compaction to ~1.6 GPa

## Objectives

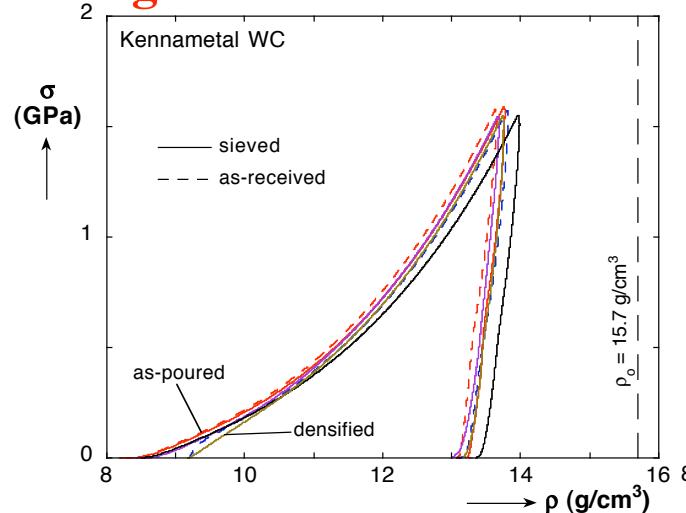
- Determine compaction curve functional form
- Examine effects of experimental parameters (grain size, grain size distribution, grain shape, initial density, loading path, etc.)
- Correlate with dynamic results



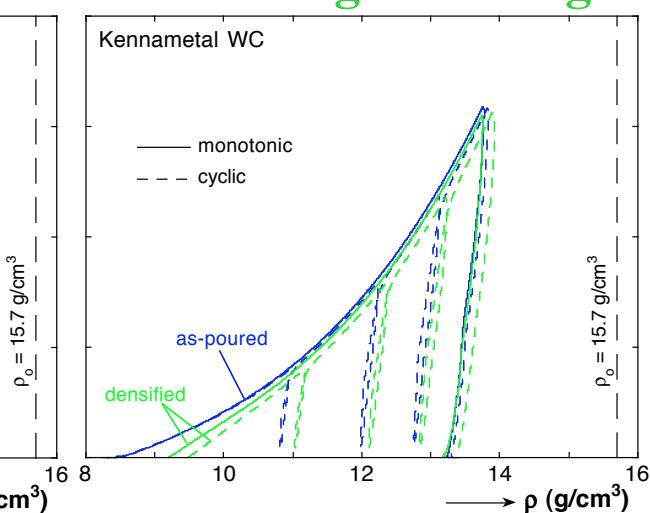
# Static Compaction Results

evaluate effects of important variables on loading response

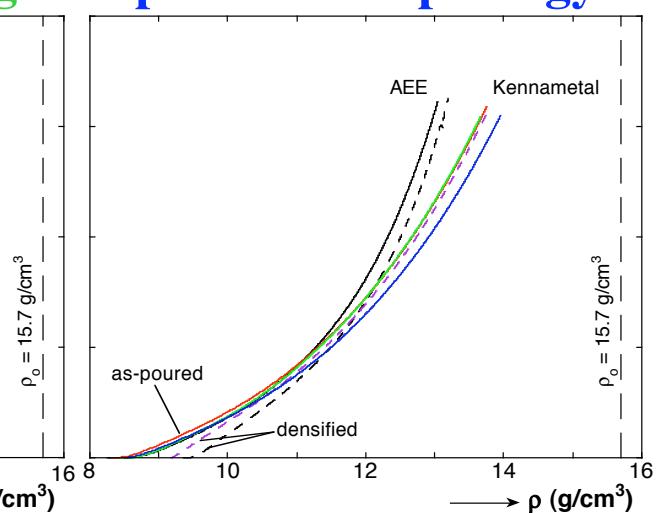
## grain size distribution



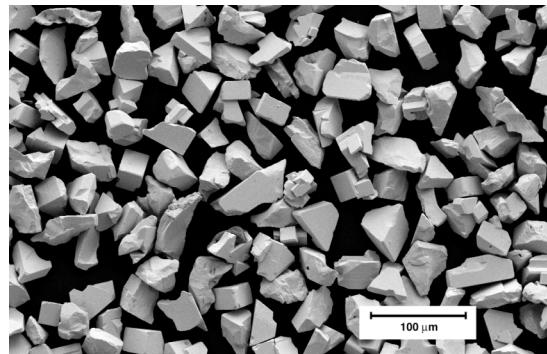
## unloading/reloading



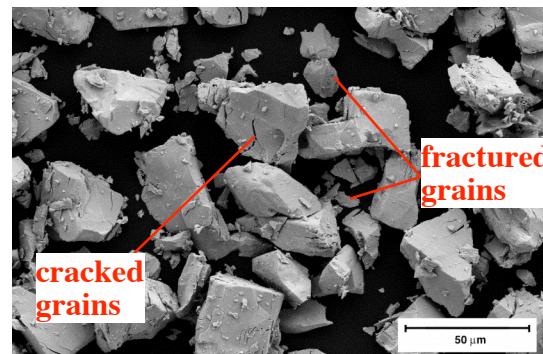
## particle morphology



## pre-compaction

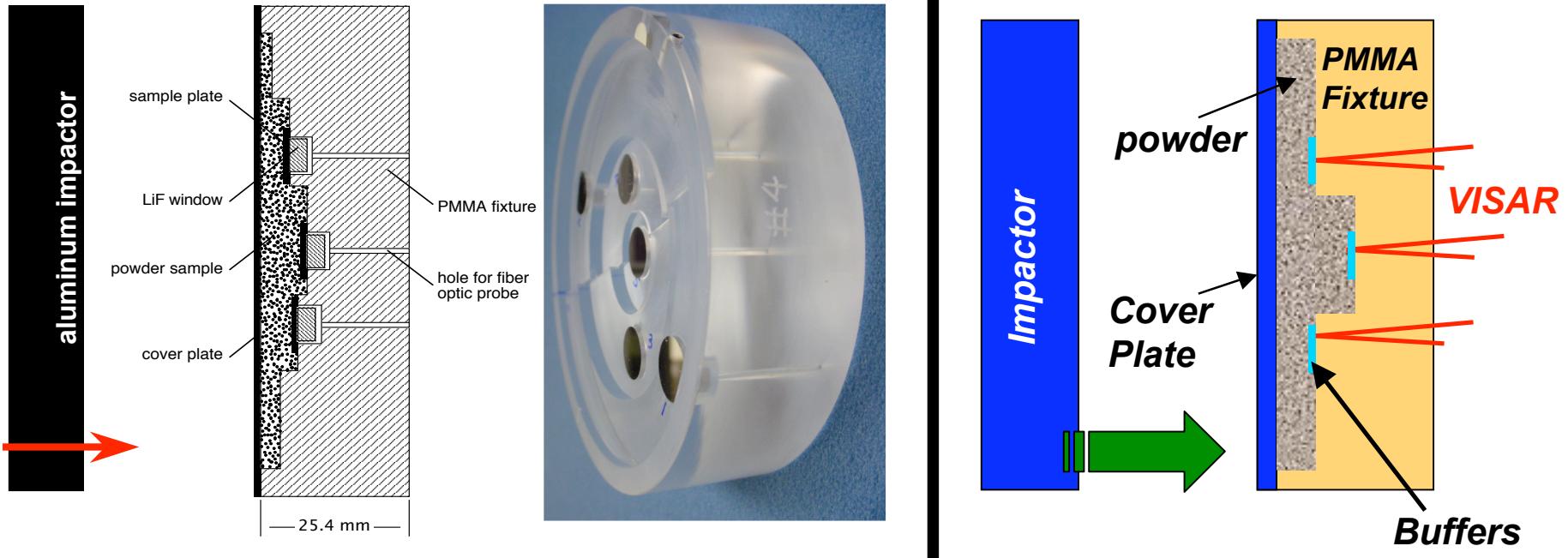


## post-compaction





# Planar Impact Experiments on Granular Materials



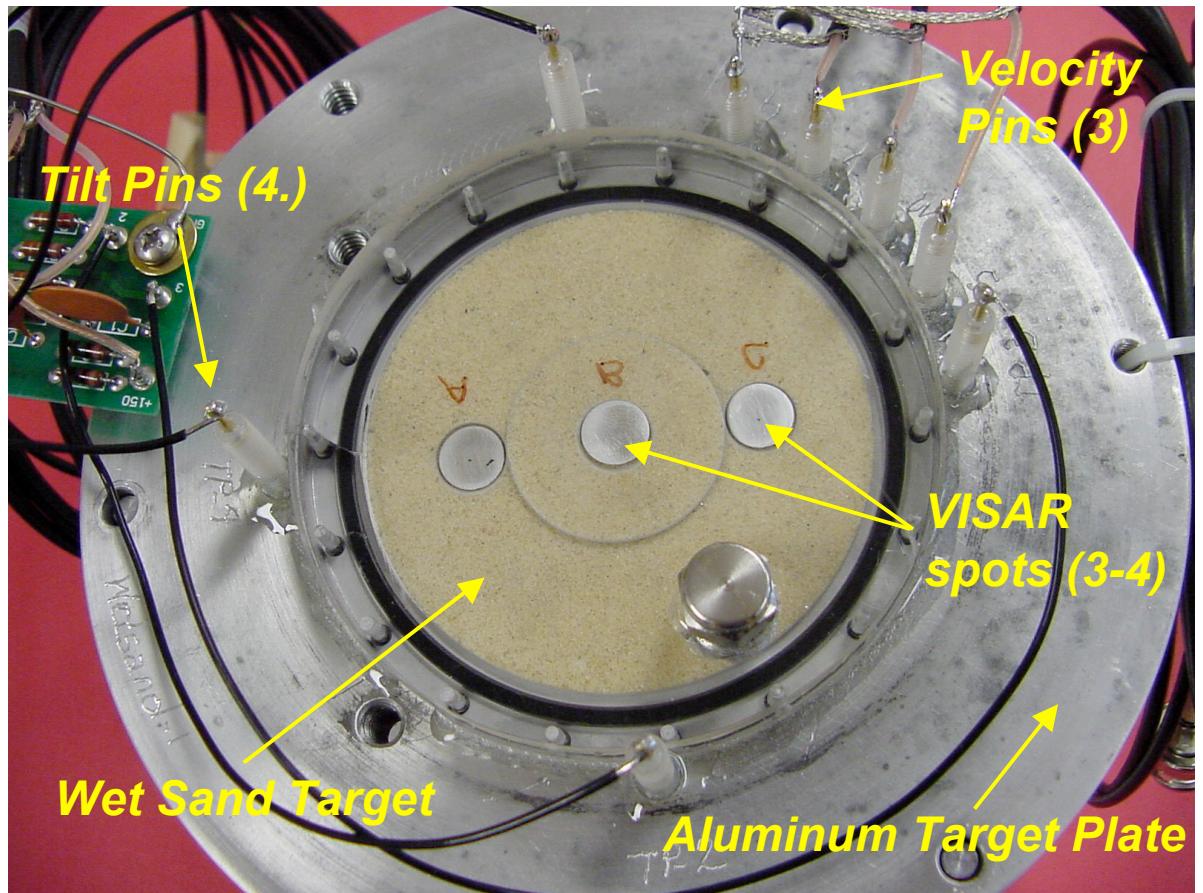
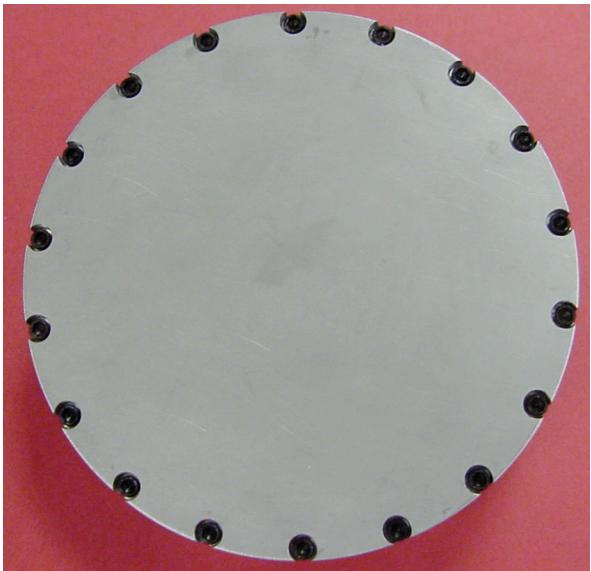
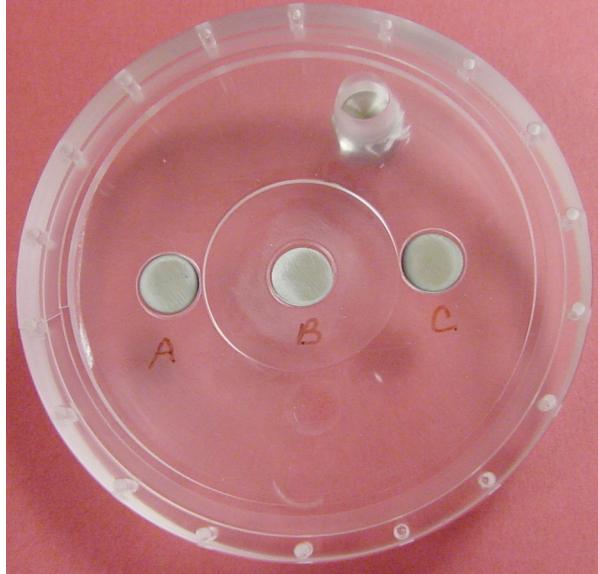
**multiple sample thicknesses on the same experiment for accurate shock velocity and uniform powder density; sealed capsule allows fluid / powder mixtures**

Vogler, T.J., Lee, M.Y., Grady, D.E., 2007. "Static and dynamic compaction of ceramic powders." *International Journal of Solids and Structures* **44**, 636-658.

Brown, J.L., Thornhill, T.F., Reinhart, W.D., Chhabildas, L.C., Vogler, T.J., 2007. "Shock response of dry sand." in Shock Compression of Condensed Matter – 2007, American Institute of Physics, 1363-1366.



# Wet Sand Targets



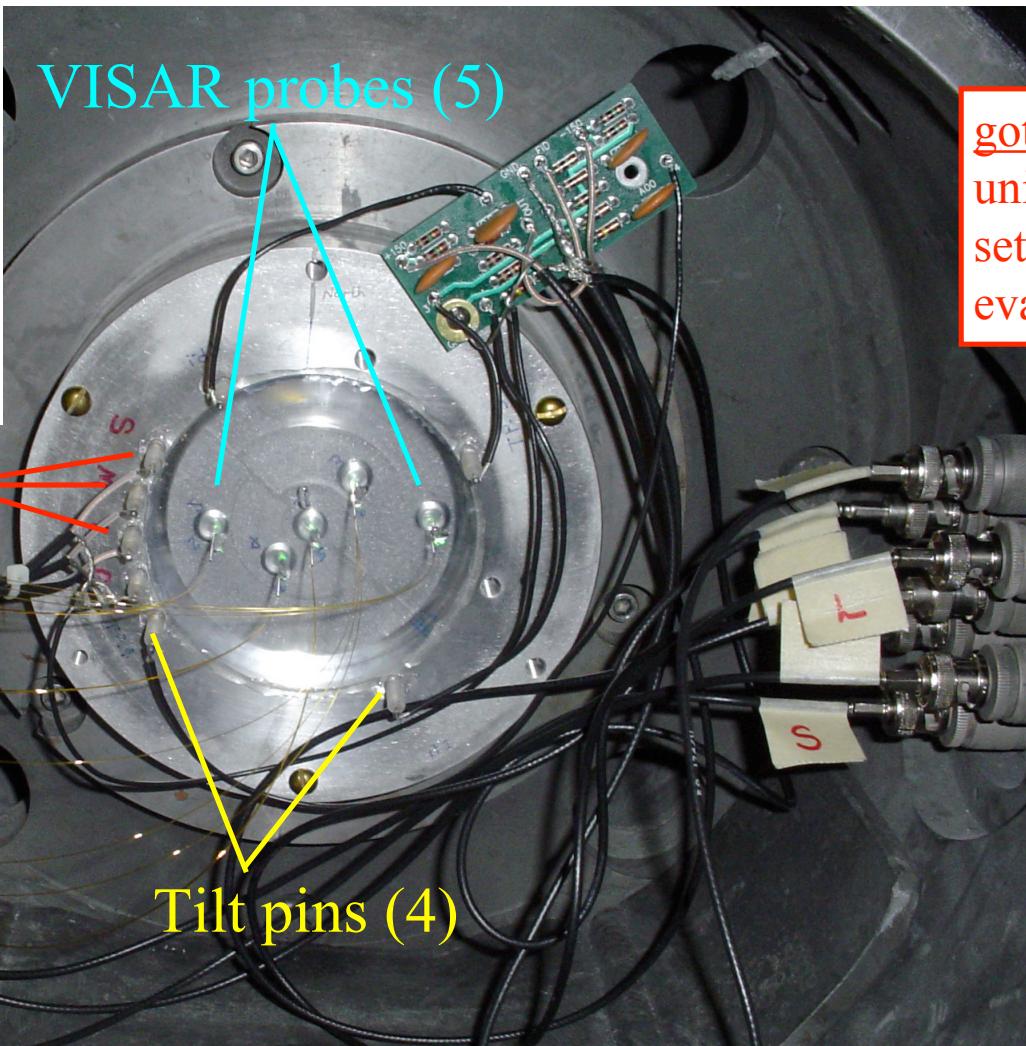


# Target Mounted in Gas Gun

**Single Stage Gun 100mm**



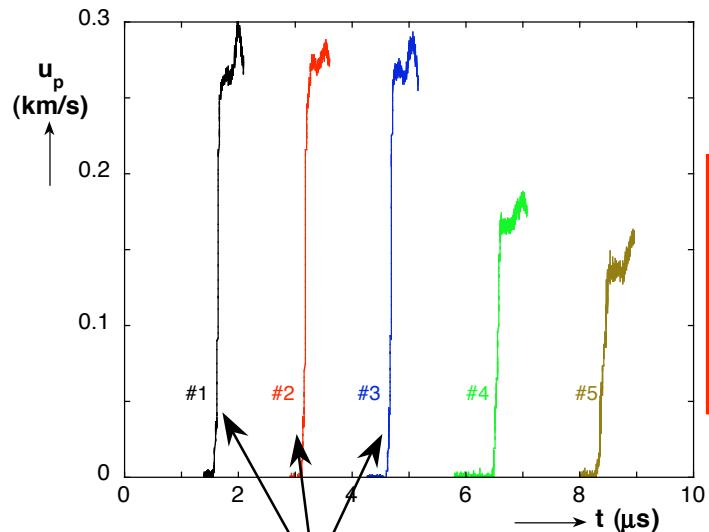
$\sim 1 \text{ km/s}$   
 $\sim 30 \text{ GPa}$



gotcha's:  
uniformity  
settling  
evacuation

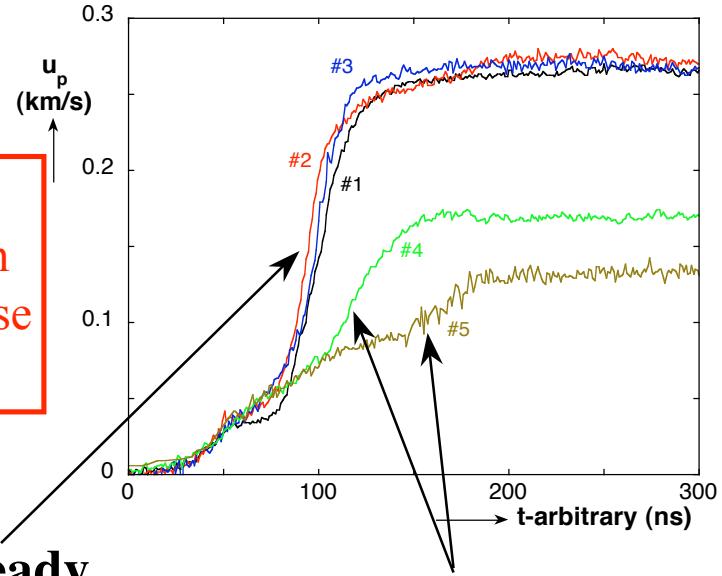


# Measured Steady Waves



**shock velocity calculated based  
on powder thicknesses and  
arrival times**

**gotcha's:  
attenuation  
edge release  
steadiness**



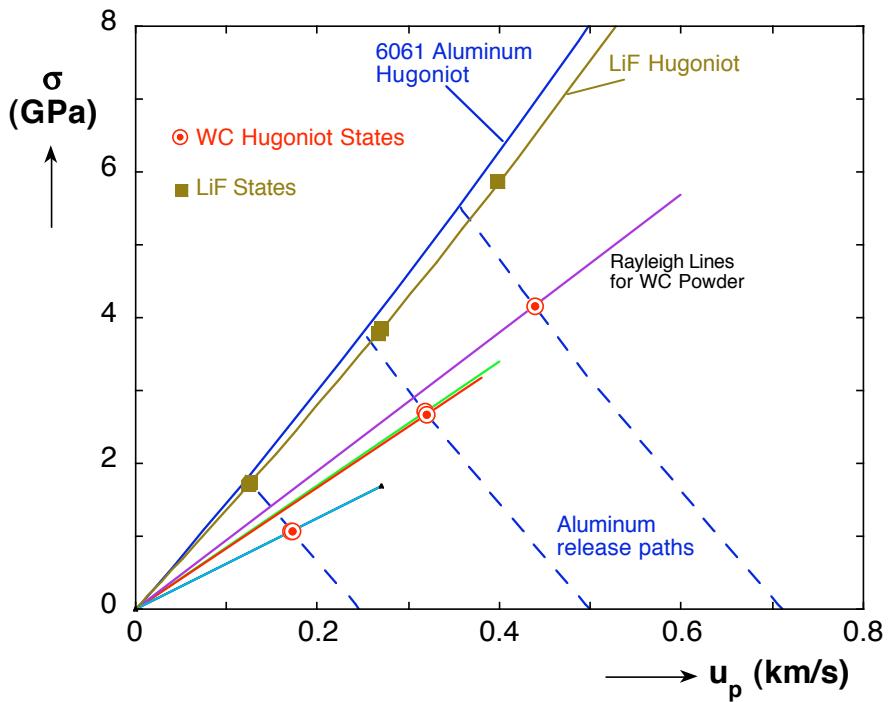
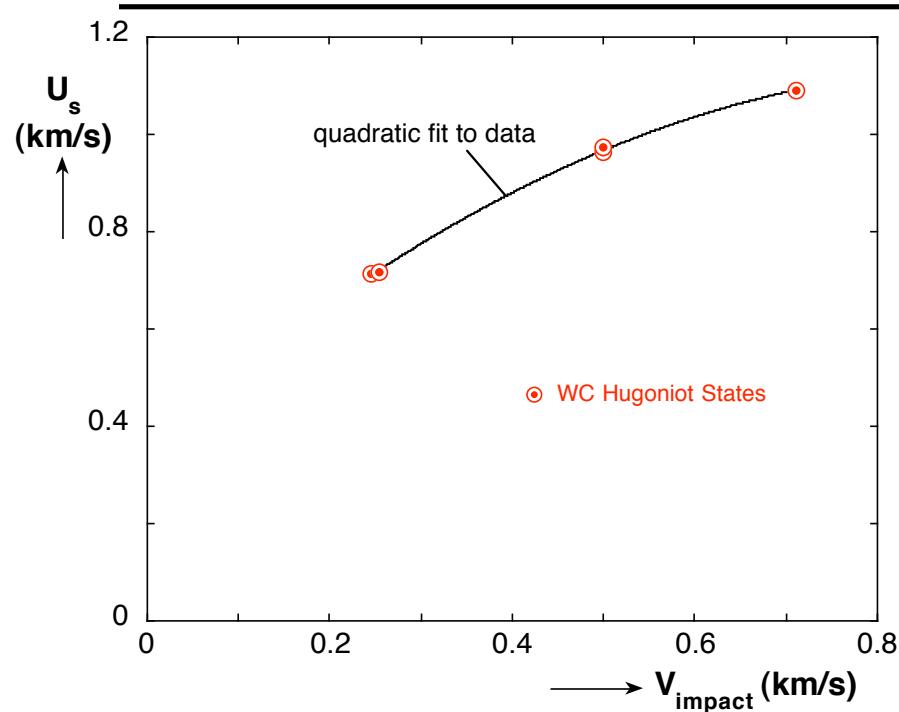
**steady,  
structured  
waves**

**attenuated  
waves**

- seem to be first time-resolved measurements of steady waves in granular materials
- since waves are steady, Rankine-Hugoniot jump conditions can be used even though waves have finite rise times



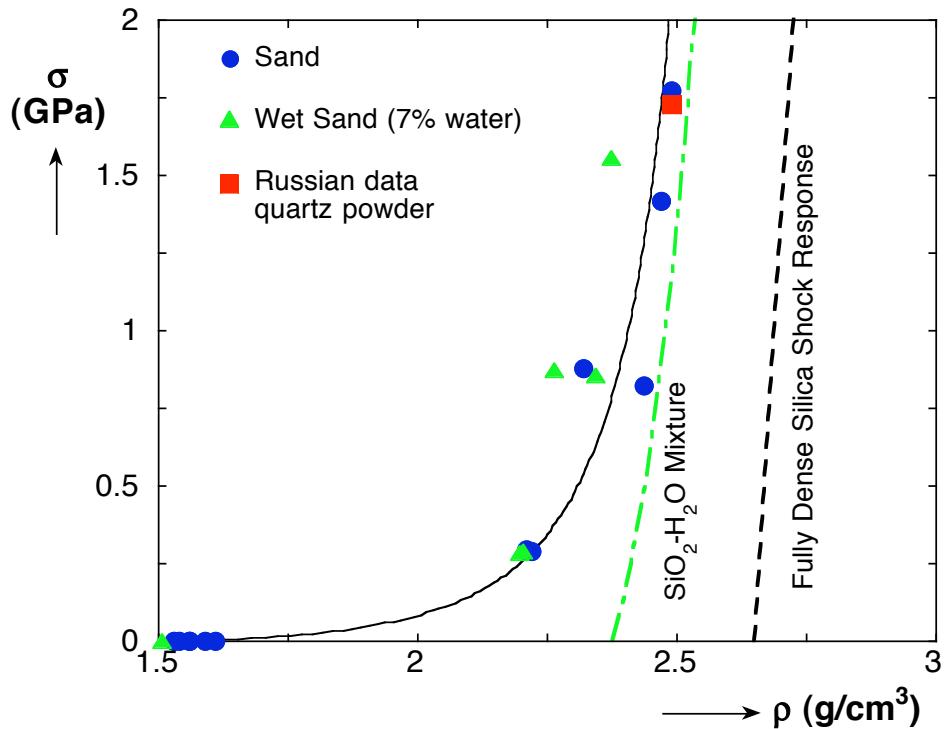
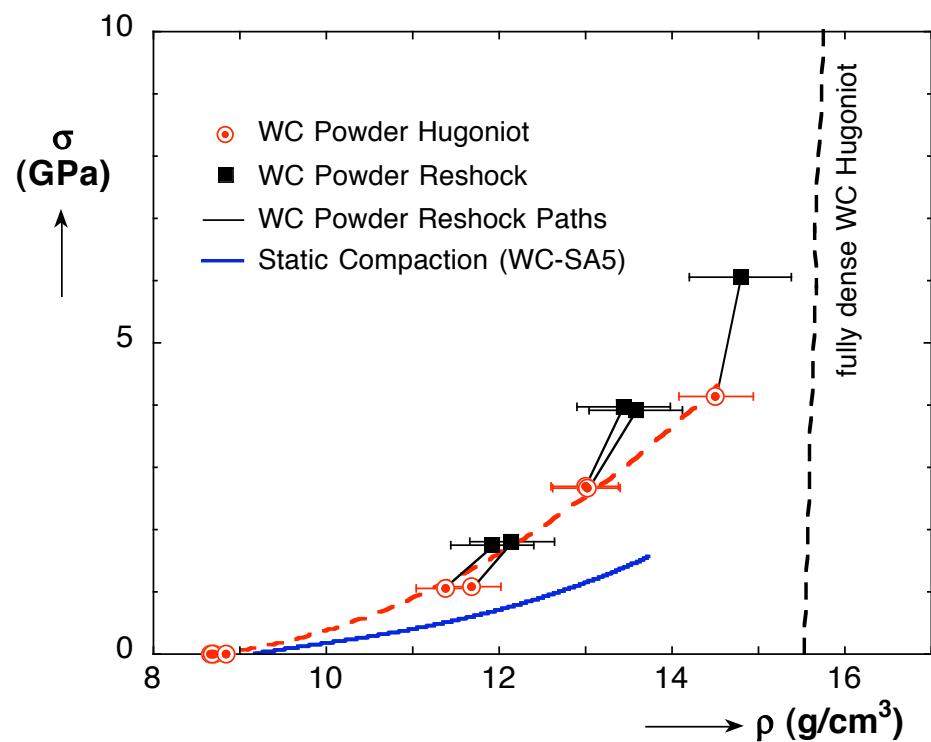
# Shock Velocities and Hugoniot States



- impedance matching to aluminum impactor used to determine Hugoniot stress and particle velocity ( $\sigma = \rho_o U_s u_p$ )
- density then calculated from  $\rho = \rho_o U_s / (U_s - u_p)$



# Compaction Response for WC and Wet/Dry Sand

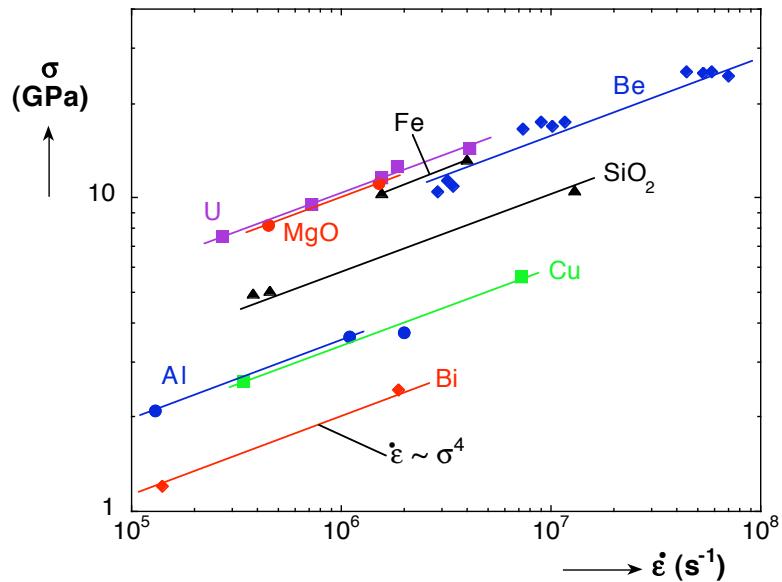


- first reshock state lies above Hugoniot suggesting elastic response of compacted material
- the difference between static and dynamic responses appears to be due to the relatively thin compaction front over which deformation occurs

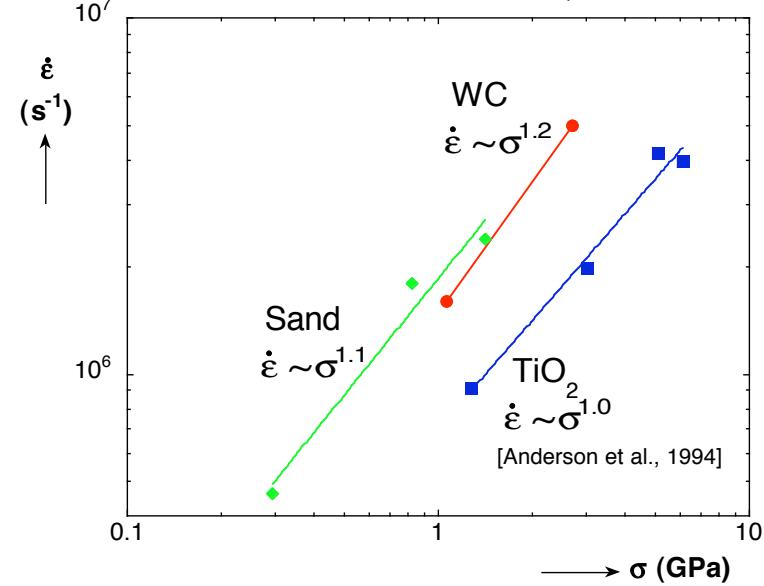
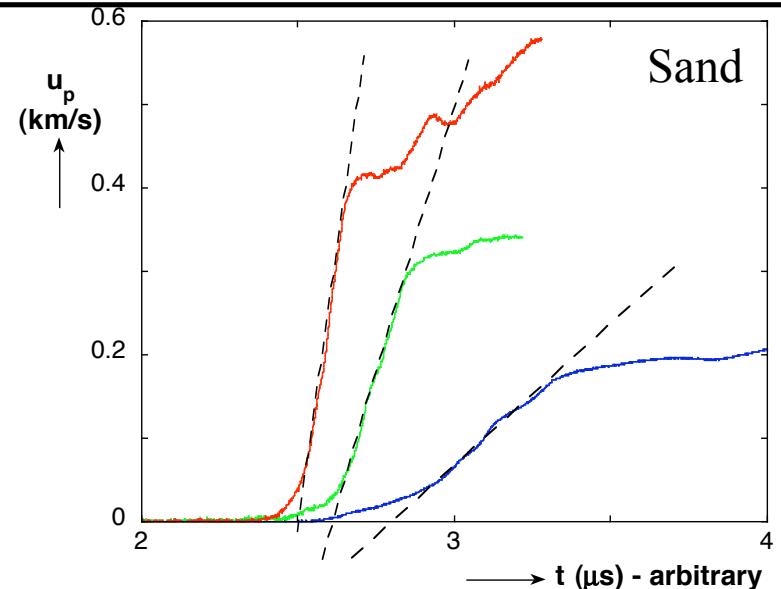


# Scaling Between Rise Time of Wave and Stress

for many fully dense materials (Al, Be, Bi, Cu, Fe, MgO, SiO<sub>2</sub>, U), rise times of steady waves scale as  
•  $\dot{\varepsilon} \sim \sigma^4$  (Swegle & Grady, 1985)



data on three granular ceramics suggest a linear scaling between stress and strain rate

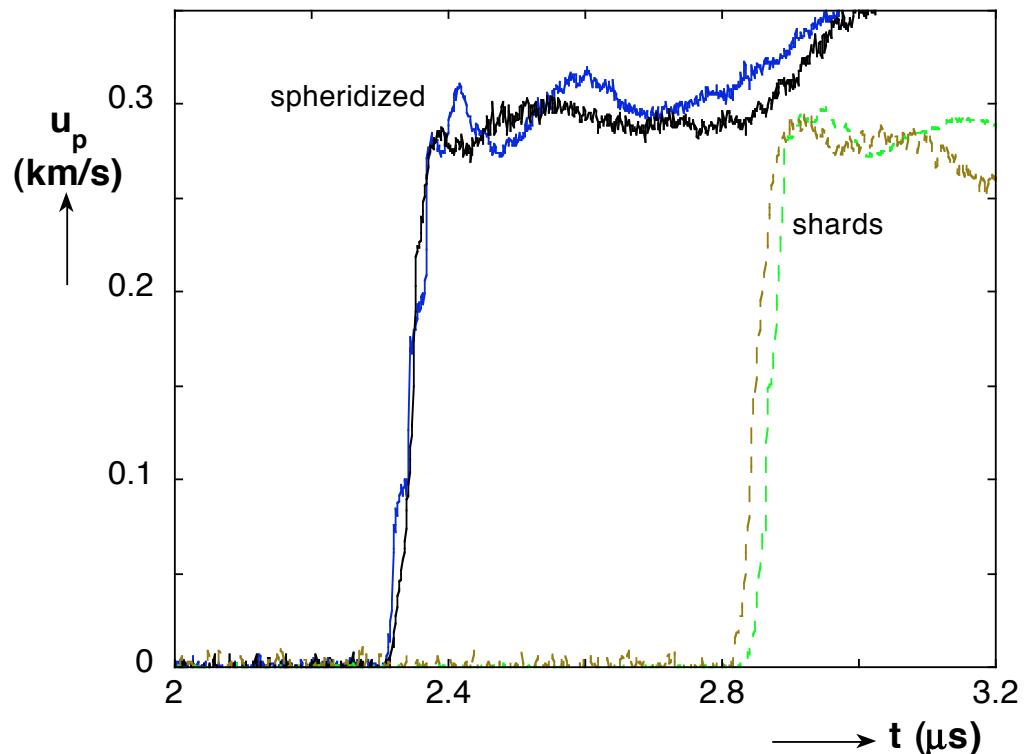
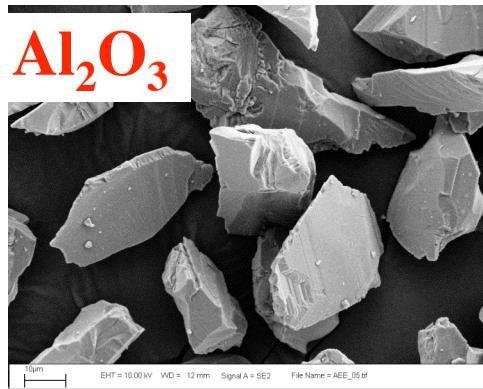


[Anderson et al., 1994]



# Effect of Particle Morphology

plasma processing used to create spheres, changing particle morphology

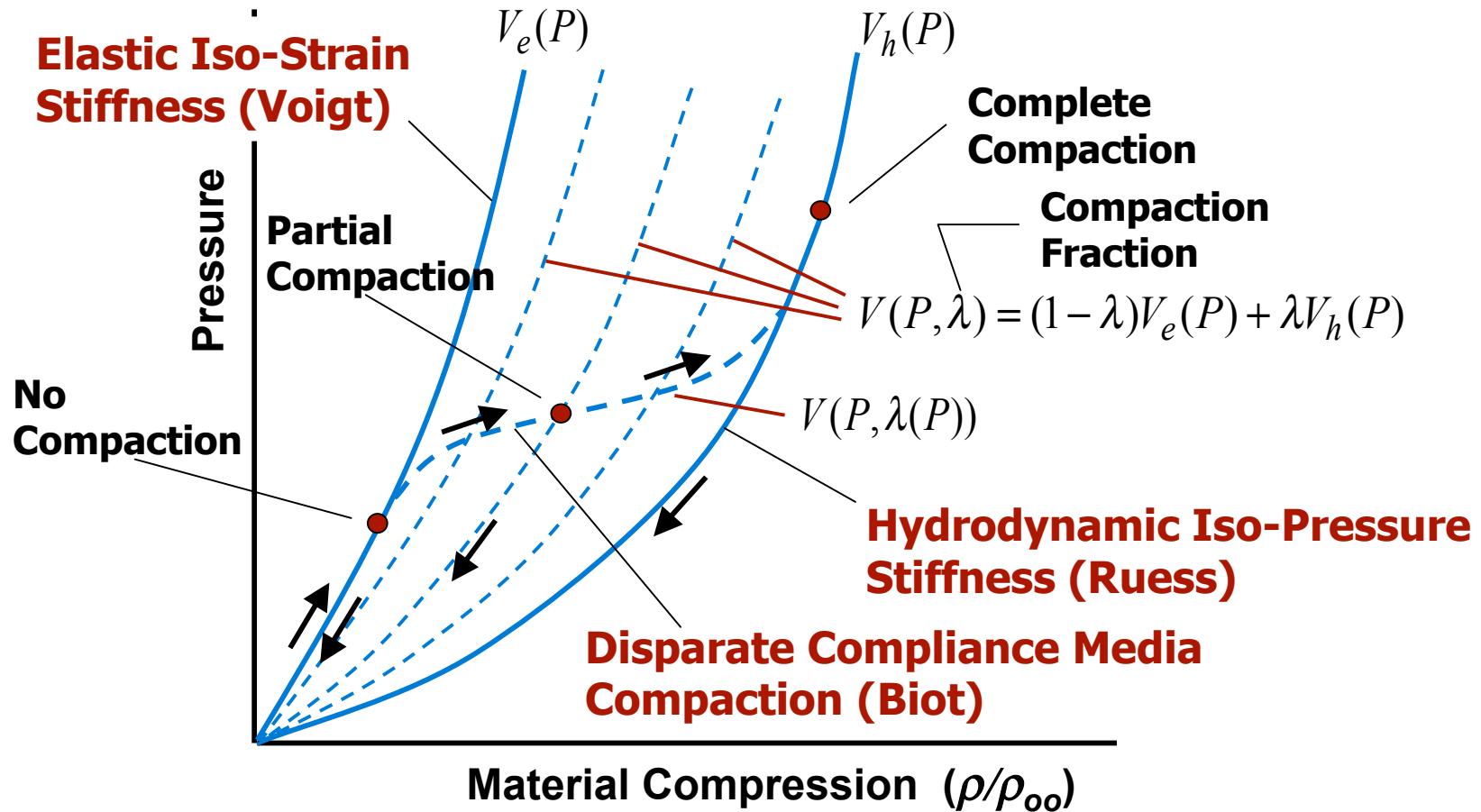


compaction results indistinguishable, but small differences in VISAR records; other materials with more significant morphology changes show greater differences in VISAR (but none in compaction)



# Continuum P- $\lambda$ Model

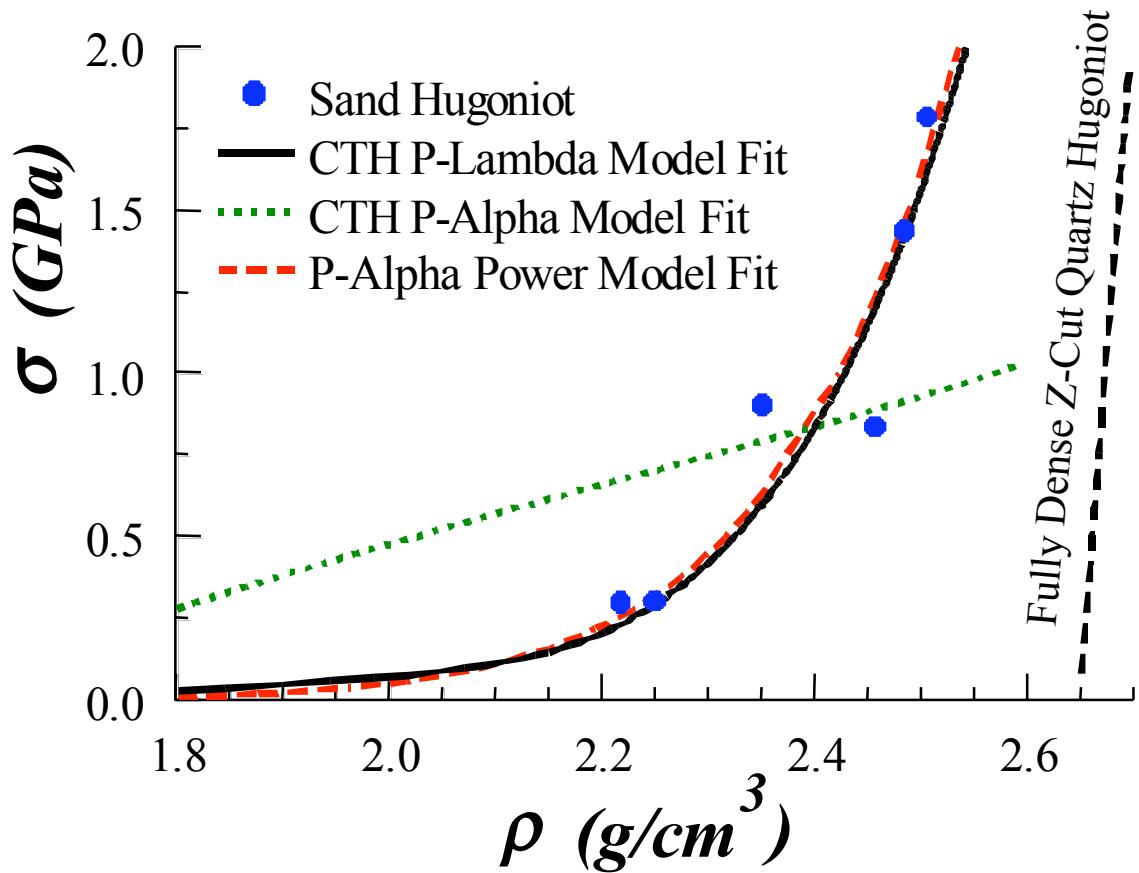
more flexible variation on P- $\alpha$  developed by Grady *et al.*; allows multiple materials but maintains simplicity of P- $\alpha$  model



Grady, D.E., 2007. "Shock wave compression of ceramics with microstructures." *International Journal of Plasticity* (in press).



# Continuum Model (P- $\alpha$ and P- $\lambda$ ) Calibration for Sand



$$\alpha = \frac{\rho_m}{\rho}$$

CTH form

$$\alpha(p) = 1 + (\alpha_0 - 1) \left( \frac{p_s - p}{p_s - p_e} \right)^n$$

alternate form

$$p(\alpha) = p_s \alpha^{-n}$$

$$v_m(p) = \lambda v_R(p) + (1 - \lambda) v_V(p)$$

$$\lambda = 1 - e^{-\left(\frac{p}{p_c}\right)^n}$$



# Mesoscale Modeling of Granular Materials



- follow approach of Benson et al. for 2-D simulations
- particles idealized as circles (rods) for initial work
- constant velocity boundary condition applied
- run in CTH (explicit Eulerian finite difference code)
- Mie-Gruneisen EOS, elastic-perfectly plastic strength for WC

Borg, J.P., Vogler, T.J., (2008). "Mesoscale calculations of the dynamic behavior of a granular ceramic." *International Journal of Solids and Structures* (in press).

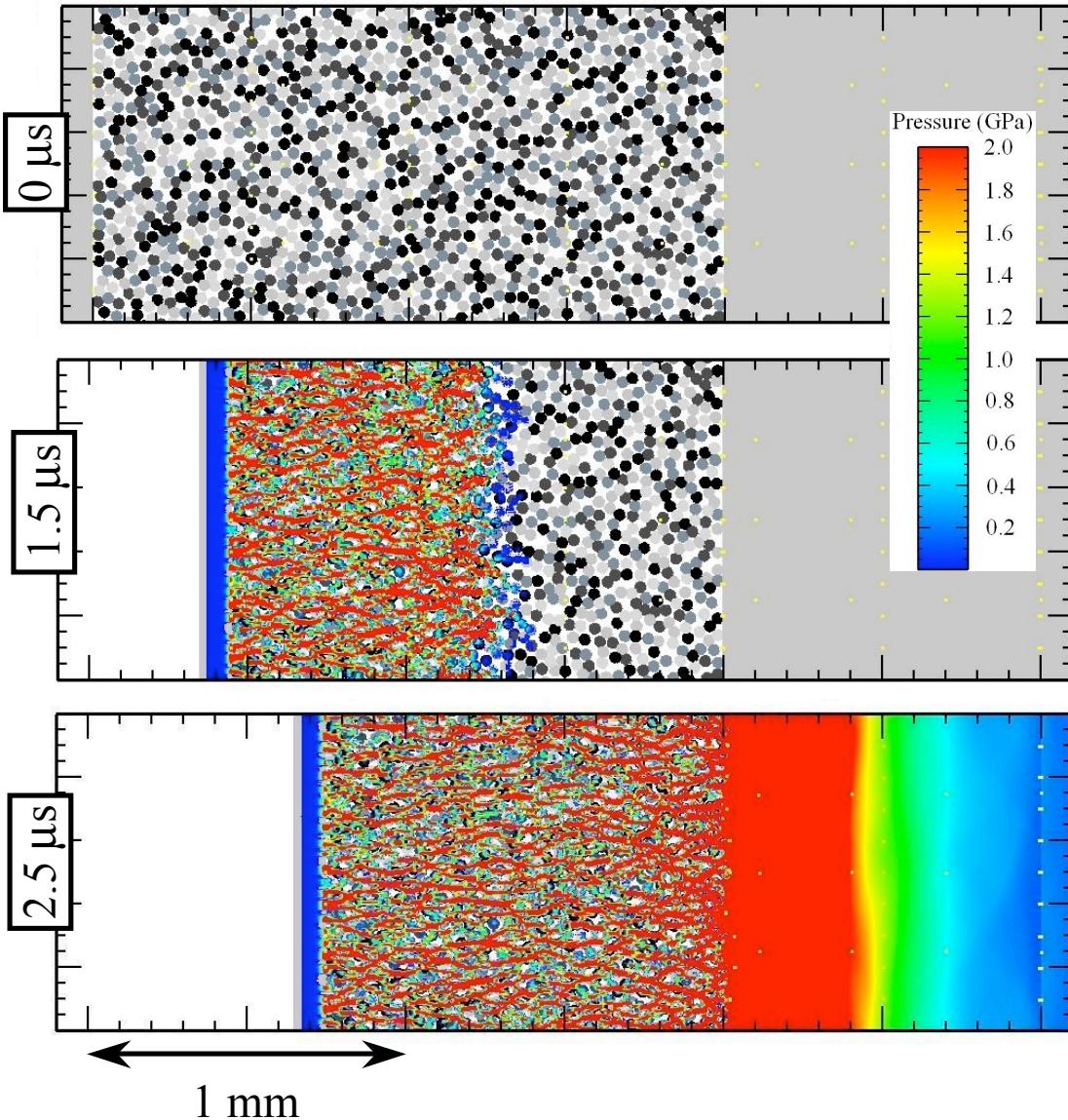
Borg, J.P., and Vogler, T.J. (2008). "Mesoscale simulations of a dart penetrating sand," *Int. J. Impact Eng.* (in press).

Borg, J.P., and Vogler, T.J. (2007). "Mesoscale calculations of shock loaded granular ceramics," in Shock Compression of Condensed Matter – 2007, American Institute of Physics, 227-230.

*get at underlying physics of granular materials*



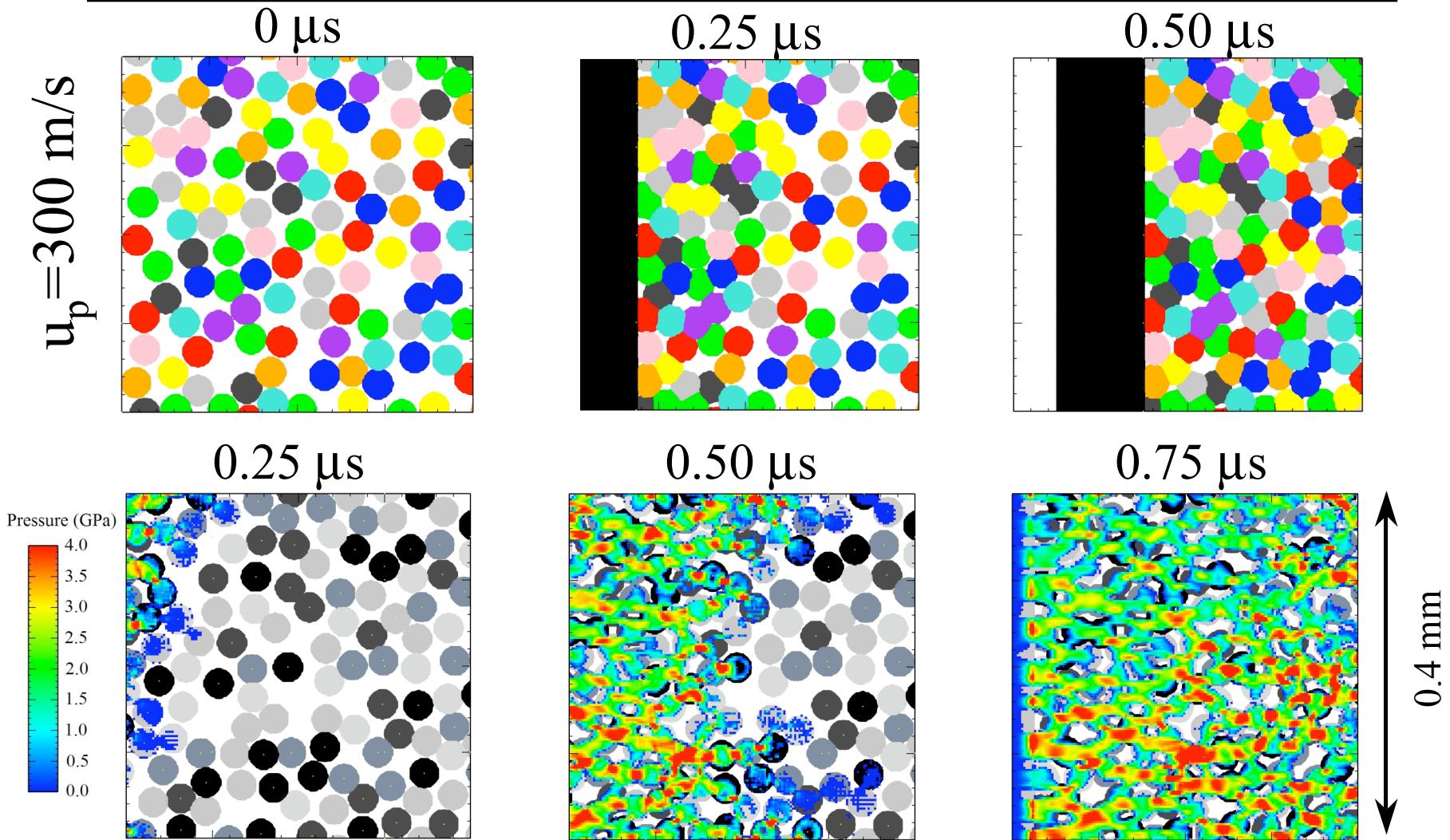
# Computational Dynamic Compaction



- **driver plate velocity**  
 $u_p = 300 \text{ m/s}$
- **shock thickness on the order of  $\sim 2\text{-}5$  particles**
- **strong force chains observed**
- **wave smooths in aluminum buffer**



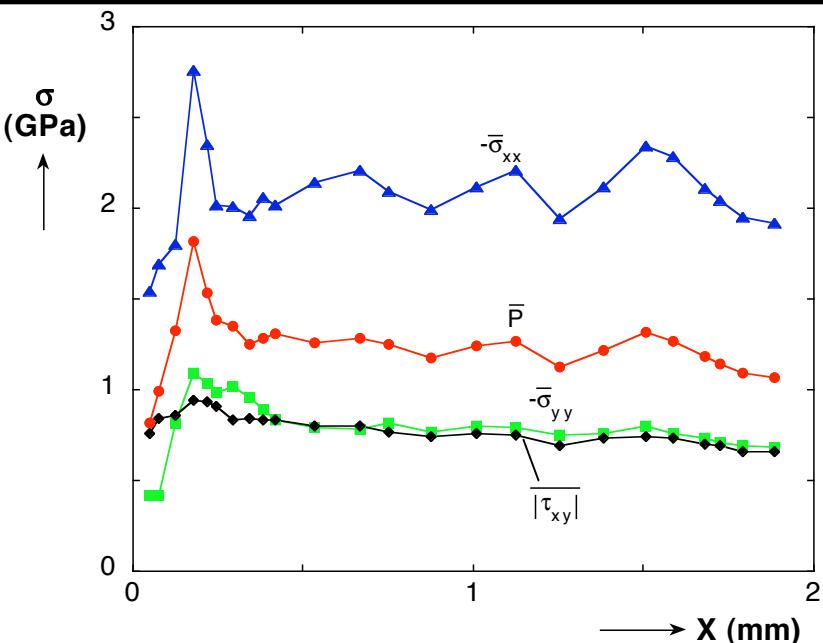
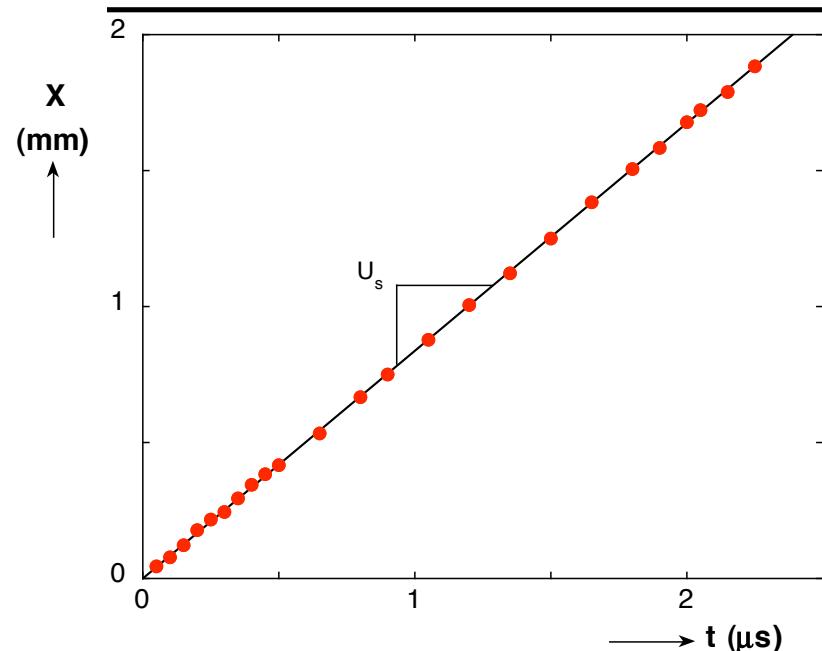
# Close-Up of Compaction Process



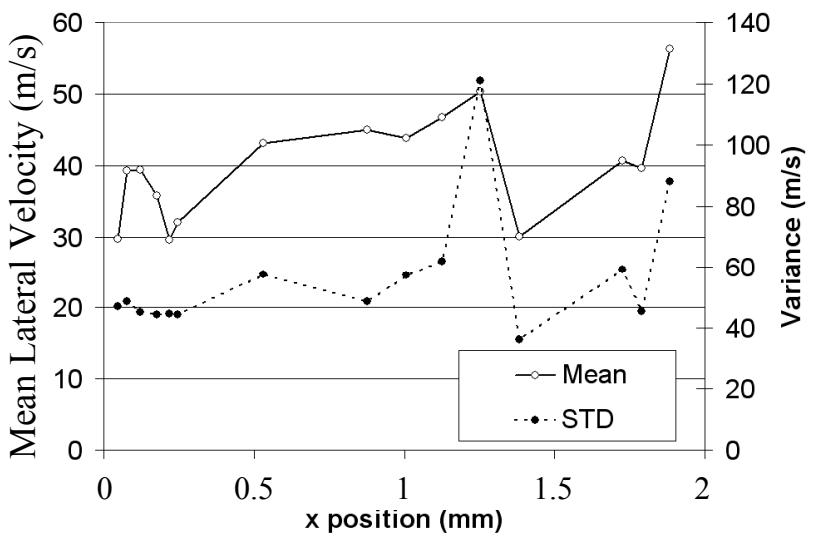
no jetting or vortices so deformation is “*quasi-static*”  
(Benson et al., 1997)



# Properties of Propagating Wave

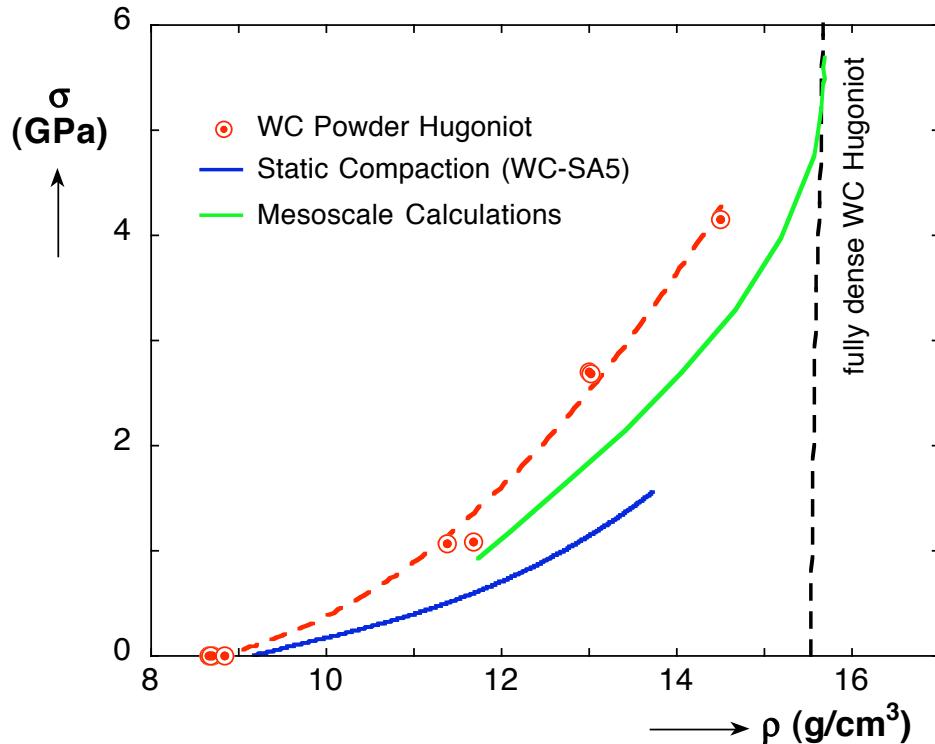


- arrival time of wave suggests steadiness at all times
- stresses in wave front indicate nearly 0.5 mm required to reach steady state
- lateral motion  $>10\%$  of longitudinal velocity





# Calculated Hugoniot from Literature Parameters

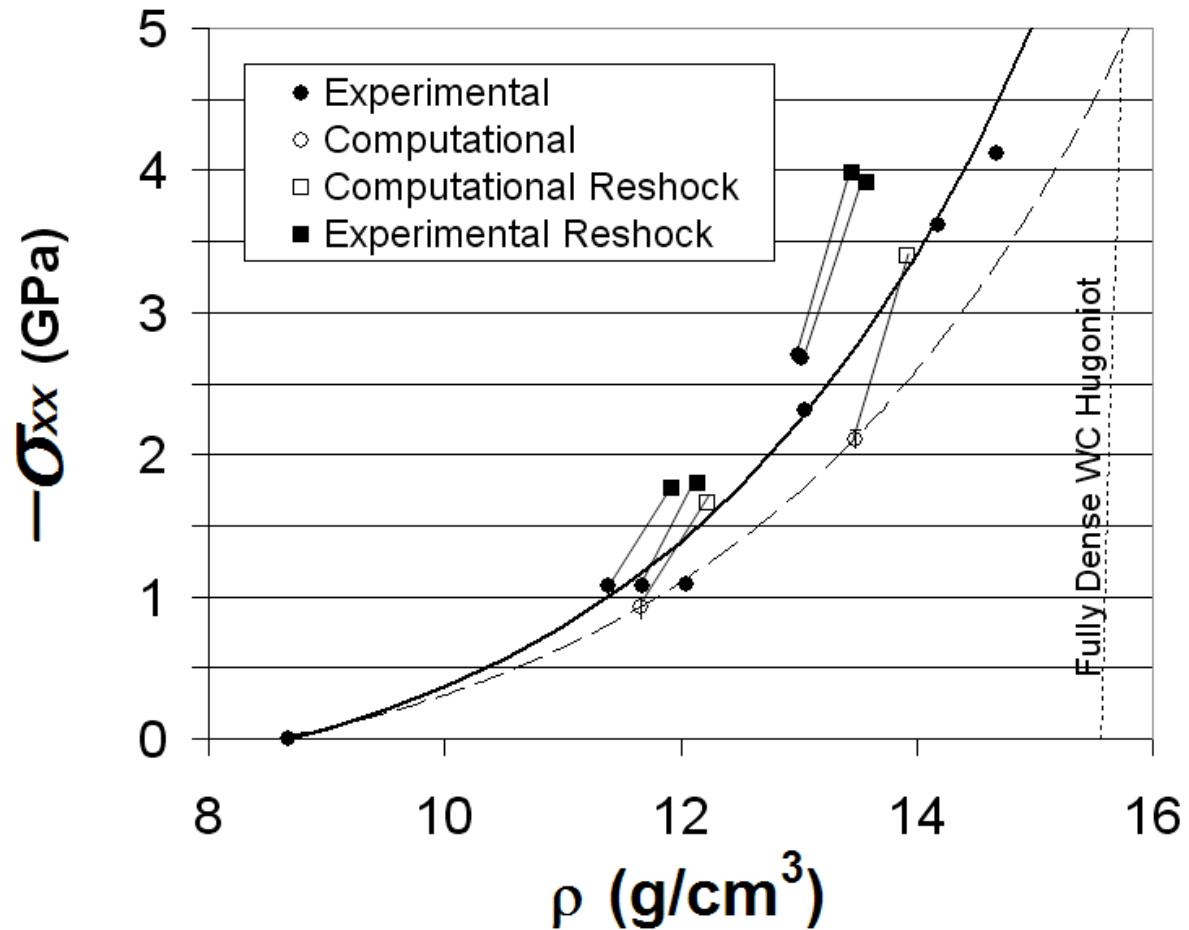


$$\sigma = \rho_o U_s u_p$$
$$\rho = \rho_o \frac{U_s}{U_s - u_p}$$

- simulations provide reasonable estimate for Hugoniot
- shortcomings of model:
  - missing physics of granular contact and fracture
  - wrong connectivity in 2-D
  - spherical particles unrealistic
  - inaccurate strength for small particles



# Reshock Behavior of Simulations



reshock behavior of the model agrees well with the experiments



# Sensitivity to Simulation Parameters

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## Material Properties

- Particle size distribution (**negligible effect**)
- Dynamic yield strength (**strong effect**)
- Material EOS (**negligible effect**)
- Spall strength (**strong effect but threshold**)

## Two-Dimensional Properties

- Material distribution (**strong effect**)
- Variations in boundary conditions (**small effect**)

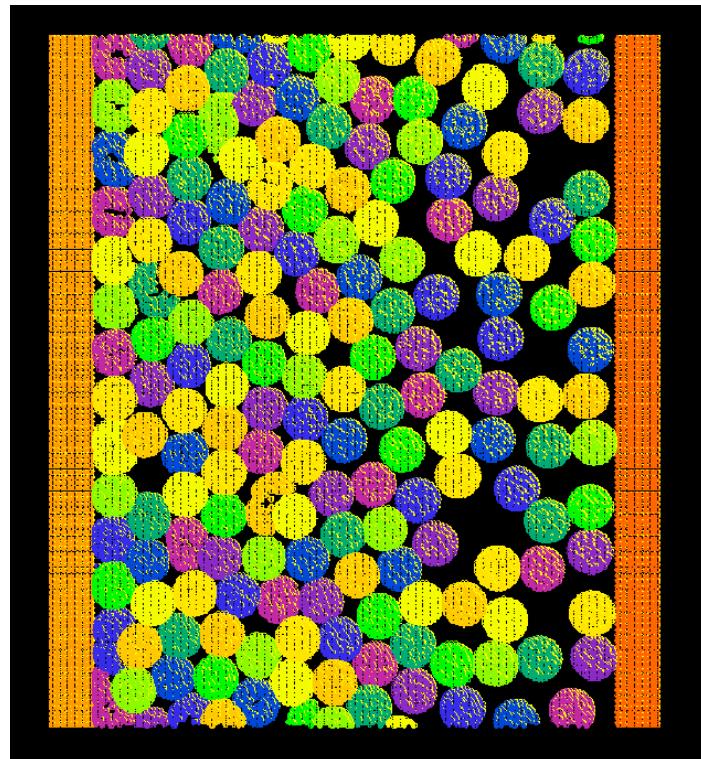
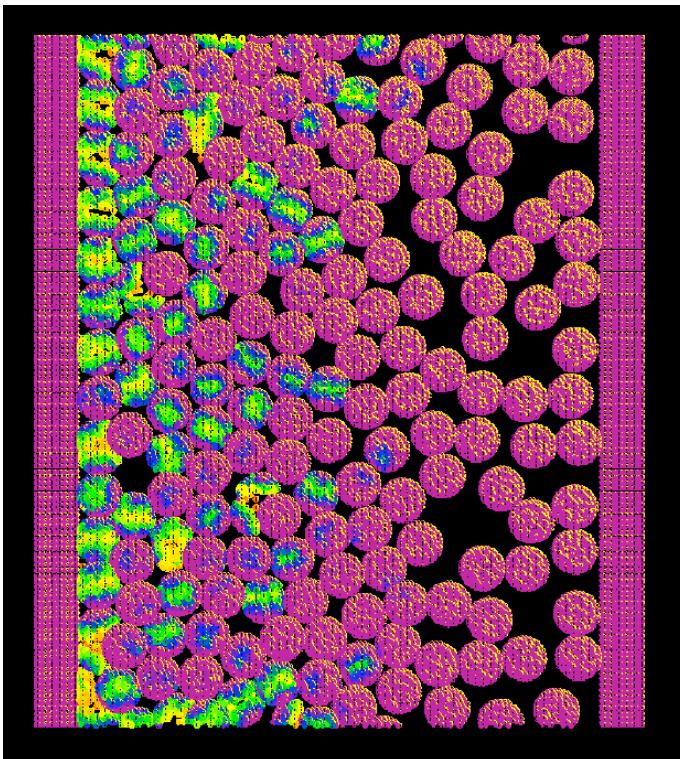
## Hydrocode Behavior

- Mixed cell strength (**very strong effect**)



# Initial Mesoscale Calculations with Peridynamics

- non-local method based on reformulation of governing equations in integral form
- model framework still under development
- includes fracture and contact missing from CTH
- interaction between fracture and plasticity complicated

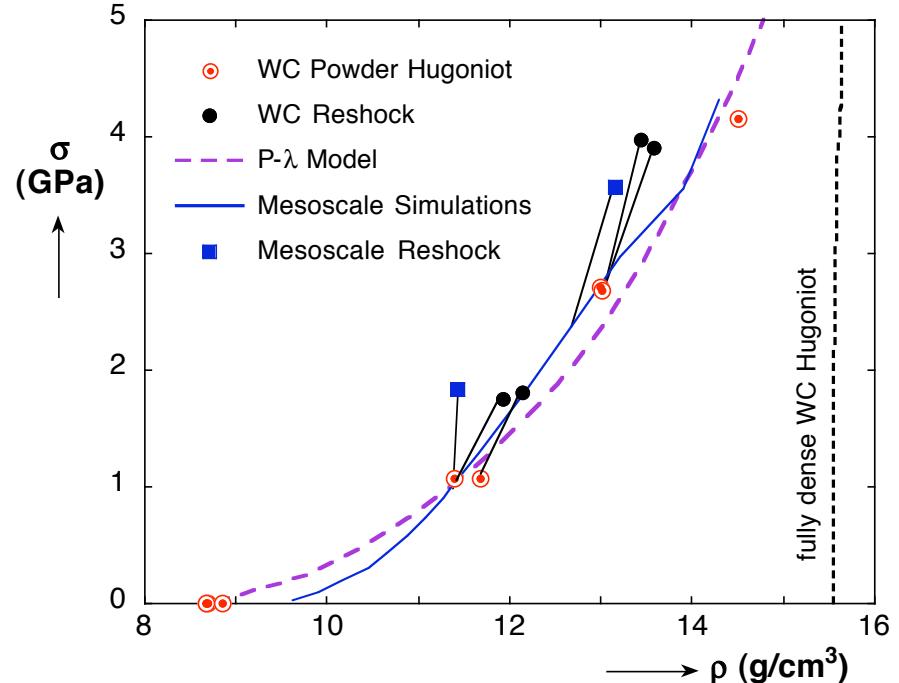




# Validation Experiments: Attenuating Waves



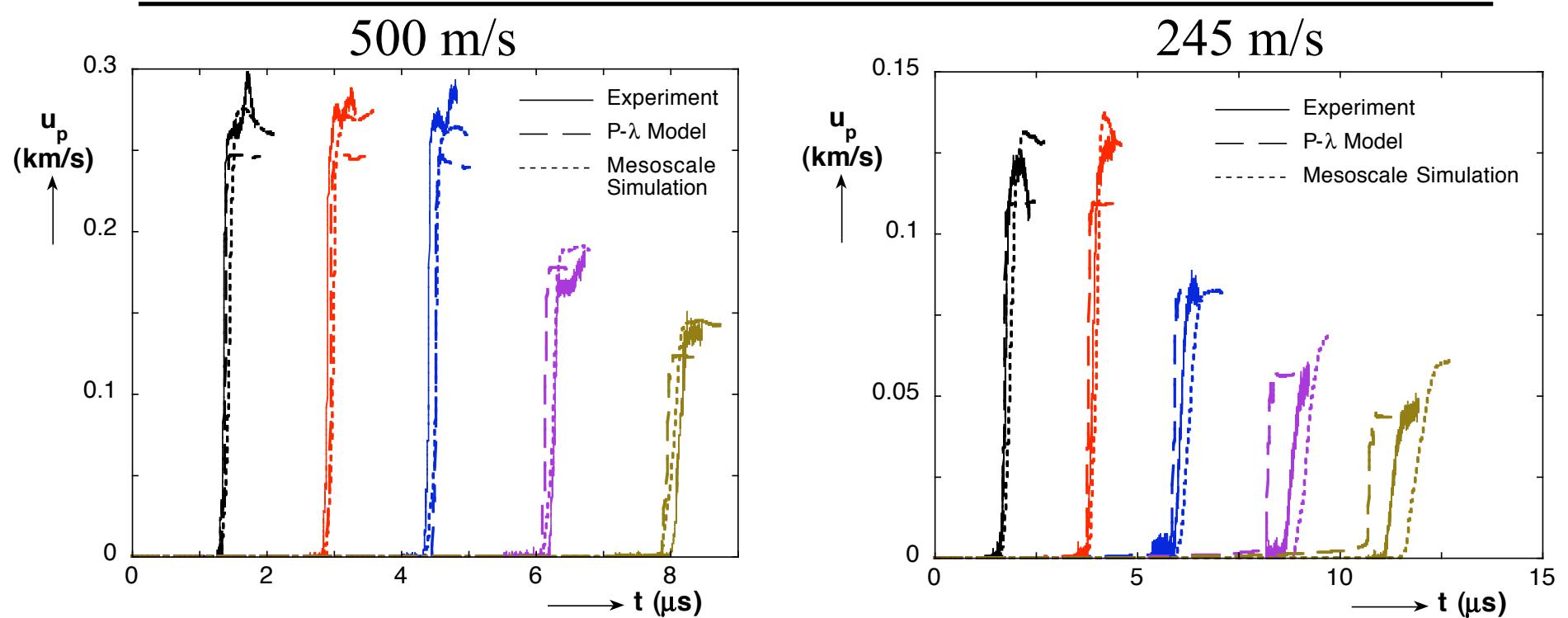
- P- $\lambda$  model calibrated to WC data
- mesoscale strength set to 8 GPa to match data
- duplicate geometry of experiments for 1 mm wide slice
- velocity averaged at nine points along buffer/window interface



Vogler, T.J., and Borg, J.P. (2007). "Mesoscale and continuum calculations of wave profiles for shock-loaded granular ceramics," in Shock Compression of Condensed Matter – 2007, American Institute of Physics, 291-294.



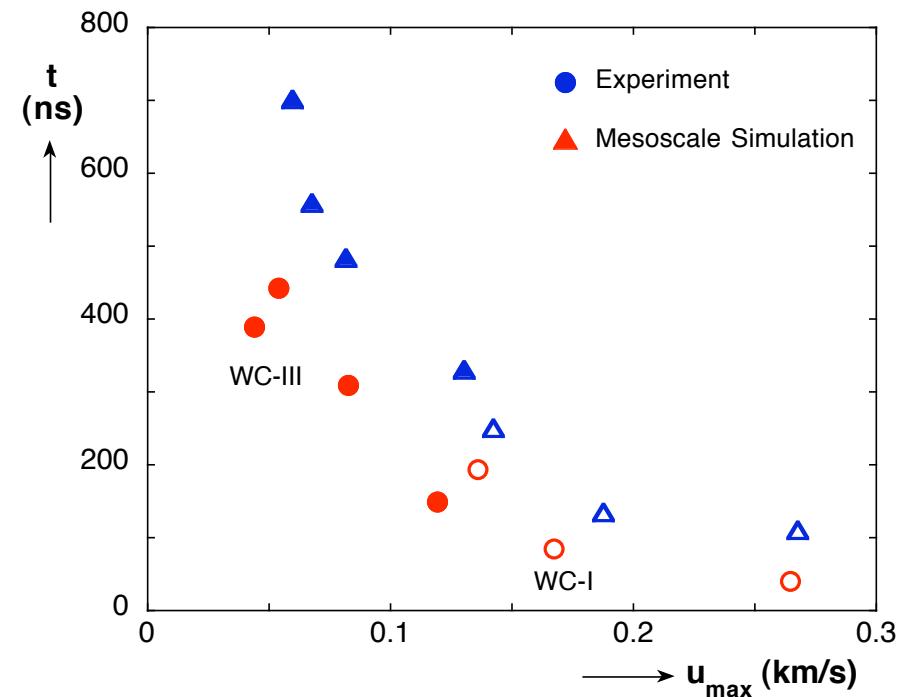
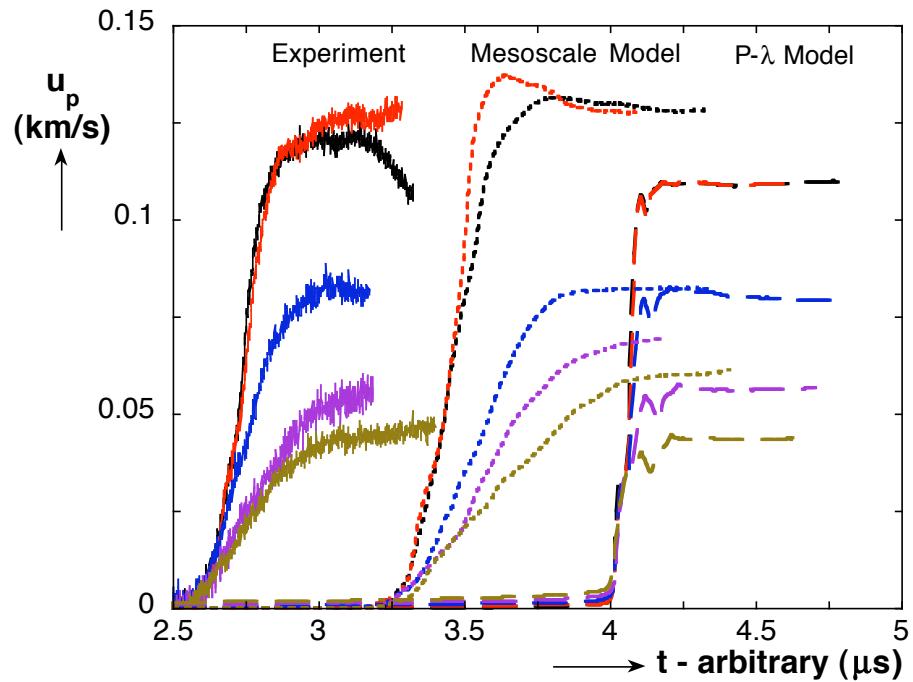
# Attenuating Waves: Comparison to Experimental Profiles



- steady wave arrival times good for both models, but amplitudes more accurate with mesoscale model due to stiffer reshock
- attenuating wave arrivals slightly better with mesoscale
- low stress levels seem to lie between mesoscale and P-λ, sampling regime where there is no data



# Attenuating Waves: Wave Shapes

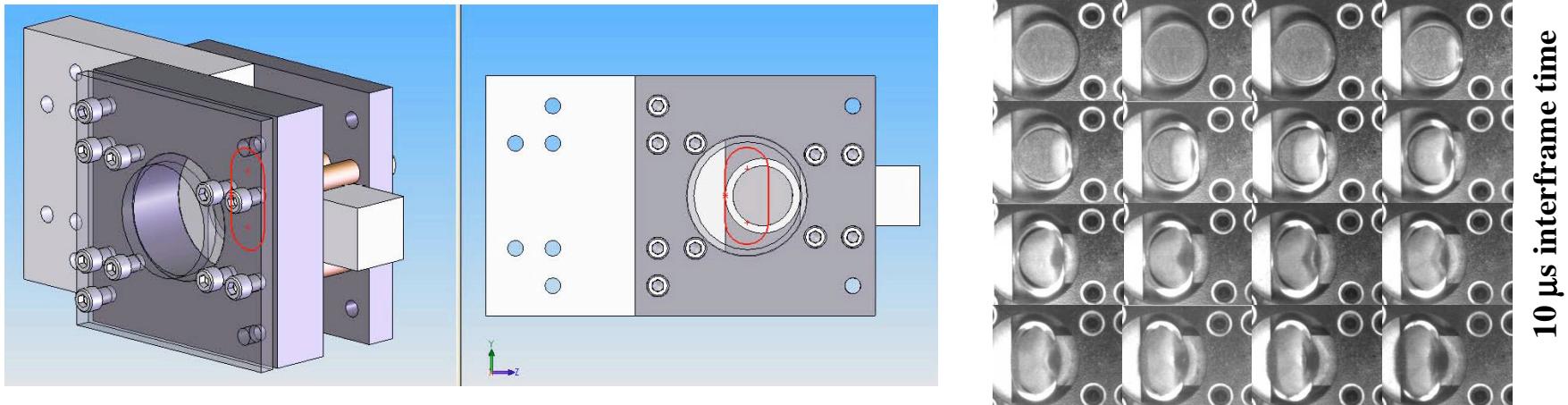


- shape from mesoscale approx. correct; P- $\lambda$  inaccurate
- rise time seems to depend only on current amplitude

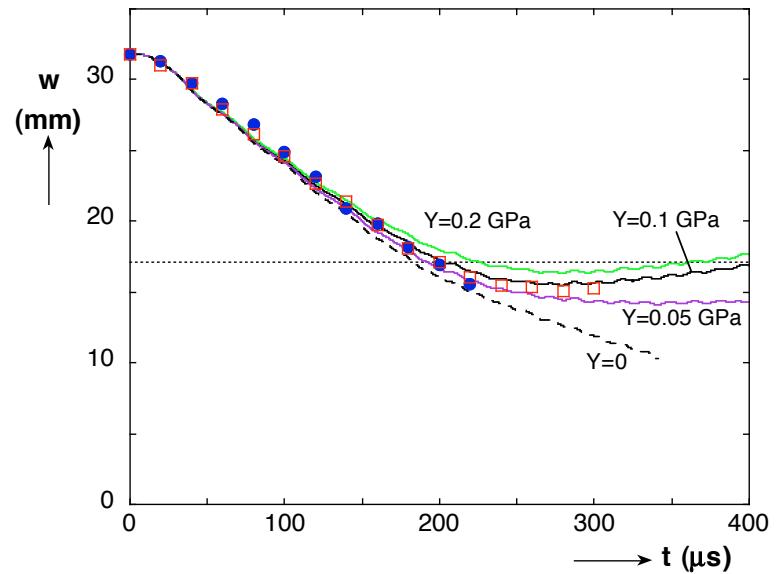
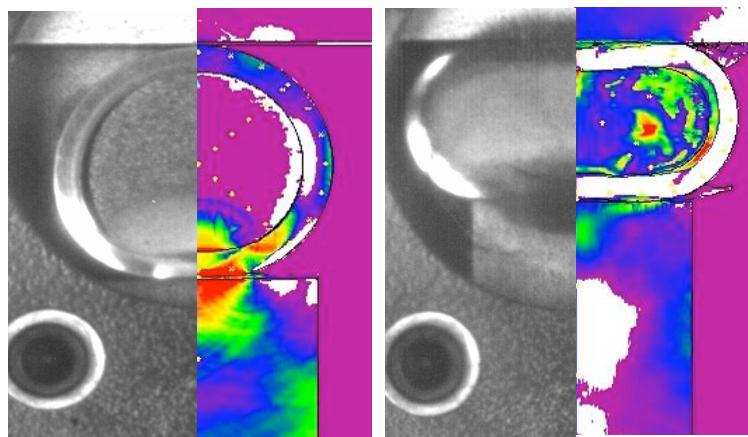


# Validation Experiments: Ring Compaction

ring compaction experiments provide data for non-planar deformation

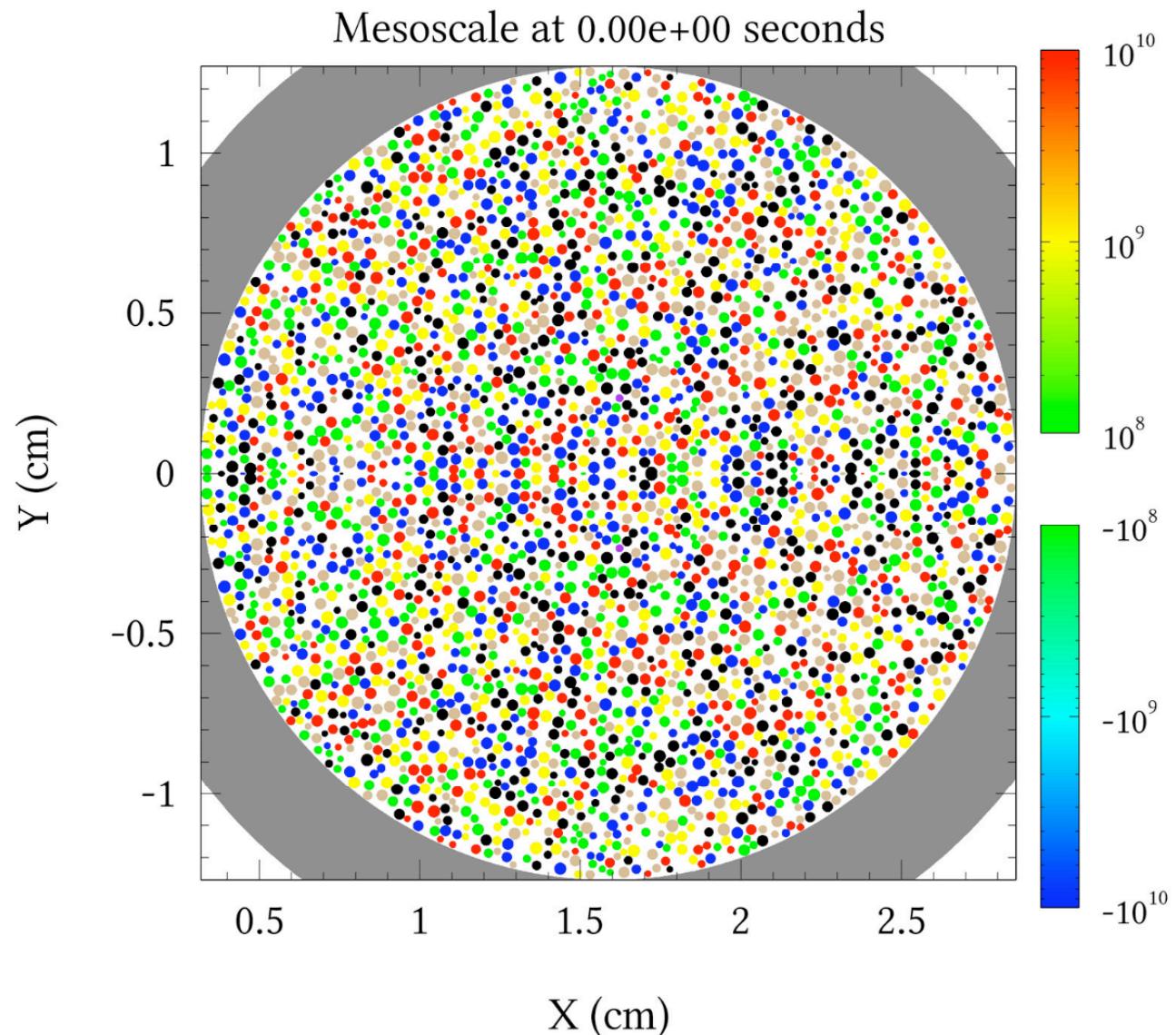


## 2-D CTH continuum calculation



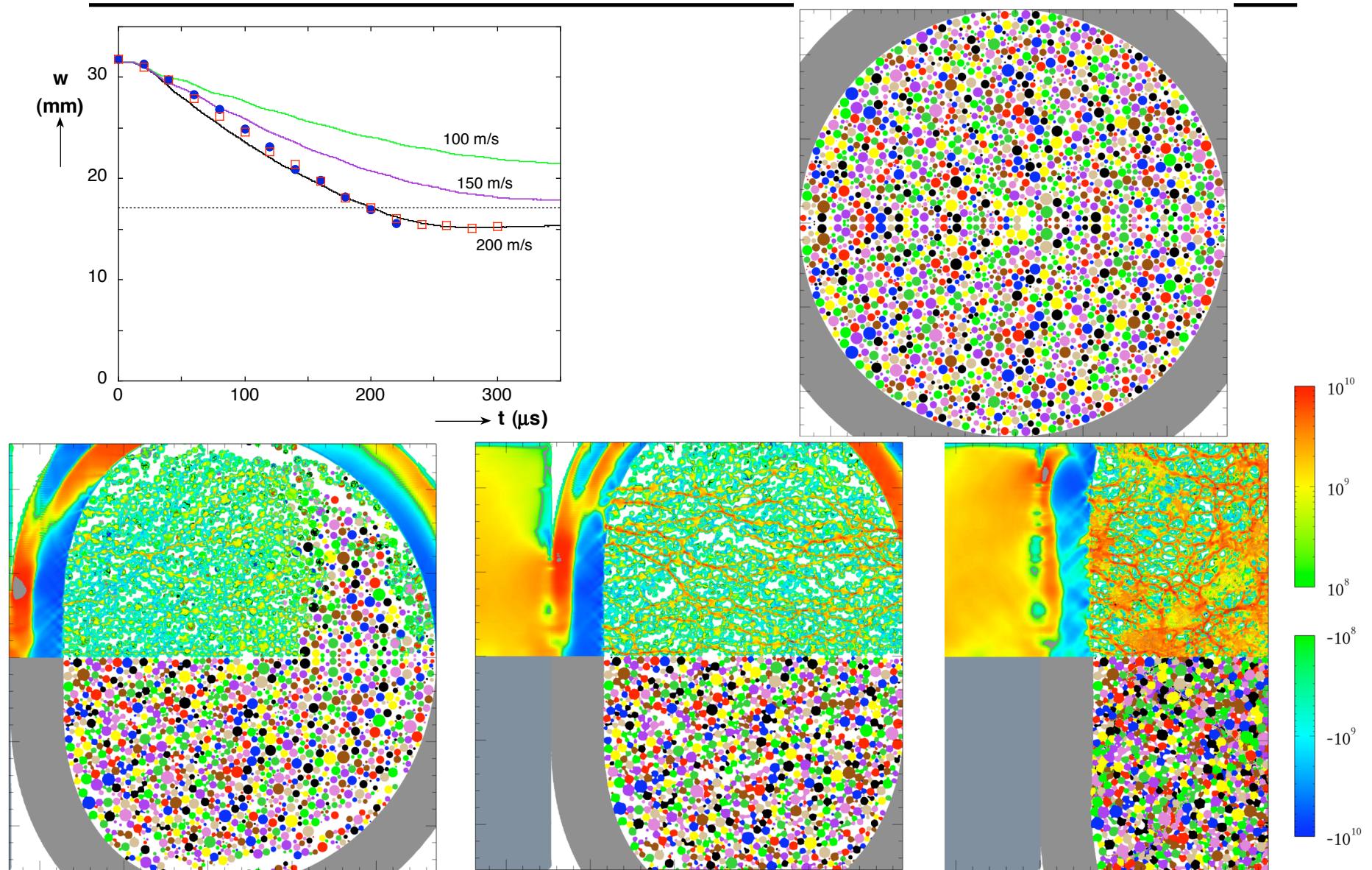


# Mesoscale Simulations of Rings (movie)



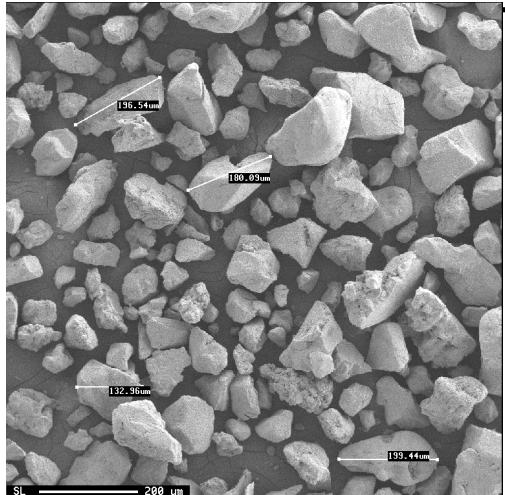


# Mesoscale Simulations of Rings

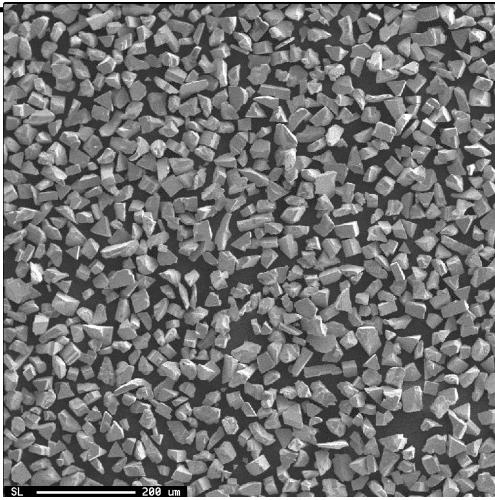




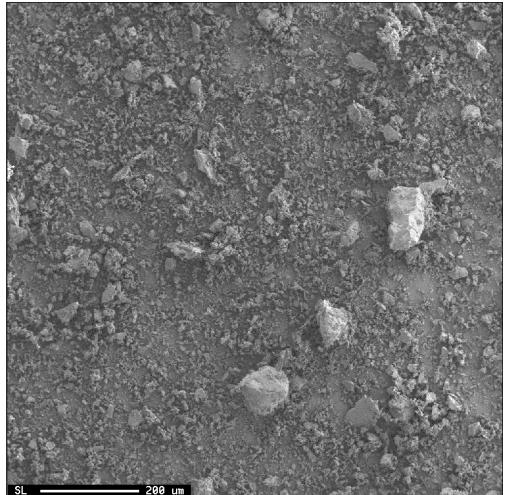
# Evolution of Particle Size Distribution



Sand



WC

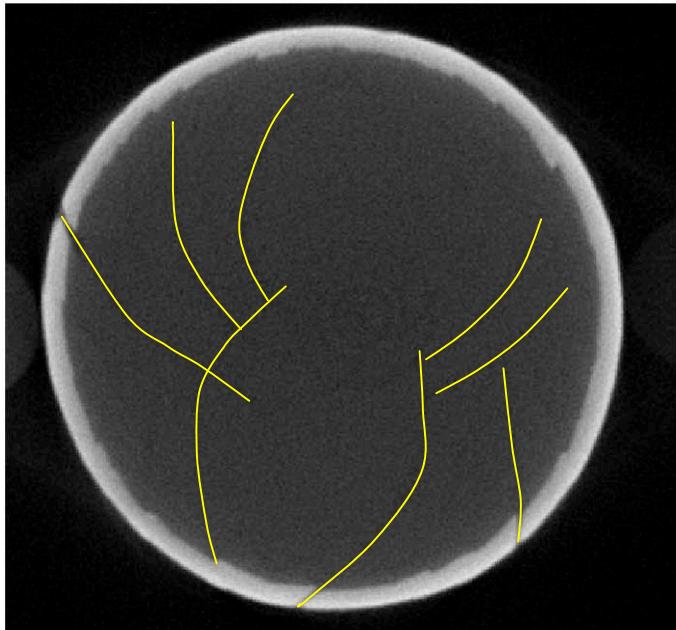


Impacted Sand

Name	Tap Density (g/cc)	Solid Crystal Density g/cc	Mean Particle Size _m	Particle Size St. Dev.
Sand	1.53	2.56	298.1	169.8
Sand			28.7	280
Impacted	2.25			
WC		7.7	39.9	11.6
WC			28.0	13.5
Impacted				



# Validation Experiments: Explosively Loaded Cylinder



- explosively compacted cylinders to allow comparison with simulations and analytic solutions
- more difficult than expected; also late time effects
- tomographic analysis of compaction difficult and reveals localizations





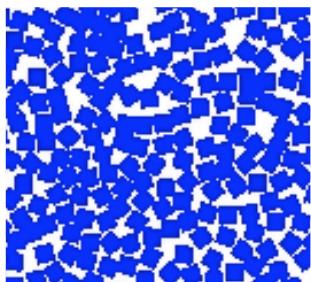
# Conclusions

- **planar waves in granular ceramics:**
  - very slow wave speeds
  - steady waves observed for several sample thicknesses
  - waves have finite rise times; strain rate  $\sim \sigma$
  - reloading stiffer than loading
  - dynamic response significantly stiffer than static response
- **validation experiments:**
  - suggest shortcomings of P- $\lambda$  model
  - wave attenuation, shape, and amplitude can constrain models
  - additional validation experiments needed
  - must rely on real-time diagnostics (VISAR, photography, etc.)
- **mesoscale simulations:**
  - nonuniform stress distribution (force chains) and localizations
  - significant lateral motion and distance to reach steady state
  - techniques such as peridynamics needed to capture missing physics
  - may be suitable for some macroscopic simulations

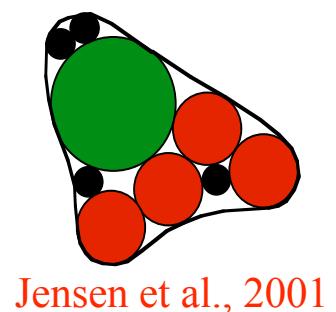
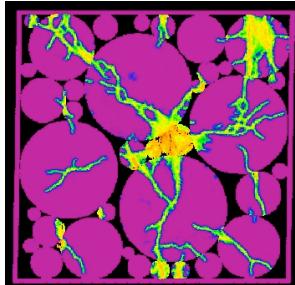


# Future Work

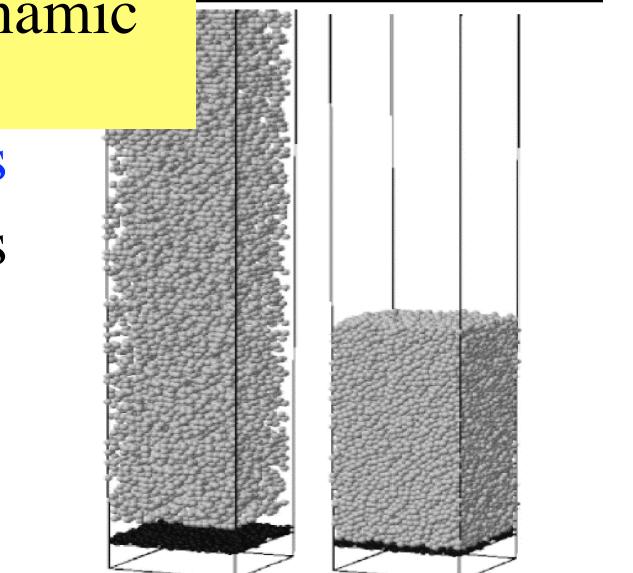
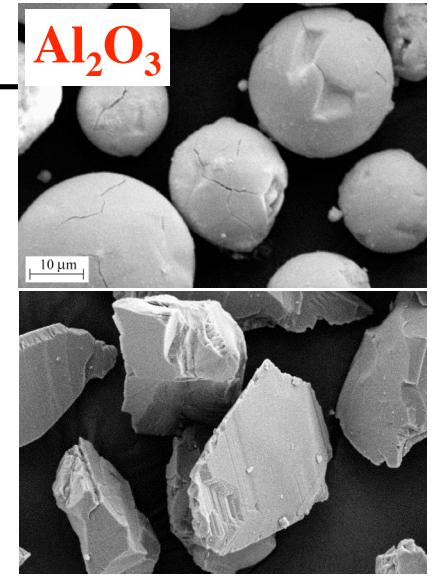
- further work on validation experiments with improved diagnostics
- additional study of morphology effects
- probe full compaction region
- characterize comminution of grains in recovered material
- predictive capability for variations in material
- understand relationship between static and dynamic behavior
- mesoscale modeling of validation experiments
- 3-D simulations with spheres and other shapes
- determine suitability of peridynamics



Silling, 2007



Jensen et al., 2001



Silbert, Ertas, Grest, Halsey and Levine,  
Physical Review E, 65, 031304, 2002