



Office of Nonproliferation Research and Development

Mechanical Properties of CeBr₃ for Calibration of an Embedded-Ion Method Model

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Advanced Inorganic Scintillators



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Project overview



- Determine cause of mechanical failure in LnX_3 scintillators;
- Develop practical strategies to scale detectors to large sizes

Goals:

Mitigate material limitations; Improve single crystal growth methods

Technical approach:

1. Measure thermal and mechanical properties
2. Model deformation and fracture mechanisms
3. Investigate alloy strengthening to improve fracture toughness
4. Develop seeded Bridgman growth to reduce thermal stresses

Deliverables:

Improved alloys, growth methods, and predictive model for elasticity and fracture of lanthanide halide scintillator materials

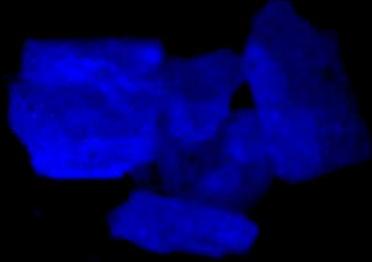
Capability improvement addressed:

Large, low cost gamma spectrometers for detection and monitoring of SNM



Alloys enable successful HGF crystals

UV luminescence images

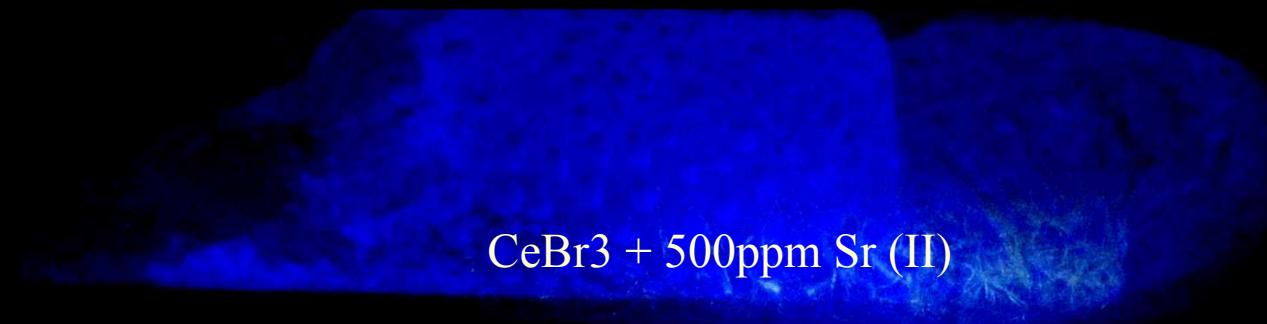


CeBr_3

*Strengthening agents increased unfractured size
from ≤ 1 centimeter to several inches*



$\text{CeBr}_3 + 500\text{ppm Hf (IV)}$



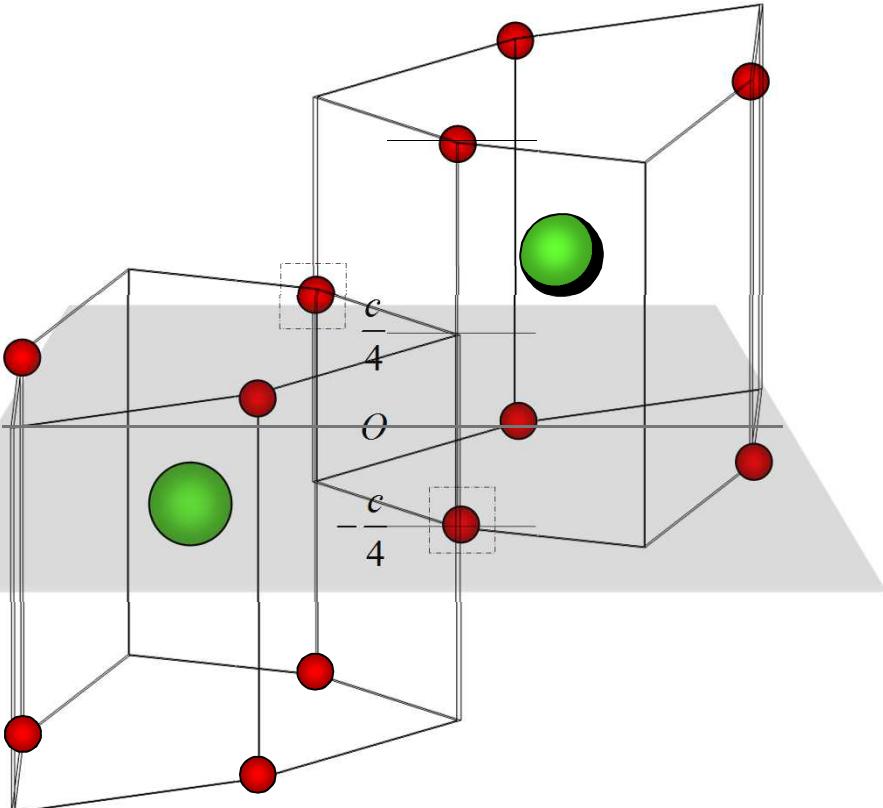
$\text{CeBr}_3 + 500\text{ppm Sr (II)}$

1 inch

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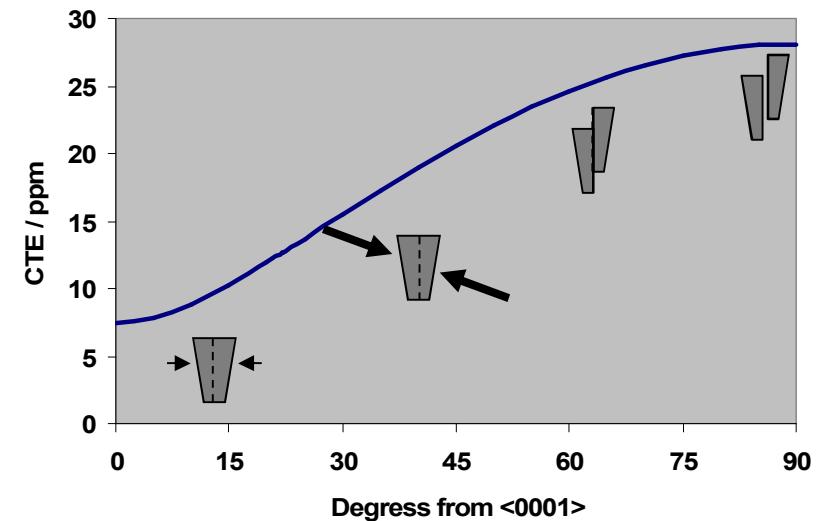
Model Development: Motivation

Limited and anisotropic slip result in formation of critical flaws on cleavage planes



Large anisotropy of thermal expansion results in shear forces on cleavage planes if gradient is not aligned with c-axis

- Pure compression for c-axis T gradient
- Both magnitude and orientation of shears increase rapidly for off-axis

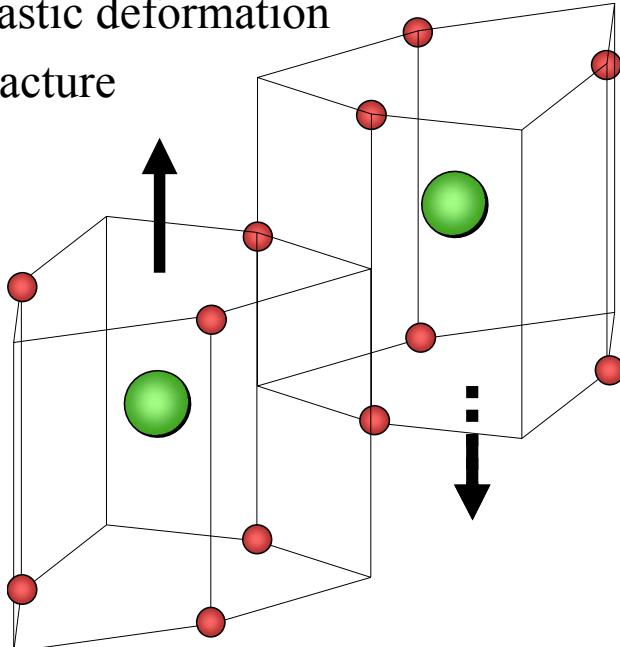


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Model Development: Limitations of current approaches

Problem: Develop modeling approach to simulate mechanics of LnX_3 crystals

- Thermal stress during growth
- Slip systems and dislocation reactions
- Plastic deformation
- Fracture



Slip and Fracture in LnX_3

1st generation ionic potentials: Fixed Charge

- Overestimates cohesive energy by factor of four!
- Stoichiometric compositions ONLY
- Can not treat defects

2nd generation: Variable Charge

- Charges solved by minimizing potential for each δt
- *Computationally VERY expensive.*
- Energy is not rigorously conserved!

3rd generation: This Work

The embedded ion method that we are developing solves these problems

- Equilibrium charges are analytically integrated:
- No energy minimization is required
- Energy is rigorously conserved

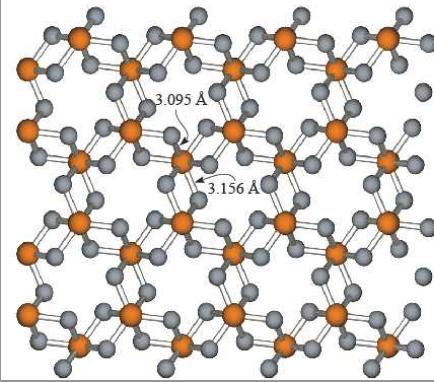
100 ns time scale, 1,000,000 atoms

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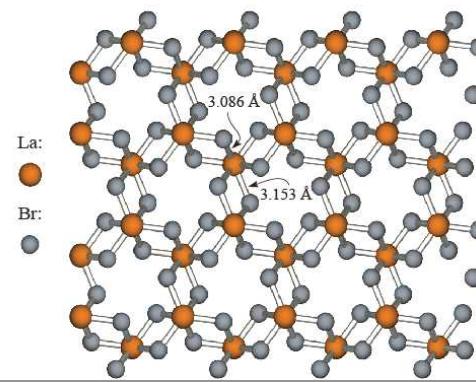
Model Development: Molecular Dynamics Simulations

Bond Length Prediction

(a) experimental LaBr_3 structure

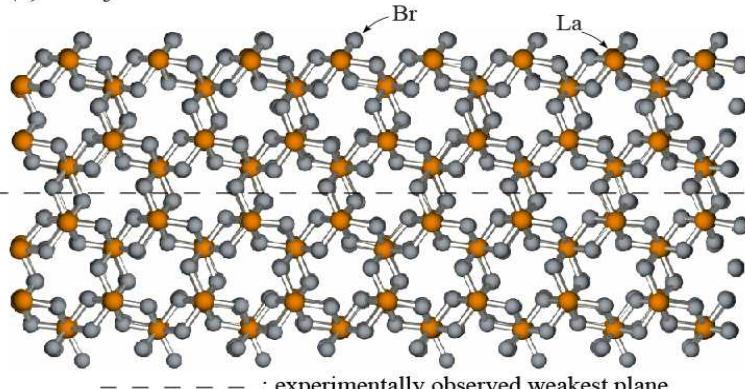


(b) predicted LaBr_3 structure



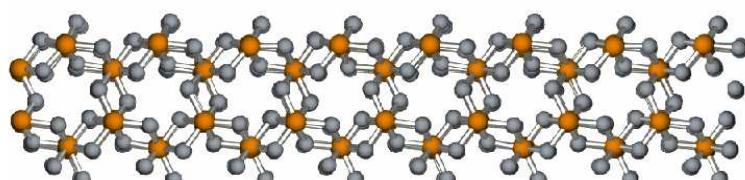
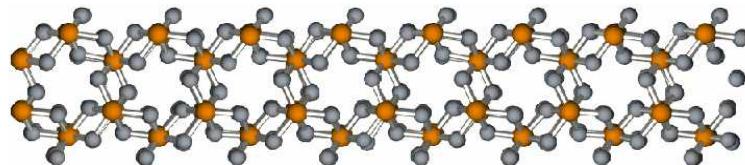
Cleavage Prediction

(a) LaBr_3 structure



--- : experimentally observed weakest plane

(b) Cleavage during MD straining simulation at 300 K



LaBr_3 Property Prediction

lattice constants (Å)				cohesive energy (eV/atom)		thermal expansion coefficient ($\times 10^{-8}$)			
a		c				a-axis		c-axis	
cal.	exp.	cal.	exp.	cal.	exp.	cal.	exp.	cal.	exp.
8.0	8.0	4.5	4.5	-4.3	-4.3	750	2800	860	800



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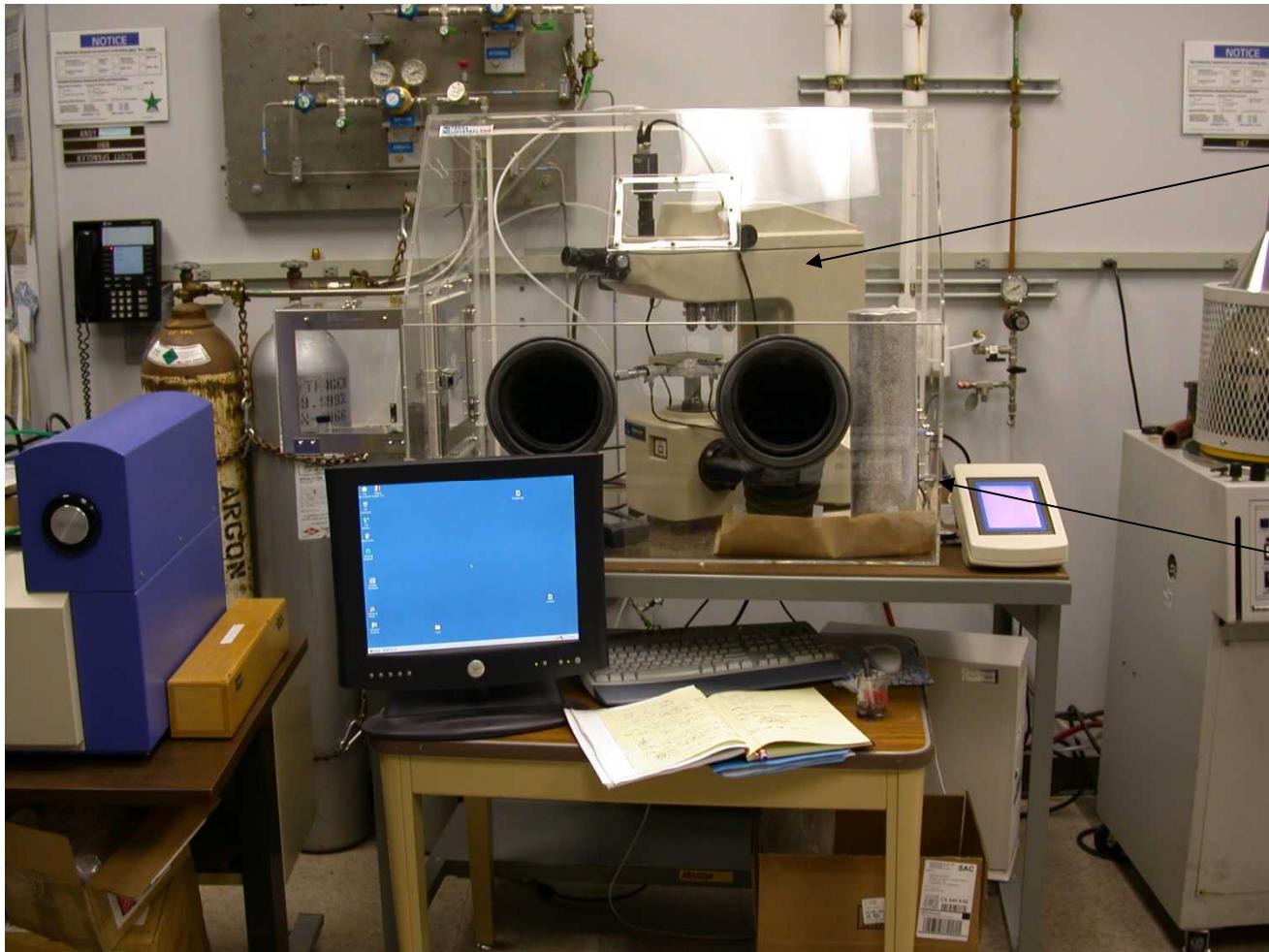
Summer overview



- **Calibration of embedded-ion method (EIM) model with mechanical property data**
 - I. Set-up a Vickers hardness tester with a moisture free environment
 - II. Validate indenter set-up and specimen preparation procedure
 - III. Analyze alloy strengthening with hardness and fracture toughness data
 - IV. Determine if non-destructive testing method is applicable for lanthanide halide alloys

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I. Vickers micro-indentation test set-up in controlled atmosphere



Vickers
hardness tester

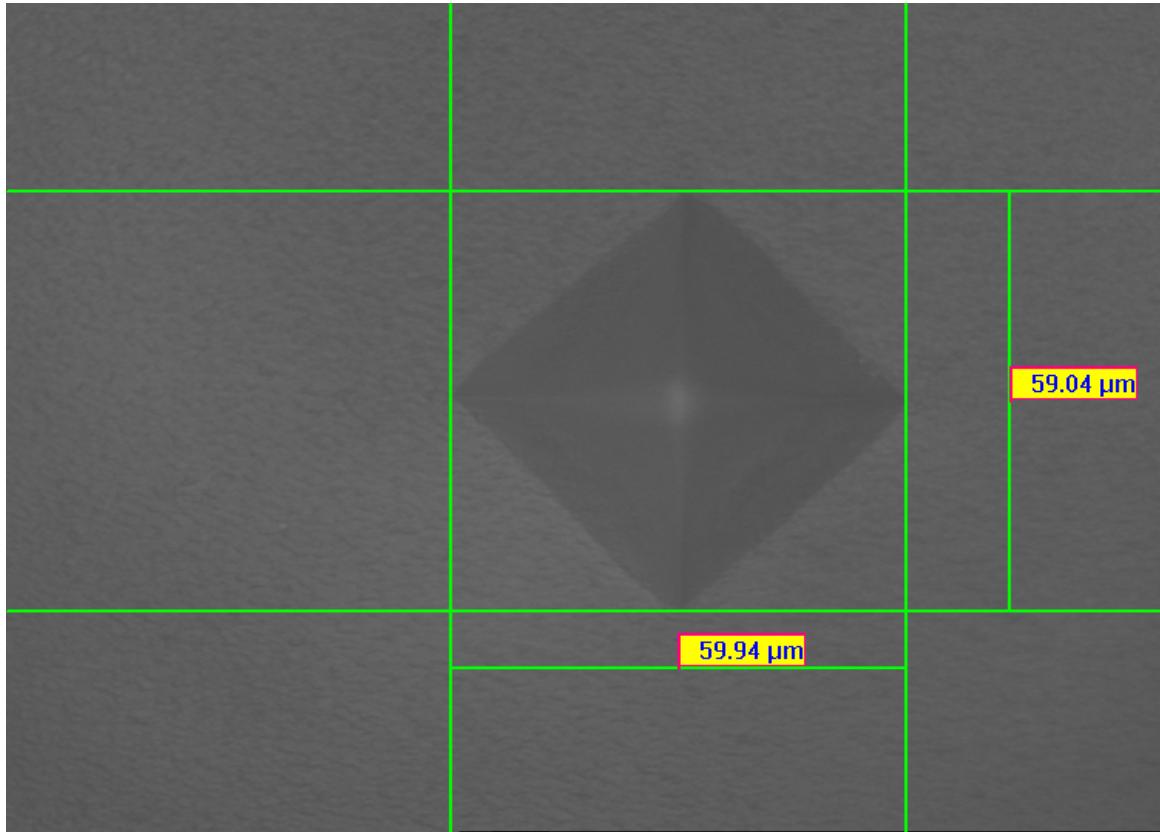
Dry nitrogen
atmosphere
filled glove box



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II. Validation of Vickers micro-indentation set-up and specimen preparation procedure



Lithium Fluoride hardness data cleaved {001} faces	Lithium Fluoride hardness data polished with 0.5 μm silica
HV0.2/20 (GPa) Roberts and Page, 1986	HV0.2/20 (GPa) 15 indents
1.10 ± 0.04	1.04 ± 0.01

$$HV = 0.0018544(P/d^2)$$

P = load, N

d = average length of the two diagonals of the indentation, mm

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IV. Use of NDT methods

Use longitudinal (V_L) and shear (V_T) wave velocities for determination of:

- a) Poisson's ratio
- b) Elastic modulus
- c) Shear modulus

$$\text{Velocity} = \frac{\text{Thickness}}{\frac{1}{2}(\text{TOF})}$$

$$\text{Poisson's Ratio, } \mu = \frac{1 - 2\left(\frac{V_T}{V_L}\right)^2}{2 - 2\left(\frac{V_T}{V_L}\right)^2}$$

$$\text{Modulus of Elasticity, } E = \frac{V_L^2 \rho (1 - \mu)(1 - 2\mu)}{(1 - \mu)}$$



$$\text{Shear Modulus, } G = V_T^2 \rho$$

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IV. Use of NDT methods

Property values determined for CeBr_3 strengthened with Cd

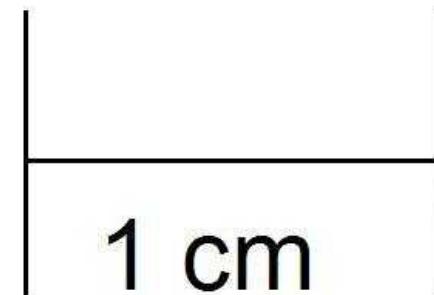
Longitudinal velocity, $V_L = 3.655 \times 10^5 \text{ cm/s}$

Transverse velocity, $V_T = 2.851 \times 10^5 \text{ cm/s}$

Poisson's ratio = -0.276

Elastic Modulus = 54 GPa

Bulk Modulus = 37 GPa





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Summary



EIM Model Calibration

Micro-indentation

- Set-up Vickers micro-indenter with a controlled atmosphere
- Validated set-up and specimen prep procedure with LiF
- Expanded property database of lanthanide halide alloys with additional hardness and fracture toughness data

Ultrasonic NDT

- Examined possibility of novel technique for lanthanide halide alloys
- Investigated appropriate coupling agents and transducers for determination of longitudinal and shear wave velocities.
- Begun NDT determination of mechanical properties (Poisson's ratio, elastic modulus, and bulk modulus) of strengthened lanthanide halide materials