



# **Connecting Microstructure and Micromechanics**

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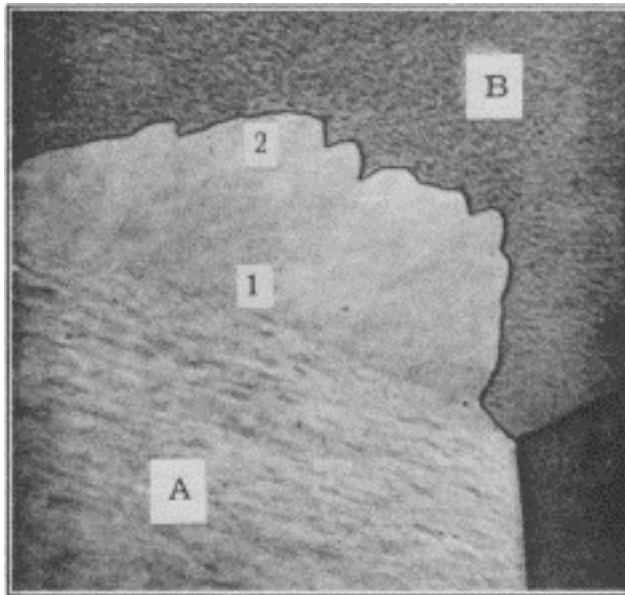
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## Motivation: Stress-Induced Grain Boundary Migration

- Grain boundaries move not only to minimize interfacial energy, but also to minimize stored elastic and plastic strain energy.

**Example:** Stress-induced grain boundary migration (SIGBM) in aluminum



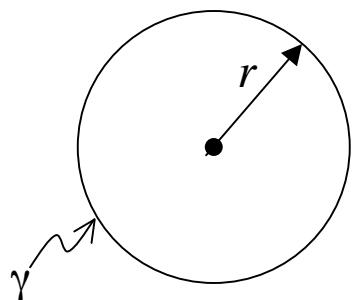
R. E. Reed-Hill, *Physical Metallurgy*, 1973.

- Can microstructural models capture the interaction between grain structure and mechanical state?

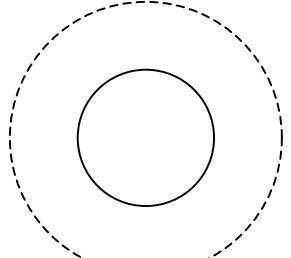


# Evolution mechanisms in SIGBM

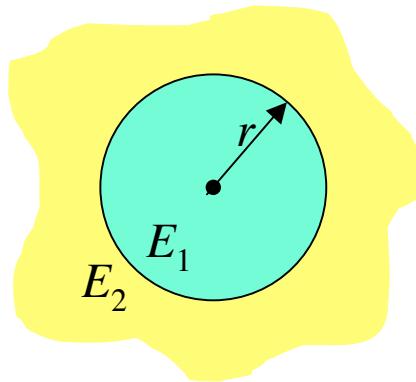
Curvature



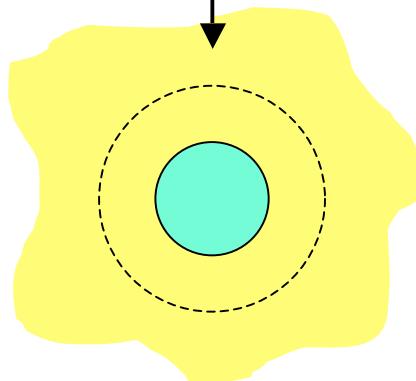
$$v_\kappa = -M_\kappa \gamma \kappa$$



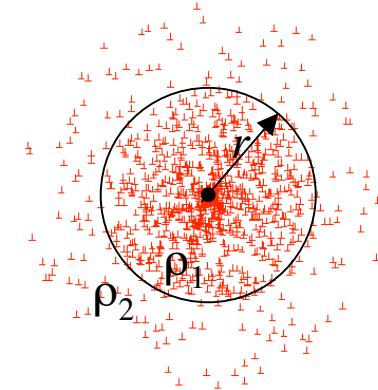
Elastic Energy



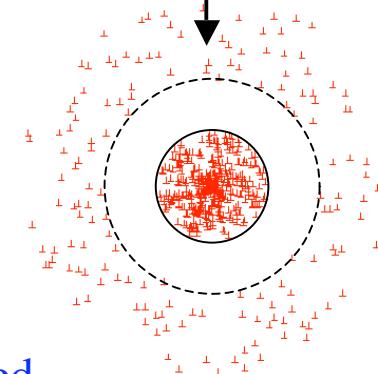
$$v_\epsilon = M_\epsilon (E_2 - E_1)$$



Defects



$$v_\perp = \begin{cases} -M_\perp F_\perp \rho_1 & \rho_1 > \rho_2 \\ M_\perp F_\perp \rho_2 & \rho_1 < \rho_2 \\ 0 & \rho_1 = \rho_2 \end{cases}$$



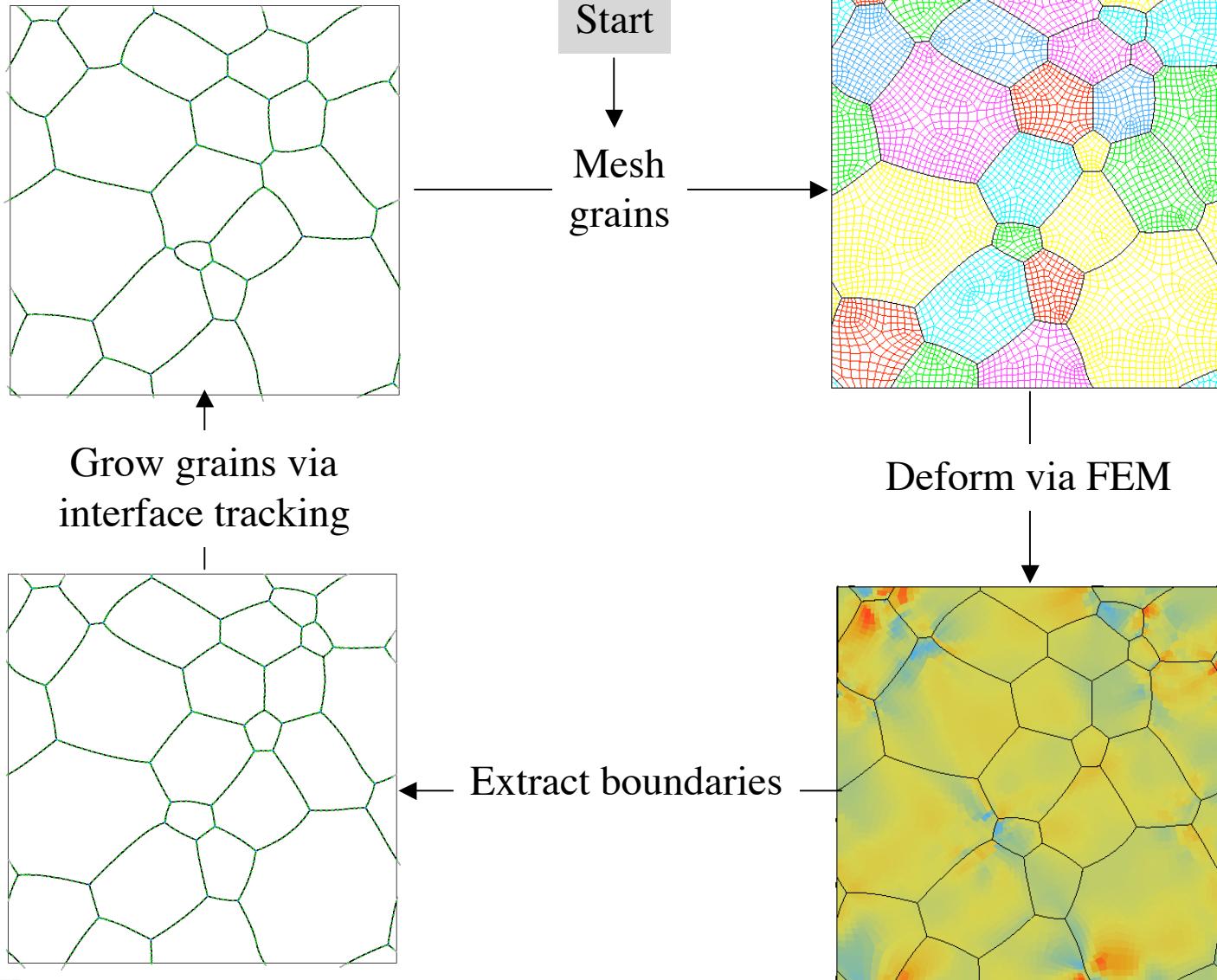
\*Each mechanism also causes stresses to be re-distributed.



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# Schematic of fully-coupled SIGBM model





# Grain growth and stress evolution in 1% tensile hold test

- Perform tensile hold test: Pull to 1% elongation, hold while grains grow.
- Interfacial, elastic, and plastic driving forces are included.
- Note stress concentrations at triple junctions and increasing internal stress.

## Inputs:

$$C_{11} = 168.4 \text{ MPa}$$

$$C_{12} = 121.4 \text{ MPa}$$

$$C_{44} = 75.4 \text{ MPa}$$

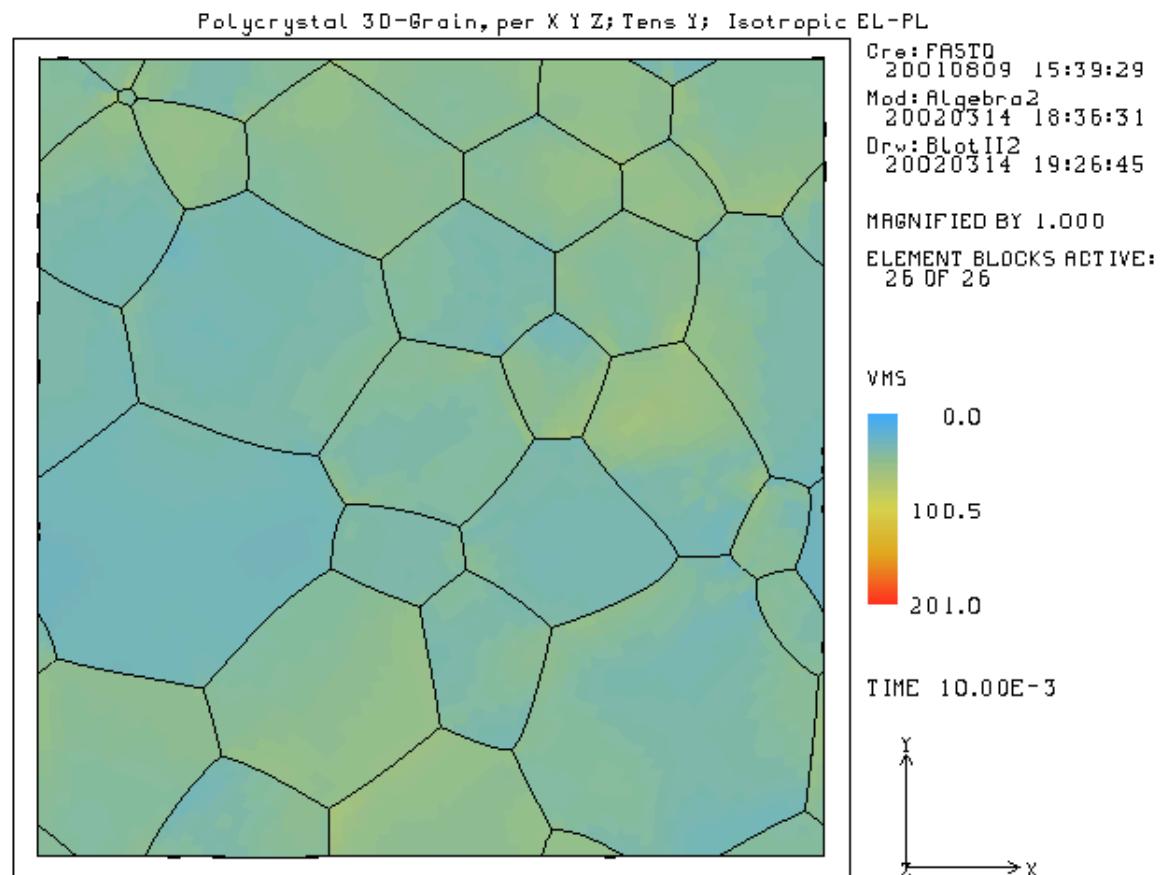
$$\tau_o = 168.4 \text{ MPa}$$

$$A = 121.4 \text{ MPa}$$

$$n = 75.4 \text{ MPa}$$

## Output:

von Mises Stress [MPa]



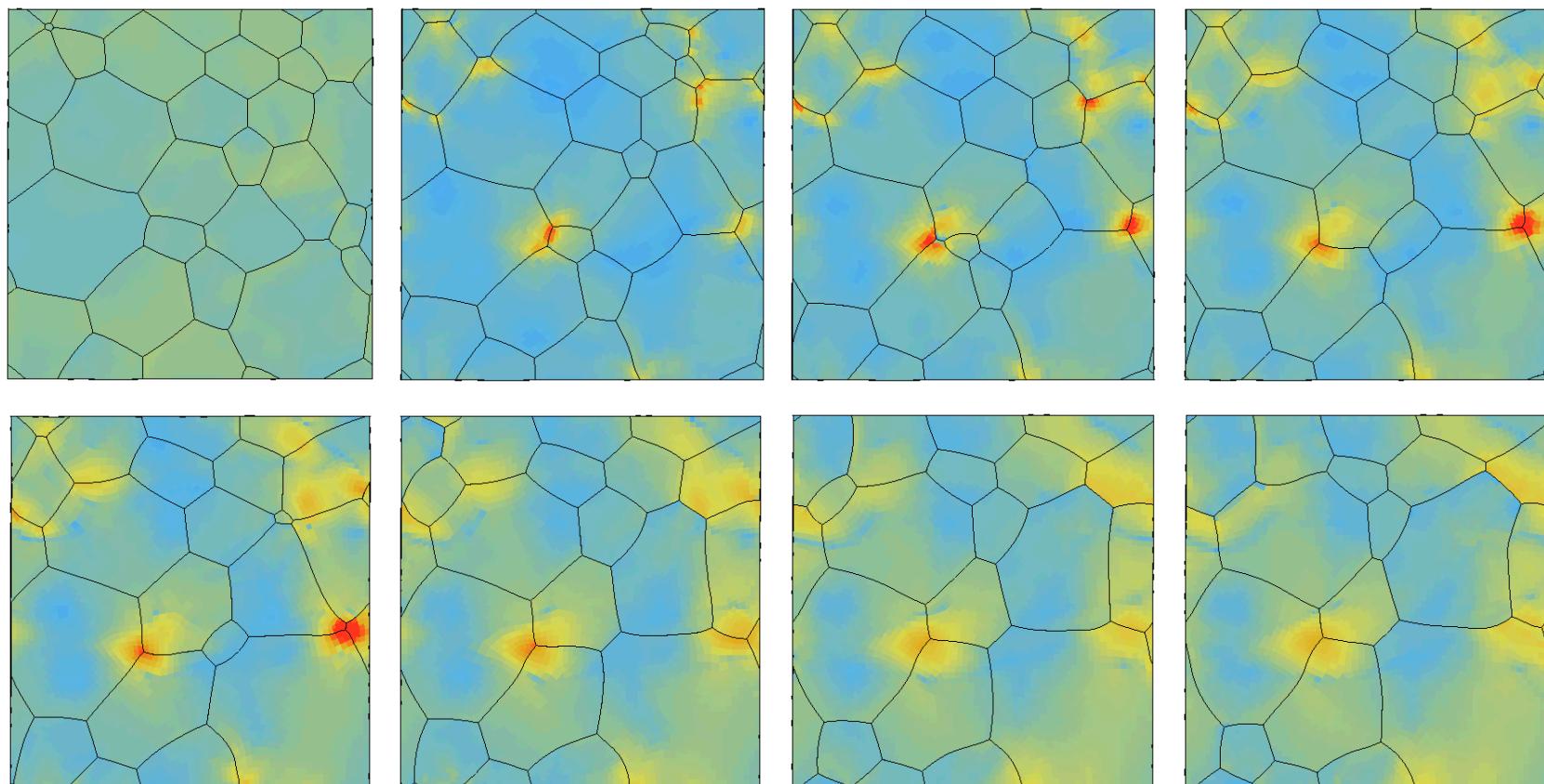


# Grain growth and stress evolution in 1% tensile hold test

Von Mises Stress [MPa]



0.0 201.0





# Dislocation density evolution in 1% tensile hold test

- Pull to 1% elongation, hold while grains grow.
- Dislocations are swept out by moving boundaries.
- Dislocation density increases at triple junctions.

## Inputs:

$$C_{11} = 168.4 \text{ MPa}$$

$$C_{12} = 121.4 \text{ MPa}$$

$$C_{44} = 75.4 \text{ MPa}$$

$$\tau_o = 168.4 \text{ MPa}$$

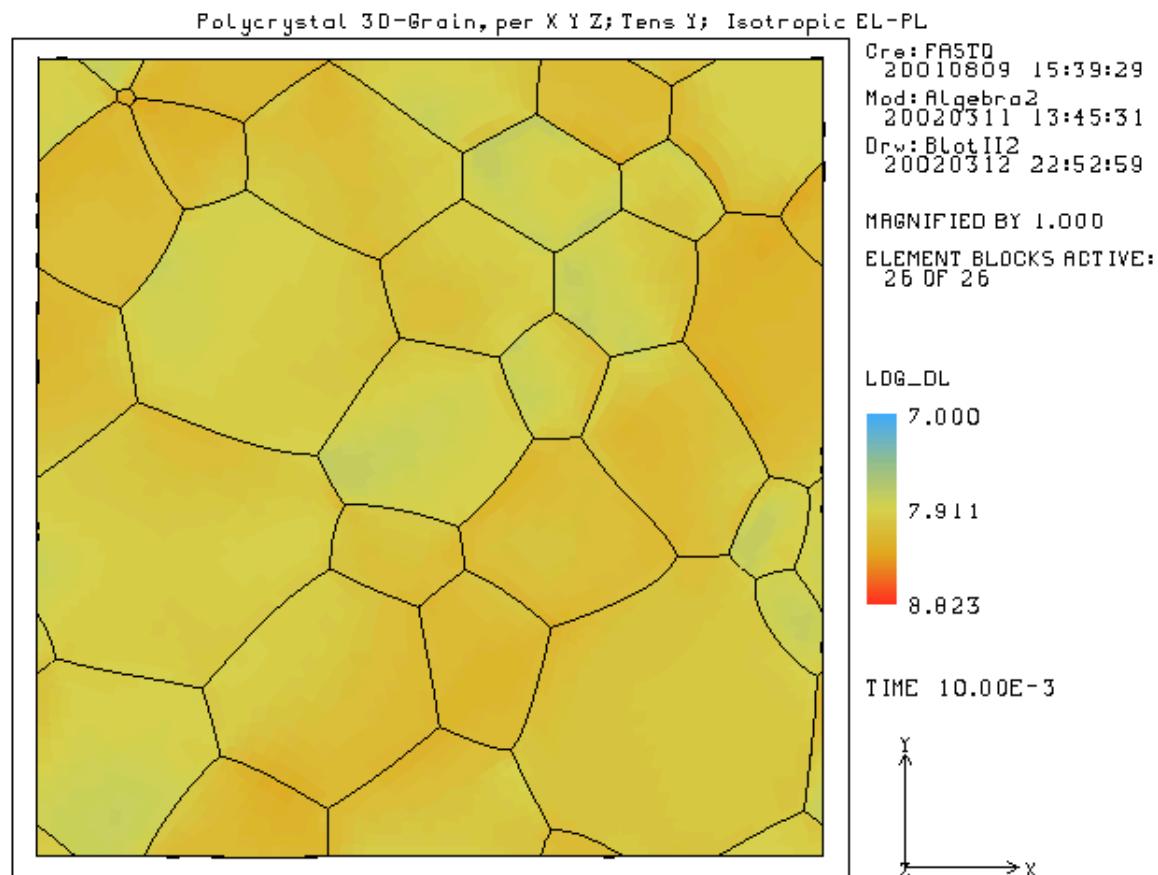
$$A = 121.4 \text{ MPa}$$

$$n = 75.4 \text{ MPa}$$

## Output:

$$\log(\rho_{\perp})$$

$$\rho_{\perp} = \left( \frac{\tau_{crss} - \tau_o}{\alpha G b} \right)^2 \text{ [cm}^{-2}\text{]}$$

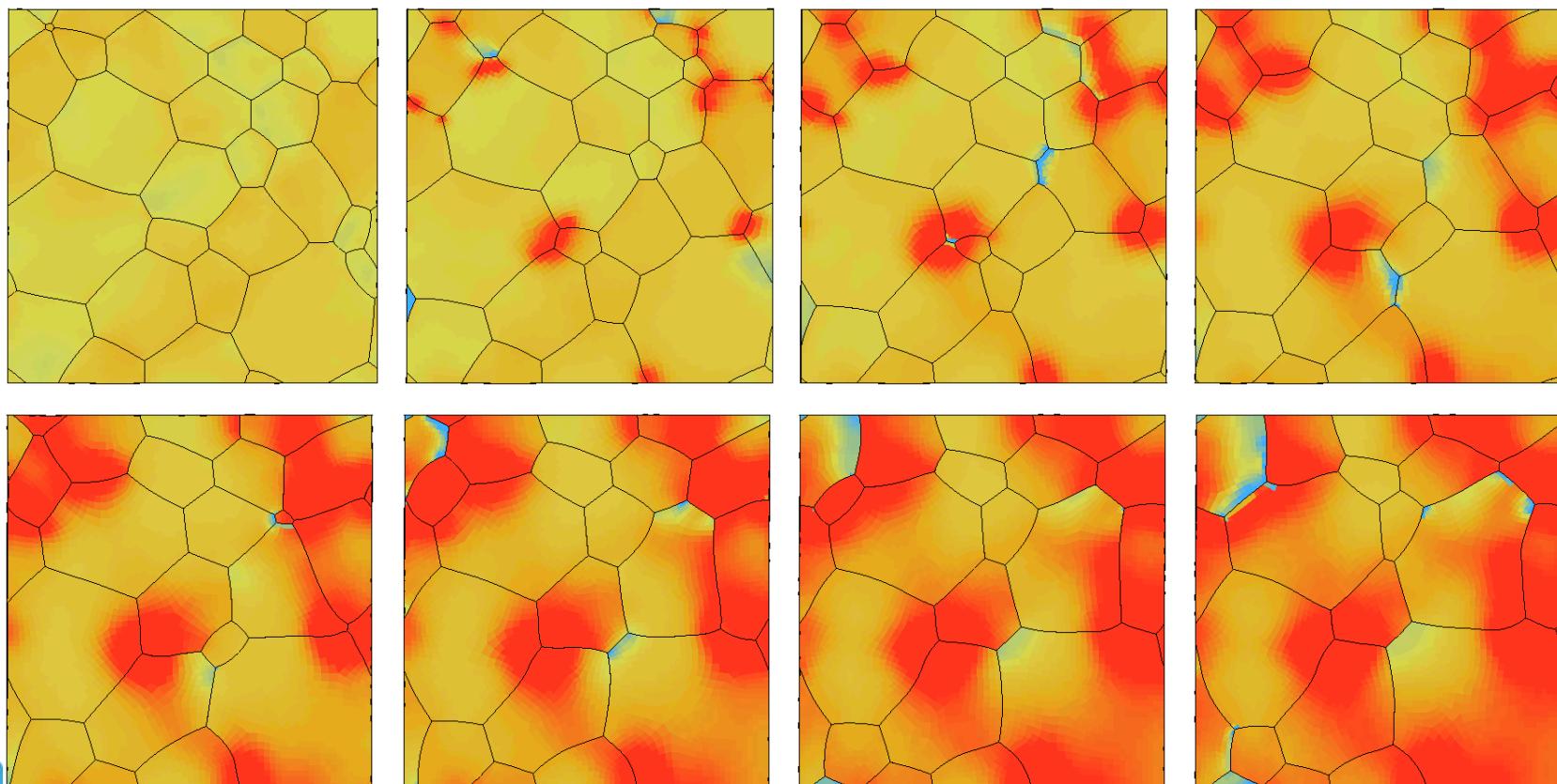




# Dislocation density evolution in 1% tensile hold test

$$\log(\rho_{\perp}) \quad \rho_{\perp} = \left( \frac{\tau_{crss} - \tau_o}{\alpha G b} \right)^2 \quad [\text{cm}^{-2}]$$


7.000 8.823



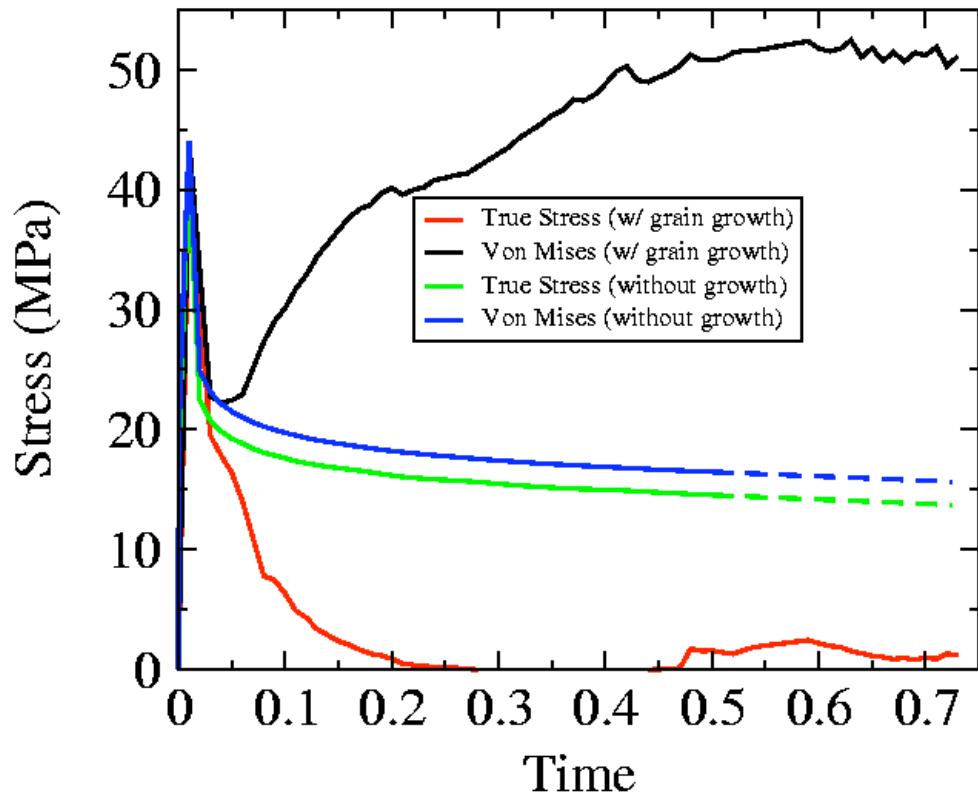
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## Stress evolution during 1% tensile hold test

- Load drops during grain growth, but internal stresses rise.
- This effect is directly attributable to the actions and interactions of evolving grains.
- Traditional continuum models do not exhibit this behavior.

⇒ The power of microstructural modeling is revealing the effects of the discrete microstructural network.





## Conclusion

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- **To capture the link between microstructure and plasticity, we have directly coupled the evolution of microstructure and micromechanics.**
- **Microstructure and micromechanics are interdependent; both are required for a full representation of materials response.**