

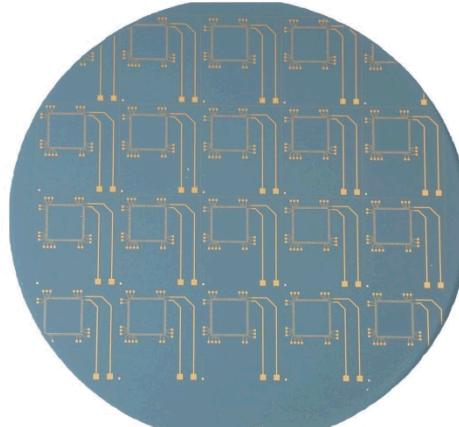
NM Tech, Graduate Seminar , April 4th, 2014

Synthesis and Thermal Stability of Gold-Zinc Oxide Nano-Composite Thin Films for Electrical Contacts

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Outline

- **Technical Gold Usage Demand**
- **What is Hard Gold?**
- **Electroplating methods & problems**
- **Physical Vapor Deposition Methods**
- **Characterization of PVD Au-ZnO Thin Film**
- **Thermal Stability of Film**
 - DSC, Resistivity, In-situ TEM



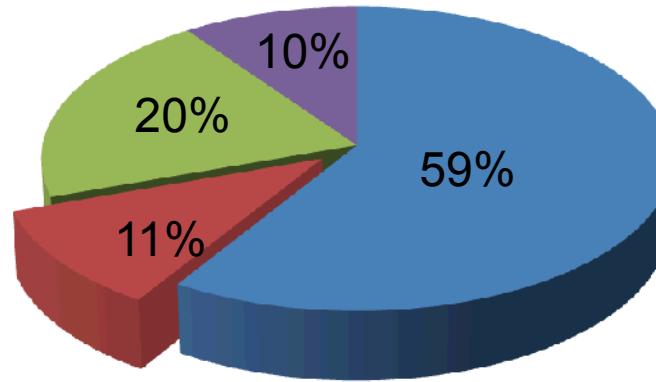
Gold Usage

World Gold Council, Gold Demand Report Feb. 2014

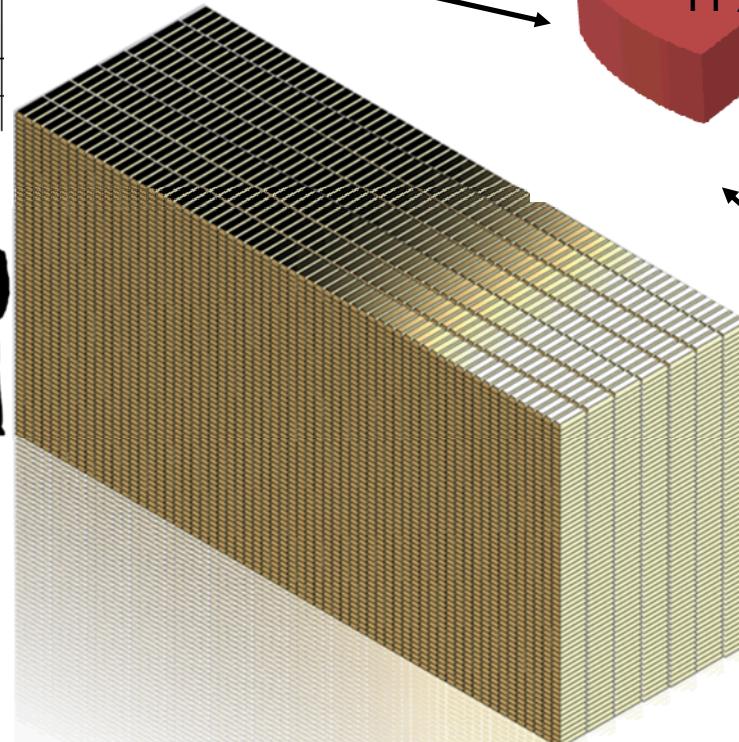
Tonnes	2012	2013 ¹
Jewellery	1896.1	2,209.50
Technology	407.5	404.8
Electronics	284.5	282.4
Other Industrial	84.4	85
Dentistry	38.6	37.3
Investment	1,568.10	773.3
Total bar and coin demand	1,289.00	1,654.10
Physical Bar demand	962.7	1,266.90
Official Coin	213	283.4
Medals/Imitation Coin	113.4	103.8
ETFs & similar products ³	279.1	-880.8
Central bank net purchases	544.1	368.6
Gold demand	4,415.80	3,756.10
London PM fix, US\$/oz	1,669.00	1,411.20

8% Electronic Appl.
(300,000 kg / year)

WGC Gold Demand 2013



- Jewellery
- Technology
- Investment
- Central Bank



1% Dentistry
(included in Tech. usage)

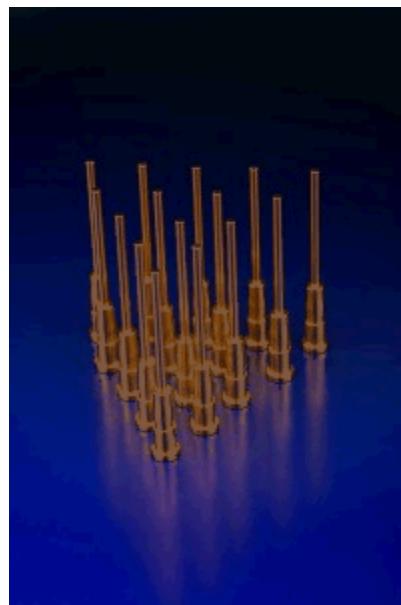


Technical Application

Electronic connectors and switches

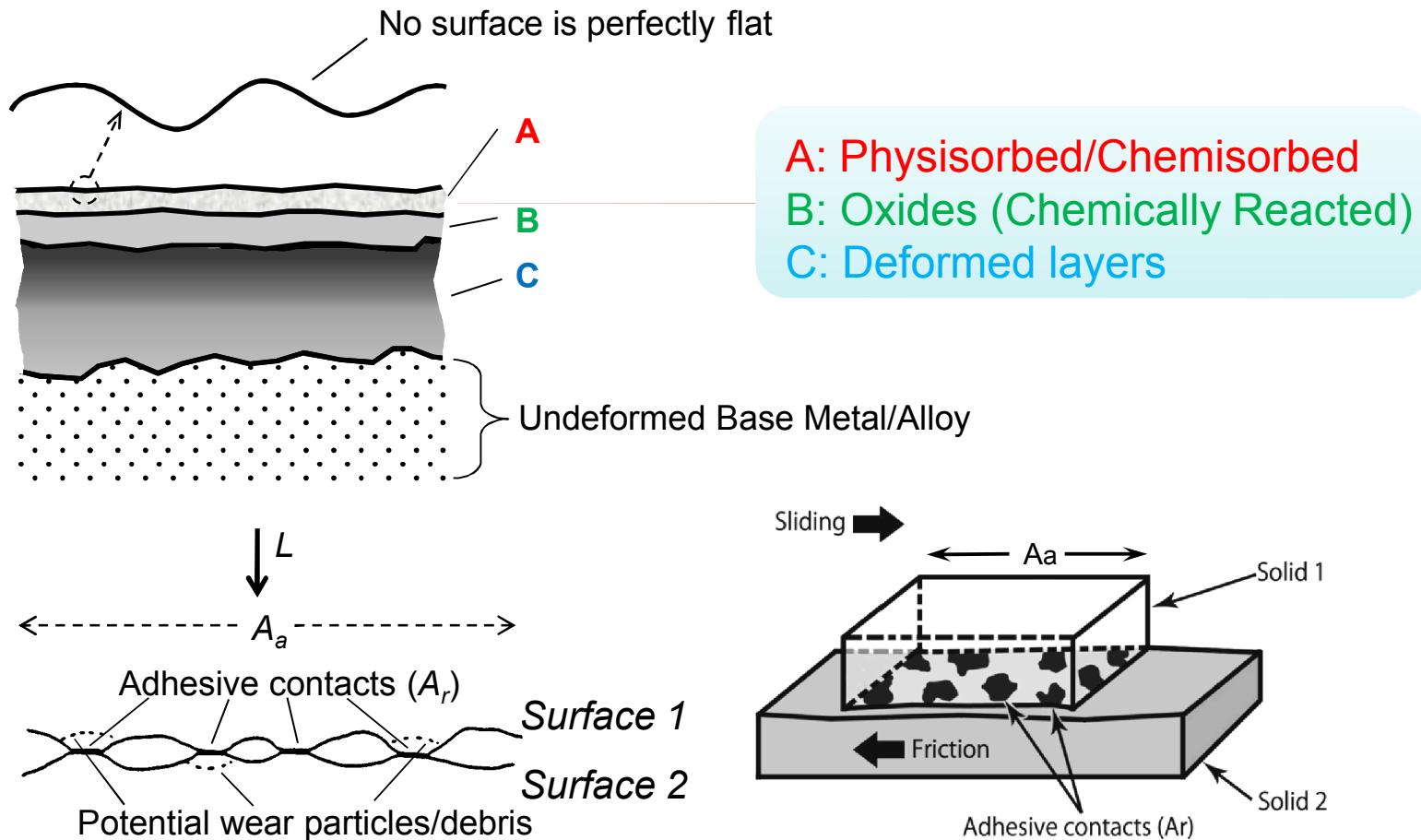
Electronics Applications:
Connectors and contact pads on
printed circuit boards

Chemically Inert and low electrical
resistance



Nature of Metallic Surfaces

Sliding electrical contacts



*Real area of contact (A_r) to be minimized for low adhesion (Low Adhesive Wear)
Or maximized for reduced electrical contact resistance (ECR)*

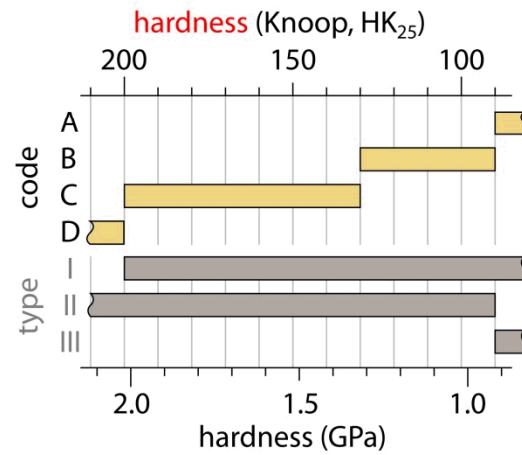
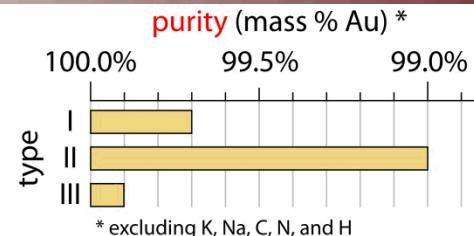
Hard Gold

ASTM Types

From ASTM B488-11 / MIL-DTL-45204D:

	type	suggested applications (ASTM)
> 99.7% Au (hardest)	I	general-purpose, high-reliability electrical contacts
> 99.0% Au	II	general-purpose, wear resistance; low temperature only
(softest)	III IIIA	soldering; limits impact of oxidation of codeposited material semiconductor components, nuclear eng., high temperature

- Pure gold is soft (low yield point) and has unacceptable amount of friction and wear
- Gold is typically hardened with minute alloying of Ni or Co (referred to as hard gold) to achieve the desired balance between friction, wear and ECR
- Current practice is to apply hard gold by electrodeposition
- *Nickel Underplating is used any time the substrate alloy contains Copper to prevent diffusion of Cu into Au coating.*



class	minimum thickness μinch	μm
00	20	0.51
0	30	0.76
1	50	1.27
2	100	2.54
3	200	5.08
4	300	7.62
5	500	12.70
6	1500	38.10

Hall-Petch Strengthening

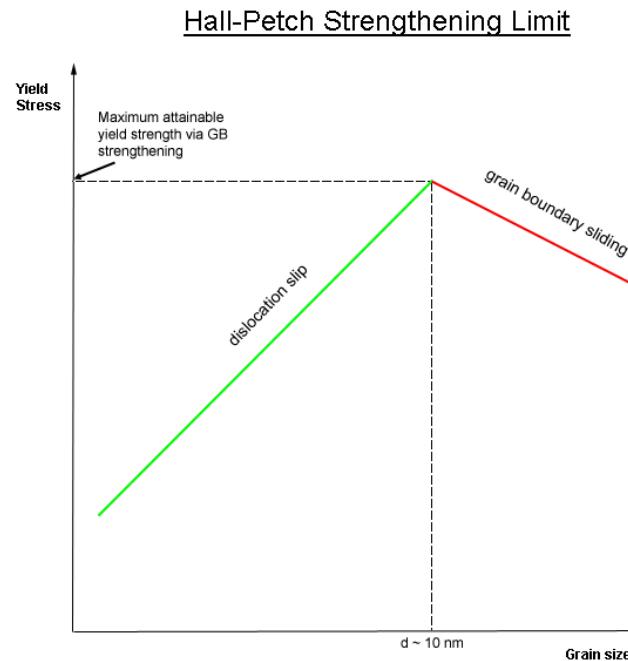
Grain Refinement

Hall-Petch relationship:

$$H = H_o + K_H d^{-1/2}$$

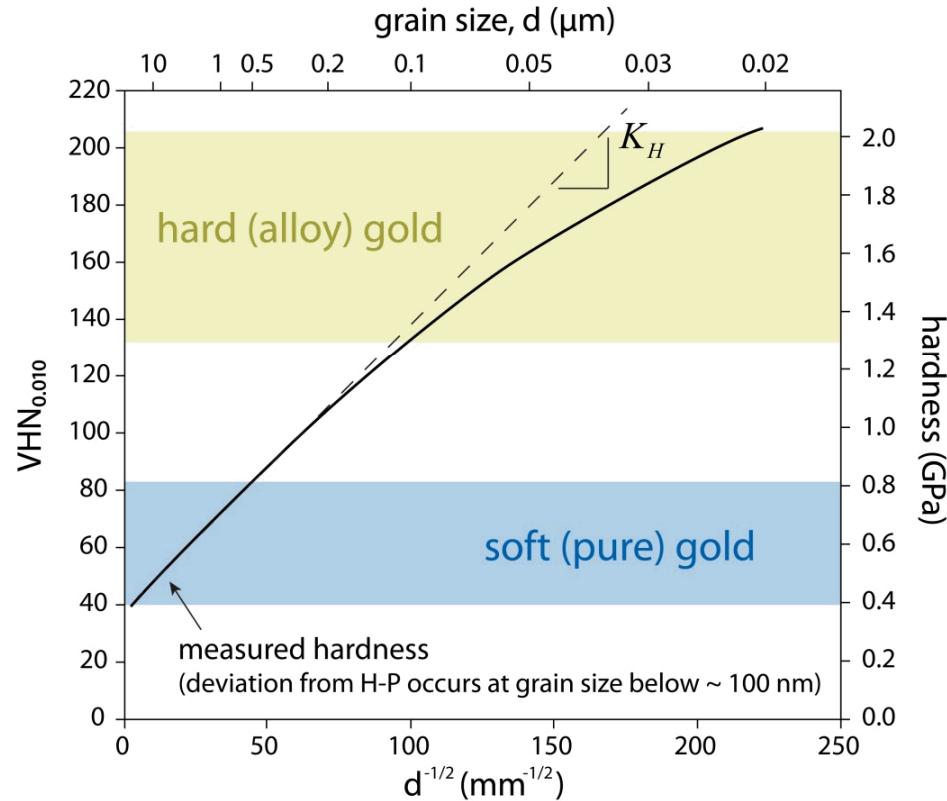
H - hardness

d - avg. grain diameter



Theoretical maximum strength
at ~ 10 nm

From: Lo, Augis, and Pinnel, JAP (1979)



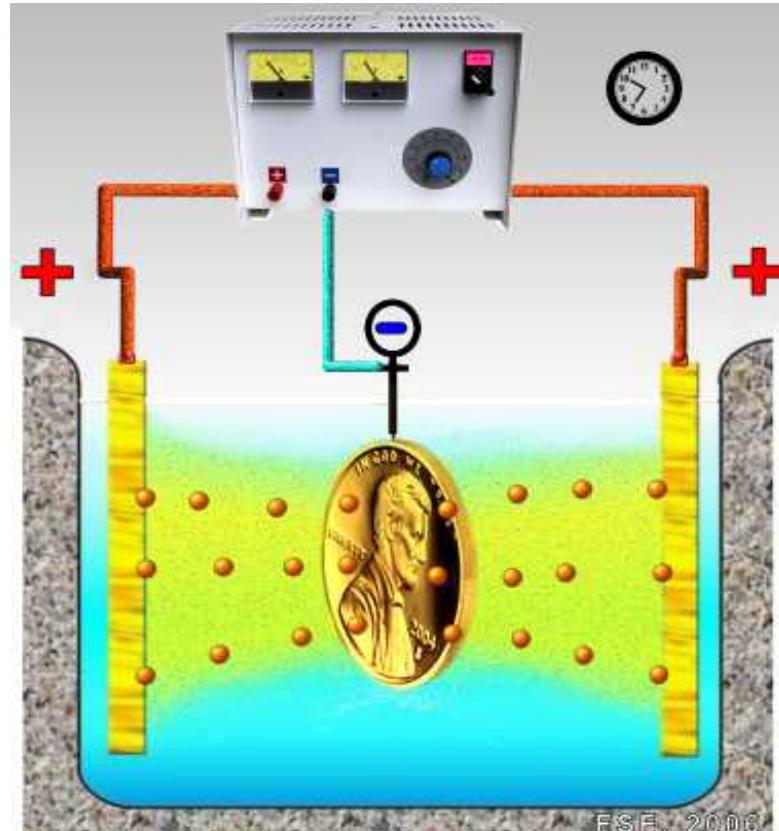
Electrochemical Deposition



Toxic plating baths



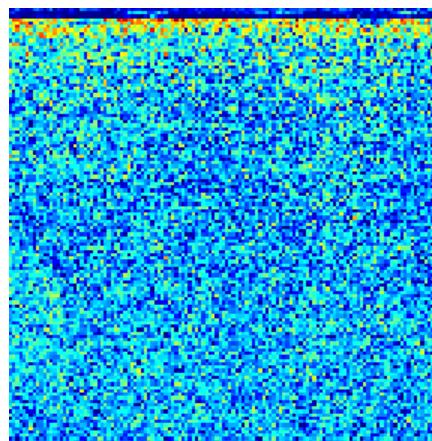
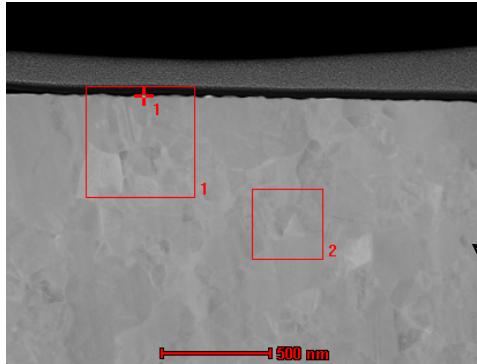
Hard Gold is typically plated from cyanide solution $\text{KAu}(\text{CN})_2$, a citrate buffer solution modifiers of As, Cd or Tl, a small amount of a hardening agent such as Ni or Co Nickel barrier layer applied first



Issues With Electroplated hard Au

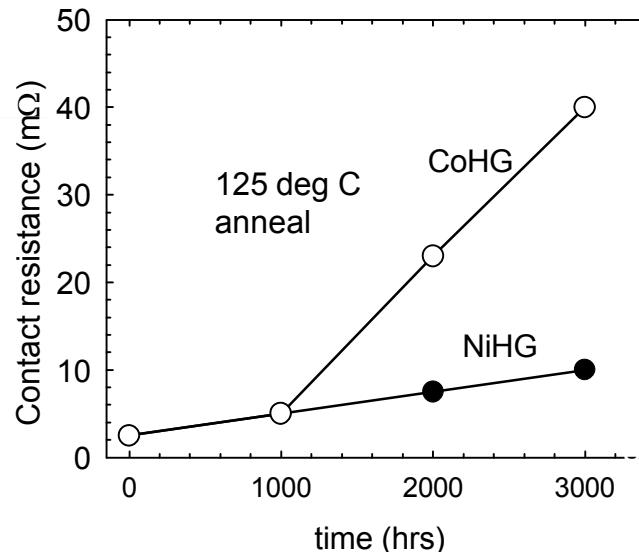
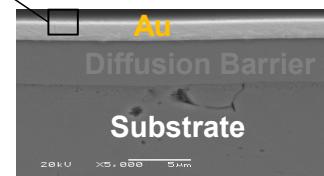
Surface oxide formation

Cross-sectional TEM and Spectral Imaging



Relative Ni concentration
After 35+ years

Ni or Co used for hardening Au may diffuse to the surface over time

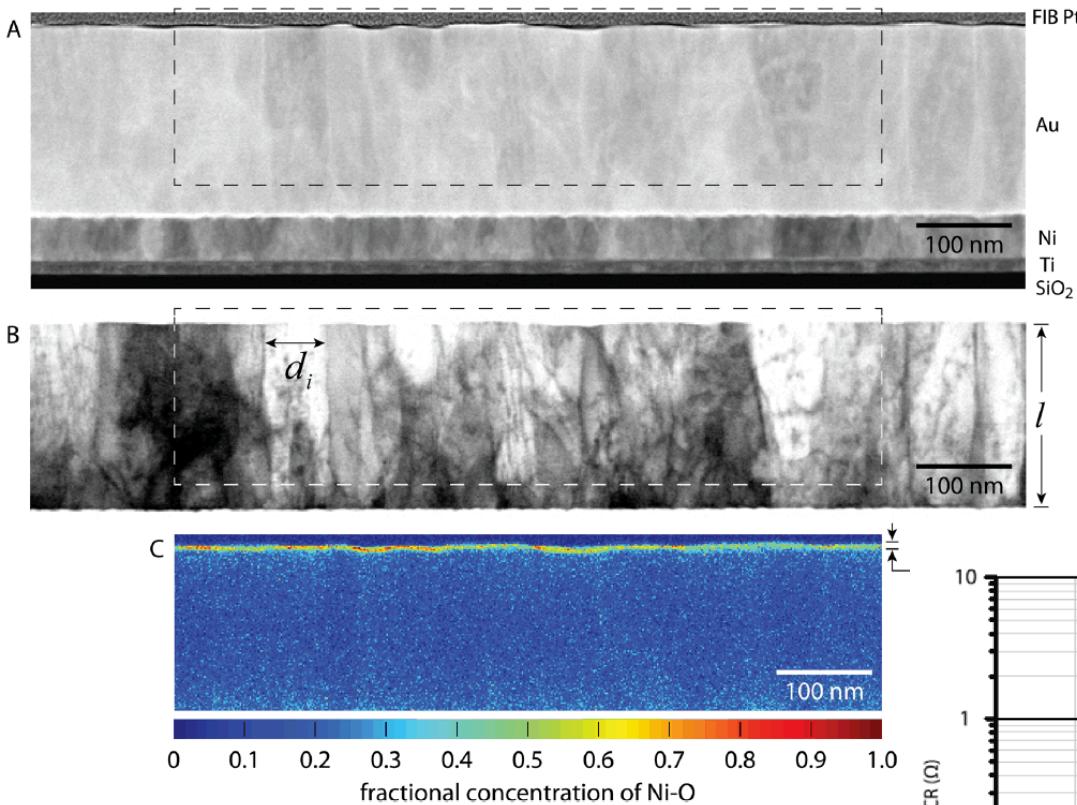


Y. Okinaka and M. Hoshino, *Gold Bulletin*, 31(1), 3 (1998).

- Diffusion and segregation of hardeners and elements from “diffusion barriers” to the surface (ECR degradation)
- Limited electrochemistry (hardeners/diffusion barriers)
- Non-Technical issues...

Surface Oxide Film

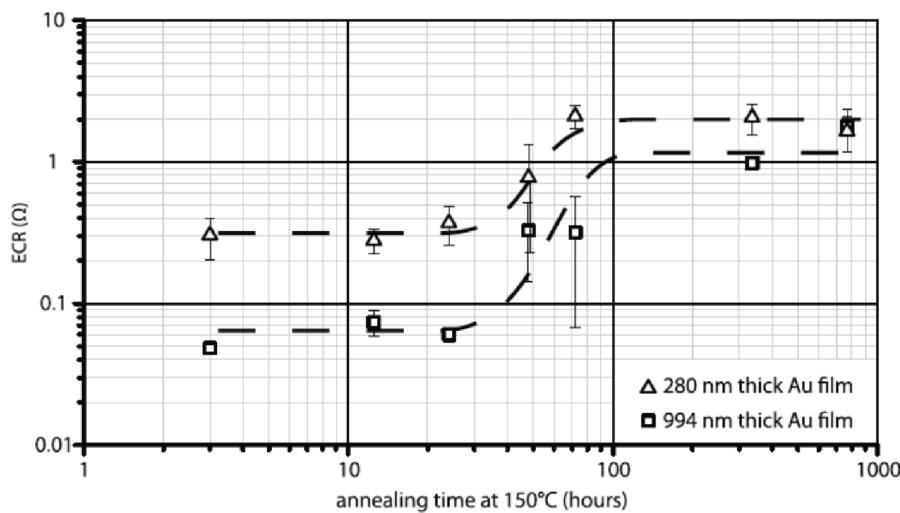
ECR degradation



STEM EDS after 150°C and 32 days
NiO surface layer 1.5 – 4.5 nm thick

Sputtered Au 280nm Film on
Silicon w/Ti adhesion layer
Ni Barrier layer

ECR degradation with time
(diffusion through grain boundaries)

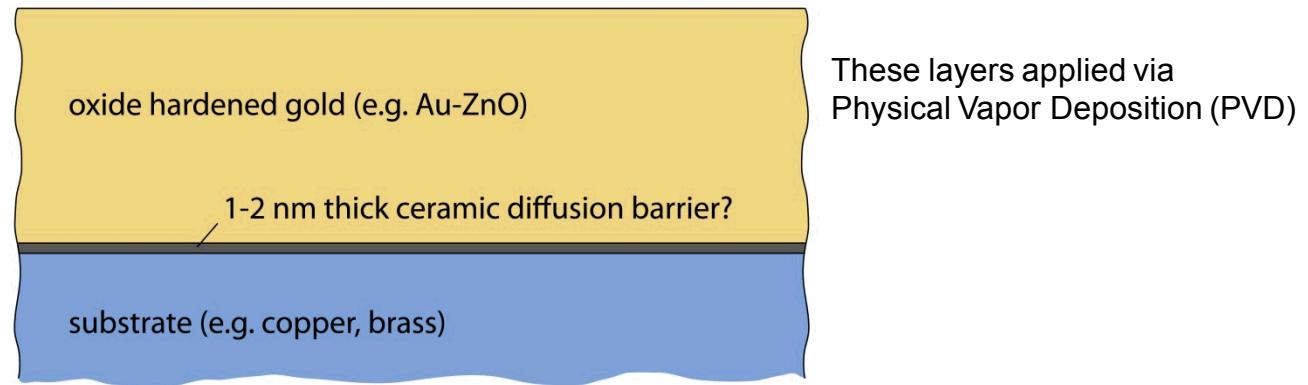


Novel Materials and Synthesis

Routes to Mitigate Diffusion

Novel routes: shut down solid diffusion of codeposited and underlayer materials via:

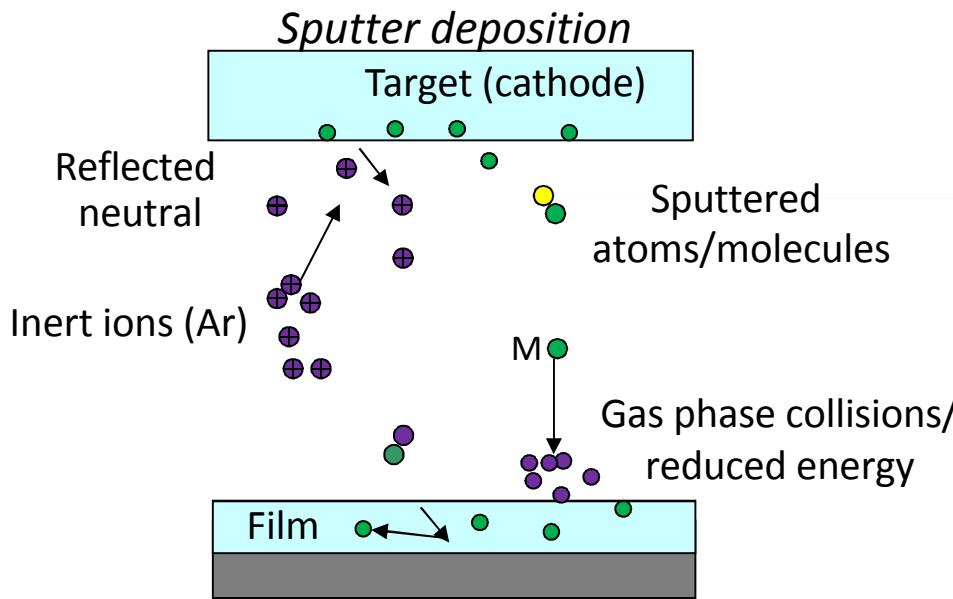
1. ceramics to harden Au in place of non-noble metals
2. introduce electron-tunneling-thin ceramic diffusion barrier layers
(discussion of its effect on ECR)



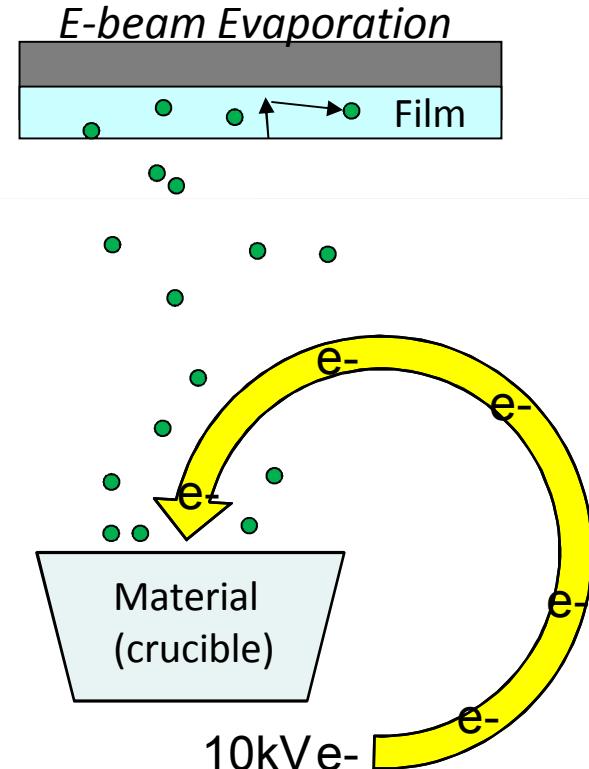
- *Au-ZnO codeposition by E-beam evaporation*
- *Ion implantation of noble gasses into the PVD Au*
- *Novel ceramic diffusion barrier layers (not possible by electrochemical techniques)*

Physical Vapor Deposition (PVD)

Sputtering vs E-beam Evaporation



- Target material removed by kinetic energy of inert ions
- Requires plasma ignition for ionization of sputter gas (Ar)
- Minimum energy for ignition limits deposition rate ratio $\sim 50:1$ (2%)
- Good control over film properties (pressure, power, biasing, temperature)



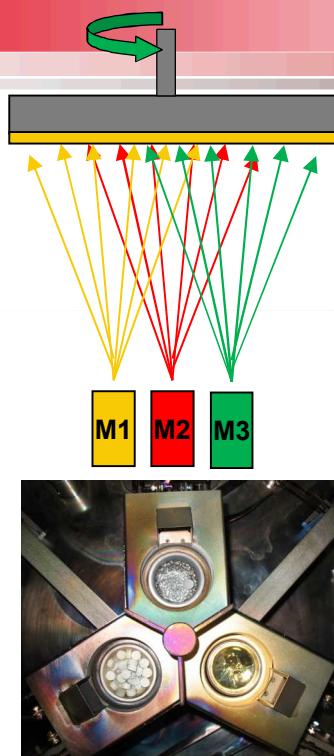
- Target material vaporized by thermal energy from electron beam
- Terrific rate control with feedback from QCM
- Can deposit at extremely slow rates (ppm level composition control)

Co-Deposition (PVD)

Thin Film Capabilities

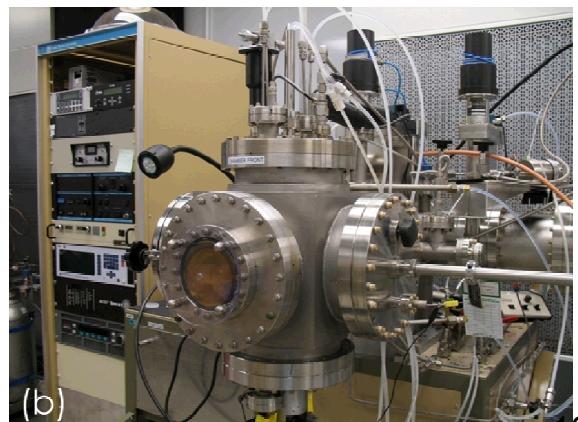
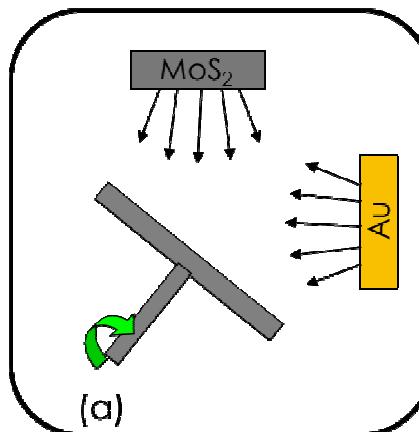
Evaporation:

- Triad e-beam evaporation of ternary alloy thin films
- Shutter in front of substrate for consistent composition, graded or layered films
- Independent QCM control of material deposition rate
- Compositional control to < 0.1%



Sputtering:

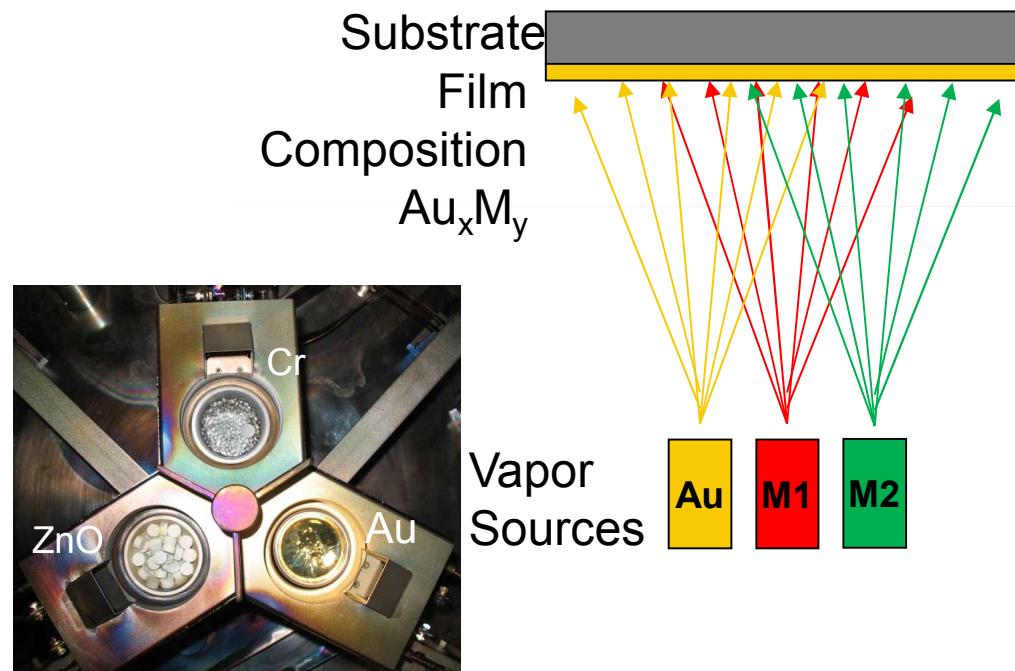
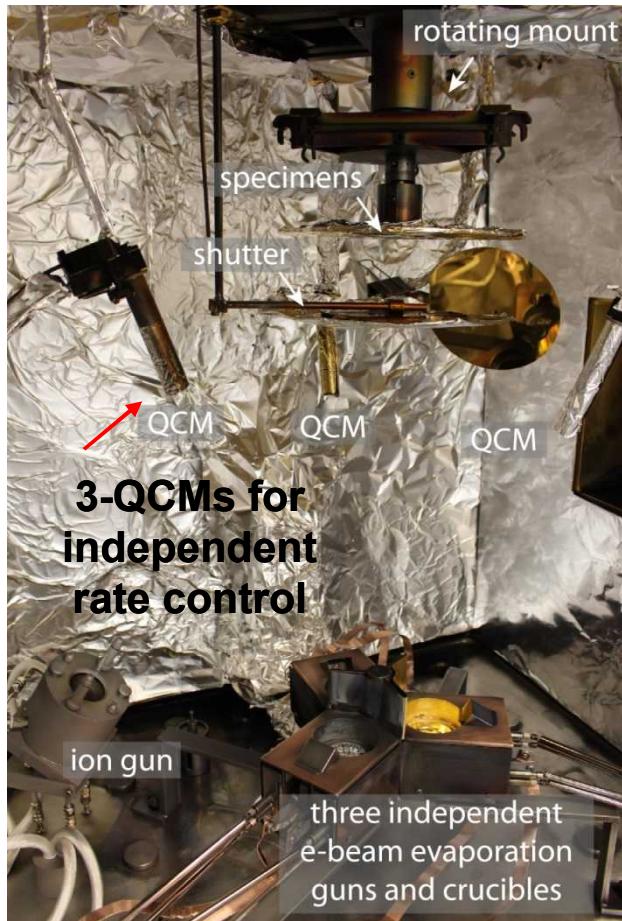
- Co-deposition of elements, alloys and compounds
- Composition control to ~1%



Triad E-Beam Deposition



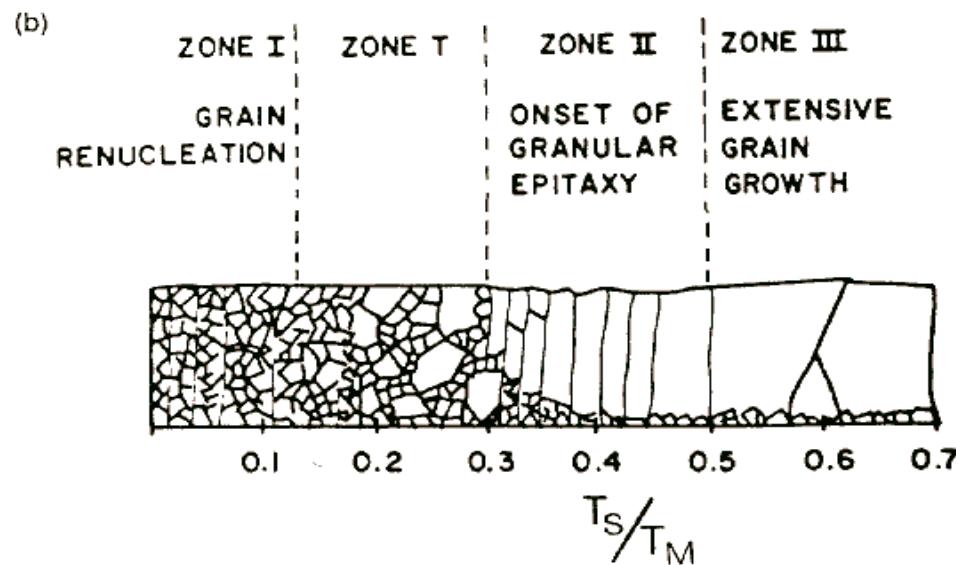
E-beam approach chosen for compositional control



- Triad electron gun for E-beam evaporation
- Co-deposition of ternary alloy thin films
- Shutter in front of substrate for consistent composition
- Substrate rotation for improved uniformity
- Line of sight shields on QCMs eliminate cross-talk

Film Morphology ZT

Transitional Zone



Nucleation and subsequent recombination lead to the final film microstructure.

Morphology is influenced by: Substrate temperature, deposition rate, bulk and surface diffusion

Zone I : All grain boundaries are immobile

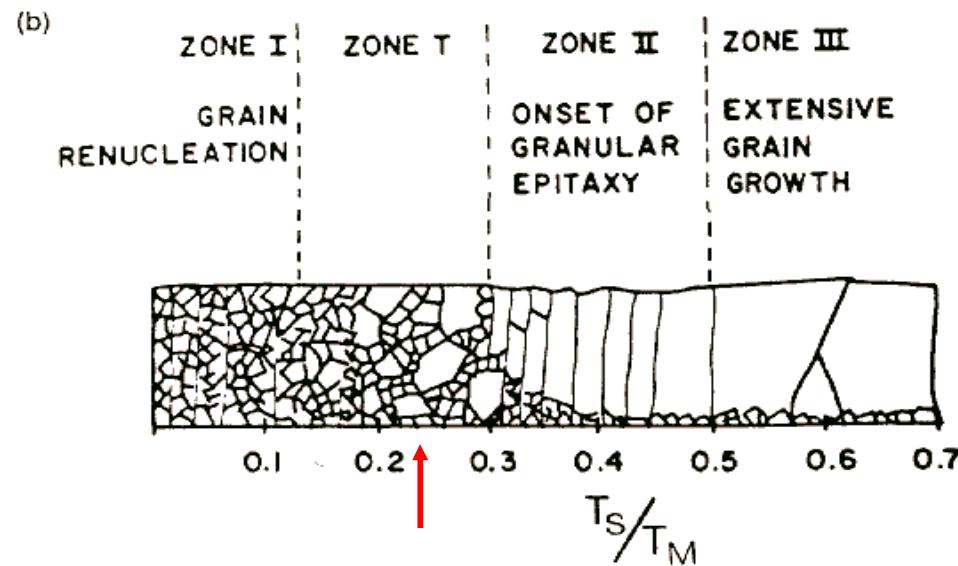
Zone T: small diameter columns with poor crystallinity. High dislocation density

Zone II: Surface diffusion is becoming dominant. Grain boundaries are mobile. Growth of columns with tight grain boundaries. Voids are filled by surface diffusion. Fewer defects.

Zone Model for Evaporated Films



Substrate Temperature



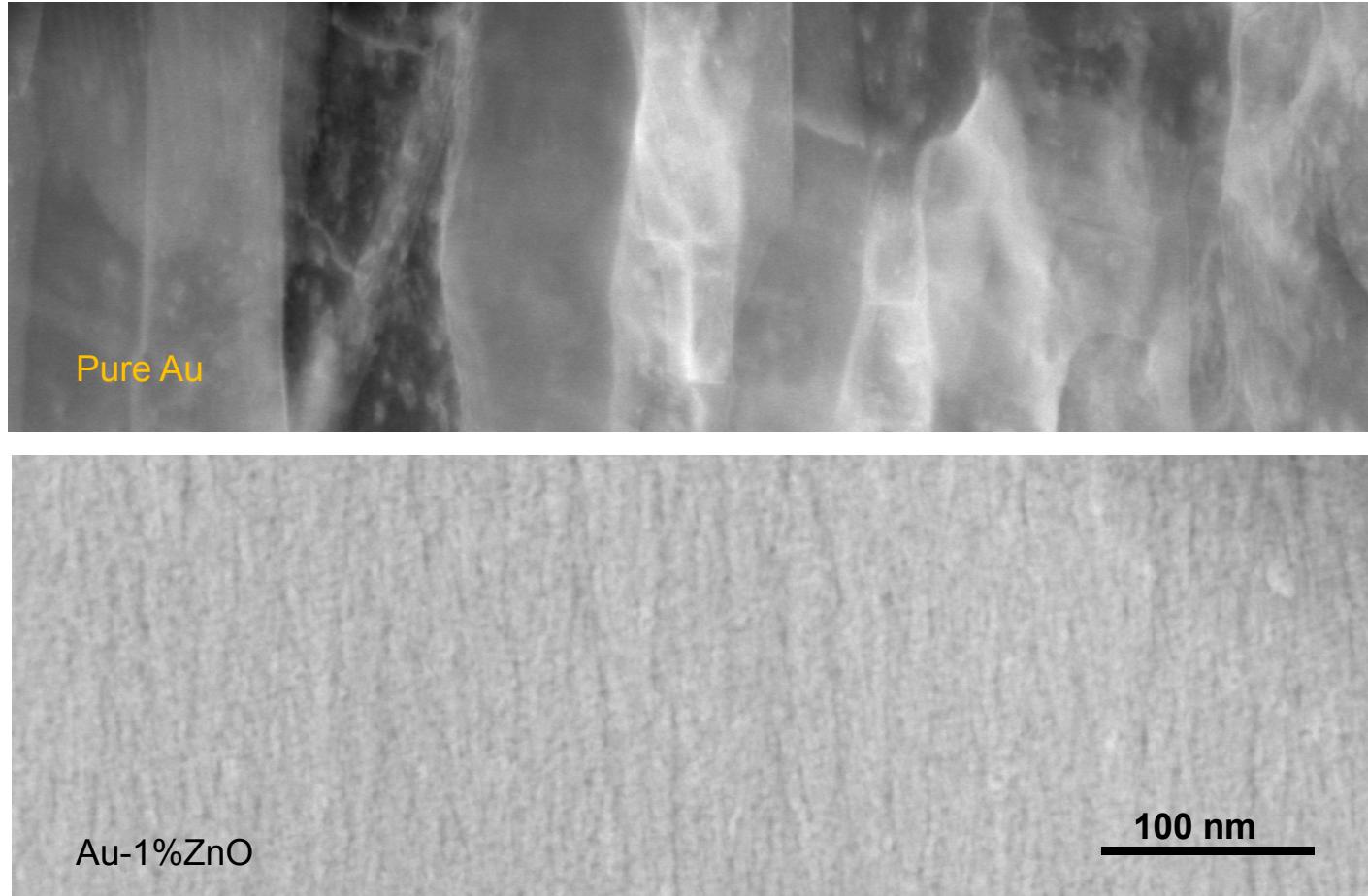
Fraction of T_m	Au Temp (°C)	Au Temp (K)	ZnO Temp (°C)	ZnO Temp (K)
T_m	1064	1337	2248	2521
$0.5 T_m$	396	669	988	1261
$0.4 T_m$	262	535	735	1008
$0.3 T_m$	128	401	483	756
$0.22 T_m$	25	298	281	554

Thin Film Characterization

- Electron backscatter detection (EBSD) in SEM
- X-Ray Florescence XRF & Electron Microprobe
- Aberration corrected scanning transmission electron microscopy (AC-STEM)
- TEM EDS Spectral imaging
- ECR-Tribology
 - Friction and wear analysis
- Nano-indentation
- 4-Point probe
- Differential Scanning Calorimetry DSC

Cross-Sectional TEM

(TEM Specimens prepared by FIB)

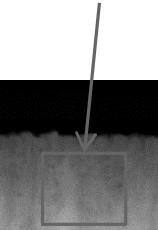


Columnar grain structure is clearly observed with a significant reduction in grain size in the columnar grain diameter in Au-(1%)ZnO

Spectral Analysis

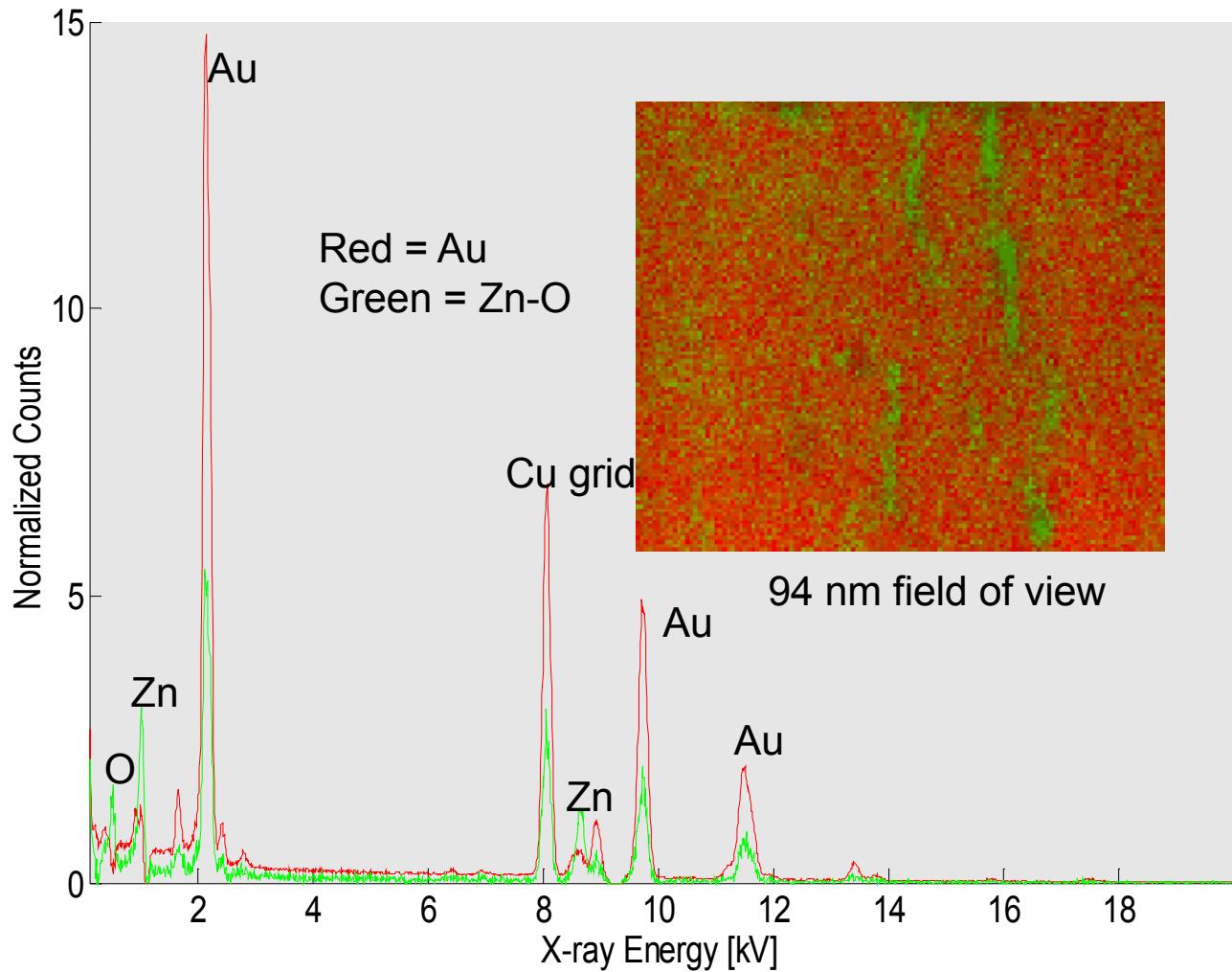
Distribution of ZnO (Green)

Region of spectral analysis



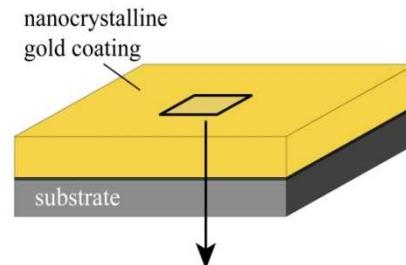
STEM cross-section of
Au-(5%)ZnO

200 nm

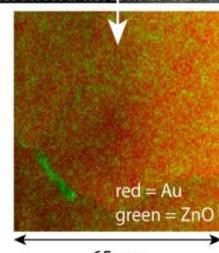
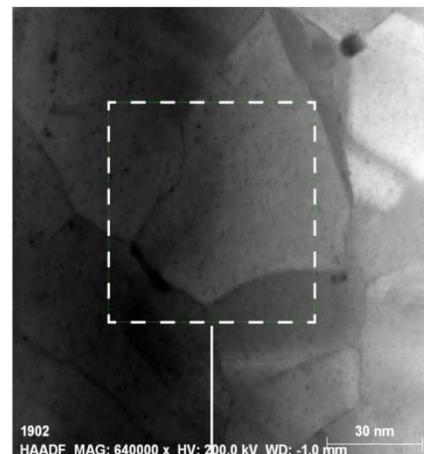


Titan STEM

Real time EDS while scanning

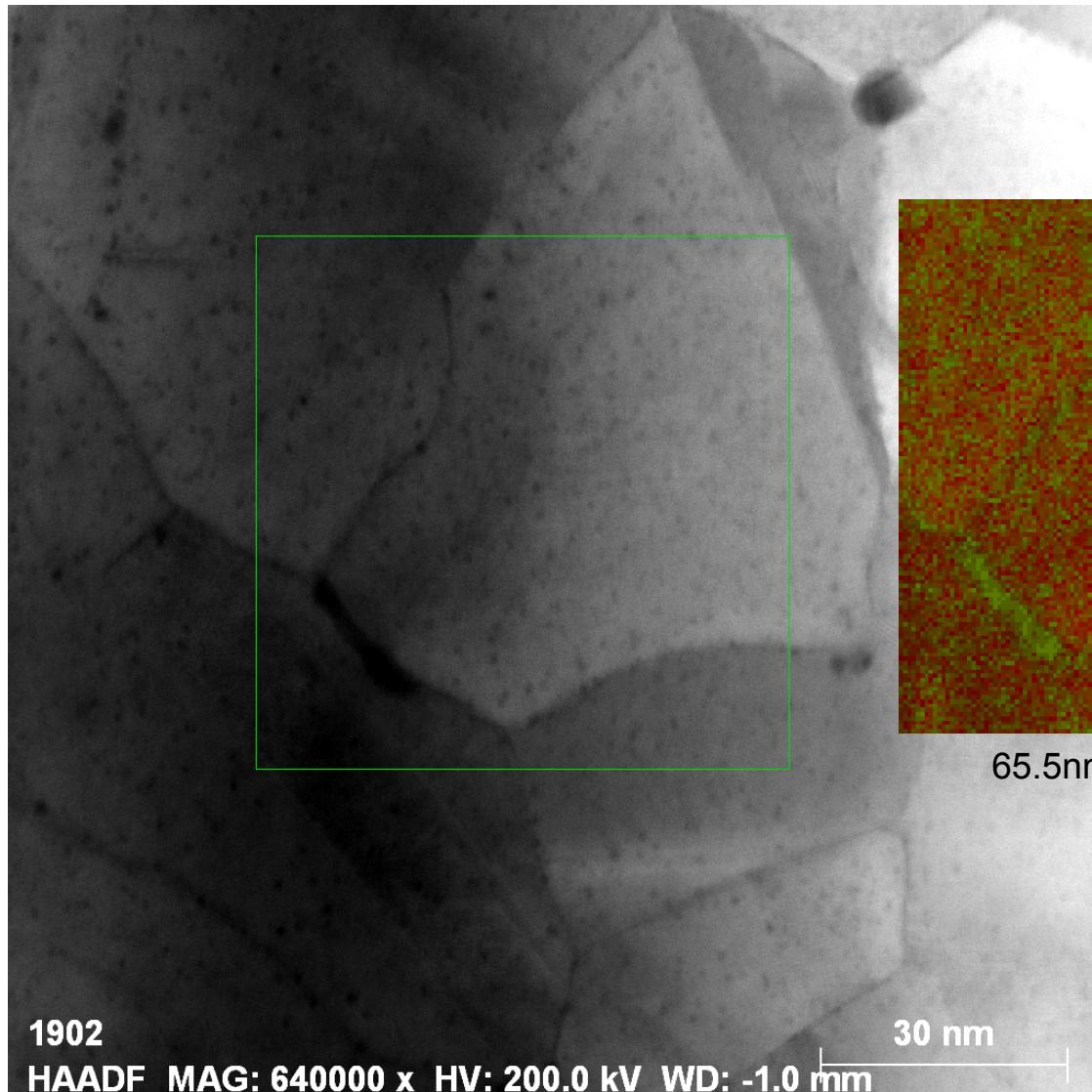


electron micrograph showing
grain boundary segregated ZnO (98 vol. % Au)



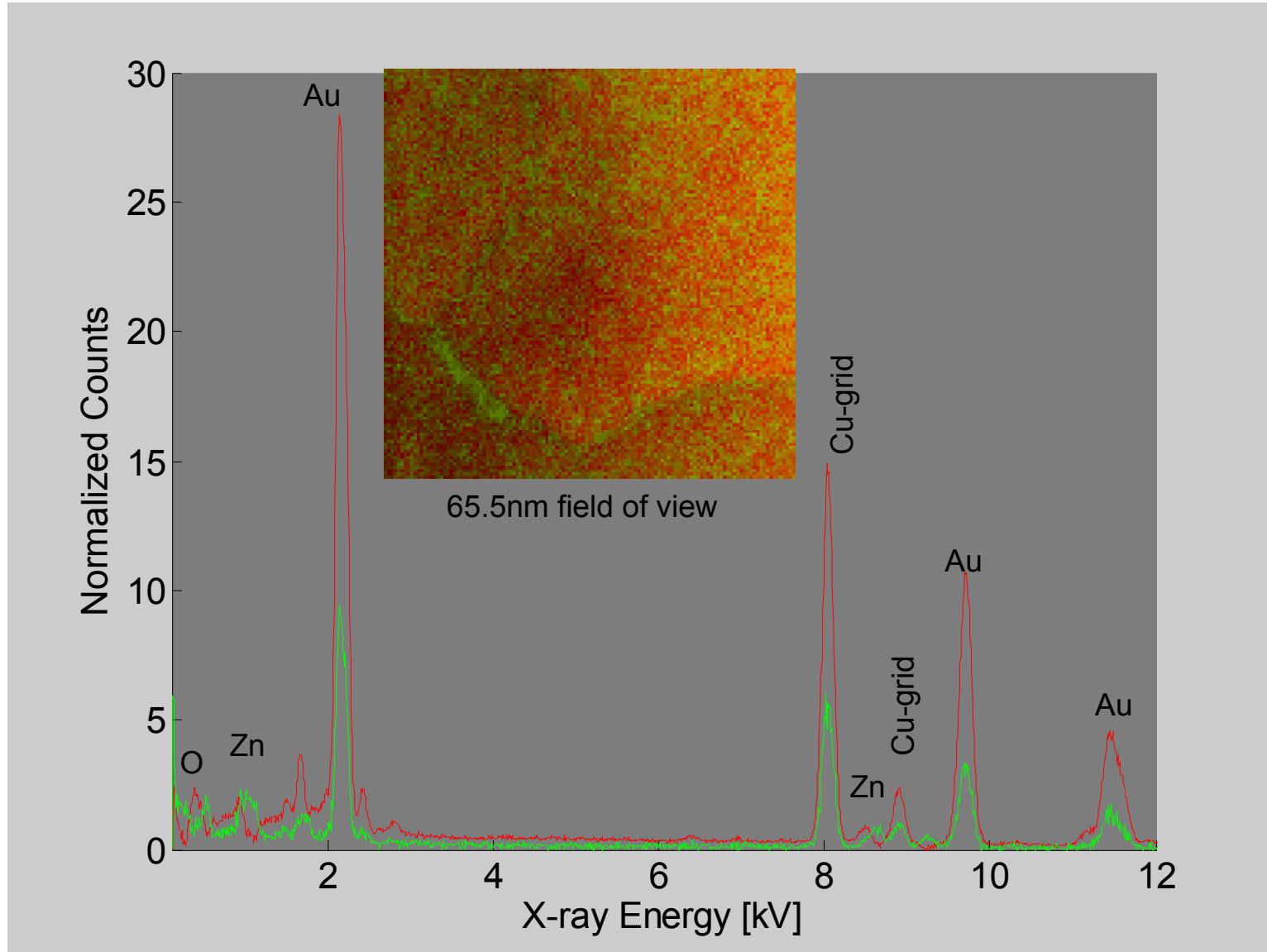
AC-TEM

Au + 2% ZnO



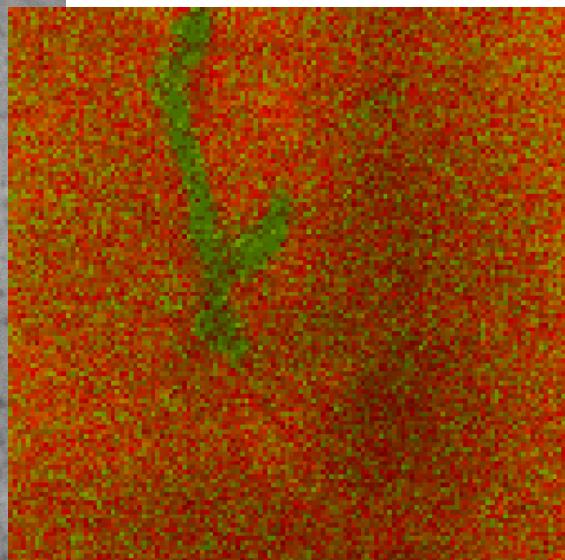
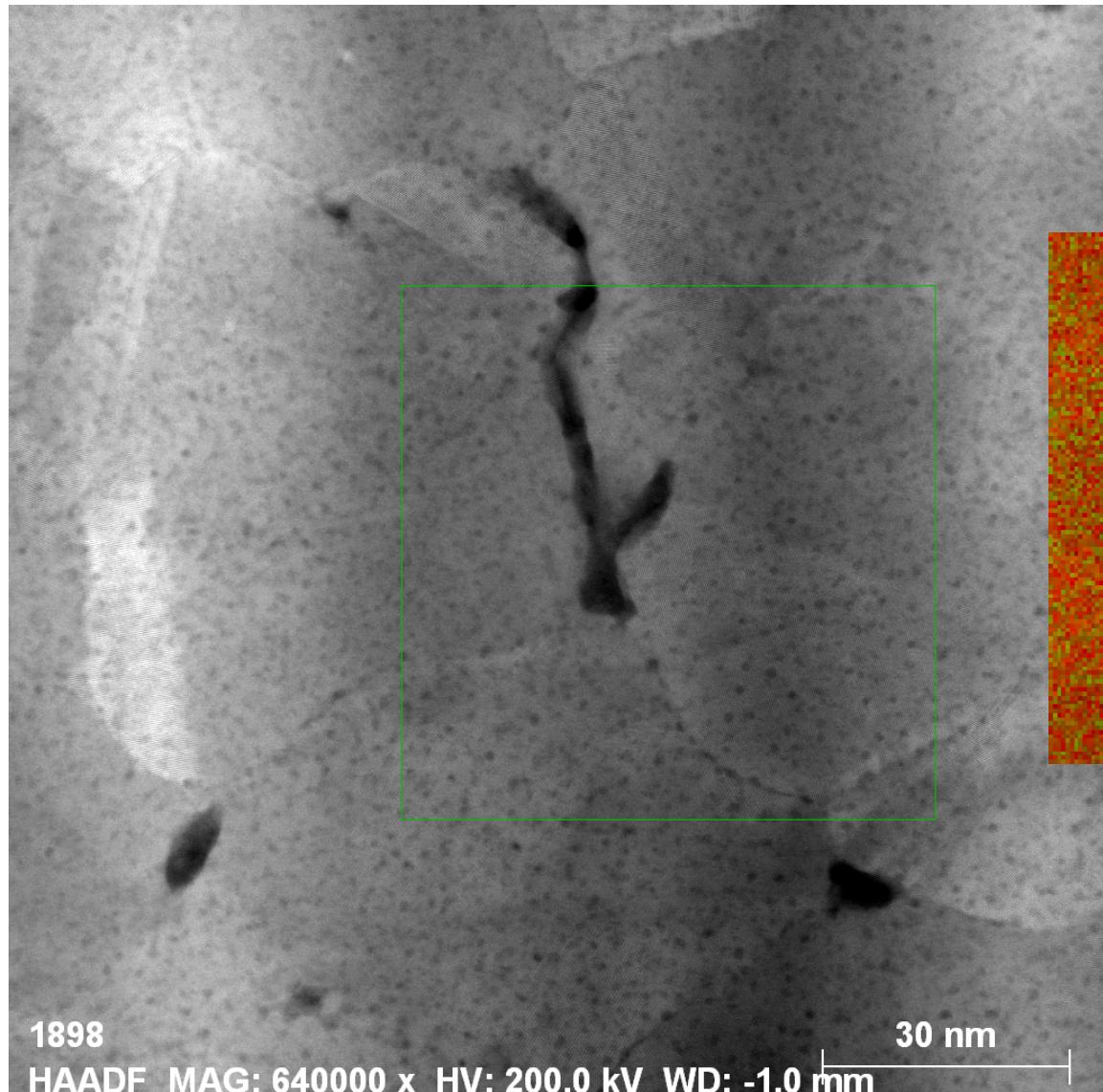
EDS Map

ZnO predominately at grain boundaries



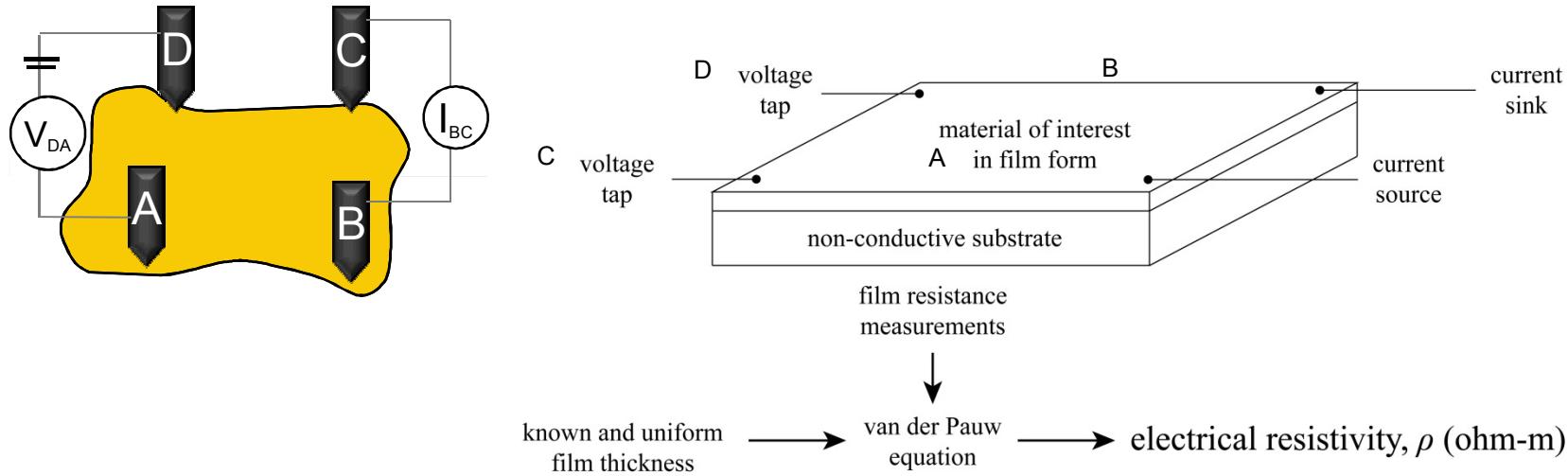
AC-TEM

Au + 10% ZnO



Measurement of Film Resistivity, R_s

Van der Pauw Method



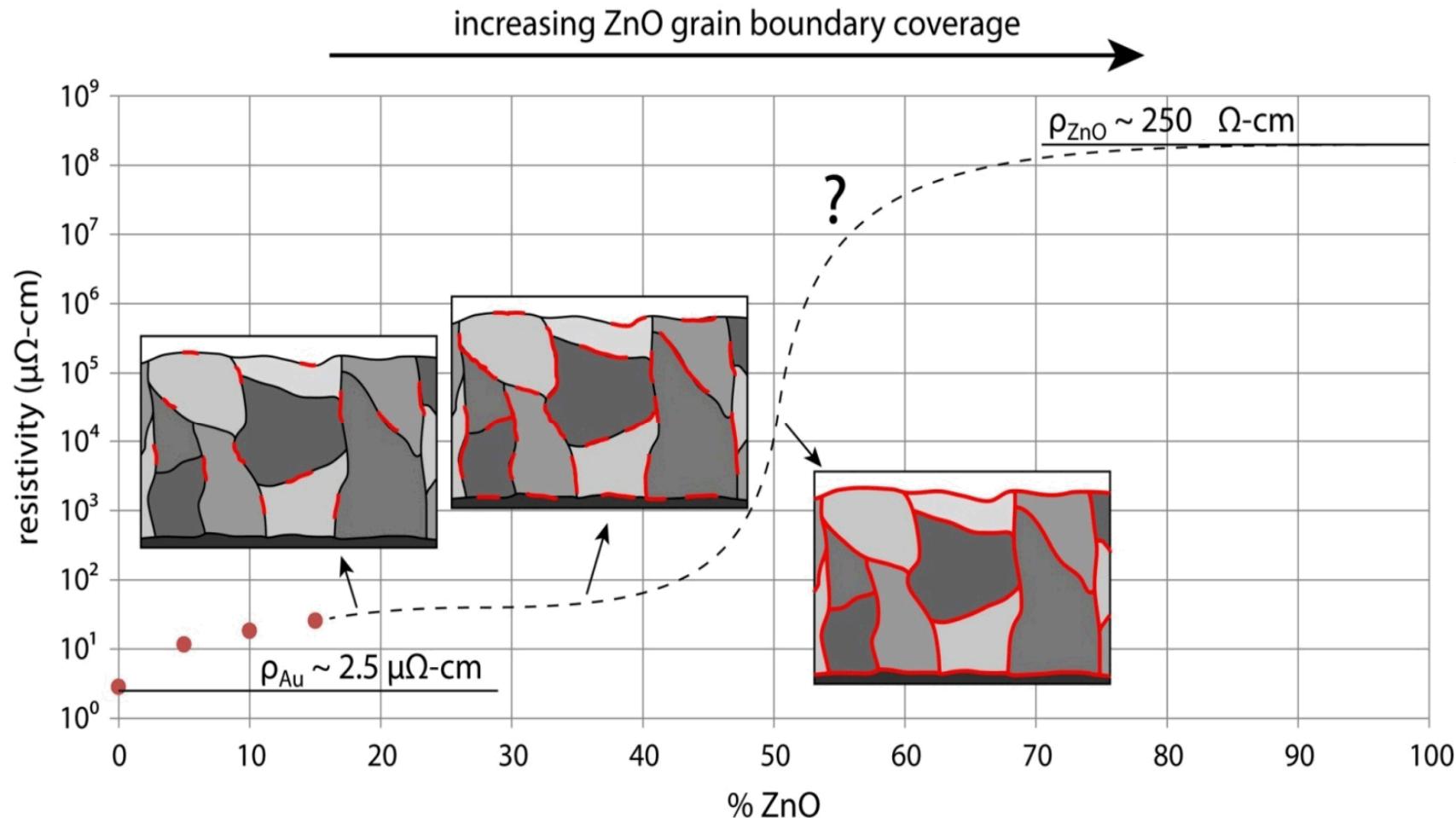
$$\exp\left(-\frac{\pi}{R_s} \cdot \frac{V_{CD}}{I_{AB}}\right) + \exp\left(-\frac{\pi}{R_s} \cdot \frac{V_{DA}}{I_{BC}}\right) = 1$$

$$\rho = R_s \cdot t$$

Bulk material resistivity is sheet resistance (calculated from measured values) times film thickness. Film thickness confirmed by TEM and QCM

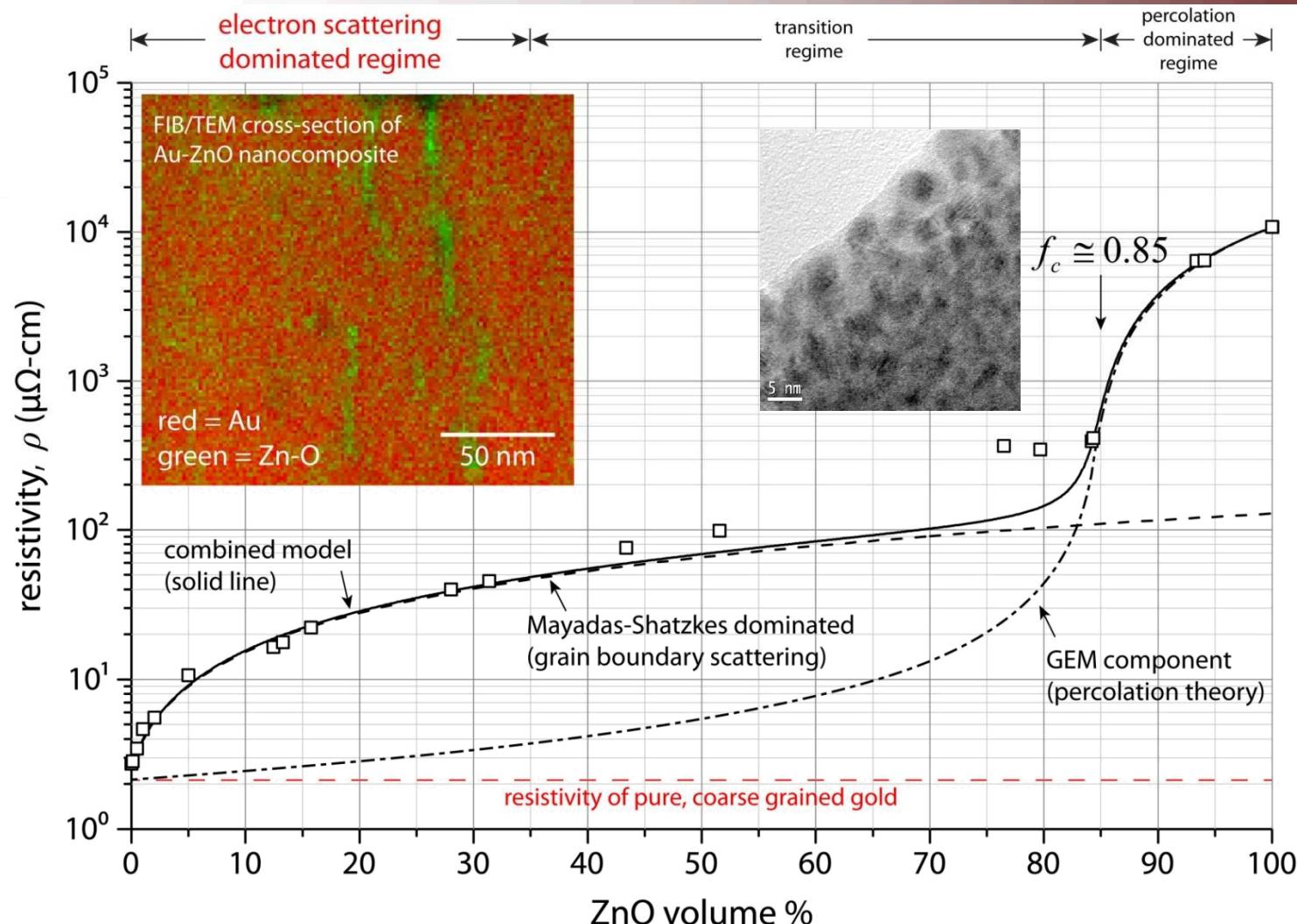
Evolution of Grain Structure

with increasing ZnO content



Electrical Resistivity Modeling

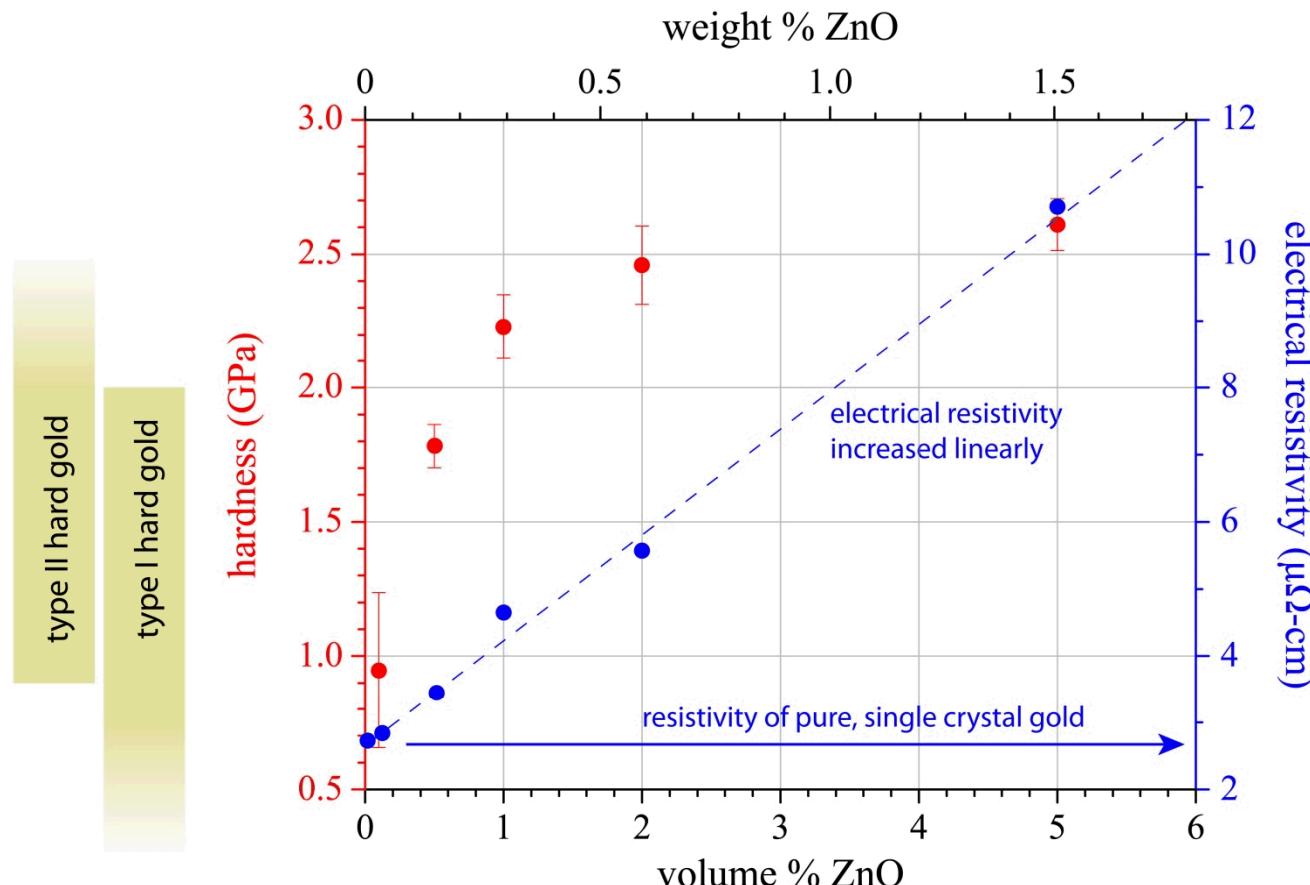
Resistivity explained by grain size



N. Argibay, R.S. Goeke, J. R. Michael, M.T. Dugger, and S.V. Prasad, "Electrical Resistivity of Au-ZnO Nanocomposite Films", *Journal of Applied Physics* 113 (2013), 143712.

Hardness and Electrical Resistivity

Comparison to hard gold specification



for reference:

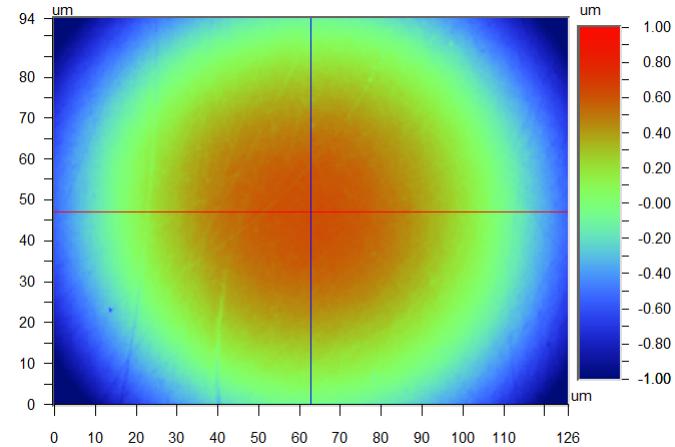
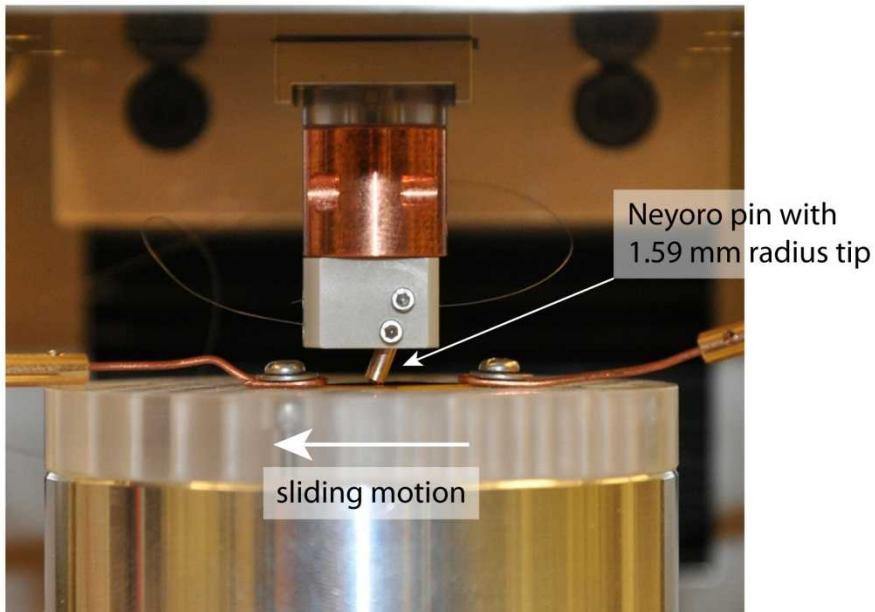
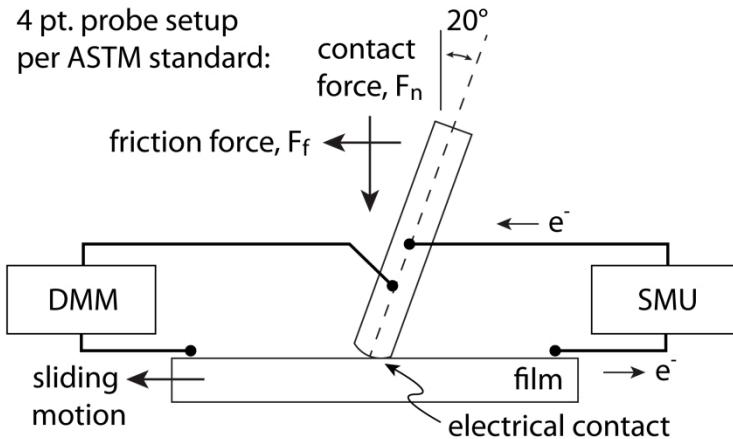
0.7 vol % Ni is \sim 0.3 wt % (type I, best ECR performance)

2.2 vol % Ni is ~ 1 wt % (type II, max allowed)

Electrical resistivity measured via van der Pauw method -- square Si wafers pieces coated with composite, no adhesion layers

Four-Point Probe ECR Setup

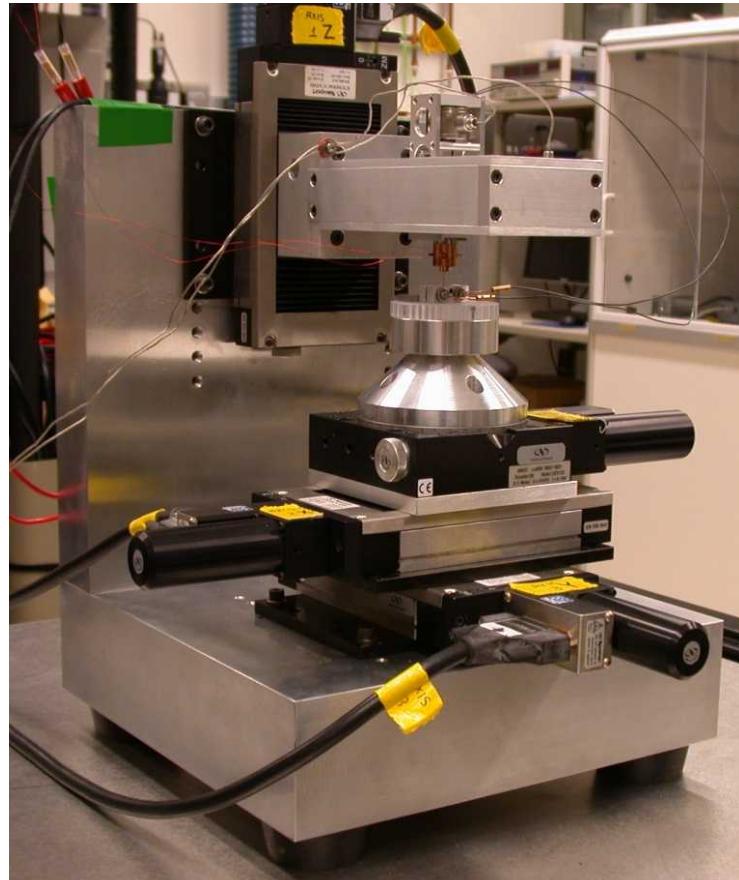
Measured with hemi-spherically tipped Au-Cu alloy rider



Hemi-Spherically tipped rider

ECR-Friction Tribometer

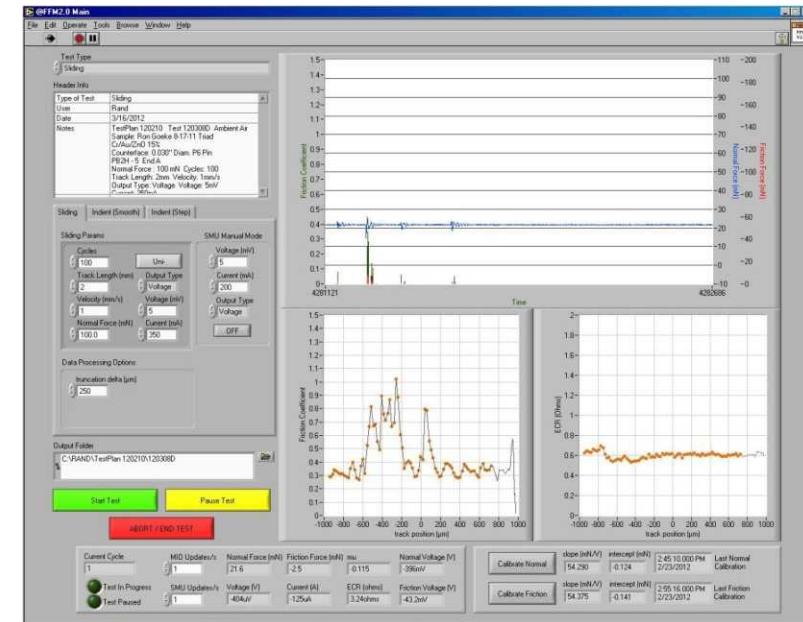
Simultaneous friction force and contact resistance



Up to 2000 mA
1 mN to 1.5 N

Test Conditions

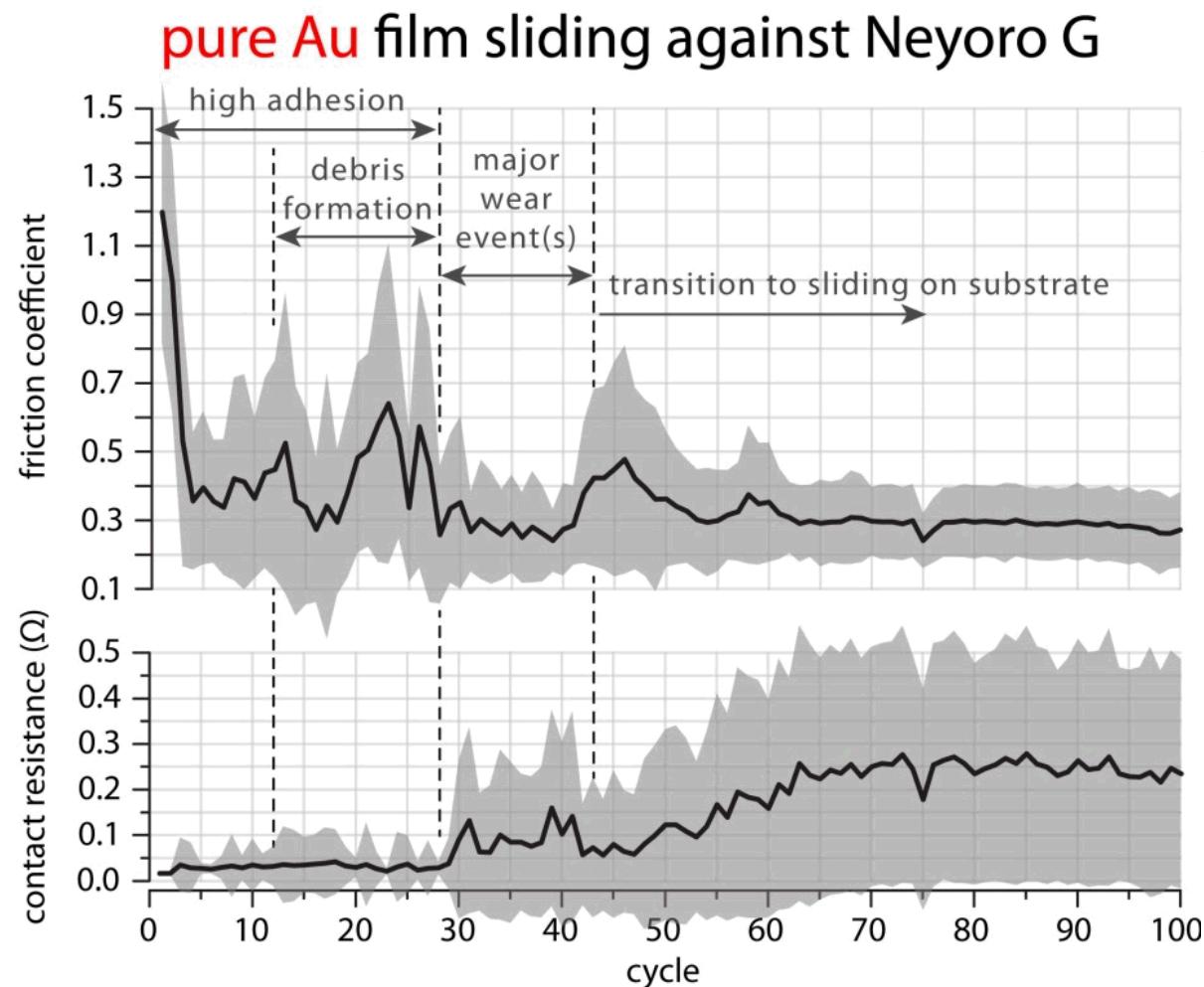
- Neyoro G (Au-Cu), $\frac{1}{16}$ in. radius hemispherical tip rider
- $F_n = 100$ mN (≈ 290 MPa contact stress)
- 100 Cycles @ $v = 1$ mm/s
- 1 – 2 mV bias to achieve approximately 100 mA
- Lab air environment at room temperature



Data Acquisition

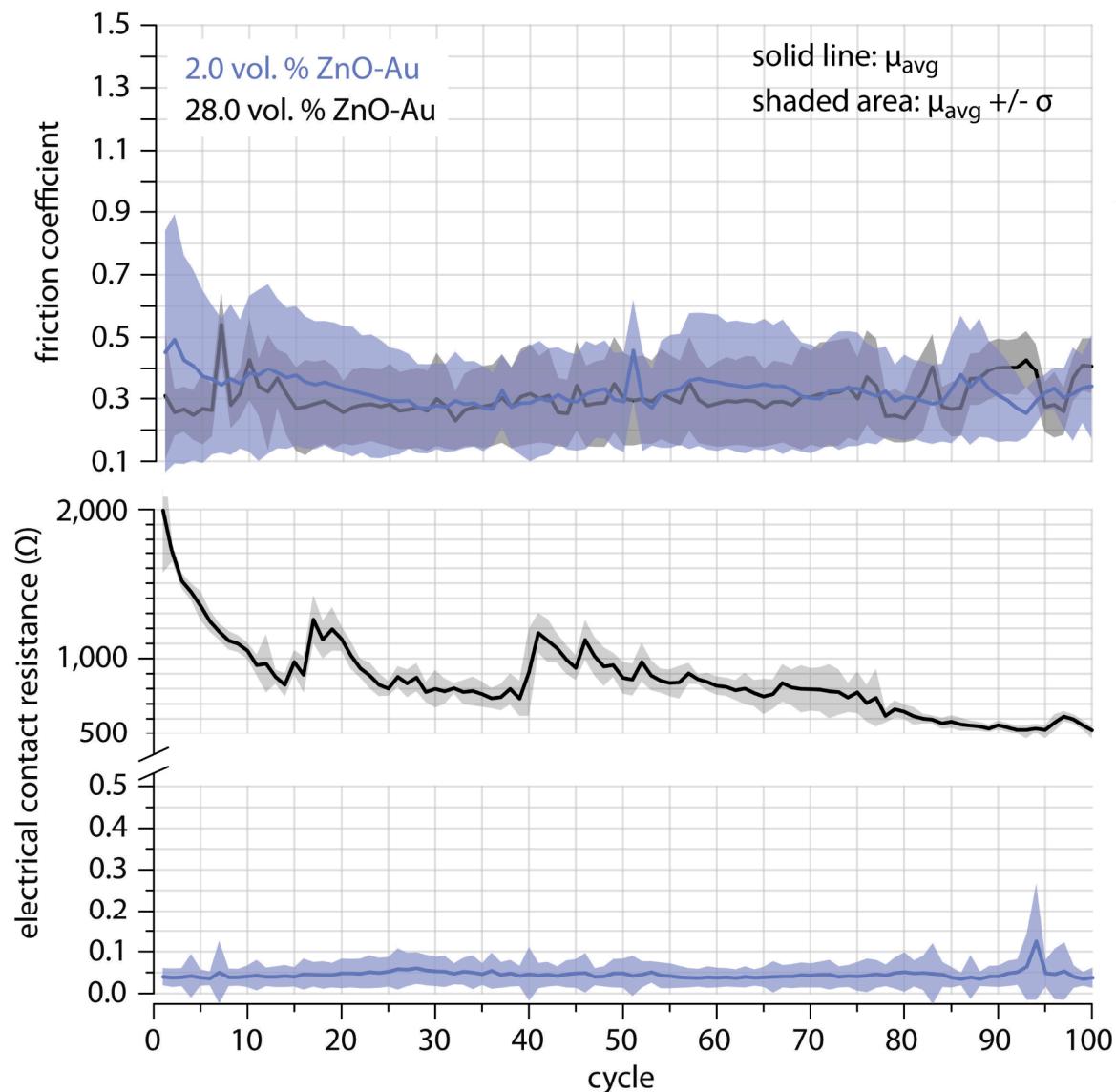
ECR-Friction Behavior

Pure Au



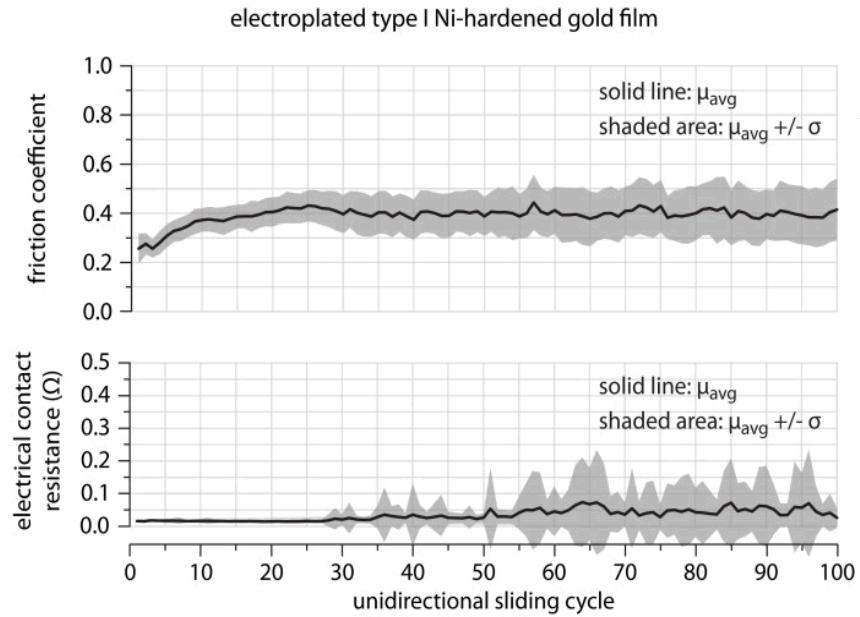
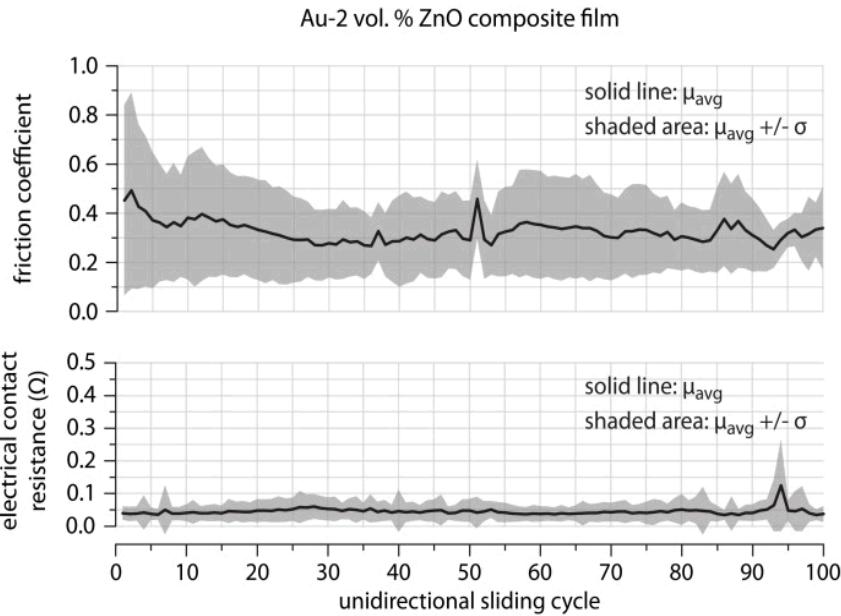
ECR-Friction Behavior

Au-ZnO



ECR-Friction Behavior

Comparison to electroplated hard gold



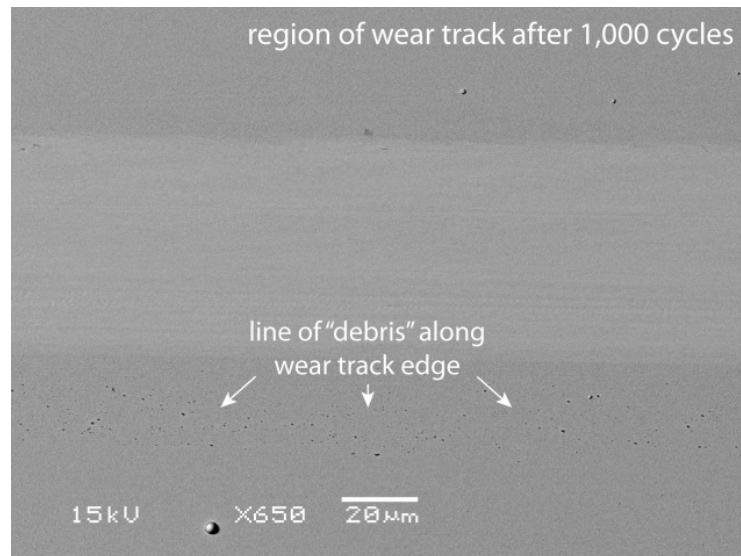
common parameters:

- sliding against a bulk hard gold alloy rider or pin (nominally 72-14-8-5-1 wt. % Au-Cu-Pt-Ag-Zn)
- rider tip radius was 3.175 mm
- contact force was 100 mN

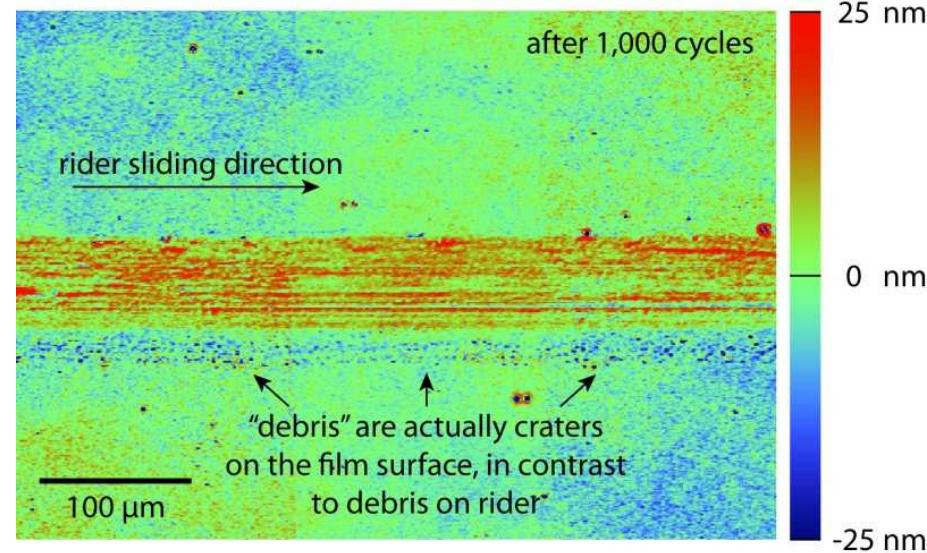
- electrical current was approx. 100 mA (voltage driven)
- sliding environment was lab air and room temperature
- substrate material was alloy 52 (nominally 50/50 wt. % Fe/Ni)
- film thicknesses 2 - 5 μm ; Ti/Pt bonding layers

Wear Surfaces

Au-2% Nanocomposite ZnO after 1000 cycles of sliding



SEM micrograph of wear scar

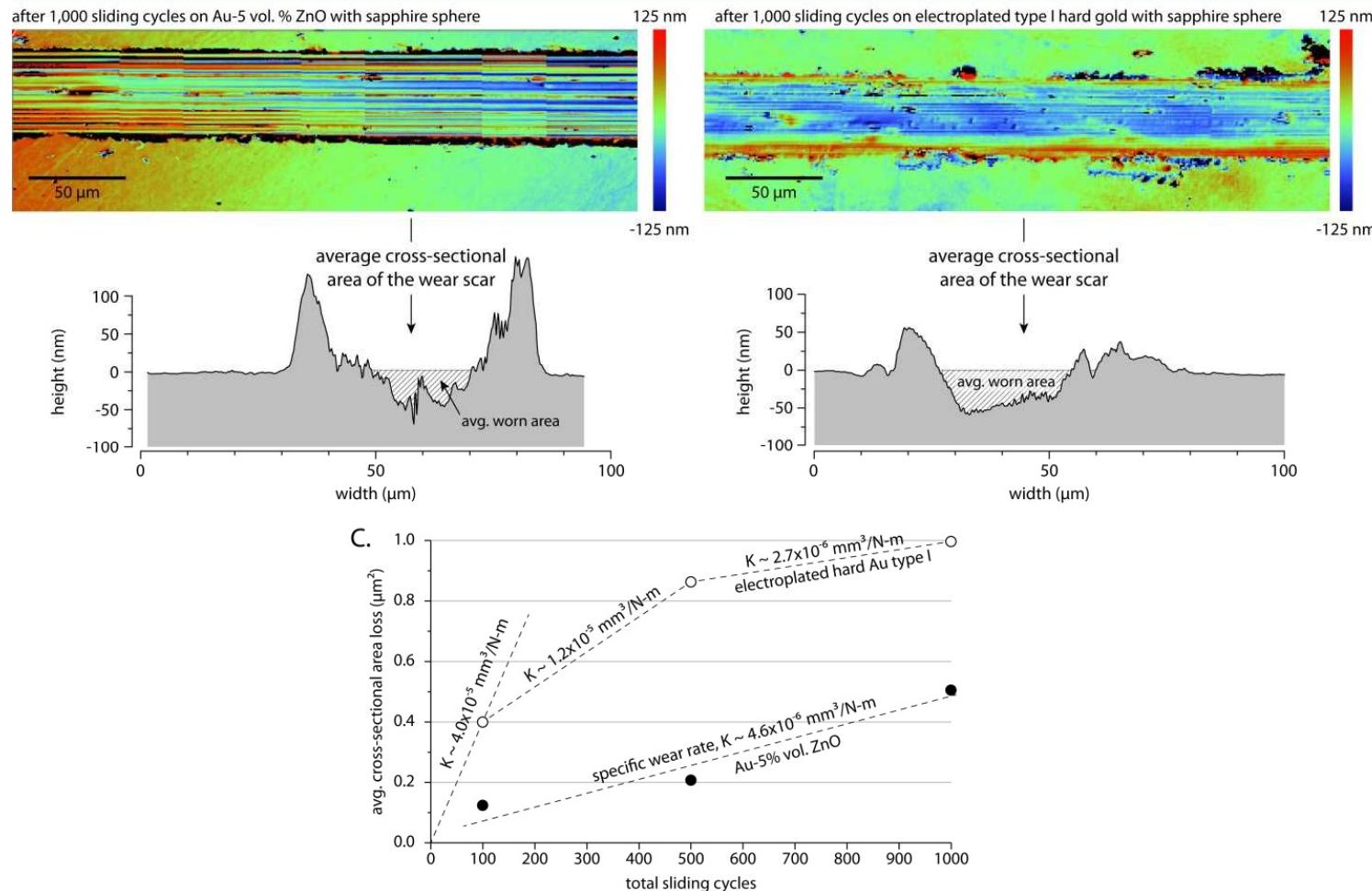


SWLI topography Map

N. Argibay, S. V. Prasad, R. S. Goeke, "Wear Resistant Electrically Conductive Au-ZnO Nanocomposite Coatings Synthesized by E-Beam Evaporation", Wear 302 (2013) 955-962.

Wear Scar

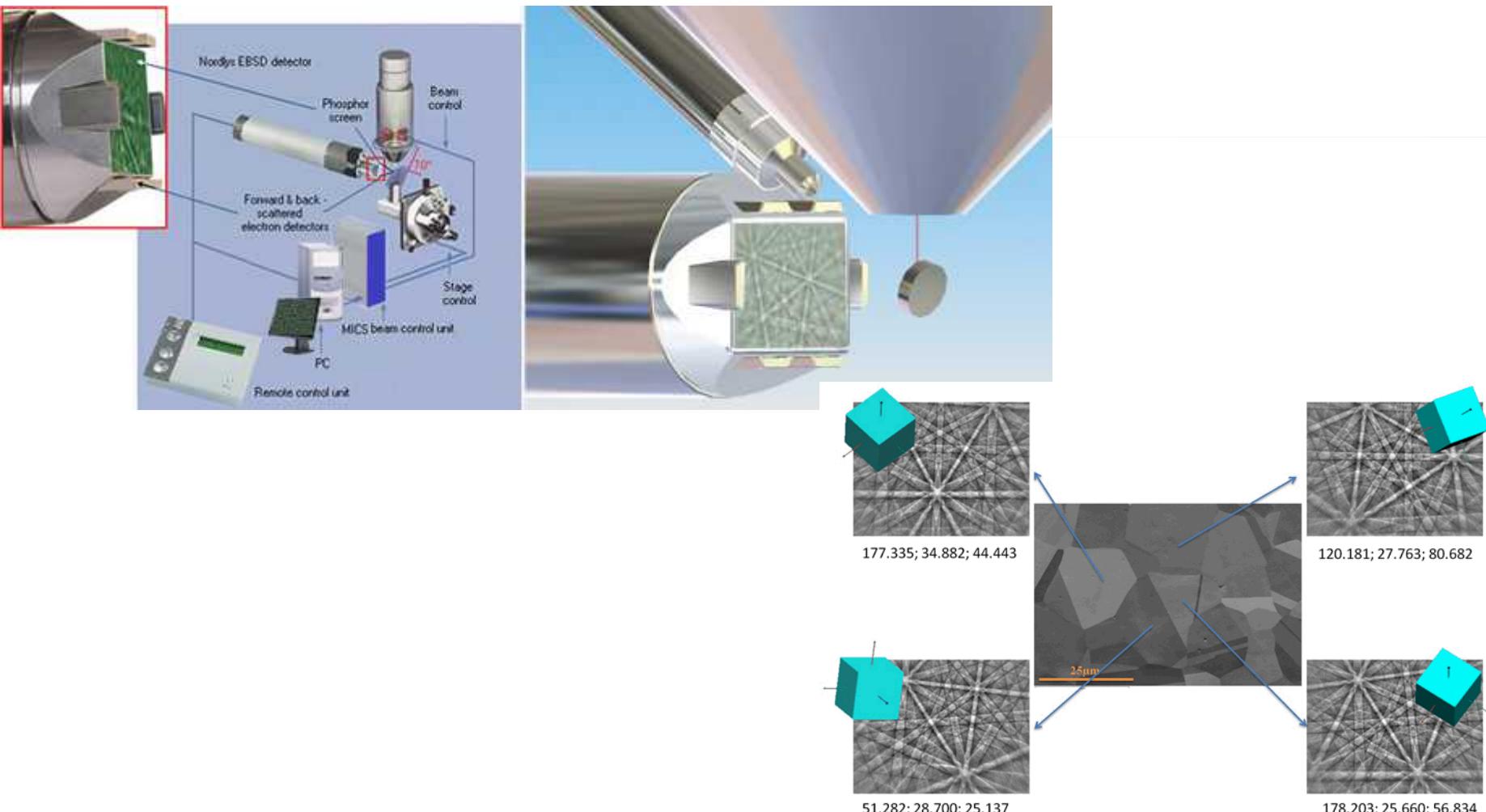
Material loss



Electron BackScatter Diffraction



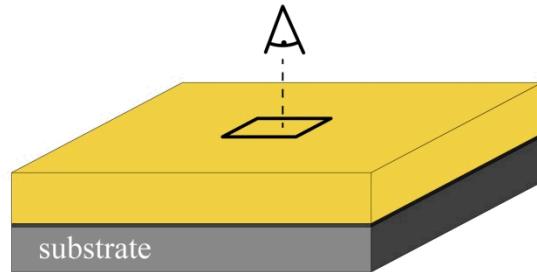
EBSD - Kikuchi patterns



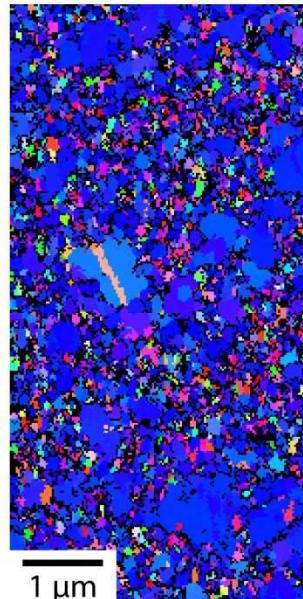


Grain size and texture impact

surface normal EBSD maps

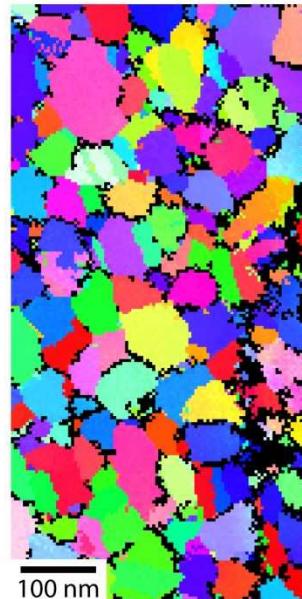


pure Au film:



large avg. grain size (> 250 nm)
preferential $<111>$ surface texture
bimodal distribution
hardness ~ 900 MPa

2.0 vol. % ZnO film

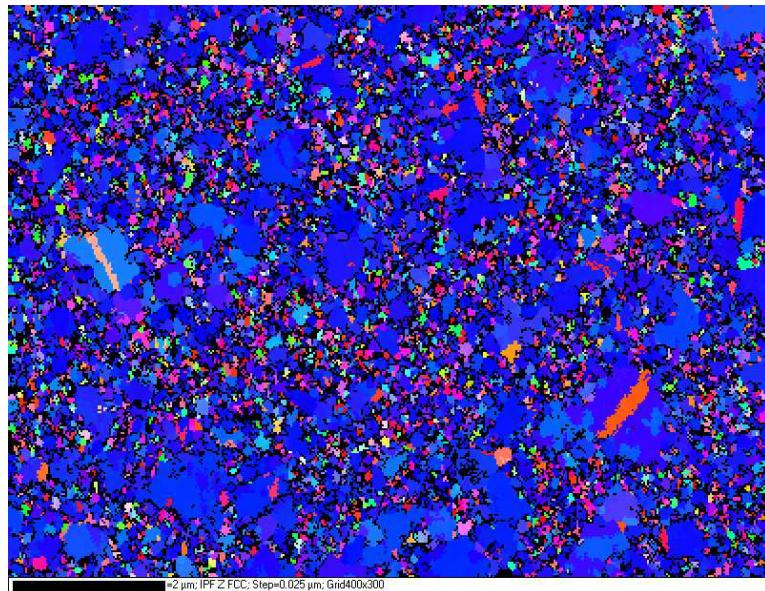


equiaxed & non-textured
avg. grain size ~ 50 nm
hardness ~ 2.5 GPa

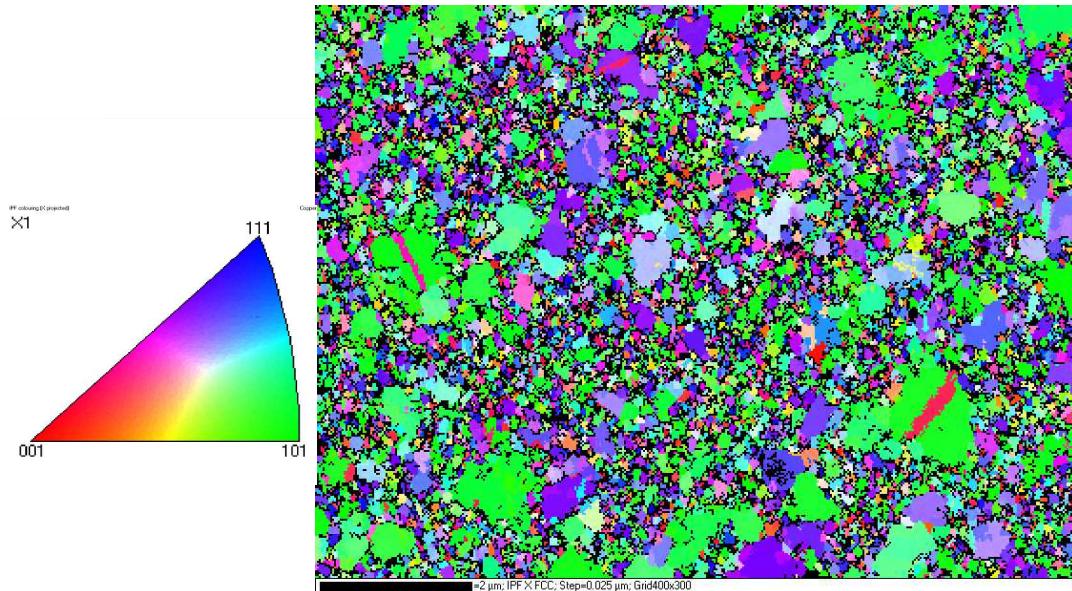
* note the difference in scale bars *

EBSD on pure e-beam deposited Au

showing (111) texture



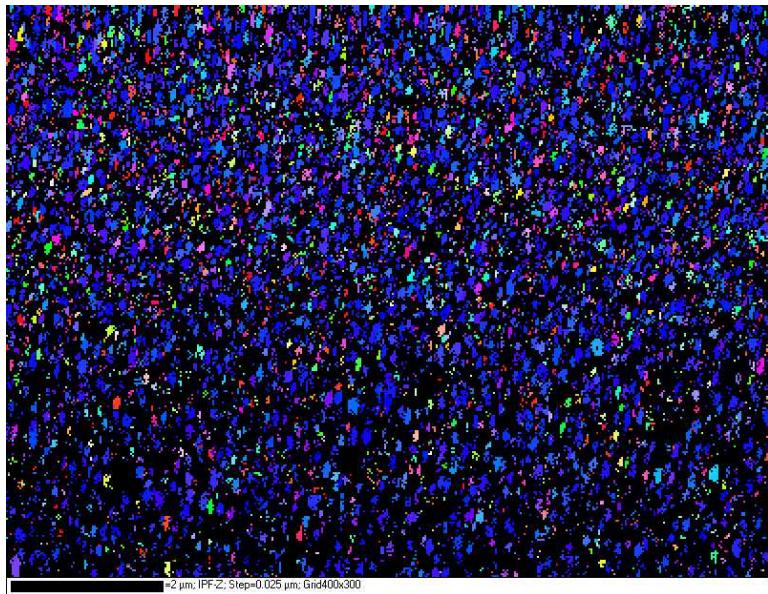
Surface normal direction



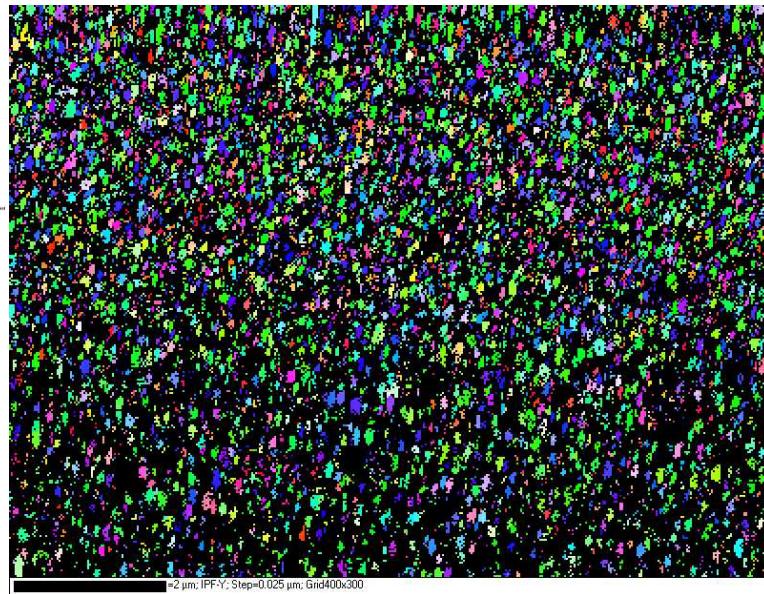
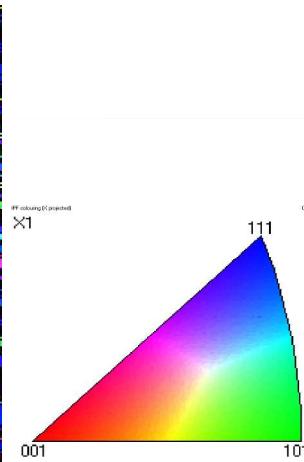
In-plane x direction (horizontal)

EBSD on e-beam deposited

Au-(1.0 vol.%)ZnO Composite



Surface normal direction



In-plane x direction (horizontal)

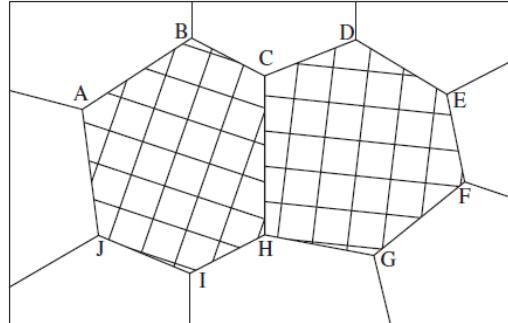
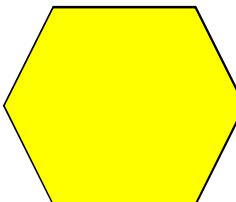
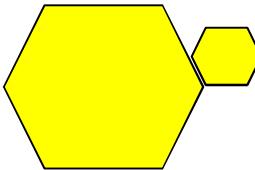
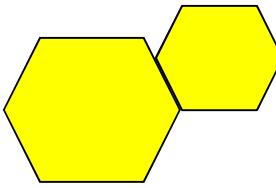
Grain size is significantly reduced but the (111) texture remains

Sintering

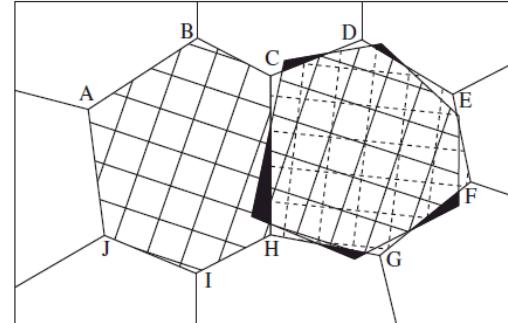
Grain Growth Mechanisms

The two common mechanisms for grain growth are:

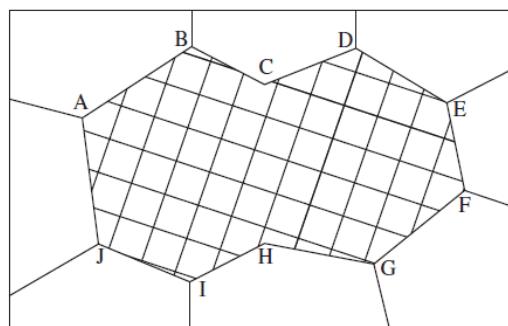
1. Ostwald Ripening – Diffusion of atoms from smaller grain to larger grain
2. Coalescence – adjacent crystallites join to become one larger grain



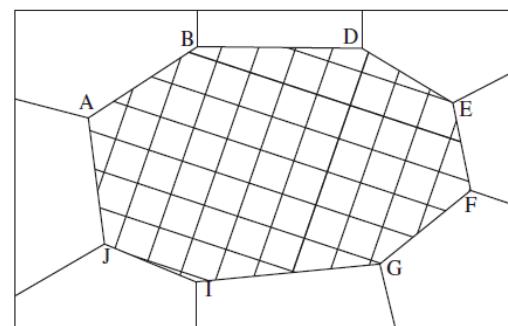
(a)
The original subgrain structure before coalescence



(b)
One subgrain is undergoing a rotation



(c)
The subgrain structure just after coalescence

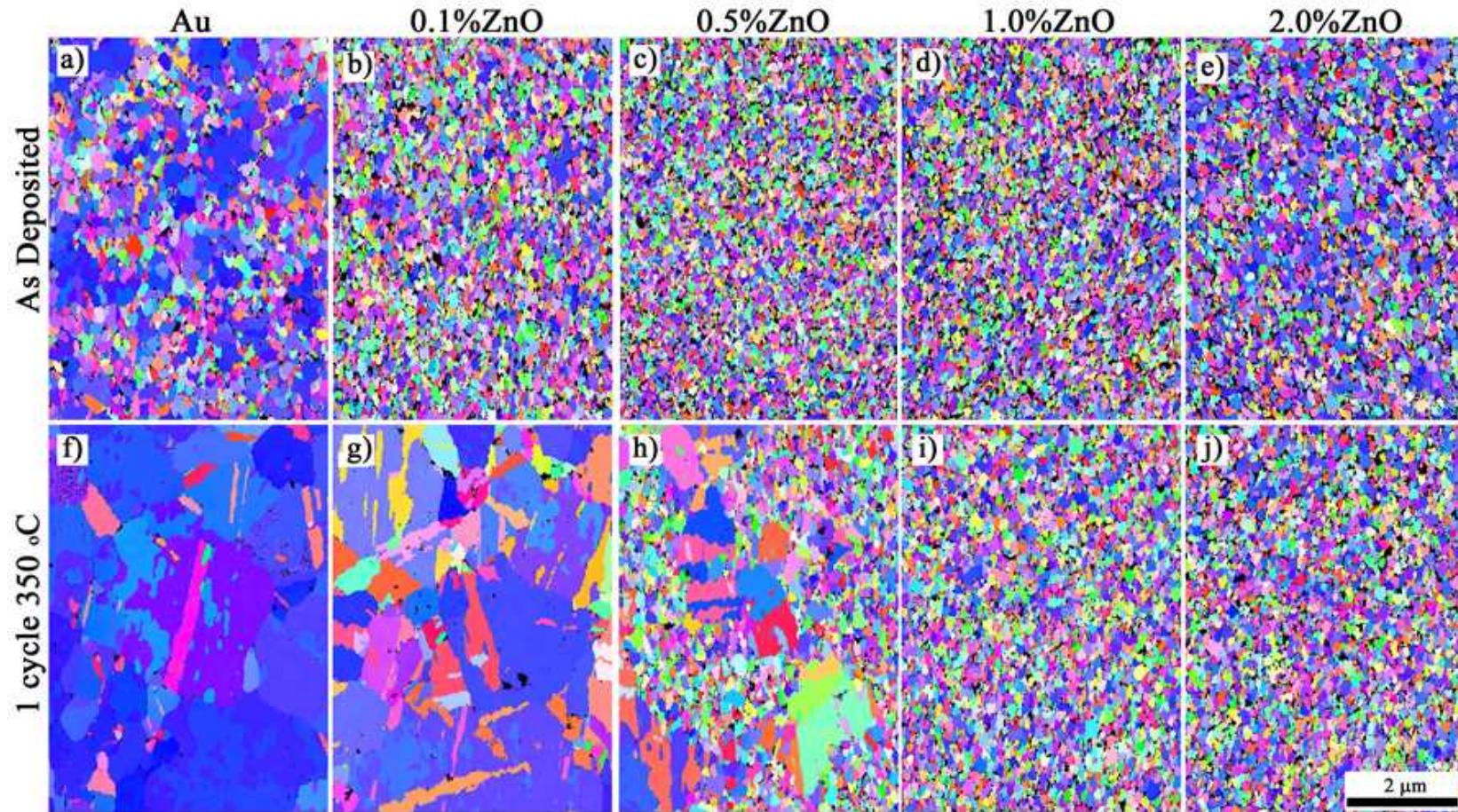


(d)
The final subgrain structure after some subboundary migration

Thermal Stability

EBSD

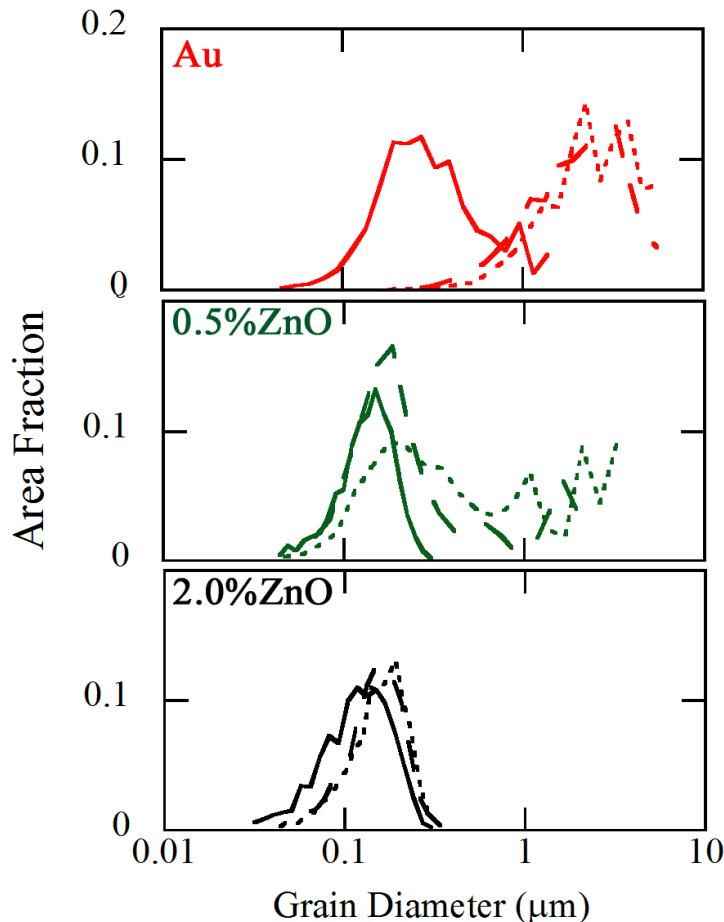
Au-ZnO thin films 2 μm thick on Pt/Ti/Si



Temperature cycled to 350°C at 10°C/min

Thermal Stability

Grain Size Distribution



Large grain growth

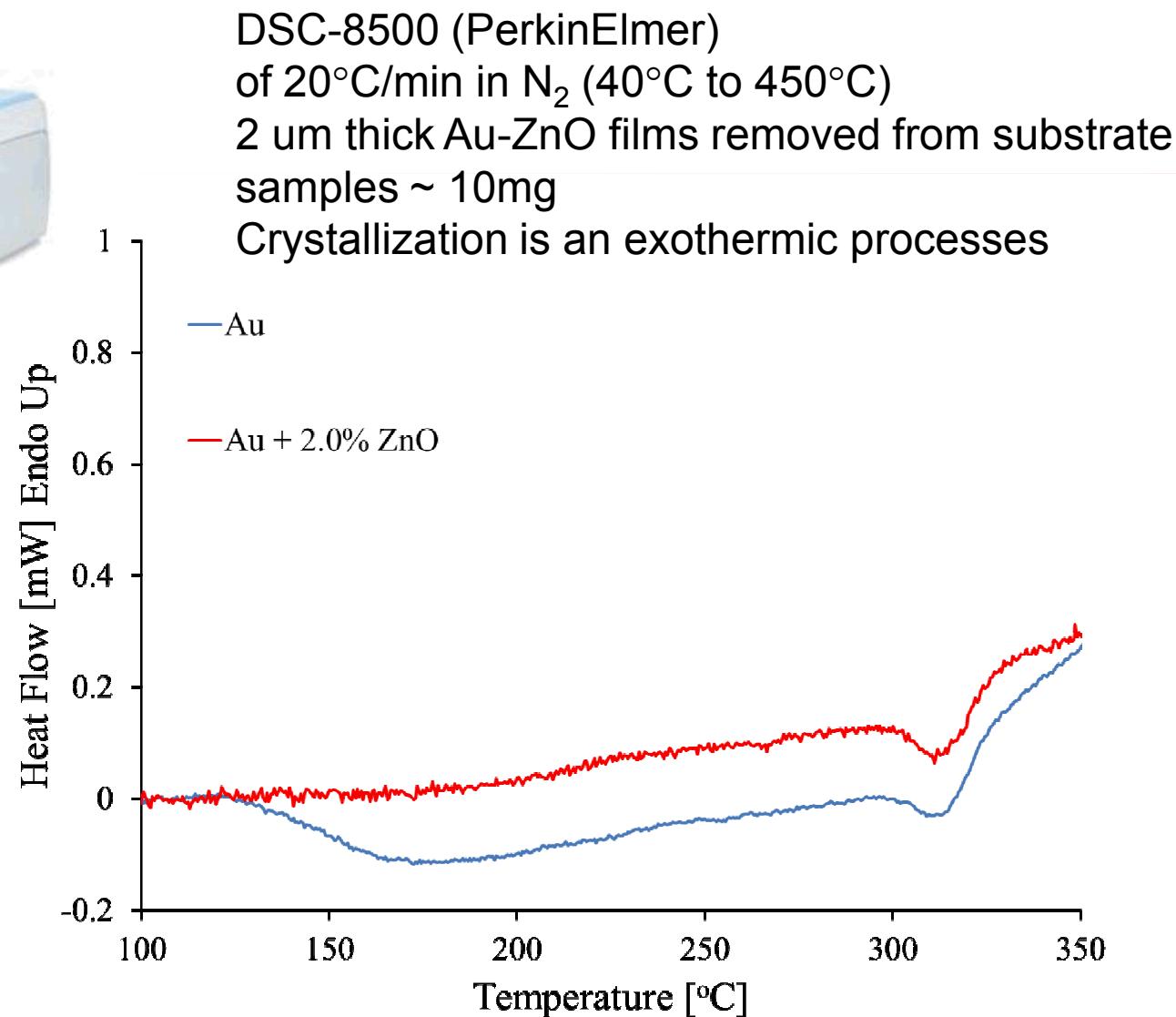
Abnormal grain growth, large grain sintering observed only in regions

Addition of ZnO impeded grain sintering

Differential Scanning Calorimeter



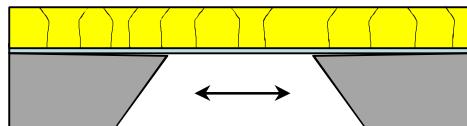
DSC



In Situ Heating

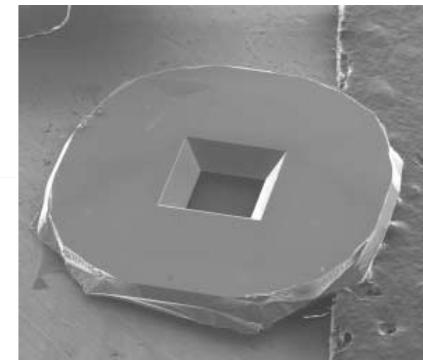
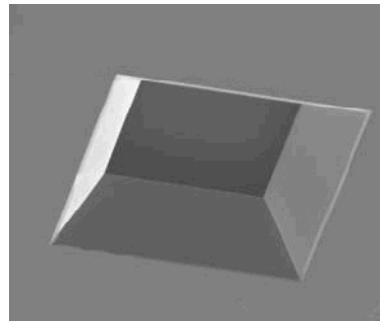
TEM Study

Au – ZnO Thin Films Deposited Directly on SPI Si_3N_4 TEM Membranes



100 nm
window

50 nm Au + ZnO
20 nm Si_3N_4
200 μm Si

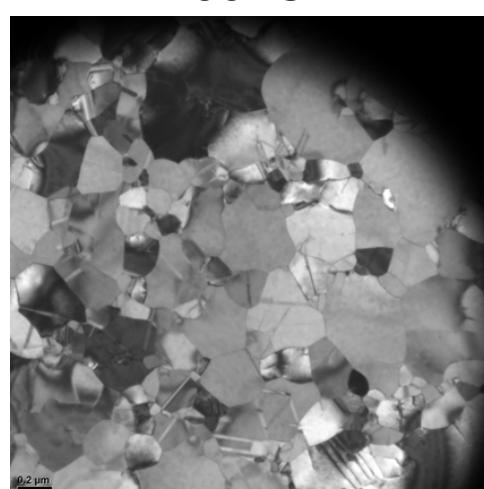
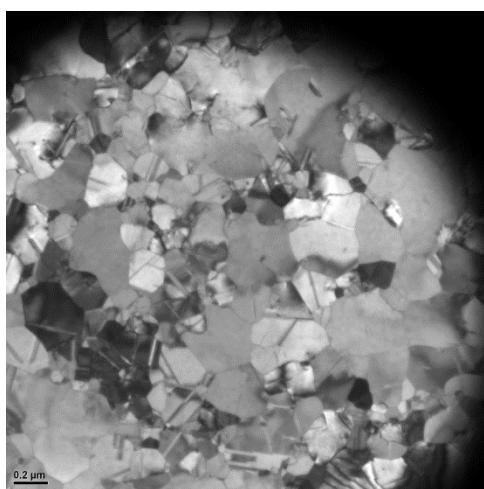
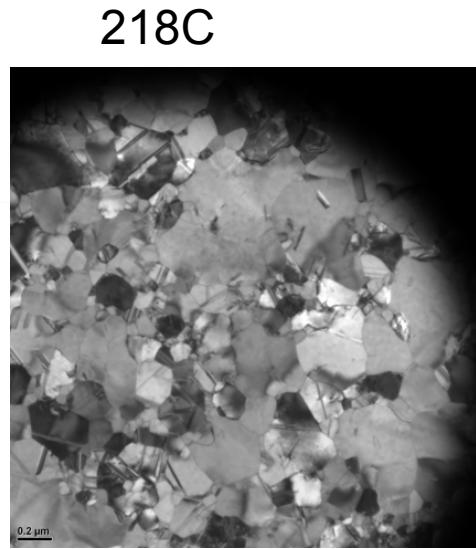
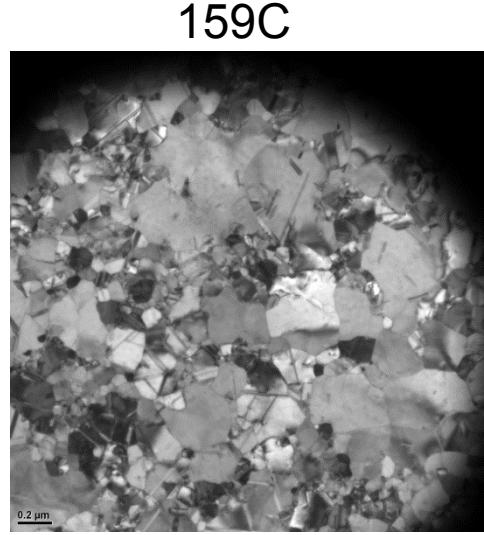
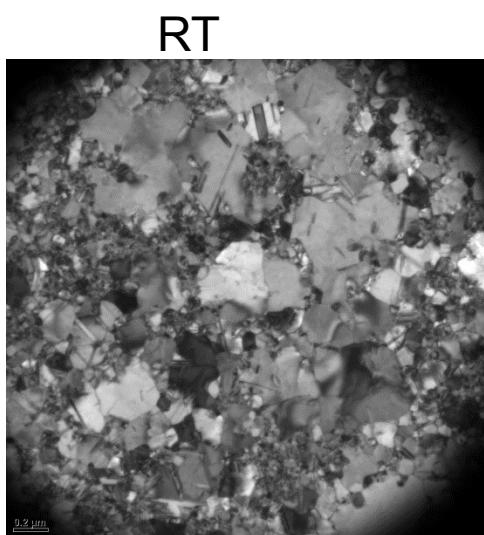


Imaged on Philips CM30
Transmission Electron
Microscope in Bright Field

Heating in 10C steps
from 150C to 350C

In Situ Heating TEM

Pure Au - 50nm thick



FOV 2.78 μm

As dep. Grain size 50 – 200nm

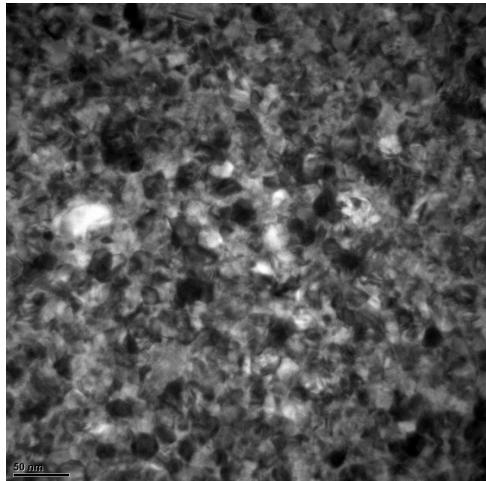
Small grains gone by 159°C

@ 352°C grain size 100 – 400nm

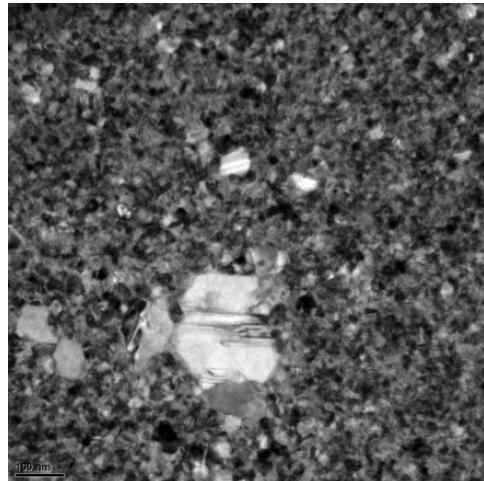
In Situ Heating TEM

Au – 2% ZnO 50nm thick

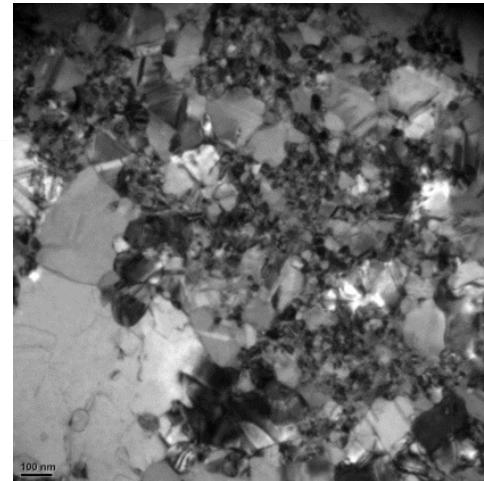
RT



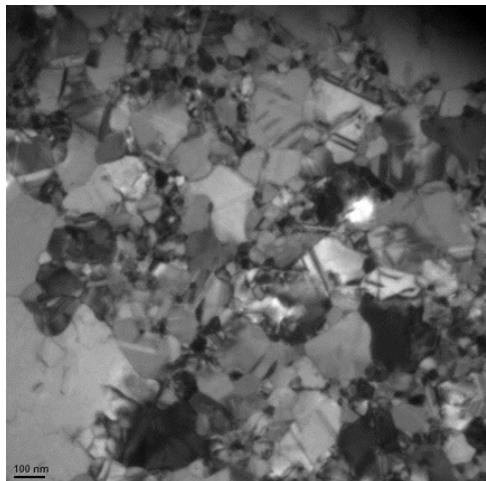
155°C



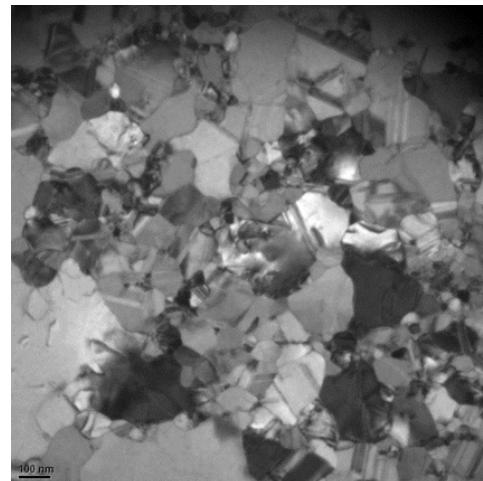
222°C



300°C



347°C



FOV 1.5 μ m (1st image 450nm)

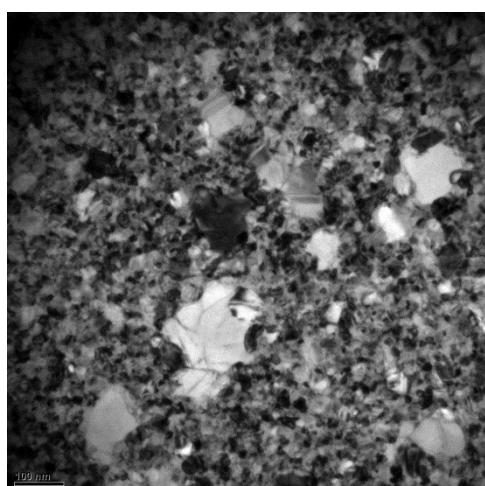
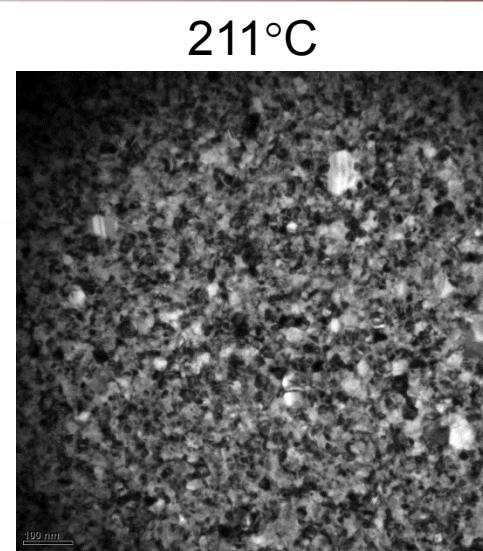
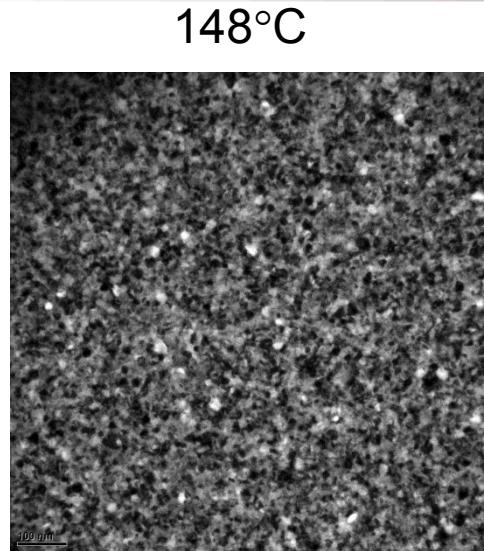
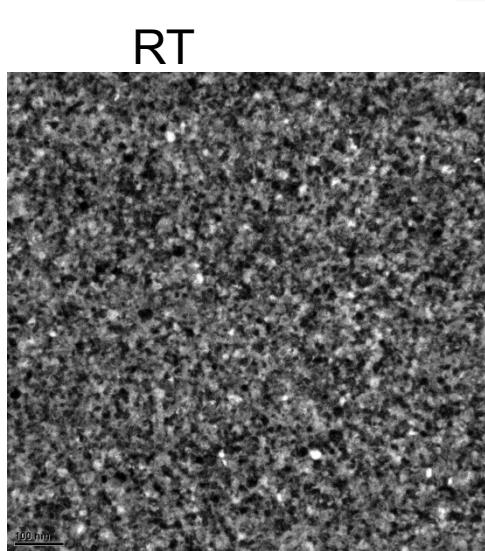
As dep. Grain size 10 – 20nm

Abnormal grain growth
starts @ 155°C

@ 347°C grain size 50 – 200nm

In Situ Heating TEM

Au 5% ZnO - 50nm thick



FOV 960nm

As dep. Grain size ~10 nm

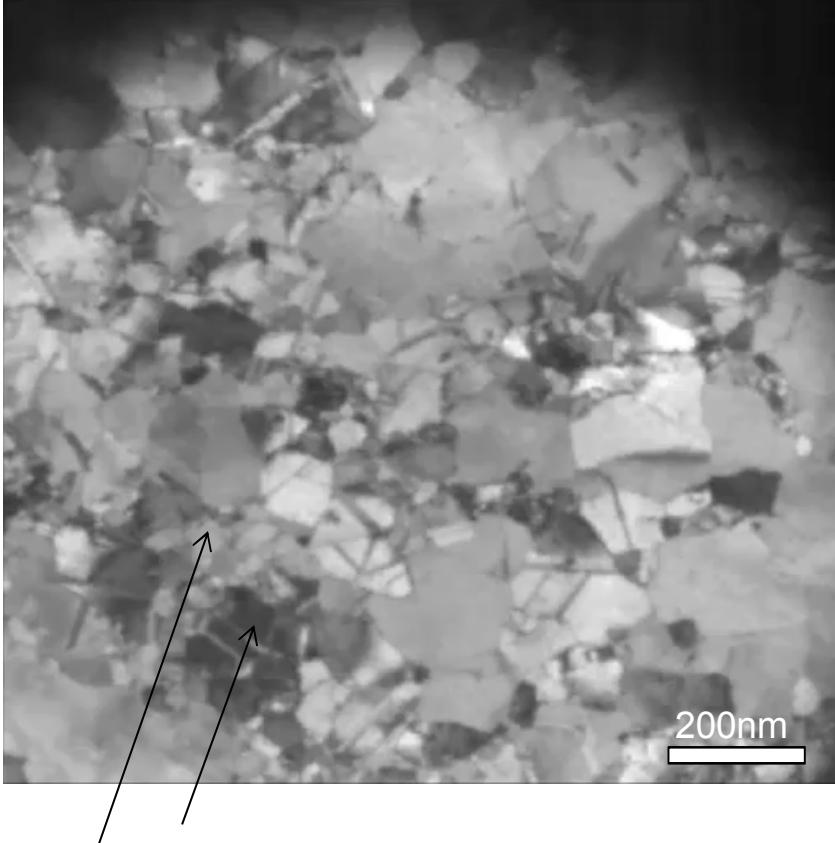
minor grain growth starts @ 211°C

@ 349°C grain size 10 & 100nm

In Situ TEM

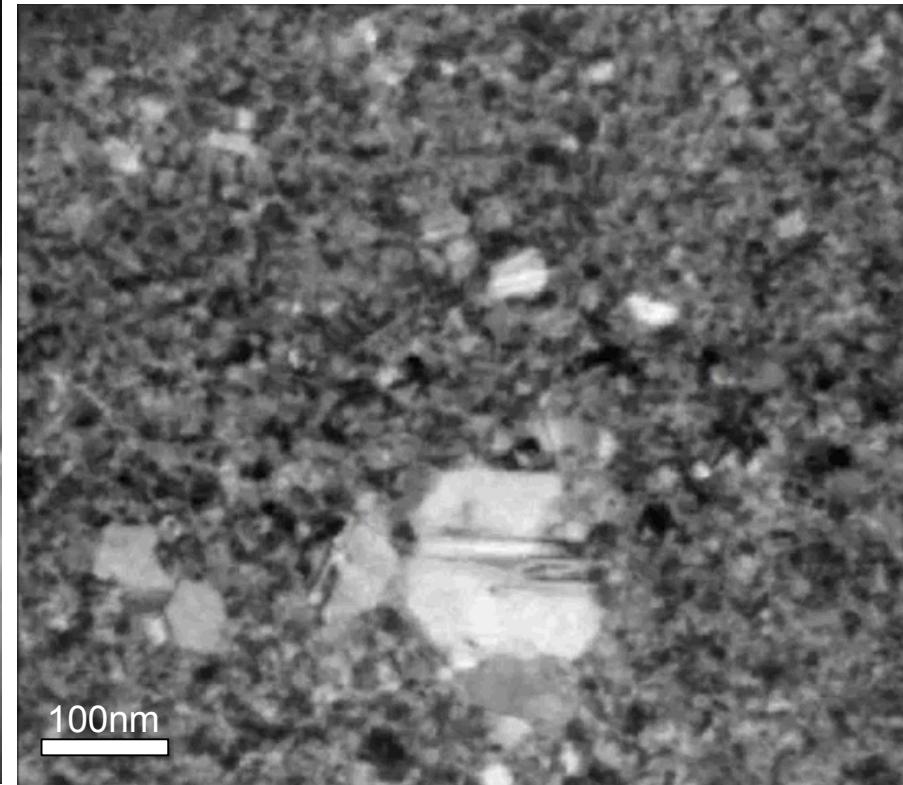
Grain Boundary Motion

Au @ 180°C (1X speed)



Watch these areas

Au – 2% ZnO @ 155°C (16X speed)



Abnormal growth is when a few grains grow much larger than the remaining majority

Conclusions

- A hard gold thin film has been synthesized by co-evaporation comprising nanocrystalline Au pinned by small amounts of ZnO
- Au-ZnO material has potential for electrical contact applications
- Thermal stability of Au-ZnO is significantly enhanced over pure gold and shows no surface layer formation which would impact electrical contact resistance
- PVD process are environmentally friendly compared with electroplating.

Acknowledgements:

Somuri Prasad for project lead and tribology testing
Jon-Eric Mogonye, Nic Argibay, Rachael Schoepner
Kahlid Hattar, Paul Kotula, Joe Michael for Microscopy

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